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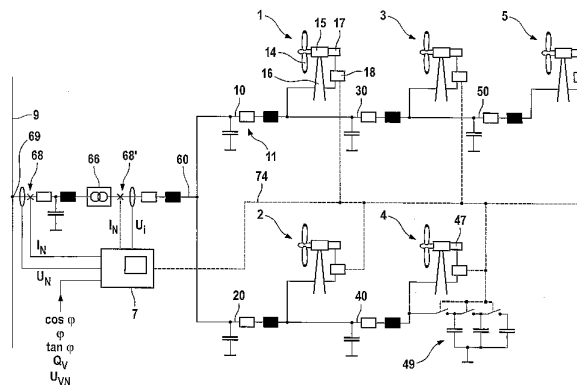
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(54) Title: WIND PARK WITH ROBUST REACTIVE POWER ADJUSTMENT SYSTEM AND METHOD FOR THE OPERA-
TION THEREOF

(54) Bezeichnung: WINDPARK MIT ROBUSTER BLINDELEISTUNGSREGELUNG UND VERFAHREN ZUM BETRIEB



(57) Abstract: The invention relates to a wind park comprising at least two wind power systems (1-5) which are connected to a main line (60) via two connecting lines (10), a linkage point (69) connecting the main line (60) to a power transfer network (9), and a park master (7) for reactive power adjustment, and communication lines (74) for transmitting control signals to the wind power systems (1-5). According to the invention, reactive power adjustment system is embodied in the form of a distributed controller, comprising a main controller (73) on the park master (7), configured in such a way as to determine a set-point voltage (U_{set}) and to produce a signal via the communication lines (74) in order to adjust an overall power coefficient of the power supplied to the energy transmission network, and a sub-controller (184) on the wind energy systems (1-5) which is respectively configured in such a way as to calculate local reactive power setpoint values from the signal for the setpoint voltage, to detect the actual voltage given off by the wind power systems (1-5) and to correct the local reactive power setpoint values upon comparison with the setpoint voltage (U_{set}). The invention also relates to a method for operating said wind park.

(57) Zusammenfassung: Die Erfindung betrifft einen Windpark mit mindestens zwei Windenergieanlagen (1-5), die über Verbindungsleitungen (10) mit einer Hauptleitung (60) verbunden sind, einer Verknüpfungsstelle (69), welche die Hauptleitung (60) mit einem Energieübertragungsnetz (9) verbindet, und einem Parkmaster (7), der zur Blindleistungsregelung ausgebildet ist und Kommunikationsleitungen (74) zur Übermittlung von Steuersignalen an die Windenergieanlagen (1-5)

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Erklärungen gemäß Regel 4.17:

- hinsichtlich der Identität des Erfinders (Regel 4.17 Ziffer i)
- hinsichtlich der Berechtigung des Anmelders, ein Patent zu beantragen und zu erhalten (Regel 4.17 Ziffer ii)
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Zur Erklärung der Zweibuchstaben-Codes und der anderen Abkürzungen wird auf die Erklärungen ("Guidance Notes on Codes and Abbreviations") am Anfang jeder regulären Ausgabe der PCT-Gazette verwiesen.

aufweist. Erfindungsgemäß ist vorgesehen, dass die Blindleistungsregelung als verteilter Regler ausgeführt ist. Er umfasst einen Oberregler (73) am Parkmaster (7), der dazu ausgebildet ist, zur Einstellung eines globalen Leistungskoeffizienten der in das Energieübertragungsnetz (69) abgegebenen Leistung eine Sollspannung (Usoll) zu ermitteln und als Signal über die Kommunikationsleitungen (74) auszugeben, und Unterregler (184) an den Windenergieanlagen (1-5), der jeweils dazu ausgebildet ist, aus dem Signal für die Sollspannung lokale Blindleistungssollwerte zu berechnen, die tatsächlich abgegebene Spannung der Windenergieanlage (1-5) zu erfassen und nach Vergleich mit der Sollspannung (Usoll) die lokalen Blindleistungssollwerte zu korrigieren. Die Erfindung betrifft ferner ein Verfahren zum Betrieb eines solchen Windparks.

