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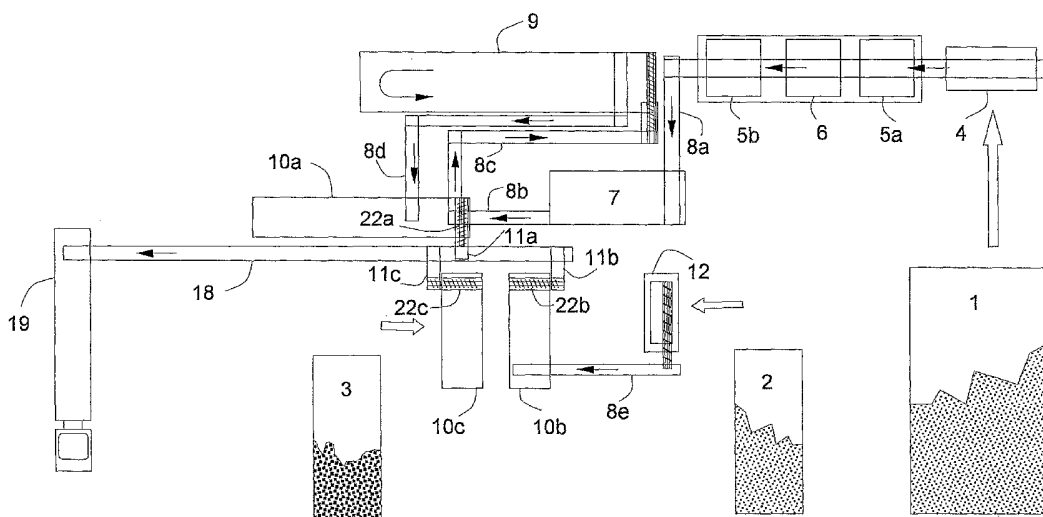
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(54) Title: PROCESS AND PLANT FOR PRODUCING A REFUSE DERIVED SOLID FUEL



(57) Abstract: Process and plant for producing a refuse derived solid fuel (RDSF), comprising a first component comprising a dry fraction of a solid urban waste (MSW) in a shredded form and at least one second component in a shredded form selected from an elastomeric material and a thermoplastic material, or mixtures thereof, wherein the dry fraction of the MSW, the elastomeric polymer material and/or the thermoplastic polymer material are stored in separate containers and when required are metered and fed in subsequent layers onto a continuous conveyor which discharges into a temporary accumulating container, for example the box body of a motor vehicle, intended to directly feed the combustion plant wherein the RDSF is burnt. In this way there is no need to pre-mix the various fractions of the RDSF during the production stage and to maintain the resulting mixture constantly stirred in order to prevent compaction and/or separation of fractions. In fact mixing between the various fractions only takes place at the end of the production process when the RDSF is placed in the temporary accumulation container which feeds the combustion plant.

WO 2005/093019 A1

“Process and plant for producing a refuse derived solid fuel”

DESCRIPTION

This invention relates to a plant and a method for preparing a refuse derived solid fuel (RDSF).

5 EP-A-0 930 353 discloses a solid fuel composition having a bulk density of less than 0.6 g/cm^3 , consisting of a mixture comprising a first fraction consisting of the dry fraction deriving from municipal solid waste (MSW), a second fraction consisting of elastomeric material and a third
10 fraction consisting of non-elastomeric polymer material. The ratios between the fractions vary as the desired calorific value varies.

EP-A-0 953 628 discloses a combustible composition which burns instantaneously comprising from 40 to 95% by weight of a fossil fuel and from 60 to 5% by weight of a non-fossil solid fuel selected from the group comprising municipal solid waste (MSW), elastomeric polymer
15 material and non-elastomeric polymer material and mixtures thereof. In the combustion plants disclosed in EP-A-0 953 628 the non-fossil solid fuel is stored in a silo from which it is then delivered to the burner.

The Applicant has first noted that direct feed of the RDSF from the production plant to the combustion plant without storage stages is not
20 normally practicable, since the flow rates required by the latter are generally different from those provided by a plant for the production of RDSF. It should be noted that typically a combustion plant works continuously for 24 hours a day, while the output of RDSF is subject to its production methods, in particular the material collection, which is
25 inherently of a discontinuous nature, and, for example, may be carried out in two shifts a day, for about 16 hours per day.

- 2 -

The Applicant has also noted that the storage of a RDSF consisting of the dry fraction deriving from municipal solid waste (MSW) when mixed with elastomeric polymer material and/or thermoplastic (non-elastomeric) polymer material gives rise to a number of disadvantages.

