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Collier et al.

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(45) **Date of Patent: *Apr. 4, 2017**

(54) **AXILINEAR SHAPED CHARGE ARRAY**

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(73) Assignee: **Innovative Defense, LLC**, Smithville, TX (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

This patent is subject to a terminal disclaimer.

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(22) Filed: **Jun. 2, 2016**

(65) **Prior Publication Data**

US 2016/0349021 A1 Dec. 1, 2016

Related U.S. Application Data

(63) Continuation of application No. 14/724,497, filed on May 28, 2015, now Pat. No. 9,360,222.

(51) **Int. Cl.**

F42B 1/00	(2006.01)
F42B 1/028	(2006.01)
F42B 1/036	(2006.01)
F42C 19/12	(2006.01)

(52) **U.S. Cl.**

CPC ***F42B 1/028*** (2013.01); ***F42B 1/036*** (2013.01); ***F42C 19/12*** (2013.01)

(58) **Field of Classification Search**

USPC 102/306, 475, 476, 311, 310, 307; 166/298; 175/4.6

See application file for complete search history.

(56) **References Cited**

U.S. PATENT DOCUMENTS

4,753,170 A *	6/1988	Regalbuto	C06C 5/04 102/200
9,360,222 B1 *	6/2016	Collier	F42B 1/028
2005/0126420 A1 *	6/2005	Givens	F42B 1/02 102/310

* cited by examiner

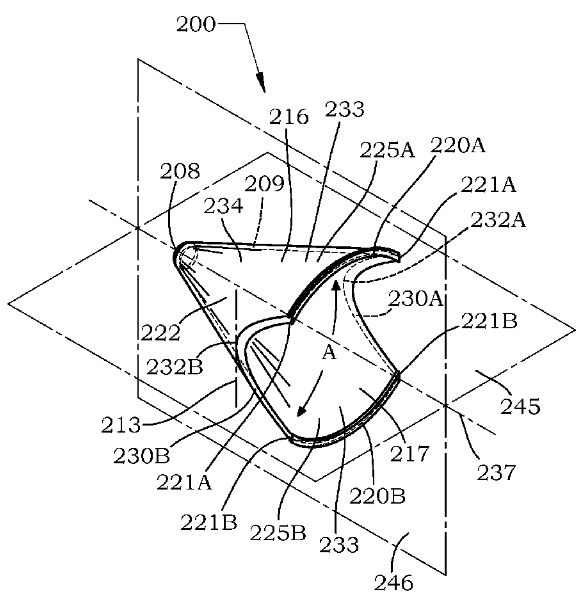
Primary Examiner — J. Woodrow Eldred

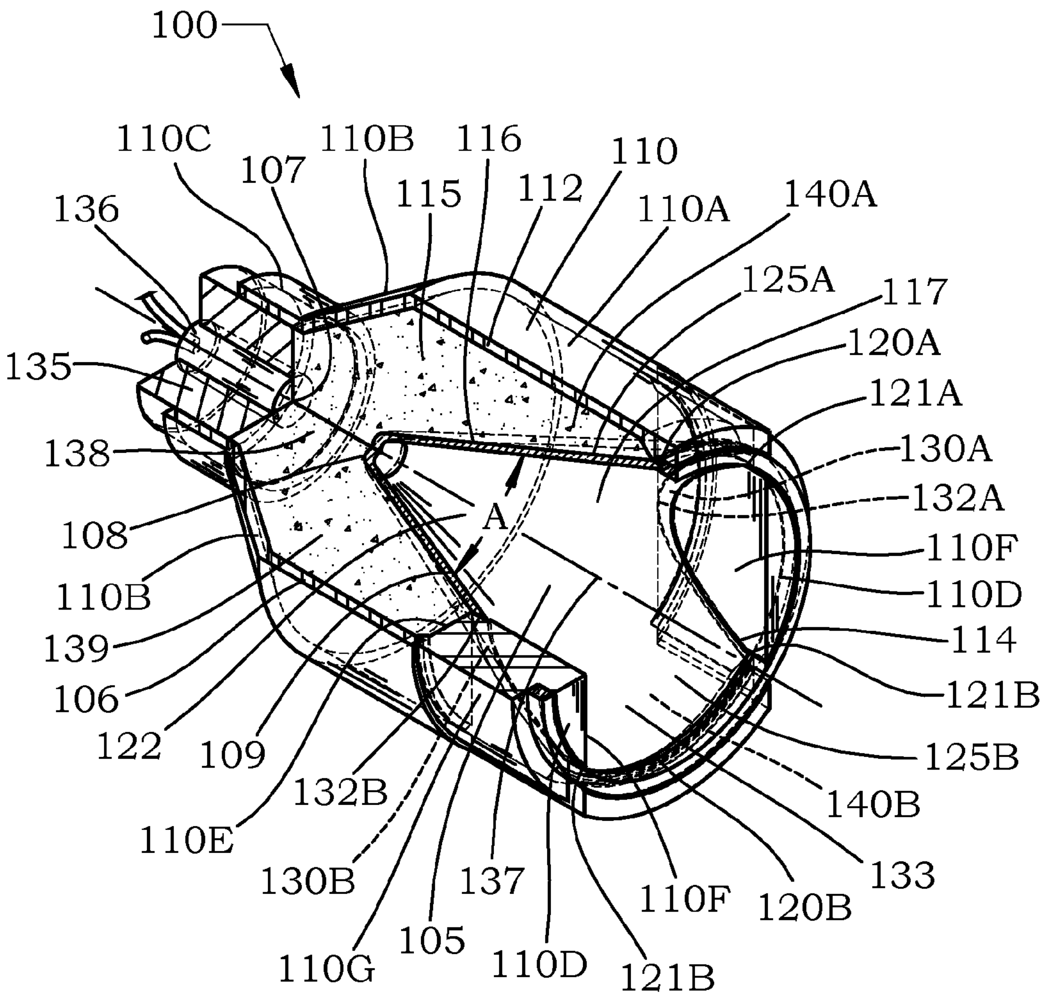
(74) *Attorney, Agent, or Firm* — Hemingway & Hansen, LLP; D. Scott Hemingway

(57) **ABSTRACT**

This invention is a unique arrangement of shaped charge devices in an array to produce a patterned or arranged explosive pattern in a target area. The Axilinear design, in a plural array configuration, solves the limitations of a smooth walled circular linear liner by having opposing corrugations or flutes that have sufficient curvature to converge the liner material so as to obtain ductile Munroe jetting, longer jets, and higher velocities. The individual shaped explosive devices have a liner that produces a single combination jet consisting of a forward rod portion and rearward flattened spade shaped portion, this jet has a velocity gradient form tip to tail. This Axilinear device will produce a combination jet, consisting of a rod forward portion, followed by and connected to a planar symmetric wide spade shaped rear portion.

38 Claims, 16 Drawing Sheets

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110B
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139
121B
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110E
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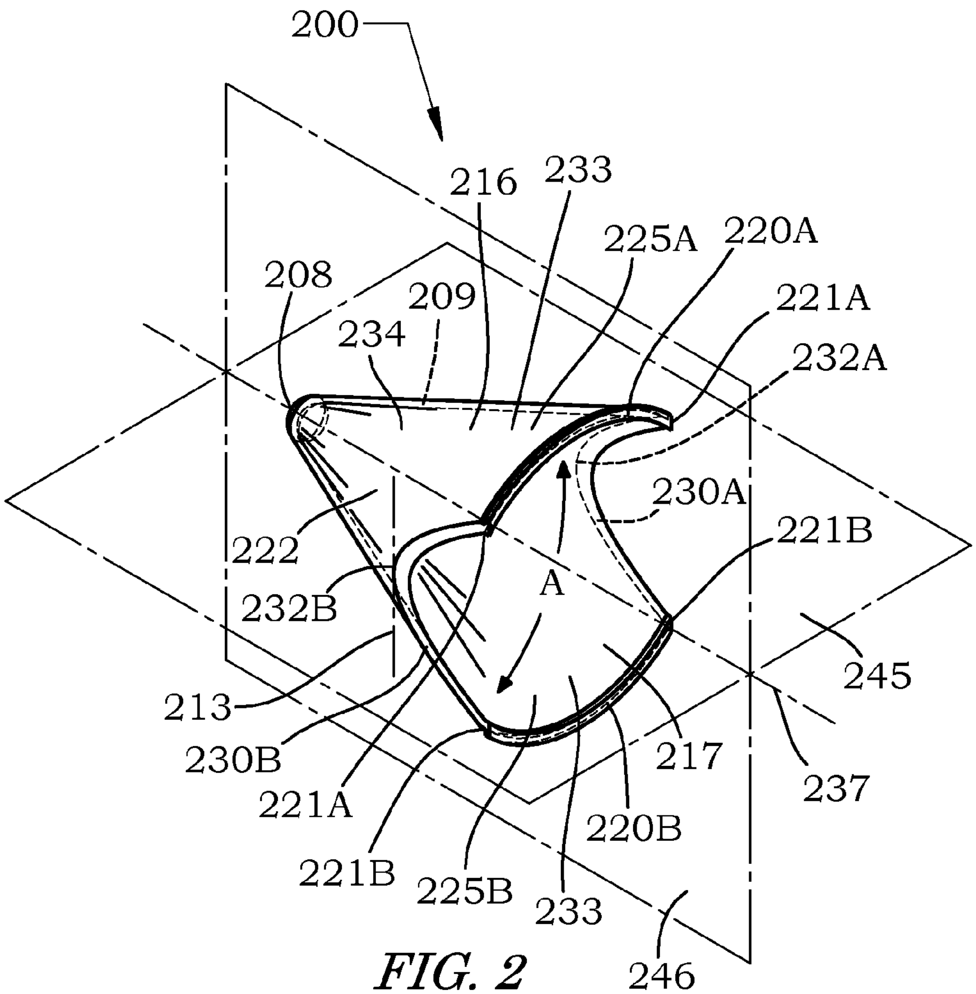
110F
120B
105
110D
121B
110G

FIG. 1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221A
220B
221B
225B
233
246

FIG. 2

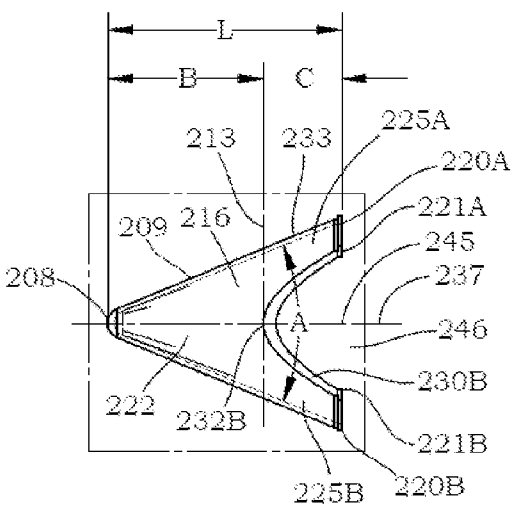
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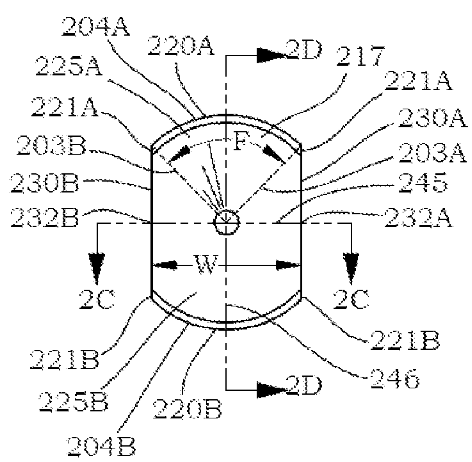
FIG. 2A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2D
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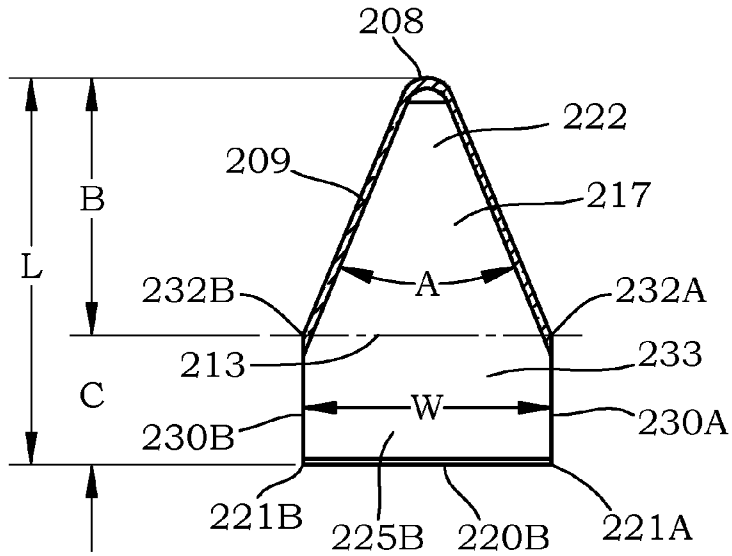
FIG. 2B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221A

FIG. 2C

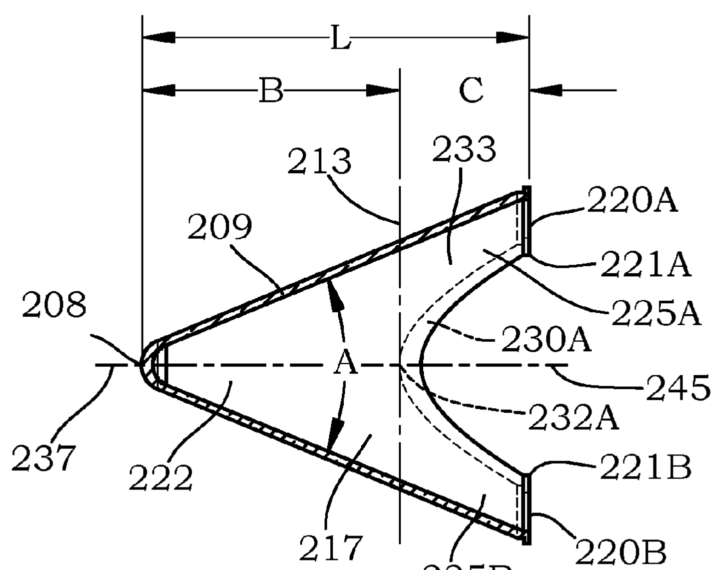
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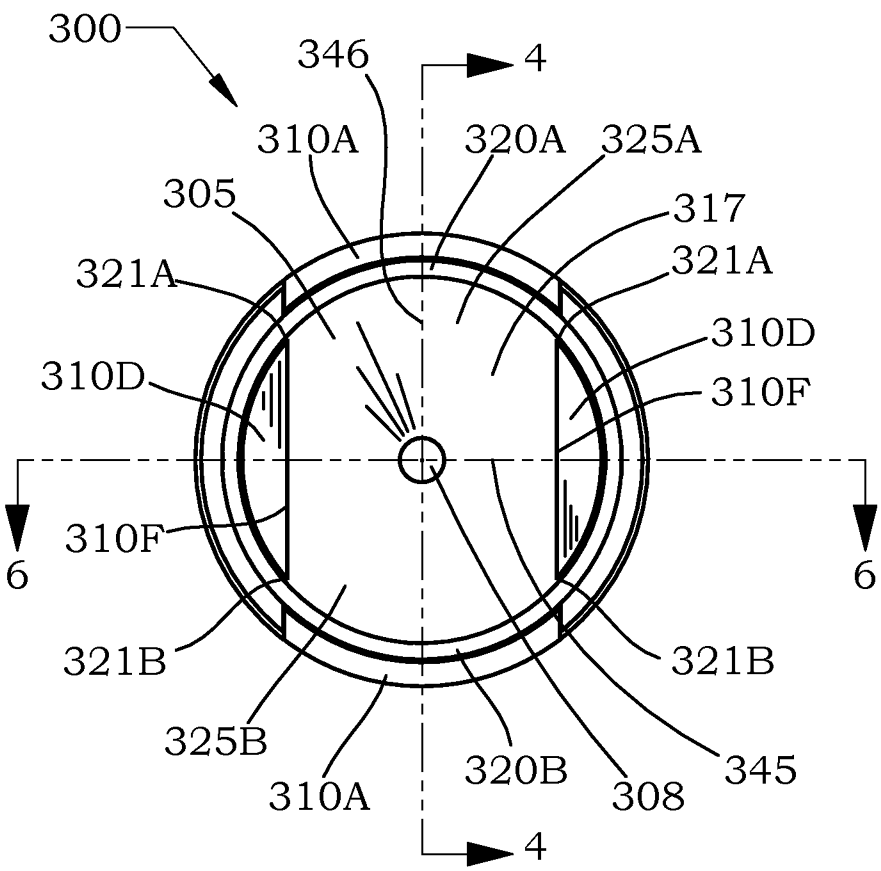
FIG. 2D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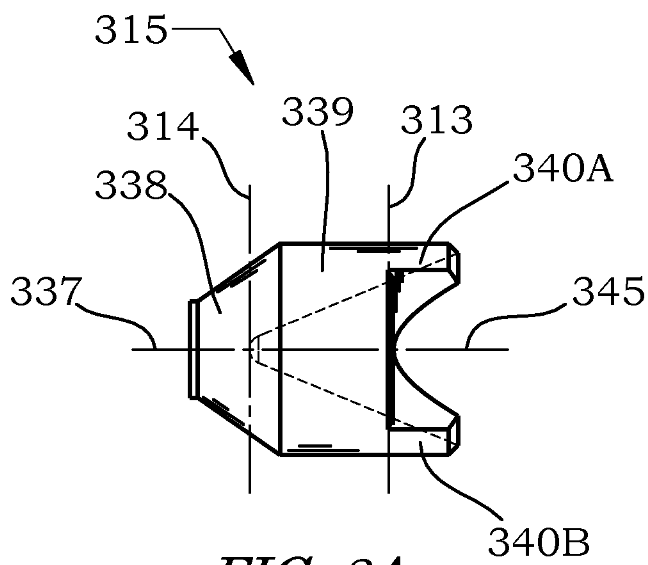
320B
308
345
4

FIG. 3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340B

FIG. 3A

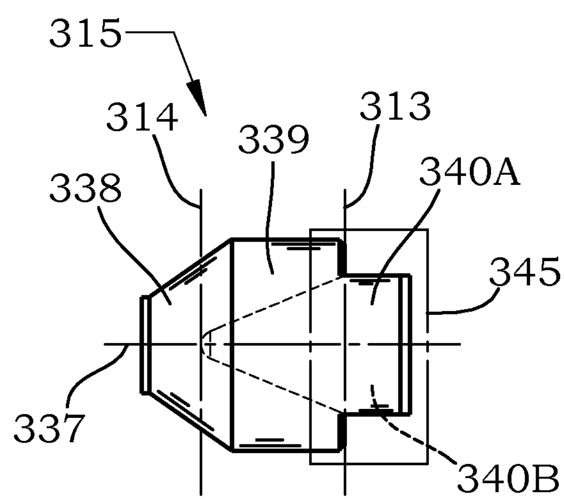
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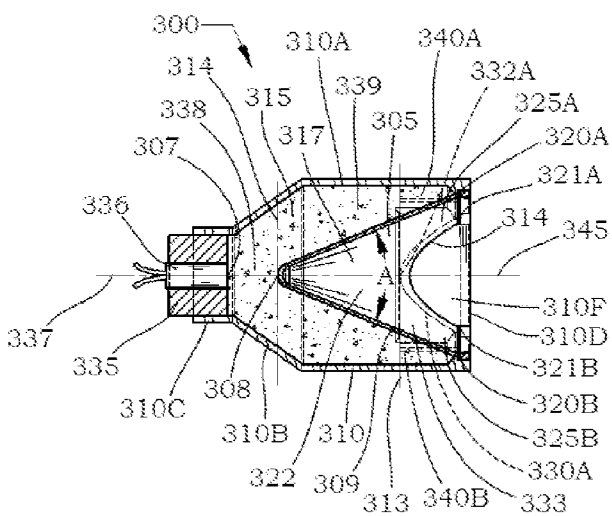
FIG. 3B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310B
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340B
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330A
325B
320B
321B
310D
310F
A

FIG. 4

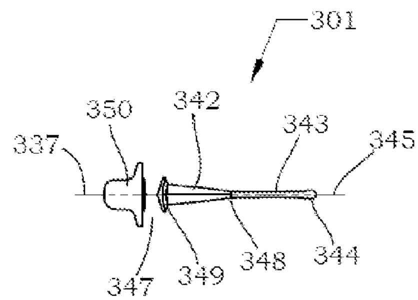
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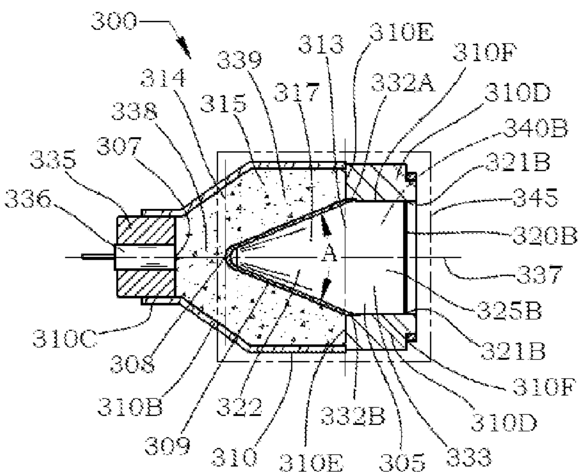
FIG. 5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340B
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321B
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320B
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321B
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332B
310D
309
310
310E
305
333

FIG. 6

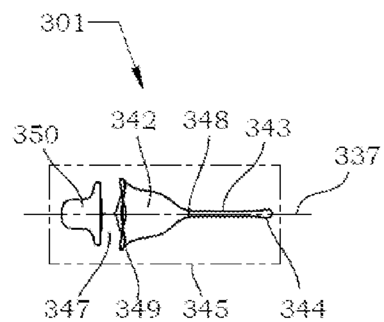
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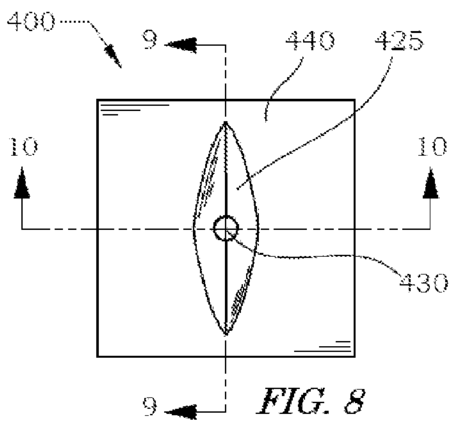
FIG. 7



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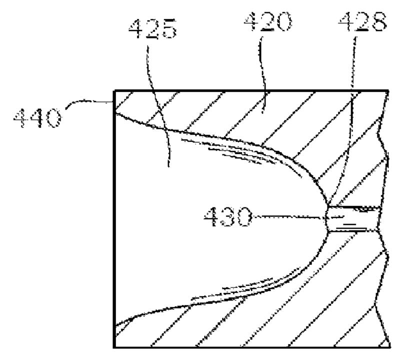

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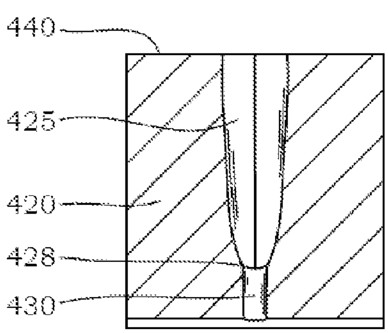

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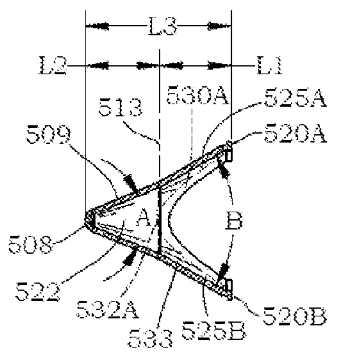

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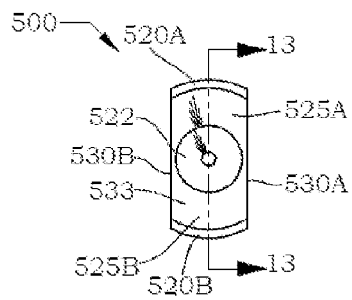

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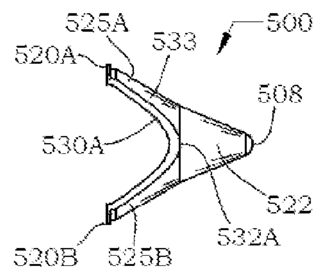

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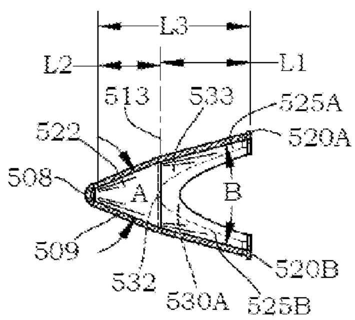

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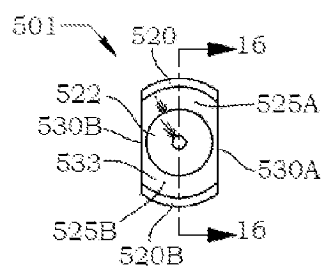

