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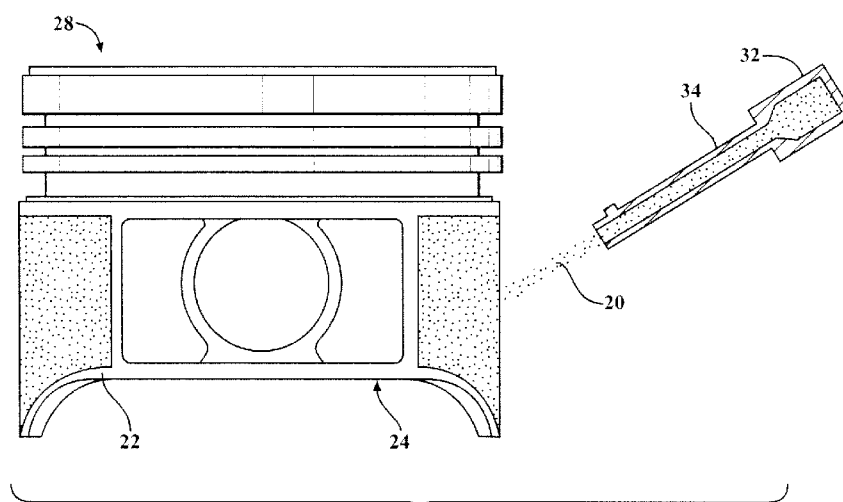


FIG. 1

(57) Abstract: A thermal spray powder 20 is provided for use in a thermal spray technique, such as flame spraying, plasma spraying, cold spraying, and high velocity oxygen fuel spraying (HVOF). The thermal spray powder 20 is formed by water or gas atomization and comprises 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the thermal spray powder 20. The thermal spray powder 20 can be applied to a metal body, such as a piston or piston ring, to form a coating. The thermal spray powder 20 can also provide a spray-formed part.



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THERMAL SPRAY APPLICATIONS USING IRON BASED ALLOY POWDER

CROSS REFERENCE TO RELATED APPLICATION

[0001] This application claims the benefit of Provisional Application Serial No. 61/608,853 filed March 9, 2012, the entire contents of which is hereby incorporated by reference in its entirety.

BACKGROUND OF THE INVENTION

1. Field of the Invention

[0002] This invention relates generally to wear resistant thermal spray powders, methods of forming the same, and applications thereof.

2. Related Art

[0003] Thermal spray techniques are used to apply wear resistant coatings to automotive engine components, such as pistons and piston rings. The coatings can protect the surface of the piston rings from wear as the piston slides along the cylinder. The coatings also reduce corrosion and oxidation of the piston caused by exposure to extreme temperatures and pollutants in the combustion chamber of the engine. Such wear resistant coatings have been formed from various ceramic materials, chromium-based powders, and molybdenum based powders. Examples of thermal spraying techniques include combustion, electrical discharge, cold spraying, and laser.

SUMMARY OF THE INVENTION

[0004] One aspect of the invention provides a powder metal material for use in a thermal spray technique, comprising: 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the powder metal composition.

[0005] Another aspect of the invention provides a method of forming a powder metal material for use in a thermal spray technique, comprising the steps of: providing a melted iron based alloy including 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the melted iron based alloy; and atomizing the melted iron based alloy to provide water atomized droplets of the iron based alloy.

[0006] Yet another aspect of the invention provides a wear resistant component, comprising: a thermal-sprayed powder metal material, wherein the thermal-sprayed powder metal material comprises 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the thermal-sprayed powder metal material.

[0007] Another aspect of the invention provides a method of forming a wear resistant component comprising the steps of: spraying a powder metal material, wherein the powder metal material comprises 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the powder metal material.

[0008] The thermal spray powder provides exceptional wear resistance at a low cost relative to other materials used in thermal spray techniques. The thermal spray powder also has a lower melting point and therefore requires lower temperatures during the thermal spray technique, which conserves energy. The thermal spray powder may also be applied to a metal body, such as a piston or piston ring, without causing damage to the body. In addition, during the thermal spray technique, the thermal spray powder may provide

improved oxidation resistance compared to other ferrous based materials used in thermal spray techniques.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009] Other advantages of the present invention will be readily appreciated, as the same becomes better understood by reference to the following detailed description when considered in connection with the accompanying drawings wherein:

[0010] Figure 1 illustrates a high velocity oxygen fuel spraying (HVOF) chamber gun spraying a thermal spray powder on an outer surface of a piston according to one embodiment of the invention;

[0011] Figure 2 illustrates the HVOF chamber gun spraying the thermal spray powder on an outer surface of a piston ring according to another embodiment of the invention;

[0012] Figure 3 is a cross-sectional view of the piston ring of Figure 2 along line 3;

[0013] Figure 4 illustrates the HVOF chamber gun spraying the thermal spray powder to form a spray-formed part according to another embodiment of the invention; and

[0014] Figure 5 is a schematic illustration of an exemplary process used to form the thermal spray powder.

DETAILED DESCRIPTION

[0015] One aspect of the invention provides a wear resistant powder metal material for use in a thermal spray technique, also referred to as a thermal spray process or application. The powder metal material, also referred to as a thermal spray powder **20**, is formed by atomizing a melted iron based alloy including carbon (C), chromium (Cr), tungsten (W), vanadium (V), molybdenum (Mo), and iron (Fe). The thermal spray powder **20** is iron-based and optionally includes other components, such as cobalt (Co), niobium

(Nb), titanium (Ti), manganese (Mn), sulfur (S), silicon (Si), phosphorous (P), zirconium (Zr), and tantalum (Ta).