- 5 For the purposes of the present description, by "dry fraction deriving from municipal solid waste (MSW)" is meant a fraction obtained by treating MSW as such by: removal of the wet fraction consisting of putrescible organic material, separation of metal materials, shredding and possibly, if necessary, drying.
- 10 A first disadvantage of the storage of RDSF derives from the fact that during storage the aforesaid materials, in particular the dry fraction deriving from the MSW, tend to aggregate, forming compact agglomerations. This could be avoided by using large storage containers provided with complex mixing equipments, for example
- 15 paddle machines, capable of keeping the stored materials under constant stirring.

However, in addition to resulting in high initial plant costs and then in operating costs for the same, and considerable problems associated with the use of space on account of the large storage volumes required,

20 such storage containers could have the further disadvantage of not hindering but instead favouring separation of the heavier and/or more voluminous particles from the lighter and/or less voluminous particles as a consequence of the action of the mixing equipment itself.

This would therefore result in a non-uniform mixture in terms of

25 composition and density which, if fed to a burner, would cause considerable instability in the combustion process and in particular

- 3 -

would not be capable of ensuring a calorific value which was substantially constant over time.

A further problem derives from the fact that it is frequently necessary to vary the composition of the RDSF produced in relation to use requirements in a combustion process, in particular the desired calorific value. It would therefore be necessary to provide a plurality of containers for the storage of different types of RDSF required by the users.

It has now been found that it is possible to overcome the abovementioned disadvantages deriving from the storage of an RDSF comprising a dry fraction of municipal solid waste (MSW) in admixture with elastomeric polymer material and/or thermoplastic polymer material through a process wherein the dry fraction of the MSW, the elastomeric polymer material and/or the thermoplastic polymer material are stored in separate containers and, when required, are metered and fed in successive layers onto a continuous conveyor which discharges them into a temporary accumulation container, for example the box body of a lorry, intended to directly feed the combustion plant where the RDSF is burnt.

In this way it is not necessary to premix the various fractions of the RDSF during the production stage and to maintain the resultant mixture constantly stirred to prevent agglomeration and/or separation of the fractions. In fact mixing between the various fractions only takes place at the end of the production process when the RDSF is placed in the temporary accumulation container which feeds the combustion plant.

- 4 -

The so obtained mixing is surprisingly effective and is in any event sufficient to guarantee substantial uniformity of composition in the RDSF fed to the combustion plant.

5 The temporary accumulation container (for example an articulated trailer) is then transported to the combustion plant and the RDSF contained therein is taken from the said container, metered and fed to the burners of the combustion plant, for example by means of an extraction, weighing and pneumatic transportation line.

10 In this way the period of time from the mixing of the various RDSF fractions to the use of the RDSF in the combustion plant is reduced to a few hours; in addition to this, the volume of mixed RDSF is a relatively small quantity, for example approximately 80-100 cubic metres. This solution allows to avoid the formation of agglomerations and impacting of the materials constituting the RDSF, and to control the moisture
15 content of the final product so that the physical and thermal characteristics of the product are guaranteed. Additionally, large storage silos are not present both at the RDSF production plant and at the combustion plant, thus avoiding investment and maintenance costs and the use of dedicated spaces.

20 In a first aspect this invention therefore relates to a process for producing a refuse derived solid fuel (RDSF) and feeding the said fuel to a combustion plant, which comprises:

providing a first component consisting of a dry fraction of solid urban waste (MSW) in a shredded form,

25 providing at least one second component in a shredded form selected from an elastomeric material and a thermoplastic material, or mixtures thereof,

- 5 -

separately metering and feeding the said first component and the said
at least one second component onto a continuous conveyor so as to
form overlapping layers of the said components,
discharging the said components so assembled into at least one
5 temporary accumulation container so as to mix the said components to
form the RDSF,
feeding the RDSF so obtained to a combustion plant.

According to a preferred embodiment of the process according to the
invention the RDSF produced is subjected to a compaction phase, is
10 transported to the combustion plant and then, before the stage of being
fed to the combustion plant, is subjected to a disaggregation stage.

According to a preferred embodiment of the process according to the
invention the continuous conveyor collects the various components in
the form of successively overlapping layers having a bulk density which
15 increases from the bottom to the top.

According to a further aspect this invention relates to a plant for the
production of a refuse derived solid fuel, comprising:
at least one storage container for a first component consisting of a dry
fraction of a solid urban waste (MSW) in a shredded form,
20 at least one metering and feeding device for the said first component,
at least one storage container for at least one second component in a
shredded form selected from an elastomeric material and a
thermoplastic material, or mixtures thereof,
at least one metering and feeding device for the said at least one
25 second component,
at least one continuous conveyor onto which the said components are
fed separately from the said storage and metering devices so as to form
overlapping layers of the said components,

- 6 -

at least one temporary accumulation container into which the said components are discharged from the said at least one continuous conveyor.

According to a preferred embodiment the plant according to the invention also comprises at least one storage container for at least one
5 third component in a shredded form also selected from an elastomeric material and a thermoplastic material, but different from the second component. Preferably, when the second component is a thermoplastic material the third component, if present, will be an elastomeric material
10 and vice versa.

