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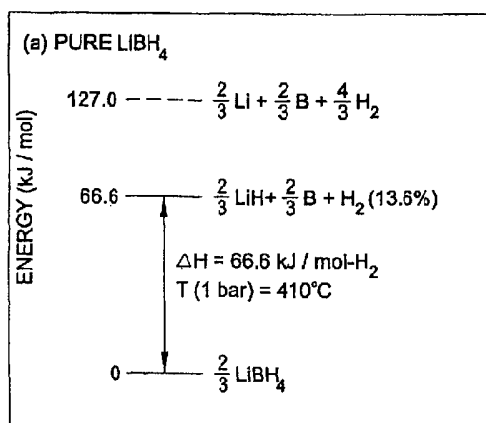
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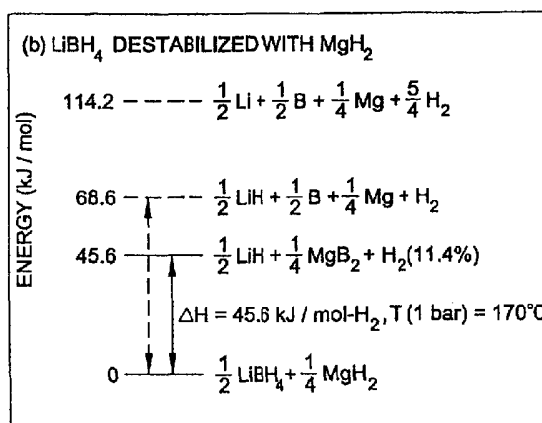
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(54) Title: REVERSIBLE HYDROGEN STORAGE SYSTEM AND METHODS FOR USE THEREOF



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B

(57) Abstract: The invention provides a method of reversibly storing hydrogen at industrially practicable temperature and pressure conditions. A stable hydrogen storage hydride is mixed with a destabilizing hydride. The stable hydride is capable of releasing hydrogen at a first energy level. When the stable hydride is in the presence of the destabilizing hydride, the stable hydride releases hydrogen at a second energy level. The second energy level is significantly reduced from the first energy level. The invention further provides hydrogen storage material systems comprising stable hydrides and destabilizing hydrides.



For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

REVERSIBLE HYDROGEN STORAGE SYSTEM AND METHODS FOR USE THEREOF

5 CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the benefit of both U.S. Provisional Application No. 60/618,870 filed on October 14, 2004 and U.S. Provisional Application No. 60/557,038 filed on March 26, 2004. The disclosures of the above applications are incorporated herein by reference.

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FIELD OF THE INVENTION

[0002] The present invention relates to hydrogen storage compositions that reversibly release hydrogen, the method of making such hydrogen storage compositions and use thereof for storing hydrogen.

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BACKGROUND OF THE INVENTION

[0003] Hydrogen is desirable as a source of energy because it reacts cleanly with air producing water as a by-product. In order to enhance the desirability of hydrogen as a fuel source, particularly for mobile applications, it is desirable to increase the available energy content per unit volume of storage. Presently, this is done by conventional means such as storage under high pressure, at thousands of pounds per square inch, cooling to a liquid state, or absorbing hydrogen into a solid such as a metal hydride. Pressurization and liquification require relatively expensive processing and storage equipment.

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[0004] Storing hydrogen in a solid material provides relatively high volumetric hydrogen density and a compact storage medium. Hydrogen stored in a solid is desirable since it can be released or desorbed under appropriate temperature and pressure conditions, thereby providing a controllable source of hydrogen.

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[0005] Presently, it is desirable to maximize the hydrogen storage capacity or content released from the material, while minimizing the weight of the material to improve the gravimetric capacity. Further, many current materials only absorb or desorb hydrogen at very high temperatures and pressures, which results in costly and industrially impractical energy

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requirements. Additionally, many of these systems are not readily reversible, in that they cannot absorb hydrogen upon contact at reasonable temperature and pressure conditions, and as such do not cyclically absorb and desorb hydrogen in an industrially practicable manner. Thus, it is desirable to find a hydrogen storage material that generates (releases) and reabsorbs hydrogen at relatively low temperatures and pressures, and further has a high gravimetric hydrogen storage density. There is an ever growing demand for a reversible high hydrogen content hydrogen storage material that minimizes required energy input.

[0006] Therefore, in response to the desire for an improved hydrogen storage medium system, the present invention provides a method of storing and releasing hydrogen from storage materials, as well as improved hydrogen storage material systems.

SUMMARY OF THE INVENTION

[0007] In one aspect, the present invention provides a method of reversibly storing hydrogen at industrially practicable temperature and pressure conditions. The method comprises providing a mixture comprising a stable hydrogen storage hydride and a destabilizing hydride. The stable hydride is capable of releasing hydrogen at a first energy level (E_1). The stable hydride is reacted with the destabilizing hydride in a reaction to release hydrogen at a second energy level (E_2). The second energy level E_2 is less than the first energy level E_1 . The reaction is substantially reversible at the industrially practicable pressure and temperature conditions.

[0008] In another aspect, the present invention provides a method of reversibly storing hydrogen comprising providing a mixture of a stable hydrogen storage hydride and a destabilizing hydride. The stable hydride is capable of releasing hydrogen at a first energy level (E_1) and is represented by the nominal general formula AH_x , wherein A comprises an element selected from Groups 13 or 15 of the Periodic Table. The destabilizing hydride is represented by the nominal general formula MH_y . The method comprises reacting the stable hydride with the destabilizing hydride to release hydrogen at a second energy level (E_2). E_2 is less than E_1 . The reacting occurs by the following reaction:



wherein M is one or more cationic species that are distinct from A, and n, m, x, and y are selected so as to maintain electroneutrality. The reaction is substantially reversible at the industrially practicable pressure and temperature conditions.

[0009] In yet another aspect, the present invention provides a method of reversibly storing hydrogen at industrially practicable temperature and pressure conditions. The method comprises providing a mixture having a stable hydrogen storage hydride and a destabilizing hydride. The stable hydride is capable of releasing hydrogen at a first energy level (E_1). The reacting of the stable hydride with the destabilizing hydride releases hydrogen at a second energy level (E_2). E_2 is less than E_1 , and E_2 is related to a free energy of less than about 10 and greater than 0 kJ/mol- H_2 . The reaction is substantially reversible at industrially practicable pressure and temperature conditions.

[0010] In another aspect, the present invention provides a reversible hydrogen storage material comprising a stable hydrogen storage hydride represented by the nominal general formula AH_x and a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y , M is a cationic species that contains one or more cationic species distinct from those in A. In certain preferred embodiments, wherein A is a cationic species that comprises at least one element selected from Groups 13 and 15 of the Periodic Table. In other preferred embodiments, A is a cationic species that comprises boron (B). The "x" and "y" are selected to maintain electroneutrality. The stable hydride is capable of releasing hydrogen at a first energy level. When the stable hydride is in the presence of the destabilizing hydride, hydrogen is released at a second energy level. In accordance with the present invention, the second energy level is significantly reduced from the first energy level.

[0011] In yet another aspect, the present invention provides a reversible hydrogen storage material comprising a stable hydrogen storage hydride represented by the nominal general formula AH_x , where A comprises at least one element selected from Groups 13 or 15 of the Periodic Table. The material also comprises a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y , where M is one or more cationic species

that are distinct from A, and x and y are selected so as to maintain electroneutrality. The stable hydride is capable of releasing hydrogen at a first energy level and the stable hydride in the presence of the destabilizing hydride releases hydrogen at a second energy level. The second energy level is significantly reduced from the first energy level.

[0012] Additionally, the present invention relates to a reversible hydrogen storage material comprising a stable hydrogen storage hydride represented by the nominal general formula AH_x and a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y . A is a cationic species that comprises one or more elements selected from the group consisting of: lithium (Li), sodium (Na), potassium (K), beryllium (Be), magnesium (Mg), calcium (Ca), and mixtures thereof. M is a cationic species that contains one or more cationic species distinct from those in A and is selected from the group consisting of aluminum (Al), arsenic (As), boron (B), barium (Ba), beryllium (Be), calcium (Ca), cadmium (Cd), cerium (Ce), cesium (Cs), copper (Cu), europium (Eu), iron (Fe), gallium (Ga), gadolinium (Gd), germanium (Ge), hafnium (Hf), mercury (Hg), indium (In), potassium (K), lanthanum (La), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), neodymium (Nd), nickel (Ni), lead (Pb), praseodymium (Pr), rubidium (Rb), antimony (Sb), scandium (Sc), selenium (Se), silicon (Si), samarium (Sm), tin (Sn), strontium (Sr), thorium (Th), titanium (Ti), thallium (Tl), vanadium (V), tungsten (W), yttrium (Y), ytterbium (Yb), zinc (Zn), and zirconium (Zr), methyl group (CH_3) and mixtures thereof. X and y are selected so as to maintain electroneutrality. The stable hydride is capable of releasing hydrogen at a first energy level and when the stable hydride is in the presence of the destabilizing hydride, it releases hydrogen at a second energy level. The second energy level is at least about 10 % less than the first energy level.

[0013] Further areas of applicability of the present invention will become apparent from the detailed description provided hereinafter. It should be understood that the detailed description and specific examples, while indicating the preferred embodiment of the invention, are intended for purposes of illustration only and are not intended to limit the scope of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0014] The present invention will become more fully understood from the detailed description and the accompanying drawings, wherein:

[0015] Figure 1 shows comparative energy diagrams of a prior art stable hydride, lithium borohydride or LiBH_4 (Figure 1A), and one embodiment of a hydrogen storage material of the present invention combining a stable hydride LiBH_4 and a destabilizing hydride, magnesium hydride or MgH_2 (Figure 1B);

[0016] Figure 2 shows a comparative volumetric analysis in a custom Sieverts' apparatus showing dehydrogenation of one embodiment of a hydrogen storage material of the present invention (LiBH_4 and MgH_2) versus time and the weight loss of a prior art stable hydride (LiBH_4) versus time as temperature is increased to 450°C and then held constant;

[0017] Figure 3 shows a comparative volumetric analysis of hydrogen absorption of both an embodiment of a hydrogen storage material of the present invention (LiBH_4 and MgH_2) as compared to a prior art stable hydride (LiBH_4), where heat is applied at a constant rate of 120°C per hour or 2°C per minute;

[0018] Figure 4 is an x-ray diffraction pattern of a hydrogen storage material according to the present invention (LiBH_4 and MgH_2) taken after milling a stable hydride with a destabilizing hydride (curve a), after dehydrogenation (curve b), and after rehydrogenation (curve c);

[0019] Figure 5 is another volumetric analysis showing cyclic dehydrogenation and rehydrogenation of an embodiment of a hydrogen storage material of the present invention (LiH and MgB_2);

[0020] Figure 6 shows absorption and desorption isotherms for multiple samples of hydrogen storage materials of the present invention (LiH and MgB_2 with TiCl_3) where the filled symbols indicate absorption and the open symbols at 400°C indicate desorption;

[0021] Figure 7 is a van't Hoff plot showing equilibrium pressures obtained from absorption isotherms corresponding to the 4 weight % data of Figure 6, indicated therein by the "X" mark designations; and

[0022] Figure 8 shows an X-ray diffraction (XRD) graph showing dehydrogenation of a stable hydride and a destabilizing hydride under a hydrogen atmosphere and an argon atmosphere.

5 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0023] The following description of the preferred embodiment(s) is merely exemplary in nature and is in no way intended to limit the invention, its application, or uses. The following definitions and non-limiting guidelines must be considered in reviewing the description of this invention set forth herein. The
10 description and any specific examples, while indicating embodiments of the invention, are intended for purposes of illustration only and are not intended to limit the scope of the invention. Moreover, recitation of multiple embodiments having stated features is not intended to exclude other embodiments having additional features, or other embodiments incorporating different combinations
15 the stated of features. Specific Examples are provided for illustrative purposes of how to make and use the compositions and methods of this invention and, unless explicitly stated otherwise, are not intended to be a representation that given embodiments of this invention have, or have not, been made or tested.