[0016] The thermal spray powder **20** includes chromium, tungsten, vanadium, and molybdenum in amounts sufficient to provide exceptional wear resistance at a reduced cost, compared to other thermal spray materials. These elements are also present in amounts sufficient to form metal carbides. In one embodiment, the thermal spray powder **20** includes 10.0 to 25.0 wt. % chromium, preferably 11.0 to 15.0 wt. % chromium, and most preferably 13.0 wt. % chromium; 1.0 to 5.0 wt. % tungsten, preferably 1.5 to 3.5 wt. % tungsten, and most preferably 2.5 wt. % tungsten; 3.5 to 7.0 wt. % vanadium, preferably 4.0 to 6.5 wt. % vanadium, and most preferably 6.0 wt. % vanadium; 1.0 to 5.0 wt. % molybdenum, preferably 1.0 to 3.0 wt. % molybdenum, and most preferably 1.5 wt. % molybdenum.

[0017] The thermal spray powder **20** includes the carbon in an amount sufficient to provide metal carbides in an amount greater than 15 vol. %, based on the total volume of the thermal spray powder **20**. In one embodiment, the thermal spray powder **20** includes at least 3.0 wt. % carbon, or 3.0 to 7.0 wt. % carbon, and preferably about 3.8 wt. % carbon, based on the total weight of the thermal spray powder **20**. As the amount of carbon in the thermal spray powder **20** increases so does the hardness of the thermal spray powder **20**. This is because greater amounts of carbon form greater amounts of carbides during the atomization step, which increases the hardness. The amount of carbon in the thermal spray powder **20** is referred to as carbon total (C_{tot}).

[0018] The thermal spray powder **20** also includes a stoichiometric amount of carbon (C_{stoich}), which represents the total carbon content that is tied up in the alloyed carbides at equilibrium. The type and composition of the carbides vary as a function of the carbon content and of the alloying elements content.

[0019] The C_{stoich} necessary to form the desired amount of metal carbides during atomization depends on the amount of carbide-forming elements present in the thermal spray powder **20**. The C_{stoich} for a particular composition is obtained by multiplying the amount of each carbide-forming element by a multiplying factor specific to each element. For a particular carbide-forming element, the multiplying factor is equal to the amount of carbon required to precipitate 1 wt. % of that particular carbide-forming element. The multiplying factors vary based on the type of precipitates formed, the amount of carbon, and the amount of each of the alloying elements. The multiplying factor for a specific carbide will also vary with the amount of carbon and the amount of the alloying elements.

[0020] For example, to form precipitates of $(\text{Cr}_{23.5}\text{Fe}_{7.3}\text{V}_{63.1}\text{Mo}_{3.2}\text{W}_{2.9})_8\text{C}_7$, also referred to as M_8C_7 , in a thermal spray powder **20**, the multiplying factors of the carbide-forming elements are calculated as follows. First, the atomic ratio of the M_8C_7 carbide is determined: 1.88 atoms of Cr, 0.58 atoms of Fe, 5.05 atoms of V, 0.26 atoms of Mo, 0.23 atoms of W, and 7 atoms of C. Next, the mass of each element per one mole of the M_8C_7 carbide is determined: V = 257.15 grams, Cr = 97.76 grams, Fe = 32.62 grams, Mo = 24.56 grams, W = 42.65 grams, and C = 84.07 grams. The weight ratio of each carbide-forming element is then determined: V = 47.73 wt. %, Cr = 18.14 wt. %, Fe = 6.05 wt. %, Mo = 4.56 wt. %, W = 7.92 wt. %, and C = 15.60 wt. %. The weight ratio indicates 47.73 grams of V will react with 15.60 grams of C, which means 1 gram of V will react with 0.33 grams of C. To precipitate 1.0 wt. % V in the M_8C_7 carbide you need 0.33 wt. % carbon, and therefore the multiplying factor for V is 0.33. The same calculation is done to determine the multiplying factor for Cr = 0.29, Mo = 0.06, and W = 0.03.

[0021] The C_{stoich} in the thermal spray powder **20** is next determined by multiplying the amount of each carbide-forming element by the associated multiplying factor, and then adding each of those values together. For example, if the thermal spray powder **20**

includes 4.0 wt. % V, 13.0 wt. % Cr, 1.5 wt. % Mo, and 2.5 wt. % W, then $C_{\text{stoich}} = (4.0 \times 0.33) + (13.0 \times 0.29) + (1.5 \times 0.06) + (2.5 \times 0.03) = 5.26 \text{ wt. \%}$.

[0022] In addition, the thermal spray powder **20** includes a $C_{\text{tot}} / C_{\text{stoich}}$ amount less than 1.1. Therefore, when the thermal spray powder **20** includes carbon at the upper limit of 7.0 wt. %, the C_{stoich} will be 6.36 wt. % carbon (7.0 wt. % carbon / 1.1).

[0023] The table below provides examples of other carbide types that can be found in the thermal spray powder **20**, and multiplying factors for Cr, V, Mo, and W for generic carbide stoichiometry. However, the metal atoms in each of the carbides listed in the table could be partly replaced by other atoms, which would affect the multiplying factors.