The invention will now be further described with reference to the following figures wherein:

- Figure 1 is a diagrammatical view in plan of a plant according to the present invention,
- 15 - Figure 2 is a diagrammatical view in longitudinal cross-section of a storage container of the plant in Figure 1,
- Figure 3 is a diagrammatical view of a longitudinal cross-section of the continuous conveyor of the plant in Figure 1.

As illustrated in Figure 1, in a preferred embodiment the plant according
20 to the present invention comprises a first zone (1) for storage of the dry fraction of the MSW, a second zone (2) for the storage of a thermoplastic polymer material, and a third zone (3) for the storage of an elastomeric polymer material.

In the preferred embodiment illustrated in Figures 1-3, a thermoplastic
25 polymer material, mainly consisting of material obtained from the shredding of disposable chlorine-free plastics materials originating from separate collection (PLA) and an elastomeric material mainly consisting

- 7 -

of material obtained from the shredding of vulcanised rubber articles, in particular waste tyres, after separation of the metal and/or textile reinforcing members, (WT), reach the plant ready to be metered and fed to a continuous conveyor (18).

- 5 The dry fraction of the MSW may be obtained by removing the wet fraction (essentially consisting of putrescible organic components, such as plant waste, food waste, etc.) from the raw MSW using purely mechanical processes (for example shredding and subsequent screening), as described for example in the already mentioned patent application EP-A-0 930 353. Subsequently the dry fraction of the MSW
10 may be further shredded and, if necessary, dried to obtain a water content not higher than 15% by weight, preferably not higher than 10% by weight.

As an alternative the dry fraction of the MSW may be obtained in
15 accordance with the known art by subjecting the MSW to a process of biostabilisation, and subsequently to a process of removal of the fine fraction (by screening, for example). The biostabilisation process is a process of biological degradation, in general through microorganisms acting under anaerobic conditions (biooxidation) under controlled
20 temperature and humidity conditions (see for example F. Adani et al., *Waste Management and Research*, Volume 18 Issue 5, page 471 – October 2000). At the end of this process the organic fraction which has been transformed by the microorganisms is removed by screening as a fine fraction, that is as a fraction having average dimensions which are
25 generally less than 80 mm, preferably less than 60 mm. The dry fraction so obtained in general has a low moisture content, not more than 15% by weight, preferably not more than 10% by weight, as a result of which a subsequent drying process is not required.

- 8 -

The particle size of the dry fraction of the MSW obtained according to the methods described above is generally further reduced by shredding in order to achieve dimensions not exceeding 25 mm for at least 90% by weight of the material.

- 5 The dry fraction of the MSW generally comprises paper and its derivatives (cardboard, multi-ply materials), wood, fabrics, leather and wastes from other fractions of materials.

In case the dry fraction of the MSW reaches the plant at an intermediate processing stage, a unit is provided in the plant according to the
10 invention for its processing, which may comprise a first magnetic separator (5a), a conveyor belt for manual sorting (6), a second magnetic separator (5b) and a drier (9).

In greater detail, in the embodiment in Figure 1 the dry fraction of the MSW is discharged to the appropriate storage area (1) from motor
15 vehicles. A mechanical rubber-coated loader (not illustrated) picks up the dry fraction of the MSW from the storage area (1) and discharges it into a hopper lying above a feed conveyor (4). The dry fraction of the MSW is subjected to a first sorting with a magnetic separator (5a) in order to remove any ferrous materials. Subsequently the dry fraction
20 may possibly be caused to pass on a sorting conveyor belt (6) where a manual sorting may be performed to remove any undesirable wastes, such as for example stones or other inert materials which might accidentally be present in the MSW which could damage the equipment used in the subsequent stages. A further sorting using a magnetic
25 separator (5b) may remove any residual ferrous materials.

A conveyor belt (8a) then carries the MSW to a shredding device (7), preferably comprising two shredders in series.

When the residual moisture content of the dry fraction of the MSW is not greater than a predetermined value, and in particular is not greater than 15% by weight, this is delivered directly to the storage container (10a) by means of a conveyor belt (8b).

- 5 However, when the residual moisture content of the dry fraction of the MSW is greater than that predetermined value it is delivered to a drier (9) via a conveyor belt (8c). The drier generally operates on hot air at a temperature of between 60°C and 80°C, obtained for example by heating ambient air with a methane burner. The drier (9) also comprises
- 10 a blower system to remove the exiting moist air. Once the desired moisture content has been reached, the dry fraction of the MSW is delivered to the storage container (10a) by means of a conveyor (8d).