[0024] As used herein, the words "preferred" and "preferably" refer to
20 embodiments of the invention that afford certain benefits, under certain circumstances. However, other embodiments may also be preferred, under the same or other circumstances. Furthermore, the recitation of one or more preferred embodiments does not imply that other embodiments are not useful, and is not intended to exclude other embodiments from the scope of the
25 invention.

[0025] As used herein, the word "include," and its variants, is intended to be non-limiting, such that recitation of items in a list is not to the exclusion of other like items that may also be useful in the materials, compositions, devices, and methods of this invention.

30 [0026] As referred to herein, all compositional percentages are by weight of the total composition, unless otherwise specified.

[0027] As used herein, the term "about," when applied to the value for a parameter of a composition or method of this invention, indicates that the

calculation or the measurement of the value allows some slight imprecision without having a substantial effect on the chemical or physical attributes of the composition or method. If, for some reason, the imprecision provided by "about" is not otherwise understood in the art with this ordinary meaning, then "about" as
5 used herein indicates a possible variation of up to 5% in the value.

[0028] As used herein, the term "composition" refers broadly to a substance containing at least the preferred chemical compound, but which may also comprise additional substances or compounds, including impurities. The term "material" also broadly refers to matter containing the preferred
10 compounds or compositions.

[0029] The present invention provides a hydrogen storage material system that is capable of releasing relatively high hydrogen content and reversibly storing hydrogen at industrially practicable temperature and pressure conditions. In various embodiments of the present invention, a mixture is
15 provided of a stable hydrogen storage hydride composition combined with a destabilizing composition to provide a reversible high-hydrogen content hydrogen storage material. The destabilizing composition preferably comprises at least one destabilizing hydride. While in the presence of the destabilizing hydride, the stable hydride releases hydrogen and reversibly absorbs hydrogen
20 at significantly lower temperature and pressure conditions, making the hydrogen storage material of the present invention particularly suitable for mobile hydrogen applications.

[0030] By "reversible" it is meant that one or more of the hydrogen starting materials is capable of being regenerated at temperature and pressure
25 conditions which are economically and industrially useful and practicable. In the same manner, a "non-reversible reaction" generally applies to both reactions that are traditionally considered irreversible because they generally are not capable of reacting via the same reaction mechanism pathway, but also includes those reactions where regenerating a species of a hydrogen containing
30 starting material by exposure to hydrogen is carried out at impractical processing conditions, such as, extreme temperature, extreme pressure, or cumbersome product removal, which prevents its widespread and practical use. Currently, hydrogen storage compositions that release hydrogen

endothermically are typically considered the best candidates for reversible hydrogen storage at desirable temperature and pressure conditions.

[0031] Particularly preferred "reversible" reactions include those where exposing one or more product compositions to hydrogen regenerates a species of one or more of the starting materials, while enabling a hydrogen release of about 5 weight % or more, and in preferably about 7 weight % or more. As appreciated by one of skill in the art, the concept of industrially practicable reversibility includes evaluating the weight percent of hydrogen released, as balanced with the energy input necessary to reversibly cycle (release and absorb) hydrogen. For example, an endothermic hydrogen storage material may require a high energy input to release hydrogen. However, this energy input may be offset by a relatively high hydrogen content (concentration of hydrogen released from the material) such that some of the hydrogen being released can be consumed as energy to fuel additional release of hydrogen. Yet, overall the hydrogen storage material releases a sufficient amount of hydrogen to be a suitable candidate for fuel cell applications.

[0032] One aspect of the present invention is a hydrogen storage material system that has a reduction in the overall energy requirements for storing and subsequently releasing hydrogen. Minimizing the overall enthalpy changes associated with the hydrogen storage material system results in an improvement in the overall efficiency an associated fuel cell system. As the overall enthalpy change increases, so does the requirement for managing heat transfer systems (heating and cooling operations). In particular, it is highly advantageous to minimize heating and cooling systems in mobile units containing fuel cells that consume hydrogen (e.g., vehicles or electronic devices), because additional systems draw parasitic energy and increase the overall weight of the mobile unit, thereby decreasing its gravimetric efficiency.

[0033] A brief background is provided herein to enable a better understanding of the inventive concepts of the present invention. Higher hydrogen capacities have been deemed necessary for commercial development of vehicles and other mobile products powered by hydrogen/oxygen proton exchange membrane fuel cells. Based on the current understanding of hydrogen storage materials, it appears that most transition metal-based hydride

materials do not have hydrogen capacities of greater than 4 - 6 wt %. Thus, development has focused on low-Z complex hydrides, where Z is the atomic number of an element and "low-Z" refers to compounds having relatively low atomic numbers that are light-weight compounds. Such low-Z complex hydrides, include, for example, alanates (AlH_4^-), amides (NH_2^-), and borohydrides (BH_4^-). Use of such hydrides for hydrogen storage is challenging because of both the kinetic and thermodynamic limitations. For example, the reversible formation of many complex hydrides is associated with slow kinetics, although, it is possible to improve reaction rates with appropriate catalysts. Thermodynamically, the stability of a complex hydride must lie within a specific range in order for the hydrogenation/dehydrogenation phase boundary to occur at practical pressures and temperatures. Many low-Z alanates are generally considered too unstable and difficult to control because they readily release hydrogen at ambient temperatures and pressures. However, some alanates, such as for example, NaAlH_4 , do form hydrides that require higher temperatures and pressures to evolve hydrogen. Most borohydrides, such as for example, LiBH_4 and NaBH_4 are very stable, and as such are difficult to use at typical fuel cell operating temperature and pressure conditions.

[0034] Figure 1A shows an energy diagram of a prior art hydrogen storage hydride material, pure lithium borohydride, LiBH_4 . Figure 1A shows the energy diagram for LiBH_4 calculated based on predicted products and performed using HSC chemistry. While the total hydrogen content of LiBH_4 is relatively high at above about 18 wt %, pure LiBH_4 does not reversibly store significant hydrogen, and the products of the decomposition of LiBH_4 have not been clearly identified. A predicted partial decomposition reaction produces LiH , B , and $3/2 \text{H}_2$ and has a theoretical yield of 13.6 wt % hydrogen. However, the calculated standard enthalpy for this reaction is about + 67 kJ/mol- H_2 and thus, even if reversible, an equilibrium pressure of 1 bar requires a temperature of greater than 400° C. Such a temperature is generally considered too high for practical hydrogen storage applications.

[0035] In such a manner, LiBH_4 can be defined as a "stable" hydride, meaning that the composition requires a prohibitive input of energy in order to release hydrogen because it is thermodynamically stable. By the term

“prohibitive” it is meant that the energy required is industrially impracticable, particularly for mobile consumer products, and tends to preclude the use of the material due to excessive energy requirements.

[0036] The modification of hydrogenation/dehydrogenation thermodynamics can be accomplished with various material systems by using destabilizing additives that form alloys or compounds with a stable hydride composition. When a destabilizing composition is added to a stable hydrogen storage composition to favorably alter the thermodynamics for hydrogen storage applications, the equilibrium pressure is increased, and thus reduces the energy input requirements for the overall system. In one example, a destabilizing compound reacts with the stable hydrogen storage compound to form additional or modified reactants and/or products to arrive at more favorable thermodynamics. Hydrides of many Period 2 and 3 elements (of the Periodic Table) are known in the art to have relatively high hydrogen densities, for example greater than 5-6 wt %. However, most of these hydrides are quite stable and do not release hydrogen until the temperature exceeds 250°C at 1 bar.

[0037] Two examples of such materials are lithium hydride (LiH) and magnesium hydride (MgH₂). Lithium hydride contains 12.5 wt % hydrogen, but requires 910°C for an equilibrium pressure of 1 bar. Magnesium hydride contains 7.7 wt % hydrogen and has a 1 bar equilibrium pressure at 275°C. The thermodynamics of the magnesium hydride can be altered by using additives that form alloys or compounds with Mg in either or both the hydrogenated and/or dehydrogenated states. A well-known example is adding nickel to the magnesium to form Mg₂Ni in the starting materials, which, upon hydrogenation, forms Mg₂NiH₄ with 3.6 wt % hydrogen and an equilibrium pressure of 1 bar at 245° C. Elemental aluminum has been found to destabilize MgH₂ by forming a Mg/Al alloy upon dehydrogenation. The reaction is reversible with MgH₂ and Al reforming and segregating during hydrogenation. At 280° C, the more favorable equilibrium pressure is a factor of 3 larger than that of pure MgH₂.

[0038] To achieve a higher equilibrium pressure for strongly bound stable hydride systems (that translates to reduced energy requirements to

desorb hydrogen), additives can be introduced to the stable hydride to form compounds or alloys with the dehydrogenated metals. Destabilization occurs because the system can cycle between the hydride and the newly formed and more thermodynamically favorable compound(s) instead of the less favorable dehydrogenated elemental metal(s). A destabilizing element, such as for example, silicon (Si) destabilizes certain stable hydride storage systems, such as lithium hydride or magnesium hydride. The added silicon forms relatively strongly bonds with either lithium or magnesium. These newly formed strong bonds reduce dehydrogenation enthalpies and increase equilibrium hydrogen pressures. Other useful elemental destabilizers for stable hydrides, include by way of example, silicon (Si), aluminum (Al), and copper (Cu).

[0039] Thus, in one aspect the present invention provides methods of destabilizing one or more stable hydride species. To this end, one object is to increase the equilibrium pressure of various strongly bound stable hydrides to in essence reduce the required system enthalpy and stabilize the dehydrogenated state. Stabilizing the dehydrogenated state reduces the enthalpy for dehydrogenation, thereby increasing the equilibrium hydrogen pressure. Using this approach, the thermodynamic properties of reversible hydrogen storage material systems can potentially be tuned to a finer extent than would be possible with individual materials to achieve reversible hydrogen release at practical temperature and pressure conditions.

[0040] However, it is also desirable to increase the hydrogen content of the overall hydrogen storage system. The present invention provides a relatively high yield of hydrogen gas from a hydrogen storage material, while minimizing the energy input required for the reversible system. In various embodiments, the present invention provides relatively light-weight reversible hydrogen storage materials. In certain embodiments of the present invention, the reversible hydrogen storage materials have gravimetric system capacities of greater than 5 to 9 wt % hydrogen.

[0041] Thus, the present invention provides in various embodiments a high hydrogen content hydrogen storage system that comprises a stable hydride material and a destabilizing hydride material, where each of the reactants potentially contribute to the amount of released hydrogen for

consumption in the fuel cell. Hence, both the stable hydride and the destabilizing hydride provide hydrogen to increase the hydrogen content released. Additionally, in accordance with the present invention, as previously described, the addition of a destabilizing hydride with a stable hydride favorably improves the reaction thermodynamics, such that the required energy input or enthalpy is reduced by increasing the equilibrium pressure of the hydrogen storage system. It should be noted that predicted thermodynamics and equilibrium pressures are useful for selecting hydrogen storage materials of the present invention, however a discrepancy between the calculated or predicted values associated with energy levels (e.g., equilibrium pressure, enthalpy) and the actual values is often observed.