Windpark with robust power factor control, and method
for operation

The invention relates to a windpark having at least two
5 wind energy installations, which each have a rotor, a
generator driven by it and a control device, and which
are connected via connecting lines to a main line, a
linking point which connects the main line to a power
transmission network and a parkmaster, which is
10 designed for power factor control and has communication
lines for transmission of control signals to the wind
energy installations. The invention also relates to a
method for operating such a windpark

15 The development in the field of wind energy
installations is characterized by a size trend. This
relates not only to the individual wind energy
installation, but also to windparks, which are formed
from ever greater numbers of wind energy installations
20 that are becoming ever larger. The installed power,
which is therefore rising to a major extent, is
currently leading to difficulties in the on-shore area
where most windparks, and in particular large
windparks, are located, owing to the restricted
25 capacity of the power transmission network. In order to
allow an adequate supply quality to be maintained,
windparks are subject to increasingly more stringent
requirements for network compatibility.

30 One important criterion for safe operation on the
network is voltage stability. This is even more
important for high feed powers, that is to say in
particular for windparks which are connected to high-
voltage and extra-high-voltage networks. It is known
35 that it is advantageous to feed a wattless component
(in particular a capacitive wattless component) into
the network, in order to support the voltage level.
Further important criteria are the transmission
capability of the networks, such as the current load

capacity, connection criteria such as mains flicker, and other effects, such as network losses.

5 It is known for a measurement point for the voltamperes to be provided at a point where the windpark is linked to the network, and for this to be compared with nominal presets for the power factor, by means of a windpark host computer (parkmaster) (EP-A-1 519 040, WO-A-01/73518). The parkmaster uses this to determine
10 power factor or wattless-component nominal values for the individual wind energy installations. These implement the requirements by producing a greater or lesser wattless component. However, this results in a change in the voltages and currents on the lines and transformers in the windpark. A
15 similar concept with distributed regulation has been proposed in EP-A-1 512 869. The known concepts have the disadvantage that, particularly in the case of wind energy installations which are located at the end of a long line in the windpark, undesirable voltage rises can occur, leading to instabilities. This can
20 result in undesirable disconnection of individual wind energy installations, or even damage to converters.

It would be advantageous if the present invention would provide a windpark of the type mentioned initially and an operating
25 method so as to achieve better network support.

The present invention provides in a first aspect a windpark having at least two wind energy installations, which each have a rotor, a generator driven by the rotor and a control device, and
30 which are connected via connecting lines to a main line, a linking point which connects the main line to a power transmission network and a parkmaster which is designed for power factor control and has communication lines for transmission of control signals to the wind energy
35 installations,

characterized in that

the power-factor control is in the form of a distributed
5 regulator, comprising a higher-level regulator at the parkmaster
which is designed to determine a nominal voltage (U_{nom}) in order
to set a global power coefficient for the power which is emitted
to the power transmission network, and to emit the nominal
voltage as a signal via the communication lines, and lower-level
10 regulators at the wind energy installations, which are in each
case designed to calculate a local wattless-component nominal
value from the signal for the nominal voltage, to detect an
actual emitted voltage from the wind energy installations, and
to correct the local wattless-component nominal value after
15 comparison with the nominal voltage (U_{nom}).

Embodiments of the invention are based on the idea of coupling the setting of the desired power coefficient to a voltage maintenance method. Distributed regulation is provided for this purpose. In order to maintain a specific power coefficient, with respect to the power transmission network (network), the parkmaster presets a specific nominal voltage for the individual wind energy installations. This is calculated by the higher-level regulator such that the desired (global) power coefficient is set efficiently for the network. The nominal voltage is emitted as a signal, and is applied via the communication lines to the lower-level regulators for the individual wind energy installations. On the basis of the signal for the nominal voltage, the lower-level regulators autonomously determine local wattless-component nominal values. The generators are operated by means of the control device so as to generate power and a wattless

component in accordance with the requirements. The output voltage is measured, and is fed back to the lower-level regulator in a closed control loop. The control devices for the individual wind energy
5 installations therefore set the desired nominal voltage, as far as possible. The higher-level regulator at the parkmaster determines the actually resultant overall power coefficient, and if necessary corrects the nominal voltage for the lower-level regulators.