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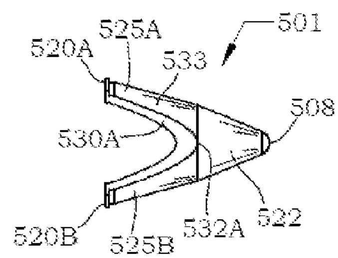

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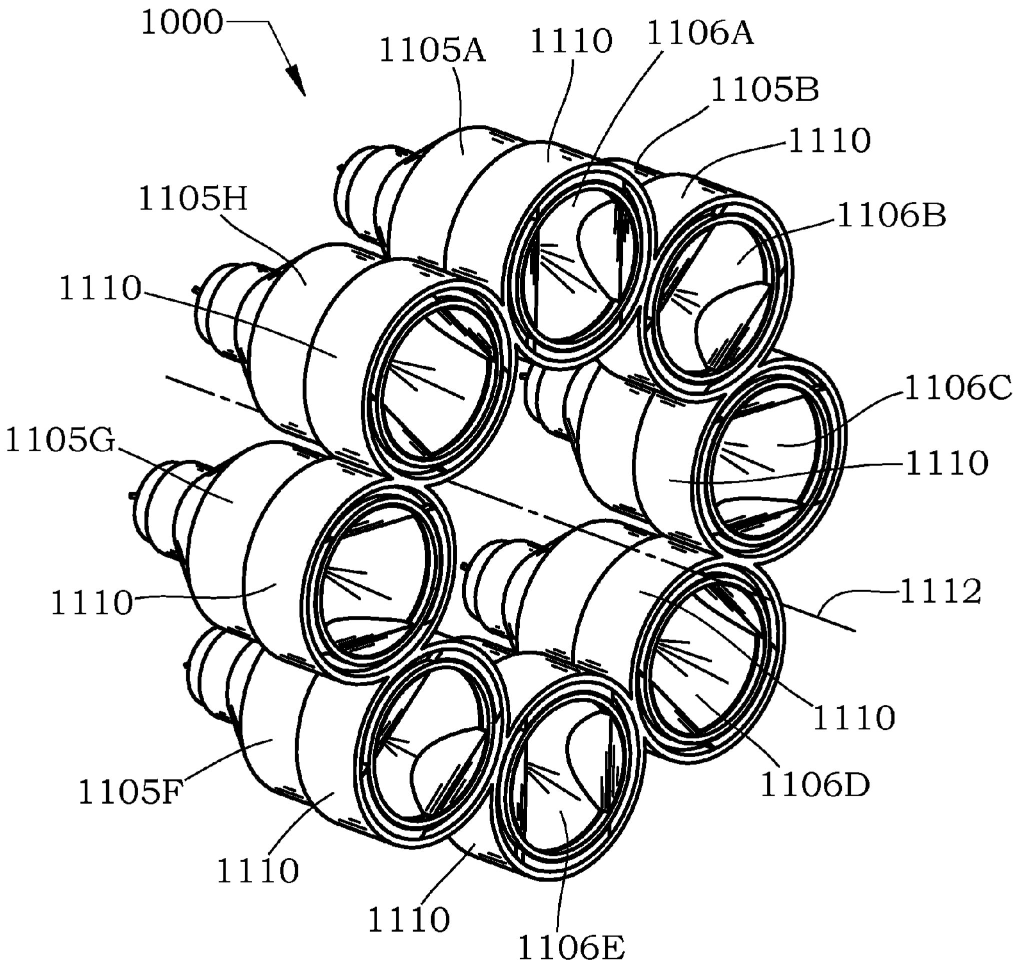
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1106A
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1105H
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1112
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1106D
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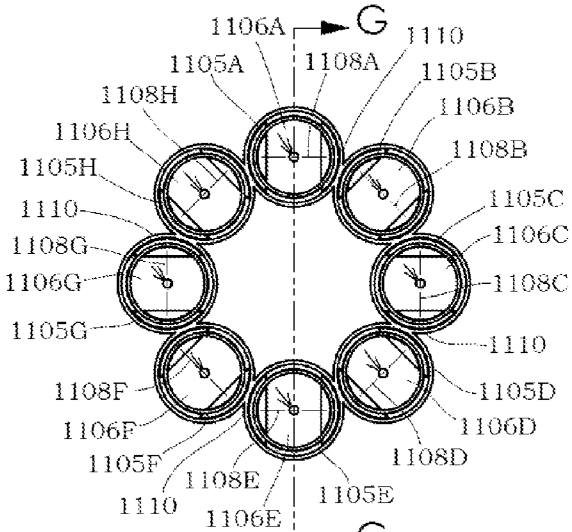
1110
1106E

FIG. 18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1108G
1106G
1108C
1105G
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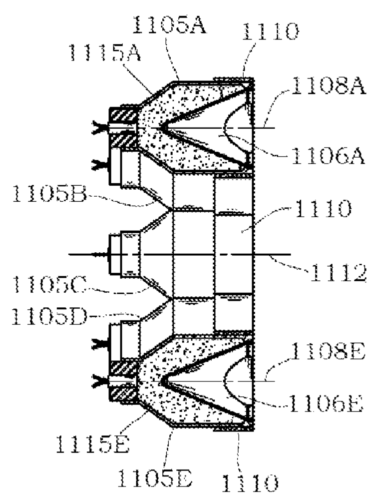
1110
1105E
1106E
G

FIG. 19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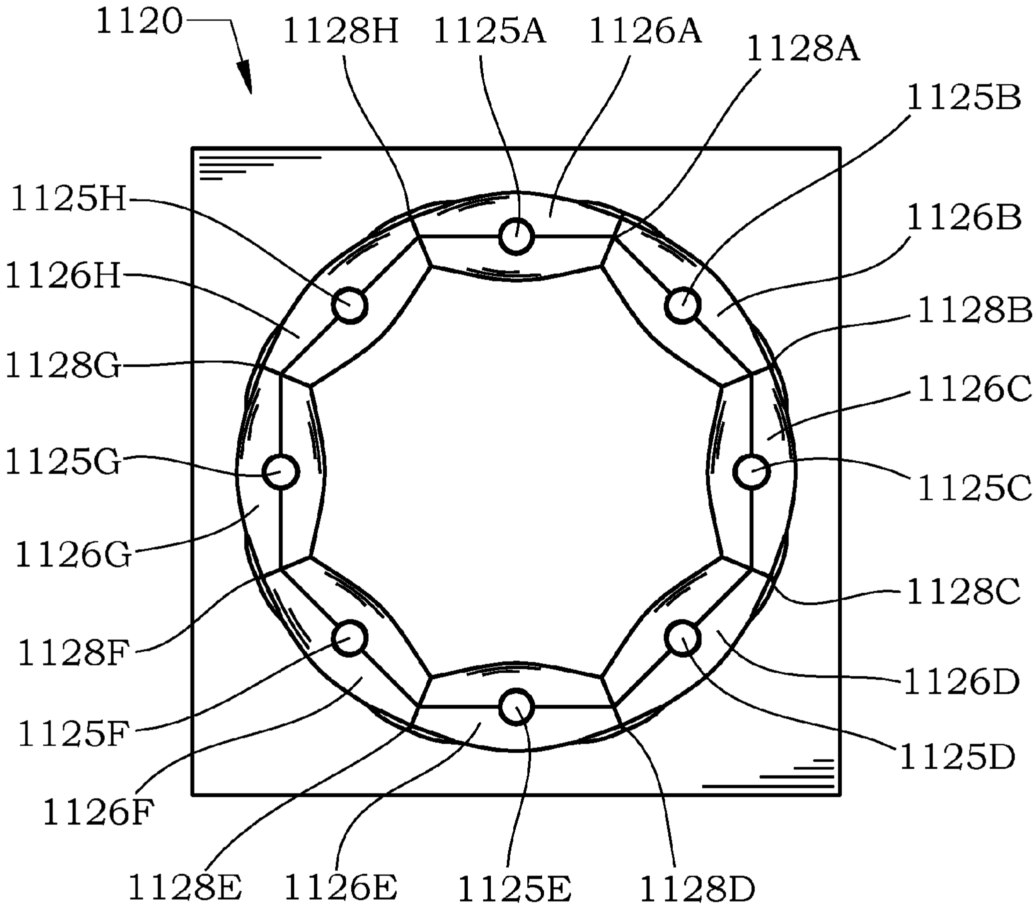
1105E
1110

FIG. 20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1126B
1128B
1126C
1125C
1128C
1126D
1125D
1128D
1125E
1126E
1128E
1126F
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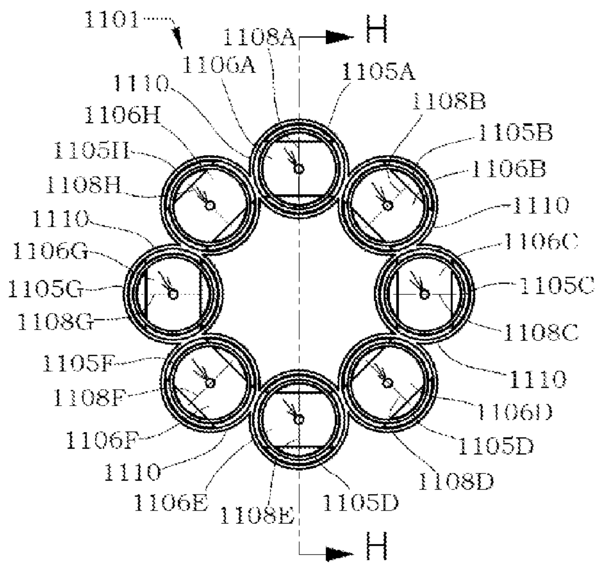
1128F
1126G
1125G
1128G
1126H
1125H

FIG. 21



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1106A
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1108B
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1106B
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1106C
1106G
1105G
1105C
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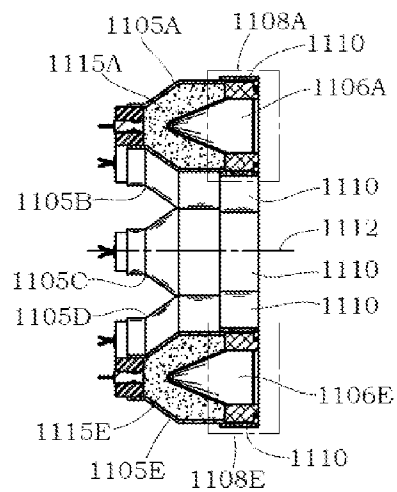
FIG. 22



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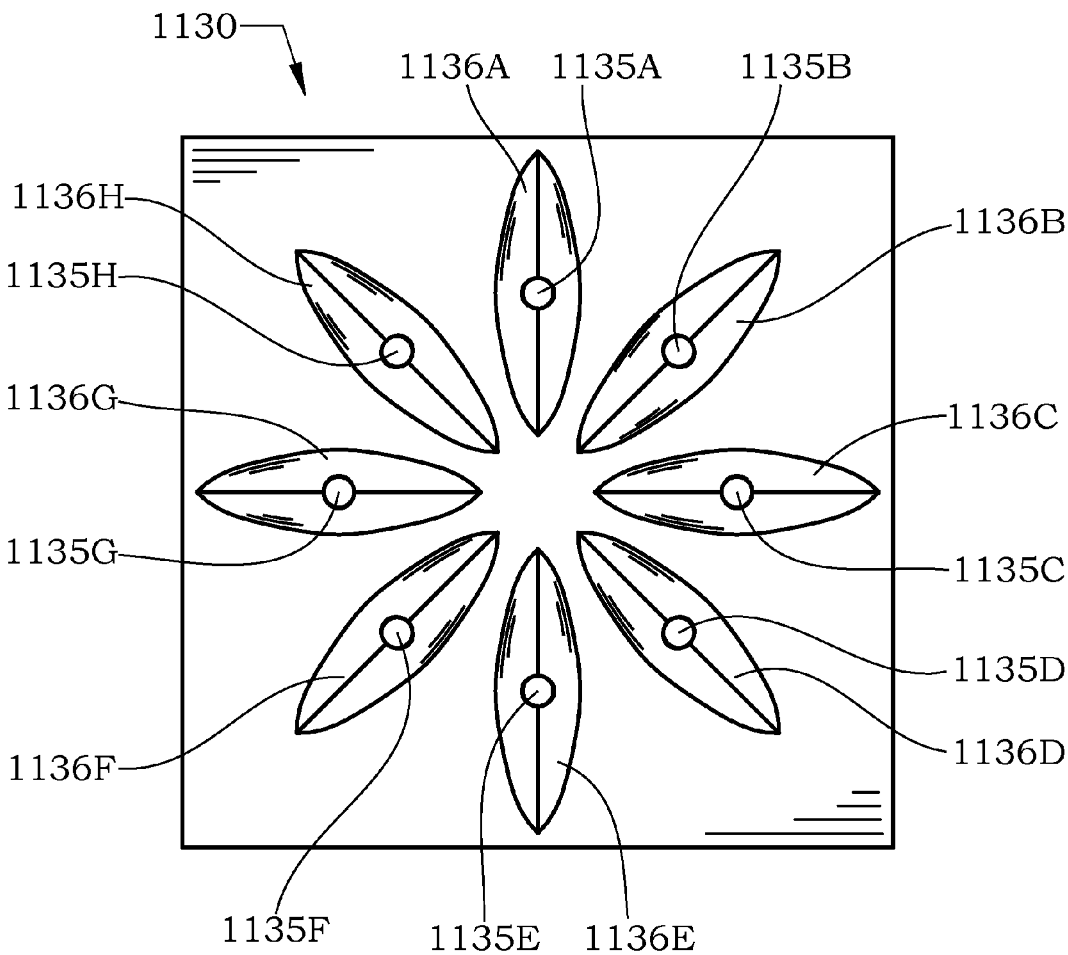
1110
1105E
1108E

FIG. 23



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1135E
1136E

FIG. 24

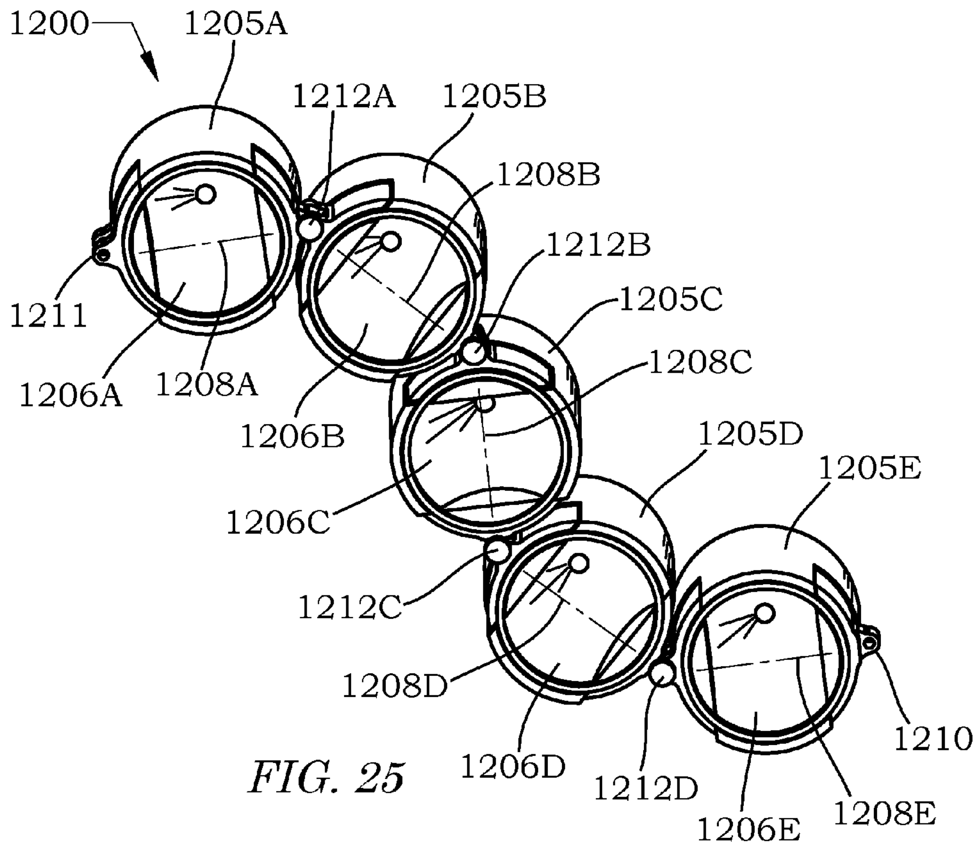

FIG. 25

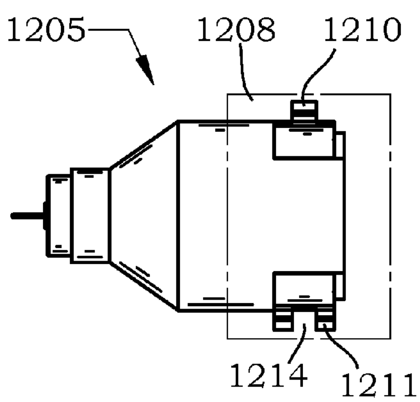

FIG.26

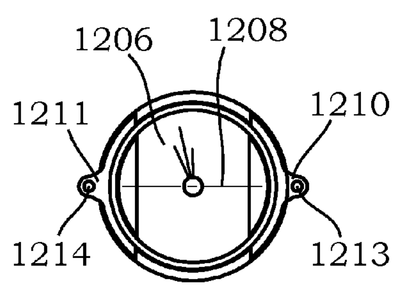

FIG.27

AXILINEAR SHAPED CHARGE ARRAY

RELATED APPLICATION DATA

This application is a Continuation-in-Part Application that claims priority under 35 U.S.C. §120 to application Ser. No. 14/724,497 filed on May 28, 2015, issued on Jun. 7, 2016 as U.S. Pat. No. 9,360,222.

TECHNICAL FIELD OF INVENTION

The technical field of the invention relates to explosive devices and, in particular, an array of arranged shaped charge explosive devices.

BACKGROUND OF INVENTION

As described in "The History of Shaped Charges" by Donald R Kennedy, the concept of shaping an explosive charge, in order to focus its energy was known in 1792. In 1884 Max von Forester conducted experiments in Germany showing that an explosive charge with a hollow cavity will focus the explosive energy and produce a collimated jet of high speed gasses along the longitudinal axis of the cavity. When this cavity is lined with a ductile metal it will produce a high speed collimated stretching jet of liquefied material capable of penetrating all known materials.

In 1888, while conducting research for the U.S Navy, at Newport R.I., Charles Munroe discovered that not only could explosive energy be focused, but lining the hollow cavity in the explosive with metal increased the penetration dramatically, the effect is commonly called the Munroe Effect. These discoveries were further studied in 1910 by Egon Neumann of Germany who conducted similar experiment's, which showed that a cylinder of explosive with a metal lined conical hollow cavity could penetrate through steel plates. The military implications of this phenomenon were not realized until the lead up to World War II.

In the 1930's flash x-ray technology was developed which allowed the in depth study of the Shaped Charge jetting process. With this new diagnostic, it was possible to take X-Ray pictures of the collapse of the liner and the resulting jet. This new diagnostic led to a more scientific and complete understanding of the Munroe principle and emphasized the power of shaped charges.

Generally, when a cylinder of explosive with a hollow conical cavity at one end is detonated at the center of the opposite end, the energy of the explosive is focused into a rod-like jet of high temperature, high pressure and high velocity gases along the axis of a conical cavity. This is an axisymmetric collapse and is generally known as the Munroe effect. The pressures created behind the detonation front in the explosive are of such magnitude that it causes the metal of the liner to liquefy and flow like a fluid. As the liner material is collapsed toward the axis of the hollow cavity, the flowing material radially converges, creating a rod-like stretching jet of high velocity, between five and ten kilometers per second.

These jets are primarily copper and will penetrate all known materials. The conventional shaped charge will give typically a hole size that is, in a semi-infinite target; could be as high as 20% of the diameter of the shaped charge. In order to achieve the greatest jet length and penetration depth, the jetting process of a shaped charge requires the liner material to reach a high temperature during collapse, which allows plastic flow of the collapsed liner material that produces a long stretching jet.

Plastic flow is accomplished by forcing the liner material under great pressures to collapse and converge radially onto the liners symmetrical axis. A typical linear or circular linear shaped charge liner has non-fluted or non-corrugated walls, is driven from only two dimensions and has insufficient convergence to cause plastic flow and high velocities, so these devices do not produce ductile stretching jets but instead produce explosively formed projectiles EFP.

Modern shaped charges are used for various purposes, such as oil field perforators, and they produce a long stretching rod-like metal jet that penetrates 4 to 8 charge diameters in steel and as much as three times deeper in masonry or rock. The average diameter of a 5 CD deep hole from these conventional shaped charges is less than 15% of the diameter of the explosive charge CD. These types of charges are designed to have long, stretching rod-like jets, primarily to penetrate the walls of a vehicle or other target, which has been the focus of a vast majority of research in this field. The small holes produced by these types of charges do not permit a follow-through device in the case of surgical destruction of a protected enclosure.

Modern shaped charges can produce a long stretching rod like metal jet that penetrates about 5 to 8 charge diameters in steel, deeper in masonry or rock. The average diameter of a five charge diameter CD through hole from these type charges is less than 15% of the explosive charge diameter. These small diameter holes made by conventional jets do not produce a hole of sufficient diameter to provide a means to deliver follow on shaped charges of equal charge diameter to the standoff needed from the bottom of a hole with the intent of making an equal size hole diameter and depth of penetration as the last charge.

There have been some specialized efforts by Halliburton to produce shaped charges other than conical type shaped charges for special purposes such as pipe cutting and anchor chain cutting. These type of charges are called linear shaped charges and use the Munroe principle to produce a thin sheet like jet with somewhat similar cutting power to the usual conical shaped charge. The liner is wide angle and the device is used against light structures such as wooden doors and thin walls. The vast majority of research and development in shaped charges over the past hundred years or so has been devoted to deep penetration in both military and commercial applications. Some efforts have been directed to increasing the internal angle of the liner and a shorter standoff.

Other devices using flexible linear shaped charges have been designed for breaching man-size holes in light walls, such as described in Wall AXE British, 1960. These line charge devices are collapsed from only two opposing directions producing a very irregular thin sheet-like jet that is unpredictable in its penetrating ability due to the lack of a simultaneous initiation along the apex of the line explosive. These line charges are limited in the thickness or toughness of the target they can address and are mainly used for light walls. Additionally, sometimes users such as police or firefighters are badly injured or killed trying to use these awkward and clumsy devices.

U.S. Pat. No. 7,753,850 places an interrupter along the jet axis inside the liner, in the flow path of the liner material. The permissible size of the interrupter for this concept can only be a small portion of the liner diameter so as to leave room for the liner to collapse. The small diameter of the interrupter does not form a large enough diameter jet to produce a full caliber hole or to hold its annular shape after it separates from the interrupter; the jet will converge into a rod and some of the precious liner length is wasted.

U.S. Pat. Publ. No. US2011/0232519 A1 shows outside and inside walls making up the circular trough of the liner. The mass of the outer wall of the liner trough, because of its greater diameter, is much greater than the mass of the inner wall. The outer wall is converging whereas the inner wall, with much less mass, is diverging; the same problem exists with the explosive quantities driving each wall of the liner. To obtain a circular or annular jet, these masses must be equal in forces when they converge on the projected axis of the liner cavity.

In steel-making, small conical shaped charges are often used to pierce taps that have become plugged with slag. Linear shaped charges, or line charges, are another type of shaped charge used in the demolition of buildings to cut through steel beams and collapse the building in a desired pattern. This type of flexible line charge creates a sheet-like jet from a two-dimensional collapse. SWAT teams and fire departments are another user of line charges, using the Munroe principle to generate high speed material for urban wall breaching and rescue. These line charges are very inefficient and difficult to initiate in a manner conducive to achieving their full potential. Very little research has been conducted in this area of shaped charge technology, and all of these applications of shaped charges would benefit greatly from a larger-diameter penetration capability.

Hole diameters in casing from these conventional charges are not greater than ½ inch in diameter. The expected perforated holes sizes can be inconsistent, varying in size to more than 50% from the target diameter. This inconsistency causes many fracturing operation issues, and small hole size limits product flow into and from the formation; if too small, the perforation will get fouled with debris and can stop flowing altogether. The hole diameter produced by a present day oil well perforator is only approximately 12% of its explosive charge diameter. Great efforts have been made over the last 50 or so years to enlarge the entry hole diameter in oil well casing without much success.

Some effort has been made with placing a conventional shaped charge ahead of the projectile in order to create a pilot hole in the rock; however, only a small gain in depth of penetration is achievable with this method because of the very small hole diameter produced by a conventional shaped charge. The hole diameter made by a conventional shaped charge jet is small, on the order of one-tenth the diameter of the explosive charge forming the jet, and it penetrates approximately 6-8 times the diameter of the charge in steel (more in rock or masonry).

There is clearly a need for innovation in this industry to have a shaped explosive device that produces a combination of a forward rod and rearward flattened Spade shaped stretching jet. There is also a need for innovation in arranging shaped charge devices together in an array to produce a patterned or arranged explosive pattern in a target area.

SUMMARY OF THE INVENTION

This invention is a unique arrangement of shaped charge devices in an array to produce a patterned or arranged explosive pattern in a target area. The Axilinear design, in a plural array configuration, solves the limitations of a smooth walled circular linear liner by having opposing corrugations or flutes that have sufficient curvature to converge the liner material so as to obtain ductile Munroe jetting, longer jets, and higher velocities. Since jet length and depth of target penetration, are directly proportional, the present invention provides a longer and most robust jet stream than previously possible.

