

[54] **PROCESS FOR THE PROCESSING OF CONTAMINATED BORIC ACID**

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[51] Int. Cl.⁵ **G21F 9/16; G21F 9/08; C09K 13/08; B08B 9/00**

[52] U.S. Cl. **252/628; 134/1; 134/3; 134/22.11; 134/22.16; 134/24; 134/27; 134/28; 204/1.5; 204/130; 204/140; 204/141.5; 252/79.3; 252/626; 252/631; 252/632; 423/2; 423/4; 423/18; 423/20**

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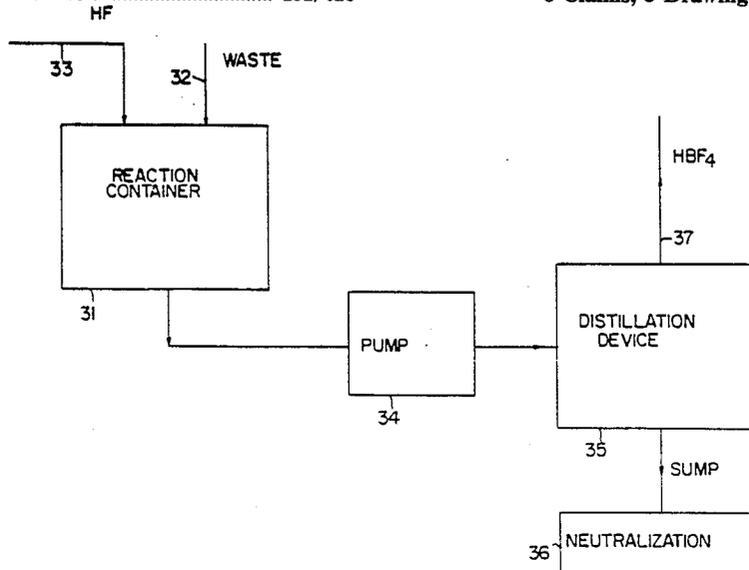
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Primary Examiner—Howard J. Locker
Attorney, Agent, or Firm—Thomas W. Speckman; Douglas H. Pauley

[57] **ABSTRACT**

Contaminated surface layers are decontaminated by treatment with an aqueous fluorine base-containing decontamination solution. The aqueous decontamination solution contains 0.05 to 50 Mol of decontamination agent per liter, and the decontamination agent preferably at least one substance from the group: hexafluorosilicate acid, fluoroboric acid, and the salts of both of these. The decontamination solution produces the required high decontamination factors on pressurized water reactors, boiling water reactors, metallic substances, high temperature alloys and brickworks as well. The used decontamination solution can, after regeneration, be recycled into the decontamination process. Release of decontaminated material by dissolution of the surface layer of the decontaminated objects provides decontamination of objects having complicated and hard-to-measure geometries. The decontamination agent (NBF₄-acid) is advantageously produced from contaminated boric acid from pressurized water reactor wastes by reaction with fluoride or hydrofluoric acid. The HBF₄-acid thus produced is, through distillation, separated from the contaminants and impurities.