10

A number of the expressions that are used will be explained in the following text:

The expression "power coefficient" should be understood
15 as meaning a parameter which describes the wattless component that is required for the respective power. In the relatively narrow sense, this includes the power factor $\cos \varphi$ and its variants $\tan \varphi$, $\sin \varphi$ and the angle φ itself, but in the wider sense also preset
20 values for the wattless component Q_v and a desired network voltage U_{VN} . The latter is expedient in particular for relatively large power stations which are connected directly to the high-voltage network. In
a situation such as this, a so-called wattless-
25 component characteristic is provided in the windpark, by means of which appropriate preset values for the required wattless component and for the power coefficients are determined from the preset value for the desired network voltage.

30

A generator should be understood to be a machine which converts mechanical energy to electrical energy. This covers not only direct-current machines but also single-phase or polyphase alternating-current machines.
35 These machines may also be synchronous or asynchronous machines, which may be single-fed or double-fed. The generator generally, but not necessarily, has a converter. The converter may be in the form of a full

converter or a partial converter. Any desired type may be used,
and in particular the converter may be in the form of a direct
5 converter or an intermediate-circuit converter.

The expression a windpark should be understood as meaning a
total entity which is formed from at least two wind energy
installations and a central control device. The latter is
10 referred to as the parkmaster and monitors the behavior of the
entire windpark with respect to the power supply network to
which the windpark is connected. It influences the operation of
the individual wind energy installations to carry out this
function.

15 The global power coefficient relates to the power emitted from
the windpark as an entity to the network, the local power
coefficient relates to the power emitted from the individual
wind energy installation, possibly including associated
20 compensation installations.

Embodiments of the invention have identified the fact that the
stability of the operating behavior of a windpark can be
improved considerably if the parkmaster presets nominal voltages
25 for the individual wind energy installations, and it is left to
the control devices for the individual wind energy installations
to ensure, on the basis of this, appropriate local wattless
component presets, and their implementation, so as to achieve
the desired power coefficient, overall, at the linking point.

30 Embodiments of the invention result in considerable advantages:

Firstly, the voltage is controlled at the individual wind energy
installations. The maximum possible wattless components of the
35 individual wind energy

installations can thus be called up without any problems. There is no risk of instabilities or damage to components occurring, since no damaging voltage discrepancies occur. Safety reductions are not required, or are required only to a reduced extent.

Secondly, the problem of a new $\cos \varphi$ being calculated in the event of pulsed voltage changes in the network (spikes) but it no longer being possible to transmit this quickly enough to the individual wind energy installations, owing to the restricted communication speed, so that these wind energy installations still attempt to follow the spike using the old $\cos \varphi$, as in the case of the previous concepts, no longer occurs. Thanks to the invention, the individual wind energy installations respond correctly even in the event of rapid processes such as these, and remain at the selected wattless component nominal value.

Thirdly, despite presetting a specific nominal value for the power coefficient at the linking point, the power coefficient for the individual wind energy installations does not need to be predetermined individually and precisely in each case. The respectively correct ratio of the power coefficient to the wattless component is set automatically there, thanks to the lower-level regulator. This also results in the windpark having a robust response to an incorrect response or to an inadequate supply of wattless component of individual wind energy installations.

The embodiments of the invention therefore combine advantages relating to the robust and rapid response, in an elegant form.

The higher-level regulator expediently has a compensation device for the connecting lines to the wind energy installations. This makes it possible to

take account of influences caused by the connecting lines, possibly including the main line and/or intermediate transformers, in the calculation of the nominal voltage. This is important because changes in
5 the (nominal) voltages on the connecting lines also affect other relationships relating to the voltage drop over the connecting lines etc.

According to one preferred embodiment, the higher-level
10 regulator has a correction-value memory which contains individual correction values for the wind energy installations, in particular section parameters, for the connecting lines. This makes it possible to take account of differences in the (complex) section
15 parameters. The nominal value can be individually matched to the respective transmission line, with its electrical parameters, for each wind energy installation. This is a major advantage, particularly in the case of windparks having a plurality of wind
20 energy installations arranged in series on one line. Other correction values can also be included individually for each wind energy installation. This results in better control of the individual wind energy installations even in the event of an electrically
25 highly different behavior of the individual wind energy installations with the parkmaster.