The individual shaped explosive devices have a liner that produces a single combination jet consisting of a forward rod portion and rearward flattened spade shaped portion, this jet has a velocity gradient form tip to tail. The jet produced by the shaped charge is axisymmetric for the forward rod portion and planar symmetric for the aft wide spade portion somewhat like linear shaped charge, thusly termed the "Axilinear" shaped charge. This Axilinear device will produce a combination jet, consisting of a rod forward portion, followed by and connected to a planar symmetric wide spade shaped rear portion.

The high explosive billet has three distinct sections, a rear or boat tailed HE section "A" as measured longitudinally between HE initiation point and liner apex, a mid-section or full conic HE section "B" as measured longitudinally from apex to wing vertex, section "B" fully encompassing the liner conical section, and forward HE section "C" that contains two partial circumference wing HE sections as measured longitudinally from wing vertex to base ends that conform to the shape of the liner wing extensions. The EW liner is the working material of the shaped charge and is mounted to body at the forward end of device, at the base ends of the liner wing extensions; and adjacent to the wings the liner parabolic faces are mounted to the body parabolic faces.

The body of the explosive device consists of four distinct areas, a aft cylindrical area that provides mounting for an initiation device that is coupled to the aft end of HE device, followed by a boat tailed area that contains the rear HE section A, followed by cylindrical area that contains mid-section HE section B that is coupled to the full conical liner section; and forward HE section C containing wing sections that are coupled to the extended wings of liner section, and body area at the forward end of cylindrical section that transitions from a cylindrical shape into two parallel flat parabolic faces that are planar symmetric to each other and are coupled to the parabolic liner faces.

Body area has two functions—it provides two opposing side mounting faces for the liner extended wings and also has flat faces that is the forward containment boundary of HE section; this boundary is located at wing vertex, and is also the liner wing transition point from the full circumference conical section to the extended wing section. The containment of HE pressures during the detonation time period by body area is important for proper collapse of the wings and spade jet formation.

The rod or axisymmetric portion of the jet produces a large diameter deep penetration and the flattening of the rear portion causes the jet to spread in two opposing directions which produces a wide flat jet that gives a penetration of an elongated slot. The forward rod portion of each jet erodes a round hole in the target followed by the aft flattened spade portion of the jet creating a long slotted deep cavity centered on the round hole and in the lateral direction of the spade jet. The purpose for producing a dual purpose or hybrid jet where the forward portion being a focused small diameter rod and the aft portion being spread into a flattened wider spade like jet is so that the jet energy is spread over a bigger area and produces a larger detonation hole, or a shape for the detonation hole that is different than a round hole, in a target while simultaneously maintaining control of the direction of the elongation of the hole.

Although there are other designs and shapes possible, the circular arrangement offers the most efficient removal of target material. The circular design also offers the symmetry needed and ease of fabrication and deployment. A single Axilinear shaped charge device is capable of producing two types of penetrations in a common hole, which includes a linear slot combined with a deep hole penetration.

DESCRIPTION OF THE FIGURES

The inventor will use descriptive drawings and text to describe the device and how it functions.

FIG. **1** is a quarter cut sectional perspective view of a single Axilinear shaped charge device.

FIG. **2** is a perspective view of a single conical Axilinear extended wing liner used in the FIG. **1** embodiment.

FIG. **2**A-**2**B are elevation and end views of a single conical Axilinear extended wing liner used in the FIG. **1** embodiment illustrating the direction of reference planes relative to the liner wings.

FIG. **2**C is a sectional view along horizontal line **2**C-**2**C in FIG. **2**B of a single conical Axilinear extended wing liner used in the FIG. **1** embodiment that further illustrates the full and partial conical sections.

FIG. **2**D is a sectional view along vertical line **2**D-**2**D in FIG. **2**B of a single conical Axilinear extended wing liner used in the FIG. **1** embodiment that further illustrates the full and partial conical sections.

FIG. **3** is an end view of the embodiment shown in FIG. **1** illustrating the liner wings in the 12 and 6 o'clock positions.

FIG. **3**A-**3**B are elevation views of the high explosive billet used in the FIG. **1** embodiment.

FIG. **4** is a sectional view along vertical line **4-4** in FIG. **3** that is perpendicular to the horizontal collapse plane of the liner wings, of the Axilinear shaped charge embodiment of FIG. **1**.

FIG. **5** is a view of the jet formed by the device embodiment of FIG. **1** that illustrates the orientation of the spade jet with respect to the liner wings of FIG. **4**.

FIG. **6** is a sectional view along horizontal line **6-6** in FIG. **3** that is coplanar to the horizontal collapse plane of the liner wings, of the Axilinear shaped charge embodiment of FIG. **1**.

FIG. **7** is a view of the jet formed by the device embodiment of FIG. **1** that illustrates the orientation of the spade jet with respect to the liner wings in FIG. **6**.

FIG. **8** is an end view of a target surface with a cavity created by a single Axilinear shaped charge jet from the embodiment shown in FIG. **1**.

FIG. **9** is a vertical sectional view along line **9-9** in FIG. **8** that is coplanar with the collapse plane of the liner wings of the embodiment of FIG. **1** and further clarifies the wide direction of the cavity created by the spade jet.

FIG. **10** is a horizontal sectional view along line **10-10** in FIG. **8** that is perpendicular with the collapse plane of the liner wings of the embodiment of FIG. **1** and further clarifies the narrow direction of the cavity created by the spade jet.

FIG. **12-14** is a diverging wing variation of the liner embodiment shown in FIG. **2**.

FIG. **15-17** is a converging wing variation of the liner embodiment shown in FIG. **2**.

FIG. **18** is a perspective view of a circular array of eight Axilinear shaped charge devices.

FIG. **19** is a front view of the embodiment shown in FIG. **18**.

FIG. **20** is a longitudinal sectional view along line G-G in FIG. **19**.

FIG. **21** is an illustrated view of a target surface with a ring of cavities created by the detonation and the resultant jetting of the embodiment shown in FIG. **18**.

FIG. **22** is a front view of a variation of the embodiment with rotated shape charge devices shown in FIG. **18**.

FIG. **23** is a longitudinal sectional view along line H-H in FIG. **22**.

FIG. **24** is an illustrated view of a target surface with a radial extended pattern of cavities created by the detonation and the resultant jetting of the embodiment shown in FIG. **22**.

FIG. **25** is a perspective view of an articulated splined array embodiment of the invention.

FIG. **26** is a side view of an individual shaped charge used in FIG. **25**.

FIG. **27** is a front view of an individual shaped charge used in FIG. **25**.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

This invention is a unique arrangement of shaped charge devices in an array to produce a patterned or arranged explosive pattern in a target area. The Axilinear design, in a plural array configuration, solves the limitations of a smooth walled circular linear liner by having opposing corrugations or flutes that have sufficient curvature to converge the liner material so as to obtain ductile Munroe jetting, longer jets, and higher velocities. Since jet length and depth of target penetration, are directly proportional, the present invention provides a longer and most robust jet stream than previously possible.

The individual shaped explosive devices used in the array configuration of the present invention produce a combination of a forward rod and rearward flattened Spade shaped stretching jet. This explosive device herein after referred to as "The Axilinear" device or Axilinear shaped charge, consists of a liner, an explosive billet, a body and a means of initiation. The invention described and depicted herein produces a two part stretching jet, the forward portion is a rod like jet and the aft portion is spread into a spade like shape reminiscent of the jetting of a linear shaped charge but at much higher velocities, having a velocity gradient or stretch rate and directionally controllable.

For clarity, all references in this document to a shaped charge means, "a shaped charge" is an explosive device, having a shaped liner, driven by a similarly shaped mating explosive billet, having an initiation device, the necessary containment, confinement and retention of the liner to the explosive billet. The result of detonation of this device is a high speed stream of material produced from the convergence of the liner driven by the explosive. This is commonly known as the Munroe Effect. The shape and size of this stream of material commonly called a jet, is dependent on the starting shape and size of the liner and explosive billet.

The Axilinear liner in the present invention consists of two sections, aft section "B", and forward section "C." The aft section "B" is a full circumference of one of, or combination of the liner profiles, shown in the figure section of this document. This section B produces an axisymmetric rod like stretching jet with length proportional to the length of the liner section, the stretch rate, and time of flight of the jet.

The forward section "C" consists of less than full circumference walls extending beyond the end of section B, these wing extensions are symmetrically one hundred eighty degrees apart. These wing extensions have axisymmetric cavity as viewed from inside the hollow liner form, this cavity functions to provide the convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow. The jet from section C produces a planar symmetric stretching wide non round jet which cuts a slot rather than a round hole as produced by the rod portion of the jet.

More particularly, the Axilinear shaped charge device **100** shown in FIG. **1**, consist of a body **110**, EW liner **105**, high explosive (HE) billet **115**, having an axisymmetric aft area with detonator **136**, detonator holder **135**, detonation initiation point **107**, and liner apex **108**, and a axisymmetric as well as planar symmetric (Axilinear) fore area that consists of liner extended wings **125**A and **125**B and liner base ends **120**A and **120**B. Initiation of the HE billet of this novel device can be achieved by any suitable readily available detonation initiation devices.

Device **100** is axisymmetric or symmetrical about a longitudinal axis **137** from the aft end near detonator **136** to the middle liner wing vertex **132**A and **132**B of the EW liner **105**; forward of wing vertex **132**A and **132**B device **100** is Axilinear with two symmetrical curved extended wings **125**A and **125**B being axisymmetric with axis **137** and also planar symmetric about two central perpendicular reference planes, a horizontal plane in the 3 and 9 o'clock positions, and a vertical plane in the 12 and 6 o'clock positions.

The vertical 12 and 6 o'clock reference plane (FIG. **2** vertical plane **246**) is coincident with axis **137** and passes through the middle of each extended wing **125**A and **125**B, the parabolic faces **130**A and **130**B are planar symmetric or mirrored about this plane. Front edge **114** of face vacancy or void in the winged vertex **132**A of the liner **105**. The horizontal 3 and 9 o'clock reference plane (FIG. **2** horizontal collapse plane **245**) is coincident with axis **137** and passes through each wing vertex **132**A and **132**B, this plane is also known as the wing collapse plane and the wings **125**A and **125**B are planar symmetric or mirrored about this plane. The jet produced by detonating an Axilinear shaped charge device **100** is axisymmetric for the forward rod portion of the jet and planar symmetric for the aft portion, this aft spade portion of the jet being shaped somewhat like a linear shaped charge jet, thusly named Axilinear.

The Axilinear shaped charge device **100** is shown with a conical EW liner **105**, other geometrical shaped (i.e. hemispherical, tulip, or trumpet) hollow cavity formed liners with extended liner wings can also be used. EW liner **105** has a full circumference axisymmetric conical profile section **122** with included angle A that is longitudinally between aft apex **108** and middle liner wing vertex **132**A and **132**B, and a Axilinear partial circumference wing section **133** toward the fore end with two symmetrically opposing conical fluted wing extensions **125**A and **125**B with included angle A that extend longitudinally from the middle liner wing vertex **132**A and **132**B to the forward liner base ends **120**A and **120**B.

The forward liner wing extensions **125**A and **125**B are symmetrical to each other and positioned one hundred and eighty degrees apart, opposing each other planar symmetrically about the horizontal plane and is axisymmetric about longitudinal axis **137** of the device. The absence of liner wall material on opposing sides of the wing section **133** at the forward base end of the liner forms two parabolic faces **130**A and **130**B that are parallel and symmetric with each other about longitudinal axis **137** and the vertical plane. Both liner parabolic faces **130**A and **130**B have a vertex at wing vertex **132**A and **132**B and open toward the base ends **120**A and **120**B with parabolic end points at the wing arc ends **121**A and **121**B.

EW liner **105** maintains its conical profile and liner wall **109** thickness profile from aft end apex **108** of the full circumference conical section **122** to wing vertex **132**A and continues with the same profile to the fore end of the extended wings **125**A and **125**B at the base ends **120**A and **120**B of the partial circumference wing section **133**. Liner wall **109** transitions from a full circumference conical profile at wing vertex **132**A and **132** B into 180 degree symmetrically opposing wing like or fluted extensions **125**A and **125**B that extend from the full circumference conical profile section **122** at wing vertex **132**A and **132**B to the base end **120**A and **120**B of the liner.

The liner wing extensions **125**A and **125**B shown in FIG. **1** retain the same curvature, included angle A, and wall **109** thickness profile as the full conical profile section **122** portion of the liner; but the extended wings **125**A and **125**B could also have a larger or smaller included angle A and wall thickness **109** than the conical section **122**, as long as they maintain planar symmetry to one another. Being planar symmetric and having partial circumference conical curvature allows the wing-like extensions or flutes **125**A and **125**B to converge at very high pressures on the collapse plane, raising the temperature and ductility of the converging wing material to the required level for Munroe jetting.

HE billet **115** can be pressed, cast or hand packed from any commercially available high order explosive. HE billet **115** is in intimate contact with the outer liner surface **116** of EW liner **105** from the aft apex **108** to the forward wing vertex **132**A and **132**B of the conical profile section **122** and from the wing vertex **132**A and **132**B to the base ends **120**A and **120**B and wing arc ends **121**A and **121**B of the wing section **133**. HE billet **115** has three distinct sections, a head height or aft HE section "A" **138** as measured longitudinally between HE initiation point **107** and liner apex **108**, a mid-section or full conic HE section "B" **139** as measured longitudinally from apex **108** to wing vertex **132**A and **132**B, that fully encompasses the liner conical section **122**, and forward HE section "C" that contains two partial circumference wing HE sections **140**A and **140**B as measured longitudinally from wing vertex **132**A and **132**B to base ends **120**A and **120**B that conform to the shape of the liner wing extensions **125**A and **125**B.

HE section A **138** can be lengthened or shortened longitudinally by increasing or decreasing the length of body **110**, greater head height gives a flatter detonation wave before it comes in contact with the liner. Flatter detonation waves at time of liner impact typically increase jet tip velocity and target penetration, head height optimization is a balance between jet performance and minimizing the explosive charge. The optimum head height can be determined by computer code and live testing to obtain the least amount HE volume needed to efficiently obtain maximum jet mass, velocity and target penetration. A typical head height for a conical lined shaped charge would be ½ inch space permitting.

The shape and volume of HE section B **139** is defined by the area between the inside surface **112** of body **110** and outside surface **116** of EW liner **105** from aft apex **108** to forward body face **110**E located at wing vertex **132**A and **132**B, and makes a full circumference or revolution around liner section **122**. The shape and volume of the two symmetrical wing HE sections **140**A and **140**B of HE section C are defined by the area between the inside surface **112** of body **110** and outside surface **116** of EW liner **105** from aft wing vertex **132**A and **132**B to forward base ends **120**A and **120**B, and are partial circumference volumes about each wing between the wing arc end points **121**A and **121**B. HE billet **115** can have a super-caliber diameter (i.e. larger than the liner base diameter) necessary for full convergence of the base end of the liner wing extensions **125**A and **125**B to obtain maximum velocity and mass of the spade jet.

The forward section C **133** consists of two less than full circumference liner walls **109** extending beyond the end of section B **122**, creating partial conical or curved wing extensions **125**A and **125**B, wing vertices **132**A and **132**B and parabolic faces **130**A and **130**B that are symmetrically one hundred and eighty degrees apart. The wing vertex **132**A and **132**B and flat parabolic faces **130**A and **130**B are formed from the absence of material on two symmetrically opposing sides of the base end of the conical profile. The wing extensions **125**A and **125**B create an axisymmetric and planar symmetric opposing partial radial hollow concavities on the inside liner wall surface **117**; HE detonation pressures on these concavities provides a partial radial convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow and hydrodynamic jetting.

The collapse of the wing extensions **125**A and **125**B of section C **133** produces a wide planar symmetric stretching non round spade shaped jet which cuts a deep slot rather than a round hole; the mass, width, length, stretch rate, velocity, and time of flight of the spade jet is directly proportional to the liner wall length of section C **133**, included angle A, and liner wall **109** thickness of section C **133**. If section C **133** is shortened and the overall length "L" is unchanged section B **122** will become longer. Increasing the length of section B **122** will increase the rod jet length, mass and penetration depth, and will decrease the length, width, mass and penetration depth of the spade jet; length adjustments to sections B and C work in concert, when the rod jet is lengthened the spade jet will be shortened and vice versa shortening the rod jet will lengthen the spade jet.

During collapse of the liner full conical section **122**, liner material radially converges along the longitudinal axis **137** into a rod jet from the detonation of HE section A **138** and HE section B **139**; the collapse of full conical section **122** is followed by the collapse of the extended liner wings **125**A and **125**B of the partial circumference section **133** into a spade jet from the detonation of wing HE sections **140**A and **140**B of HE section C. Wing HE sections **140**A and **140**B are coupled to the outer liner surface **116** of each wing from the aft wing vertex **132**A and **132**B to the forward wing base ends **120**A and **120**B and the wing arc ends **121**A to **121**B.

The radial curvature of the opposing liner wing extensions **125**A and **125**B provides the radial material convergence during collapse needed to raise the temperature and pressure of the collapsed liner material, to the required level for plastic flow and Monroe jetting to occur, this increases the ductility allowing for longer jet breakup length. During collapse the full conical section **122** of the liner will form an axisymmetric rod jet along the longitudinal axis **137** followed by the concave liner wing extensions **125**A and **125**B being driven to a common collapse plane by HE **140**A and **140**B, the colliding wing extensions material will form into a high velocity flat planar symmetric spade shape jet.

As the collapsed wing extensions material moves forward along longitudinal axis **137** it also spreads laterally outward forming the spade shaped jet along the horizontal collapse plane. The formation of the spade jet is due to the absence of liner material, explosive and confinement on the liner sides with the two flat parabolic faces **130**A and **130**B that are adjacent to and ninety degrees out of phase from the flutes or wing extensions **125**A and **125**B. The orientation of device **100** can be rotated about axis **137** and the spade jet orientation will rotate equally in the same direction, if device **100** is rotated 45 degrees clockwise about axis **137** the collapse plane will also rotate 45 degrees clockwise and the spade jet will stretch longitudinally forward on axis **137** and laterally along the rotated collapse plane.

The EW liner **105** is the working material of the shaped charge and is mounted to body **110** at the forward end of device **100**, at the base ends **120**A and **120**B of the liner wing extensions **125**A and **125**B; and adjacent to the wings the liner parabolic faces **130**A and **130**B are mounted to the body **110** parabolic faces **110**F. Body **110** consist of four distinct areas, a aft cylindrical area **110**C that provides mounting for an initiation device that is coupled to the aft end of HE **115**, followed by a boat tailed area **110**B that contains the HE section A **138**, followed by cylindrical area **110**A that contains HE section B **139** that is coupled to the full conical liner section **122**; and HE section C containing wing sections **140**A and **104**B that are coupled to the extended wings of liner section **133**, and body area **110**D at the forward end of cylindrical section **110**A that transitions from a cylindrical shape into two parallel flat parabolic faces **110**F that are planar symmetric to each other and are coupled to the parabolic liner faces **130**A and **130**B.

Body area **110**D has two functions, it provides two opposing side mounting faces **110**F for the liner extended wings and also has flat faces **110**E that is the forward containment boundary of HE section **139**; this boundary is located at wing vertex **132**A and **132**B, and is also the liner wing transition point from the full circumference conical section **122** to the extended wing section **133**. The containment of HE pressures during the detonation time period by body area **110**D is important for proper collapse of the wings and spade jet formation. Shape charge liners for the most part are made from copper but liners may be made from most any metal, ceramic, powdered metals, tungsten, silver, copper, glass or combination of many materials. Body **110** would typically be made from aluminum or steel but could be made of almost any metal or plastic as long as it provides the correct amount of tamping for proper jet formation and desired jet velocity during the detonation of HE billet **115**.

The EW liner **105** is a modified cone or other shape with two distinct geometrical sections, the aft end of the liner is a full conical profile section **122** with an apex **108**, followed by the forward end wing section **133** with two liner wing extensions **125**A and **125**B that extend forward from the full conical or other shape profile section **122** at wing vertex **132**A and **132**B to the wing base ends **120**A and **120**B at the fore end of EW liner **105**. The liner wing extensions **125**A and **125**B maintain the same included angle A liner wall **109** thickness profile and curvature of the full conical profile section **122**.

The included angle A of EW liner **105** needed to obtain Munroe effect jetting should be from 36 to 120 degrees. The jet velocity achieved from a shaped charge is dependent on the liner wall **109** thickness and included angle A of the liner; a narrower included angle results in a faster less massive jet, and a wider included angle results in a slower more massive jet. Jet velocities can vary from 4 to 10 km/s depending on the type and quality of liner material, included angle A of the liner, liner wall **109** thickness, the charge to mass ratio of HE to liner, bulk density of the liner, surface finish of the liner wall, and body geometries; very small changes of any of these variables can make large differences in jet velocity and trajectory.

The HE billet **115** is contained between the inner surface **112** of body **110** and the outer surface **116** of the EW liner **105**. HE billet **115** provides the energy to collapse the EW liner **105**, increasing the ductility of the EW liner **105** material, causing it to form a compound jet in the shape of a very high speed rod jet from the full conical section **122** material followed by a flattened spade shaped jet from the liner wing section **133** material; the spade jet is slower than the rod jet from conical section **122** but much faster than a typical "V" shaped liner found in common linear shaped charge because of the cavity of the wing section **133**.

Body **110** provides a mounting surface for EW liner **105** which is held to body **110** at the liner base ends **120**A and **120**B and at the parabolic faces **130**A and **130**B. The base end of EW liner **105** does not form a full circumference; it consists of two opposing concave surfaces or wing extensions **125**A and **125**B and the corresponding wing base ends **120**A and **120**B at the forward end of the liner. Body **110** also serves as a containment vessel for the delicate HE billet **115** and protects it from damage or impact by supporting the outer diameter of HE billet **115**. Body **110** also provides tamping for the HE billet **115** depending on body wall **106** thickness and material density, HE tamping can be increased or decreased if needed to improve jet performance or reduce total HE mass.

The purpose of removing the base end material on symmetrically opposing sides of EW liner **105** and creating the wing-like extensions **125**A and **125**B is twofold. The first purpose is to form the partial circumference conical wing-like extensions or flutes **125**A and **125**B and when collapsed converge to form the flat aft spade shaped portion of the jet; the flattened spade jet spreads laterally and erodes an elongated slot in target material. The second purpose being to allow for close lateral proximity of multiple adjacent devices resulting in multiple tightly spaced rod and intersecting spade jet perforations, creating a large coupled slotted target perforation.

Since the EW liner **105** material is not being confined along the two removed portions of the liner at parabolic faces **130**A and **130**B, the collapse of the wing-like extensions or flutes **125**A and **125**B will produce a flat jet, much like a linear shaped charge, but at a much higher velocity, stretching laterally and longitudinally. The transition from the conical profile section **122** to the remaining wing-like extensions or flutes **125**A and **125**B of EW liner **105** is very gradual so as to maintain continuity between the rod and spade portions of the jet.

The shaped charge body **110** has a frustoconical or boat tailed portion **110**B near the aft end of the shaped charge device **100** that begins at detonator holder **135** and increases in diameter longitudinally to about the apex **108** of EW liner **105**. The cylindrical portion **110**A of the body **110** begins at about the apex **108** of the EW liner **105** and extends longitudinally to the forward end of device **100**. The forward end of cylindrical portion **110**A has two planar symmetrical **110**D portions, each with a cylindrical outer face **110**G, an inner parabolic flat face **110**F and internal flat face **110**E. The two internal parabolic flat faces **110**F of the body begin at the liner wing vertex **132**A and **132**B and end at wing arc ends **121**A and **121**B; faces **110**F are symmetrical and parallel to each other, and perpendicular with the wing collapse plane that is centrally located and collinear with longitudinal axis **137** between the two flat faces **110**F.

Flat faces **110**F and faces **110**E of the shaped charge body **110**D help confine the wing HE **140**A and **140**B portion of HE billet **115** by providing cavity closure between the flat faces **110**F and the liner parabolic faces **130**A and **130**B on each side of the wing-like extensions or flutes **125**A and **125**B of the EW liner **105**. The body **110** preferably tapers or boat tails smaller in some manner toward the rearward end **110**B from aft of the liner apex **108** toward the detonator holder **135** minimizing the overall mass of HE billet **115**, reducing the amount of explosive by boat tailing body **110** increases the charge efficiency without affecting the liner collapse performance, and reduces unwanted collateral target damage from excessive explosive mass.

The invention described and depicted herein produces a two part stretching jet, the forward portion is a rod like asymmetric jet and the aft portion is spread into a sheet like planar symmetric shape reminiscent of the jetting of a linear shaped charge. In order to achieve the greatest jet length and penetration depth the jetting process of a shaped charge requires the liner material to reach a high temperature during collapse, which allows plastic flow of the collapsed liner material and produces a long stretching jet. Since jet length and penetration are directly proportional it is reasonable to make the greatest effort to provide the longest and most robust jet possible.

The above description of the directions of the shaped charge body and liner can be reversed whereby the axisymmetric jet is aft of the spade jet, there can be multiple sections alternating from axisymmetric and planar symmetric sections that produce alternating spade rod spade rod jet. The sections making up a liner do not have to have the same internal angle, thickness profile or material. The internal angles of these sections can vary from 36 degrees to 120 degrees and still produce Munroe jetting, that is to say a ductile jet having a velocity gradient from tip to tail. The arc length of each wing as encompassed by radial lines radiating from the central axis and intersecting each cord end of the arc of the wing can vary from 90 to 140 degrees.

