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(54) Title: METHOD TO PRODUCE HIGH SPECIFIC IMPULSE AND MODERATE THRUST FROM A FUSION-POWERED ROCKET ENGINE

(57) Abstract: A system and method for producing and controlling high thrust and desirable specific impulse from a continuous fusion reaction is disclosed. The resultant relatively small rocket engine will have lower cost to develop, test, and operate than the prior art, allowing spacecraft missions throughout the planetary system and beyond. The rocket engine method and system includes a reactor chamber and a heating system produce fusion reactions the stable plasma. Magnets produce a magnetic field that confines the stable plasma. A fuel injection system and a propellant injection system are included. Cold propellant into a gas box for converting a cold propellant into a warm propellant plasma at one end of the reactor chamber. The propellant and fusion products are directed out of the reactor chamber through a magnetic nozzle and are detached from the magnetic field lines producing thrust.



METHOD TO PRODUCE HIGH SPECIFIC IMPULSE AND MODERATE THRUST
FROM A FUSION-POWERED ROCKET ENGINE

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CROSS REFERENCE TO RELATED APPLICATIONS

[0001] This application is an international application filed under the Patent Cooperation Treaty and claims priority to U.S. Provisional Application Serial No. 61/645,459 filed May 10, 2012, which is incorporated by reference as if fully disclosed

10 herein.

FIELD OF THE INVENTION

[0002] The disclosed scenarios relate generally to the field of plasma physics and, in particular, to methods and devices for producing thrust from a fusion reactor.

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STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR
DEVELOPMENT

[0003] This invention was made with government support under Grant #DE-AC02-09CH11466 awarded by the Department of Energy. The government has certain rights in

20 this invention.

BACKGROUND

[0004] Many nuclear fusion reactors have been proposed to produce thrust for rocket propulsion from the fusion of atomic particles such as deuterium, tritium, and helium.

[0005] Fusion reactors can be broadly classified as those that use magnetic
25 confinement and those that use inertial confinement. In the former, magnetic fields from magnet external coils or produced by plasma currents confine hot plasma, allowing for

steady or pulsed fusion to occur. In inertial confinement, by contrast, external particle beams or lasers compress the reactants to produce pulsed fusion.

[0006] Dozens of fusion reactor configurations have been proposed for spacecraft propulsion including tokamaks, dipoles, mirror machines, stellarators, theta-pinch, and the field-reversed configuration (FRC). One benefit of the latter is its high ratio of magnetic pressure to plasma pressure, meaning that it requires less magnetic mass than an equivalent strength tokamak. This mass savings is crucial in rocket design. Further benefits of a FRC for space propulsion are its simple, cylindrical magnet geometry and its natural diverter. This allows for a compact thruster engine in which the fusion products can be used directly for propulsion.

[0007] U.S. Patent Application Publication No. 2008/0093506 describes an electric propulsion system where a gas is injected into a chamber, ionized, and accelerated using electromagnets. Other ion thruster configurations are disclosed. These thrusters require a separate system to generate power for producing electric, magnetic, or electromagnetic fields to ionize gas and heat and accelerate the plasma thus formed.

[0008] U.S. Patent No. 6,334,302 discloses a method to control the specific impulse of plasma thruster using two separate RF generators powering two separate RF heating sections, one before and the other after a magnetic nozzle. The source of electrical power for the RF generators is unspecified. Thrust is controlled by adding neutral gas into the plasma stream, as disclosed in U.S. Patent No. 4,815,279 and 4,893,470.

[0009] European Patent No. 1 856 702 describes a $p\text{-}^{11}\text{B}$ -fueled FRC that combines power and thrust production by using half of the fusion products for electrical generation and the second half for direct thrust. The former's energy is captured using an inverse cyclotron converter, while the latter particles are directed and expelled via a magnetic

nozzle. The exhaust velocity of the propellant in this design is simply the velocity of the fusion products and 50% of the power goes out in thrust.

[0010] A system for modifying thrust called side-injection is disclosed in U.S. 3,325,103. It involved the injection of a high-speed, pencil size flow of fluid into the main thrust stream to deflect the thrust vector through the main nozzle. This system was proposed for a chemical rocket and is limited in purpose to thrust vector control through flow deflection.

[0011] Neutral beam injection is disclosed in U.S. 4,480,185. The process involves ionizing particles, in this case deuterium, and then accelerated into a gas cloud, where charge exchange neutralized the beam.

[0012] Teller, *et al.* (Fusion Technology 22, 8 (1992)), describes a D-³He fueled dipole fusion reactor for spacecraft propulsion. The device is large, over 1 GW power. Insufficient ³He source exist on earth to fuel this engine for more than 1 month. Propellant, introduced as gas from an annular ring near the reactor's midplane, is ionized then exhausted from the plasma edge by following the field lines to a neutralizer region in a low field region where detachment of ions from the dipole's magnetic field would be accomplished by charge exchange neutralization. The decrease in magnetic field from the propellant injection region to the neutralizer region results in the transfer of most ion energy to the axial direction. The parameters of the plasma edge are determined by transport rates and stability criteria, which allow little control of thrust and specific impulse. Inefficiencies may occur due to ionization and charge exchange energy and particle losses.

[0013] Slough (49th AIAA Aerospace Sciences Meeting (2001)) has described several D-T fueled FRC fusion reactors for spacecraft propulsion. FRCs are formed, perhaps by

the theta-pinch method, then compressed, perhaps by imploding liners or passing through constricting channels. Compression causes increase of the plasma temperature and density to such values that rapid burn (fusion) of the fuel occurs. The heated FRC plasmoid then expands and accelerates as emerges from the constricting channel. The liners are also accelerated by the expanding FRC plasmoid and contribute to the thrust. Repeated pulses could provide a time-averaged power of tens of MW.

