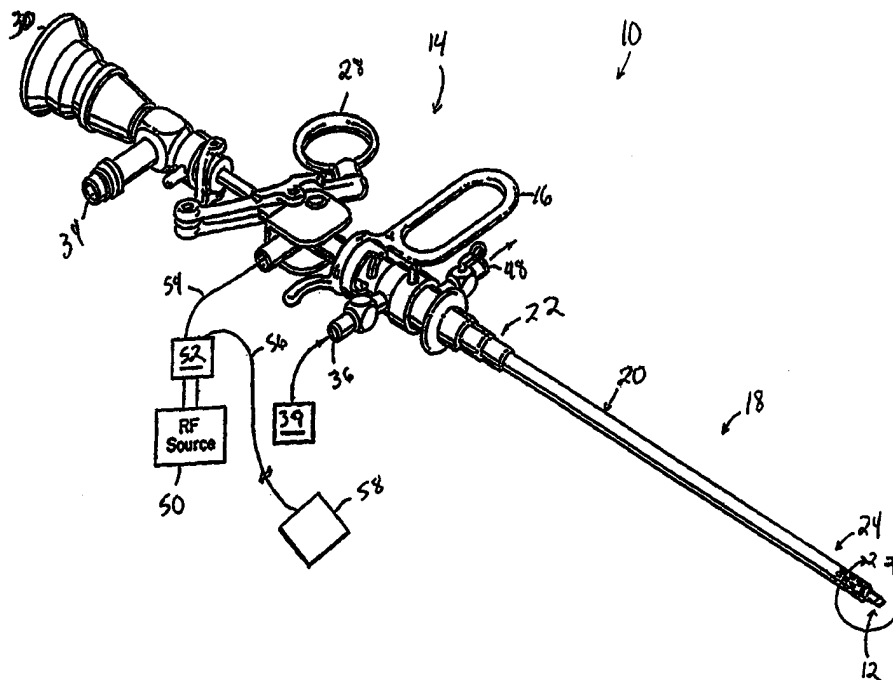




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<b>(21) International Application Number:</b> PCT/US98/11720 <b>(22) International Filing Date:</b> 5 June 1998 (05.06.98)  <b>(30) Priority Data:</b> 60/049,363      6 June 1997 (06.06.97)      US  <b>(71) Applicant:</b> MEDICAL SCIENTIFIC, INC. [US/US]; 125 John Hancock Road, Taunton, MA 02780 (US).  <b>(72) Inventors:</b> NARDELLA, Paul, C.; 12 Cromesett Point, Wareham, MA 02571 (US). WRUBLEWSKI, Thomas, A.; 5 Tall Tree Road, Sharon, MA 02067 (US). VIDYARTHI, Piush; 2955 Van Ness Avenue, San Francisco, CA 94109 (US). N'GUYEN, Trinh, N.; 1057 Shell Boulevard #1, Foster City, CA 94404 (US). TON, Dai, T.; 1514 Mount Diablos Avenue, Milpitas, CA 95035 (US). BACICH, Steven, R.; 20 Fairway Place, Half Moon Bay, CA 94019 (US).  <b>(74) Agents:</b> GEARY, William, C., III et al.; Nutter, McClen- nen & Fish, LLP, One International Place, Boston, MA 02110-2699 (US).		<b>(81) Designated States:</b> AU, CA, JP, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report.</i>

**(54) Title:** SELECTIVELY COATED ELECTROSURGICAL INSTRUMENT



**(57) Abstract**

This invention is an electrosurgical instrument (10) having an active electrode (12) with a portion that is coated with an insulative material. An exposed portion of the electrode (12) is effective to treat tissue, while the insulative coating minimizes energy dissipation into surrounding isotonic solution.

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## SELECTIVELY COATED ELECTROSURGICAL INSTRUMENT

### FIELD OF THE INVENTION

The present invention relates to electrosurgical instruments and more particularly to electrosurgical instruments including an electrode with exposed and non-exposed portions.

### BACKGROUND OF THE INVENTION

Electrosurgical devices utilize electrical current, such as radio frequency (RF) energy, to cut and to cauterize tissue. The electrical current is delivered via a tissue-contacting portion of the device. The current facilitates a clean tissue cut with little or no bleeding by rapidly heating the tissue without unnecessarily damaging adjacent tissue. Electrosurgical tools can also cauterize tissue separately from or together with a cutting procedure.

Instruments for performing electrosurgery generally include an energy source or generator, an active electrode for delivering electrical energy to tissue to be treated, a return electrode to complete the electrical circuit and conductors for coupling the energy source to the active and return electrodes. A monopolar electrosurgical instrument includes an active electrode for cutting tissue and a remotely located return electrode for providing a current return path. Typically, the return electrode is in contact with a relatively large tissue area, such as a portion of the lower torso, for dispersing exiting current to prevent burning of tissue.

Various types of open and closed surgical procedures utilize electrosurgical devices. Closed surgical procedures include arthroscopic, endoscopic, hysteroscopic, urologic, resectoscopic and laparoscopic procedures. For example, a hysteroscope is used in a closed surgical procedure for treatment of various conditions within a woman's uterine cavity. Typical uses of hysteroscopes include fibroid removal, intrauterine adhesion removal, endometrial ablation and correction of abnormal uterine bleeding.

Some surgical procedures, such as arthroscopic and hysteroscopic procedures, require distension of the surgical area in order to increase visibility at the treatment site or to minimize space constraints. In some instances the surgical area is distended using a fluid.

5 An electrolyte-free (i.e., hypotonic) distension fluid is typically used in such procedures to prevent the electrical current delivered by the active electrode from dissipating to an ineffective level. However, absorption of excess quantities of hypotonic solution into a patient's bloodstream can alter the patient's electrolyte levels and potentially result in dangerous conditions, including cardiac arrhythmia, 10 brain swelling and even death. The risk of these dangers may cause the surgeon to terminate the procedure before completion. Furthermore, hypotonic solutions are expensive as compared to isotonic solutions.

Although monopolar electrosurgical instruments are useful, there is a need for instruments that are effective in isotonic solutions, especially those instruments 15 useful in closed surgical procedures, such as arthroscopy, endoscopy, hysteroscopy, laparoscopy and resectoscopy.

## SUMMARY OF THE INVENTION

The present invention is directed to an electrosurgical instrument having an active electrode with a coated or covered first portion and an exposed second portion 20 which is intended for contacting a treatment site of a patient. The coating or covering is at least partially insulative and serves to direct the delivery of electrosurgical energy from the exposed portion of the active electrode. With this arrangement, the conductive surface area of the electrode in contact with surrounding fluid is reduced, thereby minimizing current dissipation into the 25 surrounding fluid. The electrosurgical instrument of the present invention thus enables the effective use of monopolar electrosurgical tools in an isotonic fluid medium.

In one embodiment, an electrosurgical instrument includes an active electrode selectively coated on a first portion thereof with an insulative or semi-insulative 30 material so as to leave a second, tissue-contacting portion exposed. Generally, a tip

portion of the tool is exposed. The geometry of the tissue-contacting or tissue-affecting portion of the active electrode may take various forms depending on the intended application of the electrosurgical instrument. Preferably, the coating material is insulative. More generally however, the coating material has an impedance greater than the impedance of the exposed portion, thus creating a path of lower electrical resistance between the energy source and the exposed portion so as to direct the energy to the exposed portion. In a preferred embodiment, the impedance from the electrode through the coating to the isotonic medium, including any reactance due to parasitic capacitance associated with the coating, is at least one order of magnitude greater than the impedance of the desired current path for an operating frequency of the instrument.

In an exemplary embodiment, the active electrode of the electrosurgical instrument has a channel shape, with one or both sides of the channel being blade-like. An intermediate portion of the electrode is coated with an at least semi-insulative material and the blade-like sides of the electrode are exposed. Alternatively, the active electrode can be in the shape of a loop wherein a portion of the surface area of the loop is coated with an insulative or semi-insulative material. In other embodiments, the active electrode has a generally spherical or cylindrical shape with an exposed portion and a coated portion. Other electrode shapes, such as truncated spheres and cylinders, are also possible

In a further embodiment in accordance with the present invention, an electrosurgical instrument includes an electrode assembly which is pivotally secured to a frame via a coupling mechanism. The electrode assembly includes an electrode having a portion that is coated with an insulative material and an uncoated exposed portion. In one embodiment, the electrode is pivotable from a first position to a second position upon the application of pressure generally along a longitudinal axis of the frame. The pivotable nature of the electrode allows a surgeon to selectively contact tissue with the exposed portion of the electrode by increasing the electrode/tissue contact area.

In still another embodiment, an electrode assembly includes a body formed from a non-conductive material and a conductive coating disposed on a portion of the non-conductive body. The electrode can be formed in a variety of geometries including spherical, hemispherical, cylindrical, and that of a surgical loop. The conductive coating, which is in electrical communication with a source of electrosurgical energy, is effective to treat tissue while the non-conductive body is effective to reduce energy dissipation in an isotonic solution environment.