FIG. **2**, FIG. **2**A, FIG. **2**B, FIG. **2**C, and FIG. **2**D illustrate a EW liner **200** used in the device of the FIG. **1** embodiment, that consist of a apex **208** toward the aft end of the full circumference conical section "B" **222**, and a partial circumference wing section "C" **233** with base ends **220**A and **220**B, liner wing extensions **225**A and **225**B, and wing base arc ends **221**A and **221**B toward the forward end of EW liner **200**. The liner wing extensions **225**A and **225**B extend or protrude in a forward direction from section A **222** beginning at wing vertex **232**A and **232**B and ending at the base ends **220**A and **220**B. Wing vertex **232**A and **232**B are positioned longitudinally at vertical line **213** where the liner transitions from the full circumference conical section B **222** into a partial circumference conical or other shape wing section C **233**. Liner wall **209** of section B **222** and section C **233** can vary in thickness, curvature, and included angle A can be increased or decreased to achieve desired rod and spade jet velocities and mass.

The conical section B **222** and wing section C **233** share a common longitudinal symmetrical axis **237**, section C **233** also has a horizontal collapse plane **245** in the 3 to 9 o'clock position and vertical plane **246** in the 12 to 6 o'clock position they are perpendicular to each other and intersect each other at symmetrical axis **237**. Section B **222** is axisymmetric or symmetrical about axis **237** in all radial planes for 360 degrees, whereas section C **233** has two parabolic faces **230**A and **230**B that are planar symmetric about vertical plane **246**; and two extended wings **225**A and **225**B that are planar symmetric about horizontal plane **245** and also axisymmetric between the wing arc ends **221**A and **221**B about axis **237**. The EW liner **200** is a modified hollow cone, but could also be other relative hollow shapes (i.e. hemisphere, trumpet, tulip), having two opposing equal sections removed at the base end of the liner, creating two extended wings like **225**A and **225**B and two parabolic faces like **230**A and **230**B.

The absence of the two opposing equal liner wall sections at the liner base end creates two equal 180 degree opposed liner wing extensions **225**A and **225**B or flutes. The included angle A of the hollow conical liner and the longitudinal length of the full section B **222** portion of the liner determines the longitudinal wing length from wing vertex **232**A and **232**B to the base end **220**A and **220**B of the extended wings **225**A and **225**B or fluted portions of the liner and thusly the amount of the liner wall **209** material that is dedicated to producing the spade or flattened portion of the jet. The longitudinal length of section B **222** and the extended wings **225**A and **225**B or flutes can be increased or decreased to achieve the desired ratio of rod to spade length of the jet created from EW liner **200**. The thickness of the liner wall **209** can gradually increase or decrease from the apex **208** to the base end **220**A and **220**B or anywhere along the wall length; a tapering liner wall **209** thickness will help balance the liner to HE mass ratio as the liner cone diameter increases toward the base end **220**A and **220**B.

Liner thickness of shaped charges are dependent on the overall diameter of the device, the liner wall **209** should increase in thickness as the device diameter increases and decrease in thickness as the device diameter decreases. Shaped charges scale very nicely and for the person skilled in this art making this device in any size would be evident based on the information given. Shaped charges by their very nature have varying liner wall thicknesses and profiles depending on liner material type, liner density, the jet velocity required, and desired effect on a target. The winged exterior of the liner **200** is 216 and the full conical section of the liner **200** is 234. The EW liner **200** could be made from many profiles including cones, tulips, trumpets, hemispherical, etc. to accomplish desired effects on targets.

The axisymmetric wing extensions **225**A and **225**B curvature, section C **233** of the Axilinear liner wall **209** material support the convergence of material to create a high velocity flattened deep penetrating spade jet on horizontal plane **245**. The axisymmetric curvature of the liner wings prevents the formation of a conventional planar symmetric "V" shaped low velocity linear shaped charge.

The combination of the hybrid axisymmetric and planar symmetric EW liner **200** used in a precision Axilinear shaped charge produces the necessary material convergence for a high velocity rod and spade shaped stretching jet above 4.0 km/s that is capable of producing deep hydrodynamic plastic target material penetrations from a much lower HE to liner mass ratio than a conventional linear shaped charge. The present invention avoids the problems associated with conventional linear shaped charges having large explosive to liner mass ratios; namely, the formation of low velocity (about 2.0 km/s) thin blade or ribbon jet that produce shallow target cuts (mostly non-plastic erosion much like water jet cutting) from "V" shaped planar symmetric liner walls.

The present invention is a high velocity precision shape charge, which can be distinguished from conventional linear charges that are non-precision low efficiency cutting charges, without axisymmetric radial convergence. Two types of shaped charges include an Axisymmetric shape charge and a Linear or planar symmetric. An axisymmetric shaped charge is basically a hollow cone or other similar shaped liner that is symmetric about a central longitudinal axis. Liners are usually made from copper, although it could be made of many other materials, having an explosive billet to which the outside of the liner is exactly mated.

A Linear shaped charge, sometimes referred to as a line charge, is essentially a V shaped straight hollow thin walled trough backed on the outside of the V by an appropriately shaped explosive mass. When detonated above the apex of the liner, this linear shaped charge produces sheet or ribbon-like jetting. The velocity from this type of shaped charge is in the 2-3 km/s range with little or no velocity gradient and consequent shorter jet and less penetration. The jetting occurring in this device is not Munroe jetting as the collapse is only two dimensional (does not have axisymmetric convergence) and does not reach the required temperature for plastic flow to take place. As a further recognition of the inefficiency of a conventional linear shaped charge, the detonation wave does not reach the full length of the liner apex simultaneously, this causes an undesirable dispersion of the resulting spray of liner material and no real continuity to the spray.

The jet produced by each Axilinear shaped charge in the present invention is a stretching combination of a rod and spade shaped like projectile having a velocity gradient from tip to tail, tip velocity of the this jet could be as high as 10 km/s depending on the included angle, charge to mass ratio, confinement, and shape of the liner, jet tail velocities are about 2 km/s. The present invention achieves higher velocity precision formation of an explosive jet without the need to increase the explosive mass, which would be required in the prior art conventional charge. The present invention is much more efficient and effective in that conventional linear charges cannot make precision deep target cuts or penetrations like the claimed invention because of their large HE to liner mass ratio, and typically, prior art shape charges produce a wide cratering effect from the collateral damage of the large amount of explosive which is avoided in the present invention.

When the EW liner **200** wing extensions **225**A and **225**B are collapsed to horizontal plane **245** the jet energy is spread longitudinally forward and laterally outward over a larger spade shaped area parallel to and centered on horizontal plane **245**, and upon target impact forms a plastic flowing region of jet and target material, that produces an elongated slotted hole that is parallel with horizontal plane **245** in the target material.

Since the liner wing extensions **225**A and **225**B are not connected or confined on the two opposing sides with parabolic faces **230**A and **230**B, the collapse of the liner wing extensions **225**A and **225**B material will spread in the direction of no confinement producing a flat spade shaped jet that stretches longitudinally on axis **237** and widens laterally on horizontal plane **245**; somewhat like a linear shaped charge, but at a much higher velocity and directionally controlled by horizontal plane **245** orientation about axis **237**. The liner wall **209** transition at vertical line **213** from the axisymmetric section B **222** portion of the EW liner **200** to the remaining axisymmetric and planar symmetric section C **233** is gradual so as to maintain jet continuity between the rod and spade portions of the jet.

Axisymmetric shaped charge liners come in cone, hemispherical, trumpet, and tulip shapes, included liner angles from 30 to 120 degrees and almost any base diameter within manufacture capability, the hybrid axisymmetric planar symmetric or Axilinear liner disclosure in this patent application intends to include this wide variety of profiles as part and parcel of the claims of this application.

For description purposes the Axilinear liner can be sectioned at vertical line **213** shown in FIG. **2**A, FIG. **2**C, and FIG. **2**D, with an aft full circumference conical section "B" **222**, and forward partial circumference wing section "C" **233**, the aft section B **222**, being a full circumference of one of, or combination of the liner profiles, cone, tulip, trumpet, hemispherical, or other. HE detonation pressures on the full conical section B **222** produces an axisymmetric rod like stretching jet with mass, length, stretch rate, velocity, and time of flight of the jet proportional to the length, included angle A, and liner wall **209** thickness of section B **222**; and on impact produces a deep round target material penetration.

The forward section C **233** consists of two less than full circumference liner walls **209** extending beyond the end of section B **222**, creating partial conical or curved wing extensions **225**A and **225**B, wing vertices **232**A and **232**B and parabolic faces **230**A and **230**B that are symmetrically one hundred and eighty degrees apart. The wing vertex **232**A and **232**B and flat parabolic faces **230**A and **230**B are formed from the absence of material on two symmetrically opposing sides of the base end of the conical profile.

The wing extensions **225**A and **225**B create an axisymmetric and planar symmetric opposing partial radial hollow concavities on the inside liner wall surface **217** as viewed from horizontal plane **245**; HE detonation pressures on these concavities provides a partial radial convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow and hydrodynamic jetting. The outer surface of liner **200** along the winged extension **216** is shown in FIG. **2**, while the outer surface of the liner **200** in the full conical section **234** is also shown in FIG. **2**.

The collapse of the wing extensions **225**A and **225**B of section C **233** produces a wide planar symmetric stretching non round spade shaped jet which cuts a deep slot rather than a round hole; the mass, width, length, stretch rate, velocity, and time of flight of the spade jet is directly proportional to the liner wall length of section C **233**, included angle A, and liner wall **209** thickness of section C **233**. If section C **233** is shortened and the overall length "L" is unchanged section B **222** will become longer. Increasing the length of section B **222** will increase the rod jet length, mass and penetration depth, and will decrease the length, width, mass and penetration depth of the spade jet; length adjustments to sections B and C work in concert, when the rod jet is lengthened the spade jet will be shortened and vice versa shortening the rod jet will lengthen the spade jet.

FIG. **2**B is a base end view of liner **200** that further clarifies the liner construction and positions of the wing extensions **225**A and **225**B to the descriptive planes. FIG. **2**B shows the wing extensions **225**A and **225**B at the 12 and 6 o'clock positions with a horizontal plane **245** dividing the distance between the two wings; and the flat parabolic faces **230**A and **230**B in the 3 and 9 o'clock positions with a vertical plane **246** dividing the distance between the two parabolic faces.

Wing width "W" represents the width from parabolic face **230**A to face **230**B, increasing the width W will make the wing arc length or distance between the wing arc endpoints **221**A longer and angle F larger. Radial lines **203**A and **203**B that radiate from the central axis to each wing arc end point **221**A of wing **225**A illustrate the wing arc cord length **204**A; the cord length can be increased or decreased by changing arc angle F. Arc angle F of the wings **225**A and **225**B can vary from 90 to 140 degrees but each wing on EW liner must have the same angle F and cord length **204**A and **204**B to have the symmetry needed for axisymmetric convergence of the wings.

FIG. **2**C is a horizontal section view of EW liner **200** taken along line **2**C-**2**C of FIG. **2**B showing an elevated view of wing **225**B and the inside liner surface **217**, that further clarifies the profile of section B **222** with included angle A and section C **233** with wing width W. If width W increases and angle A and the overall length L is held constant the length of section C **233** and the extended wings will become shorter, the horizontal line **213** will move toward base end **220**B and the length of section B **222** will become longer which will increase the length of the rod jet. Changing the length of section C **233** and section B **222** will change the length ratio of rod to spade jet. To improve the liner to HE mass ratio and rod jet performance liner wall thickness **209** may be held constant or can taper by increasing or decreasing the wall thickness **209** from apex **208** to wing vertex **232**A and **232**B.

FIG. **2**D is a vertical section of EW liner taken along line **2**D-**2**D of FIG. **2**B showing an elevated view of the inside liner surface **217** and parabolic face **230**A that further clarifies the profile of conical section B **222** and wing section C **233** with included angle A. Conical section B **222** and wing section C **233** have the same included angle A, and if angle A and the overall length L is held constant and the length of wing section C **233** increases, the vertical line **213** will move toward apex **208**, which will increase the length of the spade jet and will decrease the length of the rod jet and vice versa if section C becomes shorter the spade jet length will decrease and the rod jet will increase. To improve the liner to HE mass ratio and spade jet performance, liner wall thickness **209** may be held constant or can taper by increasing or decreasing the wall thickness **209** from apex **208** to wing base end **220**A and **220**B.

FIG. **3** is an end view of the Axilinear shaped charge device of the FIG. **1** embodiment, which shows the orientation of the EW liner **305** wing extensions **325**A and **325**B in the 12 and 6 o'clock position with a vertical plane **346** and a horizontal wing collapse plane **345**. An apex **308** with base ends **320**A and **320**B, liner wing extensions **325**A and **325**B, and wing base arc ends **321**A and **321**B toward the forward end of EW liner **300**. The liner wing extensions **325**A and **325**B extend or protrude in a forward direction from section A beginning at wing vertex and ending at the base ends **320**A and **320**B. Wing vertex is positioned longitudinally where the liner transitions from the full circumference conical section B into a partial circumference conical or other shape wing section C. Liner wall of section B and section C can vary in thickness, curvature, and included angle A can be increased or decreased to achieve desired rod and spade jet velocities and mass.

The conical section B and wing section C **333** share a common longitudinal symmetrical axis, section C also has a horizontal collapse plane **345** in the 3 to 9 o'clock position and vertical plane **346** in the 12 to 6 o'clock position they are perpendicular to each other and intersect each other at symmetrical axis. Section B is axisymmetric or symmetrical about axis **337** in all radial planes for 360 degrees, whereas section C has two parabolic faces that are planar symmetric about vertical plane **346**; and two extended wings **325**A and **325**B that are planar symmetric about horizontal plane **345** and also axisymmetric between the wing arc ends **321**A and **321**B about axis **337**. The EW liner **300** is a modified hollow cone, but could also be hemisphere, trumpet, tulip shapes, each having two opposing equal sections removed at the base end of the liner, creating two extended wings like **325**A and **325**B and two parabolic faces like **310**F and **310**F.

The absence of the two opposing equal liner wall sections at the liner base end creates two equal 180 degree opposed liner wing extensions **325**A and **325**B or flutes. The included angle A of the hollow conical liner and the longitudinal length of the full section B portion of the liner determines the longitudinal wing length from wing vertex A to the base end **320**A and **320**B of the extended wings **325**A and **325**B or fluted portions of the liner and thusly the amount of the liner wall material that is dedicated to producing the spade or flattened portion of the jet. The longitudinal length of section B and the extended wings **325**A and **325**B or flutes can be increased or decreased to achieve the desired ratio of rod to spade length of the jet created from EW liner **300**. The thickness of the liner wall can gradually increase or decrease from the apex **308** to the base end **320**A and **320**B or anywhere along the wall length; a tapering liner wall thickness will help balance the liner to HE mass ratio as the liner cone diameter increases toward the base end **220**A and **220**B.

EW liner **305** has a liner wall thickness that can remain constant or gradually decrease in thickness from the aft apex **308** to the base end **320**A and **320**B. The charge body **310** has two flat faced parabolic sides **310**F in the 9 and 3 o'clock position that have parabolic faces that geometrically match the EW liner **305** parabolic faces **330**A and **330**B, when coupled together these faces make a tight fitting body and liner coupling that supports the EW liner **305** wings and serves as containment for HE billet **315** along the partial circumference portion of EW liner **305**. There is no HE or EW liner **305** material confinement laterally outside of the two parabolic sides **310**F.

After the collapse of full conical section B by HE section B into a rod jet the curved wing-like extensions or flutes **325**A and **325**B of wing section C **333** are driven to horizontal plane **345** and symmetrical axis **337** of the EW liner **305** by the HE section C with wing explosive **340**A and **340**B, the colliding material forms a flat blade shape jet instead of a round jet because of the lack of liner material and HE confinement on the flat faced sides **310**F that are ninety degrees out of phase from the wing-like extensions or flutes **325**A and **325**B. The transition from conical section B to wing section C is gradual which allows the spade jet to stay connected to the forward rod jet as both portions of the jet stretch longitudinally forward along axis **337**; and because of the lack of liner confinement on the two opposing parabolic faces **310**F the spade jet will widen laterally on horizontal plane **345** as it stretches longitudinally forward with the forward rod jet. The body area **310**D at the forward end of cylindrical section **310**A that transitions from a cylindrical shape into two parallel flat parabolic faces **310**F that are planar symmetric to each other and are coupled to the parabolic liner faces.

FIG. **3**A and FIG. **3**B further clarify the shape and orientation of HE billet **315** of the FIG. **3** embodiment and as shown in FIG. **4** and FIG. **6**, respectively. The orientation of HE **315**, axis **337** and horizontal plane **345** in FIG. **3**A being the same as in FIG. **4**; with the aft head height HE section "A" **338** and forward vertical line **314**, full circumference conical HE section "B" **339** being located between aft vertical line **314** forward vertical line **313**, and HE section "C" with wing explosive **340**A and **340**B forward of vertical line **313**. The orientation of HE **315**, axis **337** and horizontal plane **345** in FIG. **3**B being the same as in FIG. **6**; with the aft head height HE section A **338** and forward vertical line **314**, full circumference conical HE section B **339** located between aft vertical line **314** and forward vertical line **313**, and HE section C with wing explosive **340**A and **340**B forward of vertical line **313**.

Vertical line **313** and **314** of FIG. **3**A and FIG. **3**B share the same longitudinal position with **313** and **314** as FIG. **4** and FIG. **6**. Vertical line **314** is located longitudinally at apex **308** of FIG. **4** and FIG. **6**, and vertical line **313** is longitudinally located at wing vertex of FIG. **4** and FIG. **6**. FIG. **4** is a vertical sectional view taken along line **4-4** of FIG. **3** that extends from the aft end detonator holder **336** through the fore radial midpoint of the wing-like extensions or flutes **325**A and **325**B at the base end **320**A and **320**B of EW liner **305** with an elevated view of parabolic flat face **310**F.

The lateral cross section of FIG. **4** along line **4-4** is coincident with Axilinear device **300** symmetrical axis **337**, and extends perpendicular to the horizontal plane **345**, which is also coincident with axis **337** and equidistant from the wing-like extensions or flutes **325**A and **325**B. EW liner **305** has a liner wall thickness that can remain constant or gradually decrease in thickness from the aft apex **308** to the base end **320**A and **320**B. The charge body **310** has two flat faced parabolic sides **310**F in the 9 and 3 o'clock position that have parabolic faces that geometrically match the EW liner **305** parabolic faces **330**A and **330**B, when coupled together these faces make a tight fitting body and liner coupling that supports the EW liner **305** wings and serves as containment for HE billet **315** along the partial circumference portion of EW liner **305**. There is no HE or EW liner **305** material confinement laterally outside of the two parabolic sides **310**F.

As shown in FIG. **4**, the Axilinear shaped charge device **300** consists of a body **310**, EW liner **305**, high explosive (HE) billet **315**, having an axisymmetric aft area with detonator **336**, detonator holder **335**, detonation initiation point **307**, and liner apex **308**, and a axisymmetric as well as planar symmetric (Axilinear) fore area that consists of liner extended wings **325**A and **325**B and liner base ends **320**A and **320**B. Initiation of the HE billet of this novel device can be achieved by any suitable readily available detonation initiation devices.

Device **300** is axisymmetric or symmetrical about a longitudinal axis **337** from the aft end near detonator **336** to the middle liner wing vertex **332**A and **332**B of the EW liner **305**; forward of wing vertex **332**A and **332**B device **300** is Axilinear with two symmetrical curved extended wings **325**A and **325**B being axisymmetric with axis **337** and also planar symmetric about two central perpendicular reference planes, a horizontal plane in the 3 and 9 o'clock positions, and a vertical plane in the 12 and 6 o'clock positions.

Vertical line **313** and **314** of FIG. **3**B and FIG. **3**B share the same longitudinal position with vertical line **313** and **314** in FIG. **4** and FIG. **6**. Vertical line **314** is located longitudinally at apex **308** of FIG. **4** and FIG. **6**, and vertical line **313** is longitudinally located at wing vertex of FIG. **4** and FIG. **6**. The vertical 12 and 6 o'clock reference plane (FIG. **2** vertical plane **246**) is coincident with axis **337** and passes through the middle of each extended wing **325**A and **325**B, the parabolic faces **330**A and **330**B are planar symmetric or mirrored about this plane. The horizontal 3 and 9 o'clock reference plane (FIG. **2** horizontal collapse plane **245**) is coincident with axis **337** and passes through each wing vertex **332**A and **332**B, this plane is also known as the wing collapse plane and the wings **325**A and **325**B are planar symmetric or mirrored about this plane. The jet produced by detonating an Axilinear shaped charge device **300** is axisymmetric for the forward rod portion of the jet and planar symmetric for the aft portion, this aft spade portion of the jet being shaped somewhat like a linear shaped charge jet, thusly named Axilinear.

The Axilinear shaped charge device **300** is shown with a conical EW liner **305**, other geometrical shaped (i.e. hemispherical, tulip, or trumpet) hollow cavity formed liners with extended liner wings can also be used. EW liner **305** has a full circumference axisymmetric conical profile section **322** with included angle A that is longitudinally between aft apex **308** and middle liner wing vertex **332**A and **332**B, and a Axilinear partial circumference wing section **333** toward the fore end with two symmetrically opposing conical fluted wing extensions **325***a* and **325**B with included angle A that extend longitudinally from the middle liner wing vertex **332**A and **332**B to the forward liner base ends **320**A and **320**B.

The forward liner wing extensions **325**A and **325**B are symmetrical to each other and positioned one hundred and eighty degrees apart, opposing each other planar symmetrically about the horizontal plane and is axisymmetric about longitudinal axis **337** of the device. The absence of liner wall material on opposing sides of the wing section **333** at the forward base end of the liner forms two parabolic faces **330**A and **330**B that are parallel and symmetric with each other about longitudinal axis **337** and the vertical plane. Both liner parabolic faces **330**A and **330**B have a vertex at wing vertex **332**A and **332**B and open toward the base ends **320**A and **320**B with parabolic end points at the wing arc ends **321**A and **321**B.

EW liner **305** maintains its conical profile and liner wall **309** thickness profile from aft end apex **308** of the full circumference conical section **322** to wing vertex **332** and continues with the same profile to the fore end of the extended wings **325**A and **325**B at the base ends **320**A and **320**B of the partial circumference wing section **333**. Liner wall **309** transitions from a full circumference conical profile at wing vertex **332**A and **332** B into 180 degree symmetrically opposing wing like or fluted extensions **325**A and **325**B that extend from the full circumference conical profile section **322** at wing vertex **332**A and **332**B to the base end **320**A and **320**B of the liner.

The liner wing extensions **325**A and **325**B shown in FIG. **4** retain the same curvature, included angle A, and wall **309** thickness profile as the full conical profile section **322** portion of the liner; but the extended wings **325**A and **325**B could also have a larger or smaller included angle A and wall thickness **309** than the conical section **322**, as long as they maintain planar symmetry to one another. Being planar symmetric and having partial circumference conical curvature allows the wing-like extensions or flutes **325**A and **325**B to converge at very high pressures on the collapse plane, raising the temperature and ductility of the converging wing material to the required level for Munroe jetting.

HE billet **315** can be pressed, cast or hand packed from any commercially available high order explosive. HE billet **315** is in intimate contact with the outer liner surface **316** of EW liner **305** from the aft apex **308** to the forward wing vertex **332**A and **332**B of the conical profile section **322** and from the wing vertex **332**A and **332**B to the base ends **320**A and **320**B and wing arc ends **321**A and **321**B of the wing section **333**. HE billet **315** has three distinct sections, a head height or aft HE section "A" **338** as measured longitudinally between HE initiation point **307** and liner apex **308**, a mid-section or full conic HE section "B" **339** as measured longitudinally from apex **308** to wing vertex **332**A and **332**B, that fully encompasses the liner conical section **322**, and forward HE section "C" that contains two partial circumference wing HE sections **340**A and **340**B as measured longitudinally from wing vertex **332**A and **332**B to base ends **320**A and **320**B that conform to the shape of the liner wing extensions **325**A and **325**B.

HE section A **338** can be lengthened or shortened longitudinally by increasing or decreasing the length of body **310**, greater head height gives a flatter detonation wave before it comes in contact with the liner. Flatter detonation waves at time of liner impact typically increase jet tip velocity and target penetration, head height optimization is a balance between jet performance and minimizing the explosive charge. The optimum head height can be determined by computer code and live testing to obtain the least amount HE volume needed to efficiently obtain maximum jet mass, velocity and target penetration. A typical head height for a conical lined shaped charge would be ½ inch space permitting.

The shape and volume of HE section B **139** is defined by the area between the inside surface **312** of body **310** and outside surface **316** of EW liner **305** from aft apex **308** to forward body face **310**E located at wing vertex **332**A and **332**B, and makes a full circumference or revolution around liner section **322**. The shape and volume of the two symmetrical wing HE sections **340**A and **340**B of HE section C **340** are defined by the area between the inside surface **312** of body **310** and outside surface **316** of EW liner **305** from aft wing vertex **332**A and **332**B to forward base ends **320**A and **320**B, and are partial circumference volumes about each wing between the wing arc end points **321**A and **321**B. HE billet **315** can have a super-caliber diameter (i.e. larger than the liner base diameter) necessary for full convergence of the base end of the liner wing extensions **325**A and **325**B to obtain maximum velocity and mass of the spade jet.