It will frequently be adequate to store predetermined values in the correction-value memory. However, an
30 adaptive identification device is advantageously provided for the individual correction values, in particular the section parameters, optionally also interacting with the compensation device. This means that there is no longer any need for the user to
35 actively preset values. This is a considerable advantage, especially in the case of windparks which are difficult to define because of their topology. Furthermore, this results in the correction values

being automatically matched to gradual changes resulting from environmental influences or component ageing.

5 The linking point is expediently arranged on the high-voltage network, and is connected to the main line via a high-voltage transformer. This is a good approach for network connection, particularly for windparks with a high installed rating. However, it results in the
10 disadvantage that high-voltage lines have a so-called natural rating for optimum operation because their capacitances are not negligible - in contrast to the situation with medium-voltage lines. Any discrepancies must be compensated for as appropriate by the wattless
15 component. It is advantageous for the measurement point to be arranged on the high-voltage side of the transformer, for this purpose. However, this involves complex and expensive high-voltage measurement devices. It is therefore preferable for the measurement devices
20 to be arranged on the main-line side of the high-voltage transformer. Provided that the transmission characteristics of the high-voltage transformer are known, this makes it possible to use lower-cost sensors.

25 The distributed regulator is preferably designed such that its control response has a time constant which is considerably longer than that of pulsed, short voltage fluctuations (voltage transients). This has the
30 advantage that pulsed short voltage fluctuations have no influence on the regulator. Furthermore, this makes it possible to design the lower-level regulator such that it can react quickly to disturbances. This maintains a robust windpark operational response even
35 in disturbed conditions.

In one proven embodiment, the distributed regulator has a limiting device for the nominal voltage. This ensures

that excessively high nominal voltages do not cause any damage to the generator or its converter. This is particularly important for those wind energy installations which are connected to a relatively long
5 connecting line. In this case, the complex impedance of the connecting line results in the voltage level not being the same as that of the parkmaster, and in particular it may be higher. Without limiting, damage could easily occur, and this is prevented by the
10 limiting. The limiting device is expediently provided at each lower-level regulator. This allows improved individual matching to the individual wind energy installations. However, an arrangement can also be provided at the higher-level regulator.

15 A return channel leading from the lower-level regulator to the higher-level regulator is expediently provided for signal feedback, transmitting any overload signal emitted from the lower-level regulator. This results in
20 a signal being passed to the higher-level regulator when a wind energy installation cannot supply a desired wattless component. The higher-level regulator is therefore able to implement appropriate compensation measures with respect to the other wind energy
25 installations.

Additional phase shifters are preferably provided, and may be designed in various ways, that are known per se. Capacitor banks at the wind energy installations have
30 been proven. On the one hand, they result in an increased control range for wattless-component provision. On the other hand, it is possible to reduce the frequency at which the distributed regulator has to switch. This allows the windpark to be operated in a
35 material-conserving manner.

The present invention provides in a second aspect a method for operation of a windpark having at least two wind energy
5 installations, which each have a rotor, a generator driven by the rotor and a control device, and which are connected via connecting lines to a main line, a linking point which connects the main line to a power transmission network and a parkmaster, which is designed for power factor control and has communication
10 lines for transmission of control signals to the wind energy installations,

characterized by

15 power-factor control by means of a distributed control system, comprising
a higher-level regulator at the parkmaster for setting a nominal voltage (U_{nom}) in order to set a global power coefficient for the power which is emitted to the power transmission network,
20 and to emit this as a signal via the communication lines, and a lower-level regulator at the wind energy installations, which is in each case designed to calculate local wattless-components nominal values from the signal for the nominal voltage, to detect the actual emitted voltage from the wind energy
25 installation, and to correct the local wattless-component nominal values after comparison with the nominal voltage (U_{nom}).

The invention will be explained in more detail in the following text with reference to the drawing, in which one advantageous
30 exemplary embodiment is illustrated, and in which:

figure 1 shows a schematic illustration of one exemplary embodiment of a windpark according to the invention, with a parkmaster and wind energy installations;

figure 2 shows a schematic illustration of the parkmaster with
a higher level regulator based on the exemplary
embodiment illustrated in figure 1; and

figure 3 shows a schematic illustration of a control device
for the wind energy installation, with a lower-level
regulator based on the exemplary embodiment
illustrated in figure 1.

