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(54) Title: PROCESS FOR REMOVING SULPHUR COMPOUNDS INCLUDING HYDROGEN SULPHIDE AND
MERCAPTANS FROM GAS STREAMS

(57) **Abrégé/Abstract:**

The invention concerns a process for the removal of hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide from a gas stream comprising hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide, by removing in a first step most of the hydrogen sulphide, part of the, mercaptans and optionally part or most of the carbon dioxide and carbonyl sulphide by washing the gas stream with an aqueous washing solution comprising 10 to 40 wt% based on total solution of water, 10 to 45 wt% based on total solution of a physical solvent and 20 to 60 wt% based on total solution of an amine, which first removal step is followed by a second removal step in which mercaptans are removed by means of molecular sieves, in which process the amount of mercaptans which is removed by the aqueous washing stream is between 60 and 96 wt% (of total removed mercaptans in steps one and two), and the amount which is removed by the mol sieves is between 40 and 4 wt% (of total removed mercaptans in step one and two).

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PROCESS FOR REMOVING SULPHUR COMPOUNDS INCLUDING HYDROGEN SULPHIDE AND MERCAPTANS FROM GAS STREAMS

The present invention relates to a process for the removal of hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide from a gas stream containing these compounds.

5 The removal of sulphur-containing compounds from gas streams comprising such compounds has always been of considerable importance in the past and is even more so today in view of continuously tightening environmental regulations. This holds for combustion gases as obtained
10 in the combustion of organic compounds as coal, as well as for natural gas streams to be used for e.g. the preparation of synthesis gas and for residential use or to be transported as liquid natural gas.

 Sulphur contaminants in natural gas streams include
15 hydrogen sulphide and mercaptans. Mercaptans, due to their odorous nature, can be detected at parts per million concentration levels. Thus, it is desirable for users of natural gas to have concentrations of mercaptans lowered to e.g. less than 5, or even less than 2 ppmv,
20 and total concentration of sulphur compounds to e.g. less than 30 or, preferably, less than 20 ppmv, e.g. 15 or 10 ppmv. Sales gas specifications often mention total sulphur concentrations less than 4 ppmv.

 Numerous natural gas wells produce what is called
25 "sour gas", i.e. natural gas containing hydrogen sulphide, often in combination with mercaptans, the total amount of sulphur compounds being present in concentrations that makes the natural gas unsuitable for direct use. Considerable effort has been spent to find

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effective and cost-efficient means to remove these
undesired compounds. In addition, the natural gas may
also contain varying amounts of carbon dioxide and
carbonyl sulphide, which depending on the use of the
5 natural gas often have to be removed at least partly.

A number of processes are known for the removal of
sulphur compounds and optionally carbon dioxide and
carbonyl sulphide from gas streams as natural gas. These
processes are based on physical and/or chemical
10 absorption, solid bed adsorption and/or chemical
reaction. Physical and/or chemical absorption processes
suffer from the fact that they frequently encounter
difficulties in reaching the low concentration of the
undesired sulphur compounds, unless (extremely) large
15 reactors are used. Solid bed adsorption processes suffer
from the fact that they are only able to adsorb limited
amounts of undesired compounds, while regeneration is
relatively cumbersome. Especially large solid beds take
relatively large amounts of time for regeneration and
20 disproportionately large amounts of regeneration gas is
needed. Chemical processes in general are able to remove
carbon dioxide and/or hydrogen sulphide without large
difficulties, however, they suffer from the fact that
they do not effectively remove mercaptans and often
25 produce large amounts of waste.

A special problem exist in processes in which
hydrogen sulphide has to be removed in combination with a
relatively high amount of mercaptans. Such processes have
been described in the literature. In US 4,957,715 a
30 process is described in which hydrogen sulphide, alkyl
mercaptans and carbon dioxide are removed from a gas
stream by using an adsorbent in a first step to remove
hydrogen sulphide and part of the mercaptans, followed by

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washing treatment in a second step to remove carbon dioxide and a further part of the mercaptans. Such a process, however, requires large amounts of (regenerable) adsorbents, especially when the amount of sulphur compounds in the feed gas is high. In US 5,700,438 a process is described to remove hydrogen sulphide and mercaptans from gas streams by contacting the stream with copper compounds. This, however, is an expensive and laborious process. In US 5,424,051 a process is described in which carbon dioxide, mercaptans and hydrogen sulphide are removed by first removing carbon dioxide by means of an adsorbent and removing in a second step carbon dioxide, hydrogen sulphide and mercaptans by means of alkaline scrubbing. This process is expensive and laborious. In US 4,311,680 a process is described for the removal of hydrogen sulphide and mercaptans by using an iron oxide fixed bed, followed by regeneration of the absorbent by reaction with hydrogen peroxide. Such a process needs large amounts of absorbents, while regeneration is expensive and laborious.