The forward section C **333** consists of two less than full circumference liner walls **309** extending beyond the end of section B **322**, creating partial conical or curved wing extensions **325**A and **325**B, wing vertices **332**A and **332**B and parabolic faces **330**A and **330**B that are symmetrically one hundred and eighty degrees apart. The wing vertex **332**A and **332**B and flat parabolic faces **330**A and **330**B are formed from the absence of material on two symmetrically opposing sides of the base end of the conical profile. Wing arc ends **321**A and **321**B are parabolic end points on the forward edge of liner **305**.

The wing extensions **325**A and **325**B create an axisymmetric and planar symmetric opposing partial radial hollow concavities on the inside liner wall surface **317**; HE detonation pressures on these concavities provides a partial radial convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow and hydrodynamic jetting.

The collapse of the wing extensions **325**A and **325**B of section C **333** produces a wide planar symmetric stretching non round spade shaped jet which cuts a deep slot rather than a round hole; the mass, width, length, stretch rate, velocity, and time of flight of the spade jet is directly proportional to the liner wall length of section C **333**, included angle A, and liner wall **309** thickness of section C **333**. If section C **333** is shortened and the overall length "L" is unchanged section B **322** will become longer. Increasing the length of section B **322** will increase the rod jet length, mass and penetration depth, and will decrease the length, width, mass and penetration depth of the spade jet; length adjustments to sections B and C work in concert, when the rod jet is lengthened the spade jet will be shortened and vice versa shortening the rod jet will lengthen the spade jet.

During collapse of the liner full conical section **322**, liner material radially converges along the longitudinal axis **337** into a rod jet from the detonation of HE section A **338** and HE section B **339**; the collapse of full conical section **322** is followed by the collapse of the extended liner wings **325**A and **325**B of the partial circumference section **333** into a spade jet from the detonation of wing HE sections **340**A and **340**B of HE section C. Wing HE sections **340**A and **340**B are coupled to the outer liner surface **316** of each wing from the aft wing vertex **332**A and **332**B to the forward wing base ends **320**A and **320**B and the wing arc ends **321**A to **321**B.

The radial curvature of the opposing liner wing extensions **325**A and **325**B provides the radial material convergence during collapse needed to raise the temperature and pressure of the collapsed liner material, to the required level for plastic flow and Monroe jetting to occur, this increases the ductility allowing for longer jet breakup length. During collapse the full conical section **322** of the liner will form an axisymmetric rod jet along the longitudinal axis **337** followed by the concave liner wing extensions **325**A and **325**B being driven to a common collapse plane by HE **340**A and **340**B, the colliding wing extensions material will form into a high velocity flat planar symmetric spade shape jet.

As the collapsed wing extensions material moves forward along longitudinal axis **337** it also spreads laterally outward forming the spade shaped jet along the horizontal collapse plane. The formation of the spade jet is due to the absence of liner material, explosive and confinement on the liner sides with the two flat parabolic faces **330**A and **330**B that are adjacent to and ninety degrees out of phase from the flutes or wing extensions **325**A and **325**B. The orientation of device **300** can be rotated about axis **337** and the spade jet orientation will rotate equally in the same direction, if device **300** is rotated 45 degrees clockwise about axis **337** the collapse plane will also rotate 45 degrees clockwise and the spade jet will stretch longitudinally forward on axis **337** and laterally along the rotated collapse plane.

The EW liner **305** is the working material of the shaped charge and is mounted to body **310** at the forward end of device **300**, at the base ends **320**A and **320**B of the liner wing extensions **325**A and **325**B; and adjacent to the wings the liner parabolic faces **330**A and **330**B are mounted to the body **310** parabolic faces **310**F. Body **310** consist of four distinct areas, a aft cylindrical area **310**C that provides mounting for an initiation device that is coupled to the aft end of HE **315**, followed by a boat tailed area **310**B that contains the HE section A **338**, followed by cylindrical area **310**A that contains HE section B **339** that is coupled to the full conical liner section **322**; and HE section C containing wing sections **340**A and **304**B that are coupled to the extended wings of liner section **333**, and body area **310**D at the forward end of cylindrical section **310**A that transitions from a cylindrical shape into two parallel flat parabolic faces **310**F that are planar symmetric to each other and are coupled to the parabolic liner faces **330**A and **330**B.

Body area **310**D has two functions, it provides two opposing side mounting faces **310**F for the liner extended wings and also has flat faces **310**E that is the forward containment boundary of HE section **339**; this boundary is located at wing vertex **332**A and **332**B, and is also the liner wing transition point from the full circumference conical section **322** to the extended wing section **333**. The containment of HE pressures during the detonation time period by body area **310**D is important for proper collapse of the wings and spade jet formation. Shape charge liners for the most part are made from copper but liners may be made from most any metal, ceramic, powdered metals, tungsten, silver, copper, glass or combination of many materials. Body **310** would typically be made from aluminum or steel but could be made of almost any metal or plastic as long as it provides the correct amount of tamping for proper jet formation and desired jet velocity during the detonation of HE billet **315**.

The EW liner **305** is a modified cone or other shape with two distinct geometrical sections, the aft end of the liner is a full conical profile section **322** with an apex **308**, followed by the forward end wing section **333** with two liner wing extensions **325**A and **325**B that extend forward from the full conical or other shape profile section **322** at wing vertex **332**A and **332**B to the wing base ends **320**A and **320**B at the fore end of EW liner **305**. The liner wing extensions **325**A and **325**B maintain the same included angle A liner wall **309** thickness profile and curvature of the full conical profile section **322**.

The included angle A of EW liner **305** needed to obtain Munroe effect jetting should be from 36 to 120 degrees. The jet velocity achieved from a shaped charge is dependent on the liner wall **309** thickness and included angle A of the liner; a narrower included angle results in a faster less massive jet, and a wider included angle results in a slower more massive jet. Jet velocities can vary from 4 to 10 km/s depending on the type and quality of liner material, included angle A of the liner, liner wall **309** thickness, the charge to mass ratio of HE to liner, bulk density of the liner, surface finish of the liner wall, and body geometries; very small changes of any of these variables can make large differences in jet velocity and trajectory.

The HE billet **315** is contained between the inner surface **312** of body **310** and the outer surface **316** of the EW liner **305**. HE billet **315** provides the energy to collapse the EW liner **305**, increasing the ductility of the EW liner **305** material, causing it to form a compound jet in the shape of a very high speed rod jet from the full conical section **322** material followed by a flattened spade shaped jet from the liner wing section **333** material; the spade jet is slower than the rod jet from conical section **322** but much faster than a typical "V" shaped liner found in common linear shaped charge because of the cavity of the wing section **333**.

Body **310** provides a mounting surface for EW liner **305** which is held to body **310** at the liner base ends **320**A and **320**B and at the parabolic faces **330**A and **330**B. The base end of EW liner **305** does not form a full circumference; it consists of two opposing concave surfaces or wing extensions **325**A and **325**B and the corresponding wing base ends **320**A and **320**B at the forward end of the liner. Body **310** also serves as a containment vessel for the delicate HE billet **315** and protects it from damage or impact by supporting the outer diameter of HE billet **315**. Body **310** also provides tamping for the HE billet **315** depending on body wall **306** thickness and material density, HE tamping can be increased or decreased if needed to improve jet performance or reduce total HE mass.

The purpose of removing the base end material on symmetrically opposing sides of EW liner **305** and creating the wing-like extensions **325**A and **325**B is twofold. The first purpose is to form the partial circumference conical wing-like extensions or flutes **325**A and **325**B and when collapsed converge to form the flat aft spade shaped portion of the jet; the flattened spade jet spreads laterally and erodes an elongated slot in target material. The second purpose being to allow for close lateral proximity of multiple adjacent devices resulting in multiple tightly spaced rod and intersecting spade jet perforations, creating a large coupled slotted target perforation.

Since the EW liner **305** material is not being confined along the two removed portions of the liner at parabolic faces **330**A and **330**B, the collapse of the wing-like extensions or flutes **325**A and **325**B will produce a flat jet, much like a linear shaped charge, but at a much higher velocity, stretching laterally and longitudinally. The transition from the conical profile section **322** to the remaining wing-like extensions or flutes **325**A and **325**B of EW liner **305** is very gradual so as to maintain continuity between the rod and spade portions of the jet.

The shaped charge body **310** has a frustoconical or boat tailed portion **310**B near the aft end of the shaped charge device **300** that begins at detonator holder **335** and increases in diameter longitudinally to about the apex **308** of EW liner

305. The cylindrical portion **310**A of the body **310** begins at about the apex **308** of the EW liner **305** and extends longitudinally to the forward end of device **300**. The forward end of cylindrical portion **310**A has two planar symmetrical **310**D portions, each with a cylindrical outer face **310**G, an inner parabolic flat face **310**F and internal flat face **310**E. The two internal parabolic flat faces **310**F of the body begin at the liner wing vertex **332**A and **332**B and end at wing arc ends **321**A and **321**B; faces **310**F are symmetrical and parallel to each other, and perpendicular with the wing collapse plane that is centrally located and collinear with longitudinal axis **337** between the two flat faces **310**F.

Flat faces **310**F and faces **310**E of the shaped charge body **310**D help confine the wing HE **340**A and **340**B portion of HE billet **315** by providing cavity closure between the flat faces **310**F and the liner parabolic faces **330**A and **330**B on each side of the wing-like extensions or flutes **325**A and **325**B of the EW liner **305**. The body **310** preferably tapers or boat tails smaller in some manner toward the rearward end **310**B from aft of the liner apex **308** toward the detonator holder **335** minimizing the overall mass of HE billet **315**, reducing the amount of explosive by boat tailing body **310** increases the charge efficiency without affecting the liner collapse performance, and reduces unwanted collateral target damage from excessive explosive mass.

The invention described and depicted herein produces a two part stretching jet, the forward portion is a rod like asymmetric jet and the aft portion is spread into a sheet like planar symmetric shape reminiscent of the jetting of a linear shaped charge. In order to achieve the greatest jet length and penetration depth the jetting process of a shaped charge requires the liner material to reach a high temperature during collapse, which allows plastic flow of the collapsed liner material and produces a long stretching jet. Since jet length and penetration are directly proportional it is reasonable to make the greatest effort to provide the longest and most robust jet possible.

The above description of the directions of the shaped charge body and liner can be reversed whereby the axisymmetric jet is aft of the spade jet, there can be multiple sections alternating from axisymmetric and planar symmetric sections that produce alternating spade rod spade rod jet. The sections making up a liner do not have to have the same internal angle, thickness profile or material. The internal angles of these sections can vary from 36 degrees to 120 degrees and still produce Munroe jetting, that is to say a ductile jet having a velocity gradient from tip to tail. The arc length of each wing as encompassed by radial lines radiating from the central axis and intersecting each cord end of the arc of the wing can vary from 90 to 140 degrees.

An apex **308** toward the aft end of the full circumference conical section "B" **322**, and a partial circumference wing section "C" **333** with base ends **320**A and **320**B, liner wing extensions **325**A and **325**B, and wing base arc ends **321**A and **321**B toward the forward end of EW liner **300**. The liner wing extensions **325**A and **325**B extend or protrude in a forward direction from section A **322** beginning at wing vertex **332**A and **332**B and ending at the base ends **320**A and **320**B. Wing vertex **332**A and **332**B are positioned longitudinally at vertical line **313** where the liner transitions from the full circumference conical section B **322** into a partial circumference conical or other shape wing section C **333**. Liner wall **309** of section B **322** and section C **333** can vary in thickness, curvature, and included angle A can be increased or decreased to achieve desired rod and spade jet velocities and mass.

The conical section B **322** and wing section C **333** share a common longitudinal symmetrical axis **337**, section C **333** also has a horizontal collapse plane **345** in the 3 to 9 o'clock position and vertical plane **346** in the 12 to 6 o'clock position they are perpendicular to each other and intersect each other at symmetrical axis **337**. Section B **322** is axisymmetric or symmetrical about axis **337** in all radial planes for 360 degrees, whereas section C **333** has two parabolic faces **330**A and **330**B that are planar symmetric about vertical plane **346**; and two extended wings **325**A and **325**B that are planar symmetric about horizontal plane **345** and also axisymmetric between the wing arc ends **321**A and **321**B about axis **337**. The EW liner **300** is a modified hollow cone, but could also be other relative hollow shapes (i.e. hemisphere, trumpet, tulip), having two opposing equal sections removed at the base end of the liner, creating two extended wings like **325**A and **325**B and two parabolic faces like **330**A and **330**B.

The absence of the two opposing equal liner wall sections at the liner base end creates two equal 180 degree opposed liner wing extensions **325**A and **325**B or flutes. The included angle A of the hollow conical liner and the longitudinal length of the full section B **322** portion of the liner determines the longitudinal wing length from wing vertex **332**A and **332**B to the base end **320**A and **320**B of the extended wings **325**A and **325**B or fluted portions of the liner and thusly the amount of the liner wall **309** material that is dedicated to producing the spade or flattened portion of the jet. The longitudinal length of section B **322** and the extended wings **325**A and **325**B or flutes can be increased or decreased to achieve the desired ratio of rod to spade length of the jet created from EW liner **300**. The thickness of the liner wall **309** can gradually increase or decrease from the apex **308** to the base end **320**A and **320**B or anywhere along the wall length; a tapering liner wall **309** thickness will help balance the liner to HE mass ratio as the liner cone diameter increases toward the base end **320**A and **320**B.

After the collapse of full conical section B **322** by HE section B into a rod jet the curved wing-like extensions or flutes **325**A and **325**B of wing section C **333** are driven to horizontal plane **345** and symmetrical axis **337** of the EW liner **305** by the HE section C with wing explosive **340**A and **340**B, the colliding material forms a flat blade shape jet instead of a round jet because of the lack of liner material and HE confinement on the flat faced sides **310**F that are ninety degrees out of phase from the wing-like extensions or flutes **325**A and **325**B. The transition from conical section B **322** to wing section C **333** is gradual which allows the spade jet to stay connected to the forward rod jet as both portions of the jet stretch longitudinally forward along axis **337**; and because of the lack of liner confinement on the two opposing parabolic faces **310**F the spade jet will widen laterally on horizontal plane **345** as it stretches longitudinally forward with the forward rod jet.

The horizontal plane **345** of the wing section C **333** is seen as a horizontal longitudinal line that is coincident with symmetrical axis **337** in FIG. **4**. Horizontal plane **345** is where the liner material of the two 180 degree opposing extended axisymmetric and planar symmetric wing extensions **325**A and **325**B of EW liner **305** will converge from the detonation pressures of HE section C with wing explosive **340**A and **340**B forming the spade jet **342** shown in FIG. **5**. Horizontal plane **345** also represents the orientation and direction of the wide lateral cross-section of spade jet **342**, which are coplanar and coincident to each other. The liner wing extensions **325** of FIG. **4** and the view of jet **301** of FIG. **5** are correctly oriented to each other to represent the collapse of the EW liner **305** from this viewpoint, the spade jet **342** is seen as a thin section along symmetrical axis **337** and horizontal plane **345** that decreases in thickness from the aft end spade jet tail **349** to the forward end rod/spade transition point **348** where it is connected to the aft end of rod jet **343**. Jet **301** would form within the hollow cavity of EW liner **305** of device **300** and at some time after liner collapse would eventually stretch past the base end **325**A and **325**B, it is shown in FIG. **5** fully outside of and to the right of the device for easier viewing.

Body **310** contains and protects HE billet **315** and provides a mounting surface for EW liner **305** at its base ends **320**A and **320**B. The HE billet **315** detonation is initiated by any suitable commercially available detonator **336** on the device symmetrical axis **337** at initiation point **307**. With respect to the longitudinal symmetrical axis **337** of device **300**, the liner full circumference conical section B **322** is aft of wing vertex **332**A and the liner wing section C **333** is forward of the wing vertex **332**A. The jet **301** produced by device **300** has three distinct regions and shapes; a high velocity 7-9 km/s round axisymmetric rod jet **343** with forward jet tip **344** and aft rod/spade jet transition point **348**, followed by a lower velocity 4-7 km/s planar symmetric flattened spade jet **342** mid-section and jet tail **349**, followed by the slug separation area **347** and a low velocity ½ km/s slug **350**.

The forward axisymmetric rod jet **343** in FIG. **5** is formed from the conical section B **322** of EW liner **305** that starts at apex **308** and ends at the wing vertex **332**A of the parabolic flat face **330**A. At wing vertex **332**A the conical section B **322** of the liner transitions into the wing section C **333** with two opposing concave liner wing extensions **325**A and **325**B or flutes, formed due to the liner side truncation. The aft spade jet **342** is formed from the collapse of the liner wing section C **333** opposing liner wing extensions **325**A and **325**B portions of EW liner **305**. The aft spade jet **342** being flat and wide, similar to a conventional linear shaped charge jet but more massive, directionally controllable and at a much higher velocity, thus the Axilinear name. The amount of liner material designated to the aft and forward portions of the combination spade and rod jet can be adjusted by shortening or lengthening conical section B **322** and wing section C **333** of EW liner **305** to give differing lengths and widths of rod and spade shaped jet sections.

In FIG. **5**, the jet **301** consists of an aft slug **350**, spade jet tail **349**, spade jet **342**, rod/spade jet transition point **348**, rod jet **343**, and forward jet tip **344**. Jet and slug velocities, angle of projection, thickness, spade blade width and length of both jet sections can vary depending on device **300** design. The forward longitudinal velocity of jet **301** is greatest at jet tip **344** and has a velocity gradient from the forward end jet tip **344** to the aft end spade jet tail **349**. Jet **301** velocity and the velocity gradient are factors of device design, type of explosive, and the type of material used to make EW liner **305**. Amongst many other design factors of device reducing the liner included angle A will increase jet velocity and the velocity gradient. The jet velocity gradient and material ductility directly affects the stretch rate of jet **301** and ultimately the length and width of both the rod jet **343** and spade jet **342** portions of jet **301**, higher velocity gradients will result in a thinner and longer jet. This depiction of the jet is at a finite time after the detonation of device. The jet at an earlier time frame after detonation of HE billet **315** would be shorter in length and thicker, at a later time it would have stretched forward becoming longer and thinner because of the velocity gradient and ductile stretching of the EW liner **305** material.

The longitudinal depiction of jet **301** in FIG. **5** has the forward jet tip **344** and rod jet **343** on the right hand side of aft spade jet **342** with a middle jet transition point **348**. The jet transition point **348** is where the material contributed to rod jet **343** from the collapse of the conical section B ends and the spade jet **342** material contributed by the collapse of wing section C **333** begins. The FIG. **5** jet orientation is an edge view of spade jet **342** and collapse plane **345** which is the thinnest cross-section of the spade and the result of the liner wings **325**A and **325**B of FIG. **3** being in the 6 and 12 o'clock positions. The spade portion of jet **301** in FIG. **5** is slightly thicker at the aft end jet tail **349** with a thinning cross-section toward the foreword end jet transition point **348** this is due to stretching from a higher velocity forward end, matching the rod jet thickness due to the longitudinal jet stretch rate.

The jet **301** is formed from the collapse of EW liner **305** caused by a detonation shock wave and converging pressure toward symmetrical axis **337** from detonating HE billet **315**, that is traveling longitudinally from aft HE initiation point **307** to forward base ends **320**A and **320**B of device. As the detonation wave created from detonating HE billet **315** progresses from the aft end HE section A **338** forward to HE section B **339** of device it first collapses the section B of EW liner **305** starting at apex **308** and continuing forward to vertex **332**A and **332**B creating the rod jet **343** portion of jet **301**, the collapse and jetting from section B of the liner resembles that of a typical axisymmetric conical lined shaped charge. As the detonation wave moves forward of wing vertex **332**A and **332**B the HE section C wing explosive **340**A and **340**B collapse the extended wings **325**A and **325**B of section C **333** starting at vertex **332**A and **332**B and ending at base end **320**A and **320**B forming the spade jet **342** portion of jet **301**. Both rod and spade portions of jet **301** stretch and elongate longitudinally forward along axis **337** and spade portion **342** also widens laterally on plane **345**; as time progresses after initial detonation and collapse of EW liner **305**, and at some elongation length and time after collapse the higher velocity rod and spade jet will break free of the collapsed liner mass. The remaining liner mass becomes a lower velocity slug **350** represented by slug separation area **347**.

FIG. **6** is a horizontal sectional view taken along line **6-6** of FIG. **3** that further illustrate the embodiment of FIG. **1** with an elevated view of collapse plane **345**, the inside liner surface **317** and EW liner wing **325**B. That is, the orientation of HE **315**, axis **337** and horizontal plane **345** in FIG. **3**B being the same as in FIG. **6**; with the aft head height HE section A **338** and forward vertical line **314**, full circumference conical HE section B **339** located between aft vertical line **314** and forward vertical line **313**, and HE section C with wing explosive **340**A and **340**B forward of vertical line **313**. The FIG. **6** cross-sectional cut taken along line **6-6** of FIG. **3** is coincident with vertical collapse plane **345** which intersects the axis of symmetry **337** that extends longitudinally through the middle of device **300** from the aft detonator holder **335** to the fore base end **320**B of EW liner **305**. FIG. **6** further clarifies how body **310**, **310**D and parabolic flat face **310**F contain HE billet **315** and provide mounting surfaces for EW liner **305**.

As shown in FIG. **6**, the Axilinear shaped charge device **300** consists of a body **310**, EW liner **305**, high explosive (HE) billet **315**, having an axisymmetric aft area with detonator **336**, detonator holder **335**, detonation initiation point **307**, and liner apex **308**, and a axisymmetric as well as planar symmetric (Axilinear) fore area that consists of liner extended wings **325**A and **325**B and liner base ends **320**A and **325**B. Initiation of the HE billet of this novel device can be achieved by any suitable readily available detonation initiation devices.

Device **300** is axisymmetric or symmetrical about a longitudinal axis **337** from the aft end near detonator **336** to the middle liner wing vertex **332**A and **332**B of the EW liner **305**; forward of wing vertex **332**A and **332**B device **300** is Axilinear with two symmetrical curved extended wings **325**A and **325**B being axisymmetric with axis **337** and also planar symmetric about two central perpendicular reference planes, a horizontal plane in the 3 and 9 o'clock positions, and a vertical plane in the 12 and 6 o'clock positions.

Vertical line **313** of FIG. **3**B share the same longitudinal position with HE **313** in FIG. **6**. Vertical line **313** is longitudinally located at wing vertex of FIG. **4**. The vertical 12 and 6 o'clock reference plane (FIG. **2** vertical plane **246**) is coincident with axis **337** and passes through the middle of each extended wing **325**A and **325**B, the parabolic faces **330**A and **330**B are planar symmetric or mirrored about this plane. The horizontal 3 and 9 o'clock reference plane (FIG. **2** horizontal collapse plane **245**) is coincident with axis **337** and passes through each wing vertex **332**A and **332**B, this plane is also known as the wing collapse plane and the wings **325**A and **325**B are planar symmetric or mirrored about this plane. The jet produced by detonating an Axilinear shaped charge device **300** is axisymmetric for the forward rod portion of the jet and planar symmetric for the aft portion, this aft spade portion of the jet being shaped somewhat like a linear shaped charge jet, thusly named Axilinear.

The Axilinear shaped charge device **300** is shown with a conical EW liner **305**, other geometrical shaped (i.e. hemispherical, tulip, or trumpet) hollow cavity formed liners with extended liner wings can also be used. EW liner **305** has a full circumference axisymmetric conical profile section **322** with included angle A that is longitudinally between aft apex **308** and middle liner wing vertex **332**A and **332**B, and a Axilinear partial circumference wing section **333** toward the fore end with two symmetrically opposing conical fluted wing extensions **325***a* and **325**B with included angle A that extend longitudinally from the middle liner wing vertex **332**A and **332**B to the forward liner base ends **320**A and **320**B.

The forward liner wing extensions **325**A and **325**B are symmetrical to each other and positioned one hundred and eighty degrees apart, opposing each other planar symmetrically about the horizontal plane and is axisymmetric about longitudinal axis **337** of the device. The absence of liner wall material on opposing sides of the wing section **333** at the forward base end of the liner forms two parabolic faces **330**A and **330**B that are parallel and symmetric with each other about longitudinal axis **337** and the vertical plane. Both liner parabolic faces **330**A and **330**B have a vertex at wing vertex **332**A and **332**B and open toward the base ends **320**A and **320**B with parabolic end points at the wing arc ends **321**A and **321**B. Forward body face **310**E is located at wing vertex **332**A and **332**B, and fills the face hollow concavity **310**F.

EW liner **305** maintains its conical profile and liner wall **309** thickness profile from aft end apex **308** of the full circumference conical section **322** to wing vertex **332** and continues with the same profile to the fore end of the extended wings **325**A and **325**B at the base ends **320**A and **320**B of the partial circumference wing section **333**. Liner wall **309** transitions from a full circumference conical profile at wing vertex **332**A and **332** B into 180 degree symmetrically opposing wing like or fluted extensions **325**A and **325**B that extend from the full circumference conical profile section **322** at wing vertex **332**A and **332**B to the base end **320**A and **320**B of the liner.