8 Claims, 3 Drawing Sheets



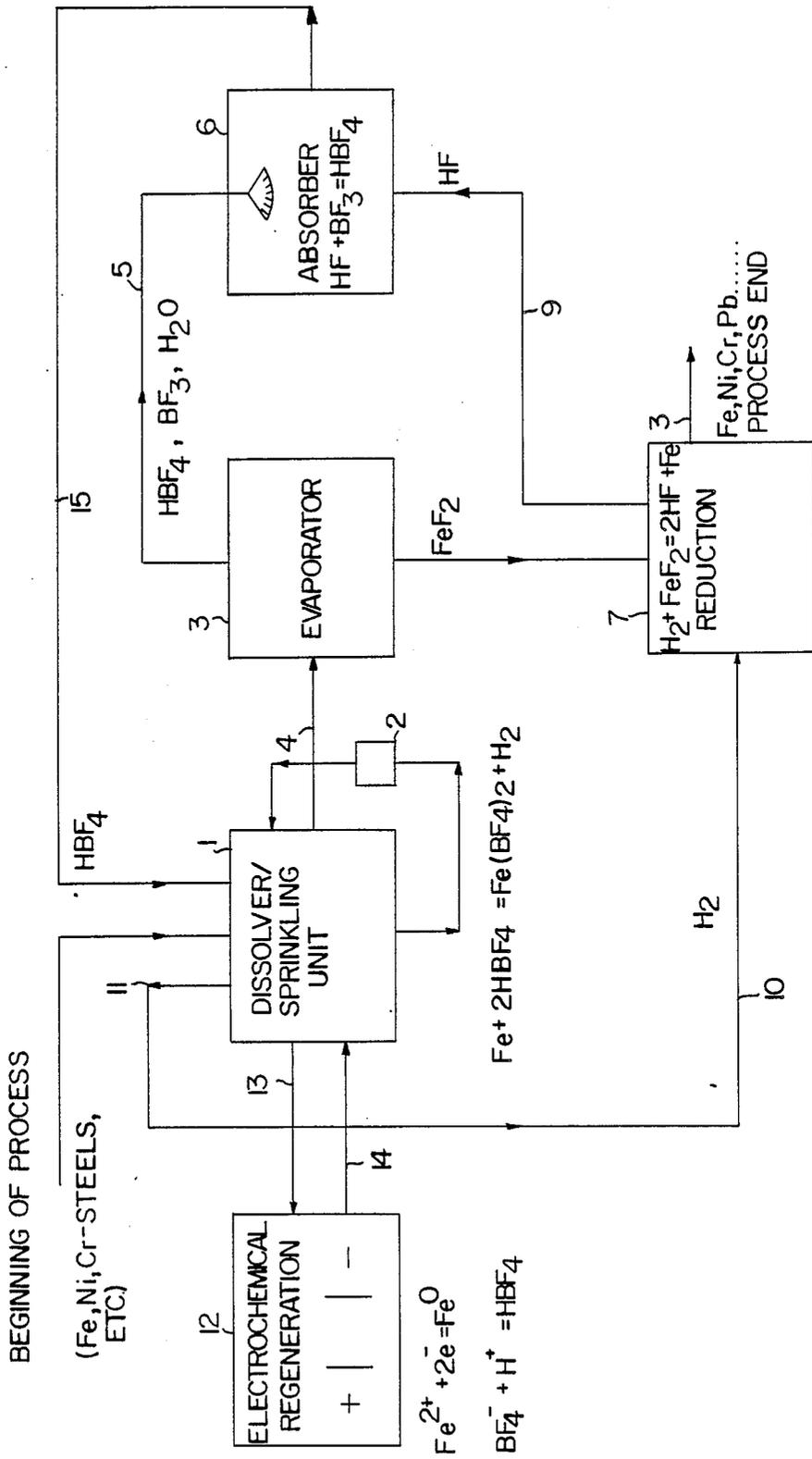


FIG. 1

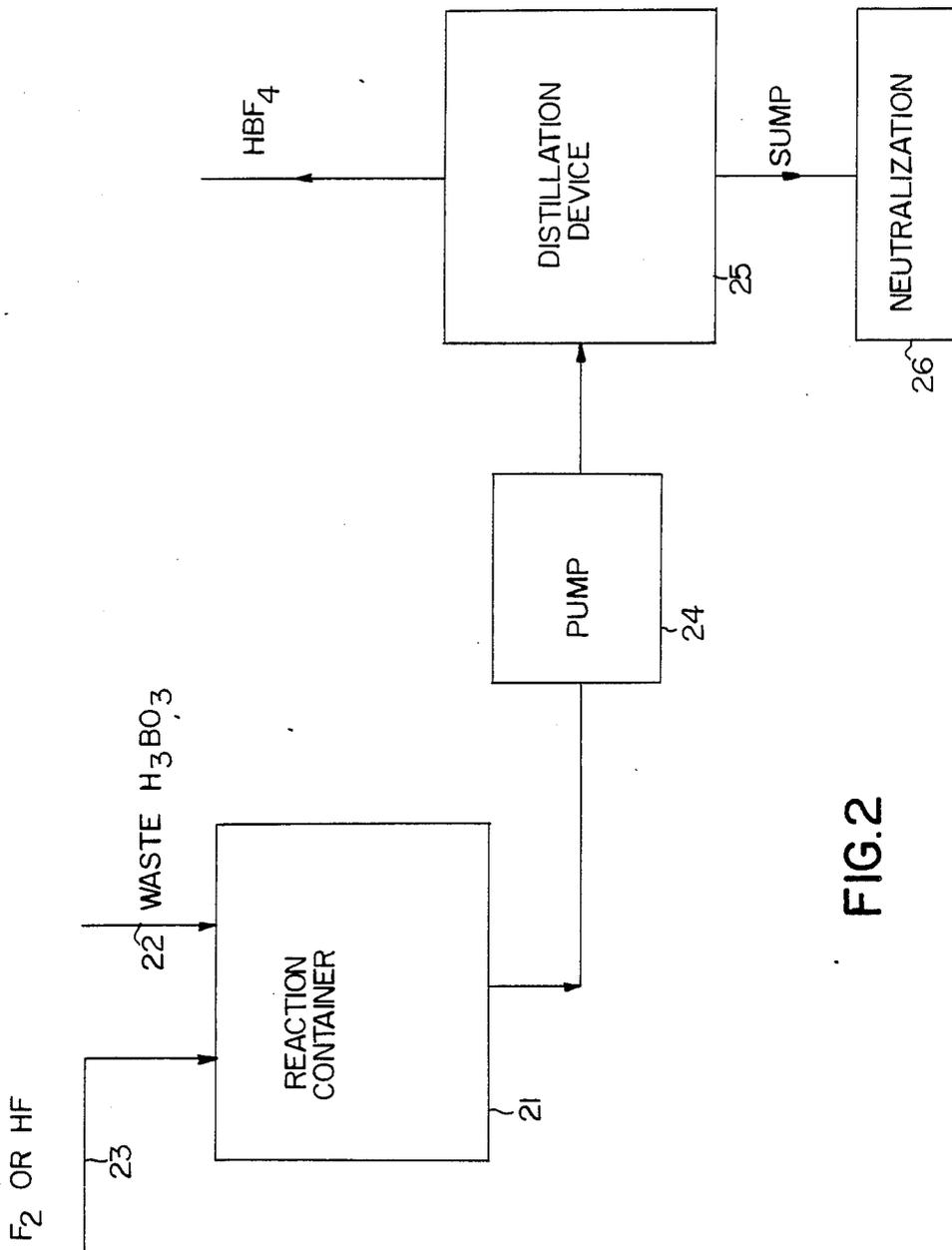


FIG.2

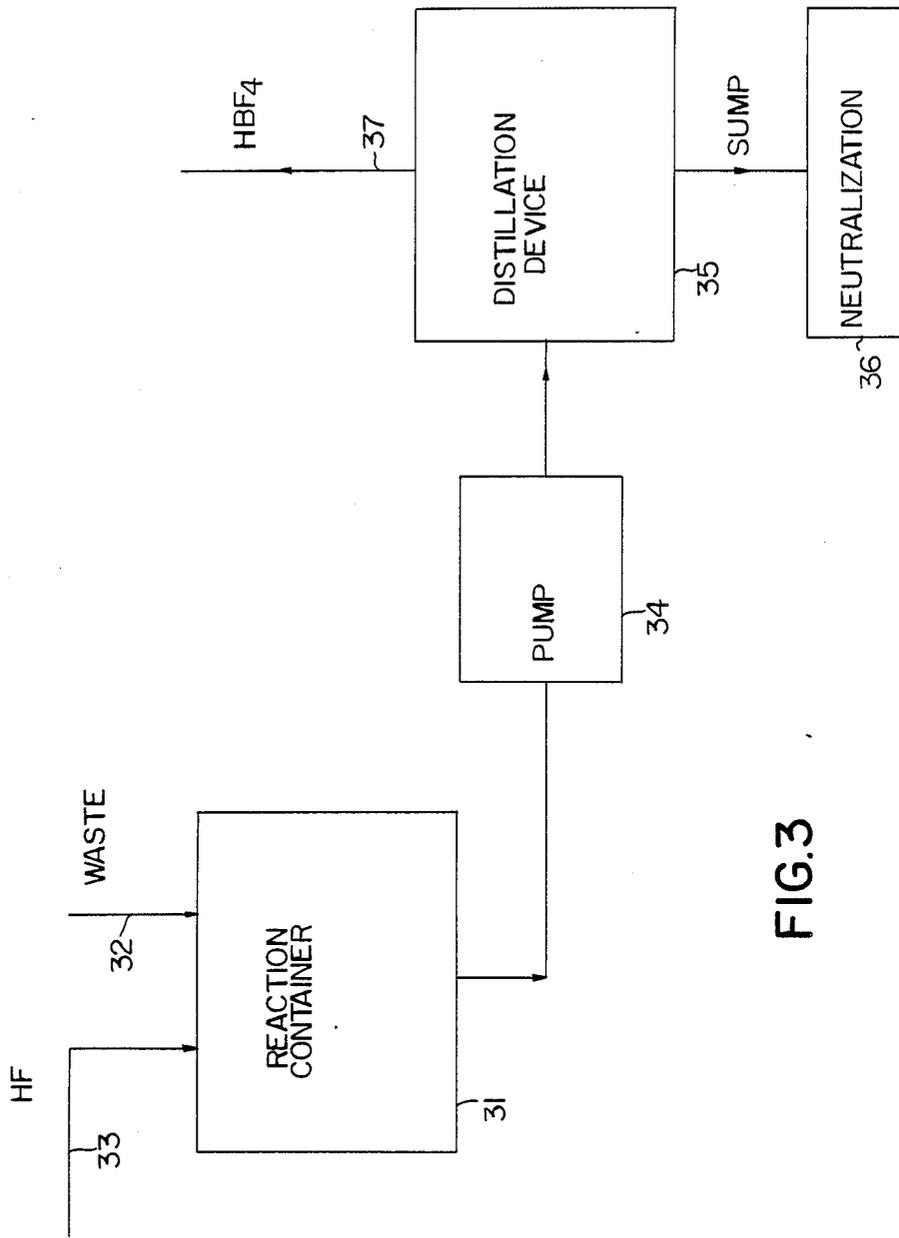


FIG.3

PROCESS FOR THE PROCESSING OF CONTAMINATED BORIC ACID

CROSS REFERENCE TO RELATED APPLICATIONS

This is a continuation-in-part patent application of my earlier application, Ser. No. 019,799, filed May 27, 1986, now U.S. Pat. No. 4,828,759.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention concerns an agent for decontaminating contaminated metallic or cement-containing substances. The invention also concerns, however, a process for the production of this decontamination agent by using boric acid, which is contained in the primary cycles of pressure water reactors. The invention further concerns processes for using the decontamination agent. Although the decontamination agent in accordance with the invention is not restricted to the use of radioactively contaminated materials, the primary emphasis in the following description will be laid on this application.

2. Description of the Prior Art

In the past, the contaminated surface layers of reactor cooling conduits were frequently removed by means of aqueous mineral acid solutions. One such decontamination solution, with 20% nitric acid and 3% hydrofluoric acid, is cited, for example, in "Kernenergie", 11th year, 1968, page 285. Since, because of the aggressive nature of such mineral acid solutions, the removal process can only be controlled with great difficulty, there exists the danger that the pure metal below the contaminated surface layer will be corroded, so that weak points may arise, which may lead to the