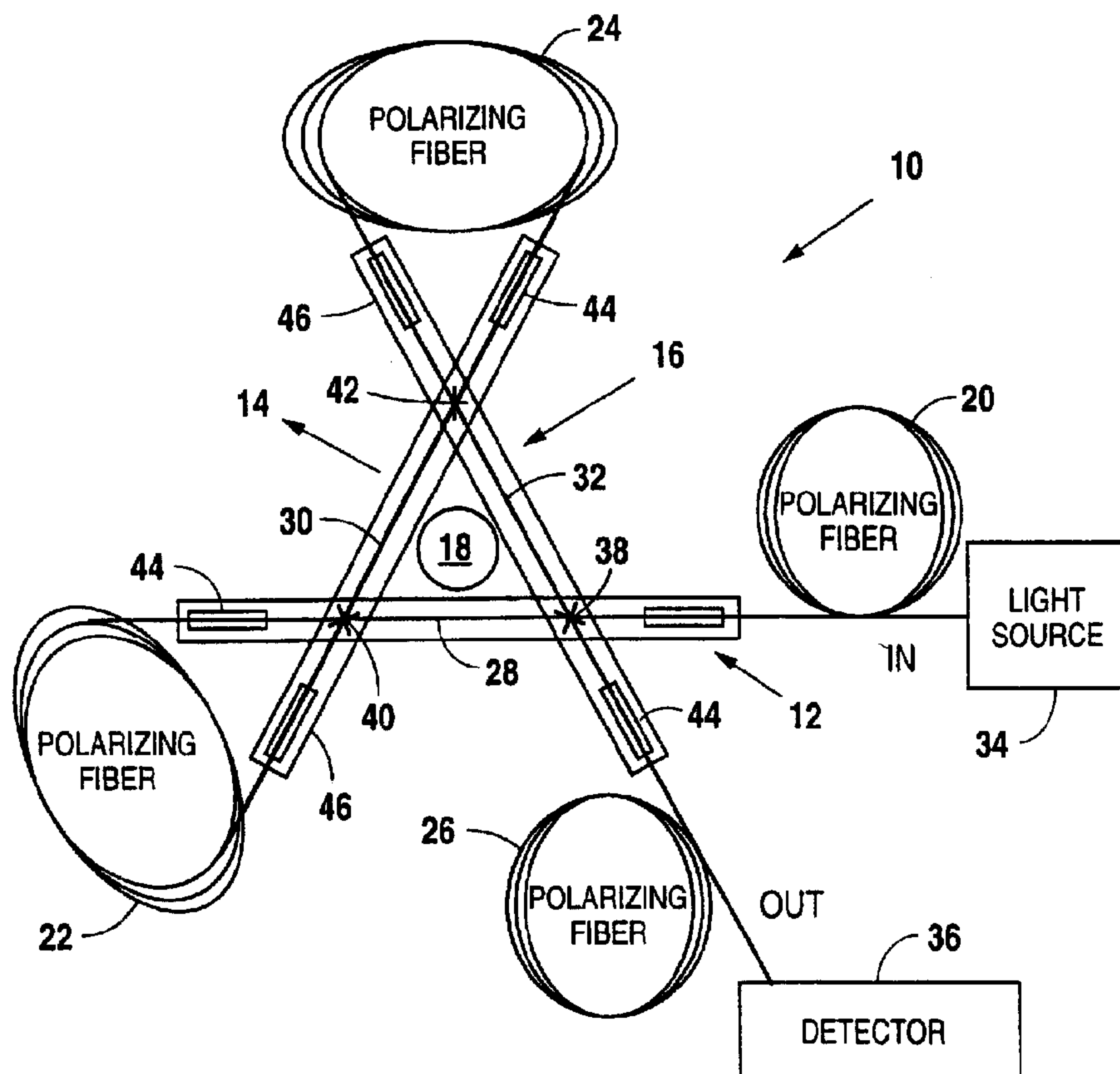




(86) Date de dépôt PCT/PCT Filing Date: 1996/09/12
 (87) Date publication PCT/PCT Publication Date: 1997/05/29
 (45) Date de délivrance/Issue Date: 2009/02/03
 (85) Entrée phase nationale/National Entry: 1998/05/05
 (86) N° demande PCT/PCT Application No.: US 1996/014579
 (87) N° publication PCT/PCT Publication No.: 1997/019361
 (30) Priorité/Priority: 1995/11/22 (US08/561810)

(51) Cl.Int./Int.Cl. *G01R 19/00* (2006.01),
G01R 33/032 (2006.01)
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(54) Titre : CAPTEURS CONCATENES DE CHAMPS UTILISANT L'EFFET MAGNETO-OPTIQUE
 (54) Title: CONCATENATED MAGNETO-OPTIC FIELD SENSORS



(57) Abrégé/Abstract:

A Faraday effect current sensor uses a plurality of concatenated field sensors, with a single light source and a single detector. At least two Faraday effect sensing elements (single mode sensing fibers) are used, preferably at least three, the sensing elements being interconnected by fusion spliced, polarizing fibers. The sensing fibers may be oriented generally straight, and arranged to form a regular polygon, e.g., an equilateral triangle for a three-element sensor. The locations of the splices between the sensing fibers and the polarizing fibers may further be advantageously arranged such that the sensing fibers form a substantially closed

(57) **Abrégé(suite)/Abstract(continued):**

path which may be placed about the current-carrying conductor. The linearity of the sensor response may be improved by selecting an appropriate value of the bias angle of each sensing element optimally equal to $\arctan[1/\sqrt{(2n-1)}]$ where n is the number of sensing elements. The present invention may also be adapted for use as a differential current sensor wherein each sensing element is housed in a separate package allowing the elements to be placed about different conductors at a Y-branch, or about a single conductor at different locations.