The liner wing extensions **325**A and **325**B shown in FIG. **6** retain the same curvature, included angle A, and wall **309** thickness profile as the full conical profile section **322** portion of the liner; but the extended wings **325**A and **325**B could also have a larger or smaller included angle A and wall thickness **309** than the conical section **322**, as long as they maintain planar symmetry to one another. Being planar symmetric and having partial circumference conical curvature allows the wing-like extensions or flutes **325**A and **325**B to converge at very high pressures on the collapse plane, raising the temperature and ductility of the converging wing material to the required level for Munroe jetting.

HE billet **315** can be pressed, cast or hand packed from any commercially available high order explosive. HE billet **315** is in intimate contact with the outer liner surface **316** of EW liner **305** from the aft apex **308** to the forward wing vertex **332**A and **332**B of the conical profile section **322** and from the wing vertex **332**A and **332**B to the base ends **320**A and **320**B and wing arc ends **321**A and **321**B of the wing section **333**. HE billet **315** has three distinct sections, a head height or aft HE section "A" **338** as measured longitudinally between HE initiation point **307** and liner apex **308**, a mid-section or full conic HE section "B" **339** as measured longitudinally from apex **308** to wing vertex **332**A and **332**B, that fully encompasses the liner conical section **322**, and forward HE section "C" that contains two partial circumference wing HE sections **340**A and **340**B as measured longitudinally from wing vertex **332**A and **332**B to base ends **320**A and **320**B that conform to the shape of the liner wing extensions **325**A and **325**B.

HE section A **338** can be lengthened or shortened longitudinally by increasing or decreasing the length of body **310**, greater head height gives a flatter detonation wave before it comes in contact with the liner. Flatter detonation waves at time of liner impact typically increase jet tip velocity and target penetration, head height optimization is a balance between jet performance and minimizing the explosive charge. The optimum head height can be determined by computer code and live testing to obtain the least amount HE volume needed to efficiently obtain maximum jet mass, velocity and target penetration. A typical head height for a conical lined shaped charge would be ½ inch space permitting.

The shape and volume of HE section B **139** is defined by the area between the inside surface **312** of body **310** and outside surface **316** of EW liner **305** from aft apex **308** to forward body face **310**E located at wing vertex **332**A and **332**B, and makes a full circumference or revolution around liner section **322**. The shape and volume of the two symmetrical wing HE sections **340**A and **340**B of HE section C **340** are defined by the area between the inside surface **312** of body **310** and outside surface **316** of EW liner **305** from aft wing vertex **332**A and **332**B to forward base ends **320**A and **320**B, and are partial circumference volumes about each wing between the wing arc end points **321**A and **321**B. HE billet **315** can have a super-caliber diameter (i.e. larger than the liner base diameter) necessary for full convergence of the base end of the liner wing extensions **325**A and **325**B to obtain maximum velocity and mass of the spade jet.

The forward section C **333** consists of two less than full circumference liner walls **309** extending beyond the end of section B **322**, creating partial conical or curved wing extensions **325**A and **325**B, wing vertices **332**A and **332**B and parabolic faces **330**A and **330**B that are symmetrically one hundred and eighty degrees apart. The wing vertex **332**A and **332**B and flat parabolic faces **330**A and **330**B are formed from the absence of material on two symmetrically opposing sides of the base end of the conical profile. The wing extensions **325**A and **325**B create an axisymmetric and planar symmetric opposing partial radial hollow concavities on the inside liner wall surface **317**; HE detonation pressures on these concavities provides a partial radial convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow and hydrodynamic jetting.

The collapse of the wing extensions **325**A and **325**B of section C **333** produces a wide planar symmetric stretching non round spade shaped jet which cuts a deep slot rather than a round hole; the mass, width, length, stretch rate, velocity, and time of flight of the spade jet is directly proportional to the liner wall length of section C **333**, included angle A, and liner wall **309** thickness of section C **333**. If section C **333** is shortened and the overall length "L" is unchanged section B **322** will become longer. Increasing the length of section B **322** will increase the rod jet length, mass and penetration depth, and will decrease the length, width, mass and penetration depth of the spade jet; length adjustments to sections B and C work in concert, when the rod jet is lengthened the spade jet will be shortened and vice versa shortening the rod jet will lengthen the spade jet.

During collapse of the liner full conical section **322**, liner material radially converges along the longitudinal axis **337** into a rod jet from the detonation of HE section A **338** and HE section B **339**; the collapse of full conical section **322** is followed by the collapse of the extended liner wings **325**A and **325**B of the partial circumference section **333** into a spade jet from the detonation of wing HE sections **340**A and **340**B of HE section C. Wing HE sections **340**A and **340**B are coupled to the outer liner surface **316** of each wing from the aft wing vertex **332**A and **332**B to the forward wing base ends **320**A and **320**B and the wing arc ends **321**A to **321**B.

The radial curvature of the opposing liner wing extensions **325**A and **325**B provides the radial material convergence during collapse needed to raise the temperature and pressure of the collapsed liner material, to the required level for plastic flow and Monroe jetting to occur, this increases the ductility allowing for longer jet breakup length. During collapse the full conical section **322** of the liner will form an axisymmetric rod jet along the longitudinal axis **337** followed by the concave liner wing extensions **325**A and **325**B being driven to a common collapse plane by HE **340**A and **340**B, the colliding wing extensions material will form into a high velocity flat planar symmetric spade shape jet.

As the collapsed wing extensions material moves forward along longitudinal axis **337** it also spreads laterally outward forming the spade shaped jet along the horizontal collapse plane. The formation of the spade jet is due to the absence of liner material, explosive and confinement on the liner sides with the two flat parabolic faces **330**A and **330**B that are adjacent to and ninety degrees out of phase from the flutes or wing extensions **325**A and **325**B. The orientation of device **300** can be rotated about axis **337** and the spade jet orientation will rotate equally in the same direction, if device **300** is rotated 45 degrees clockwise about axis **337** the collapse plane will also rotate 45 degrees clockwise and the spade jet will stretch longitudinally forward on axis **337** and laterally along the rotated collapse plane.

The EW liner **305** is the working material of the shaped charge and is mounted to body **310** at the forward end of device **300**, at the base ends **320**A and **320**B of the liner wing extensions **325**A and **325**B; and adjacent to the wings the liner parabolic faces **330**A and **330**B are mounted to the body **310** parabolic faces **310**F. Body **310** consist of four distinct areas, a aft cylindrical area **310**C that provides mounting for an initiation device that is coupled to the aft end of HE **315**, followed by a boat tailed area **310**B that contains the HE section A **338**, followed by cylindrical area **310**A that contains HE section B **339** that is coupled to the full conical liner section **322**; and HE section C containing wing sections **340**A and **304**B that are coupled to the extended wings of liner section **333**, and body area **310**D at the forward end of cylindrical section **310**A that transitions from a cylindrical shape into two parallel flat parabolic faces **310**F that are planar symmetric to each other and are coupled to the parabolic liner faces **330**A and **330**B.

Body area **310**D has two functions, it provides two opposing side mounting faces **310**F for the liner extended wings and also has flat faces **310**E that is the forward containment boundary of HE section **339**; this boundary is located at wing vertex **332**A and **332**B, and is also the liner wing transition point from the full circumference conical section **322** to the extended wing section **333**. The containment of HE pressures during the detonation time period by body area **310**D is important for proper collapse of the wings and spade jet formation. Shape charge liners for the most part are made from copper but liners may be made from most any metal, ceramic, powdered metals, tungsten, silver, copper, glass or combination of many materials. Body **310** would typically be made from aluminum or steel but could be made of almost any metal or plastic as long as it provides the correct amount of tamping for proper jet formation and desired jet velocity during the detonation of HE billet **315**.

The EW liner **305** is a modified cone or other shape with two distinct geometrical sections, the aft end of the liner is a full conical profile section **322** with an apex **308**, followed by the forward end wing section **333** with two liner wing extensions **325**A and **325**B that extend forward from the full conical or other shape profile section **322** at wing vertex **332**A and **332**B to the wing base ends **320**A and **320**B at the fore end of EW liner **305**. The liner wing extensions **325**A and **325**B maintain the same included angle A liner wall **309** thickness profile and curvature of the full conical profile section **322**.

The included angle A of EW liner **305** needed to obtain Munroe effect jetting should be from 36 to 120 degrees. The jet velocity achieved from a shaped charge is dependent on the liner wall **309** thickness and included angle A of the liner; a narrower included angle results in a faster less massive jet, and a wider included angle results in a slower more massive jet. Jet velocities can vary from 4 to 10 km/s depending on the type and quality of liner material, included angle A of the liner, liner wall **309** thickness, the charge to mass ratio of HE to liner, bulk density of the liner, surface finish of the liner wall, and body geometries; very small changes of any of these variables can make large differences in jet velocity and trajectory.

The HE billet **315** is contained between the inner surface **312** of body **310** and the outer surface **316** of the EW liner **305**. HE billet **315** provides the energy to collapse the EW liner **305**, increasing the ductility of the EW liner **305** material, causing it to form a compound jet in the shape of a very high speed rod jet from the full conical section **322** material followed by a flattened spade shaped jet from the liner wing section **333** material; the spade jet is slower than the rod jet from conical section **322** but much faster than a typical "V" shaped liner found in common linear shaped charge because of the cavity of the wing section **333**.

Body **310** provides a mounting surface for EW liner **305** which is held to body **310** at the liner base ends **320**A and **320**B and at the parabolic faces **330**A and **330**B. The base end of EW liner **305** does not form a full circumference; it consists of two opposing concave surfaces or wing extensions **325**A and **325**B and the corresponding wing base ends **320**A and **320**B at the forward end of the liner. Body **310** also serves as a containment vessel for the delicate HE billet **315** and protects it from damage or impact by supporting the outer diameter of HE billet **315**. Body **310** also provides tamping for the HE billet **315** depending on body wall **306** thickness and material density, HE tamping can be increased or decreased if needed to improve jet performance or reduce total HE mass.

The purpose of removing the base end material on symmetrically opposing sides of EW liner **305** and creating the wing-like extensions **325**A and **325**B is twofold. The first purpose is to form the partial circumference conical wing-like extensions or flutes **325**A and **325**B and when collapsed converge to form the flat aft spade shaped portion of the jet; the flattened spade jet spreads laterally and erodes an elongated slot in target material. The second purpose being to allow for close lateral proximity of multiple adjacent devices resulting in multiple tightly spaced rod and intersecting spade jet perforations, creating a large coupled slotted target perforation.

Since the EW liner **305** material is not being confined along the two removed portions of the liner at parabolic faces **330**A and **330**B, the collapse of the wing-like extensions or flutes **325**A and **325**B will produce a flat jet, much like a linear shaped charge, but at a much higher velocity, stretching laterally and longitudinally. The transition from the conical profile section **322** to the remaining wing-like extensions or flutes **325**A and **325**B of EW liner **305** is very gradual so as to maintain continuity between the rod and spade portions of the jet.

The shaped charge body **310** has a frustoconical or boat tailed portion **310**B near the aft end of the shaped charge device **300** that begins at detonator holder **335** and increases in diameter longitudinally to about the apex **308** of EW liner **305**. The cylindrical portion **310**A of the body **310** begins at about the apex **308** of the EW liner **305** and extends longitudinally to the forward end of device **300**. The forward end of cylindrical portion **310**A has two planar symmetrical **310**D portions, each with a cylindrical outer face **310**G, an inner parabolic flat face **310**F and internal flat face **310**E. The two internal parabolic flat faces **310**F of the body begin at the liner wing vertex **332**A and **332**B and end at wing arc ends **321**A and **321**B; faces **310**F are symmetrical and parallel to each other, and perpendicular with the wing collapse plane that is centrally located and collinear with longitudinal axis **337** between the two flat faces **310**F.

Flat faces **310**F and faces **310**E of the shaped charge body **310**D help confine the wing HE **340**A and **340**B portion of HE billet **315** by providing cavity closure between the flat faces **310**F and the liner parabolic faces **330**A and **330**B on each side of the wing-like extensions or flutes **325**A and **325**B of the EW liner **305**. The body **310** preferably tapers or boat tails smaller in some manner toward the rearward end **310**B from aft of the liner apex **308** toward the detonator holder **335** minimizing the overall mass of HE billet **315**, reducing the amount of explosive by boat tailing body **310** increases the charge efficiency without affecting the liner collapse performance, and reduces unwanted collateral target damage from excessive explosive mass.

The invention described and depicted herein produces a two part stretching jet, the forward portion is a rod like asymmetric jet and the aft portion is spread into a sheet like planar symmetric shape reminiscent of the jetting of a linear shaped charge. In order to achieve the greatest jet length and penetration depth the jetting process of a shaped charge requires the liner material to reach a high temperature during collapse, which allows plastic flow of the collapsed liner material and produces a long stretching jet. Since jet length and penetration are directly proportional it is reasonable to make the greatest effort to provide the longest and most robust jet possible.

The above description of the directions of the shaped charge body and liner can be reversed whereby the axisymmetric jet is aft of the spade jet, there can be multiple sections alternating from axisymmetric and planar symmetric sections that produce alternating spade rod spade rod jet. The sections making up a liner do not have to have the same internal angle, thickness profile or material. The internal angles of these sections can vary from 36 degrees to 120 degrees and still produce Munroe jetting, that is to say a ductile jet having a velocity gradient from tip to tail. The arc length of each wing as encompassed by radial lines radiating from the central axis and intersecting each cord end of the arc of the wing can vary from 90 to 140 degrees.

An apex **308** toward the aft end of the full circumference conical section "B" **322**, and a partial circumference wing section "C" **333** with base ends **320**A and **320**B, liner wing extensions **325**A and **325**B, and wing base arc ends **321**A and **321**B toward the forward end of EW liner **300**. The liner wing extensions **325**A and **325**B extend or protrude in a forward direction from section A **322** beginning at wing vertex **332**A and **332**B and ending at the base ends **320**A and **320**B. Wing vertex **332**A and **332**B are positioned longitudinally at vertical line **313** where the liner transitions from the full circumference conical section B **322** into a partial circumference conical or other shape wing section C **333**. Liner wall **309** of section B **322** and section C **333** can vary in thickness, curvature, and included angle A can be increased or decreased to achieve desired rod and spade jet velocities and mass.

The conical section B **322** and wing section C **333** share a common longitudinal symmetrical axis **337**, section C **333** also has a horizontal collapse plane **345** in the 3 to 9 o'clock position and vertical plane **346** in the 12 to 6 o'clock position they are perpendicular to each other and intersect each other at symmetrical axis **337**. Section B **322** is axisymmetric or symmetrical about axis **337** in all radial planes for 360 degrees, whereas section C **333** has two parabolic faces **330**A and **330**B that are planar symmetric about vertical plane **346**; and two extended wings **325**A and **325**B that are planar symmetric about horizontal plane **345** and also axisymmetric between the wing arc ends **321**A and **321**B about axis **337**. The EW liner **300** is a modified hollow cone, but could also be other relative hollow shapes (i.e. hemisphere, trumpet, tulip), having two opposing equal sections removed at the base end of the liner, creating two extended wings like **325**A and **325**B and two parabolic faces like **330**A and **330**B.

The absence of the two opposing equal liner wall sections at the liner base end creates two equal 180 degree opposed liner wing extensions **325**A and **325**B or flutes. The included angle A of the hollow conical liner and the longitudinal length of the full section B **322** portion of the liner determines the longitudinal wing length from wing vertex **332**A and **332**B to the base end **320**A and **320**B of the extended wings **325**A and **325**B or fluted portions of the liner and thusly the amount of the liner wall **309** material that is dedicated to producing the spade or flattened portion of the jet. The longitudinal length of section B **322** and the extended wings **325**A and **325**B or flutes can be increased or decreased to achieve the desired ratio of rod to spade length of the jet created from EW liner **300**. The thickness of the liner wall **309** can gradually increase or decrease from the apex **308** to the base end **320**A and **320**B or anywhere along the wall length; a tapering liner wall **309** thickness will help balance the liner to HE mass ratio as the liner cone diameter increases toward the base end **320**A and **320**B.

After the collapse of full conical section B **322** by HE section B into a rod jet the curved wing-like extensions or flutes **325**A and **325**B of wing section C **333** are driven to horizontal plane **345** and symmetrical axis **337** of the EW liner **305** by the HE section C with wing explosive **340**A and **340**B, the colliding material forms a flat blade shape jet instead of a round jet because of the lack of liner material and HE confinement on the flat faced sides **310**F that are ninety degrees out of phase from the wing-like extensions or flutes **325**A and **325**B. The transition from conical section B **322** to wing section C **333** is gradual which allows the spade jet to stay connected to the forward rod jet as both portions of the jet stretch longitudinally forward along axis **337**; and because of the lack of liner confinement on the two opposing parabolic faces **310**F the spade jet will widen laterally on horizontal plane **345** as it stretches longitudinally forward with the forward rod jet.

Vertical plane **345** is the convergence plane where the explosively driven liner material of the 180 degree opposing concave liner wing extensions **325**A and **325**B (only one wing **325**B can be viewed from the FIG. **6** cross sectional elevated view) of EW liner **305** will converge and form spade jet **342** of FIG. **7**. The liner wing extensions **325**A and **325**B are planar symmetric to each other about vertical plane **345**, and the orientation of the resultant spade jet **342** of FIG. **7**, at a given time post detonation, is correctly oriented to represent the collapse of the EW liner **305** from the view point of FIG. **6**. The jet consists of a slug **350**, slug separation area **347**, spade jet tail **349**, spade jet **342**, spade/rod jet transition point **348**, rod jet **343**, and jet tip **344**. This depiction of the jet is at a finite time after the detonation of the device, since the jet has a velocity gradient from tip to tail the longer the time of flight after detonation the longer will be the resulting jet.

In the singular use of the Axilinear device **300**, HE billet **315** detonation is initiated at initiation point **307**, the HE billet **315** detonation wave advances from HE section A **338** forward to HE section B **339** toward the front of the device collapsing the EW liner **305** full conical section B **322** forming rod jet **343** followed by the collapse of extended wings **325**A and **325**B of section C **333** by the detonation of HE section C wing explosive **340**A and **340**B forming the wide flattened spade jet **342**.

After the collapse of full conical section B **322** by HE section B into a rod jet the curved wing-like extensions or flutes **325**A and **325**B of wing section C **333** are driven to horizontal plane **345** and symmetrical axis **337** of the EW liner **305** by the HE section C with wing explosive **340**A and **340**B, the colliding material forms a flat blade shape jet instead of a round jet because of the lack of liner material and HE confinement on the flat faced sides **310**F that are ninety degrees out of phase from the wing-like extensions or flutes **325**A and **325**B. The transition from conical section B **322** to wing section C **333** is gradual which allows the spade jet to stay connected to the forward rod jet as both portions of the jet stretch longitudinally forward along axis **337**; and because of the lack of liner confinement on the two opposing parabolic faces **310**F the spade jet will widen laterally on horizontal plane **345** as it stretches longitudinally forward with the forward rod jet.

The horizontal plane **345** of the wing section C **333** is seen as a horizontal longitudinal line that is coincident with symmetrical axis **337** in FIG. **4**. Horizontal plane **345** is where the liner material of the two 180 degree opposing extended axisymmetric and planar symmetric wing extensions **325**A and **325**B of EW liner **305** will converge from the detonation pressures of HE section C with wing explosive **340**A and **340**B forming the spade jet **342** shown in FIG. **5**. Horizontal plane **345** also represents the orientation and direction of the wide lateral cross-section of spade jet **342**, which are coplanar and coincident to each other. The liner wing extensions **325** of FIG. **4** and the view of jet **301** of FIG. **5** are correctly oriented to each other to represent the collapse of the EW liner **305** from this viewpoint, the spade jet **342** is seen as a thin section along symmetrical axis **337** and horizontal plane **345** that decreases in thickness from the aft end spade jet tail **349** to the forward end rod/spade transition point **348** where it is connected to the aft end of rod jet **343**. Jet **301** would form within the hollow cavity of EW liner **305** of device **300** and at some time after liner collapse would eventually stretch past the base end **325**A and **325**B, it is shown in FIG. **5** fully outside of and to the right of the device for easier viewing.

Body **310** contains and protects HE billet **315** and provides a mounting surface for EW liner **305** at its base ends **320**A and **320**B. The HE billet **315** detonation is initiated by any suitable commercially available detonator **336** on the device symmetrical axis **337** at initiation point **307**. With respect to the longitudinal symmetrical axis **337** of device **300**, the liner full circumference conical section B **322** is aft of wing vertex **332**A and the liner wing section C **333** is forward of the wing vertex **332**A. The jet **301** produced by device **300** has three distinct regions and shapes; a high velocity 7-9 km/s round axisymmetric rod jet **343** with forward jet tip **344** and aft rod/spade jet transition point **348**, followed by a lower velocity 4-7 km/s planar symmetric flattened spade jet **342** mid-section and jet tail **349**, followed by the slug separation area **347** and a low velocity ½ km/s slug **350**.

The forward axisymmetric rod jet **343** in FIG. **5** is formed from the conical section B **322** of EW liner **305** that starts at apex **308** and ends at the wing vertex **332**A of the parabolic flat face **330**A. At wing vertex **332**A the conical section B **322** of the liner transitions into the wing section C **333** with two opposing concave liner wing extensions **325**A and **325**B or flutes, formed due to the liner side truncation. The aft spade jet **342** is formed from the collapse of the liner wing section C **333** opposing liner wing extensions **325**A and **325**B portions of EW liner **305**. The aft spade jet **342** being flat and wide, similar to a conventional linear shaped charge jet but more massive, directionally controllable and at a much higher velocity, thus the Axilinear name. The amount of liner material designated to the aft and forward portions of the combination spade and rod jet can be adjusted by shortening or lengthening conical section B **322** and wing section C **333** of EW liner **305** to give differing lengths and widths of rod and spade shaped jet sections.

In FIG. **7**, the jet **301** consists of an aft slug **350**, spade jet tail **349**, spade jet **342**, rod/spade jet transition point **348**, rod jet **343**, and forward jet tip **344**. Jet and slug velocities, angle of projection, thickness, spade blade width and length of both jet sections can vary depending on device design. The forward longitudinal velocity of jet **301** is greatest at jet tip **344** and has a velocity gradient from the forward end jet tip

344 to the aft end spade jet tail 349. Jet 301 velocity and the velocity gradient are factors of device design, type of explosive, and the type of material used to make EW liner. Amongst many other design factors of device reducing the liner included angle A will increase jet velocity and the velocity gradient. The jet velocity gradient and material ductility directly affects the stretch rate of jet 301 and ultimately the length and width of both the rod jet 343 and spade jet 342 portions of jet 301, higher velocity gradients will result in a thinner and longer jet. This depiction of the jet is at a finite time after the detonation of device. The jet at an earlier time frame after detonation of HE billet would be shorter in length and thicker, at a later time it would have stretched forward becoming longer and thinner because of the velocity gradient and ductile stretching of the EW liner material.

The longitudinal depiction of jet 301 in FIG. 5 has the forward jet tip 344 and rod jet 343 on the right hand side of aft spade jet 342 with a middle jet transition point 348. The jet transition point 348 is where the material contributed to rod jet 343 from the collapse of the conical section B ends and the spade jet 342 material contributed by the collapse of wing section C 333 begins. The FIG. 5 jet orientation is an edge view of spade jet 342 and collapse plane 345 which is the thinnest cross-section of the spade and the result of the liner wings of FIG. 3 being in the 6 and 12 o'clock positions. The spade portion of jet 301 in FIG. 5 is slightly thicker at the aft end jet tail 349 with a thinning cross-section toward the foreword end jet transition point 348 this is due to stretching from a higher velocity forward end, matching the rod jet thickness due to the longitudinal jet stretch rate.

The jet 301 is formed from the collapse of EW liner caused by a detonation shock wave and converging pressure toward symmetrical axis from detonating HE billet, which is traveling longitudinally from aft HE initiation point to forward base ends of device. As the detonation wave created from detonating HE billet progresses from the aft end HE section A forward to HE section B of device it first collapses the section B of EW liner starting at apex and continuing forward to vertex creating the rod jet 343 portion of jet 301, the collapse and jetting from section B of the liner resembles that of a typical axisymmetric conical lined shaped charge. As the detonation wave moves forward of wing vertex the HE section C wing explosive 340A and 340B collapse the extended wings of section C starting at vertex and ending at base end forming the spade jet 342 portion of jet 301. Both rod and spade portions of jet 301 stretch and elongate longitudinally forward along axis and spade portion 342 also widens laterally on plane 345; as time progresses after initial detonation and collapse of EW line, and at some elongation length and time after collapse the higher velocity rod and spade jet will break free of the collapsed liner mass. The remaining liner mass becomes a lower velocity slug 350 represented by slug separation area 347.

FIGS. 8, 9 and 10 illustrate a target 400 with a hole profile made by the combination rod/spade jet from the detonation of Axilinear device of FIG. 6. The vertical elongated hole 425 shown in FIG. 8 on target surface 440 is made by the spade portion of the jet and the circular deep perforation 430 is made by the rod portion of the jet following detonation of an Axilinear device of FIG. 6. Elongated hole 425 will be wider by a factor of two or greater, than the charge diameter CD of the FIG. 1 embodiment when detonated at a given optimal 2-3 CD standoff from target surface 440. The bottom face 428 of elongated slot 425 is where the spade jet hydrodynamic penetration stops and the circular deep perforation 430 is centered on the bottom face 428. Multiple Axilinear devices can also be combined into a circular, polygonal, linear, splined or other patterned array to produce very large connected target penetrations.

