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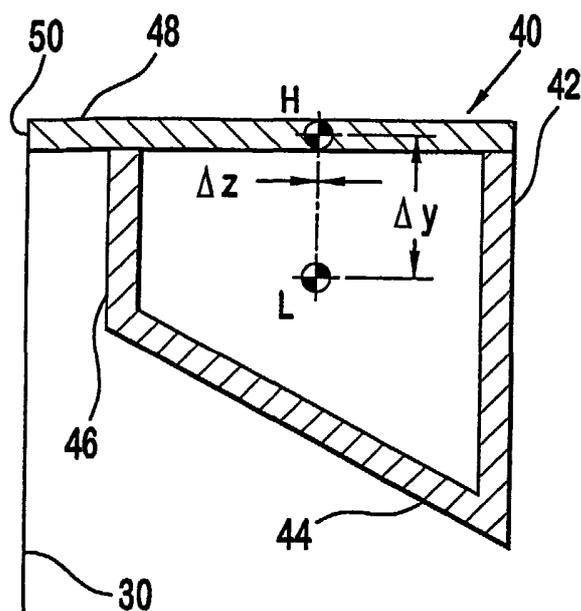
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(54) Title: TENSION MASK ASSEMBLY FOR A CATHODE RAY TUBE HAVING MASK DETENSIONING



(57) Abstract: A cathode ray tube (1) includes a tension mask (30) attached to a rectangular mask frame assembly (10) that has two long sides (22, 24) paralleling a central major axis X thereof and two short sides (26, 28) paralleling a central minor axis Y thereof. A pair of support blade members (40, 140) are attached each to one of the long (22, 24) or short sides (26, 28) at a central location. Each support blade member (40, 140) includes an inner edge having a plurality of first sides (42, 44, 46) formed from a relatively low coefficient of thermal expansion material and an outer edge having a second side formed of a material having a relatively high coefficient of thermal expansion. Each edge having a centroid separated from each other along the minor axis Y.

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**Tension Mask Assembly for a Cathode Ray Tube**  
**having Mask Detensioning**

**Field of the Invention**

5           This invention relates generally to cathode ray tubes, and more particularly to tension mask assemblies having detensioning features.

**Background of the Invention**

10           A color cathode ray tube, or CRT, includes an electron gun for forming and directing three electron beams to a screen of the tube. The screen is located on the inner surface of the faceplate panel of the tube and is made up of an array of elements of three different color-emitting phosphors. A shadow mask, which may be either a formed mask or a tension mask having strands, is located between the electron gun and the screen. The electron beams emitted from the electron gun  
15           pass through apertures in the shadow mask and strike the screen causing the phosphors to emit light so that an image is displayed on the viewing surface of the faceplate panel.

20           One type of CRT has a tension mask comprising a set of strands that are tensioned onto a mask support frame to reduce their propensity to vibrate at large amplitudes under external excitation. Such vibrations would cause gross electron beam misregister on the screen and would result in objectionable image anomalies to the viewer of the CRT.

25           The mask stress required to achieve acceptable vibration performance is below the yield point of the mask material at tube operating temperature. However, at elevated tube processing temperatures, the mask's material properties change and the elastic limit of the mask material is significantly reduced. In such a condition, the mask stress exceeds the elastic limit of the mask material and the material is inelastically stretched. When the tube is cooled after processing, the strands are longer than before processing and the mask frame is incapable of tensing the mask  
30           strands to the same level of tension as before processing. Another common problem with tension mask frame assemblies occurs when the mask strand material has a lower coefficient of thermal expansion than the mask support frame material. In such a case, tension on the mask strand increases during thermal processing causing more inelastic strain.

One detensioning system utilizes a dual compliant mask frame having a pair of support blade members centrally mounted on opposite sides of a frame wherein, tension is relieved at the center of the support blade member. Detensioning of the tension mask strands at the center when using a dual compliant frame may result in relatively greater tension on the strands toward the outsides or edges of the blade. In order to achieve a more uniform detensioning, in addition to the detensioning at the center, further detensioning is required at the edges of the mask.