[0014] Carpenter and Brennan (Acta Astronautica 44, (1999) 471) describe a mirror machine fusion reactor, fueled with either D-T or D-³He. The 80-m-long rocket engine would produce about 4 GW of fusion power. (The large amount of ³He fuel required for 4 GW would cost over 300B\$.) Hydrogen propellant is added to the plasma halo. No discussion is provided of how the propellant is heated or the specific impulse controlled to produce 11 kN of thrust. Neutralization of the exhaust stream is provided by charge exchange in the expansion region of the exhaust nozzle, with the aforementioned inefficiencies in power and particles. The fusion region is relatively open, to allow direct loss of radiation to space, reducing the need for a heat radiator but reducing the power available for thrust and subsystems by ~80%. As in all mirror machines, half of the fusion power flows in the wrong direction for thrust hence must fall onto to a direct convertor for making electricity.

[0015] Past proposals for fusion propulsion have had many disadvantages. Inertial confinement and the most common magnetic confinement configurations (i.e. tokamaks and stellarators) have non-linear geometries and must be very large to generate net power. Linear reactors using D-T or D-D produce so many neutrons that a lot of shielding is required and even with that, the reactor chamber, magnets, and other essential components located near the plasma are especially prone to damage and shortened-lifetime. Electric

propulsion using ion thrusters produce very high specific impulse but very low thrust, leading to long mission times.

SUMMARY

5 [0016] A system and method for producing and controlling high thrust and desirable specific impulse from a continuous fusion reaction using a D-³He fueled FRC. The resultant relatively small rocket engine will have lower cost to develop, test, and operate than the prior art, allowing spacecraft missions throughout the planetary system and beyond.

10 [0017] A rocket engine system employing nuclear fusion with thrust augmentation is disclosed. The engine system includes a reactor chamber for containing a stable plasma of a fusion fuel and a heating system for heating the plasma and increasing an ion energy of said plasma to produce fusion reactions in the stable plasma. A plurality of magnets are situated coaxial to the reactor chamber and produce a magnetic field that confines the
15 stable plasma and promotes rapid loss of fusion products into a scrape off layer. A fuel injection system is also included for injecting additional quantities of said fusion fuel to sustain the power output of the fusion reactions in the plasma. A propellant injection system injects cold gas propellant into a gas box at one end of the scrape off layer for producing a cold plasma which flows into the reaction chamber and is warmed there,
20 becoming a warm propellant plasma. The propellant is used to augment the mass of the scrape off layer. A magnetic nozzle for directing said warm plasma on said scrape off layer out of the other end of the reactor chamber from said gas box creates thrust. A propellant detachment system allows the expelled propellant to separate from said rocket engine's magnetic field in a well-directed stream.

[0018] A method for augmenting the thrust of a fusion powered rocket engine described above includes injecting, by the fuel injection system, the fusion fuel into the reactor chamber and heating, by the heating system, the plasma such that the fuel is ionized such that a sustained nuclear fusion reaction occurs in the plasma producing a net power. Magnets are used to form a magnetic field to confine the plasma and promote rapid loss of fusion products into a scrape off layer. A propelling injection system injects into the gas box a cold propellant, which is converted into a warm propellant plasma to increase the mass of the scrape off layer, wherein the warm propellant plasma flows through the reactor chamber and is heated by the fusion products. Finally, the warm propellant plasma and fusion products are expelled from the reactor chamber through the magnetic nozzle. The expelled propellant particles are detached from said rocket engine's magnetic field in a well-directed stream.

BRIEF DESCRIPTION OF THE DRAWINGS

15 [0019] FIG. 1 shows an example magnetic field configuration for an FRC propulsion system.

[0020] FIG. 2 shows an example technique for neutral beam injection.

[0021] FIG. 3 shows an example configuration a fusion reactor that is designed for thrust augmentation and rocket propulsion.

20 [0022] FIG 4 shows the heating of the scrape off layer for thrust augmentation.

[0023] FIG 5 shows a heat exchanger to capture radiation from fusion, for energy conversion.

[0024] FIG 6 shows a plasma detachment method using charge-exchange.

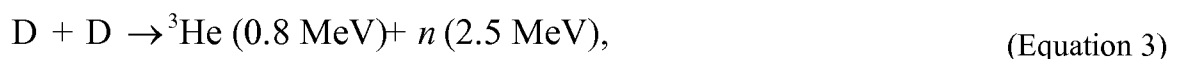
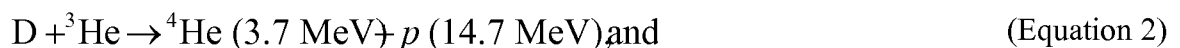
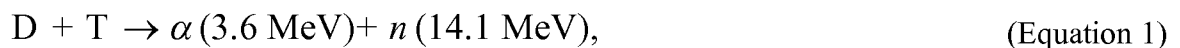
DETAILED DESCRIPTION

[0025] In the following description, for purposes of explanation, specific numbers, materials and configurations are set forth in order to provide a thorough understanding of the invention. It will be apparent, however, to one having ordinary skill in the art, that the invention may be practiced without these specific details. In some instances, well-known features may be omitted or simplified so as not to obscure the disclosed scenarios. Furthermore, reference in the specification to "one embodiment" or "an embodiment" means that a particular feature, structure or characteristic described in connection with the embodiment is included in at least one embodiment of the invention. The appearances of the phrase "in an embodiment" in various places in the specification are not necessarily all referring to the same embodiment.

[0026] During the course of this description like numbers will be used to identify like elements according to the different views, which illustrate the invention.

[0027] In nuclear fusion reactions light nuclei bind temporarily then fragment to produce fast moving reaction products comprising heavy particles, which contain vast amounts of kinetic energy. This fusion process only occurs rapidly at temperatures of 5-500 keV (58-5,800 million K) such that the Coulomb force, which repulses the positively charged nuclei, is overcome. The reactivity (*i.e.* rate of fusion) is a function of the ion temperature and plasma density.

[0028] The most important fusion reactions for practical reactors are as follows:



where D is deuterium, T is tritium, α is a helium nucleus, n is a neutron, p is a proton, and ${}^3\text{He}$ and ${}^4\text{He}$ are helium-3 and helium-4, respectively. The associated kinetic energy of each product is indicated in parentheses.