[0042] In certain embodiments, the present invention provides a method of reversibly storing hydrogen at industrially practicable temperature and pressure conditions. A stable hydrogen storage hydride is mixed with a destabilizing hydride. The stable hydride is characterized by releasing hydrogen in a first reaction having a first free energy level (E_1). The first energy level is related to a change in enthalpy denoted by ΔH . Also associated with the release of hydrogen is a change in entropy denoted by ΔS . The changes in enthalpy and entropy can be used to determine the change in Gibbs free energy which is generally expressed as:

$$\Delta G = \Delta H - T\Delta S = -RT(\ln K_{eq}) \quad (\text{Equation 1})$$

where K_{eq} is the equilibrium constant, H is the enthalpy, S is the entropy, T is the absolute temperature in Kelvins, R is the gas constant, and K_{eq} is the equilibrium constant. The Gibbs free energy change relates to the thermodynamic feasibility of a chemical reaction. If $\Delta G > 0$, the reaction cannot spontaneously occur. If $\Delta G < 0$, the reaction can occur spontaneously if there are no kinetic limitations along the reaction pathway. The temperature at which a reaction becomes thermodynamically feasible is the temperature at which $\Delta G = 0$ or alternatively $K_{eq} = 1$. This temperature is generally determined by the following equation:

$$T(\Delta G = 0) = \Delta H / \Delta S \quad (\text{Equation 2})$$

The entropic contribution to the free energy, represented by the term $T\Delta S$, compensates for the higher enthalpy or energy level that must be attained to enable a particular reaction to occur. Because hydrogen is a low molecular

weight diatomic gas, the entropy of hydrogen gas to a large extent dominates the entropy change associated with hydrogen release reactions regardless of the solid phase components that are involved. Hence, the free energy can be generally expressed as a required "energy level" that must be applied or input to the system to enable a desired reaction.

[0043] Thus, the effect of mixing a stable hydride with a destabilizing hydride is approximately determined by the associated enthalpy or energy level changes. When a stable hydride is combined with a destabilizing hydride, hydrogen release can occur in a second reaction having a lower ΔH and, consequently a lower reaction temperature. After mixing the stable hydride with the destabilizing hydride, a two phase hydrogen storage material is formed. The stable hydride is then reacted with the destabilizing hydride in a second hydrogen release reaction that has a second energy level (E_2). In accordance with the present invention, the energy level for the second reaction, E_2 , is less than the first energy level for the stable hydride by itself, E_1 . Such energy level changes are demonstrated in Figure 1B where the hydrogen storage material comprises a stable hydride lithium borohydride (LiBH_4) combined with a destabilizing compound (MgH_2). Stated in another way, the stable hydride is capable of releasing hydrogen at a first energy level. However, when the storage material comprises the stable hydride is in the presence of the destabilizing hydride, the storage material releases hydrogen at a second energy level, and the second energy level is significantly reduced from the first energy level.

[0044] As can be observed from the prior art depicted in Figure 1A, which was discussed above, in the absence of magnesium hydride, the stable hydride lithium borohydride releases hydrogen in an endothermic reaction which requires $\Delta H = +66.6 \text{ kJ/mol-H}_2$ and the equilibrium pressure at 1 bar has a temperature of 410°C . However, with the addition of the destabilizing hydride in accordance with the present invention shown in Figure 1B (where the hydrogen storage system comprises a stable hydride LiBH_4 and a destabilizing hydride MgH_2), the combined hydrogen storage material has a reduced enthalpy, $\Delta H = +45.6 \text{ kJ/mol-H}_2$, where the equilibrium pressure is calculated to be 1 bar with a temperature of 170°C . The stability of the MgB_2 alloy reduces the standard

enthalpy for dehydrogenation from about +66 kJ/mol-H₂ to about +46 kJ/mol-H₂, which translates to a reduction of 30 % in energy. The temperature reduction is 240°C at a pressure of 1 bar, which likewise equates to a reduction in the required energy input.

5 **[0045]** The second energy level E_2 is less than the first energy level for the stable hydride by itself, E_1 . It should be noted that combining the stable hydride LiBH₄ with the destabilizing hydride MgH₂ actually destabilizes both the LiBH₄ and the MgH₂ in this case, to release hydrogen at a lower enthalpy than either the stable hydride or destabilizing hydride by itself, as will be discussed in
10 more detail below.

[0046] Thus, for various embodiments of the present invention, it is preferred that the second energy level E_2 is significantly reduced from the first energy level E_1 for the hydrogen storage material. A "significant" reduction is preferably at least 10% reduction between the energy levels. In certain
15 preferred embodiments, the second energy level E_2 is at least 20% less than the first energy level E_1 , and in particularly preferred embodiments, the difference in energy level is at least 30%.

[0047] In various embodiments of the present invention, the first energy level is related to a first temperature that the system must achieve to
20 release hydrogen from the stable hydride alone, and the second energy level is related to a second temperature required to release hydrogen in the reaction between the stable hydride and destabilizing hydride. In preferred embodiments, the first temperature is greater than about 250°C and the second temperature is less than 250°C at a pressure of 1 bar. In more preferred embodiments, the
25 second temperature is less than about 200°C. In alternate embodiments, the second temperature is less than about 175°C. It is preferred that the second temperature required to release hydrogen is reduced as low as possible for the hydrogen storage material.

[0048] The reduction in the energy level can also be related to the
30 equilibrium pressure of the respective hydrogen storage systems. Thus, a prior art system, such as LiBH₄, has an equilibrium pressure that is less or equal to about 1 bar at 400°C, as where certain embodiments of hydrogen storage material systems of the present invention have a significantly increased

equilibrium pressure at 400°C of greater than 10 bar and preferably greater than 12 bar. Thus, the first energy level is related to a first equilibrium pressure reflected in an equilibrium pressure that is low (about 1 bar or less) at 400°C, as where the second energy level is related to a second equilibrium pressure that is
5 significantly higher (greater than about 10 bar) at the same temperature, correlating the reduced second energy level.

[0049] Hence, in preferred embodiments, the addition of the destabilizing hydride alters the thermodynamics of the hydrogen storage material hydrogen desorption reaction, and further enables a reversible hydrogenation
10 reaction, where one or more of the products formed during the dehydrogenation reaction can be rehydrogenated upon exposure to hydrogen gas. The ease of reversibility of the reaction is correlated to the free energy level of the products. As the overall Gibb's free energy level for the hydrogen release approaches 0, the reversibility occurs with increasingly greater ease. As previously described,
15 one particular application for the hydrogen storage materials is a mobile fuel cell application. It is preferred that hydrogen storage materials both release and recharge hydrogen at industrially practicable temperature and pressures. Generally speaking, these temperatures in the vehicular fuel cell applications correspond to a range of approximately ambient temperature to fuel cell
20 operating temperatures. Exemplary operating temperatures generally range up to about 150°C. Particularly preferred operating temperatures are from about 80°C to about 100°C. In certain embodiments, the hydrogen storage material is selected to desorb and absorb around the operating temperatures of the mobile fuel cell. For example, this can be achieved by selecting a hydrogen storage
25 material system that has a free energy that approaches zero at the appropriate temperature conditions (in that the enthalpy term (ΔH) of Equation 1 is nearly equal to the entropy term ($T\Delta S$)). In particularly preferred embodiments, the reaction enthalpy is endothermic. In certain embodiments of the present invention, the second energy level E_2 which is associated with the preferred
30 operating temperature ranges correlates to an enthalpy of less than about +45 kJ/mol- H_2 and greater than about +30 kJ/mol- H_2 at ambient temperatures (ambient temperatures include a range of temperatures at which mobile applications may operate, which include, by way of example, approximately

-35°C to 25°C) to about 150°C and ambient pressure (approximately 1 bar) demonstrating a relatively facile and controllable reversible reaction system. In particularly preferred embodiments, the enthalpy is about 35 kJ/mol-H₂, which relates to good control and reversibility at current operating temperatures in mobile fuel cell applications, although the material can be selected for any range of temperatures and corresponding enthalpy.

[0050] In certain embodiments of the present invention, the destabilizing hydride is capable of releasing hydrogen in a third reaction (in the absence of the stable hydride) and has a third energy level E₃. In the case of certain destabilizing hydrides, the second energy level E₂ is less than the third energy level E₃, thus the combined hydrides that form the hydrogen storage material of the present invention encounter a lower free energy in combination than either hydride would have by itself upon releasing hydrogen. One such example is where the destabilizing hydride is MgH₂ and the stable hydride is LiBH₄. When these compounds are combined, the free energy is less than the respective free energy for hydrogen release for the individual compounds.

[0051] Thus, in certain preferred embodiments, the present invention provides a solid state hydrogen storage material system that comprises a hydrogenated state where hydrogen is "stored" in the reactants and another dehydrogenated state subsequent to hydrogen release corresponding to the products. In certain embodiments of the present invention, the hydrogenated state comprises two separate solid phases, the first phase corresponding to a stable hydride and the second solid phase corresponding to the destabilizing compound or hydride. In various embodiments, the solid phase reactants are milled to reduce the average diameter particle size and to increase the surface area of the particles prior to reacting. It should be noted that with hydrogen storage material systems of the present invention, ball milling reduces particle size and mixes the starting reactants, but generally does not facilitate a reaction between them, as is often observed in other hydrogen storage material systems when they are ball-milled. In certain preferred embodiments, the average particle diameter size is reduced to less than about 25 μm, more preferably less than about 15 μm.

[0052] A stable hydrogen storage hydride is represented by the nominal general formula AH_x , where A comprises an element selected from Groups 13 or 15 of the Periodic Table. The hydrogen storage material also comprises a destabilizing hydrogen storage hydride which can be represented by the nominal general formula MH_y , where M is one or more cationic species distinct from A. Further, x and y are selected so as to maintain electroneutrality. In the absence of the destabilizing hydride, the stable hydride would require a prohibitive energy input to release hydrogen.

[0053] The cationic species A of the stable hydride comprises one or more elements other than hydrogen, preferably those elements selected from Groups 13 or 15 of the IUPAC Periodic Table. In certain embodiments, the cationic species A comprises aluminum (Al), boron (B), gallium (Ga), indium (In), thallium (Tl), arsenic (As), nitrogen (N), antimony (Sb), or mixtures thereof. In accordance with certain embodiments of the present invention, a particularly preferred stable hydride is one where the cationic species A comprises boron (B).

[0054] In certain preferred embodiments of the present invention, A is a complex cationic species, which comprises two or more distinct cationic species. Hydrides are often referred to as complex hydrides, which are further contemplated in the present invention. A complex hydride comprises two cationic species other than hydrogen, however one of the cationic species forms an anionic group with hydrogen, which further interacts with a second cationic species. This concept can be expressed by the following formula with a hydride expressed as A^xH_x , where A comprises two distinct cationic species, A' and A'', so that $A = A' + A''$. Thus, the hydride can generally be expressed as: $A_d^a (A'^b H_c)^{-d}$ where $(A'^b H_c)$ is an anionic group, where $d = (c - b)$ and a, b, c, and d are selected so as to maintain charge balance and electroneutrality of the compound. As appreciated by one of skill in the art, suitable complex hydrides include those where A comprises additional cationic species that differ from the general expression described above, and A may comprise multiple cationic species or a compound, so long as the charge balance and electroneutrality of the complex hydride are maintained.

[0055] In certain embodiments of the present invention, where the stable hydride is a complex cationic species, A further comprises at least one element selected from Group 1 and 2 of the Periodic Table, or mixtures thereof, in addition to the element selected from Groups 13 and 15. Thus, it is preferred that where the stable hydride is a complex hydride, that A comprises one or more elements selected from the group consisting of: barium (Ba), beryllium (Be), calcium (Ca), cesium (Cs), potassium (K), lithium (Li), magnesium (Mg), sodium (Na), rubidium (Rb), strontium (Sr), and mixtures thereof. In more preferred embodiments, where the stable hydride is a complex hydride, A comprises one or more elements selected from the group consisting of: boron (B), aluminum (Al), lithium (Li), sodium (Na), potassium (K), beryllium (Be), magnesium (Mg), calcium (Ca), and mixtures thereof. In particularly preferred embodiments, the stable hydride is a complex hydride that comprises boron (B) and also comprises a lithium (Li), magnesium (Mg), or sodium (Na). In alternate embodiments, the stable hydride is a complex hydride and A comprises a transition metal that is selected from Groups 3 to 12 of the Periodic Table.