FIG. 9 is a vertical sectional view taken along line 9-9 of FIG. 8 that further illustrates the wide elongated hole 425 in target material 420 made by the spade jet that is proceeded by a large deep circular hole 430 at its center made by the rod jet. Vertical line 9-9 is coplanar with the collapse plane of the extended wing portion of the FIG. 6 embodiment. FIG. 10 is a horizontal sectional view taken along line 10-10 of FIG. 8 that further illustrates the cavities made by the jet of the embodied FIG. 1 device in target 400, in this section view we see the narrow view of the slot made by the spade jet followed by the deep hole 430 made by the rod jet. Line 10-10 is perpendicular to the collapse plane of the spade jet. Longer or shorter standoffs of the FIG. 1 embodied device with the target surface 440 will lengthen or shorten the slot 425 width and depth. The cavity in target 400 is what would be expected if the target material 420 was a metal or other material with properties similar to metal, much larger cavities with many surrounding fractures would be expected in a masonry or rock like material.

FIGS. 12, 13, 14, 15, 16, and 17 show some possible variations of the FIG. 2 Axilinear liner embodiment that can be implemented in the FIG. 1 embodied device 100 to modify the spade jet width, length, velocity and mass.

FIG. 12 is a base end view of EW liner 500 a diverging variation with diverging extended wings. FIG. 13 is a vertical sectional view taken along line 13-13 of FIG. 12 illustrating the diverging extended wings 525A and 525B with an included angle B of the partial circumference wing section 533 being greater than included angle A of the full circumference conical section 522. FIG. 14 further clarifies the construction of the diverging EW liner 500. EW Linear 500 has all the main features and characteristics of the FIG. 2 embodiment with the addition of a diverging wing section 533 that has a included angle B wider than the conical section 522 included angle

A. EW Linear 500 has a full conical section 522 with an aft apex 508, included angle A, conical length L2 and forward wing apex 532A at vertical line 513. Namely, EW Liner 501 has a full conical section 522 with an aft apex 508, included angle A, conical length L2 and forward wing apex 532A at vertical line 513. Wing section 533 begins at vertical line 513 with two extended wings 525A and 525B protruding forward, flat parabolic faces 530A and 530B, wing length L1, and forward base ends 520A and 520B. The liner wall 509 transition at radial line 513 from the aft axisymmetric conical section 522 portion of the EW liner 500 to the remaining forward axisymmetric and planar symmetric wing section 533 is a gradual transition of the two sections at radial line 513 so as to maintain jet continuity between the rod and spade jets. The purpose of diverging wings is to decrease the velocity of the spade portion of the jet and increase its mass. EW liner 500 wings included angle B can be between 30 and 120 degrees and still produce viable spade jetting.

FIGS. 15, 16, and 17 illustrate a EW liner 501 variation with converging extended wings 525A and 525B with an section 533 with an included angle B less than included angle A of conical section 522. FIG. 15 is a base end view of the EW liner 501 converging variation with converging extended wings 525A and 525B. FIG. 16 is a vertical sectional view taken along line 16-16 of FIG. 15 illustrating the converging extended wings 525A and 525B with an included angle B of the partial circumference wing section 533 being less than included angle A of the full circumference conical section **522**. FIG. **17** further clarifies the construction of the converging EW liner **501**.

EW Liner **501** has all the main features and characteristics of the FIG. **2** embodiment except having a narrower included angle B of a converging wing section **533** than the conical section **522** included angle A. Namely, EW Liner **501** has a full conical section **522** with an aft apex **508**, included angle A, conical length L**2** and forward wing apex **532**A at vertical line **513**. Wing section **533** begins at vertical line **513** with two extended wings **525**A and **525**B protruding forward, flat parabolic faces **530**A and **530**B, wing length L**1**, and forward base ends **520**A and **520**B. The liner wall **509** transition at vertical line **513** from the aft axisymmetric conical section **522** portion of the EW liner **501** to the remaining forward axisymmetric and planar symmetric wing section **533** is a gradual transition of the two sections at radial line **513** so as to maintain jet continuity between the rod and spade jets. The purpose of diverging wings is to increase the velocity of the spade portion of the jet and decrease its mass. EW liner **501** wings included angle B can be between 30 and 120 degrees and still produce viable spade jetting.

This invention is a unique arrangement of shaped charge devices in an array to produce a patterned or arranged explosive pattern in a target area. The Axilinear design, in a plural array configuration, solves the limitations of a smooth walled circular linear liner by having opposing corrugations or flutes that have sufficient curvature to converge the liner material so as to obtain ductile Munroe jetting, longer jets, and higher velocities. Since jet length and depth of target penetration, are directly proportional, the present invention provides a longer and most robust jet stream than previously possible.

FIG. **18-20** show a circular Axilinear device array **1000** of eight individual Axilinear shaped charge devices **1105**A-**1105**H held together by a rigid retaining structure **1110** around the array axis of symmetry **1112**. Each individual Axilinear shaped charge device **1105**A-**1105**H can be, and are, configured in the manner described above with respect to the embodiments shown and described in FIGS. **1-10** and **12-17**, including all components, configurations, and possible modifications and variations thereof. Namely, each shaped charge device is configured in a manner where each shaped charge means an explosive device, having a shaped liner, driven by a similarly shaped mating explosive billet, having an initiation device, the necessary containment, confinement and retention of the liner to the explosive billet. The result of detonation of this device is a high speed stream of material produced from the convergence of the liner driven by the explosive. This is commonly known as the Munroe Effect. The shape and size of this stream of material commonly called a jet, is dependent on the starting shape and size of the liner and explosive billet.

The Axilinear liner in each shape charge device (e.g. **1105**A) in the present invention consists of two sections, aft section "B", and forward section "C". The aft section "B" is a full circumference of one of, or combination of the liner profiles, shown in the figure section of this document. This section B produces an axisymmetric rod like stretching jet with length proportional to the length of the liner section, the stretch rate, and time of flight of the jet.

The forward section "C" in each shape charge device (e.g. **1105**A) consists of less than full circumference walls extending beyond the end of section B, these wing extensions are symmetrically one hundred eighty degrees apart. These wing extensions have axisymmetric cavity as viewed from inside the hollow liner form, this cavity functions to provide the convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow. The jet from section C produces a planar symmetric stretching wide non round jet which cuts a slot rather than a round hole as produced by the rod portion of the jet.

More particularly, the Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures), consist of a body **110**, EW liner **105**, high explosive (HE) billet **115**, having an axisymmetric aft area with detonator **136**, detonator holder **135**, detonation initiation point **107**, and liner apex **108**, and a axisymmetric as well as planar symmetric (Axilinear) fore area that consists of liner extended wings **125**A and **125**B and liner base ends **120**A and **120**B. Initiation of the HE billet of this novel device can be achieved by any suitable readily available detonation initiation devices.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with an axisymmetric or symmetrical about a longitudinal axis **137** from the aft end near detonator **136** to the middle liner wing vertex **132**A and **132**B of the EW liner **105**; forward of wing vertex **132**A and **132**B device **100** is Axilinear with two symmetrical curved extended wings **125**A and **125**B being axisymmetric with axis **137** and also planar symmetric about two central perpendicular reference planes, a horizontal plane in the 3 and 9 o'clock positions, and a vertical plane in the 12 and 6 o'clock positions.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with the vertical 12 and 6 o'clock reference plane (FIG. **2** vertical plane **246**) is coincident with axis **137** and passes through the middle of each extended wing **125**A and **125**B, the parabolic faces **130**A and **130**B are planar symmetric or mirrored about this plane. Front edge **114** of face vacancy or void in the winged vertex **132**A of the liner **105**. The horizontal 3 and 9 o'clock reference plane (FIG. **2** horizontal collapse plane **245**) is coincident with axis **137** and passes through each wing vertex **132**A and **132**B, this plane is also known as the wing collapse plane and the wings **125**A and **125**B are planar symmetric or mirrored about this plane. The jet produced by detonating an Axilinear shaped charge device **100** is axisymmetric for the forward rod portion of the jet and planar symmetric for the aft portion, this aft spade portion of the jet being shaped somewhat like a linear shaped charge jet, thusly named Axilinear.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with a conical EW liner **105**, other geometrical shaped (i.e. hemispherical, tulip, or trumpet) hollow cavity formed liners with extended liner wings can also be used. EW liner **105** has a full circumference axisymmetric conical profile section **122** with included angle A that is longitudinally between aft apex **108** and middle liner wing vertex **132**A and **132**B, and a Axilinear partial circumference wing section **133** toward the fore end with two symmetrically opposing conical fluted wing extensions **125**A and **125**B with included angle A that extend longitudinally from the middle liner wing vertex **132**A and **132**B to the forward liner base ends **120**A and **120**B.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with forward liner wing extensions **125**A and **125**B are symmetrical to each other and positioned one hundred and eighty degrees apart, opposing each other planar symmetrically about the horizontal plane and is axisymmetric about longitudinal axis **137** of the device. The absence of liner wall material on opposing sides of the wing section **133** at the forward base end of the liner forms two parabolic faces **130**A and **130**B that are parallel and symmetric with each other about longitudinal axis **137** and the vertical plane. Both liner parabolic faces **130**A and **130**B have a vertex at wing vertex **132**A and **132**B and open toward the base ends **120**A and **120**B with parabolic end points at the wing arc ends **121**A and **121**B.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with an EW liner **105** that maintains its conical profile and liner wall **109** thickness profile from aft end apex **108** of the full circumference conical section **122** to wing vertex **132**A and continues with the same profile to the fore end of the extended wings **125**A and **125**B at the base ends **120**A and **120**B of the partial circumference wing section **133**. Liner wall **109** transitions from a full circumference conical profile at wing vertex **132**A and **132** B into 180 degree symmetrically opposing wing like or fluted extensions **125**A and **125**B that extend from the full circumference conical profile section **122** at wing vertex **132**A and **132**B to the base end **120**A and **120**B of the liner.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with the liner wing extensions **125**A and **125**B shown in FIG. **1** retain the same curvature, included angle A, and wall **109** thickness profile as the full conical profile section **122** portion of the liner; but the extended wings **125**A and **125**B could also have a larger or smaller included angle A and wall thickness **109** than the conical section **122**, as long as they maintain planar symmetry to one another. Being planar symmetric and having partial circumference conical curvature allows the wing-like extensions or flutes **125**A and **125**B to converge at very high pressures on the collapse plane, raising the temperature and ductility of the converging wing material to the required level for Munroe jetting.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** with an HE billet **115** that can be pressed, cast or hand packed from any commercially available high order explosive. HE billet **115** is in intimate contact with the outer liner surface **116** of EW liner **105** from the aft apex **108** to the forward wing vertex **132**A and **132**B of the conical profile section **122** and from the wing vertex **132**A and **132**B to the base ends **120**A and **120**B and wing arc ends **121**A and **121**B of the wing section **133**. HE billet **115** has three distinct sections, a head height or aft HE section "A" **138** as measured longitudinally between HE initiation point **107** and liner apex **108**, a mid-section or full conic HE section "B" **139** as measured longitudinally from apex **108** to wing vertex **132**A and **132**B, that fully encompasses the liner conical section **122**, and forward HE section "C" that contains two partial circumference wing HE sections **140**A and **140**B as measured longitudinally from wing vertex **132**A and **132**B to base ends **120**A and **120**B that conform to the shape of the liner wing extensions **125**A and **125**B.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with an HE section A **138** that can be lengthened or shortened longitudinally by increasing or decreasing the length of body **110**, greater head height gives a flatter detonation wave before it comes in contact with the liner. Flatter detonation waves at time of liner impact typically increase jet tip velocity and target penetration, head height optimization is a balance between jet performance and minimizing the explosive charge. The optimum head height can be determined by computer code and live testing to obtain the least amount HE volume needed to efficiently obtain maximum jet mass, velocity and target penetration. A typical head height for a conical lined shaped charge would be ½ inch space permitting.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with a shape and volume of HE section B **139** as defined by the area between the inside surface **112** of body **110** and outside surface **116** of EW liner **105** from aft apex **108** to forward body face **110**E located at wing vertex **132**A and **132**B, and makes a full circumference or revolution around liner section **122**. The shape and volume of the two symmetrical wing HE sections **140**A and **140**B of HE section C are defined by the area between the inside surface **112** of body **110** and outside surface **116** of EW liner **105** from aft wing vertex **132**A and **132**B to forward base ends **120**A and **120**B, and are partial circumference volumes about each wing between the wing arc end points **121**A and **121**B. HE billet **115** can have a super-caliber diameter (i.e. larger than the liner base diameter) necessary for full convergence of the base end of the liner wing extensions **125**A and **125**B to obtain maximum velocity and mass of the spade jet.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with the forward section C **133** that consists of two less than full circumference liner walls **109** extending beyond the end of section B **122**, creating partial conical or curved wing extensions **125**A and **125**B, wing vertices **132**A and **132**B and parabolic faces **130**A and **130**B that are symmetrically one hundred and eighty degrees apart. The wing vertex **132**A and **132**B and flat parabolic faces **130**A and **130**B are formed from the absence of material on two symmetrically opposing sides of the base end of the conical profile. The wing extensions **125**A and **125**B create an axisymmetric and planar symmetric opposing partial radial hollow concavities on the inside liner wall surface **117**; HE detonation pressures on these concavities provides a partial radial convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow and hydrodynamic jetting.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with collapsing wing extensions **125**A and **125**B of section C **133** that produce a wide planar symmetric stretching non round spade shaped jet which cuts a deep slot rather than a round hole; the mass, width, length, stretch rate, velocity, and time of flight of the spade jet is directly proportional to the liner wall length of section C **133**, included angle A, and liner wall **109** thickness of section C **133**. If section C **133** is shortened and the overall length "L" is unchanged section B **122** will become longer. Increasing the length of section B **122** will increase the rod jet length, mass and penetration depth, and will decrease the length, width, mass and penetration depth of the spade jet; length adjustments to sections B and C work in concert, when the rod jet is lengthened the spade jet will be shortened and vice versa shortening the rod jet will lengthen the spade jet.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures), and during collapse of the liner full conical section **122**, liner material radially converges along the longitudinal axis **137** into a rod jet from the detonation of HE section A **138** and HE section B **139**; the collapse of full conical section **122** is followed by the collapse of the extended liner wings **125**A and **125**B of the partial circumference section **133** into a spade jet from the detonation of wing HE sections **140**A and **140**B of HE section C. Wing HE sections **140**A and **140**B are coupled to the outer liner surface **116** of each wing from the aft wing vertex **132**A and **132**B to the forward wing base ends **120**A and **120**B and the wing arc ends **121**A to **121**B.

The radial curvature of the opposing liner wing extensions **125**A and **125**B provides the radial material convergence during collapse needed to raise the temperature and pressure of the collapsed liner material, to the required level for plastic flow and Monroe jetting to occur, this increases the ductility allowing for longer jet breakup length. During collapse the full conical section **122** of the liner will form a axisymmetric rod jet along the longitudinal axis **137** followed by the concave liner wing extensions **125**A and **125**B being driven to a common collapse plane by HE **140**A and **140**B, the colliding wing extensions material will form into a high velocity flat planar symmetric spade shape jet.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with collapsed wing extensions material that moves forward along longitudinal axis **137** it also spreads laterally outward forming the spade shaped jet along the horizontal collapse plane. The formation of the spade jet is due to the absence of liner material, explosive and confinement on the liner sides with the two flat parabolic faces **130**A and **130**B that are adjacent to and ninety degrees out of phase from the flutes or wing extensions **125**A and **125**B. The orientation of device **100** can be rotated about axis **137** and the spade jet orientation will rotate equally in the same direction, if device **100** is rotated 45 degrees clockwise about axis **137** the collapse plane will also rotate 45 degrees clockwise and the spade jet will stretch longitudinally forward on axis **137** and laterally along the rotated collapse plane.

The EW liner **105** is the working material of the shaped charge and is mounted to body **110** at the forward end of device **100**, at the base ends **120**A and **120**B of the liner wing extensions **125**A and **125**B; and adjacent to the wings the liner parabolic faces **130**A and **130**B are mounted to the body **110** parabolic faces **110**F. Body **110** consist of four distinct areas, a aft cylindrical area **110**C that provides mounting for an initiation device that is coupled to the aft end of HE **115**, followed by a boat tailed area **110**B that contains the HE section A **138**, followed by cylindrical area **110**A that contains HE section B **139** that is coupled to the full conical liner section **122**; and HE section C containing wing sections **140**A and **104**B that are coupled to the extended wings of liner section **133**, and body area **110**D at the forward end of cylindrical section **110**A that transitions from a cylindrical shape into two parallel flat parabolic faces **110**F that are planar symmetric to each other and are coupled to the parabolic liner faces **130**A and **130**B.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** with a body area **110**D that has two functions, it provides two opposing side mounting faces **110**F for the liner extended wings and also has flat faces **110**E that is the forward containment boundary of HE section **139**; this boundary is located at wing vertex **132**A and **132**B, and is also the liner wing transition point from the full circumference conical section **122** to the extended wing section **133**. The containment of HE pressures during the detonation time period by body area **110**D is important for proper collapse of the wings and spade jet formation. Shape charge liners for the most part are made from copper but liners may be made from most any metal, ceramic, powdered metals, tungsten, silver, copper, glass or combination of many materials. Body **110** would typically be made from aluminum or steel but could be made of almost any metal or plastic as long as it provides the correct amount of tamping for proper jet formation and desired jet velocity during the detonation of HE billet **115**.

The EW liner **105** is a modified cone or other shape with two distinct geometrical sections, the aft end of the liner is a full conical profile section **122** with an apex **108**, followed by the forward end wing section **133** with two liner wing extensions **125**A and **125**B that extend forward from the full conical or other shape profile section **122** at wing vertex **132**A and **132**B to the wing base ends **120**A and **120**B at the fore end of EW liner **105**. The liner wing extensions **125**A and **125**B maintain the same included angle A liner wall **109** thickness profile and curvature of the full conical profile section **122**.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with the included angle A of EW liner **105** needed to obtain Munroe effect jetting should be from 36 to 120 degrees. The jet velocity achieved from a shaped charge is dependent on the liner wall **109** thickness and included angle A of the liner; a narrower included angle results in a faster less massive jet, and a wider included angle results in a slower more massive jet. Jet velocities can vary from 4 to 10 km/s depending on the type and quality of liner material, included angle A of the liner, liner wall **109** thickness, the charge to mass ratio of HE to liner, bulk density of the liner, surface finish of the liner wall, and body geometries; very small changes of any of these variables can make large differences in jet velocity and trajectory.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) and the HE billet **115** is contained between the inner surface **112** of body **110** and the outer surface **116** of the EW liner **105**. HE billet **115** provides the energy to collapse the EW liner **105**, increasing the ductility of the EW liner **105** material, causing it to form a compound jet in the shape of a very high speed rod jet from the full conical section **122** material followed by a flattened spade shaped jet from the liner wing section **133** material; the spade jet is slower than the rod jet from conical section **122** but much faster than a typical "V" shaped liner found in common linear shaped charge because of the cavity of the wing section **133**.

The Axilinear shaped charge device **1105**A-H is described and shown as the shape charge device **100** shown in FIG. **1** (and related figures) with a body **110** that provides a mounting surface for EW liner **105** which is held to body **110** at the liner base ends **120**A and **120**B and at the parabolic faces **130**A and **130**B. The base end of EW liner **105** does not form a full circumference; it consists of two opposing concave surfaces or wing extensions **125**A and **125**B and the corresponding wing base ends **120**A and **120**B at the forward end of the liner. Body **110** also serves as a containment vessel for the delicate HE billet **115** and protects it from damage or impact by supporting the outer diameter of HE billet **115**. Body **110** also provides tamping for the HE billet **115** depending on body wall **106** thickness and material density, HE tamping can be increased or decreased if needed to improve jet performance or reduce total HE mass.

The purpose of removing the base end material on symmetrically opposing sides of EW liner **105** and creating the wing-like extensions **125**A and **125**B is twofold. The first purpose is to form the partial circumference conical wing-like extensions or flutes **125**A and **125**B and when collapsed converge to form the flat aft spade shaped portion of the jet; the flattened spade jet spreads laterally and erodes an elongated slot in target material. The second purpose being to allow for close lateral proximity of multiple adjacent devices resulting in multiple tightly spaced rod and intersecting spade jet perforations, creating a large coupled slotted target perforation.

The EW liner **1106**A-H is the working material of the shaped charge and is mounted to shape charge unit **1105**A-H at the forward end of device **1000**, at the base ends of the liner wing extensions as shown in FIG. **1** (and related figures); and adjacent to the wings the liner parabolic faces are mounted to the shape charge units **1105**A-H at the parabolic faces. Each shape charge unit **1105**A-H in the array **1000** consists of four distinct areas, a aft cylindrical area that provides mounting for an initiation device that is coupled to the aft end of HE, followed by a boat tailed area that contains the HE section A, followed by cylindrical area that contains HE section B that is coupled to the full conical liner section; and HE section C containing wing sections that are coupled to the extended wings of liner section, and body area **1105**A-H at the forward end of cylindrical section that transitions from a cylindrical shape into two parallel flat parabolic faces that are planar symmetric to each other and are coupled to the parabolic liner faces, which are all features shown and described in FIG. **1** (and related figures).

The rigid retaining structure **1110** surrounds and secures the shaped charge devices **1105**A-H to the array **1000** around the array axis of symmetry **1112** (shown in FIGS. **18** and **20**). When equally spaced Axilinear devices are configured in a radial array with their collapse planes **1108**A-**1108**H being normally aligned around a common symmetrical axis **1112** as depicted in FIG. **19** and FIG. **20**, simultaneous detonation of the shape charges **1105**A-H in the array **1000** will produce a series of connecting penetrations forming a large circle penetration **1120** as illustrated in FIG. **21**.

The array **1000** of Axilinear devices **1105**A-**1105**H achieves this super caliber hole by having a liner that has a aft axisymmetric full of conical section and a forward liner section that transitions into a series of opposing concave flutes in a periphery configuration such as a circle or other polygonal shape. The fluted extended wing (EW) liners **1106**A-**1106**H wing extensions are planer symmetric and axisymmetric having partial circumference directly opposed wings at the base end of the liner, and have sufficient curvature to converge the liner material into spade shaped jets in a radial pattern about planes **1108**A-**1108**H, allowing a circular or other shaped array of liner wing extensions to produce multiple connected cavities of almost any shape or length. The axisymmetric and planer symmetric liner wing extensions and the high explosive driving them increases the temperature and ductility of the liner material improving the performance of the device.

In the circular Axilinear array **1000** configuration, the linear flattened spade portions of the jets connect at overlap points **1128**A-**1128**H and combine to form a closed large diameter hollow body roughly resembling a hollow cylinder. The forward rod portion of each jet erodes deep holes **1125**A-**1125**H in the target followed by elongated holes **1126**A-**1126**H created by the flattened spade portion of the jet that connect at overlap points **1128**A-**1128**H; the array of spade jets erodes and removes the target material between the rod jet holes creating a large connected cavity. When put in a circular or other patterned array, the Axilinear shaped charges will produce deep and extremely large diameter holes greater than the overall device diameter of the array without leaving a center core plug of material in the target. When very large perimeter holes are desired multiple concentric rings of arrays can be used to remove all of the center target material with no core material left behind.

FIG. **19** illustrates the orientation of the Axilinear shaped charge devices **1105**A-**1105**H and the EW liner **1106**A-**1106**H wing collapse planes **1108**A-**1108**H of each device of the FIG. **18** embodiment. The collapse planes **1108**A and **1108**E of devices **1105**A and **1105**E are perpendicular to line G-G and all eight devices **1105**A-**1105**H in this array are oriented the same with symmetrical axis **1112** of the array. Other variations of arrays could have the collapse planes of the individual devices at any orientation or angle with the symmetrical axis and each other.

FIG. **20** is a cut-away view of the longitudinal section view along line G-G of the FIG. **19** circular array that further explains the direction and orientation of the collapse planes **1108**A-**1108**H of the Axilinear devices **1105**A-**1105**H and the EW liners **1106**A-**1106**H with axis **1112** of the FIG. **18** embodiment. The FIG. **20** section view of device **1105**A and **1106**E shows a side view of the sectioned liner wings of wing liner **1106**A and **1106**E and a side end view point of collapse plane **1108**A and **1108**E.

As shown in FIG. **20**, the HE billet **1115**A and **1115**E can be pressed, cast or hand packed from any commercially available high order explosive. HE billet **1115**A, E is in intimate contact with the outer liner surface of EW liner **1105**A-E from the aft apex to the forward wing vertex of the conical profile section and from the wing vertex to the base ends and wing arc ends of the wing section. The rigid retaining structure **1110** surrounds and secures the shaped charge devices **1105**A-E to the array **1000** around the array axis of symmetry **1112** (shown in FIGS. **18** and **20**).

HE billet **1115**A,E has three distinct sections, a head height or aft HE section "A" as measured longitudinally between HE initiation point and liner apex, a mid-section or full conic HE section "B" as measured longitudinally from apex to wing vertex, that fully encompasses the liner conical section, and forward HE section "C" that contains two partial circumference wing HE sections and **140**B as measured longitudinally from wing vertex to base ends that conform to the shape of the liner wing extensions. All the above features of HE billet **1115**A,E described herein are shown and described in more detail with respect to FIG. **1** and related figures.