#### BRIEF DESCRIPTION OF THE DRAWINGS

The invention will be more fully understood from the following detailed description taken in conjunction with the accompanying drawings, in which:

FIG. 1 is a perspective view of a monopolar electrosurgical instrument having a selectively coated active electrode in accordance with the present invention;

FIG. 2 is an enlarged perspective view of a distal end of the electrosurgical instrument of FIG. 1;

FIG. 2A is an alternative embodiment of the electrosurgical instrument of FIG. 2;

FIG. 2B is a further embodiment of the electrosurgical instrument of FIG. 2;

FIG. 3 is an enlarged perspective view of the active electrode of FIG. 1;

FIG. 3A is an alternative embodiment of the active electrode of FIG. 3;

FIG. 4A is another embodiment of the electrosurgical instrument of FIG. 2;

FIG. 4B is a further embodiment of the distal end of the electrosurgical instrument of FIG. 4A;

FIG. 4C is a sectional view of a portion of the electrosurgical instrument of FIG. 4B at lines 4C-4C.

FIG. 5A is a perspective view of another embodiment of an active electrode in accordance with the present invention;

FIG. 5B is a perspective view of a further embodiment of an active electrode in accordance with the present invention;

FIG. 6A is a side view of an electrode assembly in accordance with the present invention with the assembly having an electrode shown in a first position;

FIG. 6B is a side view of the electrode assembly of FIG. 6B with the electrode shown in second position;

5           FIG. 6C is a top view of the electrode assembly of FIG. 6A;

FIG. 7 is a perspective view of an electrode assembly in accordance with the present invention, the assembly having a non-conductive body in the form of a surgical loop and a conductive coating;

10           FIG. 8A is a perspective view of another embodiment of an electrode assembly in accordance with the present invention, the assembly having a hemispherical non-conductive body and a conductive coating;

FIG. 8B is a perspective view of a further embodiment of an electrode assembly in accordance with the present invention, the assembly having a non-conductive body with a generally hemi-cylindrical shape and a conductive coating;

15           FIG. 8C is a perspective view of a still further embodiment of an electrode assembly in accordance with the present invention, the assembly having a generally spherical non-conductive body and a conductive coating;

#### DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENT

20           Referring to FIGS. 1-3, in which like reference numbers are used to indicate the same elements, an electrosurgical instrument 10 includes a selectively coated active electrode 12 for delivering electrical current to a treatment site of a patient. The instrument is suitable for insertion into the patient in accordance with closed surgery (e.g., arthroscopic, endoscopic, hysteroscopic, urologic, resectoscopic and laparoscopic procedures) or open surgery. The illustrative instrument 10 is a  
25           hysteroscope in which the active electrode 12 is intended for insertion into the uterine cavity of a female patient for treatment of various conditions. It will be appreciated however that various types of electrosurgical instruments can be used for other procedures while utilizing and achieving the advantages of the selectively coated electrode described herein.

5 The instrument 10 includes a proximal portion 14, including a handle 16 for user handling of the instrument in order to guide the electrode 12 into contact with the treatment site, and a forward portion 18. The forward portion 18 includes an elongated probe 20 having a proximal end 22 adjacent to the handle 16 and a distal end 24 from which the active electrode 12 retractably extends. The electrode 12 is capable of being moved along the longitudinal axis of the probe 20 so as to extend through an aperture 26 (FIG. 2) at the distal end 24 of the probe 20 to contact tissue or to be retracted into the end 24 of the probe 20 through the aperture 26. An actuator 28 permits retraction and extension of the electrode 12 via a mechanical coupling within the probe 20.

10 An optical path within the instrument 10 extends between an eye piece 30 at the rearward portion 14 and a lens 32 at the distal end 24 of the probe 20. The optical path permits the surgeon to view the treatment site. To further facilitate visualization of the treatment site, a light delivery port 34 permits light to be introduced into the optical path.

15 The electrosurgical instrument 10 is capable of delivering fluid to and collecting fluid from the treatment site. To this end, the instrument 10 includes a fluid input port 36 which is adapted for coupling to an external fluid source 38. The fluid thus introduced into the instrument 10 is directed toward the distal end 24 of the probe 20 via a first, inner fluid channel 38, where the fluid exits the instrument aperture 26. More particularly, the first fluid channel 38 is defined by an inner sheath 40. A second, outer fluid channel 42 between an outer sheath 44 of the probe 20 and the inner sheath 40 serves to collect fluid from the treatment area. To this end, a fluid intake, such as apertures 46 through the outer sheath 44, permit fluid collection. Fluid from the treatment area flows through the second fluid channel 42 toward the proximal end 22 of the probe 20, where the fluid exits the instrument through a fluid output port 48. In one embodiment (FIG. 2), an end of the outer sheath 44 extends beyond an end of the inner sheath 40. In another embodiment (FIG. 2A), the inner sheath 40 extends beyond the end of the outer sheath 44.



5 An energy source 50, such as a source of radio frequency (RF) energy, provides electrical energy for delivery by the active electrode 12 to the treatment site. More particularly, a control device 52 coupled between the energy source 50 and the instrument 10 permits conventional control of alternating current provided by the source 50, including the ability to turn the energy source on and off as a function of the position of the electrode 12 relative to the treatment site. Conductors 54 and 56 carry the current from or to the energy source, and may be referred to as an active conductor 54 and a return conductor 56. In an exemplary embodiment, the current delivered to the treatment site ranges from 0.1 to 2.0 amps.

10 The selectively coated electrode of the invention can be a monopolar device, with the return conductor 56 being coupled to a return electrode in the form of a ground pad 58 which is suitable for external attachment to a patient's skin. In particular, the return electrode 58 contacts the patient's body at a remote location relative to the treatment site at which the active electrode 12 is located. The active conductor 54 is coupled to the active electrode 12 through an electrical path within the probe 20.

15 In another embodiment, at least a portion of the outer sheath and/or inner sheath can form a return electrode for the device. As shown in Figure 2B, the outer sheath 44 can have a coated portion 47 that is electrically insulated by the coating material and an exposed return electrode portion 49. The return electrode portion can be formed as desired to obtain a desired amount of surface area for the return electrode of the device. This arrangement eliminates or supplements a return electrode in contact with the patient's body.

20 It is understood that the selectively coated electrode of the invention can be used with a delivery instrument other than the hysteroscope illustrated in Figure 1. One of ordinary skill in the art will appreciate that the selectively coated electrode can be used with other scope-like instruments, with or without modification of the electrode. Further, the selectively coated electrode of the invention can be used in open surgical procedures without a scope-like delivery device.

The active electrode 12 includes a first portion 60 covered with a coating. A second, tissue-affecting portion 62 of the active electrode remains exposed. The tissue-affecting portion of the electrode is understood to be the portion of the electrode from which current is delivered to tissue. This portion of the electrode is largely responsible for cutting and/or cauterizing tissue that it contacts. A frame 64 coupled to the active electrode 12 provides a mechanism for mechanically supporting the electrode 12. Further, the frame 64 may be conductive and may provide a mechanism for coupling electrical energy from a source (not shown) to the tissue-affecting portion 62 of the electrode. The conductive frame should be coated, at least in part, with an insulative coating to reduce energy dissipation in the surrounding isotonic solution. In a further embodiment, the frame is a hollow, non-conductive member having a conductive path therein to allow the electrosurgical generator to energize the active electrode.

In one embodiment, illustrated in Figures 2 and 3, the electrode 12 is substantially channel-shaped, with the tissue-affecting portion 62 terminating at a sharp, blade-like tip 63. The coating material can extend over virtually the entire surface of the electrode, except for the sharpened edge of the blade-like tip 63. The smaller the surface area of the non-coated portion of the electrode, the greater will be the density of current emanating from the electrode. This feature increases the ability of the electrode to deliver current directly to the target tissue with little or no current dissipation in an isotonic fluid environment when the electrode is contacting target tissue or to non-target tissue.

While the coating effectively insulates the covered first portion 60 of the active electrode, there is a parasitic capacitance formed on the covered first portion due to the coating. The insulative, or partially insulative, coating acts as a dielectric between conductive isotonic solution and the first portion 60 of the electrode producing a capacitive effect. The parasitic capacitance has a reactance associated therewith that forms a portion of the impedance through the solution and the coated first portion 60 of the active electrode. Preferably, this impedance is much greater than the impedance between the exposed tissue-affecting portion 62 of the active electrode and the solution or tissue.

5 In a preferred embodiment, the impedance associated with the coated first portion 60 of the electrode is at least one order of magnitude greater than the impedance of the desired current path from the tissue affecting portion 62 of the electrode to tissue and/or isotonic solution at the desired operating frequency of the electrosurgical tool. As is understood by one of ordinary skill in the art, the reactance due to the parasitic capacitance of the coated first portion of the electrode, and therefore the impedance, is frequency dependent. Thus, impedances are measured at the operating frequency of the RF energy source 50. The impedance through the coating can be chosen to be much greater than the impedance of the desired current path by adjusting the thickness of the coating material. To provide the preferred much greater impedance through the coated portion of the electrode for a given operating frequency, a coating thickness is selected to obtain the desired impedance value.

15 In one embodiment, the coating material is an insulative or partly insulative material. It is understood that insulative, as used herein, is to be construed broadly. In an exemplary embodiment, the coating is a medical grade ceramic material, such as aluminum oxide. Other coating materials include ceramics (e.g., glass, aluminum-silicate, alumina, or boron), non-conductive epoxy, ceramic adhesive, glass enamels, glass-filled polymers, polysulfones, polytetrafluoroethylene, polysiloxanes, silicones, polyetheretherketone, Parylene, and Kevlar. It will be appreciated by those of ordinary skill in the art that the thickness of the coating material can be readily varied. In a preferred embodiment, however, the thickness is in the range of about 2 microns to about 150 microns. The ceramic coating can be applied by vacuum chamber deposition or by electrostatically spraying a ceramic material and curing the coating at a suitable temperature. Other coating techniques will be apparent to those having ordinary skill in the art.