[0056] In various embodiments of the present invention, the stable hydride is selected from the group of compounds consisting of: lithium borohydride (LiBH_4), sodium borohydride (NaBH_4), lithium aluminum hydride (LiAlH_4), magnesium borohydride $\text{Mg}(\text{BH}_4)_2$, magnesium aluminum hydride $\text{Mg}(\text{AlH}_4)_2$, sodium aluminum hydride (NaAlH_4), calcium borohydride ($\text{Ca}(\text{BH}_4)_2$), calcium aluminum hydride ($\text{Ca}(\text{AlH}_4)_2$) and mixtures thereof. In particularly preferred embodiments of the present invention, the stable hydride is selected from the group of compounds consisting of: lithium borohydride (LiBH_4), sodium borohydride (NaBH_4), magnesium borohydride $\text{Mg}(\text{BH}_4)_2$, and mixtures thereof.

[0057] It is preferred that the cationic species M in the destabilizing hydride MH_y comprises one or more cationic species distinct from those in A. The elements of the cationic species M are preferably distinct from those of the stable hydride to enable a thermodynamic modification of the hydrogen release reaction in accordance with the present invention.

[0058] It should be understood that in the present invention the cationic species M can be represented by a single cationic species or a mixture

of cationic species other than hydrogen (e.g., a complex hydride). Examples of suitable cationic species include metal cations, non-metal cations (such as boron), and non-metal cations which are organic such as CH_3 . In certain embodiments, the destabilizing hydride comprises a transition metal that is selected from Groups 3 to 12 of the Periodic Table. Certain preferred cationic species generally comprise: aluminum (Al), arsenic (As), boron (B), barium (Ba), beryllium (Be), calcium (Ca), cadmium (Cd), cerium (Ce), cesium (Cs), copper (Cu), europium (Eu), iron (Fe), gallium (Ga), gadolinium (Gd), germanium (Ge), hafnium (Hf), mercury (Hg), indium (In), potassium (K), lanthanum (La), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), neodymium (Nd), nickel (Ni), lead (Pb), praseodymium (Pr), rubidium (Rb), antimony (Sb), scandium (Sc), selenium (Se), silicon (Si), samarium (Sm), tin (Sn), strontium (Sr), thorium (Th), titanium (Ti), thallium (Tl), vanadium (V), tungsten (W), yttrium (Y), ytterbium (Yb), zinc (Zn), and zirconium (Zr), and organic cations including (CH_3) methyl groups.

[0059] Particularly preferred cations for the cationic species M of the destabilizing hydride include one or more elements selected from the group consisting of: aluminum (Al), barium (Ba), beryllium (Be), boron (B), calcium (Ca), cesium (Cs), iron (Fe), gallium (Ga), germanium (Ge), indium (In), lithium (Li), magnesium (Mg), nitrogen (N), potassium (K), rubidium (Rb), silicon (Si), sodium (Na), strontium (Sr), titanium (Ti), thallium (Tl), tin (Sn), zirconium (Zr) and mixtures thereof. In certain more preferred embodiments, where the hydride is a complex hydride, M comprises one or more elements selected from the group consisting of: aluminum (Al), beryllium (Be), boron (B), calcium (Ca), lithium (Li), magnesium (Mg), nitrogen (N), potassium (K), sodium (Na), and mixtures thereof.

[0060] In certain embodiments of the present invention, the destabilizing hydride is a "binary" hydride, meaning that the hydride comprises hydrogen and only one other cationic species M. In binary hydrides, typically the cationic species M is an alkali or alkaline earth metal (Groups 1 and 2 of the Periodic Table). Non-limiting examples of binary hydrides include LiH , NaH , MgH_2 , CaH_2 and the like.

[0061] In various embodiments of the present invention, the destabilizing hydride is selected from the group of compounds consisting of: lithium hydride (LiH), sodium hydride (NaH), potassium hydride (KH), magnesium hydride (MgH₂), calcium hydride (CaH₂), lithium aluminum hydride (LiAlH₄), sodium borohydride (NaBH₄), lithium borohydride (LiBH₄), magnesium borohydride Mg(BH₄)₂, sodium aluminum hydride (NaAlH₄), and mixtures thereof.

[0062] In accordance with an embodiment of the present invention, the hydrogen storage material comprising a stable hydride and a destabilizing hydride releases hydrogen by the following reversible reaction:



wherein n, m, x, and y are selected so as to maintain electroneutrality. The reaction produces both H₂, as well as a byproduct compound A_nM_m. It should be noted that the byproduct compound A_nM_m may thermodynamically favor decomposing into further smaller and/or distinct byproduct compounds. These further byproducts are formed of the same general constituents as the primary byproduct, but they have different valence states, atomic ratios, or stoichiometry, depending on the cationic species involved, as recognized by one of skill in the art. Such additional distinct byproduct compounds may include metal hydrides, which may slightly detract from the total amount of hydrogen generated designated as $\frac{1}{2}(nx+my) \text{H}_2$. For example, in one embodiment, where the stable hydride is a complex hydride (i.e., where A is a complex cationic species) the material releases hydrogen by the following reversible reaction:



wherein n, m, c, d, x, and y are selected so as to maintain electroneutrality.

[0063] In certain preferred embodiments of the present invention, the stable hydride is a complex hydride and the destabilizing hydride is a binary hydride. In one embodiment, a stable hydride is lithium borohydride (LiBH₄) and a destabilizing hydride is magnesium hydride (MgH₂). In another embodiment, a hydrogen storage material has a stable hydride, sodium borohydride (NaBH₄) and a destabilizing hydride, lithium hydride (LiH). Yet another embodiment is a hydrogen storage material where a stable hydride is sodium borohydride

(NaBH₄) and a destabilizing hydride is magnesium hydride (MgH₂). Other embodiments include, a stable hydride: lithium borohydride (LiBH₄) and a destabilizing hydride: sodium hydride (NaH); a stable hydride: magnesium borohydride (Mg(BH₄)₂) and a destabilizing hydride: lithium hydride (LiH); a
5 stable hydride: magnesium borohydride (Mg(BH₄)₂) and a destabilizing hydride: sodium hydride (NaH); a stable hydride: lithium borohydride (LiBH₄) and a destabilizing hydride: sodium borohydride (NaBH₄); stable hydride: lithium borohydride (LiBH₄) and a destabilizing hydride: sodium borohydride (NaBH₄); a
10 stable hydride: lithium borohydride (LiBH₄) and a destabilizing hydride: lithium aluminum hydride (LiAlH₄); a stable hydride: lithium borohydride (LiBH₄) and a destabilizing hydride: sodium aluminum hydride (NaAlH₄); a stable hydride: sodium borohydride (NaBH₄) and a destabilizing hydride: sodium aluminum hydride (NaAlH₄)

[0064] In alternate embodiments of the present invention, the
15 hydrogen storage material may comprise a plurality of distinct stable hydride compositions, or a plurality of destabilizing hydride compositions, or a plurality of both stable hydrides and destabilizing hydrides. In other embodiments, the hydrogen storage material comprises a stable hydride and a destabilizing hydride, and further comprises a destabilizing compound, that is distinct from
20 the destabilizing hydride, where the destabilizing compound promotes the release of hydrogen from the storage material at a reduced energy level from that of the stable hydride by itself. In certain embodiments, the additional destabilizing compound achieves an even greater reduction for the second energy level E₂ or second energy level than would be achieved for the mixture
25 of the destabilizing hydride and the stable hydride in the absence of the additional destabilizing compound. Examples of some destabilizing compounds include elemental forms of silicon (Si), aluminum (Al), and copper (Cu).

[0065] Examples of preferred reactions according to the present invention which reduce the energy of the hydrogen storage system comprise:

30 1) $2 \text{LiBH}_4 + \text{MgH}_2 \rightarrow 2 \text{LiH} + \text{MgB}_2 + 4 \text{H}_2$ (Reaction 1), which generates a theoretical 11.4 wt% hydrogen and has a predicted enthalpy of reaction of +45.6 kJ/mol-H₂, and a predicted equilibrium pressure of 170°C at 1 bar (although the measure equilibrium pressure was approximately 225°C at 1 bar).

[0066] Other non-limiting examples of alternate preferred embodiments according to the present invention where hydrogen generation occurs based on predicted thermodynamics, include the following exemplary reactions:

5 2) $\text{NaBH}_4 + \frac{1}{2} \text{LiAlH}_4 \rightarrow \text{NaH} + \frac{1}{2} \text{LiH} + \frac{1}{2} \text{AlB}_2 + \frac{9}{4} \text{H}_2$ (Reaction 2), which generates a theoretical 7.8 wt% hydrogen, has a predicted enthalpy of reaction at 20°C of 32.6 kJ/mol- H_2 and a predicted equilibrium pressure of 70°C at 1 bar..

3) $\text{LiBH}_4 + \frac{1}{2} \text{LiAlH}_4 \rightarrow \frac{3}{2} \text{LiH} + \frac{1}{2} \text{AlB}_2 + \frac{9}{4} \text{H}_2$ (Reaction 3), which generates a theoretical 10.9 wt% hydrogen, has a predicted enthalpy of reaction
10 at 20°C of 16.8 kJ/mol- H_2 and a predicted equilibrium pressure of 90°C at 1 bar.

4) $\text{LiBH}_4 + \frac{1}{2} \text{NaAlH}_4 \rightarrow \text{LiH} + \frac{1}{2} \text{NaH} + \frac{1}{2} \text{AlB}_2 + \frac{9}{4} \text{H}_2$ (Reaction 4), which generates a theoretical 9.1 wt% hydrogen, has a predicted enthalpy of reaction at 20°C of 23.3 kJ/mol- H_2 and a predicted equilibrium pressure of 0°C at 1 bar.

5) $\text{NaBH}_4 + \frac{1}{2} \text{NaAlH}_4 \rightarrow \frac{3}{2} \text{NaH} + \frac{1}{2} \text{AlB}_2 + \frac{9}{4} \text{H}_2$ (Reaction 5), which
15 generates a theoretical 6.9 wt% hydrogen, has a predicted enthalpy of reaction at 20°C of 39.2 kJ/mol- H_2 and a predicted equilibrium pressure of 150°C at 1 bar.

6) $\text{NaBH}_4 + \frac{1}{2} \text{MgH}_2 \rightarrow \text{NaH} + \frac{1}{2} \text{MgB}_2 + 2\text{H}_2$ (Reaction 6), which generates a theoretical 7.9 wt% hydrogen, has a predicted enthalpy of reaction
20 at 20°C of 63.6 kJ/mol- H_2 and a predicted equilibrium pressure of 350°C at 1 bar.

[0067] The hydrogen storage material preferably has a theoretical hydrogen content of greater than about 5 wt %, preferably greater than 7 wt %. In some embodiments, the hydrogen storage material has a theoretical
25 hydrogen content of greater than 9 wt %. As recognized by one of skill in the art, the theoretical yield is rarely observed empirically, and actual yields are often less than the predicted theoretical yield.

[0068] Also as appreciated by one of skill in the art, the hydrogen storage material may initially comprise the dehydrogenated products of the
30 above reactions, and may be subsequently hydrogenated, thereby cyclically releasing and storing hydrogen in accordance with the present invention. For

example, in one embodiment, the starting materials comprise LiH and MgB₂. The starting materials are exposed to hydrogen gas, where they transform to LiBH₄ and MgH₂ in a hydrogenated state, and are able to subsequently to reversibly release and absorb hydrogen, as previously described above.