formation of leaks—which must in all cases be avoided. Of all the decontamination processes later developed in order to remove such or similar defects, the best known one must be the so-called "AP-Citrox" process ("Kernenergie", 11th year, 1988, page 285), in which the contaminated surface is first treated with an oxidizing alkaline permanganate solution to prepare for dissolution, and is then treated with a reducing, aqueous solution of dibasic ammonium citrate.

In U.S. Pat. No. 3,873,362, a similar two-stage decontamination process is described, in which, during the first stage, hydrogen peroxide is preferably used for oxidation, and, during the reducing, second process state, aqueous solutions of mixtures of mineral acids (sulfuric acid and/or nitric acid) and complex-forming substances, such as oxalic acid, citronellic acid, or formic acid, are employed.

In accordance with another known decontamination process taught in German Patent DE-PS No. 27 14 245, the contaminated metallic surface is treated with a cerous solution containing at least one cerium-IV-salt and a water-bearing solvent. A further decontamination process is described in European Patent Application, publication No. 00 73 366, in which an aqueous solution of formic acid and/or acetic acid is used as a decontamination agent, and, as a reducing agent, formaldehyde and/or acetaldehyde is used. In this process, it is particularly advantageous that a relatively slight need for chemicals exists, and, during the removal of the used decontamination solution, a quantity of precipitated

radioactive substances corresponding approximately to the volume of the surface layers removed is used.