[0029] The D-T reaction produces most of its energy in neutrons, which means that
5 electrical energy can only be produced by using the neutron radiation to heat a working fluid, much like in a conventional boiler or a fission reactor. Due to temperature limitations of the working fluid, that conversion can only be about 30% efficient. An advantage of the D-T fuel mixture is that it produces net power at the lowest ion temperatures, of only 5-10 keV (1 keV = 11.6 million K, and is a more convenient unit of
10 temperature). However, the energetic neutrons liberated in this reaction represent a significant threat to the reactor's structure as the neutron flux degrades the electrical, mechanical, and thermal properties of the reactor components and also leaves many of their materials radioactive. For terrestrial power reactors, most of these energetic neutrons are used to breed tritium, a scarce material. Thus, the D-T fuel mixture poses significant
15 challenges with radiation damage, material activation, and fuel availability. Pursuing a D-T reactor would require substantial research and development of nuclear materials and tritium breeding as well as several meters worth of shielding to protect reactor components and personnel from neutron radiation.

[0030] The D-D fusion reactions are very attractive because the abundance of
20 deuterium obviates the need to breed tritium. Moreover, the neutrons generated are fewer in number and lower in energy than from D-T per unit of energy produced. By selective treatment of D-D fusion's daughter products – removing the T from the plasma before it fuses but burning the prompt and decay-formed ${}^3\text{He}$, a technique called He-catalyzed D-D

fusion – the neutron production can be reduced to 10% of the D-T level, per unit of energy produced.

[0031] The D-³He reaction is termed aneutronic, because it directly produces relatively few neutrons and requires none for breeding. The energy from the charged reaction products may be directly converted to electrical power at a much higher efficiency than D-T. However, higher ion energies or temperatures, of 50-100 keV, are required to achieve the same reactivity as D-T. Both D-D and D-³He reactions admit D-D side reactions, which for a D-³He reactor is the only source of neutron production. A known method for decreasing this neutron generation is lowering the reactant concentration ratio of D-³He, for example, from 1:1 to 1:9. In a thermal plasma with 100 keV ion temperatures and T ash promptly removed, this causes neutron production to drop from 2.6% to 0.5% of D-T's per unit of energy produced. This reduces the level of neutron shielding required to well under a meter. However, the lower D concentration reduces the power density by a factor of 4.5, adversely affecting the economics. A method for suppressing this neutron generation pathway was been presented in International Patent Application Serial No. PCT/US13/33767 which is incorporated by reference as if fully disclosed herein.

[0032] Among all fusion fuels, D-³He is preferred for the applications described in this disclosure because it produces fewer neutrons while generating net power. Various propellants can be used for thrust augmentation including deuterium and hydrogen.

[0033] The plasma is formed within a reactor chamber, which may be small enough to accommodate ion gyroradii that are about 1/10th of the plasma radius and mostly have axis encircling orbits. This promotes the plasma stability against the tilt mode. A heating system, such as radio frequency generating magnetic coils, must be able to raise the plasma's ion energy such that fusion reactions occur. By locating multiple discrete

magnets coaxially to the reactor chamber, a corrugated axial magnetic field is formed that also mediates against the unstable tilt mode.

[0034] The magnetic confinement scheme can employ either permanent magnets or magnetic coils. The magnets control the size of the plasma so that it is large enough to contain fusing plasma of sufficient power while small enough to be effectively heated and allow the fusion products to quickly move into a scrape off layer. The scrape off layer is a typical component of magnetic confinement fusion devices with internal closed field lines and is crucial for this system of thrust augmentation. It is found in tokamaks, stellarators, reversed-field pinches, spheromaks, and field-reversed configurations (FRCs).

[0035] An FRC, depicted in Figure 1, forms a quasi-toroidal, closed-field, simply connected magnetic confinement device with open field lines exiting the reactor chamber approximately paraxially. A separatrix **10** divides the closed-field region **12** from the open-field region **14**, with the latter containing the scrape-off-layer (SOL). The discrete flux conserving magnetic coils **16** provide magnetic pressure while allowing the heating method, such as an odd-parity (i.e. anti-parallel) rotating magnetic field (RMF_o) from external radio frequency magnetic coils, to penetrate the plasma. A toroidal current **18**, centered on the O-point null line **20**, is formed around the axis of the closed-field region **12**.

[0036] Various means of fuel injection can be employed to introduce the fuel into the reaction chamber, including pellets, gas puffing, cluster, and neutral beam injection. Figure 2 depicts neutral beam injection, which is used to feed a tight beam of energetic neutral D and ³He into the center of the chamber. The neutral beam is created by injecting a feedstock gas propellant **22**, such as hydrogen or deuterium, into a plasma formation box **24** and charge exchange box **26**. In the plasma formation box **24**, the feedstock gas

propellant **22** is weakly ionized. The ionized ions are ejected through an ion extraction grid **30** and then accelerated through a high-voltage ion acceleration grid **32** to form ion beam **28**. Ion beam **28** then enters the charge exchange box **26** where electrons are passed from the gas cloud formed by the feedstock gas propellant **22** forming the neutral beam

5 **34**. Neutral beam **34** is then injected into the reaction chamber.

[0037] Figure 3 illustrates an FRC configured for thrust augmentation. Fusion fuel is injected **36** near the center of the reactor chamber **37**. Fusion is achieved in the closed-field region **38** where the plasma is heated. In this arrangement, shaping and heating of the FRC is achieved with active **40** and passive flux conserving magnetic coils **42** and

10 radio frequency coils **44** that create the anti-parallel components of the RMF_o. Thrust augmentation is achieved by pumping deuterium or hydrogen into a gas box **46** (on the open field lines **48**) where it is ionized. The cold plasma flows along the open field lines, out the box and through the SOL **50**. The cold plasma density and temperature in the SOL are controlled by the rate of gas introduced into the gas box **46**. Further control can be

15 achieved by widening and constricting a variable-size orifice **52**, attached to the gas box's opening. When near the FRC's midplane **54**, the SOL plasma particles, e.g., the plasma electrons, are heated by the kinetic energy of the reaction products. The cooled fusion products, including tritium, deuterium, and/or hydrogen plasma, flows along the open-field-region magnetic-field lines **46** and is directed out of the engine through a magnetic

20 nozzle **56**.