It has now been found that sulphur compounds, especially hydrogen sulphide in combination with mercaptans, and optionally carbon dioxide and carbonyl sulphide, may be removed from gas streams, especially natural gas streams, by a combined process, in which in a first step in a physical/chemical absorption process most of the hydrogen sulphide, at least a part of the carbon dioxide (if present) and a part of the mercaptans is removed, while in a second step in a solid adsorption step the remaining hydrogen sulphide and the remaining mercaptans and other sulphur compounds are removed.

The above process uses the well-proven physical/chemical absorption process. Such a process has

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been described in for instance GB 2,103,645 and
GB 2,103,646. Almost all hydrogen sulphide is removed
in a very efficient way. When necessary, also the
carbon dioxide which needs to be removed is removed in
5 this part of the process. As only part of the
mercaptans has to be removed in the first step, the
process avoids the use of very large and inefficient
reactors. In the second step a relatively small solid
adsorption bed can be used to remove the remaining part
10 of the mercaptans. This is due to the fact that almost
all hydrogen sulphide has already been removed in the
first step together with part of the mercaptans.
Regeneration of such a bed is not very laborious or
cumbersome. Thus, the above combination of sulphur
15 removal processes results in an overall efficient
removal of hydrogen sulphide, mercaptans and optionally
part of the carbon dioxide and carbonyl sulphide, while
avoiding the disadvantages of only one technology or
other technologies. In addition, treating the
20 regeneration gas of the solid bed adsorber in a
dedicated absorber optimises the process. The laden
solvent of the dedicated absorber is then regenerated
in the same regenerator as is used for the main
process.

25 It is observed that the use of a combined
physical/chemical absorbent rather than an aqueous
chemical absorbent only, also results in the
possibility of flashing any carbon dioxide at
relatively high pressures (i.e. between 5 and 15 bara).
30 This reduces re-compression requirements, e.g. for re-
injection.

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The present invention therefore provides a process for the removal of hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide from a gas stream comprising hydrogen sulphide and mercaptans, by removing in a first step most of the hydrogen sulphide and part of the mercaptans by washing the gas stream with an aqueous washing solution comprising 10 to 45 wt% based on total solution of water, 10 to 40 wt% based on total solution of a physical solvent and 20 to 60 wt% based on total solution of an amine, which first removal step is followed by a second removal step in which mercaptans are removed by means of molecular sieves, in which process the amount of mercaptans which is removed by the aqueous washing solution is between 60 and 96 % of total removed mercaptans in steps one and two, and the amount which is removed by the molecular sieves is between 40 and 4 % of total removed mercaptans in step one and two and in which gas stream the ratio between the amount of mercaptans expressed as ppmv and the amount of hydrogen sulphide expressed as vol% is at least 50.

The gas stream might also comprise carbon dioxide and carbonyl sulphide, which is then partly or mostly removed in the first step.

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The process is especially suitable for gas streams containing large amounts of hydrogen sulphide and, optionally large amounts of carbon dioxide, as both compounds are efficiently removed in the liquid
5 adsorption process. The process is especially suitable when the ratio mercaptan/hydrogen sulphide is high, and the gas stream after the first step contains a relatively high amount of mercaptans. The process is able to deal with the common mercaptans (especially C₁-
10 C₁₀ mercaptans, more especially C₁-C₄ mercaptans), also without any problems with methyl mercaptan, which is considered to be one of the most difficult mercaptans to be removed by means of adsorption technologies.

The feed gas for the process of the present
15 invention may contain low as well as high amounts of sulphur compounds and carbon dioxide. Suitably the total feed gas stream comprises 0.05 to 20 vol% hydrogen sulphide, 10 to 1500 ppmv mercaptans and
0 to 40 vol% carbon dioxide, preferably 0.1 to 5 vol%
20 hydrogen sulphide, 20 to 1000 ppmv mercaptans and 0 to 30 vol% carbon dioxide. In

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a special embodiment of the invention, the total gas stream comprises hydrogen sulphide in an amount between 0.15 and 1.0 vol%. The presence of these amounts of H₂S hinders the removal of mercaptans, since H₂S is preferentially adsorbed. Therefore, a gas stream comprising hydrogen sulphide in an amount between 0.15 and 1.0 vol% is regarded as a very difficult gas stream to remove all mercaptans from.