Element	Carbide type	Example of stoichiometry	Multiplying factor f_M (wt. %/wt. %)
Cr	M_7C_3	$Cr_{3.5}Fe_{3.5}C_3$	0.20
		$Cr_4Fe_3C_3$	0.17
		$(Cr_{34}Fe_{66})_7C_3$	0.29
V	M_8C_7	$(V_{63}Fe_{37})_8C_7$	0.33
Mo	M_6C	Mo_3Fe_3C	0.04
		Mo_2Fe_4C	0.06
W	M_6C	W_3Fe_3C	0.02
		W_2Fe_4C	0.03

[0024] The metal carbides are formed during the atomization process and are present in an amount of at least 15.0 vol. %, but preferably in an amount of 40.0 to 60.0 vol. %, or 47.0 to 52.0 vol. %, and typically about 50.0 vol. %. In one embodiment, the thermal spray powder **20** includes chromium-rich carbides, molybdenum-rich carbides, tungsten-rich carbides and vanadium-rich carbides in a total amount of about 50.0 vol. %.

[0025] The metal carbides have a nanoscale microstructure. In one embodiment, the metal carbides have a diameter between 1 and 400 nanometers. The fine nano-carbide structure may improve the adherence of the thermal spray powder **20** to an outer surface **22**, **122** of a metal body **24**, **124**. Therefore, a wear resistant coating formed of the

thermal spray powder **20** is less prone to flaking, chipping, and delamination. The fine carbide structure may also provide a more homogeneous microstructure, and therefore an improved impact and fatigue resistance compared to thermal spray materials with coarser carbide microstructures. As alluded to above, the carbides can be of various types, including M_8C_7 , M_7C_3 , MC , M_6C , $M_{23}C_6$, and M_3C , wherein M is at least one metal atom, such as Fe, Cr, V, Mo, and/or W, and C is carbon. In one embodiment, the metal carbides are selected from the group consisting of: M_8C_7 , M_7C_3 , M_6C ; wherein M_8C_7 is $(V_{63}Fe_{37})_8C_7$, M_7C_3 is selected from the group consisting of: $(Cr_{34}Fe_{66})_7C_3$, $Cr_{3.5}Fe_{3.5}C_3$, and $Cr_4Fe_3C_3$; and M_6C is selected from the group consisting of: Mo_3Fe_3C , Mo_2Fe_4C , W_3Fe_3C , and W_2Fe_4C .

[0026] The microstructure of the thermal spray powder **20** also includes nanoscale austenite, and may include nanoscale martensite, along with the nanoscale carbides. The carbon is also present in an amount sufficient to limit oxidation of the thermal spray powder **20** during the thermal spray process. Oxidation can occur due to poor atmosphere control, lack of cleanliness, and temperature during the thermal spray process.

[0027] The thermal spray powder **20** can optionally include other elements, which may contribute to improved wear resistance or enhance another material characteristic. In one embodiment, the thermal spray powder **20** includes at least one of cobalt, niobium, titanium, manganese, sulfur, silicon, phosphorous, zirconium, and tantalum. In one embodiment, the thermal spray powder **20** includes at least one of 4.0 to 15.0 wt. % cobalt; up to 7.0 wt.% niobium; up to 7.0 wt. % titanium; up to 2.0 wt. % manganese; up to 1.15 wt. % sulfur; up to 2.0 wt. % silicon; up to 2.0 wt. % phosphorous; up to 2.0 wt. % zirconium; and up to 2.0 wt. % tantalum. In one embodiment, thermal spray powder **20** contains pre-alloyed sulfur to form sulfides or sulfur containing compounds in the powder. Sulfides (ex. MnS , CrS) are known to improve machinability and could be beneficial to wear resistance.

[0028] The remaining balance of the thermal spray powder **20** composition is iron. In one embodiment, the thermal spray powder **20** includes at least 40.0 wt. % iron, or 50.0 to 81.5 wt% iron, and preferably 70.0 to 80.0 wt. % iron. The thermal spray powder **20** typically has a microhardness of 800 to 1,500 Hv₅₀. The high hardness contributes to the exceptional wear resistance of the wear resistant coating **26** and the fine structure should improve toughness. The microhardness of the thermal spray powder **20** increases with increasing amounts of carbon.

[0029] In one exemplary embodiment, the thermal spray powder **20** includes 3.8 wt. % carbon, 13.0 wt. % chromium, 2.5 wt. % tungsten, 4.0-6.0 wt. % vanadium, 1.5 wt. % molybdenum, 0.2 wt. % oxygen, 70.0 to 80.0 wt. % iron, and impurities in an amount not greater than 2.0 wt. %.

[0030] The thermal spray powder **20** of the exemplary embodiment has a melting point of about 1,235° C (2,255° F), and it will be completely melted at that temperature. The melting point of thermal spray powder **20** will however vary slightly as a function of the carbon content and alloying element content. However, the thermal spray powder **20** may include a small fraction of a liquid phase at a temperature as low as 1,150° C. The low melting point provides several advantages during the thermal spray process, compared to thermal spray materials having higher melting points. Less energy is needed to apply the thermal spray powder **20** to the outer surface **22** of the body **24** being coated. The thermal spray powder **22** can be sprayed at a lower temperature, which may provide less heat input to the body **24** being coated, less manufacturing equipment wear, possibly lower porosity in the wear resistant coating **26**, and less oxidation of the thermal spray powder **20** during the spraying process. The lower melting point also provides the opportunity to use a cold spraying technique.

[0031] The thermal spray powder **20** is formed by water or gas atomizing a melted iron based alloy. An exemplary process of forming the thermal spray powder **20** using water atomization is shown in Figure 5. However, the water atomization step could be replaced by a gas atomization step. In one embodiment, the iron based alloy provided prior to atomization includes 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, and at least 40.0 wt. % iron. The iron based alloy is typically provided as a pre-alloy including the carbon, chromium, tungsten, vanadium, molybdenum, and iron. The iron based alloy also has a low oxygen content, preferably not greater than 0.5 wt. %. The carbon content of the iron based alloy is sufficient to protect the alloy from oxidizing during the melting and atomizing steps.