Figure 1 illustrates one exemplary embodiment of a windpark
according to the invention, which has a total of five wind
energy installations (1-5) and one central host computer
(parkmaster) 7 in the illustrated exemplary embodiment. The wind
energy installations 1-5 are connected to one end of a main line
60 via connecting lines 10, 20, 30, 40, 50.

The design of the wind energy installations 1-5 will be
explained using the wind energy installation 1 as an example.
The wind energy installation 1 has a rotor 14 which is arranged
on a machine housing 15 at the top of a tower 16 such that it
can rotate. The rotor 14 drives a generator (not illustrated).
This is preferably a

double-fed asynchronous generator, although other types are also possible. The generator is connected to a converter 17, which converts the electrical power produced by the generator to three-phase electrical power at a fixed frequency (network frequency). The operation of the wind energy installation 1 is monitored by a control device 18, which controls the individual components of the wind energy installation 1 via suitable control lines (which are not illustrated).

10 A transformer (not illustrated) is also provided for the wind energy installation 1, and transforms the voltage emitted from the converter 17 to a higher level.

15 The electrical energy which is produced by the wind energy installation 1 is passed to the main line 60 via the connecting line 10, which is shown with its electrical equivalent circuit in figure 1. This has in each case one inductance, impedance and capacitance, illustrated as a concentrated element. These are annotated in a combined form as the complex impedance 11. The connecting line 10 of the wind energy installation 1 is directly connected to the one end of the main line 60. That wind energy installation 3 that is the next arranged on this branch is connected to the main line 60 via its connecting line 30 and then via the connecting line 10. The wind energy installation 5 is connected in a corresponding manner to the main line 60 via its connecting line 50 and the connecting lines 30 and 10.

A power distribution network (network) 9 of a power supply organization is connected to the other end of the main line 60 via a linking point 69. The linking point 69 is used for feeding in the electrical power that is produced by the wind energy installations 1-5 and is fed to the main line 60. Depending on the configuration of the windpark, the main line 60 may

have a considerable length. This may be several kilometers, or even more than 50 km, in the case of offshore windparks. In the illustrated exemplary embodiment, the network 9 is a high-voltage network. A
5 high-voltage transformer 66 is provided in order to raise the voltage, which is at the medium-voltage level, on the main line 60.

The parkmaster 7 is provided in order to monitor the
10 electrical power fed in to the network 9, and carries out a control function for the wind energy installations 1-5. The parkmaster 7 comprises a host computer 70, an input/output unit 71 and a higher-level
15 regulator 73 as a component of the distributed control system according to the invention. Control strategies for the windpark are implemented in the host computer 70 while, in addition, it has an input 72 for control instructions from the operator of the power supply
20 organization network 9. This is illustrated in figure 2, in the form of an example, by an input for a desired power coefficient (φ , $\cos \varphi$, $\tan \varphi$, wattless-component Q or network voltage preset value U_{VN}). If, as is normal in the case of high-voltage networks, the power
25 coefficient is set by means of the network voltage preset value, a wattless, component characteristic module 75 is also provided. This contains a predeterminable characteristic, which relates the preset voltage to a wattless component level.
Furthermore, the parkmaster 7 is connected to
30 measurement devices 68 for the power emitted to the network, and/or for the power coefficient. In the illustrated exemplary embodiment, these measurement devices 68 comprise a voltage sensor for the network voltage U_n and a current sensor for the current I_n fed
35 into the network. However, it is also possible to provide for the measurement device to be partially (68') or completely arranged on the main-line side of the high-voltage transformer 66. This has the advantage

that it is possible to use simpler sensors, designed for the medium-voltage level.

The major components of the distributed control system according to the invention are the higher-level regulator 73 at the parkmaster 7, and the lower-level regulators of the individual wind energy installations 1-5. The higher-level regulator 73 uses the desired power coefficient to determine a value for the nominal voltage U_{nom} on the main line 60. This value is transmitted via the input/output device 71 and the communication lines 74 to the lower-level regulators for the control devices for the individual wind energy installations 1-5. The design and method of operation of the control devices will be explained in the following text using the example, as illustrated in figure 3, of the control device 18 for the wind energy installation 1.