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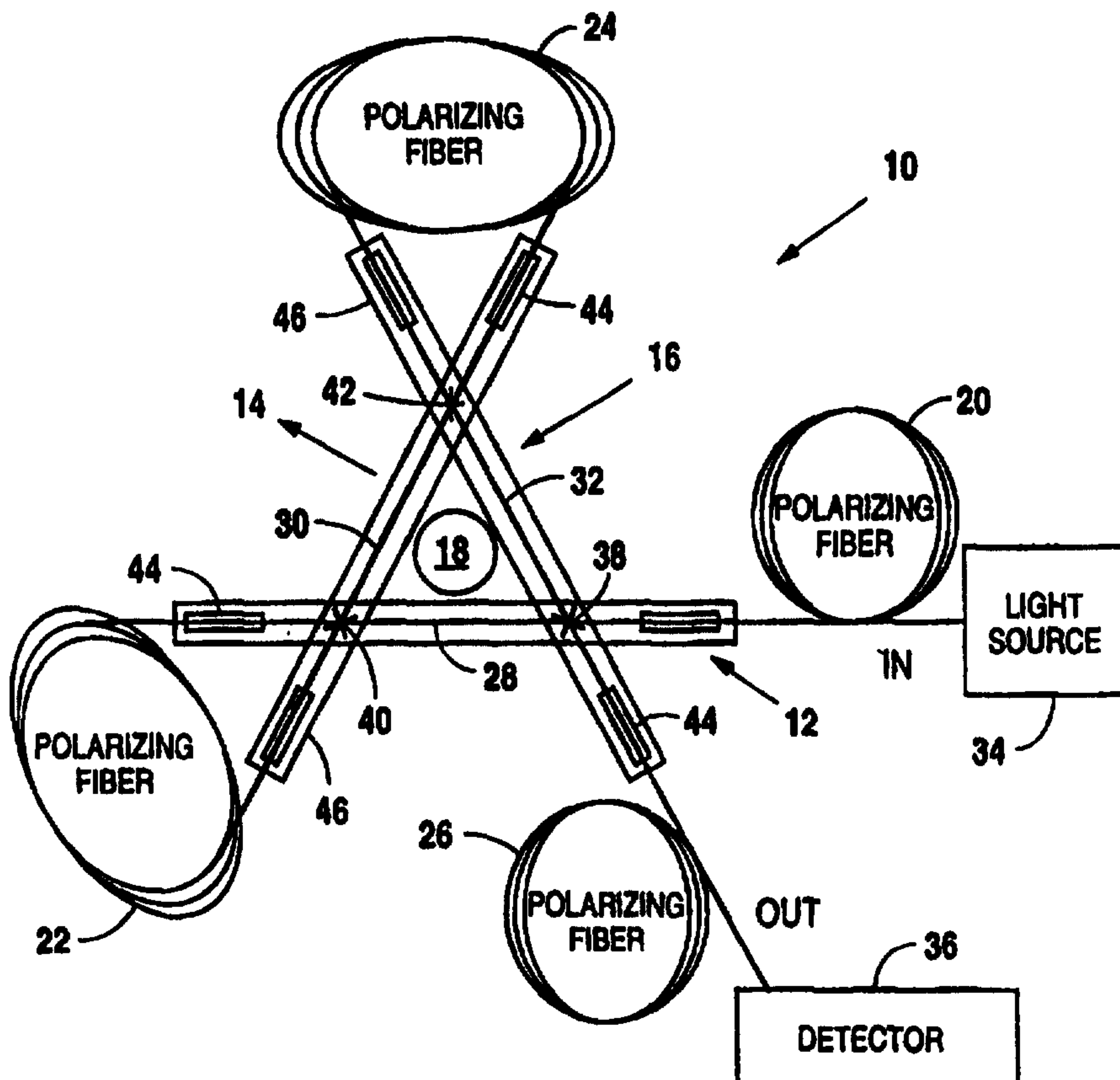
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification ⁶ : G01R 33/032</p>	<p>A1</p>	<p>(11) International Publication Number: WO 97/19361 (43) International Publication Date: 29 May 1997 (29.05.97)</p>
<p>(21) International Application Number: PCT/US96/14579 (22) International Filing Date: 12 September 1996 (12.09.96) (30) Priority Data: 08/561,810 22 November 1995 (22.11.95) US (71) Applicant: MINNESOTA MINING AND MANUFACTURING COMPANY [US/US]; 3M Center, P.O. Box 33427, Saint Paul, MN 55133-3427 (US). (72) Inventors: DAWSON, Jay, W.; P.O. Box 33427, Saint Paul, MN 55133-3427 (US). MACDOUGALL, Trevor, W.; P.O. Box 33427, Saint Paul, MN 55133-3427 (US). (74) Agents: MUSGROVE, Jack, V. et al.; Minnesota Mining and Manufacturing Company, Office of Intellectual Property Counsel, P.O. Box 33427, Saint Paul, MN 55133-3427 (US).</p>		<p>(81) Designated States: CA, CN, JP, KR, MX, SG, European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published With international search report.</p>

(54) Title: CONCATENATED MAGNETO-OPTIC FIELD SENSORS

(57) Abstract

A Faraday effect current sensor uses a plurality of concatenated field sensors, with a single light source and a single detector. At least two Faraday effect sensing elements (single mode sensing fibers) are used, preferably at least three, the sensing elements being interconnected by fusion spliced, polarizing fibers. The sensing fibers may be oriented generally straight, and arranged to form a regular polygon, e.g., an equilateral triangle for a three-element sensor. The locations of the splices between the sensing fibers and the polarizing fibers may further be advantageously arranged such that the sensing fibers form a substantially closed path which may be placed about the current-carrying conductor. The linearity of the sensor response may be improved by selecting an appropriate value of the bias angle of each sensing element, optimally equal to $\arctan[1/\sqrt{(2n-1)}]$ where n is the number of sensing elements. The present invention may also be adapted for use as a differential current sensor wherein each sensing element is housed in a separate package allowing the elements to be placed about different conductors at a Y-branch, or about a single conductor at different locations.



Concatenated Magneto-Optic Field Sensors

Background of the Invention

5 1. Field of the Invention

The present invention generally relates to Faraday effect, fiber optic current-sensors, and more particularly to an improved sensor which uses a plurality of field sensors (separate sensing fibers) connected in series.