Detonating the high explosive billet **1115** in each of the Axilinear shaped charges **1105**A-**1105**H collapses the EW liners **1106**A-**1106**H and produces a combination of a forward central longitudinal rod shaped jet followed by a aft flattened spade shaped jet about collapse planes **1108**A-**1108**H, somewhat like a linear shaped charge, but at much higher velocities with "Munroe" jetting and having a much larger velocity gradient than that of a linear shaped charge. The conical aft liner portion creates the rod shaped jet while the fluted forward liner wing portion creates the sheet-like spade shaped jet.

Axilinear charges **1105**A-**1105**H in the array **1000** are detonated in concert forming a simultaneous ring of jets that erodes the circular cavity **1120** shown in FIG. **21**. The aft portion of the jets produced by devices **1105**A-**1105**H are spade shaped and when combined edge to edge will produce a ring of connected deep elongated slotted holes **1126**A-**1126**H removing the target material at jet overlap point **1128**A-**1128**H between the series of deeper round hole perforations **1125**A-**1125**H made by the rod like forward portion of the Axilinear jets. In this configuration a super caliber hole larger than the major diameter of the shaped charge array will result from the interaction of the spade portion of the Axilinear jets with the target.

The orientation or direction of the elongated holes **1126**A-**1126**H are controlled by the Axilinear device collapse planes **1108**A-**1108**H orientation when placed in the rigid support structure **1110** of array **1000**. By rotating the collapse planes **1108**A-**1108**H with respect to axis **1112**, the same rotation of the slotted holes **1126**A-**1126**H in the target will result. With correct standoff and spacing between array segments, the Axilinear shaped charges **1105**A-H will produce a combination of high velocity stretching jets and deep hydrodynamic circular slotted penetrations that connect at **1128**A-**1128**H to form a full ring penetration of almost any diameter. The ring cavity **1120** shown in FIG. **21** is what should be expected if the target material was a metal or other material with properties similar to metal, much larger super caliber array diameter holes with no center material left behind and with many surrounding fractures would be expected in a masonry or rock like material.

In the continuing effort to produce full or super caliber deep holes using shaped charges it is necessary to reshape the energy delivery to the target in a different pattern than that of an axisymmetric shaped charge. Since axisymmetric shaped charges produce very small diameter holes in comparison to the diameter of the shaped charge it is necessary that the jet energy must be applied to a larger target surface area to produce a full caliber large volume hole. A full caliber hole in the context of a shaped charge array means a hole as large as or larger than the outer diameter of the array of Axilinear jet producing devices.

The jet produced by each Axilinear shaped charge has an axisymmetric forward rod portion that transitions into a flattened planer symmetric aft portion somewhat like a linear shaped charge thus termed Axilinear shaped charge. The Axilinear shaped charges can be deployed individually and will produce an elongated hole with length of the hole as wide as or wider than the diameter of the charge itself and when combined into a circular or other shaped array they will produce very large holes or splined cuts.

Each Axilinear shaped charge **1105**A-**1105**H or component in the array **1000** configuration can be aimed at different angles relative to the array longitudinal axis **1112** and to each other. Further, this Axilinear array **1100** can produce super caliber holes; an array of these arrays could produce extremely large holes even in the multi foot diameter range. This would give an adjustable spray pattern for larger area coverage such as attacking convoys or any massed assembly of troops or vehicles. Arrays of multiple Axilinear charge arrays could also be used in a situation where hit to kill is difficult or impossible with single charge warheads, and the wide array pattern of very high speed jets covers a large area and is more destructive than single warhead charges to aircraft, incoming missile, satellite, ship or ground vehicle. The spread pattern can be set by modifying the collapse plane **1108**A-**1108**H angle of each Axilinear shaped charge **1105**A-**1105**H component with the longitudinal axis **1112** of the array.

With the advent of a super caliber hole in a target of interest one can produce a very deep hole into an infinite thickness target by having a repetitive series of charges and or arrays of charges delivered to the bottom of the hole made by the first charges, deepening the hole and continued by succeeding charges. In oil well stimulation, this process and capability can fracture formations for many meters outside of the casing without the need for hydraulic fracturing.

Usually in the field of shaped charge development the liner is the primary item of the design, in the case of the Axilinear shaped charge this is not the case, although the liner is of the utmost importance the containment body design is a large factor of charge performance. The planer symmetric and axisymmetric shape of the Axilinear charge explosive and the containment body when deployed singularly or in an array is very important to the proper function of this multi component shaped explosive device.

The initiation timing complexity of the arrangement of the multiple Axilinear shaped charge devices **1105**A-**1105**H in array **1100** has a precision initiation device that ignites each separate Axilinear device in the array, simultaneously or at prescribed times. The Axilinear charge devices **1105**A-**1105**H in array **1100** can use single or multiple detonators that initiates a multi-purpose peripheral initiator which in turn initiates the aft end of the high explosive billet **1115**A-**1115**H of each device in the array within micro-seconds of each other. Each device **1105**A-**1105**H after initiation produces a combination rod and spade jet, the proximity of the symmetrical axis's of each device allows the aft flattened spade portions of the jets to combine forming a periphery jet of the shape of the arrangement of the individual devices. For very large applications a central charge or concentric rings of arrays can be used to remove any core material left behind.

The configuration shown in FIGS. **18**-**21** of the Axilinear device produces a full periphery of jet material that is approximately two thirds the diameter of the outer diameter or periphery of the shaped charge array and will produce a full hole in the target. Axilinear arrays can contain other numbers, sizes and quantities devices, can be arranged into many geometrical configurations including circular, polygonal and splined that will produce forward rod jets and aft spade jets in close proximity to each other that will merge together at the aft flattened spade portions of the jets. The distance between each device **1105**A-**1105**H in the array can also be aligned close enough to allow the spade portion of the jets to remove the target material between each perforation.

Many geometrical jet stream (explosive) patterns other than circular (e.g. polygonal and splined) can be achieved by changing the Axilinear device collapse plane **1108**A-**1108**H alignment, spacing and angles. For instance, in another alternative embodiment, FIG. **22**-**24** show a circular Axilinear device array **1101** of eight individual Axilinear shaped charge devices **1105**A-**1105**H held together by a rigid retaining structure **1110** around the array axis of symmetry **1112**. Each individual Axilinear shaped charge device **1105**A-**1105**H in FIGS. **22**-**24** can be, and are, configured in the manner described above with respect to the embodiments shown and described in FIGS. **1**-**10** and **12**-**17**, as well as FIGS. **18**-**21**, including all components, configurations, and possible modifications and variations thereof. Namely, each shaped charge device is configured in a manner where each shaped charge means an explosive device, having a shaped liner, driven by a similarly shaped mating explosive billet, having an initiation device, the necessary containment, confinement and retention of the liner to the explosive billet. The result of detonation of this device is a high speed stream of material produced from the convergence of the liner driven by the explosive. This is commonly known as the Munroe Effect. The shape and size of this stream of material commonly called a jet, is dependent on the starting shape and size of the liner and explosive billet.

The Axilinear liner in each shape charge device (e.g. **1105**A) in the present invention consists of two sections, aft section "B", and forward section "C". The aft section "B" is a full circumference of one of, or combination of the liner profiles, shown in the figure section of this document. This section B produces an axisymmetric rod like stretching jet with length proportional to the length of the liner section, the stretch rate, and time of flight of the jet.

The forward section "C" in each shape charge device (e.g. **1105**A) consists of less than full circumference walls extending beyond the end of section B, these wing extensions are symmetrically one hundred eighty degrees apart. These wing extensions have axisymmetric cavity as viewed from inside the hollow liner form, this cavity functions to provide the convergence and work into the liner material to cause it to rise in temperature and ductility causing plastic flow. The jet from section C produces a planar symmetric stretching wide non round jet which cuts a slot rather than a round hole as produced by the rod portion of the jet.

With respect to the Axilinear array **1101** of FIG. **22**, this embodiment is a variation of the FIG. **18** embodiment with the Axilinear devices **1105**A-**1105**H being rotated 90 degrees on their longitudinal axis within the rigid retaining structure **1110** while keeping their radial position about array symmetrical axis **1112**. FIG. **23** is a section view along line H-H of FIG. **22** that clarifies the orientation of the Axilinear shaped charge devices **1105**A-**1105**E and the EW liner collapse planes **1108**A, E with symmetrical axis **1112** within the array of the FIG. **22** embodiment. The collapse planes **1108**A and **1108**E of device **1105**A and **1105**E are parallel to line H-H and all eight devices in this array are oriented the same relative to the symmetrical axis **1112** of the array. The FIG. **23** section view of device **1105**A and **1106**E shows the inside face of one wing of EW liner **1106**A and **1106**E and a normal view point of collapse plane **1108**A and **1108**E.

FIG. **24** illustrates a target **1130** that shows a circular star like pattern of eight elongated perforated slots **1136**A-**1136**H, and the deep hole penetrations **1135**A-**1135**H made by a circular array of eight Axilinear jets from the embodiment of FIG. **22**. The orientation and direction of the elongated slots are controlled by the orientation and direction of the Axilinear device **1105**A-**1105**H collapse planes **1108**A-**1108**H, and match the direction as the array collapse planes shown in FIG. **22**. The elongated perforated slots **1136**A-**1136**H are created by the spade portion of the jets and at the center of each elongated slot are deep hole **1135**A-**1135**H penetrations created by the rod portion of the array **1101** Axilinear jets. The cavities in target **1130** is what would be expected if the target material was a metal or other material with properties similar to metal, much larger slots and diameter holes with many surrounding fractures would be expected in masonry or rock like material. The slotted holes **1136**A-**1136**H are shown in FIG. **24** separated by target material between each slot, the material between each slot could easily be removed, forming a large cavity by changing the number of charges and spacing between them and the overall diameter of the array.

The orientation of the Axilinear shaped charge devices **1105**A-**1105**H within arrays can be rotated other than perpendicular or parallel to the radial line of the array symmetrical axis **1112**. Rotating each device in the array also rotates the flattened spade portion of the jet and the resultant elongated hole made by the spade jet. Thus, rotating the devices **1105**A-H in the array **1101** shown in FIG. **22** produces a rotation of the collapse planes **1108**A-E an equal amount as shown in FIG. **23**, which changes and controls the effect of the array jet pattern **1135**A-H and **1135**A-H as shown in FIG. **24**. By rotating the shape charge devices **1105**A-H in this manner, there are a substantial number of

different target penetration patterns that can be achieved. Further, the number of array devices, the angle of inclination front to back, and orientation of the devices within the array can be adjusted and modified to produce an incredible number of different target patterns.

With respect to the Axilinear array **1200** of FIG. **25**, this embodiment is a variation of the FIG. **18** embodiment with the Axilinear devices **1205**A-**1205**E being fastened together with a clevis pin **1212**A-**1212**D forming an articulating array **1200**. The forward ends of Axilinear charges **1205**A-**1205**E has a clevis tang **1210** on one side and on the opposite side a clevis yoke **1211** that enables the charges to be held together and articulated about the clevis pin **1212**A-**1212**D longitudinal axis, the tang **1210** and yoke **1211** can be 180 degrees apart about the longitudinal axis of each component or any other angle for the desired application. Clevis pin **1212**A-**1212**D could be replaced with a ball and socket joint that would add a rotational degree of freedom to rotate collapse planes **1208**A-**1208**E in virtually any direction within the ball and socket limits.

EW liners **1206**A-**1206**E in FIG. **25** are positioned where the wing collapse planes **1208**A-**1208**E are coplanar with each clevis pin **1212**A-**1212**E longitudinal axis; when an individual Axilinear component of the array is rotated about one of its clevis pins longitudinal axis the collapse plane of that component rotates an equal amount. Rotating the Axilinear charges about a pinned joint allows infinite array shapes and infinite elongated cavity shapes formed by the spade jets after detonation of the array. Articulating arrays of Axilinear shaped charges allows in the field adaptability to solve many mining and demolition applications.

FIG. **26** and FIG. **27** clarify the construction of an individual Axilinear shaped charge of the FIG. **25** array **1200**. Axilinear charge **1205** has a clevis tang **1210** at the forward end that has a round hole **1213** through tang **1210** and the longitudinal axis of hole **1213** being coplanar with the collapse plane **1208** of EW liner **1206**. A clevis yoke **1211** at the forward end of charge **1205** with a round hole **1214** through yoke **1211** and the longitudinal axis of hole **1214** being coplanar to collapse plane **1208**. Yoke **1211** is positioned on the opposite side of charge **1205** from tang **1210**, being 180 degrees opposed to tang **1210**.

Two Axilinear charges **1205** can be mated together by placing tang **1210** of the first charge in the center space **1214** of yoke **1211** of the second charge, aligning the holes **1213** and **1214** about their longitudinal axis and inserting a clevis pin to fasten the two charges together. When detonated the Axilinear charge **1205** forms a rod and flattened spade jet, the flattened spade portion of the jet is coplanar with collapse plane **1208**. Fastening together Axilinear charges **1205** in close proximity, forming an array of charges, then detonating the charges, forming an array of jets, allows the spade potion of each charge to overlap or intersect; these overlapping jets will erode a large deep cavity in a target material that matches the geometrical shape of the array.

Any number of Axilinear components can be used, and angles between each component can be adjusted to form almost any pattern e.g. curved spline, circle, polygon or straight line, as well as adjusting the orientation rotation of the shaped charge devices **1205**A-E in the array **1200**. That is, any number of charges can be fastened together to form an array of almost any geometrical shape and size as required for the specific application.

It is also possible, the inventor further claims that multiple follow on devices of the same size can be sequentially delivered into the hole, in a semi-infinite target, and their cumulative penetrations are taken advantage of, to extend this hole to extreme depths in any direction such as in oil well stimulation. Each time a charge is detonated in a hole such as oil or gas bearing formations the shock and concussion from the explosive will fracture the formation around it. Further as the high pressure gasses from the explosive dissipate a low pressure volume is created in the perforation hole inviting the formation pressure into the hole and clearing the hole surface of any debris or coating.

Shaped charge liners come in many shapes, angles and sizes, the disclosure in this patent application intends this wide variety of options (as shown in figure section) as part and parcel of the claims of this application. With respect to the array configurations, by rotating the shape charge devices **1105**A-H or **1205**A-H in this manner, there are a substantial number of different target penetration patterns that can be achieved. Further, the number of array devices, the angle of inclination front to back, and orientation of the devices within the array can be adjusted and modified to produce an incredible number of different target patterns. While the invention has been particularly shown and described with respect to preferred embodiments, it will be readily understood that minor changes in the details of the invention may be made without departing from the spirit of the invention.

Having described the invention, we claim:

1. A shaped charge explosive array, comprising:

a plurality of explosive shaped charge devices, each said explosive shaped charge device having a longitudinal axis that extends along the length of the explosive device from a rearward end to a forward end, each said explosive shaped charge device having a liner, a high explosive billet charge, and a detonator coupled to the high explosive billet charge for initiating detonation of the explosive charge, said detonator providing initiation to the high explosive billet of each said explosive shaped charge device to produce transform the liner into a jet stream projectile oriented on a collapse plane configuration, and said liner having a first full conical liner section located from a cone apex longitudinal position to a winged vertex longitudinal position and a second winged liner section extending from said winged vertex longitudinal position to a winged base end at the forward end of the liner;

a rigid retaining structure that supports the placement of a plurality of shaped charge devices in an array orientation relative to a longitudinal array axis of symmetry where said longitudinal array axis is substantially aligned in parallel with the longitudinal axis of said plurality of explosive shaped charge devices,

said plurality of explosive shaped charge being spaced and configured so their collapse planes are aligned around a common symmetrical axis and upon a substantial simultaneous detonation of the plurality of shape charges in the array, a series of connecting penetrations forms a large circle penetration substantially in the direction of said longitudinal array axis of symmetry.

2. The shaped charge explosive array of claim **1** wherein the first full conical liner section of the liner is formed substantially in a full conical shape circumferentially rotated around the longitudinal axis with a cone apex of the first full conical liner being located substantially near said longitudinal axis and toward the rearward end of the shaped charge explosive device, and said first full conical liner section having conical walls extending circumferentially around the longitudinal axis and extending at an angle A°/2 from said cone apex forward toward the winged vertex longitudinal length of the shaped charge explosive device.

3. The shaped charge explosive array of claim **1** wherein the second winged liner section has two winged wall extensions, each winged wall extension being planar symmetric about a horizontal plane with the opposing winged wall extension, each winged wall extension having conical walls partially circumferentially rotated around the longitudinal axis between two winged arc ends and each said winged wall extensions located between said two winged arc ends extending from said winged vertex longitudinal length contiguous with the first full conical liner section forward to a forward end of the liner of the shaped charge explosive device.

4. The shaped charge explosive array of claim **3** wherein the winged arc ends at corresponding ends of opposing winged wall extensions have a face hollow concavity in the liner material on two opposing sides of the base end of the liner conical profile that extends from the winged vertex longitudinal length to each respective winged arc end for the opposing winged wall extensions.

5. The shaped charge explosive array of claim **4** wherein the said each face hollow concavity being a parabolic shape extending from each winged arc end to said winged vertex longitudinal length and each face hollow concavity being planar symmetric about a vertical plane.

6. The shaped charge explosive array of claim **1** wherein the explosive billet charge surrounds a first full conical liner section.

7. The shaped charge explosive array of claim **1** wherein the explosive billet charge surrounds a partially circumferential winged wall extensions with an additional charge located behind the conical apex of said liner.

8. The shaped charge explosive array of claim **1** further comprising an outer charge body that is an external containment casing surrounding said high explosive billet charge of the shaped charge explosive device.

9. The shaped charge explosive array of claim **1** further comprising two outer charge body walls located in the face hollow concavity in the liner material on two opposing sides of the base end of the liner conical profile that extends from the winged vertex longitudinal length to each respective winged arc end for the opposing winged wall extension.

10. The shaped charge explosive array of claim **1** wherein the detonator is coupled to rearward end of high explosive billet charge for initiating detonation of the explosive charge, said detonator providing initiation to the high explosive billet to produce transform the liner into said jet stream projectile having a rod shaped projectile portion and a flattened broad-based spade with an extended forward tip shaped projectile portion in its tip to tail configuration.

11. A shaped charge explosive array of claim **2** wherein the angle of the conical walls on the second winged liner section are substantially aligned with the conical walls of said first full conical liner section.

12. A shaped charge explosive array of claim **2** wherein the angle of the conical walls on the second winged liner section are at an angle greater than the A°/2 aligned with the conical walls of said first full conical liner section.

13. A shaped charge explosive array of claim **2** wherein the angle of the conical walls on the second winged liner section are at an angle less than the A°/2 aligned with the conical walls of said first full conical liner section.

14. The shaped charge explosive array of claim **8** further comprising:

a frustoconical portion of the outer charge body located near the rearward end of the shaped charge device and positioned proximate to a detonator holder.

15. The shaped charge explosive array of claim **1** wherein the jet stream projectile has a velocity gradient from tip to tail with a tip velocity being up to 10 km/s.

16. The shaped charge explosive array of claim **15** wherein the tip velocity will depend on the included angle of the liner, the charge to mass ratio, the confinement of the liner, or shape of the liner.

17. The shaped charge explosive array of claim **1** wherein the jet stream projectile has a velocity gradient from tip to tail with jet tail velocity being substantially 2 km/s.

18. A shaped charge explosive array, comprising:

a plurality of explosive shaped charge devices, each said explosive shaped charge device having a longitudinal axis that extends along the length of the explosive device from a rearward end to a forward end and a longitudinal angle of orientation, each said explosive shaped charge device having a liner, a high explosive billet charge, and a detonator coupled to the high explosive billet charge for initiating detonation of the explosive charge, said detonator providing initiation to the high explosive billet of each said explosive shaped charge device to produce transform the liner into a jet stream projectile oriented on a collapse plane configuration corresponding to the longitudinal angle of orientation, which is substantially aligned in parallel with the longitudinal axis of a plurality of explosive shaped charge devices, and said liner has a first full conical liner section located from a cone apex longitudinal position to a winged vertex longitudinal position and a second winged liner section extending from said winged vertex longitudinal position to a winged base end at the forward end of the liner;

one or more retaining structures that supports the placement of a plurality of shaped charge devices in an array orientation,

said plurality of explosive shaped charge being spaced and configured so their collapse planes form an array jet stream upon substantial simultaneous detonation of the plurality of shape charges in the array that are directed along said longitudinal angle of orientation.

19. The shaped charge explosive array of claim **18** wherein the first full conical liner section of the liner is formed substantially in a full conical shape circumferentially rotated around the longitudinal axis with a cone apex of the first full conical liner being located substantially near said longitudinal axis and toward the rearward end of the shaped charge explosive device, and said first full conical liner section having conical walls extending circumferentially around the longitudinal axis and extending at an angle A°/2 from said cone apex forward toward the winged vertex longitudinal length of the shaped charge explosive device.

20. The shaped charge explosive array of claim **18** wherein the second winged liner section has two winged wall extensions, each winged wall extension being planar symmetric about a horizontal plane with the opposing winged wall extension, each winged wall extension having conical walls partially circumferentially rotated around the longitudinal axis between two winged arc ends and each said winged wall extensions located between said two winged arc ends extending from said winged vertex longitudinal length contiguous with the first full conical liner section forward to a forward end of the liner of the shaped charge explosive device.

21. The shaped charge explosive array of claim **20** wherein the winged arc ends at corresponding ends of opposing winged wall extensions have a face hollow concavity in the liner material on two opposing sides of the base end of the liner conical profile that extends from the winged vertex longitudinal length to each respective winged arc end for the opposing winged wall extensions.

22. The shaped charge explosive array of claim **21** wherein the said each face hollow concavity being a parabolic shape extending from each winged arc end to said winged vertex longitudinal length and each face hollow concavity being planar symmetric about a vertical plane.

23. The shaped charge explosive array of claim **18** wherein the explosive billet charge surrounds a first full conical liner section.

24. The shaped charge explosive array of claim **18** wherein the explosive billet charge surrounds a partially circumferential winged wall extensions with an additional charge located behind the conical apex of said liner.

25. The shaped charge explosive array of claim **18** further comprising an outer charge body that is an external containment casing surrounding said high explosive billet charge of the shaped charge explosive device.

26. The shaped charge explosive array of claim **18** further comprising two outer charge body walls located in the face hollow concavity in the liner material on two opposing sides of the base end of the liner conical profile that extends from the winged vertex longitudinal length to each respective winged arc end for the opposing winged wall extension.

27. The shaped charge explosive array of claim **18** wherein the detonator is coupled to rearward end of high explosive billet charge for initiating detonation of the explosive charge, said detonator providing initiation to the high explosive billet to produce transform the liner into said jet stream projectile having a rod shaped projectile portion and a flattened broad-based spade with an extended forward tip projectile portion in its tip to tail configuration.

28. A shaped charge explosive array of claim **19** wherein the angle of the conical walls on the second winged liner section are substantially aligned with the conical walls of said first full conical liner section.

29. A shaped charge explosive array of claim **19** wherein the angle of the conical walls on the second winged liner section are at an angle greater than the A°/2 aligned with the conical walls of said first full conical liner section.

30. A shaped charge explosive array of claim **19** wherein the angle of the conical walls on the second winged liner section are at an angle less than the A°/2 aligned with the conical walls of said first full conical liner section.

31. The shaped charge explosive array of claim **25** further comprising:

a frustoconical portion of the outer charge body located near the rearward end of the shaped charge device and positioned proximate to a detonator holder.

32. The shaped charge explosive array of claim **18** wherein the jet stream projectile has a velocity gradient from tip to tail with tip velocity being up to 10 km/s.

33. The shaped charge explosive array of claim **32** wherein the tip velocity will depend on one or more of the following factors: the included angle of the liner, the charge to mass ratio, the confinement of the liner, or shape of the liner.

34. The shaped charge explosive array of claim **18** wherein the jet stream projectile has a velocity gradient from tip to tail with jet tail velocity being substantially 2 km/s.

35. A shaped charge explosive array, comprising:

a plurality of explosive shaped charge devices, each said explosive shaped charge device having a longitudinal axis that extends along the length of the explosive device from a rearward end to a forward end, each said explosive shaped charge device having a liner, a high explosive billet charge, and a detonator coupled to the high explosive billet charge for initiating detonation of the explosive charge, said detonator providing initiation to the high explosive billet of each said explosive shaped charge device to produce transform the liner into a jet stream projectile oriented on a collapse plane configuration, and said liner has a first full conical liner section located from a cone apex longitudinal position to a winged vertex longitudinal position and a second winged liner section extending from said winged vertex longitudinal position to a winged base end at the forward end of the liner;

one or more retaining structures that supports the placement of a plurality of shaped charge devices in an array orientation relative to a longitudinal array axis of symmetry,

said plurality of explosive shaped charge being aligned in parallel with each other along said longitudinal array axis of symmetry, spaced and configured so their collapse planes are aligned and upon a substantial simultaneous detonation of the plurality of shape charges in the array, a series of connecting penetrations forms an aligned penetration that extends substantially outwardly in the direction of said longitudinal array axis of symmetry.

36. The shaped charge explosive array of claim **35** wherein the jet stream projectile has a velocity gradient from tip to tail with tip velocity being up to 10 km/s.

37. The shaped charge explosive array of claim **36** wherein the tip velocity will depend on one or more of the following factors: the included angle of the liner, the charge to mass ratio, the confinement of the liner, or shape of the liner.

38. The shaped charge explosive array of claim **35** wherein the jet stream projectile has a velocity gradient from tip to tail with jet tail velocity being substantially 2 km/s.

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