The control device 18 has an input/output unit 181, an operational control unit 180, a limiting device 182 and a lower-level regulator 184 as well as a converter drive 189. The input/output unit 181 is connected to the communication lines 74. Presets and control commands transmitted from the parkmaster 7 are passed, depending on the signal, to the operational control unit 180 and/or the lower-level regulator 184. The signal for the nominal voltage U_{nom} is passed via the limiting device 182. This is designed to limit excessive values to a level that is still permissible. Furthermore, it is applied via a subtraction point 183 to the lower-level regulator 184, which uses the signal for the nominal voltage U_{nom} to calculate suitable drive signals for the converter drive 189. The drive signals are modified, if necessary, by suitable measures, for example filters, in order to avoid mutual interference between the lower-level regulators for a plurality of wind energy installations. In the

illustrated exemplary embodiment, the nominal voltage is passed on as a signal for the output voltage of the converter 17 (other variables may also be used, for example the wattless component). The operational control unit 180 in the exemplary embodiment emits a signal for the nominal power to the converter driver 189. The converter 17 is operated by the converter drive 189, in a manner known per se, in accordance with the selected drive signals. At its output, it produces electrical power P and wattless component Q for an output voltage U on the basis of the selected values, and feeds these to the connecting line 10. The output voltage is measured, and is fed back to the subtraction point 183. Any discrepancies from the nominal value Unom can thus be regulated out - the wind energy installations 2-5 in the windpark are operated in a corresponding manner.

The connecting lines 10, 20, 30, 40, 50 have complex impedances. Changes in the voltage emitted from the wind energy installations also lead to changes in the voltage drop over the connecting lines 10, 20, 30, 40, 50. In order to compensate for disturbance influences resulting from this, a compensation device 77 is provided at the upper-level regulator 73. This varies the calculated nominal voltage on the basis of the voltage drop expected across the complex impedance 11. This reduces the influence of the connecting lines 10, 20, 30, 40, 50 on the distributed control system. Since the individual wind energy installations 1-5 are arranged at different locations on the connecting lines, each of the wind energy installations have different complex impedances with respect to the main line 60. This leads to the voltage relationships at individual wind energy installations 1-5 differing from one another. This results in a high voltage drop over the connecting lines 10, 30, 50, in particular for the wind energy installation 5 that is located at the rear.

This conceals the risk of the output voltage from the wind energy installation 5 reaching an unacceptably high value, if an identical value is preset for the nominal voltage U_{nom} . A correction-value memory 78 is provided in order to counteract this. The voltage drops which result from the different complex impedances of the connecting lines 10, 20, 30, 40, 50 are individually taken into account in this memory for each of the wind energy installations 1-5. The appropriate correction value can thus be used to modify the nominal voltage U_{nom} so as to compensate for the influence of the respective connecting line to the individual wind energy installation. The respective correction values are determined by an adaptive identification device 76, using an identification method or methods, and are written to the correction-value memory 78. This results in valid correction values being determined even when the conditions of the connecting lines are varying slowly (for example as a result of ageing or environmental influences) or it is difficult to calculate them, because of the topology.

Capacitor banks 49 are optionally arranged at the wind energy installations. Only one, for the wind energy installation 4, is illustrated in figure 1, for clarity reasons; they can be provided in corresponding form at the other wind energy installations as well. These offer an additional capability for the provision of a wattless component. This widens the operating range for the distributed control system according to the invention. Furthermore, the capacitor banks 49 allow rough presetting of the wattless component. A phase-shifter switching device 79 is provided at the higher-level regulator 73 for operation of the capacitor banks 49, and may be in the form of a low-pass or moving-average filter. This means that the number of switching processes to be carried out by the converter 47 for matching of the wattless component is reduced. This has

a positive effect on the system response (in particular mains flicker) and life.

Patent Claims

- 5 1. A windpark having at least two wind energy installations,
which each have a rotor, a generator driven by the rotor
and a control device, and which are connected via
connecting lines to a main line, a linking point which
10 connects the main line to a power transmission network and
a parkmaster which is designed for power factor control
and has communication lines for transmission of control
signals to the wind energy installations,

characterized in that
15
the power-factor control is in the form of a distributed
regulator, comprising a higher-level regulator at the
parkmaster which is designed to determine a nominal
voltage (U_{nom}) in order to set a global power coefficient
20 for the power which is emitted to the power transmission
network, and to emit the nominal voltage as a signal via
the communication lines, and lower-level regulators at the
wind energy installations, which are in each case designed
to calculate a local wattless-component nominal value from
25 the signal for the nominal voltage, to detect an actual
emitted voltage from the wind energy installations, and to
correct the local wattless-component nominal value after
comparison with the nominal voltage (U_{nom}).
- 30 2. The windpark as claimed in claim 1,
characterized in that
the higher-level regulator has a compensation device for
the connecting lines to the wind energy installations.
- 35 3. The windpark as claimed in claim 1 or 2,
characterized in that