2. Description of the Prior Art

10 Optical fibers which are sensitive to magnetic fields are known in the art, and are increasingly being used as optical current transducers (OCT's) for, e.g., electric power utilities. A typical OCT uses a single-mode fiber formed into a coil surrounding the electrical conductor. The polarization of any light traversing the fiber coil shifts, in response to the change in any current flowing through the conductor, as a
15 result of the magneto-optic Faraday effect, also referred to as Faraday rotation or the Kundt effect. The Faraday effect is the manner in which the polarization of a beam of linearly polarized light rotates when it passes through matter in the direction of an applied magnetic field, and is the result of Faraday birefringence. Faraday
20 birefringence is the difference in the indices of refraction of left and right circularly polarized light passing through matter parallel to an applied magnetic field. Further discussion of field-sensitive optical fibers is provided in U.S. Patent No. 5,051,577 assigned to Minnesota Mining and Manufacturing Co. (3M--assignee of the present invention).

 Many prior art references recognize that the response of OCT's may
25 vary considerably due to temperature variations, unacceptably so for highly precise OCT's which may be used in environments having widely varying temperature ranges, such as -40° to +80° C. The prior art recognizes that temperature effects on a sensing coil relate to three different phenomena: (i) changes in the birefringence in the sensing fiber, (ii) changes in birefringence due to stresses induced by the materials
30 encapsulating the sensing fiber, and (iii) changes in the Verdet constant of the fiber core material. Many techniques have been devised to minimize the influence of

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temperature changes. The most basic technique is to compensate the output based on empirical data, i.e., use a thermometer to determine the temperature during actual measurements, and allow post-processing electronics to adjust the output accordingly. A more complicated variation of this technique is disclosed in U.S. Patent No. 5,416,860. That system requires not only additional electronic processing, but also requires additional opto-electronic components, which generally increase the cost of the unit. Another complicated method, involving the use of a beam splitter and processing of the two polarization components, is described in U.S. Patent No. 5,382,901. See also European Patent Application No. 657,740. A different approach is to minimize the temperature dependence by minimizing birefringence of the sensing fiber during its manufacture, such as by spinning the fiber, and then annealing it in a coil form, as taught by U.S. Patent No. 5,463,312. Special materials for the sensing fiber may also be used to minimize fluctuations due to the changing Verdet constant, as disclosed in "Temperature Dependence of the Verdet Constant in Several Diamagnetic Glasses", Journal of Applied Optics, Vol. 30, No. 10, pp. 1176-1178 (April 1, 1991).

Temperature sensitivity may also be caused by bend-induced birefringence. This may occur, for example, where a single sensing fiber is arranged in two or more straight sections to be placed about the current-carrying conductor, with loops of the fiber formed at the ends of the straight sections. The sensing head described in "Geometrical Separation Between the Birefringence Components in Faraday-Rotation Fiber-Optic Current Sensors," Optics Letters, Vol. 16, No. 9, pp. 687-689 (May 1, 1991), minimizes this effect by selecting appropriate geometric parameters of the loops (radius and number of turns) so that the bend-induced birefringence is a multiple of 2π . In the depicted sensing head, the single sensing fiber has been formed into four straight sections generally forming a square about the conductor. While this construction does reduce bend-induced birefringence, it still suffers from a common disadvantage of OCT's, that of installing the sensor on an "endless" cable, i.e., an existing cable that cannot be threaded through the sensor. Sensor coils, as well as square-shaped sensors, may be constructed to allow placement on an endless cable by providing a sufficient spacing between the coil loops or the

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sides of the square sensing fiber, but this increases the size of the sensor and can affect its accuracy. It would, therefore, be desirable to devise a fiber-optic current sensor having improved temperature-dependence, but which can more easily be installed on an existing cable. It would be further advantageous if the sensor could be fabricated without special materials, special optical components, or specially processed fibers.

Summary of the Invention

10 According to the present invention, there is provided a device for sensing electrical current flowing through a conductor, the device comprising: a light source, a first Faraday effect sensing element having an input and an output, first means for coupling said light source to
15 said input of said first sensing element, a second Faraday effect sensing element having an input and an output, second means for coupling said output of said first sensing element to said input of said second sensing element, an optical
20 detector, and third means for coupling said output of said second sensing element to said optical detector, wherein said first sensing element includes a first sensing fiber having first and second ends, said first end thereof being coupled to said light source, said second coupling means
25 includes a polarizing fiber having first and second ends, said first end thereof being spliced to said second end of said first sensing fiber, and said second sensing element includes a second sensing fiber having first and second ends, said first end of said second sensing fiber being spliced to said second end of said polarizing fiber, and
30 said second end of said second sensing fiber being coupled to said detector.

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The present invention provides a Faraday effect current sensor generally comprising a light source, at least two Faraday effect sensing elements each having an input and an output, means for coupling the light source to the input of a first one of the sensing elements, means for coupling the output of the first sensing element to the input of the second sensing element, an optical detector, and means for coupling the output of the second sensing element to the optical detector. In some embodiments, the first and second sensing elements are separate sections of single mode sensing fibers, individually maintained in a generally straight orientation, and the various coupling means comprise polarizing fibers which are fusion spliced to the ends of the sensing fibers. The device may include more than two sensing elements, with additional polarizing fibers connecting the elements in series.

Where the sensing elements are generally straight fiber sections, they may be arranged to form a regular polygon, e.g., an equilateral triangle for a three-element sensor. The sensing fiber sections may be mounted to a rigid substrate and held under tension. Using straight sensing fibers removes the need to anneal the fibers during production, which might otherwise be necessary to reduce birefringence effects. The locations of the splices between the sensing fibers and the polarizing fibers may further be advantageously arranged such that the sensing fibers form a substantially closed path which may be placed about the current-carrying conductor.