The storage container (10a), which is closed at the top, is provided with a walking floor (23a) and containing sides. A system of rotating paddles

15 (21a) to move the dry fraction of the MSW before delivering it to the metering screw (22a) and subsequently to a weighing system (11a) (for example a weighing belt or a load cell, or other known system) is installed close to the discharge head. Advantageously the metering screw has a rate of advance which is regulated in relation to the

20 quantity of each component weighed by the corresponding weighing system. In this way a substantially constant composition of the RDSF is obtained.

The characteristics of the dry fraction of the MSW stored in the storage container (10a) are preferably the following:

- Residual moisture content:	not greater than 15% by weight
- Dimensions of at least 90% by weight of the particles:	not larger than 25 mm

- 10 -

- Average net calorific value (NCV):	not less than 3,500 Kcal/kg
- Bulk density:	0.10-0.20 g/cm ³

The thermoplastic polymer material mainly comprises material obtained from the shredding of chlorine-free waste plastics materials (PLA) originating from separate collection, such as for example polyethylene terephthalate (PET), polypropylene (PP), polyethylene (PE) and polystyrene (PS).

According to the embodiment of the plant according to the invention illustrated in Figures 1-3, the shredded PLA is taken from the storage zone (2) by a mechanical loader and discharged into the loading hopper (12). From there a conveyor (8e), for example a chain conveyor, carries it to the storage container (10b), which has a structure similar to that of the container (10a) previously illustrated. The storage container (10b) is provided with a walking floor (23b) and containing sides. A system of rotating paddles (21b) for moving the shredded PLA before delivering it to the metering screw (22b) (Figure 2) and subsequently to a weighing system (11b) is installed close to the discharge head.

The characteristics of the shredded PLA stored in the storage container (10b) are preferably as follows:

- Dimension of at least 90% by weight of the particles:	not larger than 25 mm
- Average net calorific value (NCV):	not less than 7,000 Kcal/kg
- Bulk density:	0.10-0.15 g/cm ³ .

- 11 -

The elastomeric polymer material mainly comprises material obtained from the shredding of vulcanised rubber articles, in particular waste tyres (WT), after separation of the metal and/or textile reinforcing members.

- 5 In the embodiment of the plant according to the invention illustrated in Figures 1-3, the WT are taken from the storage area (3) and charged into the storage container (10c), which has a structure similar to that of the storage containers (10a, 10b) previously illustrated. Storage container (10c) is generally provided with a walking floor (23c) and
 10 containing sides. A system of rotating paddles (21c) to move the shredded WT before delivering it to the metering screw (22c) (Figure 2) and subsequently to a weighing system (11c) is installed close to the discharge head.

- The characteristics of the shredded WT stored in the storage container
 15 (10c) are preferably as follows:

– Dimensions of at least 90% by weight of the particles:	not larger than 25 mm
– Average net calorific value (NCV):	not less than 7,000 Kcal/kg
– Bulk density:	0.40-0.70 g/cm ³

- Once weighed the three materials pass onto a continuous conveyor (18), for example a conveyor belt or a chain conveyor. The advancing rate in the metering screws (22a, 22b and 22c) of the three components
 20 of the RDSF is controlled in relation to data obtained from the weighing systems (11a, 11b, 11c) so as to guarantee a substantially constant composition for the exiting RDSF.

- 12 -

Transfer of the three components of the RDSF (PLA, dry fraction of MSW and WT) from the corresponding metering screws (22a, 22b, 22c) to the weighing systems (11a, 11b, 11c) and subsequently to the continuous conveyor (18) advantageously takes place through gravity.

- 5 As illustrated in Figure 3, the continuous conveyor (18) preferably first collects the PLA fraction stored in the container (10b), then the dry fraction of MSW stored in the container (10a) and finally the WT fraction stored in the container (10c),

- 10 In the stratification so obtained onto the continuous conveyor (18), the lower layer (25) is formed of the lightest material (PLA), the intermediate layer (26) is formed of the material having an intermediate weight (dry fraction of the MSW) and the upper layer (27) is formed from the heaviest material (WT). In this way the lightest fraction is prevented from dispersing in the environment during the movement of
15 the so stratified materials.

Finally, the continuous conveyor (18) discharges the collected material into a temporary accumulation container, for example in the articulated trailer (19) of a motor vehicle. The said articulated trailer (19) is provided with a walking floor (24) for loading and discharging the RDSF.

- 20 As they fall into the box body (19) of the motor vehicle, the three layers (25, 26, 27) of the materials accumulated on the continuous conveyor (18) mix each other.

- 25 Surprisingly it has been observed that this mixing is particularly effective when the lower layer (25) is formed of the lightest material (PLA), the intermediate layer (26) is formed of the material having an intermediate weight (MSW) and the upper layer (27) is formed of the heaviest material (WT).

- 13 -

The bulk density of the RDSF so obtained is generally less than 0.60 g/cm³, preferably it ranges from 0.35 to 0.12 g/cm³.