The process according to the invention is especially suitable for the removal of mercaptans from gas feed streams in which the ratio of mercaptans (expressed as ppmv) and the amount of hydrogen sulphide (expressed as vol%) is high. Due to this high ratio the gas stream after the first step will have a (relatively) high content of mercaptans. These mercaptans are adsorbed without problems in the second step. Thus, the process is preferably used for the purification of gas feed streams in which the ratio between the amount of mercaptans (expressed as ppmv) and the amount of hydrogen sulphide (expressed as vol%) is at least 50, more preferably at least 100, more preferably at least 200, still more preferably above 250.

Very suitably the feed gas stream is natural or associated gas, but also other gas streams can be treated, for instance hydrogen containing refinery streams, e.g. obtained after desulphurisation reaction, and syngas streams. Natural gas is a general term that is applied to mixtures of light hydrocarbons and optionally inert gases (nitrogen, carbon dioxide, helium) derived from natural gas wells. The main component of natural gas is methane. Further, often ethane, propane and butane are present. In some cases (small) amounts of higher hydrocarbons may be present, often indicated as natural

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gas liquids or condensates. When produced together with oil, the natural gas is usually called associated gas. Hydrogen sulphide, mercaptans, sulphides, disulphides, thiophenes and aromatic mercaptans may be present in natural gas in varying amounts.

The first step of the present invention appears to be very efficient to remove the hydrogen sulphide (and at least part of the carbon dioxide). By means of a washing process the feed gas stream is washed with a chemical solvent, an aqueous amine solution, and physical solvent. The use of aqueous amine solutions comprising a physical solvent for removing so-called acidic gases as hydrogen sulphide and optionally carbon dioxide and/or COS from a gas stream containing these compounds has been described long ago. See for instance A.L. Kohl and F.C. Riesenfeld, 1974, Gas Purification, 2nd edition, Gulf Publishing Co. Houston and R.N. Maddox, 1974, Gas and Liquid Sweetening, Campbell Petroleum Series.

On an industrial scale there are chiefly two categories of absorption solvents, depending on the mechanism to absorb the acidic components: chemical solvents and physical solvents. Each solvent has its own advantages and disadvantages as to features as loading capacity, kinetics, regenerability, selectivity, stability, corrosivity, heating/cooling requirements etc.

Chemical solvents which are useful in the process of the present invention are primary, secondary and/or tertiary amines derived alkanolamines, especially amines are derived from ethanolamine, especially monoethanol amine (MEA), diethanolamine (DEA), triethanolamine (TEA), diisopropanolamine (DIPA) and methyldiethanolamine (MDEA) or mixtures thereof.

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Physical solvents which are suitable in the process of the present invention are cyclo-tetramethylenesulfone and its derivatives, aliphatic acid amides, N-methyl-pyrrolidone, N-alkylated pyrrolidones and the
5 corresponding piperidones, methanol, ethanol and mixtures of dialkylethers of polyethylene glycols or mixtures thereof.

The mixed systems show good absorption capacity and good selectivity against moderate investment costs and
10 operational costs. They perform very well at high pressures, especially between 20 and 90 bara. Preferably in the hydrogen sulphide removal step between 90 and 100 wt% of the hydrogen sulphide based on total weight of hydrogen sulphide present in the gas stream is removed,
15 preferably between 95 and 100 wt%, especially hydrogen sulphide is removed till a level of less than 10 ppmv, more especially to a level of less than 5 ppmv.

The preferred physical solvent is sulfolane. The preferred amine is a secondary or tertiary amine,
20 preferably an amine compound derived from ethanol amine, more especially DIPA, DEA, MMEA (monomethyl-ethanolamine), MDEA, or DEMEA (diethyl-monoethanolamine), preferably DIPA or MDEA.

The aqueous washing solution comprises preferably 15
25 to 35 wt%, 20 to 40 wt% of a physical solvent and 40 to 55 wt% of an amine, based on total solution of water.