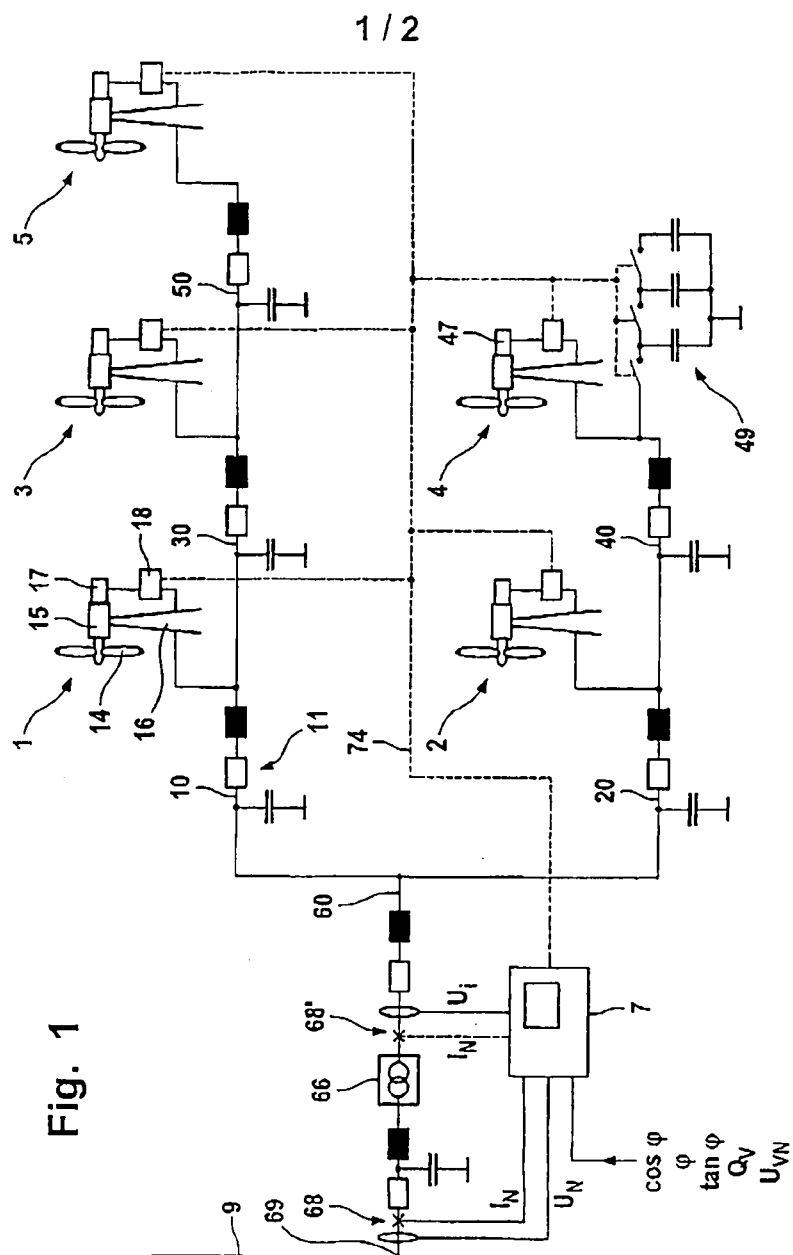
- the higher-level regulator has a correction-value memory which, in particular, contains individual correction values for the wind energy installations, in particular section parameters for the connecting lines.
- 5
4. The windpark as claimed in claim 2 or 3, characterized in that an adaptive identification device is provided for the compensation device and/or for the individual correction values.
- 10
5. The windpark as claimed in any one of the preceding claims characterized in that
- 15 the linking point is arranged on the high voltage network and is connected to the main line via a high-voltage transformer.
6. The windpark as claimed in claim 5, characterised in that
- 20 the measurement device is arranged on the main-line side of the high-voltage transformer.
7. The windpark as claimed in any one of the preceding claims, characterized in that
- 25 the control response of the distributed regulator has a time constant which is considerably longer than that of voltage transients.
8. The windpark as claimed in any one of the preceding claims, characterized in that the distributed regulator has a limiting device for the normal voltage (U_{nom}).
- 30
9. The windpark as claimed in claim 8, characterized in that
- 35 the limiting device is provided at least one of the lower-level regulators.