The linearity of the sensor response may be improved by selecting an appropriate value of the bias angle of each sensing element. This value, defined by the relative angle between slow axes of two polarizing fibers connected to a given sensing fiber, is optimally equal to

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arctan[$1/\sqrt{2n-1}$] where n is the number of sensing elements. Some embodiments of the present invention may also be adapted for use as a differential current sensor wherein each sensing element is housed in a separate package
5 allowing the elements to be placed about different conductors at a Y-branch or on the same conductor at different locations.

Brief Description of the Drawings

Examples of embodiments of the invention will now
10 be described with reference to the accompanying drawings, wherein:

Figure 1 is a top plan view of a current sensor of an embodiment of the present invention using concatenated field sensors;

15 Figure 2 is a graph depicting the response of a current sensor of an embodiment of the present invention, compared to conventional current sensors;

Figure 3 is a schematic drawing of a differential current sensor according to an embodiment of the present
20 invention; and

Figure 4 is a graph depicting the response of the differential current sensor of Figure 3.

Description of the Preferred Embodiment

With reference now to the figures, and in
25 particular with reference to Figure 1, there is depicted the one embodiment of a fiber-optic current sensor **10** of the present invention. Current sensor **10** is generally comprised of three concatenated field sensors **12**, **14** and **16**, positioned adjacent a current-carrying conductor **18**, and

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several adjoining fibers **20**, **22**, **24** and **26**. Each field sensor is essentially a separate piece of Faraday-sensing fiber, thus first field sensor **12** includes a first sensing fiber **28**, second field sensor **14** includes a second sensing fiber **30**, and third field sensor **16** includes a third sensing fiber **32**. Fiber **20** is the input fiber which carries the conditioned light signal from light source **34** (e.g., a light-emitting diode, laser diode, or superluminescent diode) to first sensing fiber **28**. Fiber **22** interconnects first sensing fiber **12** with second sensing fiber **14**, while fiber **24** interconnects second sensing fiber **12** with third sensing fiber **14**. Fiber **26** is the output fiber which carries the field-modified light signal to detector **36** (e.g., a photodiode).

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The term "concatenated" refers to the manner in which the field sensors are connected in series. In this regard, the current sensor of the present invention contemplates such serial connection of any number of field sensors. That is, there must be at least 2 field sensors and there must also be at least one optical transmission medium interconnecting the field sensors, where the interconnecting medium is not sensitive to the Faraday effect, or else the two field sensors can be connected directly together. There are preferably at least three field sensors, arranged in the depicted (equilateral) triangular shape. If more than three sensors are used, they are also preferably arranged in the shape of a regular polygon. All of the fibers are preferably attached by means of fusing splicing, although other means may suffice (such as mechanical splicing). The splice points are further preferably located so as to form a closed path or loop about conductor 18, to more accurately gauge the surrounding magnetic field. In other words, the location 38 of the splice between input fiber 20 and first sensing fiber 28 is adjacent, or overlapping, the splice between output fiber 26 and third sensing fiber 32. Similarly, the location 40 of the splice between first sensing fiber 28 and connecting fiber 22 overlaps the splice between connecting fiber 22 and second sensing fiber 30, and the location 42 of the splice between second sensing fiber 30 and connecting fiber 24 overlaps the splice between connecting fiber 24 and third sensing fiber 32. The splice points would also preferably overlap in variations with more than three field sensors. In this manner, the concatenated field sensors approximate a perfect current sensor, with any error in measurement being small enough to ignore for many applications.

The fibers may be supported by any suitable means. In the preferred embodiment, the input and output fibers 20 and 26, as well as connecting fibers 22 and 24, are secured by adhering them to mounting blocks 44 using an adhesive. Blocks 44 in turn rest on quartz bars 46, and may also be secured thereon by gluing.

In the embodiment depicted in Figure 1, each of the sensing fibers (field sensors) is a generally straight fiber section, i.e., there might be slight deviations from a perfect line but the fibers are not intended to be curved at all. This avoids the adverse effects of bend-induced birefringence, and also obviates the need for annealing the sensing fibers. Straight sections can also be more easily held stiff (by placing them

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under tension) which further makes them less sensitive to changes in temperature. Nevertheless, the sensing fibers could alternatively be curved to more closely approximate a circle about the conductor but, if so, they are preferably annealed to reduce birefringence effects.

5 By providing separate sections of sensing fibers, coupled to each other, installation is simplified. This construction imparts flexibility to current sensor 10 since its components may move relative to one another during installation, e.g., allowing the sensor to be placed about an existing (endless) cable without cutting the cable. The provision of multiple field sensors may also decrease temperature dependence since the
10 apparent angle of rotation (the main cause of temperature sensitivity in these types of sensors) should follow the rms. average of all of the sensing elements, making the sensor inherently more stable to temperature as the number of field sensors increases.

By designing the sensor so that the magneto-optic rotation is the same in all of the sensing elements and the bias angle is equal to $\arctan[1/\sqrt{(2n-1)}]$, where n
15 is the number of sensing elements, the response of the sensor to current is more linear than conventional magneto-optic current sensors ("bias angle" refers to the polarization angle between the fibers at either end of a sensing fiber, i.e., the relative angle between the slow axes of the polarizing fibers; "magneto-optic rotation" refers to the polarization angle change induced by the target current). This value of the angle is
20 derived by maximizing the linearity of the modulation transfer function. Thus, for the case of $n=3$ (Figure 1), the optimum angle between polarizers is $\arctan(1/\sqrt{5})=24.1^\circ$. The sensitivity of the sensor in this case is $1/\sqrt{(2n-1)}$ and the sensor loss approaches $1/\sqrt{e}$ as n becomes large; here, sensitivity is relative to a standard, single-loop fiber optic current sensor. As shown in Figure 2, the response of the sensor is more linear
25 than with a single-loop fiber optic current sensor, over an extended range of current; line A represents the actual current, line B represents the response from a conventional sensor, and line C represents the response of current sensor 10, where $n=3$. Testing has also shown that the temperature response of the sensor of Figure 1 is essentially limited only by the temperature dependence of the Verdet constant of the fiber
30 material, i.e., nearly perfect theoretical performance; this is the first instance of such performance in a single-detector, non-annealed current sensor. Verdet temperature

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dependence may further be compensated by attaching the fibers at predetermined, favored bias angles as taught in U.S. Patent No. 5,780,847.