[0038] Thrust control can be achieved through multiple methods. Since power P is directly proportional to the thrust T multiplied by the exhaust velocity U_E , such that $P = 0.5TU_E$, thrust can be traded for exhaust velocity at a given power. The reaction products are highly energetic. For example, if the products of $D-^3\text{He}$ were used directly

for propulsion they produce an exhaust velocity of 25,000 km/s. However, in such a case, the thrust-to-power ratio would be 1/12,500 Newtons per kW. This ratio can be improved and carefully controlled by the amount of cold propellant introduced into the gas box **46**. Another way to control the thrust is through the variable sized orifice on the gas box **52**,
5 which can alter the thickness of the scrape off layer. Finally, using different propellants changes the mass and therefore the exhaust velocity. For example, deuterium propellant would have lower exhaust velocity than hydrogen.

[0039] The actual mechanism of thrust augmentation is depicted in one possible configuration of a cross-section of such an FRC in Figure 4. The RMF_o antenna **58**
10 produces a high power density of fusion with low neutron production within the core plasma **60**. The size and magnetic field produced by superconducting magnetic coils **62** or permanent magnets are such that more than 90% of the fusion reaction products pass through the SOL **64** on their first orbit. There, they exchange energy with the warm plasma **66**, increasing its velocity. Additionally, the surface-to-volume ratio of the FRC is
15 large, reducing the neutron power-load density on the reactor chamber walls of a vacuum vessel **68** and component degradation. However, some radiation from Bremsstrahlung, synchrotron, and neutrons will occur and may be absorbed by a shield **70**.

[0040] Another configuration of the FRC wall is shown in Figure 5. Multiple techniques for protecting the reactor chamber **72** are depicted. Neutrons **74** are unaffected
20 by the magnetic field and are expelled directly out of D-D side reactions, but can cause significant damage to the reactor structure, magnets, antennae, and especially sensitive electronics. Neutron shielding **76** is usually constructed from materials with low atomic numbers, like hydrogen, water, helium, boron, and beryllium. While the Bremsstrahlung and synchrotron radiation have a fairly broad spectrum, the former is mostly released as

X-rays and the latter as microwaves. Microwaves **78** are simply reflected by surfaces with low emissivity **80**, *i.e.* that are shiny. Medium atomic weight materials can absorb X-rays **82**, heating materials in heat exchangers for energy conversion **84**.

[0041] To create useful thrust, the propellant must detach from the magnetic field lines
5 of the rocket engine because these field lines eventually reverse direction and return to the rocket's nose. Detachment may be brought about by a number of processes, one of which is depicted in Figure 6. Since neutral atoms **86** are not bound to the field lines **88**, one generic method is to neutralize the ions **90** by attaching electrons to them. This can be done in the same way as the neutral beam is generated, using charge-exchange in a gas
10 box **92**, or less easily by radiative recombination. Another detachment method is to unmagnetize the ions by accelerating them to such high speeds that their gyroradii greatly exceed the rocket size. Finally, the plasma pressure of the exiting propellant can be increased to the point where it exceeds the magnetic field energy density. For an expanding plasma, the ratio of the plasma pressure to the magnetic field energy density
15 naturally increases with increasing distance from the magnetic nozzle. Eventually this causes the entire flowing "blob" of plasma to tear itself away from the magnetic field.

[0042] As mentioned above, an important disadvantage of conventional fusion engines is that, while providing high specific impulse, they provide relatively low thrust. The system described above overcomes this disadvantage by augmenting thrust through the
20 injection of feedstock propellant gas into scrape-off-layer surrounding the fusing plasma. This fusion engine with augmented thrust capability is achieved with a substantially smaller reactor than conventional systems. This reduces the amount of helium-3 fuel required to sustain a reaction leading to longer mission duration times.

Finally, the thrust augmentation system described above provides more precise control of the augmentation processes, leading to increased efficiency.

[0043] Although the scenarios herein have been described with reference to particular embodiments, it is to be understood that these embodiments are merely illustrative of the principles and applications of the disclosed scenarios. It is therefore to be understood that
5 numerous modifications may be made to the illustrative embodiments and that other arrangements may be devised without departing from the spirit and scope of the disclosed scenarios as defined by the appended claims.

CLAIM

1. A system comprising a rocket engine employing nuclear fusion with thrust augmentation, the system comprising

a reactor chamber for containing a stable plasma comprising a fusion fuel;

5 a heating system for heating said plasma and increasing an ion energy of said plasma to a level sufficient for producing net power from fusion reactions in said stable plasma;

a plurality of magnets coaxial to said reactor chamber, the plurality of magnets producing a magnetic sufficient to confine the stable plasma and promote rapid loss of
10 fusion products into a scrape off layer;

a fuel injection system for injecting additional quantities of said fusion fuel to sustain the power output of said fusion reaction;

a gas box at one end of said scrape off layer for introducing a cold propellant to be heated in the reactor chamber into a warm propellant plasma;

15 a propellant injection system for injecting said cold propellant into said gas box to augment the mass of said scrape off layer;

a magnetic nozzle for directing said warm plasma on said scrape off layer out of the end of said reactor chamber distal from said gas box to create thrust; and

a propellant detachment system to allow the expelled propellant to separate from
20 said rocket engine's magnetic field in a well-directed stream.

2. The system of claim 1 wherein said fusion fuel comprises deuterium and helium-3.

3. The system of claim 1 wherein said plurality of magnets in conjunction with said plasma produces a magnetic field in a field-reversed configuration.

4. The system of claim 3 wherein the magnets are superconducting magnetic coils.

5

5. The system of claim 4 wherein the magnets are permanent magnets.

6. The system of claim 3 wherein the fuel injection system is a neutral beam.

10 7. The system of claim 6 wherein the propellant is deuterium.