5 **[0069]** In various embodiments of the present invention, a catalyst is employed to enhance the reaction kinetics. Such catalysts are well known to one of skill in the art. Catalysts that may be useful with the present invention, comprise an element from the following non-limiting list: Fe, Ni, Co, Pt, Pd, Sr, and compounds and mixtures thereof. Suitable catalyst compounds include
10 TiH₂, TiH_x, TiF₃, TiCl₂, TiCl₄, TiF₄, VCl₃, VF₃, VH_x. The catalyst is generally added to either one of the hydrogen storage starting materials or to both of the hydrogen storage materials. The materials are preferably milled to achieve a desirable particle size and homogeneous mixing. However, the present invention also contemplates processing the catalyst by precipitation from
15 solution, vapor phase deposition, chemical transport, or sputter deposition, *inter alia*. Preferred catalyst concentrations in the hydrogen storage material system are from between about 0.1 to about 10 atomic %.

[0070] In certain embodiments, the present invention provides a method of reversibly storing hydrogen where hydrogen is released from starting
20 materials while in the presence of a hydrogen. In such embodiments, the hydrogen generation reaction, which occurs between a stable hydride and a destabilizing hydride under a hydrogen atmosphere, is substantially reversible at industrially practicable pressure and temperature conditions. Thus, in certain embodiments, the reacting of a stable hydride and a destabilizing hydride to
25 release hydrogen is conducted in a hydrogen atmosphere comprising substantially all hydrogen gas (the hydrogen gas may contain a small level of impurities that do not detrimentally impact the reaction), one or more of the reaction products formed in the reaction are capable of re-forming the starting materials upon exposure to hydrogen (*i.e.*, the dehydrogenation reaction is
30 reversible). In certain embodiments, the minimum hydrogen pressure of the hydrogen atmosphere is at least about 10 atm (approximately about 1000 kPa), more particularly at least about 8 atm (approximately about 800 kPa); at least about 6 atm (approximately about 600 kPa); at least about 5 atm (approximately

about 500 kPa); at least about 4 atm (approximately about 400 kPa); at least about 3 atm (approximately about 300 kPa); at least about 2 atm (approximately about 200 kPa); and at least about 1 atm (approximately about 100 kPa). An example of an embodiment where the reversible hydrogen release reaction is preferably conducted in the presence of a hydrogen atmosphere is where a stable hydride is lithium borohydride (LiBH_4) and a destabilizing hydride is magnesium hydride (MgH_2). A hydrogen atmosphere appears to facilitate the formation of the more readily reversible products LiH and MgB_2 (in addition to hydrogen), rather than the alternative products of Mg and B metals, as will be described further in Example 3 below.

EXAMPLE 1

[0071] In a first experiment conducted according to a method of making a hydrogen storage compound according to one preferred embodiment of the present invention, a mixture of LiBH_4 and MgH_2 is prepared having a molar ratio of 2:1 that reacts according to the above described chemical reaction formula. The LiBH_4 is commercially available from Lancaster Synthesis, Inc. of Windham, New Hampshire (and is specified to be $\geq 95\%$ purity) and the MgH_2 is commercially available at 95% purity from Gelest. The starting powders are mixed in the molar ratio 2 LiBH_4 : 1 MgH_2 with 2 mole percent of a catalyst (TiCl_3) added during milling. The starting materials weigh 1.2 grams and are added and sealed into a 80 cm^3 hardened steel ball mill vessel under an argon (Ar) inert atmosphere. Thirty chrome-steel mill balls having a 7 mm diameter are placed in the vessel with the powder prior to sealing. The material is then high-energy ball milled for at least one hour in a Fritsch Pulversette 6 planetary mill at 400 rpm. The average particle size diameter of the compound(s) remaining in the mill are preferred to be approximately $5 \mu\text{m}$ to about $15 \mu\text{m}$.

[0072] Figure 2 shows a volumetric analysis obtained with a mass spectrometer monitoring the exhaust gas from the Sievert's apparatus. Figure 2 shows hydrogen release by weight loss as a function of time for a sample of the milled hydrogen storage composition comprising LiBH_4 and MgH_2 prepared in accordance with Example 1. Figure 2 also depicts a plot of the hydrogen release by weight loss as a function of time for a sample of milled LiBH_4

prepared in accordance with the procedure described above, however without any destabilizing hydride (e.g., MgH_2). The LiBH_4 has a TiCl_3 catalyst added, as well. Each sample is continuously heated at a rate of 2°C per minute up to 450°C (represented by the dashed line). Curve "a" represents the hydrogen storage material of the present invention having the LiBH_4 and MgH_2 , as where curve "b" represents LiBH_4 alone in accordance with the prior art. Although the behavior of the LiBH_4 and MgH_2 hydrogen storage material is complex, nearly 10 wt % of hydrogen is generated from the hydrogen storage material (the wt % of the catalyst is not included). In comparison, the LiBH_4 only produces less than 8 wt % hydrogen (not including the catalyst). Thus, the hydrogen storage material prepared in accordance with the present invention demonstrates improved hydrogen release over the prior art.

[0073] Similarly, Figure 3 shows hydrogen absorption behavior of the dehydrogenated mixture of the sample prepared in accordance with Example 1. A dehydrogenated sample of pure LiBH_4 with 0.1 TiCl_3 catalyst is also provided for comparison. For the Example 1 sample, the LiBH_4 and MgH_2 is heated at 2°C per minute up to a temperature of 300°C where it is held constant. The prior art sample of LiBH_4 is heated at a rate of 2°C per minute up to a temperature of 400°C where it is held. As can be observed from Figure 3, at 300°C , the LiBH_4 and MgH_2 mixture represented by curve "a" absorbs greater than 8 wt % hydrogen. In contrast, even at 400°C , the pure LiBH_4 represented by curve "b" absorbs less than 4 weight % hydrogen. Thus, at lower temperatures, the LiBH_4 and MgH_2 mixture of the present invention having a stable hydride and a destabilizing hydride demonstrates good hydrogen absorption at lower temperatures, as compared to the prior art stable hydride alone.

[0074] Figure 4 shows an x-ray diffraction pattern of a sample prepared in accordance with Example 1. In Figure 4, "LB" represents LiBH_4 , "MH" represents MgH_2 , "MB" represents, MgB_2 , and "LC" represents LiCl_3 . Curve "a" is taken after mechanical milling of LiBH_4 and MgH_2 together and shows that milling produces a physical mixture with no reaction products between the stable hydride and destabilizing hydride. However, as can be seen, a small concentration of lithium chloride is produced from a reaction of

TiCl₃ with LiBH₄ which may occur during milling. No diffraction from any species containing Ti was observed. After dehydrogenation occurs (represented by curve "b") the byproducts MgB₂ and LiH are produced. After rehydrogenation (represented by curve "c") the pattern at 350° C shows where
5 LiBH₄ and MgH₂ reform while the diffraction peaks from LiCl disappear. The quartet of peaks around 25° two theta together with the peak at 18° distinctly identify LiBH₄ and demonstrate its reversible formation. This data confirms that the LiBH₄/MgH₂ hydrogen storage material system is reversible.

10 EXAMPLE 2

[0075] In a second experiment, approximately 1.2 g mixtures of LiH + ½ MgB₂ (the reaction products) + 0.03 TiCl₃ (catalyst) were mechanically milled for 1 hr as described previously in the first experiment.

[0076] Figure 5 shows hydrogenation and dehydrogenation of a
15 sample prepared in accordance with Example 2. The temperature ramp dehydrogenation/hydrogenation and isotherm measurements are performed in two custom Sieverts' apparatus. The system was pumped using an oilfree pumping station (the Tribodyn 100/120-HVP model available from Danielson Associates). The pressure at the sample is measured by replacing the sample
20 container with an ionization gauge. After pumping overnight, a pressure of 1x10⁻⁶ Torr (1.3 x 10⁻⁴ Pa) can be obtained. Hydrogen pressures are measured using low-range (0-100 psia or approximately 7.0 x 10² kPa) and high-range (0-3000 psia or approximately 2.1 x 10⁴ kPa) capacitance manometers at selected temperatures over the range from 75° to 575° C.

[0077] During heating at 2°C/min, hydrogen uptake from an initial
25 hydrogen pressure of 100 bar, begins at 230° to 250° C. For the initial cycle, hydrogenation is relatively slow, with a hydrogen uptake of 2.5 wt % hydrogen after 2 hr at 300° C. Upon heating to 350° C additional hydrogen uptake occurs reaching > 9 wt %. On the second and third cycles, the uptake is faster and 9
30 wt % uptake occurs in approximately 2 hr at 300° C. Desorption, into an initially evacuated volume, begins at about 270°C. Two desorption steps appear at 270° to 340° C and 380° to 440° C, respectively. Upon heating to 450° C desorption of 8 wt % hydrogen is obtained. The desorption kinetics for the first

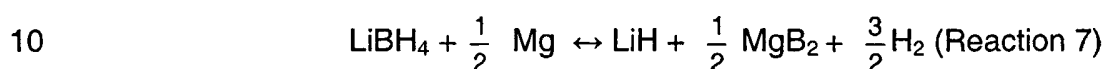
two cycles are nearly identical. Final pressures of 5 to 6 bar may be limited by equilibrium (see Figure 6 below). Mass spectrometric analysis of the desorbed gas using a residual gas analyzer (RGA) attached to the Sieverts apparatus showed only hydrogen released, although the effluent may contain low concentrations of species such as B_2H_6 or HCl .

[0078] Absorption and desorption isotherms for the sample prepared in accordance with Example 2 are shown in Figure 6. Isotherm measurements are performed manually in the same Sieverts apparatus used for the temperature ramp experiments. Absorption isotherms are shown between 315°C and 450°C (specifically at 330°C, 363°C, 400°C, and 450°C) and a desorption isotherm is shown at 400° C. The isotherms show sloping plateaus from 2 to 8 wt % with capacities of approximately 10 wt %. Equilibrium pressures vary from 4.5 bar at 315° C to 19 bar at 450° C. Absorption and desorption isotherms obtained at 400° C display a hysteresis of 2 to 3 bar.

[0079] Figure 7 is a preliminary van't Hoff plot (logarithm of the equilibrium pressure versus the inverse of the absolute temperature) using absorption equilibrium pressures at 4 wt % (see Figure 6). Curve "a" of Figure 7 shows equilibrium pressures obtained from absorption isotherms at 4 wt %. From 315°C to 400°C the behavior is linear with a dehydrogenation enthalpy of 40.5 kJ/mol- H_2 , an equilibrium pressure of 1 bar at 225°C, and an entropy of 81.3 kJ/K-mol- H_2 . At 450° C ($1000/T = 1.38$) the equilibrium pressure is lower than the pressure predicted based on an extrapolation of the linear behavior at lower temperatures.

[0080] In Figure 7, curve "b" shows an estimate of the behavior for dehydrogenation of $LiBH_4$ to $LiH + B$. Curve "c" shows equilibrium pressures for MgH_2/Mg obtained from the IEA/DOE/SNL database. The enthalpy for the $LiBH_4/ LiH + B$, system is estimated to be + 67 kJ/mol- H_2 . Compared with pure $LiBH_4$, the hydrogenation/dehydrogenation enthalpy for the $LiBH_4 + \frac{1}{2} MgH_2$ system is lower by 25 kJ/mol- H_2 and at 400° C the equilibrium pressure is increased from approximately 1 to 12 bar. Alternatively, extrapolating the linear behavior gives a temperature of 225° C for an equilibrium hydrogen pressure of 1 bar. Overall, the equilibrium pressure indicates that addition of MgH_2 significantly destabilizes $LiBH_4$ for hydrogen storage.