[0032] Once the iron based alloy is melted, it is fed to a water atomizer or a gas atomizer. The high carbon content of the iron based alloy decreases the solubility of the oxygen in the melted iron based alloy. Depleting the oxygen level in the melted iron based alloy has the benefit of shielding the carbide-forming elements from oxidizing during the melting and atomizing steps. The relatively high carbon content allows the austenite, or possibly martensite, to form in the matrix of the thermal spray powder **20**, in which the carbides precipitate, during the atomizing step. Increasing the amount of carbide-forming alloying elements in the iron based alloy can also increase the amount of carbides formed in the matrix during the atomizing step.

[0033] In the atomizer, a stream of the melted iron based alloy is impacted by a flow of high-pressure water or gas which disperses and rapidly solidifies the melted iron based alloy stream into fully alloyed metal droplets. Gas atomization typically yields particles having a round shape, whereas water atomization typically yields particles of irregular shape. Preferably, each droplet possesses the fully alloyed chemical composition of the melted batch of metal, including at least 3.0 wt. % carbon, 10.0 to 25.0 wt. % chromium,

1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, and at least 40.0 wt. % iron. Each droplet also preferably includes a uniform distribution of carbides. The main elements of the droplets are protected from oxidation by the high carbon content of the powder during the melting and atomizing steps. The high carbon content and low oxygen content also limits the oxidization during the atomizing step. However, the outside surface of the droplets may become oxidized, possibly due to exposure to water or unprotected atmosphere. Some properties can be improved using gas atomization over water atomization, for example better flow, apparent density, and lower oxygen content.

[0034] The atomized droplets are then passed through a dryer and into a grinder where the atomized material is mechanically ground or crushed, and then sieved. The hard and very fine nano-structure of the droplets improves the ease of grinding. A ball mill or other mechanical size reducing device may be employed. In addition, the droplets could be annealed prior to grinding the droplets, but no annealing step is required prior to grinding the droplets, and typically no annealing step is conducted. If an outer oxide skin is formed on the atomized droplets during the atomization step, the mechanical grinding fractures and separates the outer oxide skin from the bulk of the droplets. The ground droplets are then separated from the oxide skin to yield the atomized thermal spray powder **20** and oxide particles **30**, as shown in Figure 5. In certain cases, such as when gas atomization is used, the outer oxide skin is minimal and can be tolerated without removal. However, the mechanical grinding step can still be used to fracture and reduce the size of the droplets. The thermal spray powder **20** may be further sorted for size, shape and other characteristics normally associated with powder metal. The thermal spray powder **20** can then be used to form a wear resistant component **28**, **128**, **228** such as a piston or piston ring.

[0035] Figure 1 illustrates an example of the wear resistant component **28** including the thermal spray powder **20**. In Figure 1, the wear resistant component **28** is a

piston including a body **24**, specifically a skirt, presenting an outer surface **22**. The thermal spray powder **20** is applied to the outer surface **22** of the body **24** by a thermal spraying technique to form a wear resistant coating on the outer surface **22**. The wear resistant coating typically has a microhardness of 800 to 1,500 Hv₅₀. Figure 2 illustrates another example of the wear resistant component **128** including the thermal spray powder **20**. The wear resistant component **128** includes a body **124**, specifically an uncoated piston ring, presenting an inner surface **136** surrounding a center axis **A** and an outer surface **122** facing opposite the inner surface **136**. The thermal spray powder **20** is applied to the outer surface **122** by a thermal spraying technique to form a wear resistant coating on the outer surface **122**.

[0036] The thermal spray powder **20** can also be used to form wear resistant coatings on other components (not shown), for example turbine blades, transmission parts, exhaust system components, crankshafts, other automotive components, pulp and paper rollers, oil and petrochemical drilling components, golf clubs, and surgical applications.

[0037] Figure 4 is another example of the wear resistant component **228**, specifically a piston ring, wherein the wear resistant component **228** consists entirely of the thermal spray powder **20**. The wear resistant component **228** presents an inner surface **236** surrounding a center axis **A** and an outer surface **222** facing opposite the inner surface **236**. This wear resistant component **228** is referred to as a spray-formed part. The spray-formed part typically has a microhardness of 800 to 1,500 Hv₅₀.

[0038] Various thermal spray techniques can be used to form the wear resistant component **28**, **128**, **228**. Four typical thermal spray techniques are combustion, electrical discharge, cold spray, and laser. Each thermal spray technique includes spraying the thermal spray powder **20**, either onto the outer surface **22**, **122** of the body **24**, **124** to form the wear resistant coating, or onto a substrate **238** to form the spray-formed part. The spraying step includes accelerating the thermal spray powder **20** at a high velocity, which can

be up to a supersonic velocity. Once the thermal spray powder **20** has been sprayed at the high velocity to form the coating or the spray-formed part, it can be referred to as a thermal-sprayed powder or thermal-sprayed coating. The combustion, electrical discharge, and laser techniques include melting the thermal spray powder **20** before spraying the melted powder. These techniques include heating the thermal spray powder **20** and then accelerating the heated thermal spray powder **20** to the outer surface **22**, **122** of the body **24**, **124** or onto the substrate **238**, at a high velocity while the thermal spray powder **20** is heated.

[0039] One example of the combustion technique includes flame spraying, such as powder flame spraying or wire flame spraying. Another example of the combustion technique is high velocity oxygen fuel spraying (HVOF), which involves oxygen and gaseous fuels (HVOF-G) or liquid fuels (HVOF-K).