25 In a further embodiment shown in Figure 3A, the electrode has dual blade-like edges 63', with an insulative coating in the area between the edges. This dual-edged arrangement is well suited for certain procedures involving scraping of tissue. Many other electrode geometrics are also possible. The electrodes further may or may not have sharpened blade-like edges. An important feature of the invention is

to maximize the coated area of the electrode while minimizing the non-coated, tissue-affecting portion of the electrode. One of ordinary skill in the art will appreciate that further alternative electrode geometrics can be used without departing from the scope of the invention.

5           In other embodiments, the coating material is semi-insulative. Suitable semi-insulative coatings include those having an impedance greater than that of the exposed portion of the electrode, so as to provide a path of lower electrical resistance between the energy source and the exposed portion 62 as compared to the path between the energy-source and the coated portion 60. Thus, current is directed  
10           toward the exposed tissue-contacting portion 62 of the electrode in order to enhance the electrosurgical effect of the device. This energy focusing aspect of the instrument further serves to render the instrument suitable for use in an isotonic fluid medium by reducing the conductive surface area of the active electrode. In addition, by limiting the surface area of the exposed portion 62 of the electrode, a  
15           glow associated with the use of an energized electrode in an isotonic solution is reduced. This enhances the field of vision of the surgeon when treating tissue with the electrode.

          In an illustrative embodiment, the electrode 60 is tungsten, but other biologically compatible materials having suitable conductivity and strength can be  
20           used. Examples of suitable materials include stainless steel, tungsten, titanium, platinum, silver, gold, brass, nickel-titanium alloys and other biocompatible metals.

          Figure 4A is another embodiment of a monopolar electrosurgical instrument having an active electrode 12" in the form of a loop 70 that extends from an inner sheath 40 that is disposed with an outer sheath as discussed in conjunction with  
25           Figure 2A. The loop 70 includes a coated portion 72 and an exposed tissue-affecting portion 74. The tissue-affecting portion 74 cuts and/or cauterizes tissue under the control of an operator, such as a surgeon. Current density is maximized at the tissue-affecting portion 74 of the loop so that current dissipation in isotonic solution and non-target tissue is minimized.

Figure 4B is a further embodiment of an active electrode 12" in the form of a loop 70 having a coated first portion 72 and an exposed tissue-affecting portion 74. The loop 70 extends from a frame 64 that supports the loop during use. A return electrode 76 is electrically insulated from the loop and is disposed on the frame to provide a return path for current from the loop.

Various coating patterns can be used. Ideally, only a minimal portion of the blade should remain uncoated. Preferably the portion of the loop that is to be in contact with tissue should remain uncoated while the remainder of the loop, that is to be in contact with an isotonic solution, should be coated. Figure 4C illustrates an example of a coating pattern in which virtually the entire loop is coated except for a rear-facing circumferential portion 74. Other coating patterns may be used as well. For example, the entire loop can be coated, except for an uncoated distal-most end.

FIG. 5A shows another embodiment of an active electrode 100 having an insulative coating 102 disposed on a portion of an outer surface 104 of the electrode so as to form a coated portion 106 and a non-coated exposed portion 108. It is understood that the apportionment between the coated portion 106 and the exposed portion 108 can vary. In general, the exposed portion 108 of the electrode should be minimized to reduce energy dissipation into a conductive solution while providing a desired surface area for contact between the electrode and the tissue.

The electrode 100 can be formed in a variety of geometries including cylindrical, spherical, arcuate, convex, and hemispherical. In one embodiment, the electrode 100 is generally cylindrical with opposite first and second ends 110,112. A frame 114 includes a first structural member 116a coupled to the first end 110 of the electrode and a second structural member 116b coupled to the second end 112. The structural members 116 are affixed to the first and second ends 110,112 such that the electrode 100 remains in a predetermined position with respect to the structural members 116a,b. It is understood that the frame 114 can be affixed to the electrode 100 at a range of angles depending upon the particular orientation of the target tissue in relation to the exposed portion 108 of the electrode.

FIG. 5B shows an alternative embodiment of the electrode 100 of FIG. 5A wherein the electrode 100' has a generally spherical shape. The electrode 100' has a portion 106' coated with an insulative material and an exposed portion 108' for treating tissue.

5 In FIGS. 6A-C, an electrode assembly 200 is shown having an electrode 202 which is movable between a first position (FIG. 6A) and a second position (FIG. 6B). The electrode 202 has a portion 204 coated with an insulative material and an exposed portion 206 adapted for treating tissue. In one embodiment, a frame 208 includes first and second structural members 210a,b pivotally coupled to opposite  
10 locations on the electrode 202 via first and second coupling mechanisms 212a,b.

The coupling mechanisms 212 can be formed from a variety of mechanisms that allow selective movement of the electrode 202 with respect to the frame 208. Exemplary mechanisms include positive and negative surface features, hinges and pivoting structures. It is understood that the electrode 202 and/or the frame 208 can  
15 provide the pivoting action of the electrode assembly. In one embodiment, the coupling mechanisms 212a,b include an arcuate groove 214 formed in the electrode 202 into which distal tips 216a,b of the structural members 210a,b are inserted. Electrical contact between the distal tips 216a,b and the electrode is maintained to  
20 provide a constant flow of energy to the electrode. The electrode 202 rotates between the first position (FIG. 6A) and the second position (FIG. 6B) as the distal tips 216 move within the grooves 214. The electrode 202 can be biased to the first (or second) position with a biasing member 218, such as a spring. The amount that the electrode 202 can rotate with respect to the frame 208 can range from about fifteen degrees to about ninety degrees.

25 The pivotal feature of the electrode 202 allows a surgeon to control the position of the exposed portion 206 of the electrode with respect to tissue 220. That is, with the application of pressure generally along a longitudinal axis 222 of the structural members 210, the exposed portion 206 of the electrode rotates so as to increase the contact area between the tissue 220 and the exposed portion 206 of the  
30 electrode. Thus, the pivotal feature of the electrode assembly 200 enhances the ability of a surgeon to selectively treat tissue with the exposed portion 206 of the

electrode. For example, the pivoting electrode assembly is well-suited for treating endometrium tissue with a dabbing type motion.

FIG. 7 illustrates another embodiment of an electrode assembly 300 in accordance with the present invention. The assembly 300 includes an electrode 302 formed from a coating 304, which is made from a conductive material, disposed on a body 306, which is formed from a non-conductive material. Coupled to the conductive coating 304 are conductors 308a,b extending along a frame 310 to an electrosurgical RF energy source 50 (FIG. 1).

The electrode assembly 300 can be formed in a variety of configurations such as surgical loops, spheres, cylinders, and hemispheres. In one embodiment, the electrode assembly 300, including the non-conductive body 306 and conductive coating 304, is configured as a surgical loop. The conductive coating 304 is selectively applied to the body 306 so as to provide a tissue-cutting electrode that is effective to minimize energy dissipation in an isotonic solution. In general, the conductive coating 304 should be of sufficient size to conduct operational current levels without excessive heating of the coating 304 and/or the adjacent body 306. An exemplary thickness range for the coating 304 is from about 0.0010 inch to about 0.1000 inch. It is understood that a relatively thin coating enhances coagulation and that a relatively thick coating increases durability.

The non-conductive body 306 can be formed from suitable materials that are sufficiently strong and rigid to resist breaking as pressure is applied to the electrode assembly during use. Exemplary materials for the non-conductive body include ceramics (e.g., glass, aluminum-silicate, alumina, or boron), non-conductive epoxy, ceramic adhesive, glass enamels, glass-filled polymers, polysulfones, polytetrafluoroethylene, polysiloxanes, silicones, polyetheretherketone, Parylene, and Kevlar.

The conductive coating 304 is formed from a material that provides a suitable circuit path for the applied electrosurgical energy. The conductive coating can be formed from a variety of materials including metals such as stainless steel, tungsten, titanium, platinum, silver, gold, brass, nickel-titanium alloys and other biocompatible metals.

In FIG. 8A, an electrode assembly 400 has an electrode 402 formed from a conductive coating 404 which covers a portion of a body 406 formed from a non-conductive material. In one embodiment, the non-conductive body 406 has a hemispherical shape with the conductive coating 404 formed on a planar surface 408 of the body. The hemispherical geometry of the electrode assembly 400 enhances the visual field of the surgeon by reducing the overall size of the electrode assembly as compared with spherical electrodes and the like.

FIG. 8B shows an alternate embodiment of an electrode assembly 400' having a cylindrical geometry with a conductive coating 404' disposed on a non-conductive body 406'. And FIG. 8C shows an electrode assembly 400" having a generally spherical shape with a conductive coating 404" covering a portion of a non-conductive body 406". In an exemplary embodiment, the coating ranges in thickness from about 0.001 inch to about 0.100 inch.

It is understood that the conductive coatings 400 are coupled to an electrosurgical RF generator 50 like that shown in FIG. 1 via conductors 308 like those shown in FIG. 7.

One of ordinary skill in the art will appreciate that the invention enables a monopolar electrosurgical tool (i.e., one that utilizes a remote ground pad to complete the electrical circuit) to be used in an environment that includes an isotonic fluid. Generally, monopolar electrosurgical devices deliver current to tissue in a non-focused manner such that the current is passed to target tissue as well as other non-target tissue in the vicinity of the electrode. As noted above, this can present a problem in closed surgical procedures that involve the use of a fluid medium. The tendency of conventional monopolar tools to dissipate current generally precludes their use in an isotonic fluid medium. However, the present invention, which permits the focused delivery of electrosurgical energy, with little or no current dissipation outside of target tissue, enables the use of a monopolar electrosurgical instrument in an isotonic fluid medium.