8. The system of claim 6 wherein the propellant is hydrogen.

9. The system of claim 6 further comprising at least one energy conversion system.

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10. The system of claim 9 wherein the heating system employs radio frequency odd-parity rotating magnetic fields produced by radio frequency magnetic coils.

11. The system of claim 10 further comprising a shield for attenuating and deflecting radiation produced from fusion.

20

12. The system of claim 11 wherein said reactor chamber is a vacuum vessel which is transparent to radio frequencies.

13. The system of claim 12 wherein said gas box includes a variable sized orifice for controlling the thickness of the scrape off layer.

14. A method for augmenting the thrust a fusion powered rocket engine that includes a
5 reactor chamber for containing a stable plasma comprising a fusion fuel, a plurality of magnets coaxial to the chamber, a heating system, a fuel injection system, a propellant injection system coupled to a gas box at one end of the reactor chamber, and a magnetic nozzle at the end of the chamber distal to the gas box, the method comprising:

injecting, by the fuel injection system, the fusion fuel into the reactor chamber;

10 heating, by the heating system, the plasma such that the fuel is ionized and heated such that a sustained nuclear fusion reaction occurs in the plasma producing a net power;

forming, by the magnets, a magnetic field to confine the plasma and promote rapid loss of fusion products into a scrape-off-layer;

injecting, by the propellant injection system, a cold propellant into the gas box;

15 introducing, in the gas box, the cold propellant for warming in the reactor chamber and converting into a warm propellant plasma to increase the mass of the scrape-off-layer, wherein the warm propellant plasma flows through the scrape-off-layer and is heated by the fusion products;

20 expelling the warm propellant plasma and fusion products from the reactor chamber through the magnetic nozzle; and

detaching the expelled propellant from said rocket engine's magnetic field in a well-directed stream.

15. The method according to claim 14 wherein said fusion fuel comprises deuterium and helium-3.

16. The method according to claim 14, where in a field-reversed magnetic field
5 configuration is produced by the plurality of magnets in conjunction with the plasma.

17. The method according to claim 16, wherein plurality of magnets are superconducting magnetic coils.

10 18. The method according to claim 17, wherein the plurality of magnets are permanent magnets.

19. The method according to claim 16, wherein the fusion fuel is injected by a neutral beam.

15

20. The method according to claim 19, wherein the injected propellant is deuterium.

21. The method according to claim 19, wherein the injected propellant is hydrogen.

20 22. The method according to claim 19, further comprising converting energy from the fusion products into electricity.

23. The method according to claim 22, wherein the heating is accomplished by radio frequency odd-parity rotating magnetic fields produced by radio frequency magnetic coils.

24. The method according to claim 23, wherein converting the energy is accomplished by capturing electro-magnetic radiation in the radio frequency spectrum using radio frequency magnetic coils.

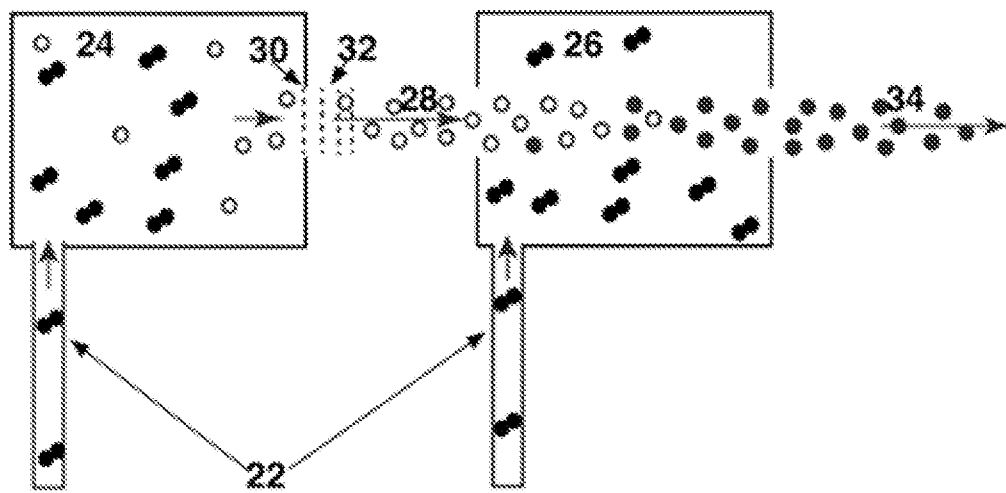
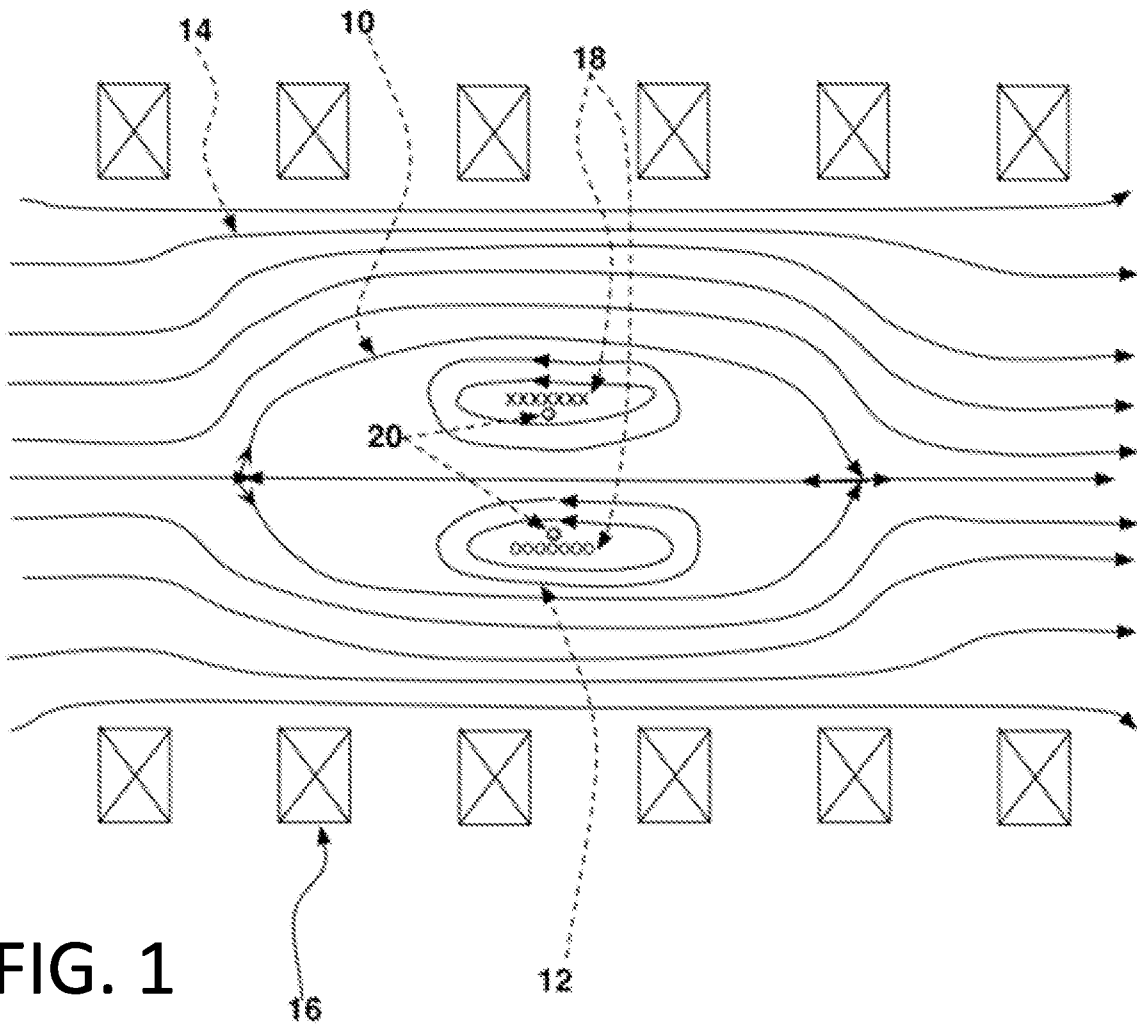
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25. The method according to claim 24, further comprising attenuating and deflecting the radiation produced from the fusion reaction with a shielding material.