It is therefore desirable to develop a mask frame assembly that allows the pattern and degree of the mask detensioning to be adjusted during the thermal cycle used in the manufacturing process of a CRT.

### **Summary of the Invention**

A tension mask assembly is provided having a frame consisting of two long sides disposed parallel to a central major axis and two short sides disposed parallel to a central minor axis which is orthogonal to the major axis. Support blade members are fixed to the frame along a central location of the long sides. Each support blade member includes an inner edge having sides formed of relatively low coefficient of thermal expansion material and an outer edge having at least one side or detensioning member formed of a relatively high coefficient of thermal expansion material. The centroid of each edge is separated from each other along the central minor axis.

### **Brief Description of the Drawings**

The invention will now be described by way of example with reference to the accompanying figures of which:

Figure 1 is a cross sectional view of a CRT showing a tension mask frame assembly.

Figure 2 is a perspective view of the tension mask frame assembly.

Figure 3 is a front diagrammatic view the tension mask frame assembly showing a support blade member at an elevated temperature.

Figure 4 is a cross sectional view taken along the line 4-4 of Figure 3.

Figure 5 is a cross sectional view similar to Figure 4 showing an alternative support blade member.

### Detailed Description of the Invention

Figure 1 shows a cathode ray tube (CRT) 1 having a glass envelope 2 comprising a rectangular faceplate panel 3 and a tubular neck 4 connected by a funnel 5. The funnel 5 has an internal conductive coating (not shown) that extends from an anode button 6 toward the faceplate panel 3 and to the neck 4. The faceplate panel 3 comprises a viewing faceplate 8 and a peripheral flange or sidewall 9, which is sealed to the funnel 5 by a glass frit 7. A three-color phosphor screen 12 is carried by the inner surface of the faceplate panel 3. The screen 12 is a line screen with the phosphor lines arranged in triads, each of the triads including a phosphor line of each of the three colors. A tension mask frame assembly 10 is removably mounted in predetermined spaced relation to the screen 12. An electron gun 13, shown schematically by dashed lines in Figure 1, is centrally mounted within the neck 4 to generate and direct three inline electron beams, a center beam and two side or outer beams, along convergent paths through the tension mask frame assembly 10 to the screen 12.

The CRT 1 is designed to be used with an external magnetic deflection yoke 14 shown in the neighborhood of the funnel-to-neck junction. When activated, the yoke 14 subjects the three beams to magnetic fields which cause the beams to scan horizontally and vertically in a rectangular raster over the screen 12.

The tension mask frame assembly 10, as shown in Figure 2, includes two long sides 22 and 24, and two short sides 26 and 28. The two long sides 22, 24 of the tension mask frame assembly 10 are parallel to a central major axis, X, of the tube; and the two short sides 26, 28 parallel a central minor axis, Y, of the tube. The two long sides 22, 24 and two short sides 26, 28 form a continuous planar mask support frame 20 along those major and minor axes.

The frame assembly 10 includes an apertured tension shadow mask 30 (shown here diagrammatically as a sheet for simplicity) that contains a plurality of metal strips (not shown) having a multiplicity of elongated slits (not shown) therebetween that parallel the minor axis, Y, of the tube. The mask 30 is fixed to a pair of support blade members 40 which are fastened to the frame 20 at attachment points 52. The support blade members 40 may vary in height from the center of each support blade member 40 longitudinally to the ends of the support blade

member 40 to permit the best curvature and tension compliance over the tension shadow mask 30.

Referring now to Figures 3 and 4, the support blade member 40 will be described in greater detail. Figure 4 shows a cross sectional view of the support blade member 40 taken along the line 4-4 of Figure 3. The support blade member 40 is a closed structure consisting of a plurality of first sides 42, 44, 46 formed of a material having a relatively low coefficient of thermal expansion hereinafter referred to as low expansion material and a side 48 consisting of a material having a relatively high coefficient of thermal expansion hereinafter referred to as high expansion material. Each of the sides 42, 44, 46, 48 may be either bent from a single piece, welded together, or attached by any other suitable means. The mask 30 is applied at a mask receiving edge 50 along the side 48. The support blade member 40 is attached to the subframe 20 at attachment points 52 located approximately at the center of opposing frame long sides 22, 24.