Generally, an isotonic fluid medium is understood to be one having an osmolarity in the range of about 260 or 295 milliosmols. Examples of suitable isotonic fluids are saline and Ringer's lactate.

5

The foregoing description of the illustrative embodiments of the invention is presented to indicate the range of constructions to which the invention applies. Variations in the physical architecture and dimensions of the invention will be apparent to those having ordinary skill in the art based upon the disclosure herein.

What is claimed is:

1. An electrosurgical device, comprising:  
a frame;  
an electrode coupled to the frame; and  
5 an insulative coating disposed on the electrode so as to form a coated portion  
and an exposed portion such that the exposed portion is effective to apply  
electrosurgical energy to tissue.
2. The device according to claim 1, wherein the electrode is channel-shaped.
3. The device according to claim 2, wherein the exposed portion of the electrode  
10 corresponds to a distal end of the electrode.
4. The device according to claim 3, wherein the distal end of the electrode  
includes an edge.
5. The device according to claim 3, wherein the exposed portion of the electrode  
further corresponds to a proximal end of the electrode.
- 15 6. The device according to claim 1, wherein the electrode comprises a surgical  
loop.
7. The device according to claim 6, wherein the exposed portion of the loop  
corresponds to an outer circumferential portion of the electrode.
8. The device according to claim 1, wherein the electrode is generally cylindrical.
- 20 9. The device according to claim 1, wherein the electrode is generally spherical.
10. The device according to claim 1, wherein the insulative coating comprises a  
material selected from the group consisting of ceramics, glass, aluminum-silicate,

alumina, boron, non-conductive epoxy, ceramic adhesive, glass enamels, glass-filled polymers, polysulfones, polytetrafluoroethylene, polysiloxanes, silicones, polyetheretherketone, Parylene, and Kevlar.

11. The device according to claim 1, wherein the insulative coating has a thickness  
5 in the range from about 2 microns to about 2500 microns.

12. The device according to claim 1, wherein the insulative coating is formed from alumina and has a thickness in the range from about 2 microns to about 150 microns.

13. An electrosurgical device, comprising:  
10       a frame having a proximal end and a distal end;  
          a coupling mechanism disposed at the distal end of the frame;  
          an electrode secured to the coupling mechanism such that the electrode is pivotable between first and second positions; and  
          an insulative coating disposed on a portion of the electrode.

14. The device according to claim 13, wherein the coupling mechanism includes a  
15 channel formed in the electrode.

15. The device according to claim 14, wherein the channel is effective to guide movement of the electrode with respect to the frame.

16. The device according to claim 14, wherein the channel is arcuate.

17. The device according to claim 13, wherein the electrode is biased to the first  
20 position.

18. The device according to claim 13, wherein pressure applied along a longitudinal axis of the frame causes the electrode to pivot to the second position.

19. The device according to claim 13, wherein the frame includes first and second structural members.

20. The device according to claim 18, wherein the electrode has a general shape selected from the group consisting of spherical, cylindrical, hemispherical, and hemi-cylindrical.

21. The device according to claim 13, wherein the insulative coating comprises a material selected from the group consisting of ceramics, glass, aluminum-silicate, alumina, boron, non-conductive epoxy, ceramic adhesive, glass enamels, glass-filled polymers, polysulfones, polytetrafluoroethylene, polysiloxanes, silicones, polyetheretherketone, Parylene, and Kevlar.

22. An electrosurgical device, comprising:

a frame having a distal end and a proximal end;

a non-conductive body coupled to the distal end of the frame; and

a tissue-contacting electrode formed by a conductive coating disposed on a portion of the non-conductive body, the conductive coating being adapted for coupling to an electrosurgical energy source.

23. The device according to claim 22, wherein the non-conductive body is loop-shaped.

24. The device according to claim 22, wherein the non-conductive body is generally spherical.

25. The device according to claim 22, wherein the non-conductive body is formed from a material selected from the group consisting of ceramics, glass, aluminum-silicate, alumina, boron, non-conductive epoxy, ceramic adhesive, glass enamels, glass-filled polymers, polysulfones, polytetrafluoroethylene, polysiloxanes, silicones, polyetheretherketone, Parylene, and Kevlar.

26. The device according to claim 22, wherein the conductive coating is formed from a metal selected from the group consisting of stainless steel, tungsten, titanium, platinum, silver, gold, brass and nickel-titanium alloys.

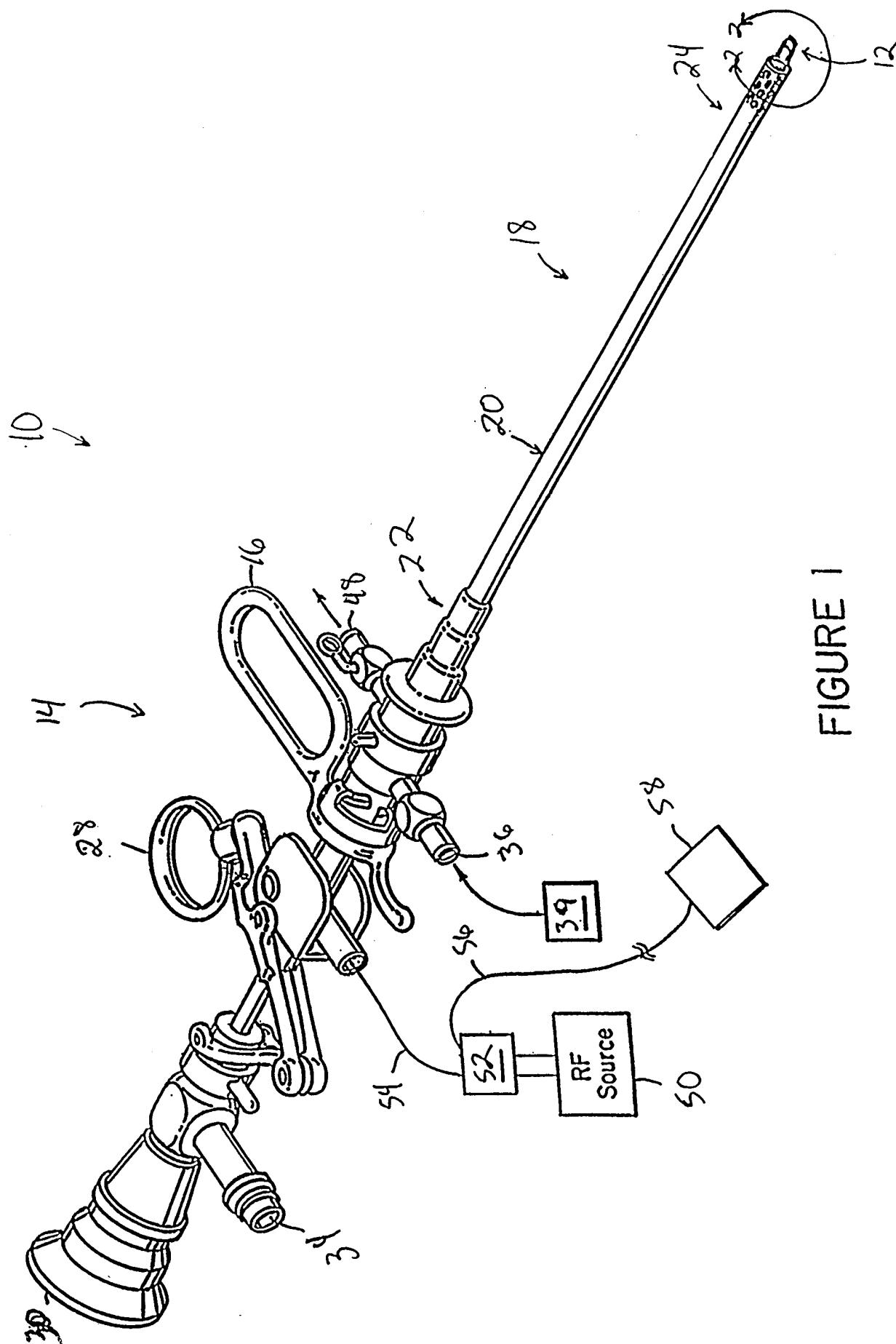
5 27. The device according to claim 22, wherein the non-conductive body has a generally hemispherical shape.

28. The device according to claim 27, wherein the conductive coating is disposed on a planar surface of the hemispherical non-conductive body.

10 29. The device according to claim 22, wherein the non-conductive body has a shape generally corresponding to a portion of a cylinder taken along a longitudinal axis thereof.

30. The device according to claim 29, wherein the conductive coating is disposed on a planar surface of the non-conductive body.

31. The device according to claim 22, wherein the conductive coating has a thickness in the range from about 0.001 inch to about 0.100 inch.