The sensor response may vary if the conductor is not located at the center of the sensor (i.e., for Figure 1, the center of the equilateral triangle formed by the sensing fibers), but any deviation in the linearity of the response is negligible provided that the deviation of the conductor location from center is no more than 10% of the circle inscribed by the polygon, so centering of the conductor should not be a critical task. The effects of external magnetic fields on the sensor should similarly be negligible providing that the source of the fields is far from the sensor relative to the sensor size.

The preferred types of fibers used with the present invention are available from 3M Specialty Optical Fibers in West Haven, Connecticut. Each of the fibers **20**, **22**, **24** and **26** are preferably polarizing (PZ) fibers available under part number FS-PZ-4611/200SA (operating wavelength 850 nm). The sensing fibers **28**, **30** and **32** are preferably spun, single mode fibers available under part number FS-SM-4611 (operating wavelength 780 nm). Blocks **44** are preferably quartz plates formed from microscope slides and cut into 1/8" x 1/2" x 1 mm pieces. Alumino-silicate substrate **46** was procured from AC Technologies of Yonkers, New York, under part number ACMA-1100. A suitable glue used to adhere the fibers is the UV cured epoxy NOA #72 from Norland Products of New Brunswick, New Jersey. A suitable glue for adhering blocks **44** to bar **46** is available from Electronic Materials of Danbury, CT, under part number XP1060-930-45-1A. A laser diode optical package for light source **22** was obtained from Point Source Ltd. of Winchester, England, under part number LDS-Pz-3-K-780-0.5-TE. The

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alternative super-luminescent diode contained in a Point Source Ltd. package was manufactured by EG&G Optoelectronics of Vaudreuil, Canada. The preferred detector **34** is the Si photo-detector model number 260 from
5 Graseby Optronics of Orlando, Florida.

Other types of magneto-optic sensing mediums may be used in place of single mode fibers, such as bulk glass, YIG (yttrium-iron-garnet crystal), etc. Other types of polarizers may also be used, including bulk optic polarizers
10 such as

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LAMPOL (available from Sumitomo Electric of Japan) or POLARCOR (available from Corning Glass, of Corning, New York).

The concept of concatenated field sensors may also be applied to a differential current sensor, as shown in Figure 3. Differential current sensor is generally comprised of a light source 52, a first field sensor 54, an input fiber 56 which carries the conditioned light signal from light source 52 to first field sensor 54, a second field sensor 58, a connecting fiber 60 which interconnects first field sensor 54 with second field sensor 58, a detector 62 and an output fiber 64 which carries the field-modified light signal to detector 62. Detector 62 is typically connected to or integrated with signal processing electronics. Differential current sensor 50 measures current by placing the two field sensors along different locations of a conductor Y-branch having an input line 66 and two output lines 68 and 70. In the positions shown in Figure 3, first field sensor 54 is placed about a portion of first output line 68, and second field sensor 58 is placed about a portion of input line 66. The serial connection between field sensors 54 and 58 results in an output which is proportional to the difference between the two currents flowing between the two sensors.

The differential current sensor of the present invention can also be placed on a single conductor, at different locations, to monitor continuity of current. Also, for long distances between sensors, it would be preferable to use standard single-mode fiber to connect the two. In this case the sensor would require a depolarizer somewhere between the two sensing fibers. The sensors must be calibrated and have their sensitivities well-characterized to allow proper differential measurement. Most applications for this architecture would probably be looking for relatively large differences in the currents (e.g., a short located somewhere between the two sensors on the same line).

Field sensors 54 and 58 may be conventional sensing coils, or sensors like sensor 10 which actually include multiple sensing fibers concatenated in a single package. The remaining components are similar to those described above. Unlike prior art differential sensors, differential current sensor 50 uses only a single light source and a single detector. This configuration simplifies use, increases reliability and decreases cost, compared to prior art differential sensors, and alleviates concerns

regarding perturbations to the connecting fibers that could potentially alter the polarization state of the propagating light wave. Figure 4 illustrates how differential current sensor 50 operates. The interaction of the first portion of the conductor with the first sensing element causes a modification of the light wave exiting the first
5 sensing element. The second sensing element, located on the second portion of the conductor, will modify this light wave a second time. If the interactions are identical in magnitude but opposite in sign (identical current flow through both sensors) the end result will be zero modification of the light wave. If the currents in the two portions of the conductor differ, the net modification of the lightwave will be non-zero. This is
10 manifested as a non-zero output signal.

Although the invention has been described with reference to specific embodiments, this description is not meant to be construed in a limiting sense. Various modifications of the disclosed embodiment, as well as alternative embodiments of the invention, will become apparent to persons skilled in the art upon reference to the
15 description of the invention. It is therefore contemplated that such modifications can be made without departing from the spirit or scope of the present invention as defined in the appended claims.

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CLAIMS:

1. A device for sensing electrical current flowing through a conductor, the device comprising:

a light source,

5 a first Faraday effect sensing element having an input and an output,

first means for coupling said light source to said input of said first sensing element,

10 a second Faraday effect sensing element having an input and an output,

second means for coupling said output of said first sensing element to said input of said second sensing element,

an optical detector, and

15 third means for coupling said output of said second sensing element to said optical detector, wherein

said first sensing element includes a first sensing fiber having first and second ends, said first end thereof being coupled to said light source,

20 said second coupling means includes a polarizing fiber having first and second ends, said first end thereof being spliced to said second end of said first sensing fiber, and

25 said second sensing element includes a second sensing fiber having first and second ends, said first end of said second sensing fiber being spliced to said second

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end of said polarizing fiber, and said second end of said second sensing fiber being coupled to said detector.