[0081] The equilibrium pressure behavior for the $\text{LiBH}_4 + \frac{1}{2} \text{MgH}_2$ system crosses the curve for MgH_2/Mg at approximately 360°C ($1000/T = 1.57$). It appears that at temperatures below 360°C the equilibrium pressures are greater than those for pure MgH_2 . Thus, in addition to LiBH_4 , the MgH_2 is also destabilized. In this region the combined LiBH_4 and MgH_2 system has equilibrium pressures higher than either individual component. Above 360°C the equilibrium pressures, obtained from the isotherms at 4 wt %, are below the equilibrium pressures for MgH_2/Mg . Under these conditions, it is believed that the system reacts in an alternate reaction mechanism:



[0082] Because hydrogenation of Mg is exothermic, the enthalpy for the alternate reaction (Reaction 7) should be less than the enthalpy for the reaction designated as Reaction 1 previously described above for the dehydrogenation reaction of $\text{LiBH}_4 + \frac{1}{2} \text{MgH}_2$. Consequently, the variation of equilibrium pressure with temperature should display a lower enthalpy, i.e., a lower slope, above approximately 360°C . The measured equilibrium pressure at 450°C is lower than the pressure extrapolated from lower temperatures. While not wishing to be bound by any particular theory, it is believed that this data point may indicate a transition from Reaction 1 at temperatures below about 360°C to the alternate reaction (Reaction 7) at higher temperatures. Although two plateaus have not been observed in the isotherm data, the temperature ramp desorption measurements, show two desorption steps which likely correspond to dehydrogenation of MgH_2 followed by reaction of Mg with LiBH_4 to form MgB_2 . In accordance with one preferred embodiment of the present invention, the addition of MgH_2 to LiBH_4 yields a reversible, destabilized hydrogen storage material system with an actual hydrogen capacity of approximately 8 to 10 wt %. The hydrogenation/dehydrogenation enthalpy is reduced by 25 kJ/mol- H_2 , as compared with pure LiBH_4 and the temperature for an equilibrium pressure of 1 bar is estimated to be 225°C .

30

EXAMPLE 3

[0083] In a third experiment, a mixture of LiBH_4 and MgH_2 is prepared having a molar ratio of 2:1 with a TiCl_3 catalyst at 2 mole %, in the same manner

as that described in Example 1 above. The ball-milled samples are dehydrogenated under two different atmospheric conditions to demonstrate the effect of hydrogen atmosphere on reaction products.

[0084] Figure 8 shows x-ray diffraction (XRD) data for the two different dehydrogenation scenarios. Scan A shows an XRD for a material dehydrogenated by heating to 400°C under flowing hydrogen at a pressure of 5 atm (approximately 500 kPa). Scan A shows that the reaction products include MgB_2 , but no detectable quantities of Mg metal were produced. The sample in Scan B was dehydrogenated by heating to 400°C under a flowing argon atmosphere at 1 atm (100 kPa). The XRD pattern in Scan B shows that Mg metal was formed as a reaction product, but no detectable amounts of MgB_2 are formed. As such, in certain embodiments of the present invention, where it is desirable to have reversibility of the hydrogen generation reaction, it is preferable to conduct the dehydrogenation reaction of the stable hydride with the destabilizing hydride in the presence of hydrogen, preferably in a hydrogen atmosphere, to enable formation of reaction products that are capable of being readily regenerated by exposure to hydrogen gas (e.g., MgB_2 , rather than elemental Mg and B).

[0085] Thus, the hydrogen storage materials according to the present invention provide a stable reversible solid phase hydrogen storage composition material, which is especially advantageous in mobile fuel cell applications. The reaction to generate hydrogen is readily controlled by temperature and pressure, and the required energy input is significantly reduced to increase efficiency of the overall system, while the hydrogen storage capacity is substantially increased. The hydrogen storage material system according to the present invention provides a stable, safe, and energy efficient means to store hydrogen for prolonged periods while enabling both hydrogen release and reversible reaction at moderate conditions. The description of the invention is merely exemplary in nature and, thus, variations that do not depart from the gist of the invention are intended to be within the scope of the invention. Such variations are not to be regarded as a departure from the spirit and scope of the invention.

CLAIMS

What is claimed is:

1. A method of reversibly storing hydrogen at industrially practicable
5 temperature and pressure conditions, the method comprising
providing a mixture comprising a stable hydrogen storage hydride
and a destabilizing hydride, wherein said stable hydride is capable of releasing
hydrogen at a first energy level (E_1); and
reacting said stable hydride with said destabilizing hydride to
10 release hydrogen at a second energy level (E_2); wherein E_2 is less than E_1 , and
said reaction is substantially reversible at the industrially practicable pressure
and temperature conditions.
2. The method of claim 1 wherein said reacting is slightly
endothermic.
- 15 3. The method of claim 1 wherein E_2 is at least about 10 % less than
 E_1 .
4. The method of claim 1 wherein E_2 is at least about 20 % less than
 E_1 .
5. The method of claim 1 wherein E_2 is at least about 30 % less than
20 E_1 .
6. The method of claim 1 wherein the material releases greater than 7
weight % hydrogen.
7. The method of claim 1 wherein the material releases greater than 9
weight % hydrogen.
- 25 8. The method of claim 1 wherein said second energy level E_2 is
related to a free energy of less than about 10 and greater than 0 kJ/mol- H_2 .
9. The method of claim 1 wherein said destabilizing hydride is
capable of releasing hydrogen in the absence of said stable hydride at a third
energy level E_3 , and wherein said second energy level E_2 is less than said third
30 energy level E_3 .
10. The method of claim 1 wherein said first energy level E_1 is related
to a first temperature that is greater than about 250°C required to release
hydrogen at a pressure of 1 bar, and said second energy level E_2 is related to a

second temperature that is less than about 250°C required to release hydrogen at a pressure of 1 bar.

11. The method of claim 10 wherein said second temperature is less than about 200°C.

5 12. The method of claim 10 wherein said second temperature is less than about 175°C.

13. The method of claim 1 wherein said first energy level E_1 is related to a first equilibrium pressure that is less than 1 bar at a temperature of 400°C, and said second energy level E_2 is related to a second equilibrium pressure
10 temperature that is greater than about 10 bar at a temperature of about 400°C.

14. The method of claim 1 wherein said mixture comprises a plurality of stable hydrides.

15. The method of claim 1 wherein said mixture comprises a plurality of destabilizing hydrides.

15 16. The method of claim 1 wherein said mixture further comprises a destabilizing compound different from said destabilizing hydride, wherein said destabilizing compound promotes release of hydrogen from the hydrogen storage material at a reduced energy level from said first energy level (E_1).

17. The method of claim 1 wherein prior to said reacting, reducing said
20 stable hydride and said destabilizing hydride to a respective average particle diameter size of less than about 25 μm .

18. The method of claim 1 wherein prior to said reacting, reducing said stable hydride and said destabilizing hydride to a respective average particle diameter size of less than about 15 μm .

25 19. The method of claim 1 wherein said mixture further comprises one or more catalysts.

20. The method of claim 1 wherein said reacting is conducted in a hydrogen atmosphere.

21. The method of claim 20 wherein said hydrogen atmosphere has a
30 hydrogen pressure of greater than or equal to 2 atmospheres (200 kPa).

22. The method of claim 20 wherein said hydrogen atmosphere has a hydrogen pressure of greater than or equal to 5 atmospheres (500 kPa).

23. A method of reversibly storing hydrogen at industrially practicable pressure and temperature conditions, the method comprising

providing a mixture comprising a stable hydrogen storage hydride and a destabilizing hydride, wherein said stable hydride is capable of releasing hydrogen at a first energy level (E_1) and is represented by the nominal general formula AH_x , wherein A comprises an element selected from Groups 13 or 15 of the Periodic Table, and said destabilizing hydride is represented by the nominal general formula MH_y ; and

reacting said stable hydride with said destabilizing hydride to release hydrogen at a second energy level (E_2); wherein E_2 is less than E_1 and where said reacting occurs by the following reaction:



wherein M is one or more cationic species that are distinct from A, and n, m, x, and y are selected so as to maintain electroneutrality and said reaction is substantially reversible at the industrially practicable pressure and temperature conditions.

24. The method of claim 23 wherein said stable hydride is represented by the nominal general formula AH_x , wherein A comprises an element selected from Groups 13 or 15 of the Periodic Table, said destabilizing hydrogen storage hydride material represented by the nominal general formula MH_y , wherein said reacting occurs by the following reversible reaction:



wherein M is one or more cationic species that are distinct from A, and n, m, c, d, x, and y are selected so as to maintain electroneutrality.

25. A method of reversibly storing hydrogen at industrially practicable temperature and pressure conditions, the method comprising

providing a mixture comprising a stable hydrogen storage hydride and a destabilizing hydride, wherein said stable hydride is capable of releasing hydrogen at a first energy level (E_1); and

reacting said stable hydride with said destabilizing hydride to release hydrogen at a second energy level (E_2); wherein E_2 is less than E_1 and E_2 is related to a free energy of less than about 10 and greater than 0 kJ/mol- H_2 ,

and said reaction is substantially reversible at the industrially practicable pressure and temperature conditions.

26. The method of claim 25 wherein said first energy level E_1 is related to a first temperature that is greater than about 250°C required to release
5 hydrogen at a pressure of 1 bar, and said second energy level E_2 is related to a second temperature that is less than about 250°C required to release hydrogen at a pressure of 1 bar.

27. A reversible hydrogen storage material comprising:
a stable hydrogen storage hydride represented by the nominal
10 general formula AH_x and a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y , wherein A is a cationic species that comprises boron, M is a cationic species that contains one or more cationic species distinct from those in A, x and y are selected so as to maintain electroneutrality, wherein said stable hydride is capable of releasing hydrogen at
15 a first energy level and wherein said stable hydride in the presence of said destabilizing hydride releases hydrogen at a second energy level, and said second energy level is significantly reduced from said first energy level.

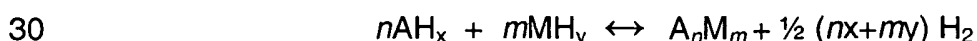
28. The material of claim 27 wherein the material releases greater than
20 7 weight % hydrogen.

29. The material of claim 27 wherein said second energy level is at
least about 10 % less than said first energy level.

30. The material of claim 27 further comprising a plurality of at least one of said stable hydrides or said destabilizing hydrides.

31. The material of claim 27 further comprising a destabilizing
25 compound different from said destabilizing hydride, wherein said destabilizing compound promotes release of hydrogen from said stable hydride at a reduced energy level from said first energy level.

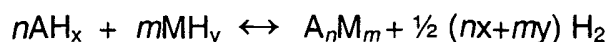
32. The material of claim 27 wherein the material releases hydrogen by the following reversible reaction:



wherein n, m, x, and y are selected so as to maintain electroneutrality

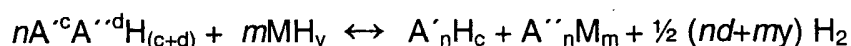
33. The material of claim 32 wherein said reaction occurs in a hydrogen atmosphere.

34. The material of claim 27 wherein the material releases hydrogen by the following reversible reaction:



wherein A comprises one or more elements selected from the group consisting of: lithium (Li), sodium (Na), potassium (K), beryllium (Be), magnesium (Mg), calcium (Ca), and mixtures thereof, wherein M comprises one or more elements selected from the group consisting of: aluminum (Al), arsenic (As), boron (B), barium (Ba), beryllium (Be), calcium (Ca), cadmium (Cd), cerium (Ce), cesium (Cs), copper (Cu), europium (Eu), iron (Fe), gallium (Ga), gadolinium (Gd), germanium (Ge), hafnium (Hf), mercury (Hg), indium (In), potassium (K), lanthanum (La), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), neodymium (Nd), nickel (Ni), lead (Pb), praseodymium (Pr), rubidium (Rb), antimony (Sb), scandium (Sc), selenium (Se), silicon (Si), samarium (Sm), tin (Sn), strontium (Sr), thorium (Th), titanium (Ti), thallium (Tl), vanadium (V), tungsten (W), yttrium (Y), ytterbium (Yb), zinc (Zn), and zirconium (Zr), methyl group (CH₃) and mixtures thereof, and n, m, x, and y are selected so as to maintain electroneutrality.