[0040] The electrical discharge technique can include plasma spraying or wire arc spraying. The plasma spraying is typically conducted under inert gas (IPS), a vacuum (VPS), or by dispersing the thermal spray powder **20** in a liquid suspension before injecting the thermal spray powder into a plasma jet (SPS). The plasma spraying can also include atmospherical plasma spraying (APS), high pressure plasma spraying (HPPS), water-stabilized plasma spraying (WSPS), reactive plasma spraying (RPS), or underwater plasma spraying (UPS). If nitrogen is used as the inert gas during the plasma spraying process, there is a potential to form vanadium carbonitrides, thus improving hardness and wear resistance. This potential is controlled by the processing parameters and the chemistry of the thermal spray powder **20** before the spraying process.

[0041] The most preferred thermal spray techniques are powder flame spraying, plasma spraying, cold spraying, and high velocity oxygen fuel spraying (HVOF). Figures 1, 2, and 4 illustrate a step in the HVOF process, wherein a HVOF chamber gun sprays the thermal spray powder **20** on the outer surface **22**, **122** of the body **24**, **124**, or onto

the substrate **238**. The HVOF chamber gun includes a pressurized combustion chamber **32** in fluid communication with a nozzle **34**. The combustion chamber **32** contains a mixture of carrier gas, such as oxygen, and fuel, such as of acetylene, hydrogen, propane, or propylene. The mixture is ignited to produce a high-pressure flame and creating a pressure in the combustion chamber. The flame is formed through the nozzle **34** to accelerate the carrier gas to a high velocity, which can be up to a supersonic velocity. The thermal spray powder **20** is then fed axially into the high pressure combustion chamber **32** or directly through the side of the nozzle **34**. The carrier gas accelerates the thermal spray powder **20** out of the HVOF chamber gun at a high velocity.

[0042] In the embodiments of Figures 1 and 2, the thermal spray powder **20** is applied to the outer surface **22**, **122** of the body **24**, **124** to form the wear resistant coating. Figure 3 shows a thickness **t** of the wear resistant coating applied to the body **124** of Figure 2. The thickness depends on the thermal spray technique used, design of the body **124**, and application of the wear resistant component **28**. In one embodiment, the thickness of the wear resistant coating is 20 to 200 microns.

[0043] The method of forming the wear resistant component **28** can optionally include a post-spraying heat treatment. In one embodiment, the method includes annealing the thermal spray powder **20** after it is applied to the body **24**, **124** or formed into the spray-formed part. The annealing or other heat treatment step could modify the microstructure of the thermal spray powder **20** by making it coarser. For example, the metal carbides could have diameter of at least one micron, rather than between 1 and 400 nanometers.

[0044] Another aspect of the invention provides a method of forming the wear resistant component **228**, wherein the wear resistant component **228** is a spray-formed part consisting of the thermal spray powder **20**, such as the piston ring of Figure 4. The spray-formed part is manufactured by spraying the thermal spray powder **20** onto the substrate **238**

to a thickness of up to 500 millimeters. The spray-forming process is a near-net-shape process and includes capturing a spray of powder on a moving substrate, as described in the ASM Handbook, Volume 7. This process provides several advantages, including densities greater than 98%, fine equiaxed grains, no macroscopic segregation, absence of prior particle boundaries, enhanced mechanical properties, material/alloying flexibility, and a high rate of deposition, such as greater than 2 kg/second.

[0045] In addition, the thermal spray powder **20** could be co-sprayed with other powders to form the wear resistant component **28**, **128**, **228**, either the resistant coating or the spray-formed part. Examples of other powders that could be co-sprayed with the thermal spray powder **20** of the present invention include intermetallics, other hard phases, and metallic alloys. The wear resistant coatings **26** and spray-formed parts including the co-sprayed powders could provide a wide range of microstructures, different from the microstructures provided by the thermal spray powder **20** alone.

[0046] Obviously, many modifications and variations of the present invention are possible in light of the above teachings and may be practiced otherwise than as specifically described while within the scope of the claims.

CLAIMS

What is claimed is:

1. A powder metal material for use in a thermal spray technique, comprising: 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the powder metal material.
2. The powder metal material of claim 1 including 3.5 to 4.0 wt. % carbon, 11.0 to 15.0 wt. % chromium, 1.5 to 3.5 wt. % tungsten, 4.0 to 6.5 wt. % vanadium, 1.0 to 3.0 wt. % molybdenum, not greater than 0.3 wt. % oxygen, and 50.0 to 81.5 wt. % iron.
3. The powder metal material of claim 2 consisting of 3.8 wt. % carbon, 13.0 wt. % chromium, 2.5 wt. % tungsten, 6.0 wt. % vanadium, 1.5 wt. % molybdenum, 0.2 wt. % oxygen, 70.0 to 80.0 wt. % iron, and impurities in an amount not greater than 2.0 wt. %.
4. The powder metal material of claim 1 including at least one of cobalt, niobium, titanium, manganese, sulfur, silicon, phosphorous, zirconium, and tantalum.
5. The powder metal material of claim 1 including metal carbides in an amount of at least 15.0 vol. %, based on the total volume of the powder metal material.
6. The powder metal material of claim 5, wherein the metal carbides are selected from the group consisting of: M_8C_7 , M_7C_3 , M_6C , wherein M is at least one metal atom and C is carbon.