In the wet chemical decontamination processes which have been briefly described above, the basic concept is connected with the fact that the activity in the contaminated surface layer decreases with mass, as the surface layer itself is dissolved by the decontamination solution. The penetration depth of active material into the surface layer can be determined or measured before decontamination.

Decontamination tests on various metallic reactor components have only one conflict with the statement above, that the amount of residual activity is solely a function of the thickness of the surface layer removed. For various decontamination solutions, there are provided various decontamination factors with the same gravimetrically determined abrasion of layers. Research with a scanning electron microscope has shown that solid layers or islands of solids have formed on the decontaminated metal surfaces, in which active material is concentrated, and which are considered undesirable by-products of the specific abrasive reactions. Such variations are particularly observed in substances which contain silicon or aluminum, and thus in stainless steels and high-temperature materials, such as, for example, are used in helium-cooled high temperature reactors, and even in slightly alloyed steels. Apart from an undesirably high residual activity, the monitoring and control of the decontamination process is, because of the irregular removal of such surface layers, difficult, so that reliable decontamination is no longer ensured, and the previously stated corrosion damage has to be taken into account.

In the primary water cycle of pressurized water reactors, boric acid is found in concentrations of up to 3000 ppm. During the operation of such reactors, small quantities of the stated fluid precipitate as waste. This waste contains, in addition to boric acid, further contaminants, such as, for example, cobalt compounds, as well as solid contaminants, such as, for example, rust residues, materials fibers, dust, and the like. This waste can, in certain cases, be treated to such an extent that it is present in the form of a solid material.

The waste was previously generally concentrated to approximately 16 weight percent by means of evaporation, so that this concentrate then had an activity of 0.1 to 3 Ci/m³, and up to 1 g/l of solids (28,000 ppm boron). Such a concentrate may be solidified with cement (see also, for example, Nagra: Nationale Genossenschaft zur Lagerung radioaktiver Abfalle Technical Report, (84-09). A quantity of 123 kg concentrate solution/200 liter matrix, with a volumetric weight of 1.89 Mg/m³, that is, 123 kg (=114 liters with a density of 1.08 Mg/m³) is solidified in a matrix weighing 378 kg. The quantities of concentrate can amount to up to 10 m³ per nuclear plant per year. To remove this amount of concentrate, approximately 88 vessels were required, according to the above assumptions, whereby the volume of each vessel amounted to about 200 liters. With a price of 5,000.00 Swiss francs per vessel, including removal, the sum of 440,000.00 Swiss francs for the removal of the annually precipitating quantity of waste results.

SUMMARY OF THE INVENTION

It is the object of the present invention to propose a decontamination agent which is more economical than the previously known agent, can be obtained by using boric acid from pressurized water reactors, and permits

a versatile application. A decontamination agent comprising a fluoroboric acid provides improved decontamination of contaminated metallic and cement-containing materials. Fluoroboric acid decontamination agent may be produced from the reaction of boric acid products from pressurized water reactors with fluorine or hydrofluoric acid. Decontamination of contaminated metallic and cement containing materials may then be achieved by contact with the fluoroboric acid decontamination agent, with subsequent separation of the decontamination agent from the contaminants and solid impurities.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows a flow diagram for producing a decontamination agent according to one embodiment of this invention;

FIG. 2 shows a flow diagram for transforming contaminated boric acid into an evaporable boron compound according to one embodiment of this invention; and

FIG. 3 shows a flow diagram for processing contaminated boric acid from pressurized water reactors.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The device for carrying out the present process, as shown in FIG. 1, has a container for receiving the objects to be decontaminated. The length of treatment of objects in dissolving unit (1) is so selected that the objects, after the termination of the process, are free from radioactivity. The decontaminated objects are then removed from (1), and can then either be reused, or discarded with other scrap.

A decontamination solution is introduced into dissolving unit (1), which solution works on the surfaces of the objects in such a manner that the contaminated surface layer is dissolved and abraded. The decontamination solution in dissolving unit (1) may be a bath, in which the objects may be immersed, or the decontamination solution may be sprayed into dissolving unit (1).

A circulating device (2) with a pump may be provided in communication with dissolving unit (1). This makes it possible to provide a long treatment period for the objects, with a relatively small quantity of decontamination solution. An evaporating unit (3) is connected to the dissolving unit (1) by means of a conduit (4). Within the evaporating unit (3), more volatile components of a concentrated solution are separated from less volatile components of the same. Vaporizable components are conducted to an absorber unit (6) by means of a further conduit (5). The sump products from the evaporating unit (3) may be introduced into a reduction device (7), in which they are reduced to metallic iron, chromium, nickel, lead, and the like. There also exists, however, the possibility of conducting the solid, steamed products without reduction of the same for reutilization as chemical, metallic compounds in the chemical industry, or discarding the same as scrap. The reduction device (7) is, by means of a conduit (9), connected to the absorber unit (6), through which HF is conducted from the reduction device (7) to the absorber unit (6). The hydrogen necessary for the reduction of metal compounds can be conducted from the dissolving unit (1) to the reduction device (7), through a conduit (10).

An electrolytic cell (12) can be connected with the dissolving unit (1) by means of a conduit (13), through which the concentrated solution is circulated from the

dissolving unit (1) into the electrolytic cell (12). During the operation of this electrolytic cell (12) BF_4^- ions are reacted at the anode to form HBF_4 . HBF_4 is conducted to dissolving unit (1) through a further conduit (14).

Inside the previously described absorber unit (6), there likewise arises HBF_4 , which is conducted to dissolving unit (1) through conduit (15). The quality of the surface of the treated objects can be influenced during and/or after the decontamination process by means of surface-active substances. As examples of such substances, we might cite, for example, soaps, water permeability inhibitors, such as formaldehyde, and the like.