2. The device of claim 1, further comprising:

5 one or more additional Faraday effect sensing elements, and

means for coupling said additional sensing element(s) in series between said first and second sensing elements, wherein each of said first, second and additional sensing elements include generally straight fiber sections
10 arranged to form a regular polygon.

3. The device of claim 2 wherein:

each of said first, second, third and additional coupling means includes a polarizing fiber,

each of said fiber sections is attached to at
15 least one of said polarizing fibers at different splice locations, and

said splice locations are arranged such that said fiber sections form a substantially closed path which may be placed about the conductor.

20 4. The device of claim 3 wherein:

there are n number of Faraday effect sensing elements each having one of said fiber sections, and

a given one of said fiber sections has a bias angle defined by the relative angle between slow axes of
25 adjacent polarizing fibers, said bias angle being approximately equal to $\arctan[1/\sqrt{(2n-1)}]$.

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5. The device of claim 2 wherein there are three and only three fiber sections, and

said three fiber sections are arranged to form an equilateral triangle.

5 6. The device of claim 1 wherein said first sensing element is secured to a first package adapted to surround a first portion of a conductor, and said second sensing element is secured to a second package adapted to surround a second portion of the conductor, such that the device may be
10 used as a differential current sensor.

7. The device of claim 1 further comprising at least one additional Faraday effect sensing element, for a total of n number of sensing elements, and additional means for coupling said additional sensing elements in series between
15 said first and second sensing elements, wherein:

each of said first, second and additional sensing elements include a sensing fiber,

each of said first, second, third and additional coupling means includes a polarizing fiber, and

20 a given one of said sensing fibers has a bias angle defined by the relative angle between slow axes of adjacent polarizing fibers, said bias angle being approximately equal to $\arctan[1/\sqrt{(2n-1)}]$.

8. The device of claim 1 further comprising one or
25 more additional Faraday effect sensing elements, and additional means for coupling said additional sensing elements in series between said first and second sensing elements, wherein:

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each of said first, second, third and additional coupling means includes a polarizing fiber,

each of said first, second and additional sensing elements include a sensing fiber attached to at least one of
5 said polarizing fibers at different splice locations, and

said splice locations are arranged such that said sensing fibers form a substantially closed path which may be placed about the conductor.

9. The device of claim 1 wherein said sensing fibers
10 are spliced to said polarizing fiber by means of fusion splicing.

10. The device of any one of claims 1 to 9 wherein said first and second sensing fibers are both straight fiber sections.

15 11. The device of any one of claims 1 to 10 wherein said first and second sensing fibers are both non-annealed.