Figure 3 illustrates that these attachment points 52 are positioned at a distance  $\alpha$  from each other. This distance  $\alpha$  increases during the thermal heating cycle of the manufacturing process due to thermal expansion of the frame 20. In a dual compliant frame arrangement, the frame 20 is designed such that the long sides 22, 24 bow inward toward each other when heated to relieve tension on the mask 30. Since the support blade members 40 are flexible and have some compliance, the center of the mask is detensioned more than the edges. As best shown in Figure 3 the support blade member 40 deflects or curls from its resting position toward the major axis, X, indicated by solid lines to a deformed position indicated by dashed lines. The deformation occurs during heating such that the distal ends of the support blade member 40 move a distance  $\beta$  indicated in Figure 3. This deformation is caused by the high expansion material being positioned on the outer edges of the support blade member 40 which acts as a detensioning feature because the outer edge essentially expands more rapidly than the inner edge. The movement indicated by the distance  $\beta$  relieves the increased tension at the distal ends of the support blade member 40 and along the edges of the mask 30 thereby providing the opportunity for detensioning the edges of the mask independently from the center and thus allowing the pattern and degree of mask detensioning to be adjusted by the amount of blade detensioning used. It should be understood that while deformation

is shown in a single support blade member 40 at the top of Figure 3, the bottom support blade member 40 also deforms similarly during heating.

The effect of the invention will be described with reference to Figure 4. A pair of centroids L, H are shown wherein L is the centroid of the first sides 42, 44, 46 which are formed of low expansion material while H indicates the centroid of the side 48 formed of high expansion material. The centroids L, H are separated from each other along the minor axis Y and both lie within the XY plane with no separation in the Z plane. The deformation of the support blade member 40 during heating is therefore controlled in the X, Y plane by the distance  $\Delta Y$  while remaining stable in the Z direction as indicated by  $\Delta Z = 0$ .

Figure 5 shows an alternative embodiment of the support blade member 140. This support blade member 140 is structurally similar to the support blade member 40 of Figure 4 except that the plurality of first sides 142, 144, 146 and the side 148 are formed from the same material to create the closed structure. This material is similarly a relatively low coefficient of thermal expansion material as was described above. A detensioning member or high coefficient member 149 is added along the side 148. It is formed of a material having a relatively high coefficient of thermal expansion. This high expansion member 149 may be welded or applied to the side 148 by other known techniques such as mechanical fasteners or adhesives. The high coefficient member 149 preferably has a rectangular cross section and extends over a majority of the side 148. It should be understood by those reasonably skilled in the art however that while shown in the cross section to cover a majority of the side, it is not necessary that this cross section extend over the entire length of the support blade member 140. The area of the side 148 which is covered by the high expansion member 149 may be adjusted to achieve various curl characteristics during heating. Alternatively, the high expansion member 149 may be segmented and secured along the length of the support blade member 140. This variation results in different amounts of detensioning on the mask at the distal ends of the support blade member 140. The effect of this alternative embodiment is similar to that described above with reference to Figure 4 wherein deformation of the support blade member 140 during heating is controlled by the distance  $\Delta Y$  between the centroids L, H while remaining stable in the Z direction.

An advantage of the present invention is the ability to detension the edge of the mask using the support blade member which is attached to the frame at a central

location. By adjusting the length of the high coefficient member the amount of detensioning at the edges may be controlled. A high expansion member extending over a longer portion of the support blade member will result in greater detensioning at the edges than a relatively shorter high coefficient member.