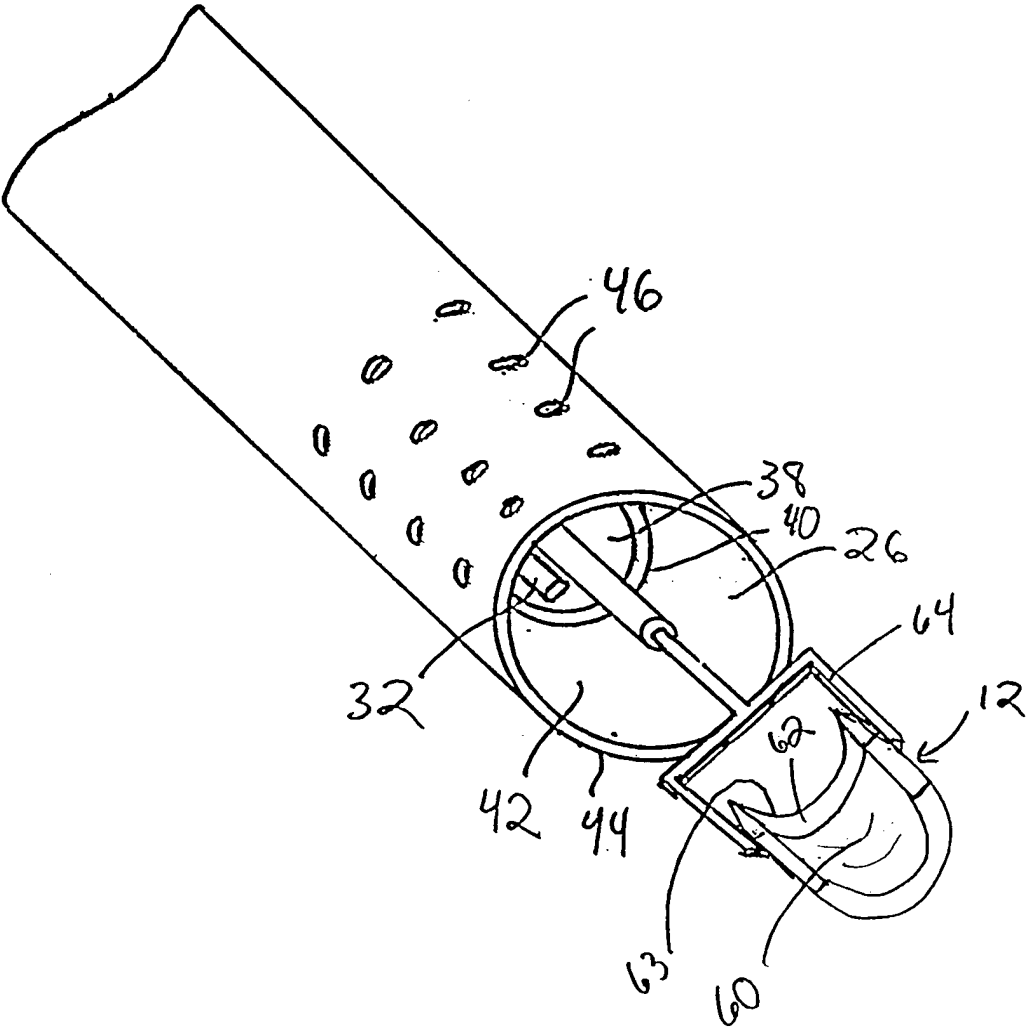


FIG. 2

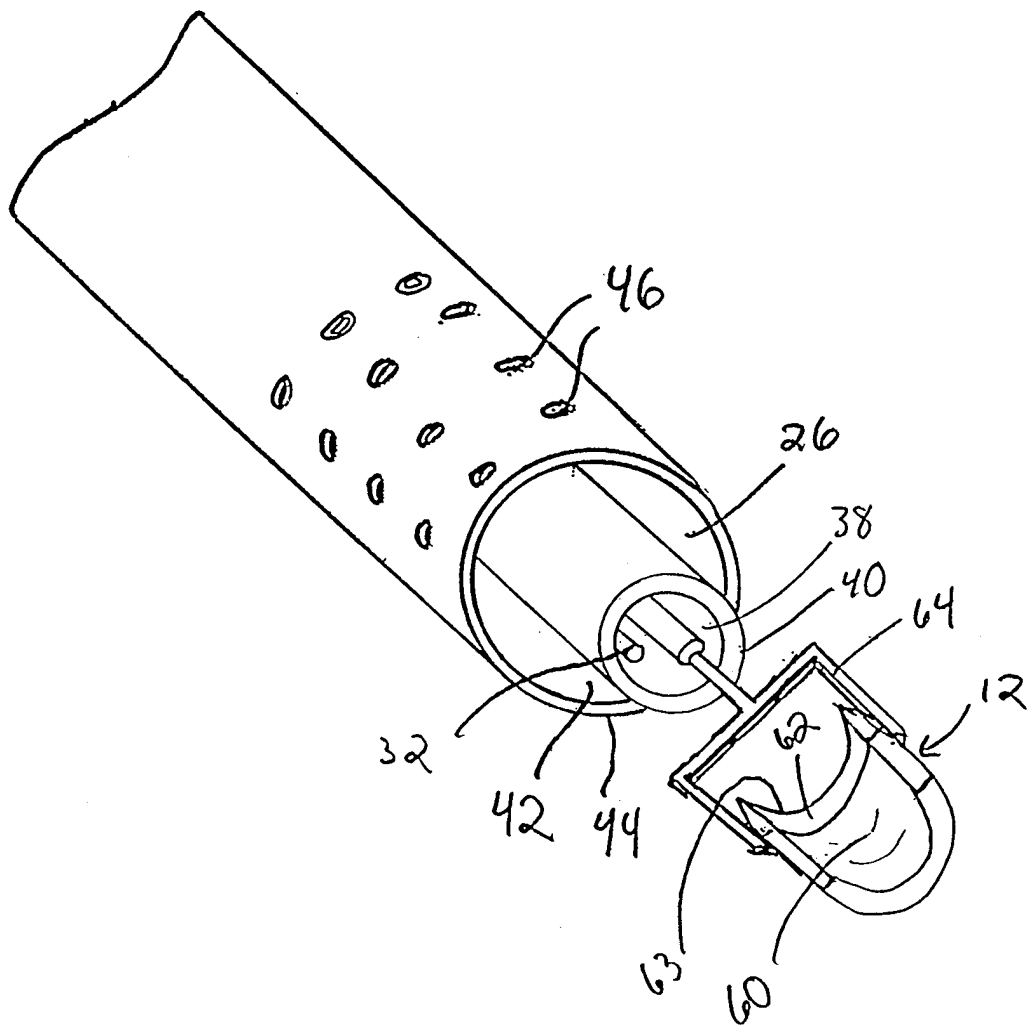
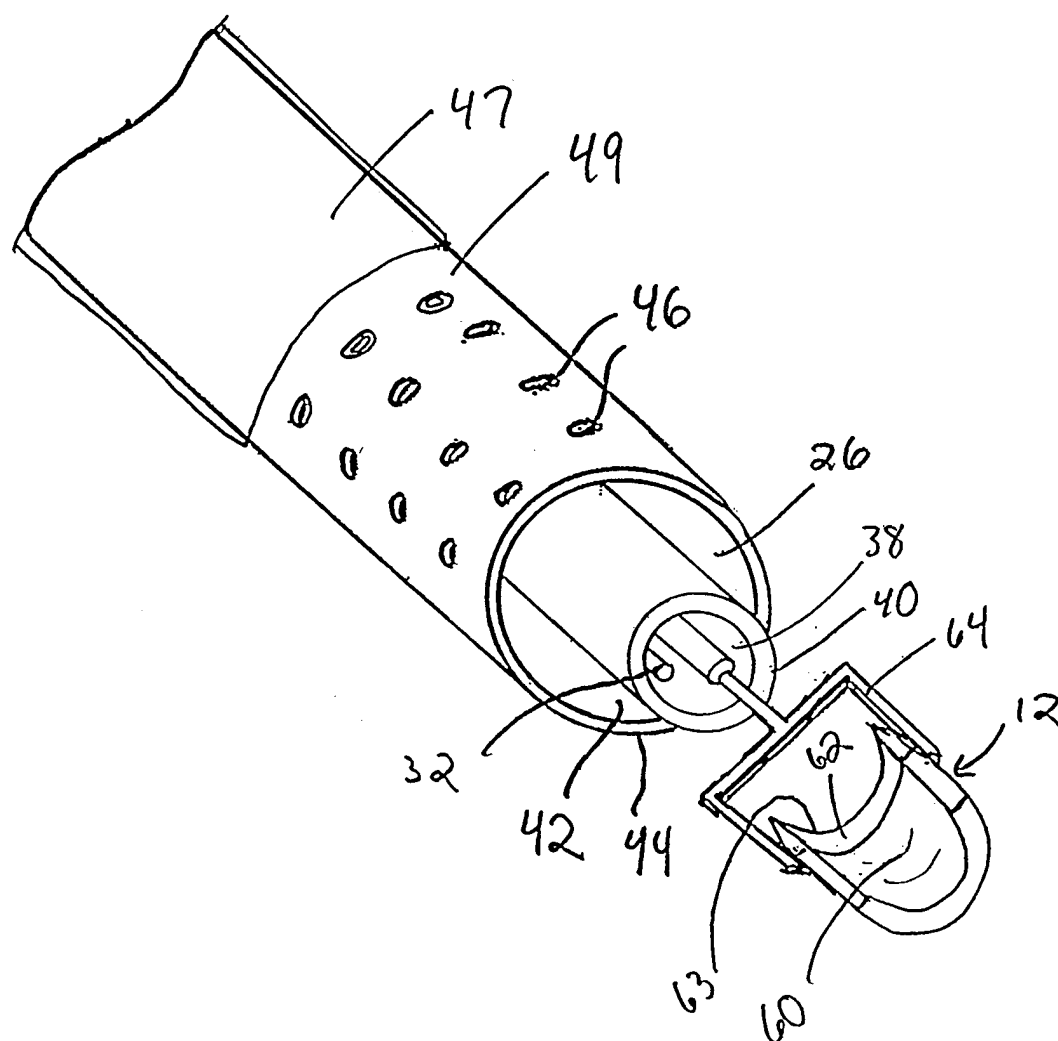