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OTTAWA, CANADA

PATENT AGENTS

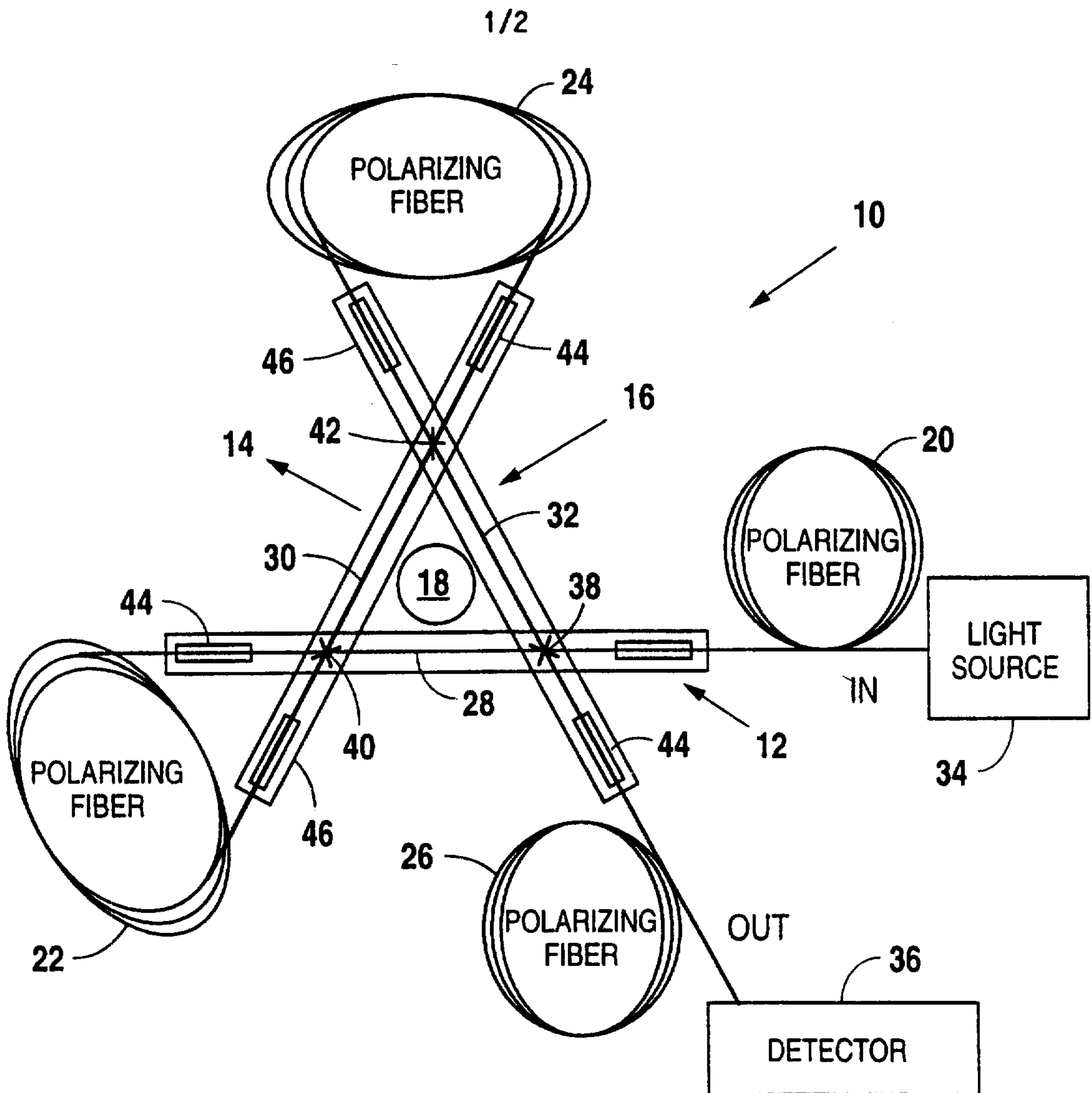


Fig. 1