The great superiority of the process described here relative to the state of the art processes concerns the nearly universal applicability of the process, the extraordinarily great reception capacity of HBF_4 for the materials treated, and the total regenerability of the decontamination solution, so that an extraordinarily small quantity of secondary yields arises.

Decontamination Effects (Table 1)

Experiments were carried out with materials from the primary circuit of boiling water reactors and with steam-producing material from a pressurized water reactor with a stronger magnetic layer. The materials had activities of approximately $10\mu\text{Ci}/\text{cm}^2$ Cobalt-60.

TABLE 1

| Material | Decontamination factors (-) | |
|---|-----------------------------|------------------------------------|
| BWR Boiling water reactor Primary circuit Stainless Steel (from KWL) | 3 h, 80° C. Df = 100 | 2.5 h, 110° C. Up to free limit |
| PWR Pressurized water reactor Steam producer/Inconel 600 (Ni-base alloy) | 2 h, 80° C. Df ~ 40 | 45 Min., 100° C. Df ~ 30 |

Corrosion Behavior (Table 2)

The abrasion kinetics of stainless steel and nickel-based alloys were investigated at 80°, 90° and 100° C.

TABLE 2

| Temperature | Abrasion Kinetics in the DECOHA Process | |
|--------------------|---|---------|
| | Micrometer/h | |
| | 80° C. | 100° C. |
| Stainless steel | 5-6 | ~30 |
| Low-alloyed steel | ~50 | >100 |
| Nickel-base alloys | 3-4 | ca. 15 |

At the beginning of the process, dissolver unit (1) is provided, in which the objects to be decontaminated are, for the purpose of free decontamination or for free measurements, either first placed in bath or sprayed by means of a spraying process. The second part of the process consists of evaporation in an evaporating unit (3). In the evaporating unit (3), concentrated solutions, with approximately 200 grams of stainless steel per liter, are, at high temperatures, concentrated at normal or lowered pressure, and then dried to solid FeF_2 or analogous fluorides of other metals.

BF_3 , $\text{B}_2\text{O}_3 \cdot \text{BF}_3$, HBF_4 , H_2O and dehydrates of the boric acid are evaporated, suctioned off, and, in the next part of the device, the absorber unit (6), dissolved in the fluids phase. In the absorber unit (6), the solution obtained is displaced with hydrofluoric acid or with hydrofluoric acid steams, to produce fresh HBF_4 -acid, which is conducted to the dissolver unit (1). The sump

products from the evaporating unit (3) are conveyed to the reduction device (7), in which they can be reduced to metallic iron, chromium, or nickel (among others). Depending on whether free decontamination or free measurement is involved, we may obtain either inactive products from the evaporating unit (3) or from the reduction device (7), or else active, solid products, which are conducted to the removal area. The decontamination solution used for the decontamination process may be tested by means such as pH testing, and/or colorimetric testing, and/or density testing, and/or radioactivity testing to determine the composition of the decontamination solution. Depending on the removal infrastructure which is present, several removal options may be provided:

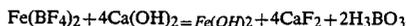
- (a) The direct removal of the decontamination agent from the dissolver unit (1);
- (b) The removal of fluorides, in an evaporated form;
- (c) The removal of metallic components after reduction steps;
- (d) Or combinations of the above.

Instead of immersing objects to be decontaminated in a decontamination bath and carrying out decontamination processes over the course of several hours, or even repeatedly, it is enough to sprinkle the contaminated objects at high temperature with a shower-like device. This treatment is effective regardless of the geometry of the objects involved. Each object can be packed in a plastic casing, which serves as the container for the device. By collecting the fluid flowing off in the lowest area, the same decontamination agent can be used again by means of the circulating device (2) with the pump (2) in the cycle. The minimal quantity of decontamination agent, which is necessary for the maintenance of the cycle and the wetting of the system, is determined by the wetting properties of the decontamination agent and the properties of the material surfaces. From practical experience, values of between 0.5 to 1.5 liters per m² of the area treated have been demonstrated. The high absorption capacity of the decontamination agent or decontamination solution (1 liter can, at 90° C., dissolve up to 220 grams of stainless steel), permits very flatly constructed decontamination lines. Such a high absorption capacity permits, with only 1 liter of decontamination solution and an abrasion level of 1 micrometer, approximately 30 m² of the surface to be decontaminated. Inside the dissolver unit (1), a concentration of up to 220 grams of stainless steel per liter can be attained at 90° C. This concentrated solution is circulated in the electrolytic cell (12), where metal is separated at the cathode, while, on the anode, BF₄-ions recombine into

HBF₄, and this is again conducted to the decontamination process.

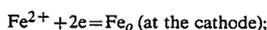
Removal of Secondary Wastes

As an example, an iron-containing Fe(BF₄)₂ concentrate will be discussed. This concentrate also contains radioactivity, which does not, however, influence the chemical balance. Dissolved stainless steel, nickel-base alloys and other contaminated materials are to be treated analogously. The following equation can be used for the direct removal of iron concentrates:



Removal in Accordance with Electrochemical Regeneration (Minimal Variants)

Iron, chromium, nickel, or copper may be electrolytically removed from the iron-containing concentrate, and then mixed with cement. The electrolysis proceeds in accordance with the following:



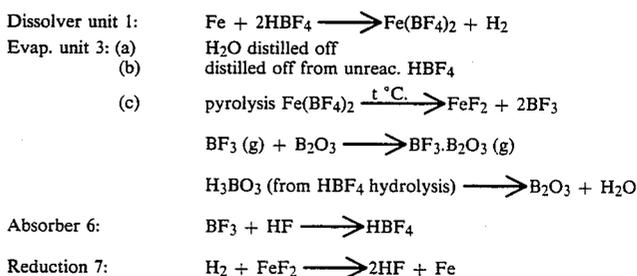
The reactions for other metals from decontaminated alloys proceed analogously. It is advantageous to use as an anode a corrosion-resistant material, such as, for example, graphite, or to use as a sacrifice anode the contaminated object itself, which accelerates the chemical dissolution and simultaneously regenerates the acid.