7. The powder metal material of claim 6, wherein M_8C_7 is $(V_{63}Fe_{37})_8C_7$; M_7C_3 is selected from the group consisting of: $(Cr_{34}Fe_{66})_7C_3$, $Cr_{3.5}Fe_{3.5}C_3$, and $Cr_4Fe_3C_3$; and M_6C is selected from the group consisting of: Mo_3Fe_3C , Mo_2Fe_4C , W_3Fe_3C , and W_2Fe_4C .

8. A method of forming a powder metal material for use in a thermal spray technique, comprising the steps of:

providing a melted iron based alloy including 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the melted iron based alloy; and

atomizing the melted iron based alloy to provide atomized droplets of the iron based alloy.

9. The method of claim 8 including grinding the atomized droplets.

10. The method of claim 8, wherein the atomizing step includes forming metal carbides in the iron based alloy in an amount of at least 15.0 vol. %, based on the total volume of the iron based alloy.

11. The method of claim 10, wherein the metal carbides are selected from the group consisting of: M_8C_7 , M_7C_3 , M_6C , wherein M is at least one metal atom and C is carbon.

12. The method of claim 11, wherein M_8C_7 is $(V_{63}Fe_{37})_8C_7$; M_7C_3 is selected from the group consisting of: $(Cr_{34}Fe_{66})_7C_3$, $Cr_{3.5}Fe_{3.5}C_3$, and $Cr_4Fe_3C_3$; and M_6C is selected from the group consisting of: Mo_3Fe_3C , Mo_2Fe_4C , W_3Fe_3C , and W_2Fe_4C .

13. A wear resistant component, comprising: a thermal-sprayed powder metal material, wherein said thermal-sprayed powder metal material comprises: 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of said thermal-sprayed powder metal material.

14. The wear resistant component of claim 13 further comprising a body with an outer surface, and wherein said thermal-sprayed powder metal material is disposed on said outer surface.

15. The wear resistant component of claim 14 wherein said body is a piston ring presenting an inner surface surrounding a center axis and an outer surface facing opposite said inner surface, and said thermal-sprayed powder metal material forms a coating on said outer surface.

16. The wear resistant component of claim 14 wherein said body is a piston presenting an outer surface, and said thermal-sprayed powder metal material forms a coating on said outer surface.

17. The wear resistant coating of claim 13 wherein said wear resistant component consists of said thermal-sprayed powder metal material.

18. The wear resistant coating of claim 17 wherein said wear resistant component is a piston ring.

19. The wear resistant component of claim 13 including a second powder metal material mixed with said thermal-sprayed powder metal material.

20. A method of forming a wear resistant component, comprising the steps of: spraying a powder metal material, wherein the powder metal material comprises 3.0 to 7.0 wt. % carbon, 10.0 to 25.0 wt. % chromium, 1.0 to 5.0 wt. % tungsten, 3.5 to 7.0 wt. % vanadium, 1.0 to 5.0 wt. % molybdenum, not greater than 0.5 wt. % oxygen, and at least 40.0 wt. % iron, based on the total weight of the powder metal composition.

21. The method of claim 20 wherein the spraying step is a thermal spray technique selected from the group consisting of: powder flame spraying, plasma spraying, cold spraying, and high velocity oxygen fuel spraying (HVOF).

22. The method of claim 20 including heating the powder metal material before the spraying step, and wherein the powder metal material is heated during the spraying step.

23. The method of claim 20 wherein the thermal spray technique includes providing a combustion chamber containing a mixture of fuel and oxygen; igniting the mixture of fuel and oxygen; and feeding the powder metal material into the combustion chamber after the igniting step to accelerate the powder metal material.

24. The method of claim 23 wherein the igniting step includes creating a pressure in the combustion chamber, and accelerating the powder metal material up to a supersonic velocity.

25. The method of claim 20 including providing a body, and wherein the spraying step includes spraying the powder metal material onto the body.

26. The method of claim 20 wherein the spraying step forms the wear resistant component, and the wear resistant component is a piston ring presenting an inner surface surrounding a center axis and an outer surface facing opposite the inner surface.