**CLAIMS**

1. A tension mask assembly (10) for use in a CRT (1) comprising:  
a mask support frame (20) formed by a pair of long sides (22, 24) and a  
5 pair of short sides (26, 28) attached together at their ends, the long sides (22, 24)  
extending parallel to a central major axis X and the pair of short sides (26, 28)  
extending parallel to a central minor axis Y; and,  
a pair of support blade members (40, 140) for securing a tension mask  
(30), each support blade member (40, 140) being attached to a respective one of the  
10 long sides (22, 24) at a central attachment point (52), the support blade members  
(40) each including a plurality of first sides (42, 44, 46, 142, 144, 146) formed of a  
first coefficient of thermal expansion material and defining a first centroid (L), and  
further including a second side (48, 148), the second side (48, 148) being secured to  
the first sides (42, 44, 46, 142, 144, 146) and formed of a second coefficient of  
15 thermal expansion material and defining a second centroid (H), the first and second  
centroid being generally defined by adjacent cross-sections of the first sides (42, 44,  
46, 142, 144, 146) and second side (48, 148) of the support blade member (40, 140),  
the first (L) and second centroid (H) separated at a predetermined distance from  
each other along the minor axis Y whereby the first and second centroids remain in  
20 alignment during thermal deflection of the support blade members (40).
2. The tension mask assembly (10) of claim 1 wherein the plurality of first  
sides (42, 44, 46, 142, 144, 146) of the support blade member (40) form a closed  
structure.
3. The tension mask assembly (10) of claim 1 wherein the second side  
25 (48, 148) of the outer edge extends over a portion of the inner edge.
4. A tension mask assembly (10) for use in a CRT (1) having a  
substantially rectangular  
mask support frame (20) including a central major axis X and a central minor axis Y  
perpendicular to each other, the frame (20) formed from a pair of opposing long  
30 sides (22, 24) extending in parallel to the major axis X and a pair opposing short  
sides (26, 28) extending in parallel to the minor axis Y, a support blade member (40,  
140) to which a tension mask (30) is attached and supported to the frame (20) at an  
attachment point (52) along one pair of opposing side, the support blade member  
(40, 140) comprising:

an inner edge facing the central major axis and formed from a material having a first coefficient of thermal expansion; and, an outer edge formed from a second material having a relatively greater coefficient of thermal expansion than the inner edge and being fixed to the inner edge wherein the centroid (L) of the inner edge and the centroid of the outer edge (H) is separated along the minor axis Y.

5           5.     A tension mask assembly (10) of claim 4 wherein the tension mask (30) is secured to the outer edge of the support blade member (40, 140).

10           6.     The support blade member (40, 140) of claim 4 wherein the outer edge extends along a portion of the inner edge whereby the distal ends of the support blade member (40, 140) curl inward toward the major axis X during thermal heating.

            7.     The support blade member (140) of claim 4 wherein the outer edge comprises a plurality of detensioning members (148, 149).