FIG. 2A





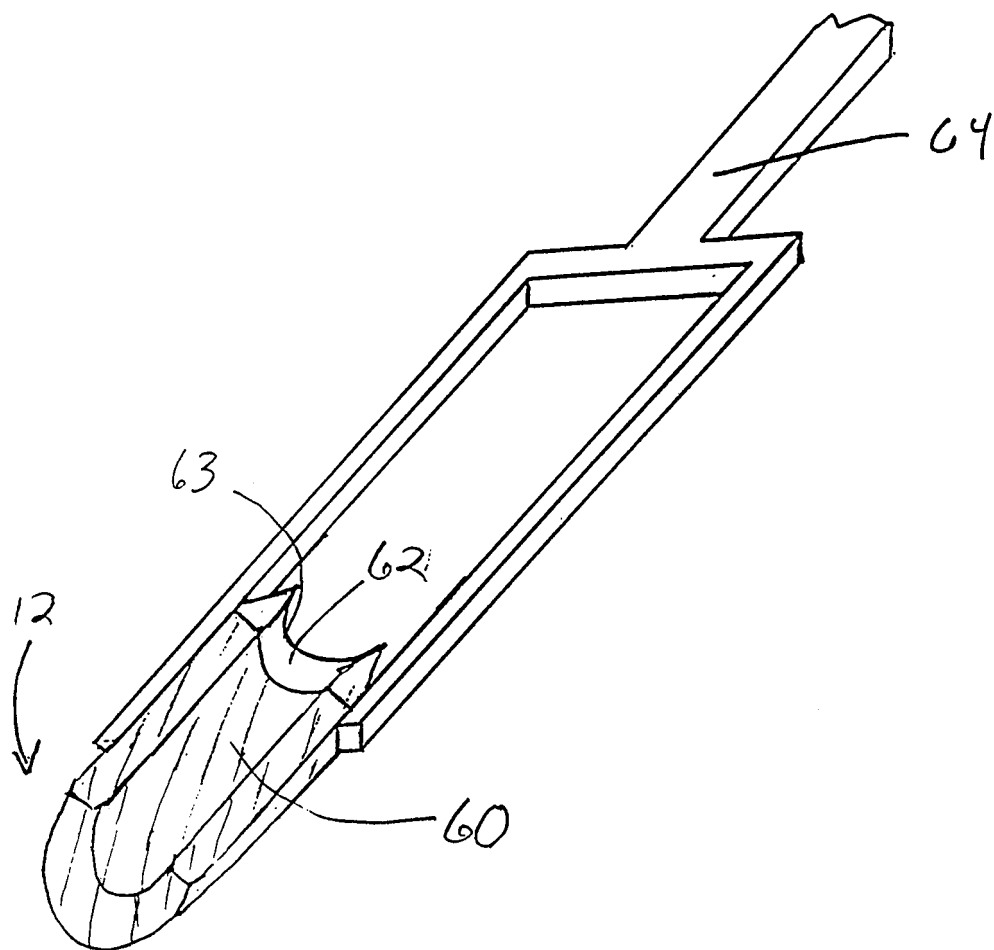


FIG. 3

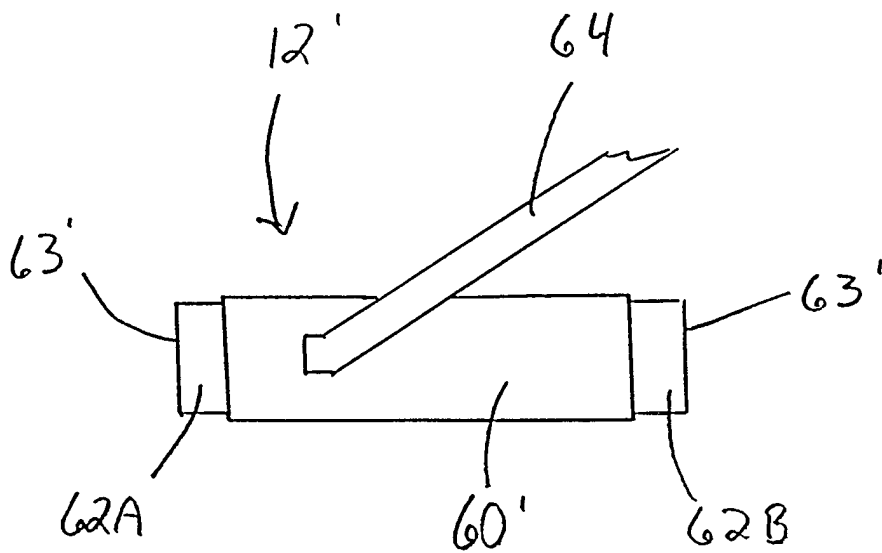


FIG. 3A

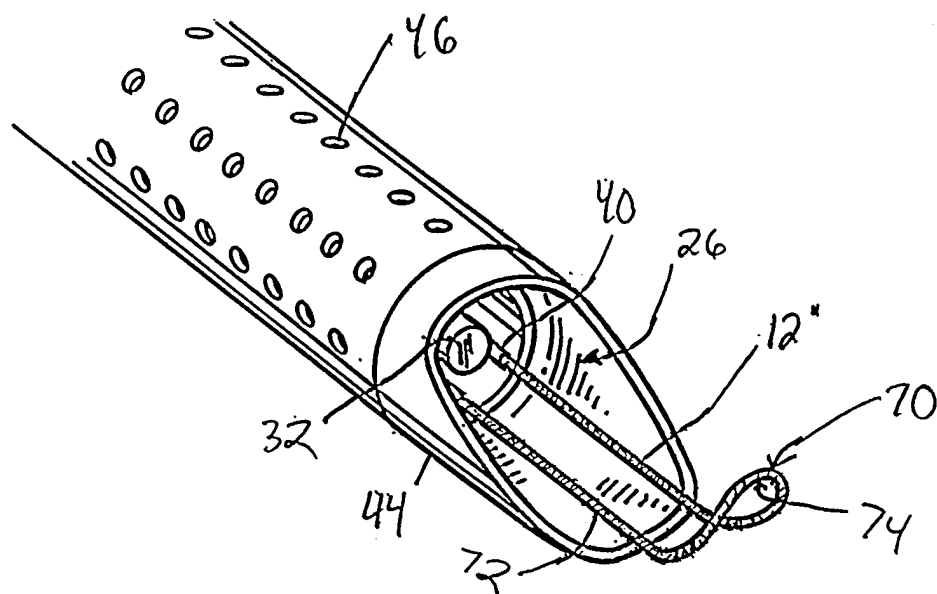


FIGURE 4A

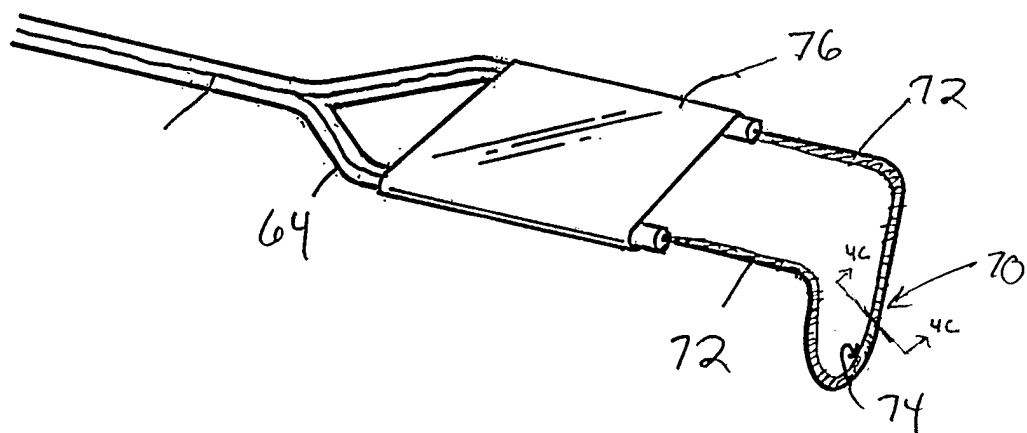