Removal Variations in Accordance with the Desiccation of HBF₄-Acid

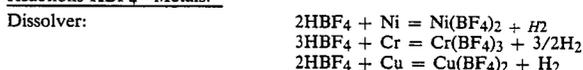
At normal pressure, at temperatures of up to 170° C., or at reduced steam pressure and lower temperatures, in accordance with the desiccation process, solid, reddish residue of FeF₂ with activity is attained. The residue yields, after the mixture with water and Ca(OH)₂, CaF₂ + Fe(OH)₂. These solid products are compatible with cement, and the weight of the cement matrix can be determined in accordance with the following formula: the number of grams of dissolved iron in the concentrate multiplied by 12.5 = the weight of the cement matrix in grams. The distillate contains vapors of HBF₄, BF₃, H₂O, boric acid, and hydrates of the same. After the condensation and collection of the vapors in the water, the desired concentration of HBF₄ can be adjusted by adding HF.

Reactions

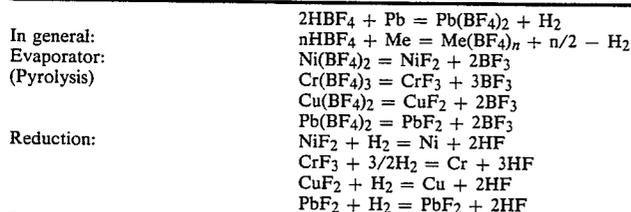
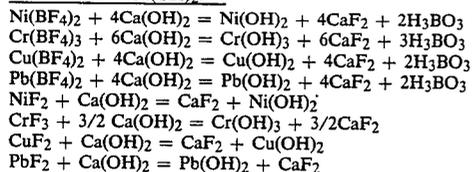
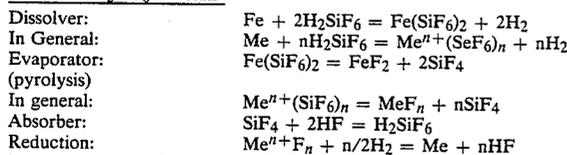
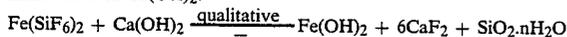
Reactions:



Reactions HBF₄ - Metals:



-continued

Removal with Ca(OH)₂:Reactions H₂SiF₆ - MetalsRemoval with Ca(OH)₂:In general: $\text{Me}(\text{SiF}_6)_n + \text{Ca}(\text{OH})_2 = \text{Me}(\text{OH})_n + \text{CaF}_2 + \text{SiO}_2 \cdot \text{H}_2\text{O}$ Reactions HF - Metals yield fluorides, the removal of which with Ca(OH)₂ has already been discussed in outline form.

Decontamination of Brickwork and Cement-Containing Surfaces

In the decontamination of porous materials, the activity is transported into the material through the mobile, fluid phase, which makes wet decontamination either more difficult or even impossible. A mechanical removal of the contaminated layer must therefore be carried out. This process is expensive, deforms the surface, and causes many secondary defects.

It is the objective of the present invention to remove the stated disadvantages of the prior art process, as well as additional ones not discussed, in the area of decontamination. This task is achieved by a decontamination agent comprising fluoroboric acid.

Example of Application and Mechanism

The brickwork surface is misted/moistened with HBF₄-and/or H₂SiF₆-acid. Through the chemical reaction between the carbonates in the brickwork and the acids, gaseous CO₂ arises. The gas bubbles form a foam with the acid, which is an outstanding flotation agent for the contaminants. The foam is subsequently suctioned off. Fluorine ions from the fluoro-complexes of the acids react with the calcium which is present, and form an insoluble, voluminous precipitate of CaF₂, which plugs the pores present on the surface. Through the impregnation of the brickwork described, the activity transport into the interior of the material is significantly impeded. In radium-contaminated concrete, decontamination factors of between 10 and 15 were attained during decontamination.

New Ice-Abrasive Decontamination Processing Methods

During treatment with the decontamination solution, undesirable solid secondary reaction products may be produced which remain on the surface of the object, and which, under certain circumstances, distinctly im-

pair the decontamination results. This layer is relatively easy to clean, as long as it has not dried out, and is crusted with the surface. After the conclusion of the previously calculated (or estimated) decontamination treatment, the entire system is abrasively treated with solid ice particles. The contaminated parts of the deposition layer are made mobile and may be wiped away and removed.

Referring to FIG. 2, the device for carrying out the present process comprises a reaction container (21), in which contaminated boric acid is transformed into an easily evaporable boron compound. Through a conduit (22), contaminated boric acid is introduced into the reaction container (21). This generally involves a fluid which, in addition to boric acid, also contains water, contaminants, such as, for example, cobalt compounds, as well as contaminants, such as, for example, rust residues, materials fibers, dust, and the like. A chemical substance, which causes the stated transformation, is conducted to the reaction container (21) through an additional conduit (23). This may be a gaseous fluorine or hydrofluoric acid. Hydrofluoric acid can be used either in the form of a fluid or in the form of a gas.