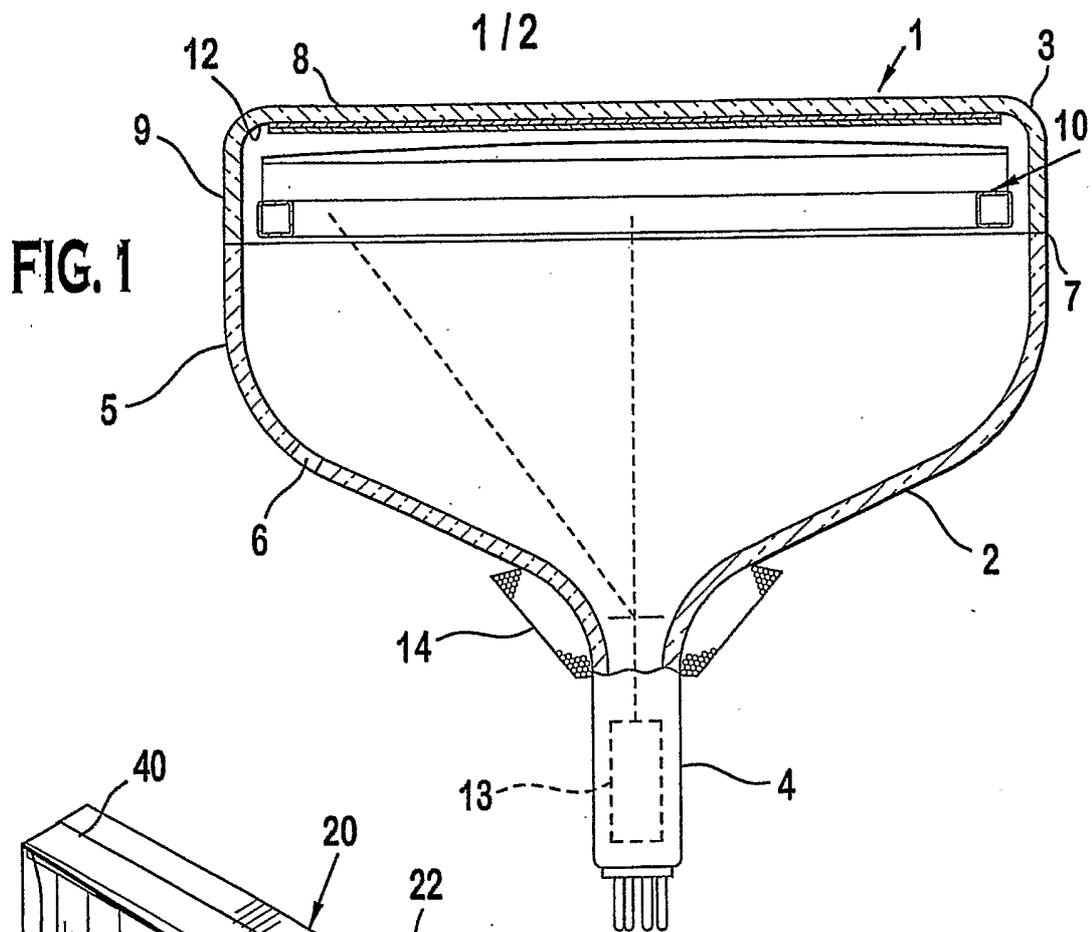


FIG. 1

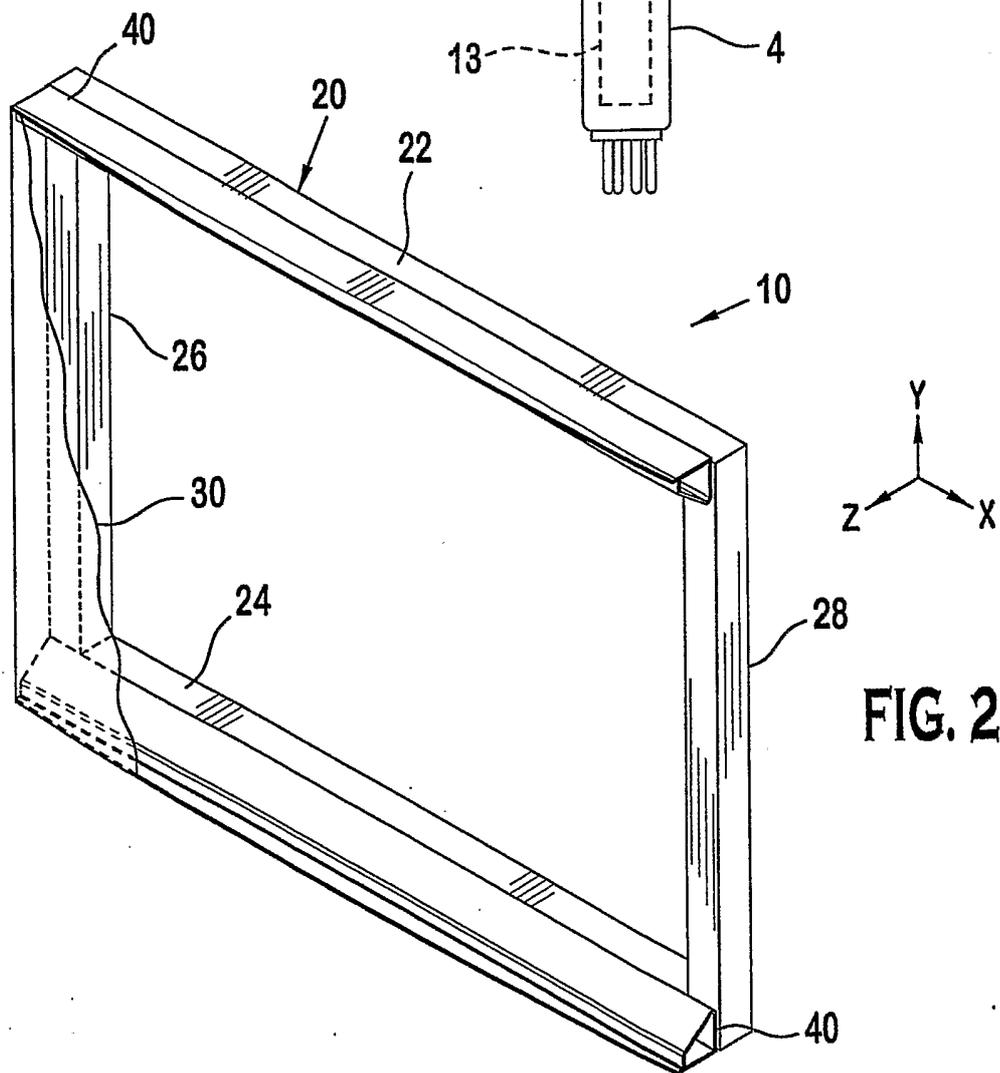