26. The method according to claim 25, wherein heating by radio frequencies is enabled
10 by the use of a vacuum vessel for the reactor chamber, which is transparent to such frequencies.

27. The method according to claim 26, wherein controlling the thickness of the scrape off layer is accomplished by a variable sized orifice attached to the gas box.

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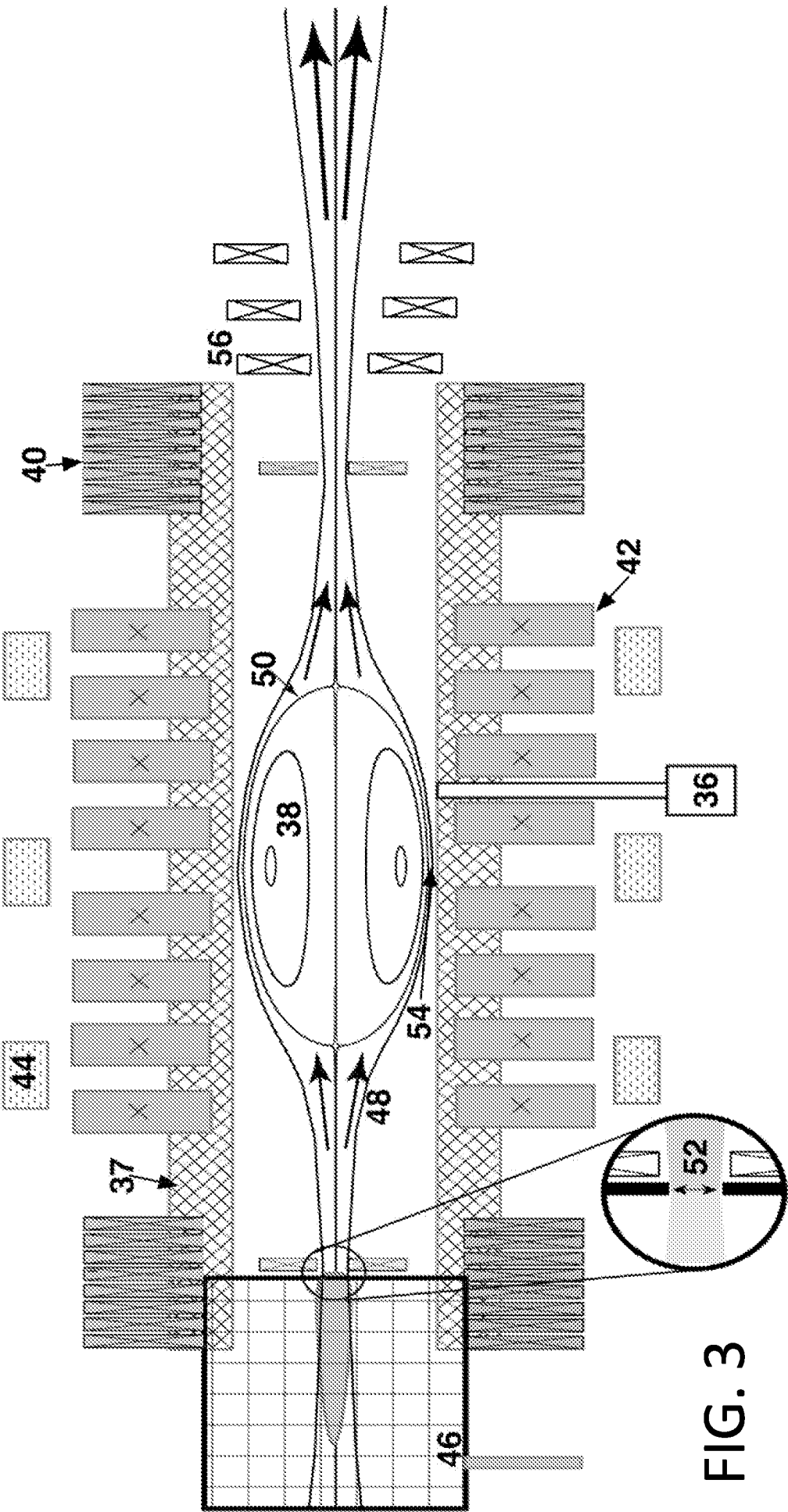