A pump (24) is connected to the reaction container (21), which moves the reaction product from the reaction container (21) into a distillation device (25) of the known type. The rate of introduction of the two named components through the conduits (22) and (23) into the reaction container (21) and the rate of the removal of the reaction product from the reaction container (21), is so selected that enough time is allowed for completion of the stated reaction to the material transport. The sump, which remains behind in the distillation device (25) is removed and conditioned. For this purpose, the sump is first of all neutralized in a further vessel (26), for example, with calcium hydroxide. The neutralized sump material can be just simply dried again, and then

removed as well. It can, however, also be reinforced with cement or bitumen, and then deposited. The heat energy necessary for distillation in the device (25) is advantageously removed in liquid or gaseous media. The distillation is advantageously carried out at low pressure, because the temperatures in the distillation device (25) are then relatively low, and, at such temperatures, practically no pyrolysis takes place.

The HBF₄-acid which is separated during the distillation is removed from the distillation device (25) through a conduit. This acid can be used as a completely regenerable decontamination agent, as is described in a Swiss patent application, No. 2238/85, of the same applicant, or the acid can be sold to the chemical industry, where it can, for example, be used in galvanizing techniques.

The essential advantages of the present process are to be seen in the fact that the fluoroboric acid, which is separated during distillation, does not reach the final storage area for radioactive material, but is sold, for example, to the chemical industry, and thus can be used again. The sump, because it has a smaller volume, can be removed, without entailing large costs. The knowledge that fluoroboric acid HBF₄, in contrast to H₃BO₃, is distillable, and can therefore be separated from the contaminants, such as, for example, Co-60, Cs-nuclides, forms the basis of the present invention. Furthermore, the fluoroboric acid can be separated into fractions of various densities during distillation. The principal reactions, which are the basis of the present process, are as follows:



In one practical case, 15.46 g of H₃BO₃ was added to 20 g HF within approximately 20 minutes.

The present invention relates to a process for decontaminating radiation contaminated boric acid, which accumulates in pressurized water reactors.

In the primary water cycle of pressurized water reactors, boric acid is found in concentrations of up to 3,000 ppm. During the operation of such reactors, smaller quantities of boric acid accumulate as waste. This waste contains, in addition to boric acid, contaminants, such as cobalt compounds, as well as solid impurities such as rust residues, materials fibers, dust, etc.

One such concentrate is compacted with cement. A quantity of 123 kg concentrate solution per 220 liters of matrix, with a space weight of 1.89 Mg/m³, that is to say, 123 kg which is equal to 114 liters with a density of 1.08 Mg/m³, is compacted in 378 kg heavy matrix. The quantities of concentrates can reach, during one year, up to 10 m³ per nuclear power plant. To accommodate this quantity of concentrate, there is required, in accordance with the above assumptions, approximately 88 vessels, whereby the volume of every vessel amounts to approximately 200 liters. With a cost of U.S. \$300 per vessel, including removal, there results the amount of U.S. \$26,400 for the removal of the annually accumulating quantity of waste, whereby this cost, is for many reasons, to be considered as being very high.

It is an objective of the present invention to process contaminated boric acid, where the removal costs are significantly reduced, and the processing of contaminated boric acid satisfies the applicable regulations.

According to one embodiment of this invention, a process for decontaminating radiation contaminated boric acid, which precipitates from pressurized water reactors includes the steps of: reacting the contaminated boric acid with hydrofluoric acid converting the con-

taminated boric acid into HBF₄-acid and vaporizable boron compounds; separating the vaporizable boron compounds from contaminants and solid impurities by distilling; accumulating the vaporizable boron compounds, contaminants and solid impurities in an accumulating sump; removing the contaminants and solid impurities from the sump; and recycling the HBF₄-acid.

The FIG. 3 shows a schematic diagram of one embodiment of a process for decontaminating radiation contaminated boric acid according to this invention. The apparatus for the execution of the present process comprises a reaction container (31) in which contaminated boric acid is converted into an easily vaporizable boron compound. Through a first line (32), contaminated boric acid is introduced to the reaction container (31). This generally involved a fluid, which, in addition to water, also contains contaminants such as cobalt compounds, as well as impurities such as rust residues, dust, etc. Through conduit (33), hydrofluoric acid is conveyed to the reaction container (31), which causes the conversion. Hydrofluoric acid can be applied in different concentrations.

A pump (34) is connected to the reaction container (31) and pumps the reaction product from the reaction container (31) into a distilling device (35) of a known type. The rate of introduction of the two stated components through the conduits (32) and (33), into the reaction container (31) and the rate of the reaction product out of the reaction container (31) is chosen so, that enough time is guaranteed to the material conveyed for a complete cycle of the stated reaction. The sump, which remains behind in the distillation device (35) is removed and is conditioned for the removal. For this purpose, the sump is first neutralized in an additional vessel (36) for example by means of calcium hydroxide. The neutralized sump material can be dried and then stored. It can, however, also be compacted with cement or bitumen and then stored.

The present process can also be carried out in a discontinuous manner in batches. In this case, it is possible to get by with simply one reaction container, in which first the conversion of boric acid and then the distillation are carried out.

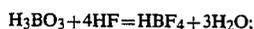
The heat energy necessary for the distillation in the distillation (35) is, advantageously, removed by means of fluid or gaseous media such as warm or hot water or oil, steam, hot gases, etc. In using electrical heating bodies for the execution of the distillation, danger exists of a generally local overheating of the distillation device (35). The distillation is advantageously carried out an underpressure, because the temperatures in the distillation device (35) are then relatively low, and at such temperatures practically no pyrolysis can take place.

The HBF₄-acid accumulating is removed from the distillation device (35) through a conduit (37). This acid can then be used as a completely regenerable decontamination agent. As such, it can be used for the decontamination of radioactively contaminated metallic or concrete surfaces. The accumulating, contaminated HBF₄-acid can again be added to the process before the distillation.