FIG. 2

FIG. 3

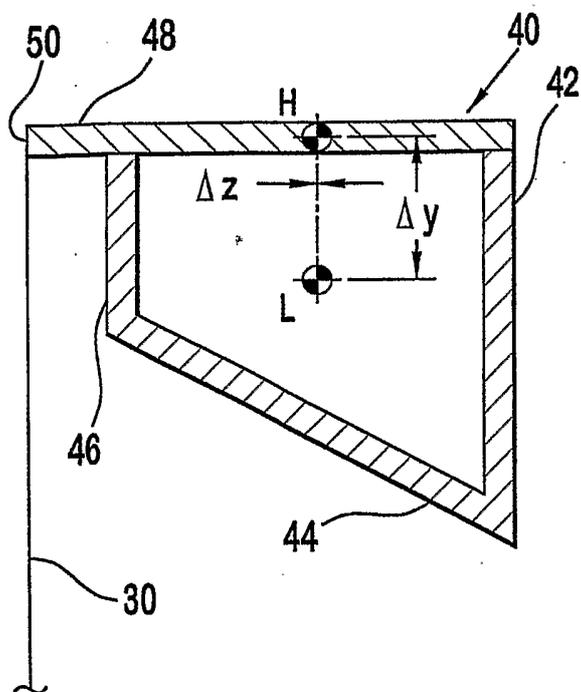
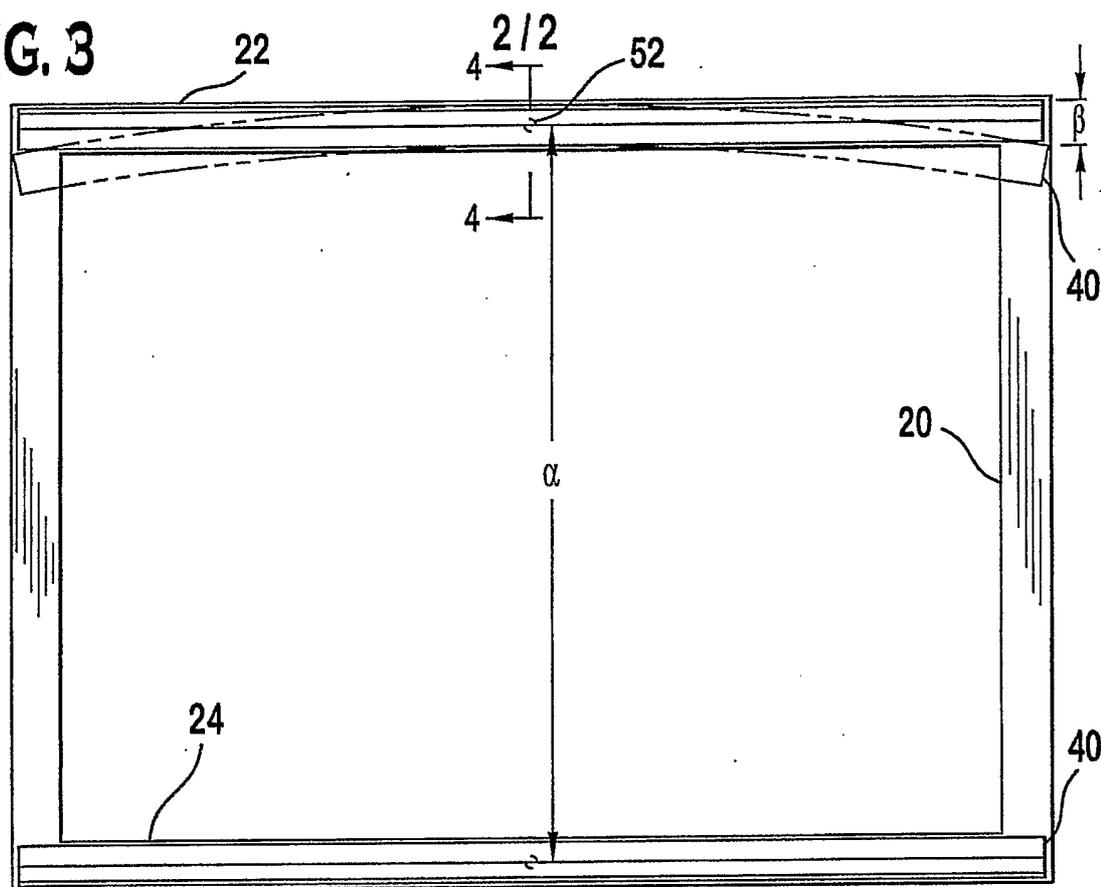