10. The windpark as claimed in any one of claims 1 to 9,
5 characterized in that additional passive phase shifters
are provided.
11. The windpark as claimed in claim 10, characterized in that
10 capacitor banks are provided as phase shifters for the
wind energy installations.
12. A method for operation of a windpark having at least two
wind energy installations, which each have a rotor, a
generator driven by the rotor and a control device and
15 which are connected via connecting lines to a main line, a
linking point which connects the main line to a power
transmission network and a parkmaster, which is designed
for power factor control and has communication lines for
transmission of control signals to the wind energy
installations,
20
characterized by

power-factor control by means of a distributed control
system, comprising
25 a higher-level regulator at the parkmaster for setting a
nominal voltage (U_{nom}) in order to set a global power
coefficient for the power which is emitted to the power
transmission network, and to emit this as a signal via the
communication lines, and a lower-level regulator at the
30 wind energy installations, which is in each case designed
to calculate local wattless-components nominal values from
the signal for the nominal voltage, to detect the actual
emitted voltage from the wind energy installation, and to
correct the local wattless-component nominal values after
35 comparison with the nominal voltage (U_{nom}).

13. A windpark or a method substantially as herein described with reference to the drawings.

Fig. 1



2 / 2

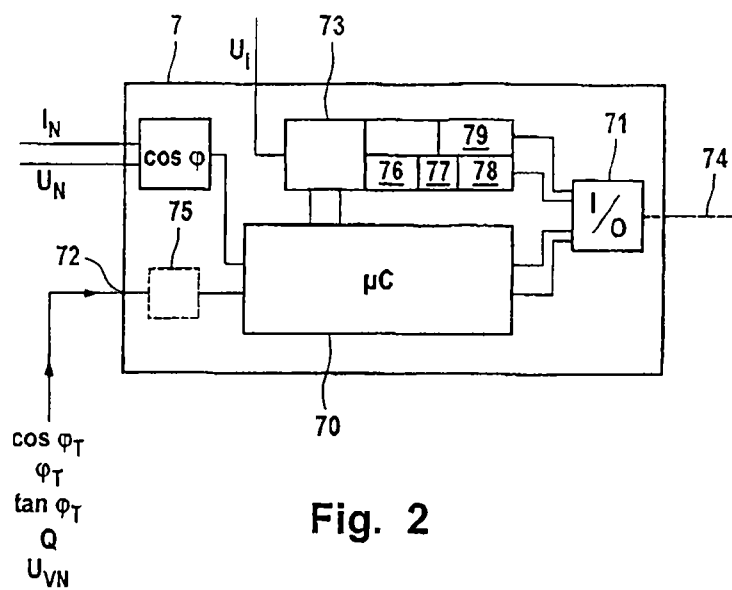


Fig. 2

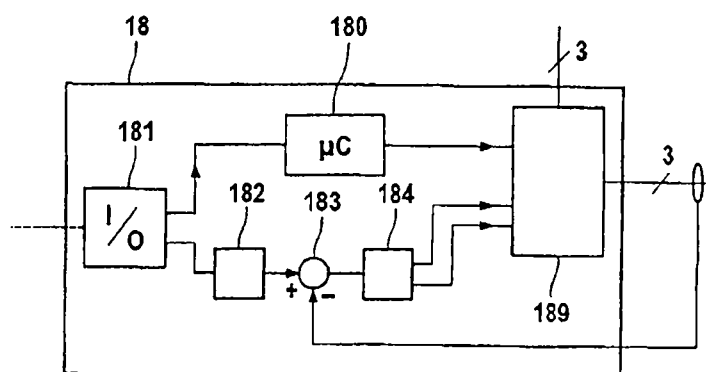


Fig. 3