FIGURE 4B

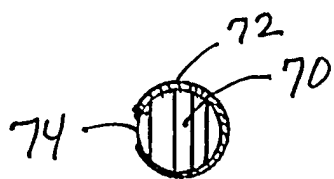
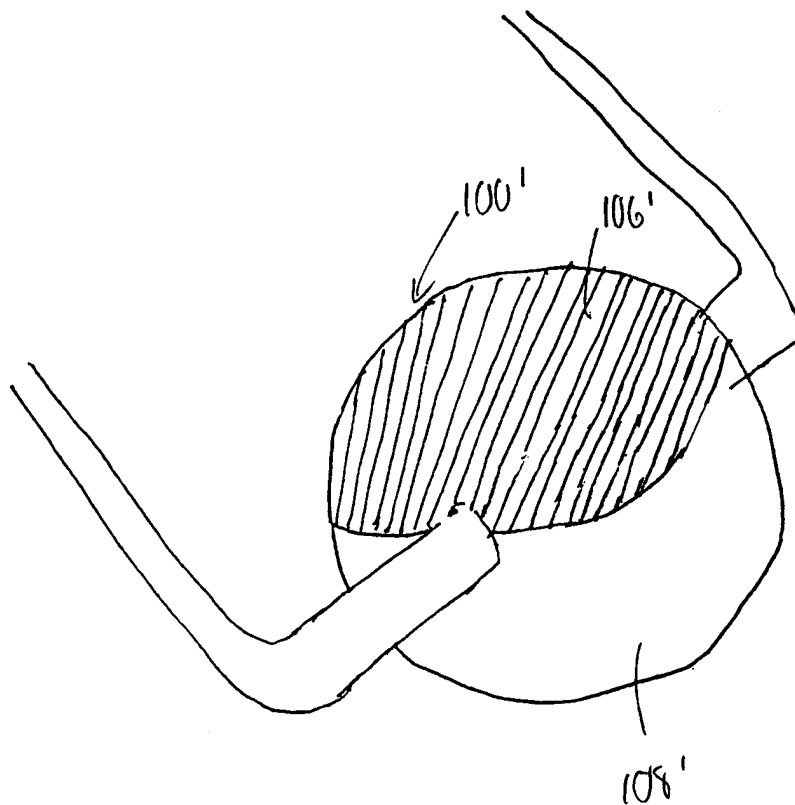
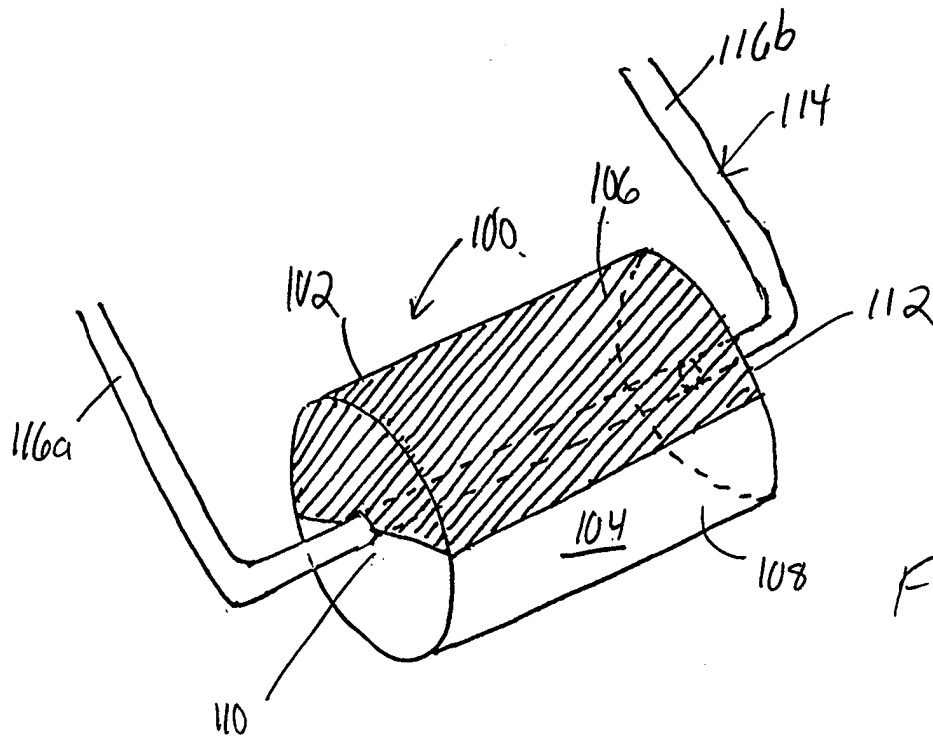
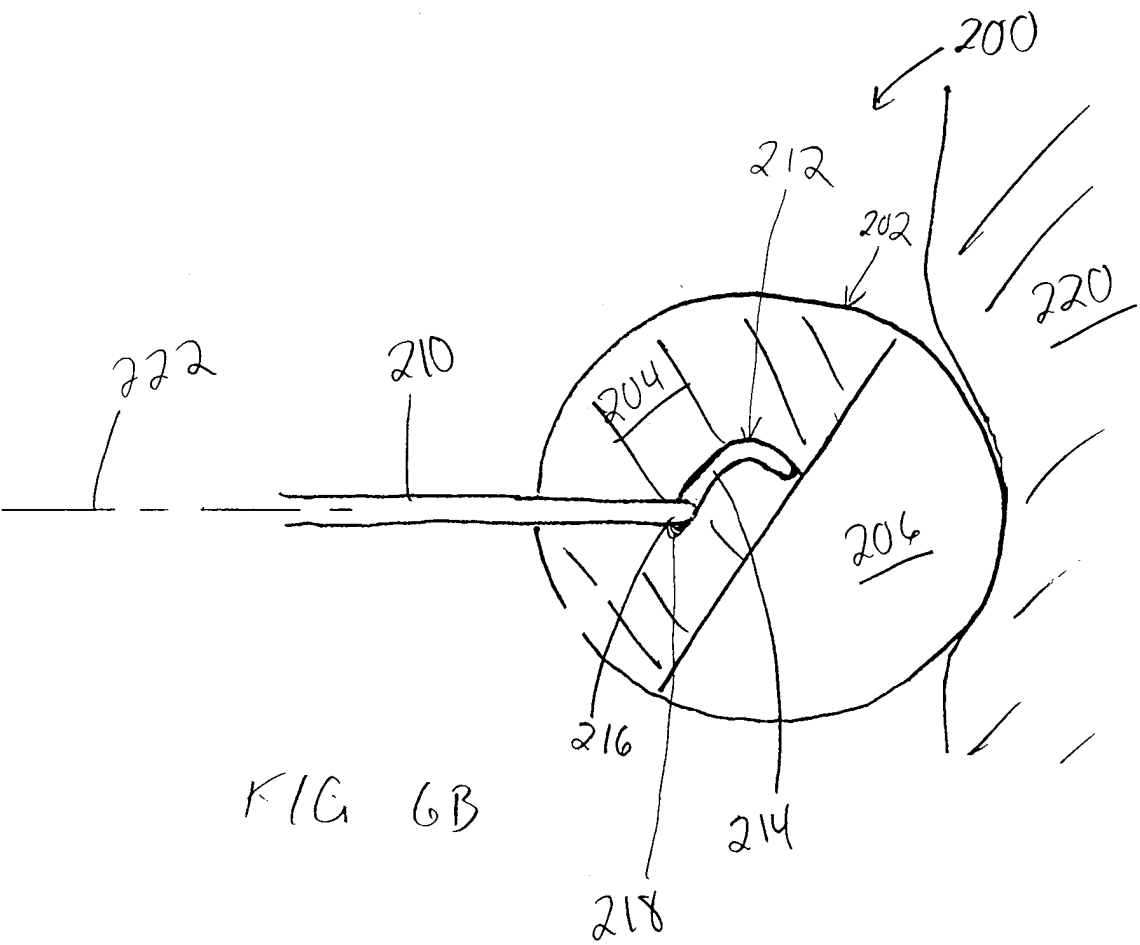
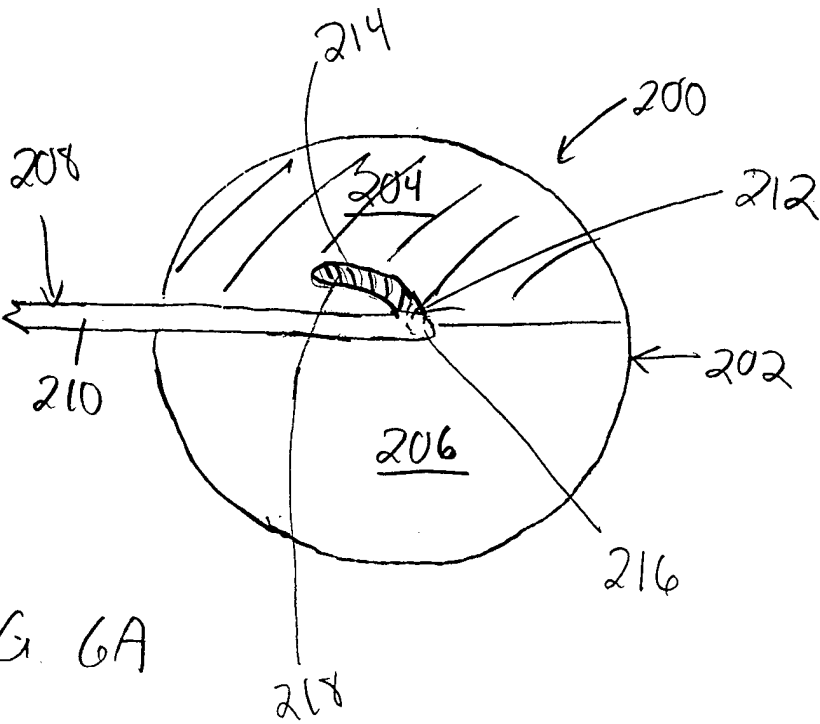