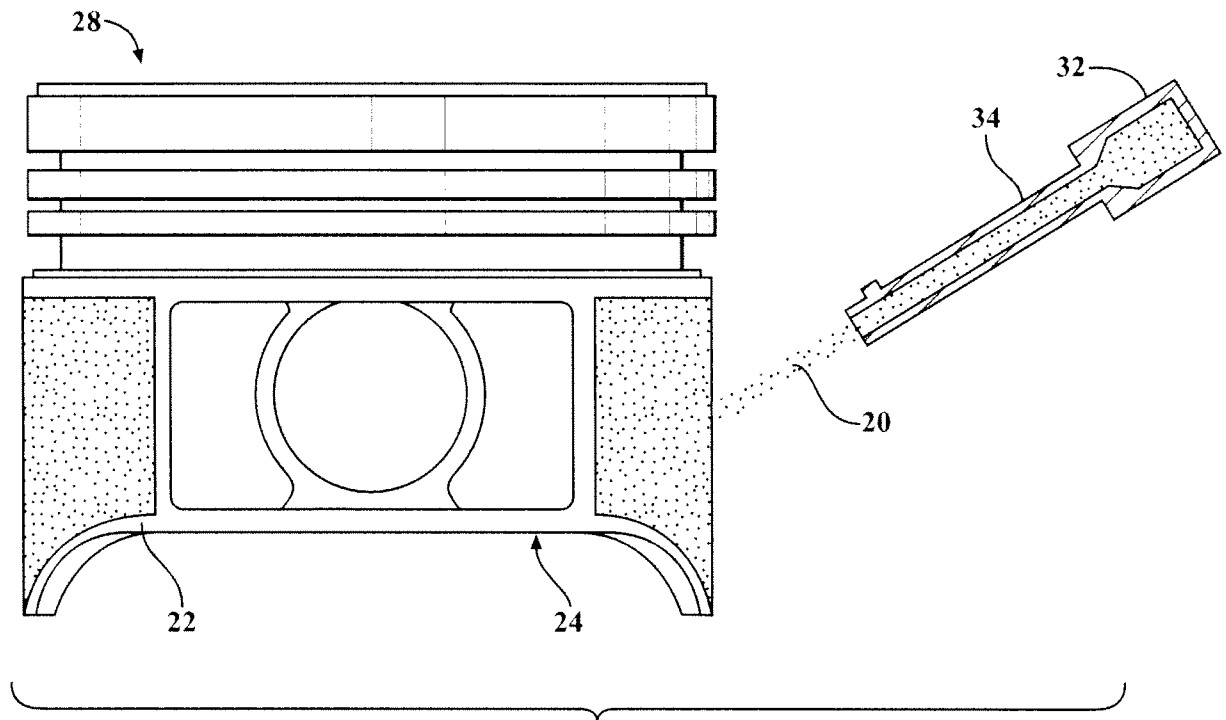


FIG. 1

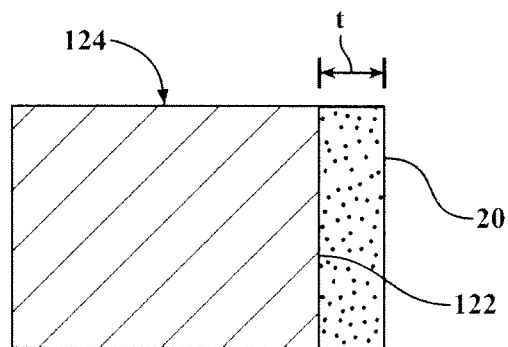


FIG. 3

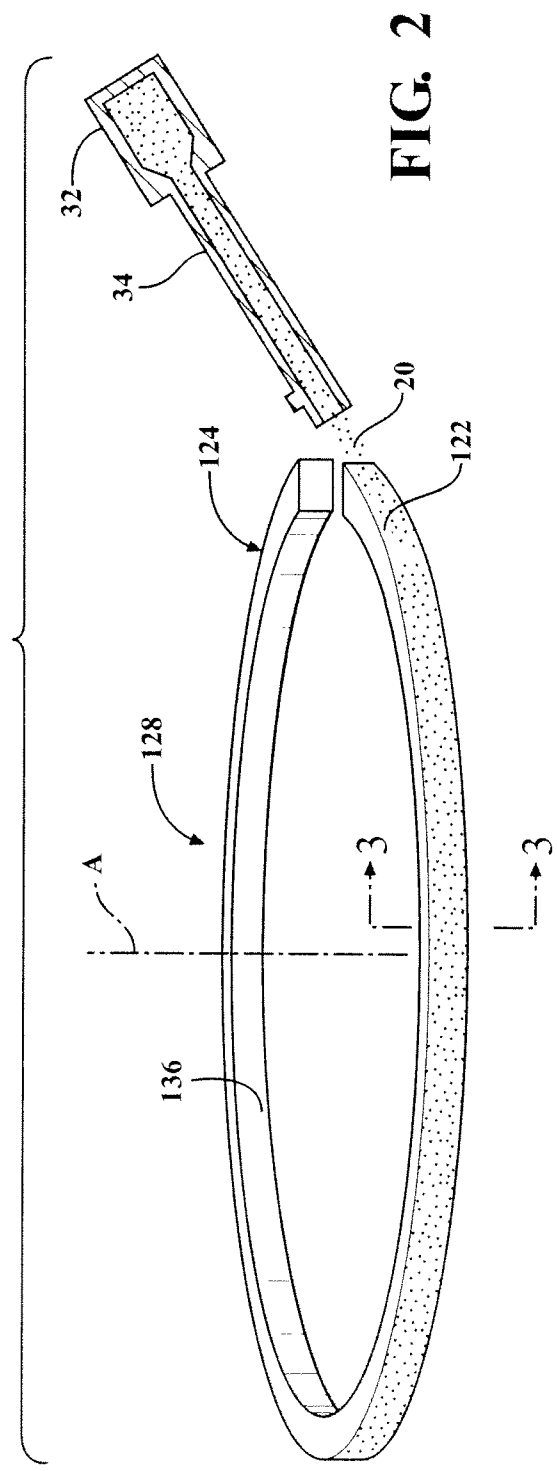
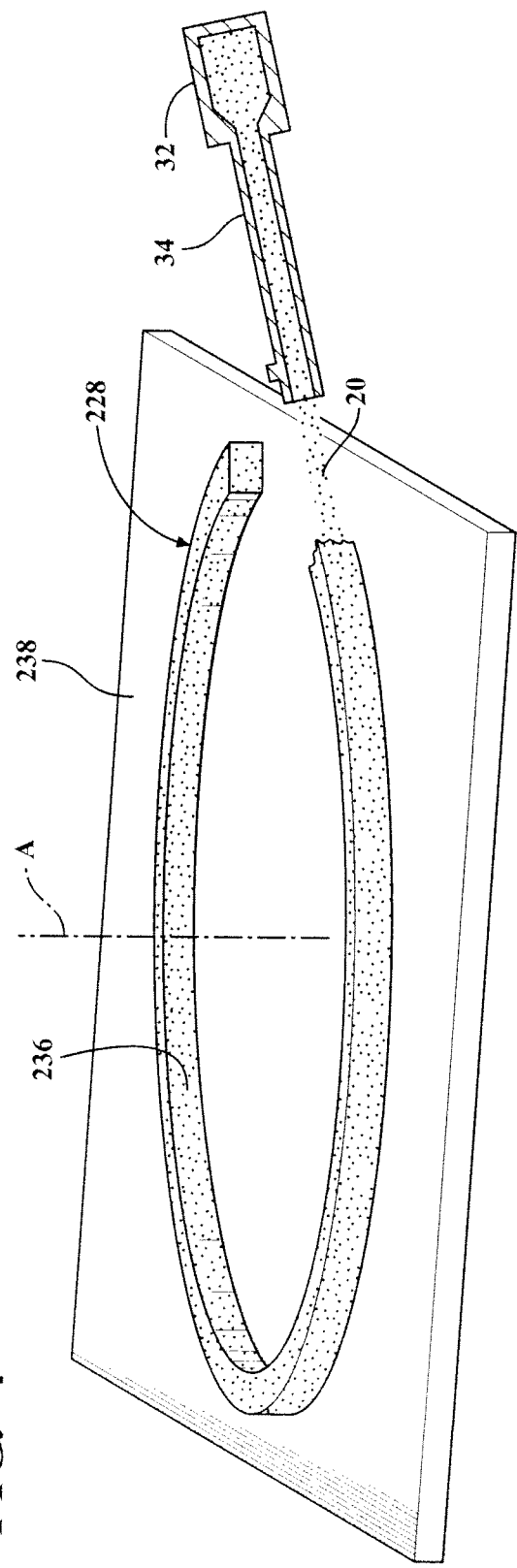