35. The material of claim 27 wherein said stable hydride is a complex stable hydride and the material releases hydrogen by the following reversible reaction:



wherein n, m, c, d, x, and y are selected so as to maintain electroneutrality.

36. The material of claim 27 wherein said stable hydride is a complex hydride and said destabilizing hydride is a binary hydride.

37. The material of claim 27 wherein said stable hydride is selected from the group of compounds consisting of: lithium borohydride (LiBH₄), lithium aluminum hydride (LiAlH₄), sodium borohydride (NaBH₄), sodium aluminum hydride (NaAlH₄), magnesium borohydride Mg(BH₄)₂, magnesium aluminum hydride Mg(AlH₄)₂, calcium borohydride Ca(BH₄)₂, calcium aluminum hydride Ca(AlH₄)₂, and mixtures thereof, and said destabilizing hydride is selected from the group of compounds consisting of: lithium hydride (LiH), sodium hydride (NaH), potassium hydride (KH), magnesium hydride (MgH₂), calcium hydride (CaH₂), lithium aluminum hydride (LiAlH₄), sodium borohydride (NaBH₄), lithium

borohydride (LiBH_4), magnesium borohydride $\text{Mg}(\text{BH}_4)_2$, sodium aluminum hydride (NaAlH_4), and mixtures thereof.

38. The material of claim 27 wherein said stable hydride is selected from the group consisting of lithium borohydride (LiBH_4), sodium borohydride (5 NaBH_4), magnesium borohydride ($\text{Mg}(\text{BH}_4)_2$), and mixtures thereof, and said destabilizing hydride is selected from the group consisting of lithium hydride (LiH), magnesium hydride (MgH_2), sodium hydride (NaH), and mixtures thereof.

39. The material of claim 27 further comprising one or more catalysts.

40. A reversible hydrogen storage material comprising:
10 a stable hydrogen storage hydride represented by the nominal general formula AH_x , wherein A comprises at least one element selected from Groups 13 or 15 of the Periodic Table; and

a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y , wherein M is one or more cationic species that are
15 distinct from A, wherein x and y are selected so as to maintain electroneutrality, and wherein said stable hydride is capable of releasing hydrogen at a first energy level and said stable hydride in the presence of said destabilizing hydride releases hydrogen at a second energy level, where said second energy level is significantly reduced from said first energy level.

20 41. The material of claim 40 wherein said second energy level is at least about 10 % less than said first energy level.

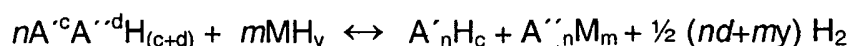
42. The material of claim 40 wherein the material releases hydrogen by the following reversible reaction:



25 wherein n, m, x, and y are selected so as to maintain electroneutrality.

43. The material of claim 42 wherein said reversible reaction occurs in a hydrogen atmosphere.

44. The material of claim 40 wherein said stable hydride is a complex hydride cationic species and said material release hydrogen by the following
30 reversible reaction:



wherein n, m, c, d, x, and y are selected so as to maintain electroneutrality.

45. The material of claim 40 wherein A further comprises at least one element selected from Groups 1 and 2 of the Periodic Table, or mixtures thereof.

46. The material of claim 40 wherein A further comprises at least one transition metal element selected from Groups 3 through 12 of the Periodic Table.

47. The material of claim 40 wherein A comprises one or more elements selected from the group consisting of: boron (B), aluminum (Al), lithium (Li), sodium (Na), potassium (K), beryllium (Be), magnesium (Mg), calcium (Ca), and mixtures thereof, and wherein M comprises one or more elements selected from the group consisting of: aluminum (Al), arsenic (As), boron (B), barium (Ba), beryllium (Be), calcium (Ca), cadmium (Cd), cerium (Ce), cesium (Cs), copper (Cu), europium (Eu), iron (Fe), gallium (Ga), gadolinium (Gd), germanium (Ge), hafnium (Hf), mercury (Hg), indium (In), potassium (K), lanthanum (La), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), neodymium (Nd), nickel (Ni), lead (Pb), praseodymium (Pr), rubidium (Rb), antimony (Sb), scandium (Sc), selenium (Se), silicon (Si), samarium (Sm), tin (Sn), strontium (Sr), thorium (Th), titanium (Ti), thallium (Tl), vanadium (V), tungsten (W), yttrium (Y), ytterbium (Yb), zinc (Zn), and zirconium (Zr), methyl group (CH₃) and mixtures thereof.

48. The material of claim 40 wherein A comprises boron (B).

49. The material of claim 40 wherein said stable hydride is selected from the group of compounds consisting of: lithium borohydride (LiBH₄), lithium aluminum hydride (LiAlH₄), sodium borohydride (NaBH₄), sodium aluminum hydride (NaAlH₄), magnesium borohydride Mg(BH₄)₂, magnesium aluminum hydride Mg(AlH₄)₂, calcium borohydride Ca(BH₄)₂, calcium aluminum hydride Ca(AlH₄)₂, and mixtures thereof, and said destabilizing hydride is selected from the group of compounds consisting of: lithium hydride (LiH), sodium hydride (NaH), potassium hydride (KH), magnesium hydride (MgH₂), calcium hydride (CaH₂), lithium aluminum hydride (LiAlH₄), sodium borohydride (NaBH₄), lithium borohydride (LiBH₄), magnesium borohydride Mg(BH₄)₂, sodium aluminum hydride (NaAlH₄), and mixtures thereof.

50. The material of claim 40 wherein said stable hydride is selected from the group consisting of lithium borohydride (LiBH₄), sodium borohydride

(NaBH_4), magnesium borohydride ($\text{Mg}(\text{BH}_4)_2$), and mixtures thereof, and said destabilizing hydride is selected from the group consisting of magnesium hydride (MgH_2), lithium hydride (LiH), sodium hydride (NaH), and mixtures thereof.

51. A reversible hydrogen storage material comprising:

5 a stable hydrogen storage hydride represented by the nominal general formula AH_x and a destabilizing hydrogen storage hydride represented by the nominal general formula MH_y , wherein A is a cationic species that comprises one or more elements selected from the group consisting of: lithium (Li), sodium (Na), potassium (K), beryllium (Be), magnesium (Mg), calcium (Ca),
10 and mixtures thereof, M is a cationic species that contains one or more cationic species distinct from those in A and is selected from the group consisting of aluminum (Al), arsenic (As), boron (B), barium (Ba), beryllium (Be), calcium (Ca), cadmium (Cd), cerium (Ce), cesium (Cs), copper (Cu), europium (Eu), iron (Fe), gallium (Ga), gadolinium (Gd), germanium (Ge), hafnium (Hf), mercury (Hg),
15 indium (In), potassium (K), lanthanum (La), lithium (Li), magnesium (Mg), manganese (Mn), sodium (Na), neodymium (Nd), nickel (Ni), lead (Pb), praseodymium (Pr), rubidium (Rb), antimony (Sb), scandium (Sc), selenium (Se), silicon (Si), samarium (Sm), tin (Sn), strontium (Sr), thorium (Th), titanium (Ti), thallium (Tl), vanadium (V), tungsten (W), yttrium (Y), ytterbium (Yb), zinc (Zn), and zirconium (Zr), methyl group (CH_3) and mixtures thereof, and x and y are selected so as to maintain electroneutrality,

wherein said stable hydride is capable of releasing hydrogen at a first energy level and wherein said stable hydride in the presence of said destabilizing hydride releases hydrogen at a second energy level, and said
25 second energy level is at least about 10 % less than said first energy level.