As already mentioned previously, in accordance with one embodiment of the invention the RDSF so obtained can be subjected to a
5 compaction stage (for example by mechanical compression) so as to provide a compacted RDSF in any form suitable for transport, for example substantially rectangular or cylindrical. The compaction stage may be carried out by any mechanical device suitable for the purpose, for example a press (not shown in the Figures). Compaction is carried
10 out in such a way as to obtain a bulk density for the compacted RDSF which generally lies between 0.50 and 0.95 g/cm³, preferably between 0.60 and 0.90 g/cm³. This makes it possible to reduce the volume of the conveyed material and therefore the transport costs, particularly over long distances.

15 In this case, at the time of use the compacted RDSF may be again disaggregated in order to reacquire the physical characteristics (in particular the bulk density values indicated above) which render it particularly suitable for combustion processes with suspension burners, and in particular co-combustion processes with fossil fuels, such as
20 those disclosed in the already cited patent application EP-A-0 953 628. With this aim at least one mechanical device capable of disaggregating the compacted RDSF, for example a shredder, is provided close to the combustion plant.

The plant in figure 1 is preferably provided with a control system (not
25 illustrated) which is capable of automating the various stages of treatment and of communicating, suitably through video terminals, with the operators operating the plant.

- 14 -

This control system essentially comprises a programmable control unit (PCU).

The control system offers the following main control choices:

- 5 – settings for the flows of the various materials delivered to the motor vehicle loading unit,
- selection of the three lines which will be subjected to processing,
- management of the operating cycles,
- monitoring of the condition of the process machines served,
- diagnosis of alarms in the machines served.

10 Automatic starting of the system will bring about starting of all the machines forming part of the selected systems in sequence. The starting sequence is structured on the basis of first starting the last machine in the selected lines (tail) and then moving backwards starting up all the others in succession until the machines at the head of the
15 lines (moving floor feeders) are started. This makes it possible to prevent the loaded material from accumulating in machines which are still stopped, clogging them. Vice versa, on the same principle, stopping of the system causes the machines to stop in succession away from the head.

20 A typical composition of a solid fuel deriving from wastes (RDSF) produced according to this invention is as follows:

40-90% by weight, preferably 60-80% by weight, of a dry fraction of MSW,

10-60% by weight, preferably 20-40% by weight, of at least one polymer
25 material selected from elastomeric material and thermoplastic material, or mixtures thereof.

Even more preferably, the solid fuel deriving from wastes (RDSF) produced according to this invention has the following composition:

- 15 -

40-90% by weight, preferably 60-80% by weight, of a dry fraction of MSW,

5-55% by weight, preferably 10-30% by weight, of at least one elastomeric polymer material,

- 5 5-55% by weight, preferably 10-30% by weight, of at least one thermoplastic polymer material.

The bulk density of the RDSF delivered to a combustion plant is generally less than 0.60 g/cm^3 , preferably ranging from 0.35 to 0.12 g/cm^3 .

- 10 The RDSF obtained according to this invention may comprise the primary fuel of a combustion plant, or it may be used as a secondary fuel in co-combustion plants, as illustrated in the already cited patent application EP-A-0 953 628 in which the primary fuel comprises a fossil fuel, for example powdered coal, methane gas or fuel oil.
- 15 The combustion plant may be of any type, for example a thermal plant for the generation of heat, a thermoelectric plant for the generation of electrical power, a plant for the manufacture of cement, and the like.

- 16 -

CLAIMS

1. A process for producing a refuse derived solid fuel (RDSF) and feeding the said fuel to a combustion plant, which comprises:
 - 5 - providing a first component consisting of a dry fraction of solid urban waste (MSW) in a shredded form,
 - providing at least one second component in a shredded form selected from an elastomeric material and a thermoplastic material, or mixtures thereof,
 - 10 - separately metering and feeding the said first component and the said at least one second component onto a continuous conveyor in such a way so as to form overlapping layers of the said components,
 - discharging the said components so assembled into at least one temporary accumulation container so as to form the
15 RDSF,
 - feeding and metering the RDSF so obtained to a combustion plant.
2. Process according to Claim 1, wherein the thermoplastic polymer material mainly comprises a material obtained from the
20 shredding of chlorine-free waste plastics materials.
3. Process according to Claim 2, wherein at least 90% of the weight of thermoplastic material has an average particle dimension not exceeding 25 mm.
4. Process according to any one of the preceding Claims, wherein
25 the elastomeric polymer material mainly consists of a material obtained from the shredding of waste tyres after separation of the metal and/or textile reinforcing members.