Very suitably the gas stream obtained in the first step is first cooled to a temperature between 5 and 45 °C, preferably between 10 and 35 °C, where after any
30 condensate is separated from the gas stream, followed by the second step.

In addition, the gas stream obtained in the first step is cooled by at least 10 °C, preferably 20 °C.

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Suitably the amount of mercaptans which is removed by the aqueous washing stream in the first step is between 70 and 93% (of removed mercaptans), preferably between 75 and 90%, and the amount which is removed by the mol
5 sieves is between 30 and 7% (of removed mercaptans), preferably between 25 and 10%.

In the first removal step at least 90 wt% of the hydrogen sulphide is removed (based on total amount of hydrogen sulphide present in the gas stream), preferably
10 95 wt%, more preferably 98 wt%.

The amount of mercaptans in the gas stream which is treated in the second step is between suitably 5 and 60 ppmv, preferably between 10 and 50 ppmv.

Suitably the first step of the invention is carried
15 out at a temperature of at least 20 °C, preferably between 25 and 90 °C, more preferably between 30 and 55 °C, at a pressure between 15 and 90 bara. In the second step preferably a crystalline molecular sieve is used, more preferably a sieve having an average pore
20 diameter of 5 ångström or more, especially between 6 and 13 ångström. The second step is suitably carried out at a temperature of 25 °C and a pressure between 15 and 90 bara. The regeneration of the mol sieve beds may be done with suitable inert gases. It is preferred to use a
25 hydrocarbon stream, especially a hydrocarbon stream which is obtained by a process according to the present invention. The regeneration gas containing the mercaptans of the second step is preferably remixed with the starting gas stream. Preferably a dedicated absorber is
30 used (similar to the absorber used in the main process).

The laden solvent of the dedicated absorber is regenerated in the same regenerator as is used in the main process.

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The process according to the present invention may be carried out in a continuous mode, preferably using a continuous regeneration process of the aqueous washing solution and two or more reactors comprising the mol
5 sieves. In the regeneration process the pressure of the laden washing solution is released, usually in one or two steps, followed by temperature increase. Preferably, the temperature increase is done in a stepwise mode. When using two or more mol sieve reactors, at least one
10 reactor will be in the adsorbing mode and at least one reactor will be in the desorption mode. Depending on the actual situation there may be a combination of two, three, four or even more reactors, one or more in absorbing mode, the others in different stages of
15 desorbing mode.

The second step of the present invention uses mol sieves. These mol sieves are commercially available.

Mol sieves comprise small zeolite particles dispersed in a binder, usually alumina. The zeolites comprise
20 preferably zeolite type A or zeolite type X.

Especially suitable in the process of the present invention is the use of an adsorbent in step two comprising at least two beds containing mol sieves, one bed comprising 3 or 4 Å pore diameter mol sieves removing
25 the water from the gas stream before it is treated in the second bed, the second bed containing mol sieves of 5 Å pore diameter or larger.

The mol sieves removing the water hardly adsorb any sulphur compounds. In general, the capacity of such mol
30 sieves is higher than larger pore diameter mol sieves. The amount of water to be removed in the small pore diameter mol sieves is preferably at least 60 wt% of the water present, preferably at least 90 wt%. Very suitably

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water is removed to a level of less than 1 wt% in the treated gas, preferably less than 100 ppmwt.

The second and further beds suitably contain mol sieves of 5 Å or more, to remove the sulphur compounds. In a further preferred embodiment at least two beds are used containing the wide pore diameter mol sieves, preferably one bed containing 5 Å mol sieves, the other bed containing mol sieves of pore diameter of 6 Å and larger, preferably 13 Å. The mol sieve having the pore diameter of 5 Å removes hydrogen sulphide (if present), methyl mercaptan and some ethyl mercaptan, while the second bed removes the remainder of the ethyl mercaptan and the higher mercaptans. It will be appreciated that the above indicated beds can be applied in one single vessel, or may be spread over two or more vessels. The advantage of using more than one vessel is that each vessel may be used and regenerated under the most optimal conditions.