FIG. 4

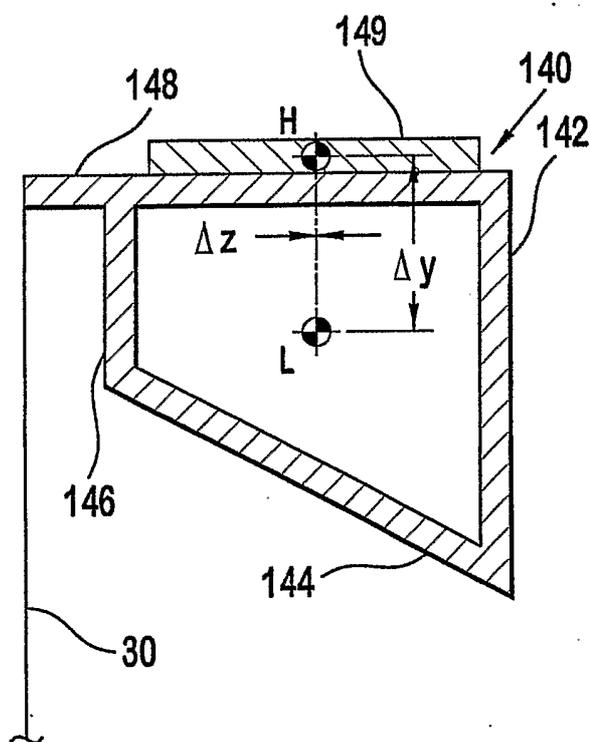


FIG. 5

INTERNATIONAL SEARCH REPORT

Int Application No  
PCT/US 02/24813

A. CLASSIFICATION OF SUBJECT MATTER  
IPC 7 H01J29/07

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 H01J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 952 774 A (DIVEN GARY LEE ET AL) 14 September 1999 (1999-09-14) figures 3-6 column 3, line 15 - line 43 ---	4
A	US 6 246 164 B1 (HEYMAN PHILIP MICHAEL ET AL) 12 June 2001 (2001-06-12) figure 3 column 2, line 54 - line 64 column 3, line 1 - line 6 column 3, line 27 - line 29 column 4, line 1 - line 6 ---	1, 4
A	US 6 084 342 A (RAGLAND JR FRANK ROWLAND) 4 July 2000 (2000-07-04) figures 5,6 -----	1, 4

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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Date of the actual completion of the international search

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# INTERNATIONAL SEARCH REPORT

Information on patent family members

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