- 17 -

5. Process according to Claim 4, wherein at least 90% by weight of the elastomeric material has an average particle dimension not exceeding 25 mm.
- 5 6. Process according to any one of the preceding Claims, wherein the dry fraction of the MSW is obtained from an unprocessed MSW by mechanical separation of putrescible organic fraction, separation of metal materials, shredding and possibly drying.
- 10 7. Process according to any one of Claims from 1 to 5, wherein the dry fraction of MSW is obtained by subjecting a raw MSW to a process of biostabilisation and subsequently a process of removing a fine fraction.
8. Process according to Claim 7, wherein the removed fine fraction has a dimension of less than 80 mm.
- 15 9. Process according to any one of the preceding Claims, wherein at least 90% by weight of the dry fraction of MSW has an average particle dimension not exceeding 25 mm.
10. Process according to any one of the preceding Claims, wherein the dry fraction of MSW has a moisture content not exceeding 15% by weight.
- 20 11. Process according to Claim 10, wherein the dry fraction of MSW has a moisture content not exceeding 10% by weight.
12. Process according to any one of the preceding Claims, wherein the produced RDSF is subjected to a stage of compaction, transported to the combustion plant and then subjected to a

- 18 -

disaggregation stage before the stage of feeding it to the combustion plant.

- 5
13. Process according to Claim 12, wherein the compacting stage is carried out so as to obtain a compacted RDSF with a bulk density ranging from 0.50 to 0.95 g/cm³.
14. Process according to Claim 13, wherein the compacting stage is carried out in such a way so as to obtain a compacted RDSF with a bulk density of from 0.60 to 0.90 g/cm³.
- 10
15. Process according to any one of the preceding Claims, wherein the stage of metering and feeding the said first component and the said at least one second component onto a continuous conveyor takes place separately, each through at least one metering screw and subsequently a weighing system.
- 15
16. Process according to Claim 15, wherein the said at least one metering screw has an advancing rate regulated in relation to the quantity of each component weighed by the corresponding weighing system.
- 20
17. Process according to any one of the preceding Claims, wherein the continuous conveyor collects the various components in the form of successive overlapping layers having a bulk density which increases from the bottom towards the top.
- 25
18. Process according to Claim 17, wherein a lower layer consisting of the thermoplastic material, an intermediate layer consisting of the dry fraction of the MSW, and an upper layer consisting of the elastomeric material is formed on the continuous conveyor belt.

- 19 -

19. Process according to any one of the preceding claims, wherein the obtained RDSF has the following composition:
40-90% by weight of the dry fraction of the RDSF,
10-60% by weight of at least one polymer material selected from
5 elastomeric material and thermoplastic material, or mixtures thereof.
20. Process according to Claim 19, wherein the obtained RDSF has the following composition:
10 60-80% by weight of the dry fraction of MSW,
20-40% by weight of at least one polymer material selected from elastomeric material and thermoplastic material, or mixtures thereof.
- 15 21. Process according to Claim 19 or 20, wherein the obtained RDSF has the following composition:
40-90% by weight of dry fraction of RDSF,
5-55% by weight of at least one elastomeric polymer material,
5-55% by weight of at least one thermoplastic polymer material.
- 20 22. Process according to Claim 21, wherein the obtained RDSF has the following composition:
60-80% by weight of the dry fraction of the MSW,
10-30% by weight of at least one elastomeric polymer material,
10-30% by weight of at least one thermoplastic polymer material.
25
23. Process according to any one of the preceding claims, wherein the obtained RDSF has a bulk density of less than 0.60 g/cm^3 .

- 20 -

24. Process according to Claim 23, wherein the RDSF obtained has a bulk density of from 0.35 to 0.12 g/cm³.
25. Plant for producing a refuse derived solid fuel, comprising:
at least one storage container for a first component consisting of
5 a dry fraction of solid urban waste (MSW) in a shredded form,
at least one metering and feeding device for the said first component,
at least one storage container for at least one second component
in a shredded form selected from an elastomeric material and a
10 thermoplastic material,
at least one metering and feeding device for the said at least one
second component,
at least one continuous conveyor onto which the said
components are fed separately by the said feeding and metering
15 devices so as to form overlapping layers of the said components,
at least one temporary accumulation container into which the
said components are discharged by the said at least one
continuous conveyor.
26. Plant according to Claim 25, also comprising at least one storage
20 container for at least one third component in a shredded form
also selected from an elastomeric material and a thermoplastic
material, different from the second component,
at least one metering and feeding device for the said at least one
third component.
- 25 27. Plant according to either of Claims 25 and 26, wherein the said
metering and feeding devices comprise at least one metering
screw and a weighing system.

- 21 -

28. Plant according to Claim 27, wherein the said at least one metering screw has a advancing rate which is regulated in relation to the quantity of each component weighed by the corresponding weighing system.
- 5 29. Plant according to any one of Claims 25 to 28, also comprising a device for compaction of the obtained RDSF.