The essential advantages of the present process include the fact that the fluoroboric acid, which accumulates during the distillation, does not reach into the final storage for radioactive material, but rather as described above, can be used again, or can be sold, for example to the chemical industry. The sump, because it has a

smaller volume, can be removed in a more cost-effective manner. Many parts of the described device for the execution of the process can be produced from acid-resistant plastic, such as polyethylene, and can be burned, if such equipment can no longer be used.

The knowledge which forms the basis of the present process is that, fluoroboric acid HBF_4 , in distinction to H_3BO_3 , can be distilled and thereby separated from the contaminants, such as Co-60, Cs-nucleides. In addition, the fluoroboric acid can, during the distillation, be separated into fractions of varying density. The primary reactions, which form the basis of the present process, are as follows:



or



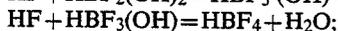
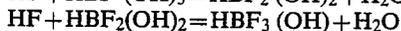
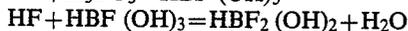
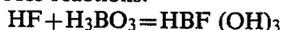
H_3BO_3 molecular weight = 61.84

HF molecular weight = 20

In one practical case, 15.46 g of H_3BO_3 were, within approximately 20 minutes, added to 20 g HF.

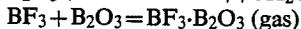
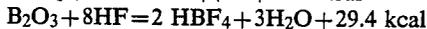
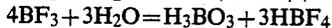
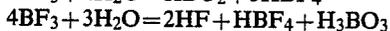
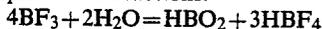
The gross reactions and the equilibrium reactions are stated as follows:

Gross reactions:



Whereby the last reaction is the slowest.

Equilibrium reactions:



The compounds BF_3 and $\text{BF}_3 \cdot \text{B}_2\text{O}_3$ are, respectively, at room temperature and at a temperature of between 100° to 150° C., gaseous, and consequently distillable.

Water loss of boric acid during temperature increases show the following equations:



Because of the removal of the volatile reaction products (BF_3 , $\text{BF}_3 \cdot \text{B}_2\text{O}_3$, HBF_4), the system is far removed from equilibrium, and, upon slight surplus of HF, an almost complete distillation (separation) of boron compounds out of the sump can be attained.

EXAMPLE

10 m³ of boron-containing concentrate (15 percent H_3BO_3) contains 1600 kg of boric acid (approximately 26,000 mol). After the concentration, four-times the mol surplus of HF (104,000 mol HF) is added to the boric acid, for example, 2457 liters of 70 percent HF, 1 liter at U.S. 7.50 (= U.S. \$18,427.50). The distillate yields approximately 26,000 mol HBF_4 , which corresponds to U.S. \$15,437.50 (1 liter = 8 mol (504) = U.S. \$4.75). We obtain, depending on how the process is carried out, 4500 kg of approximately 57 percent of HBF_4 acid or the corresponding dilution, depending on the initial concentration of the boric acid. The HBF_4 -acid obtained should contain traces of activity during the single-stage distillation, because it can be used as completely regenerable decontamination agent for compo-

nents of pressurized water reaction (PWR) and boiling water reactor (BWR). The option for an inactive use (for example, in galvotechnology) consists in the execution of a multi-stage distillation.

The strongly active sump can be cemented into 1 to 5 vessels.

EXAMPLE

10 m³ of boron-containing concentrate (16% H_3BO_3) contains 1600 kg of boric acid (approximately 26,000 Mol). After evaporation, the fourfold mol-surplus of HF is mixed with the boric acid (104,000 Mol HF), that is, for example, 2457 liters of 70% HF, 1 liter at 12.00 Swiss francs (= Sfr. 29,500.00). The distillate yields approximately 26,000 Mol HBF_4 , which comes out to 24,700.00 Swiss francs (1 liter = (8 Mol - 50%) = 7.6 Swiss francs). We obtain, according to the process used, 4500 kg of approximately 57% HBF_4 -acid, or the corresponding dilution, according to the collected concentration of boric acid. The HBF_4 -acid obtained must contain no traces of activity (with the classification distillation), since it can be used as fully regenerable decontamination agent for components of pressurized water reactors and boiling water reactors. The option for an inactive application (in galvanization technology, for example), exists with the execution of a multi-stage distillation process.

I claim:

1. A process for decontaminating radiation contaminated boric acid, which precipitates from pressurized water reactors, the steps comprising: (a) reacting said contaminated boric acid with hydrofluoric acid converting said contaminated boric acid into HBF_4 -acid and vaporizable boron compounds; (b) separating said vaporizable boron compounds from contaminants and solid impurities by distilling; (c) accumulating said vaporizable boron compounds, said contaminants and said solid impurities in an accumulating sump; (d) removing said contaminants and said solid impurities from said sump; and (e) recycling said HBF_4 -acid.

2. The process in accordance with claim 1, wherein heat energy necessary for said distillation is derived from a fluid media.

3. The process in accordance with claim 1, wherein said distillation is carried out at a relatively low pressure.

4. The process in accordance with claim 1, further comprising the step of conditioning sump containing radioactive substances for removal.

5. The process in accordance with claim 4, further comprising the steps of neutralizing said sump with calcium hydroxide, drying said sump, and storing said sump.

6. The process in accordance with claim 4, further comprising the step of neutralizing the sump with calcium hydroxide and then compacting said calcium hydroxide with at least one of cement and bitumen.

7. The process in accordance with claim 1, where said HBF_4 -acid is reused as a completely regenerable decontamination agent for the decontamination of radioactively contaminated metallic and concrete surfaces.

8. The process in accordance with claim 7, further comprising the step of accumulating said HBF_4 -acid, with the contaminants, and again conducting said HBF_4 -acid, with the contaminants, to the process before distillation.

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