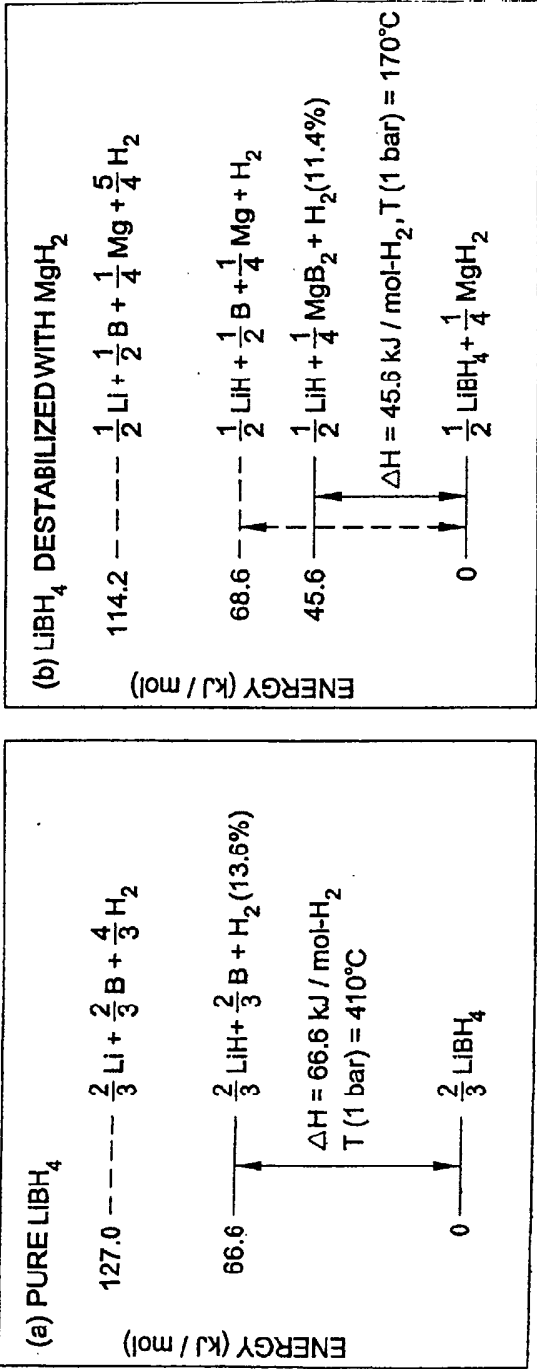


FIG 1A

FIG 1B

2/7

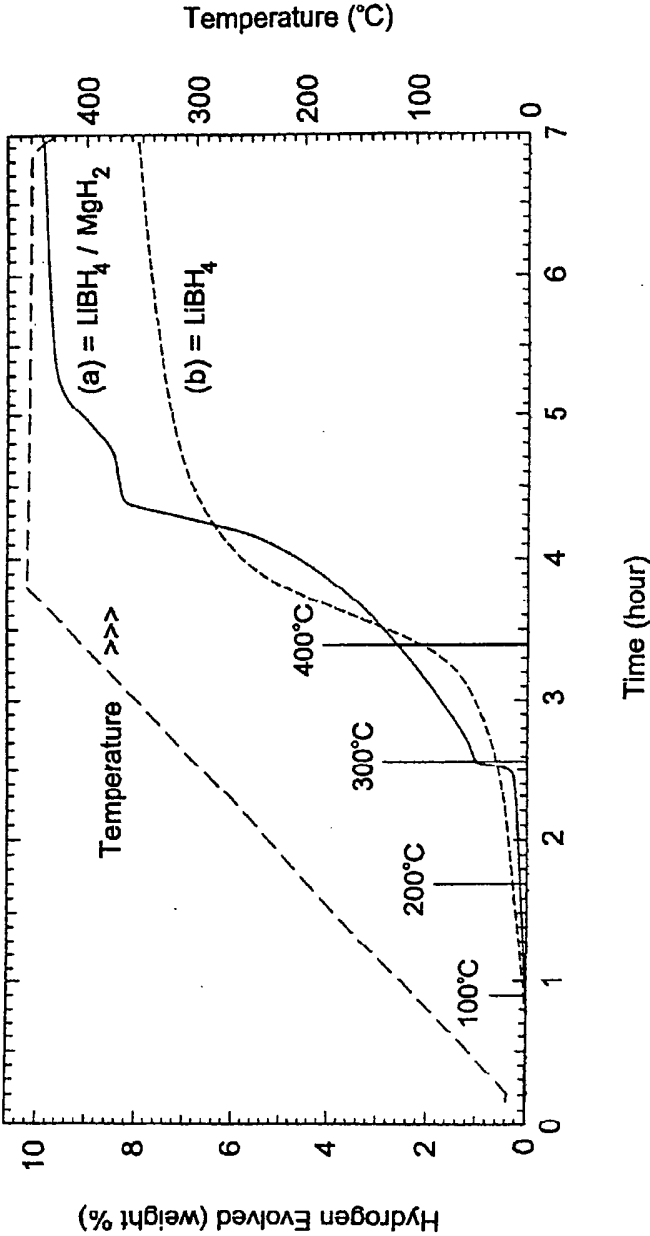


FIG 2

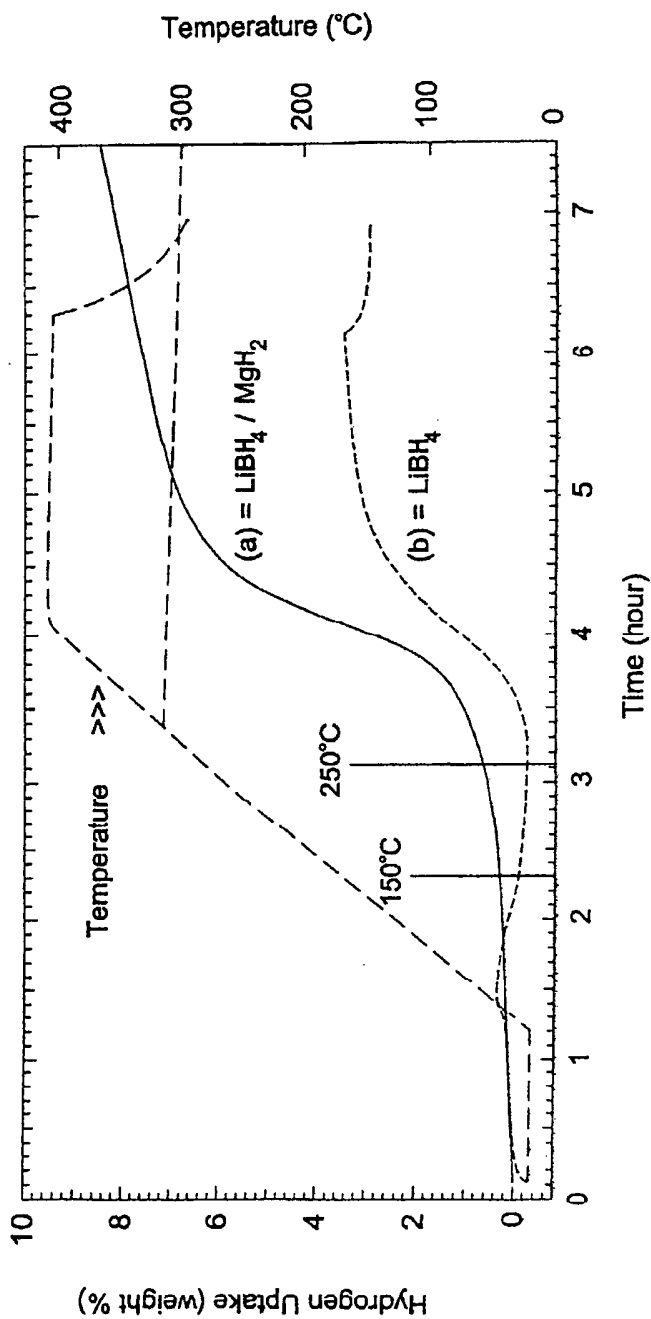


FIG 3

4/7

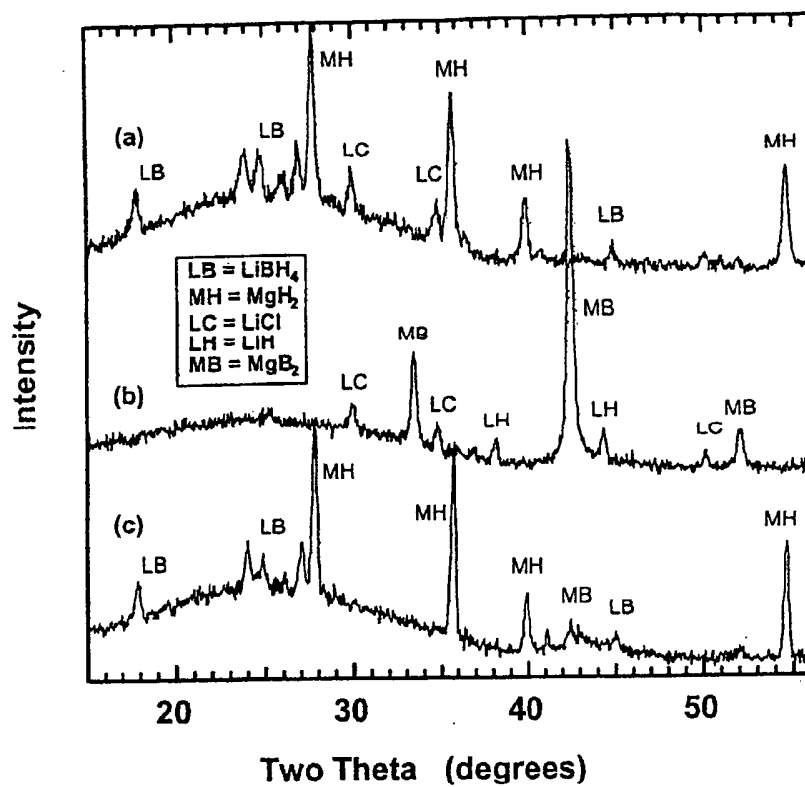


FIG. 4

5/7

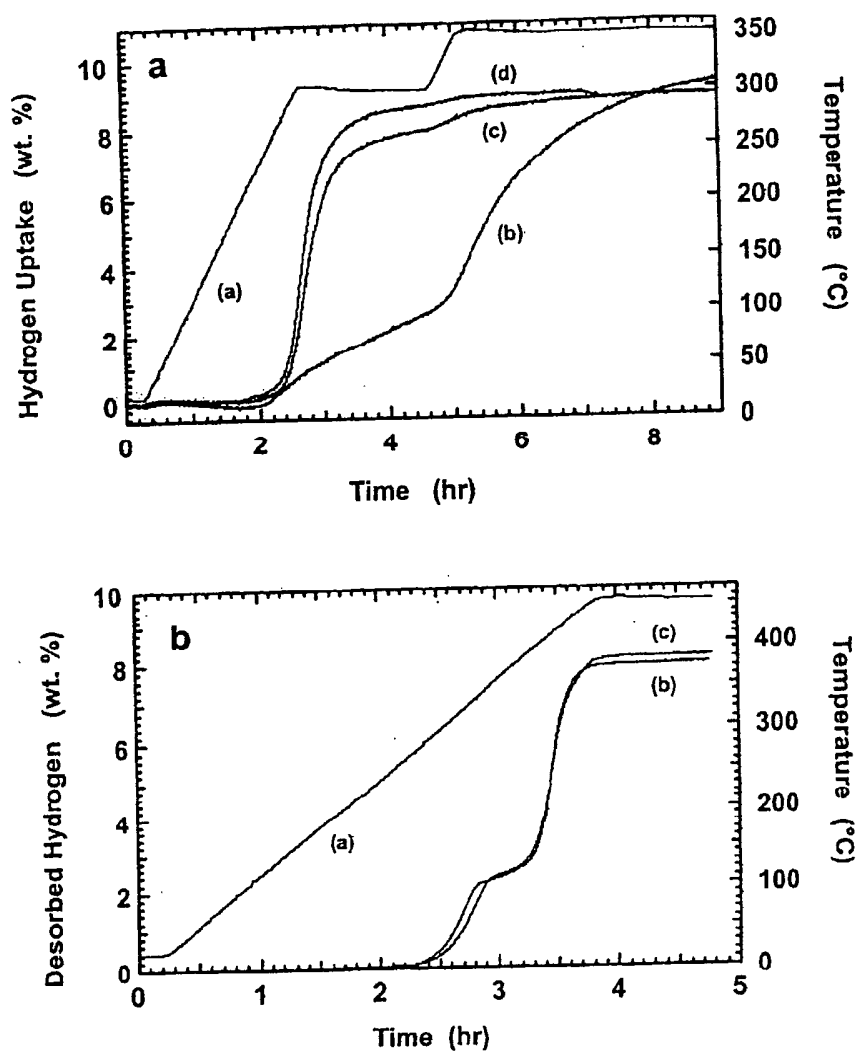


FIG. 5

6/7

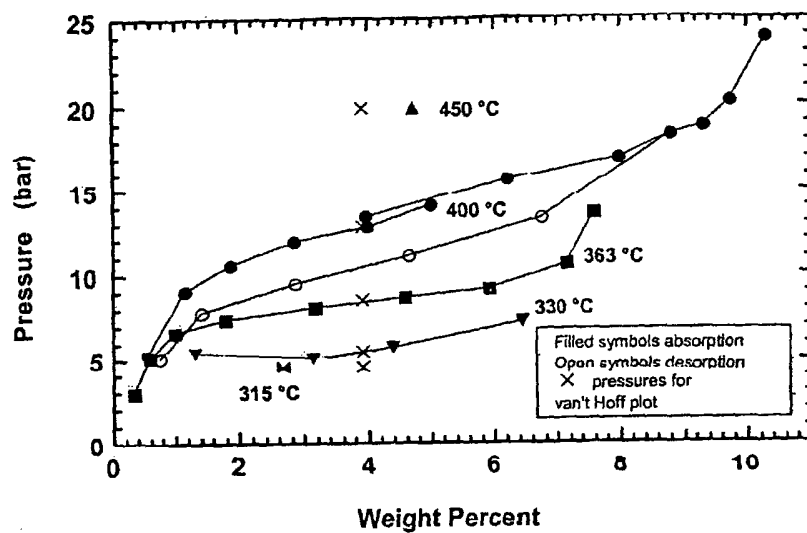


FIG. 6

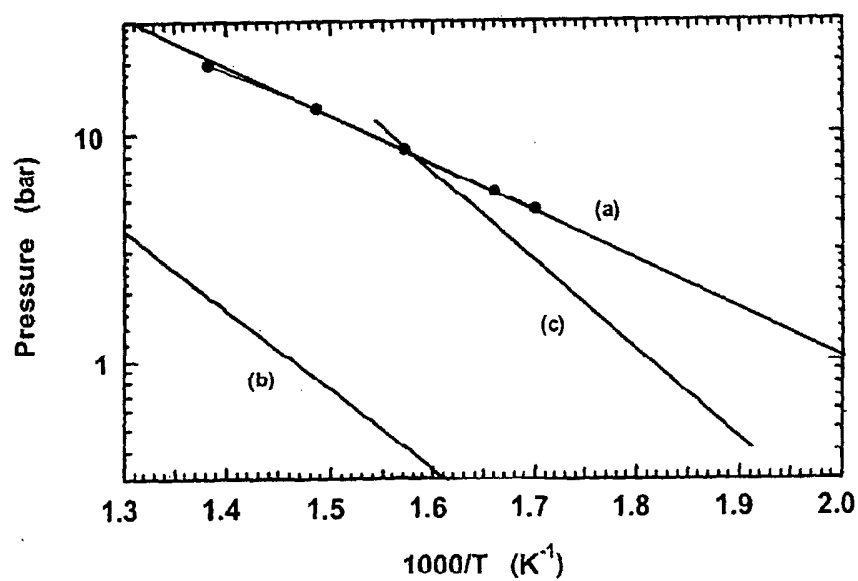


FIG. 7