FIG. 4



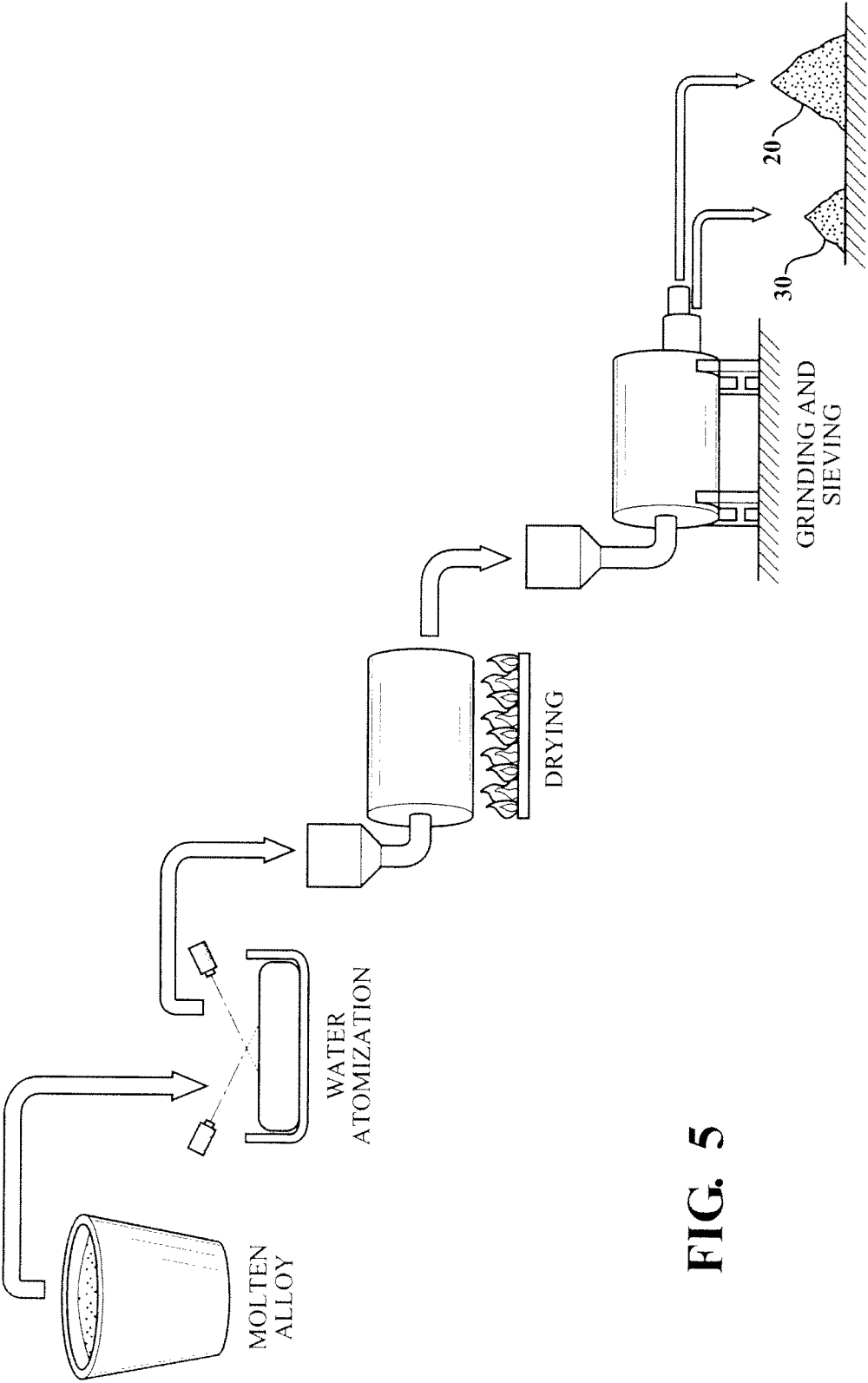


FIG. 5