FIG. 3

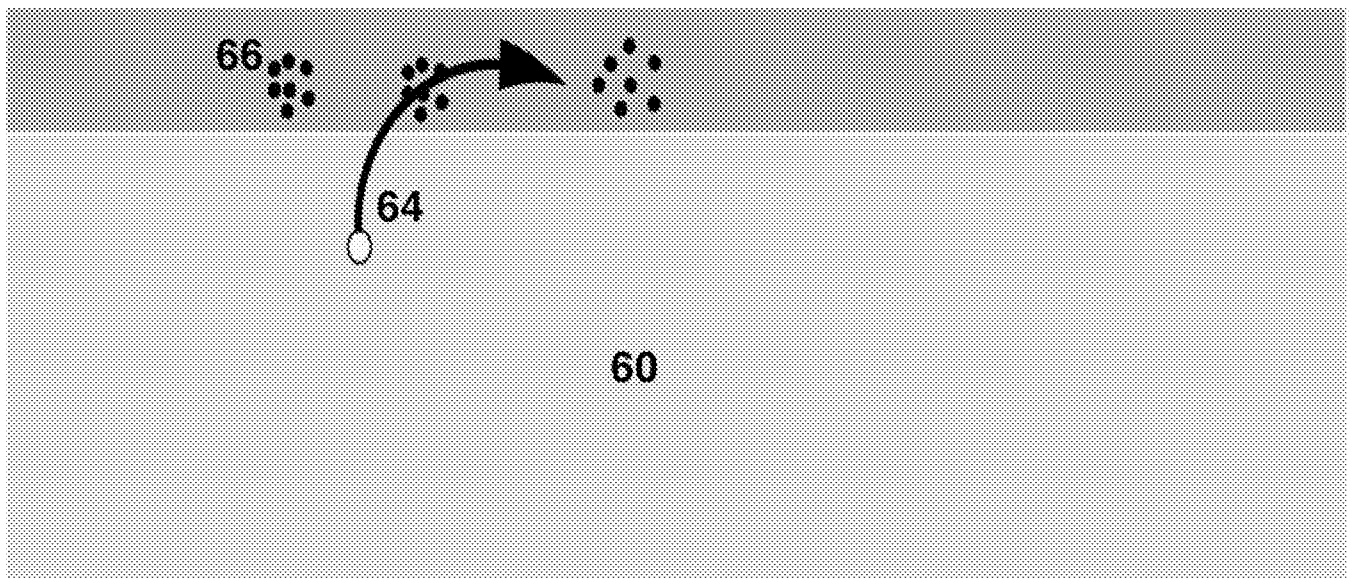
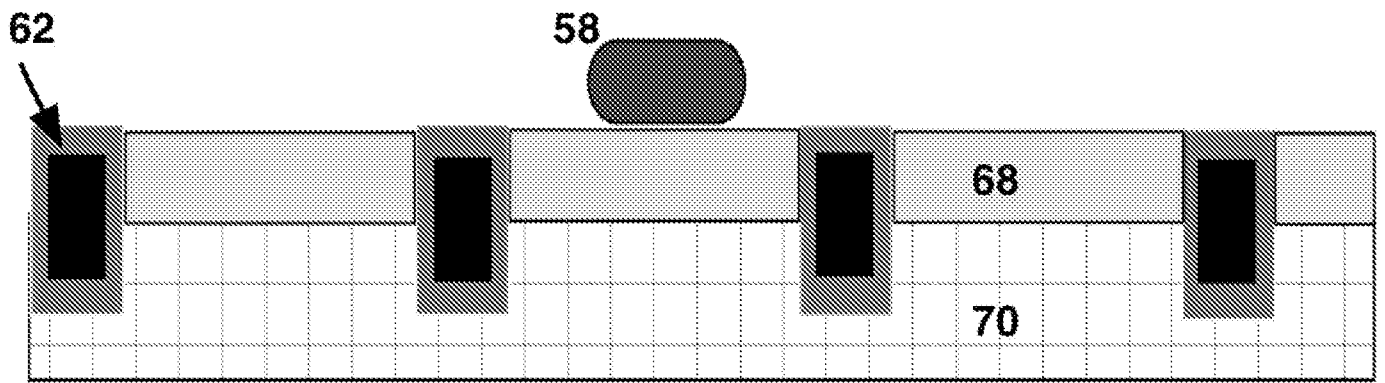