The laden solvent obtained in the process of the invention contains hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide and may also contain appreciable amounts of dissolved non-acid components from the gas mixture to be purified, e.g. hydrocarbons, carbon monoxide and/or hydrogen. Suitably, the laden solvent is regenerated in a regenerator at relatively low pressure and high temperature. A lean solvent is obtained and a gas stream comprising hydrogen sulphide, mercaptans and optionally carbon dioxide and carbonyl sulphide. It may be advantageous to remove these non-acid components at least partially from the laden solvent by flashing to a pressure which is higher than the sum of the partial pressures belonging to the hydrogen sulphide and carbon dioxide present in the laden

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solvent. In this way only small amounts of hydrogen sulphide and carbon dioxide are released from the solvent together with the non acid compounds. In a second step the laden solvent is flashed to a pressure which is below the sum of the partial pressures of the hydrogen sulphide and carbon dioxide present in the laden solvent at the prevailing temperature, i.e. to a pressure usually between 1 and 5 bara. Flashing at atmospheric pressure is preferred. The temperature in the last flashing operation is suitably in the range of from 50 to 120 °C, preferably between 60 and 90 °C.

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CLAIMS:

1. A process for the removal of hydrogen sulphide and mercaptans from a gas stream comprising hydrogen sulphide and mercaptans, by removing in a first step most of the hydrogen sulphide and part of the mercaptans by washing the gas stream with an aqueous washing solution comprising 10 to 45 wt% based on total solution of water, 10 to 40 wt% based on total solution of a physical solvent and 20 to 60 wt% based on total solution of an amine, which first removal step is followed by a second removal step in which mercaptans are removed by means of molecular sieves, in which process the amount of mercaptans which is removed by the aqueous washing solution is between 60 and 96 % of total removed mercaptans in steps one and two, and the amount which is removed by the molecular sieves is between 40 and 4 % of total removed mercaptans in step one and two and in which gas stream the ratio between the amount of mercaptans expressed as ppmv and the amount of hydrogen sulphide expressed as vol% is at least 50.

2. A process according to claim 1, in which the gas stream also comprises carbon dioxide and carbonyl sulphide, which is partly or mostly removed in the first step.

3. A process according to claim 1 or 2, in which the total gas stream comprises 0.05 to 20 vol% hydrogen

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sulphide, 10 to 1500 ppmv mercaptans and 0 to 40 vol% carbon dioxide.

4. A process according to claim 3, in which the total gas stream comprises 0.1 to 5 vol% hydrogen sulphide, 20 to 1000 ppmv mercaptans and 0 to 30 vol% carbon dioxide.

5. A process according to claim 4, in which the total gas stream comprises hydrogen sulphide in an amount between 0.15 and 0.6 vol%.

6. A process according to any one of claims 1 to 5, in which the ratio between the amount of mercaptans expressed as ppmv and the amount of hydrogen sulphide expressed as vol% is at least 100.

7. A process according to claim 6, in which the ratio is at least 200.

8. A process according to any one of claims 1 to 7, in which the gas stream is natural or associated gas.

9. A process according to any one of claims 1 to 8, in which the physical solvent is sulfolane.

10. A process according to any one of claims 1 to 9, in which the amine is a secondary or tertiary amine, or a mixture thereof.

11. A process according to claim 10, in which the amine is an amine compound derived from ethanol amine or a mixture thereof.

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12. A process according to claim 11, in which the amine is DIPA or MDEA or a mixture thereof.

13. A process according to any one of claims 1 to 12, in which the aqueous washing solution comprises 20 to 35 wt% based on total solution of water, 20 to 35 wt% of a physical solvent and 40 to 55 wt% of an amine.

14. A process according to any one of claims 1 to 13, in which the gas stream obtained in the first step is cooled to a temperature between 5 and 45 °C, where after any condensate is separated from the gas stream.

15. A process according to claim 14, in which the temperature is between 10 and 35°C.

16. A process according to any one of claims 1 to 15, in which the first step is carried out at a temperature of at least 20 °C, and at a pressure between 15 and 90 bara.

17. A process according to claim 16, in which the temperature is between 25 and 90 °C.

18. A process according to claim 17, in which the temperature is between 30 and 55 °C.

19. A process according to any one of claims 1 to 18, in which in the second step a crystalline molecular sieve is used.

20. A process according to claim 19, in which the sieve has an average pore diameter of 5 ångström or more.

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21. A process according to claim 20, in which the sieve has an average pore diameter of about 6 ångström.

22. A process according to any one of claims 1 to 21, in which the second step is carried out at a temperature of 25 °C and a pressure between 15 and 90 bara.

23. A process according to any one of claims 1 to 22, in which a regeneration gas of the second step containing mercaptans is remixed with the gas stream comprising hydrogen sulphide and mercaptans or is treated in a dedicated absorber.