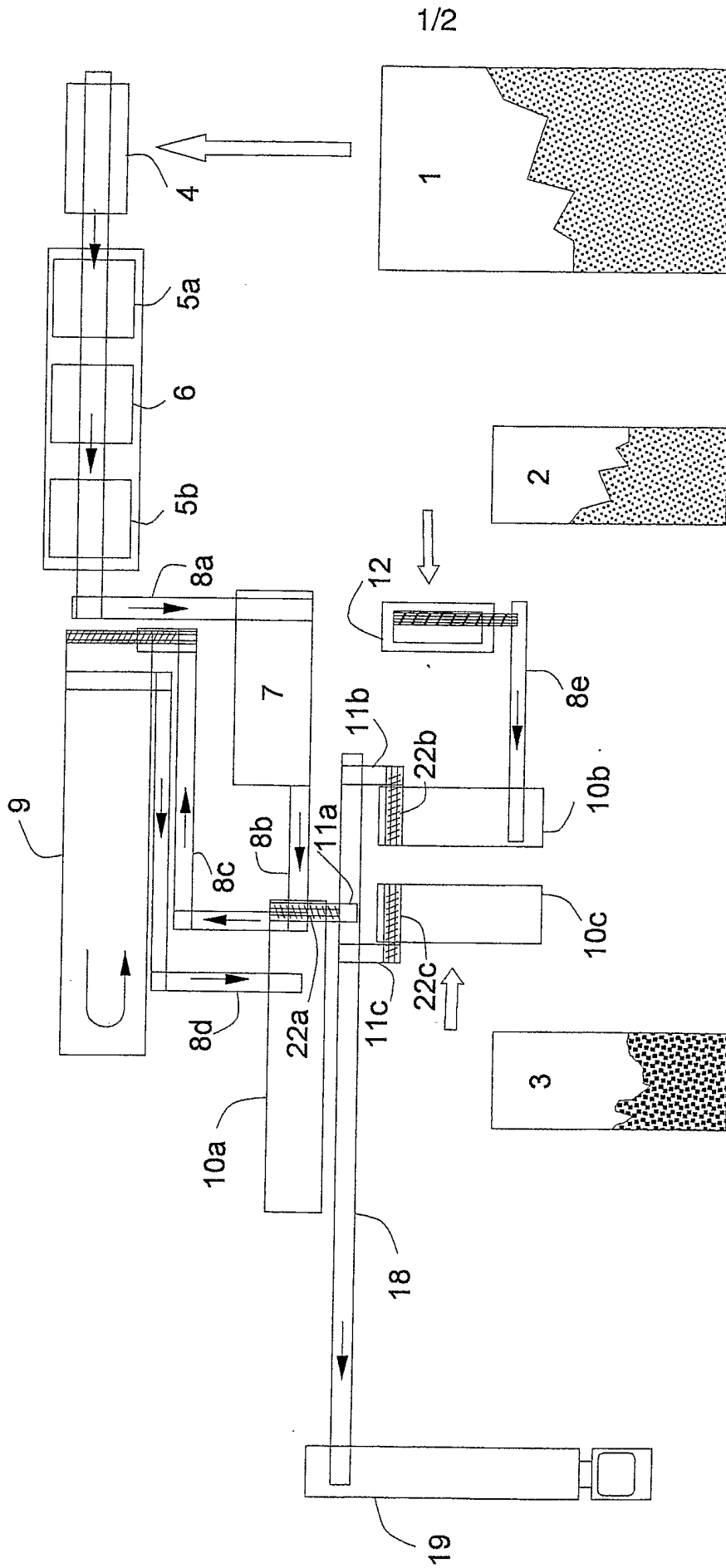


FIG. 1

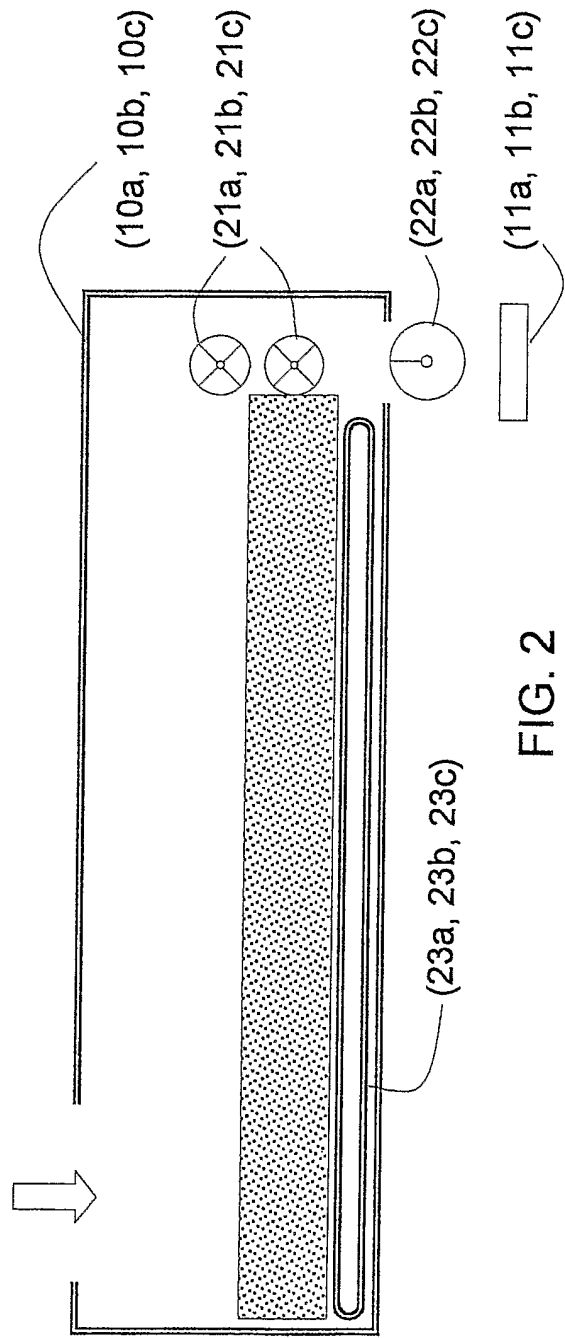


FIG. 2

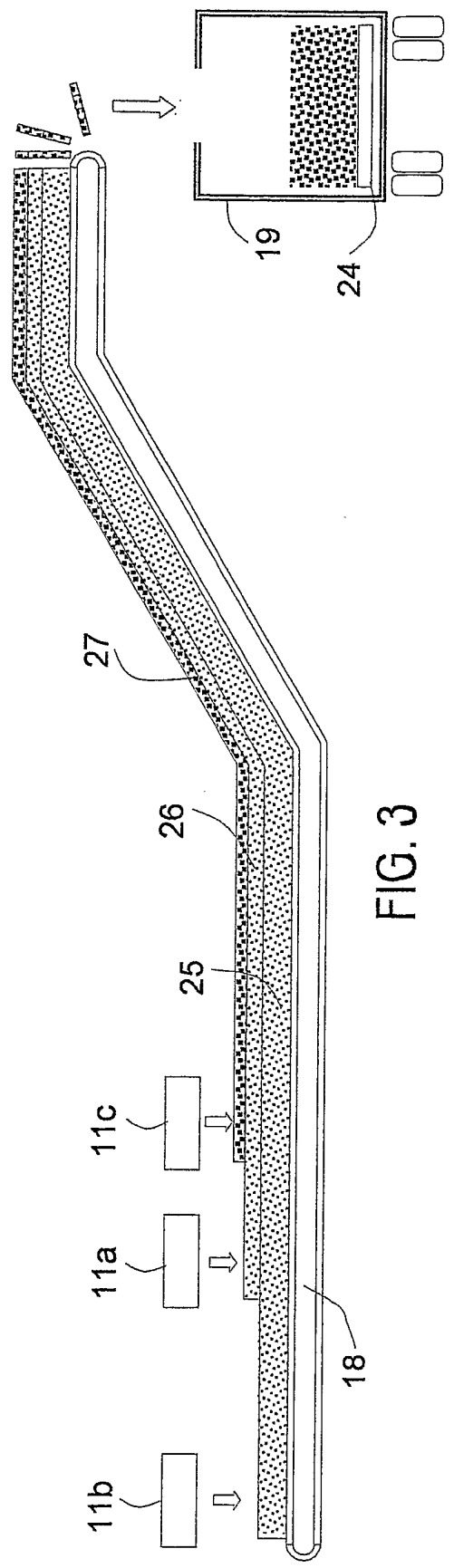


FIG. 3

INTERNATIONAL SEARCH REPORT

Int'l. Application No
PCT/IT2004/000154

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 C10L5/46 F23G5/02 F23K1/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 C10L F23G F23K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A A A A	<p>US 1 772 285 A (KNITTEL PAUL S) 5 August 1930 (1930-08-05) claims</p> <p style="text-align: center;">-----</p> <p>EP 0 930 353 A (PIRELLI AMBIENTE S P A) 21 July 1999 (1999-07-21) cited in the application abstract; claims; figures</p> <p style="text-align: center;">-----</p> <p>EP 0 953 628 A (PIRELLI AMBIENTE S P A) 3 November 1999 (1999-11-03) cited in the application abstract; claims</p> <p style="text-align: center;">-----</p> <p>DE 102 24 133 A (VOLKSWAGENWERK AG ; SICON GMBH (DE); EMSCHERGENOSSENSCHAFT LIPPEVER (D) 6 March 2003 (2003-03-06) claims</p> <p style="text-align: center;">-----</p>	<p>25-29</p> <p>1-24</p> <p>1-29</p> <p>1-29</p> <p>1-29</p>

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

° Special categories of cited documents :

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- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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Date of the actual completion of the international search

10 December 2004

Date of mailing of the international search report

17/12/2004

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/IT2004/000154

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