FIG. 4

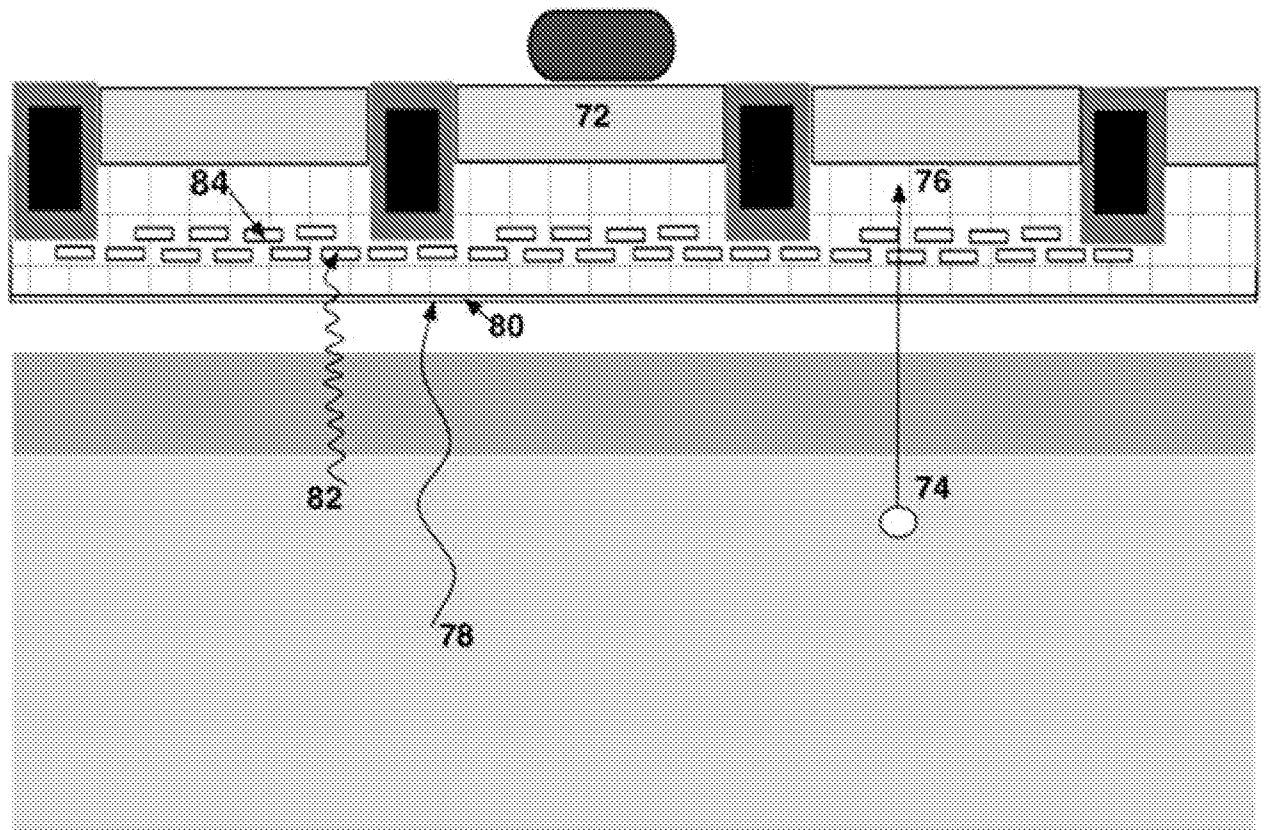


FIG. 5

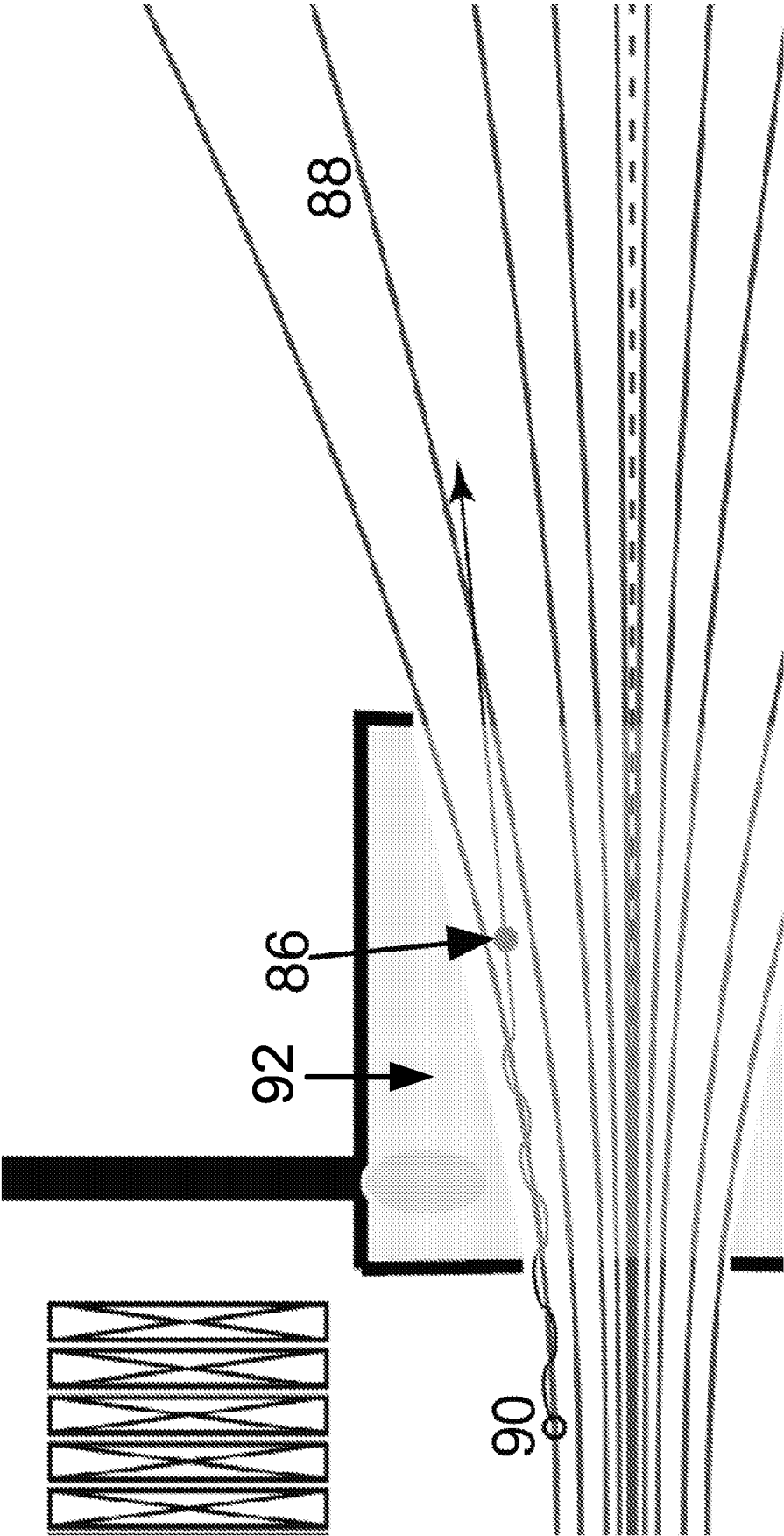


FIG. 6