FIGURE 4C





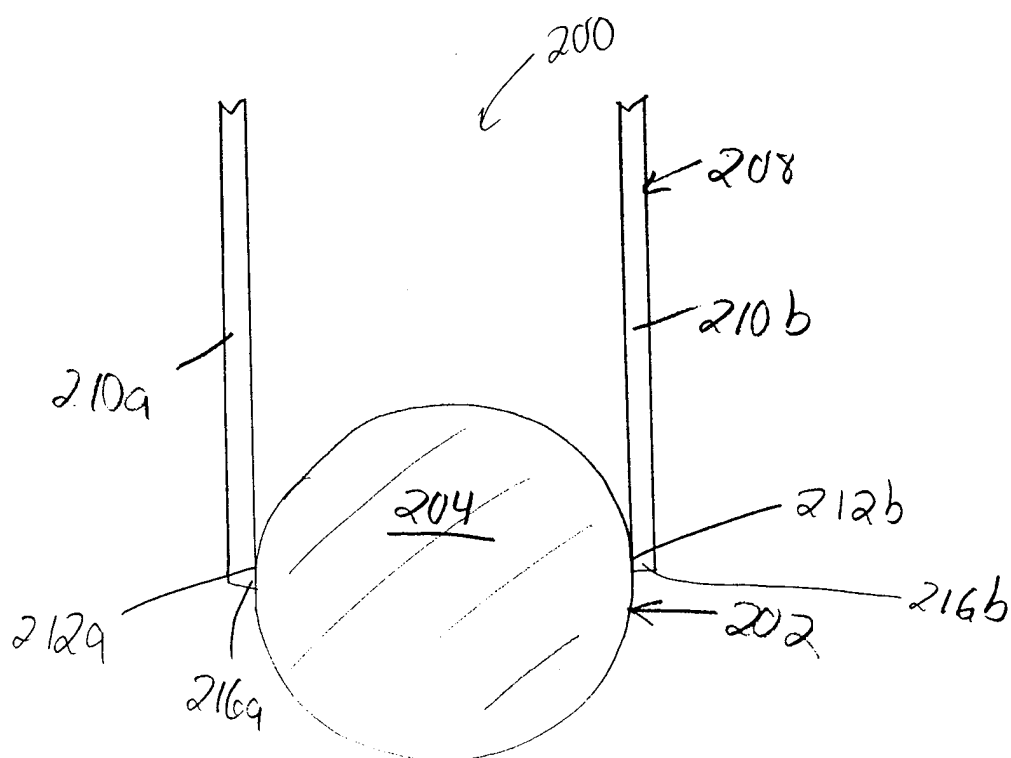


FIG 6C



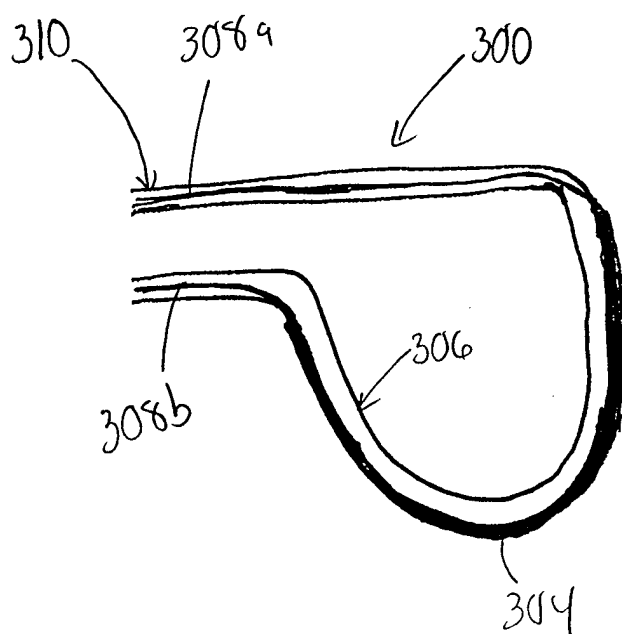


FIG 7

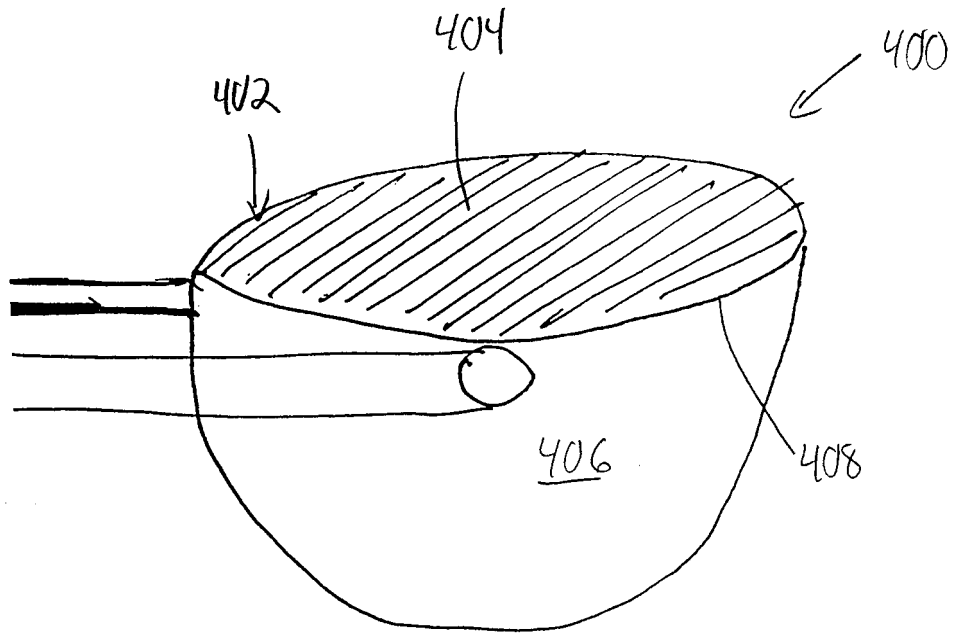


FIG. 8A

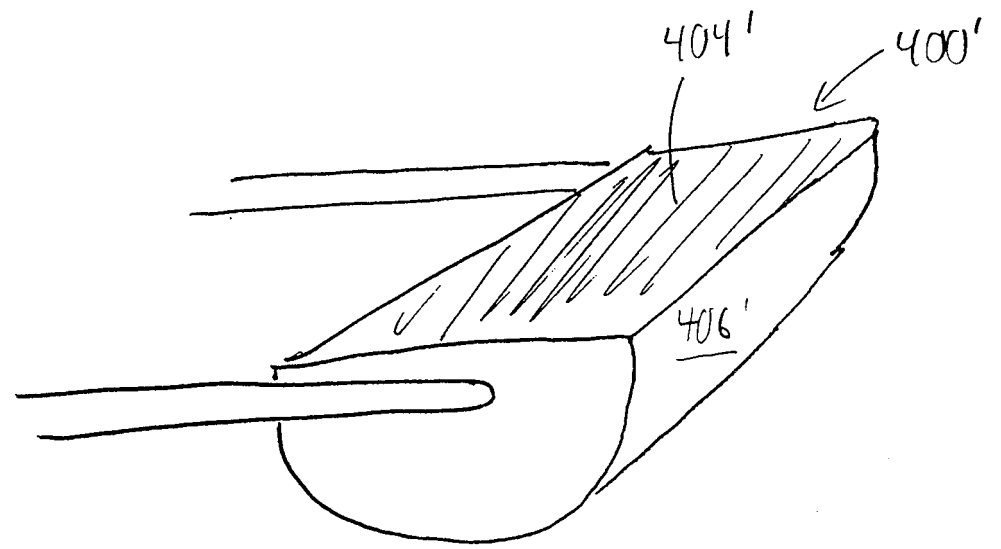


FIG. 8B

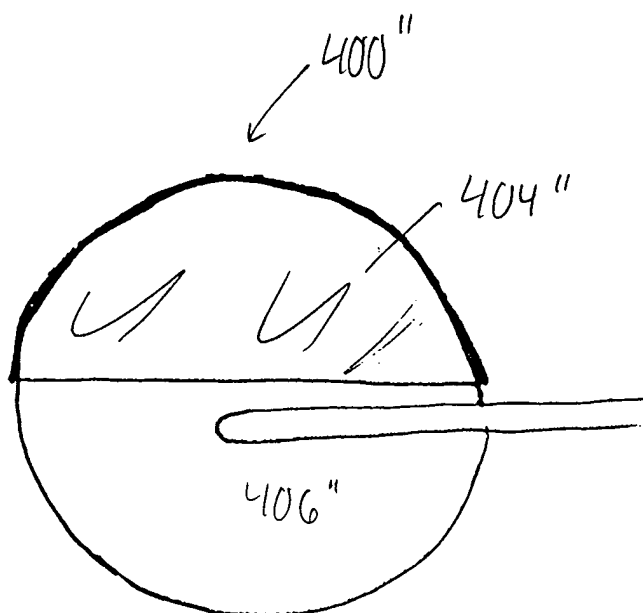


FIG 8C

# INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/11720

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :A61B 17/39

US CL :606/46

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 600/374; 606/41, 42, 45-52; 607/100-102; 600/374

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

NONE

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

NONE

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X --- Y	US 5,634,924 A (TURKEL et al) 03 June 1997, entire document.	1-5, 7, 8, 10, 13-15, 18-20, 22, 25, 26 ----- 6, 7, 9, 11, 21, 24, 31
X --- Y	US 5,395,363 A (BILLINGS et al) 07 March 1995, entire document.	1-5, 7, 13-15, 18-20 ----- 10-12, 21



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

28 JULY 1998

Date of mailing of the international search report

18 AUG 1998

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# INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/11720

## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X --- Y	US 4,532,924 A (AUTH et al) 06 August 1985, entire document.	22, 25, 26 ----- 31
X	US 5,462,545 A (WANG et al) 31 October 1995, entire document.	1-5, 7, 8, 10
X --- Y	US 5,396,900 A (SILATER et al) 14 March 1995, entire document.	13-15, 17-19 ----- 21