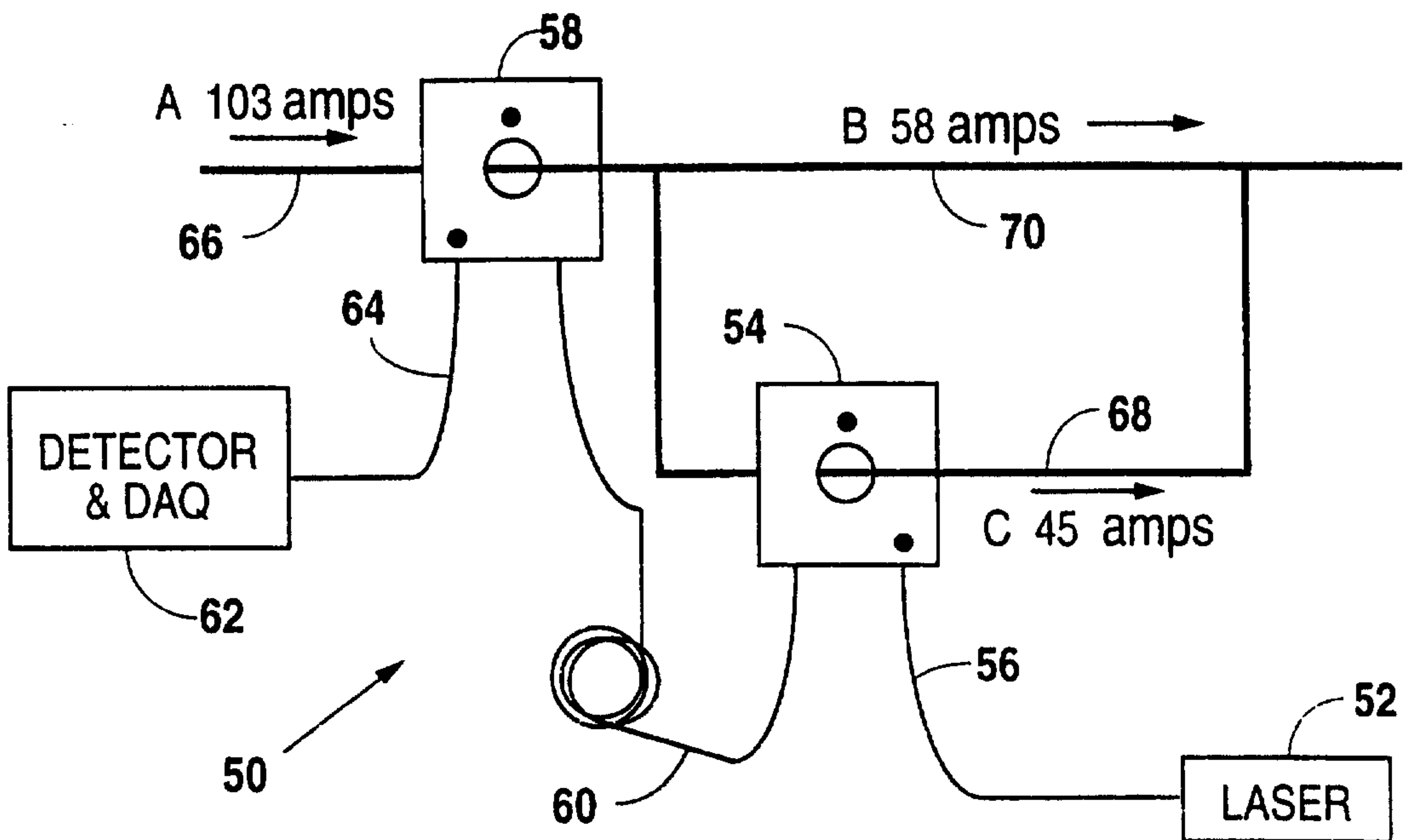


Fig. 3

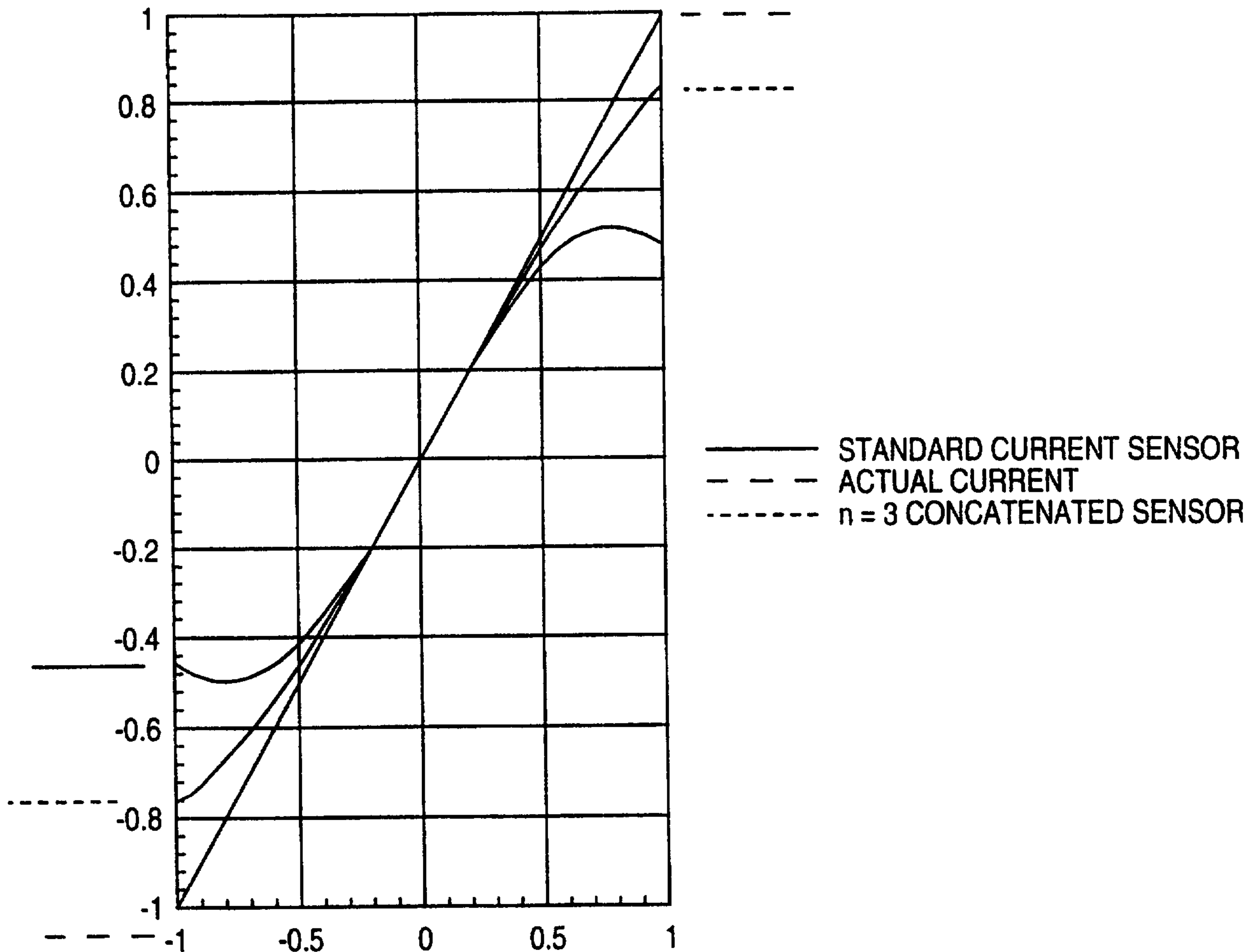


Fig. 2

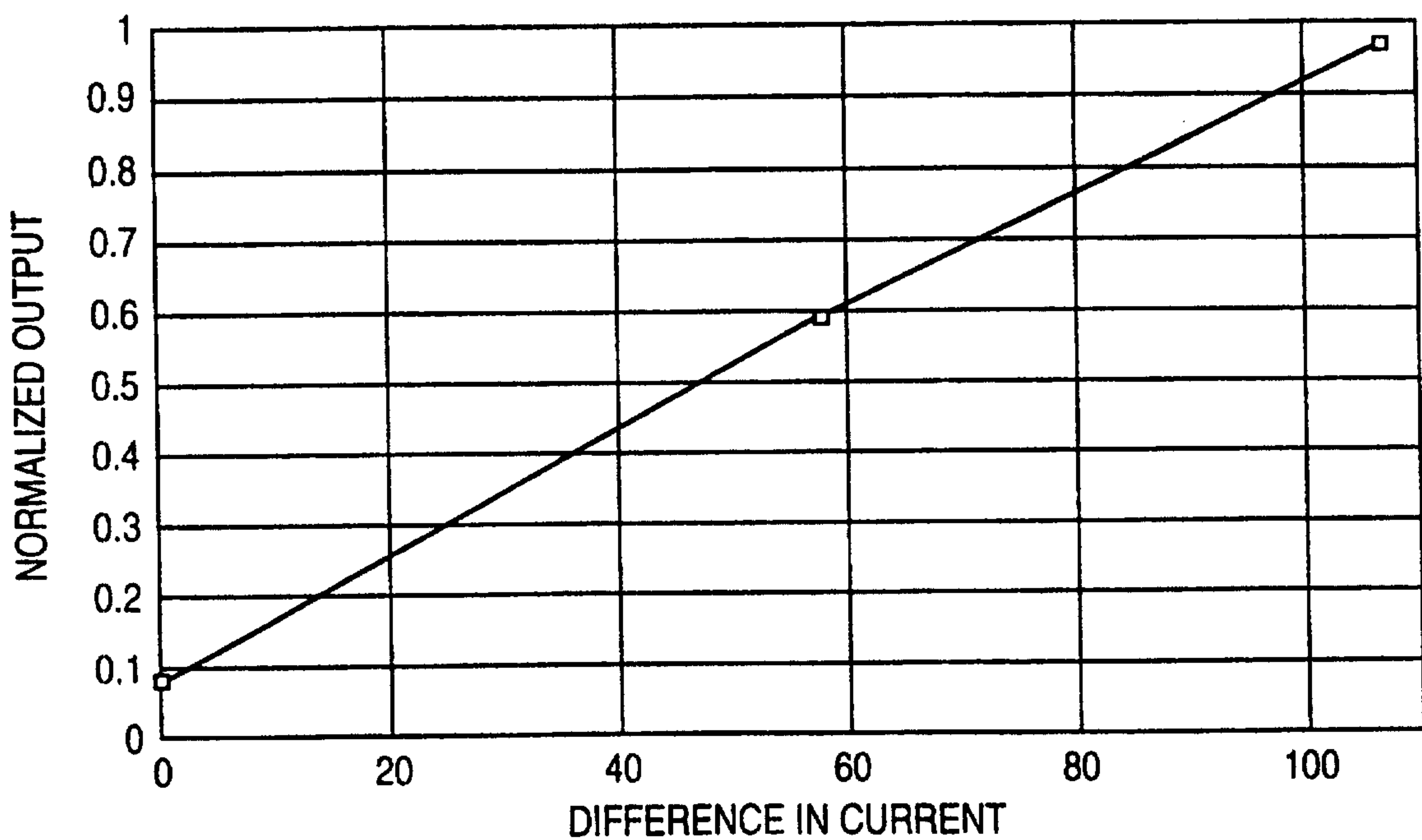


Fig. 4

