

March 18, 1947.

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2,417,543

TUNING INDICATOR FOR FREQUENCY SHIFT CARRIER TELEGRAPH SYSTEMS

Filed Jan. 5, 1946

3 Sheets-Sheet 1

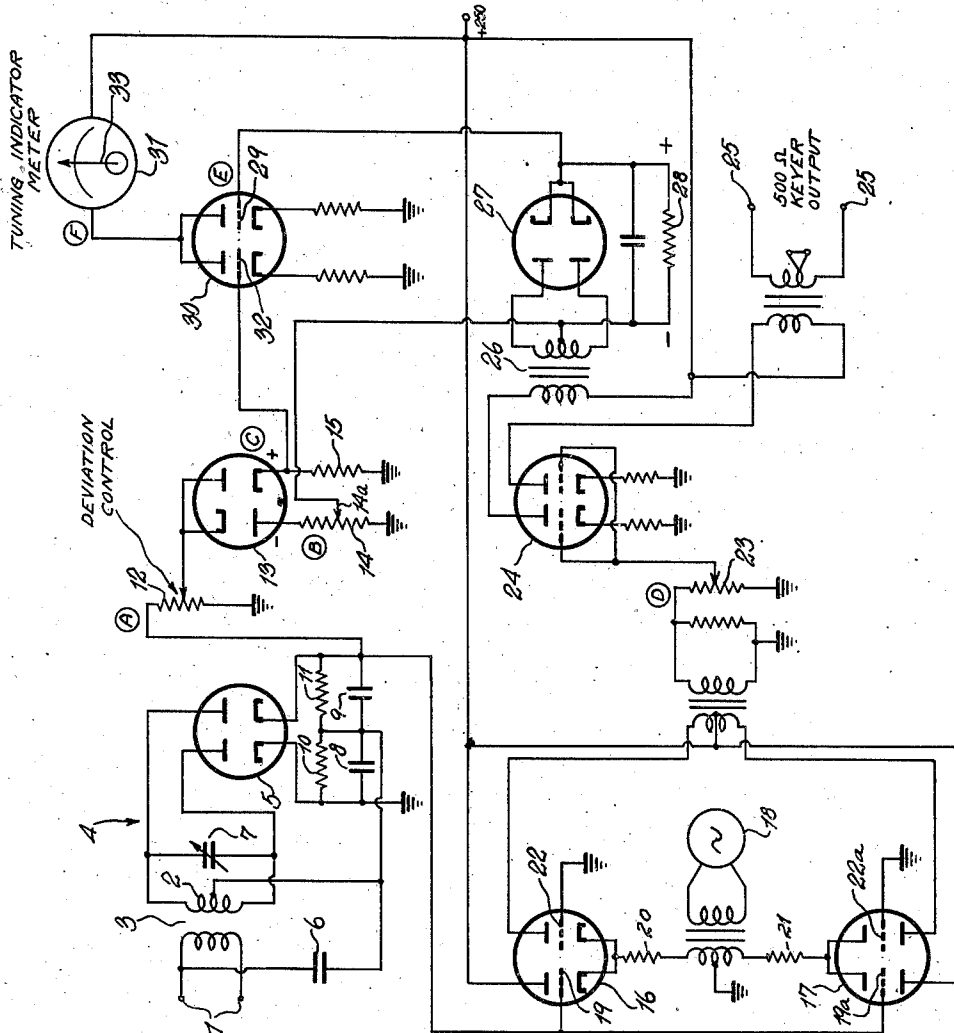


Fig. 1

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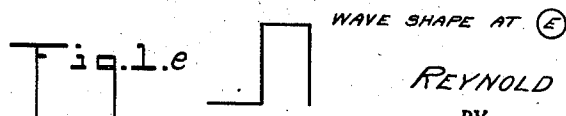
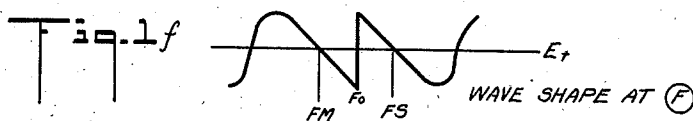
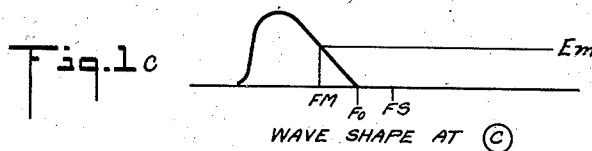
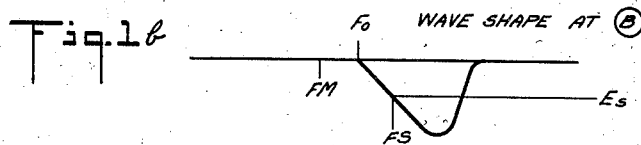
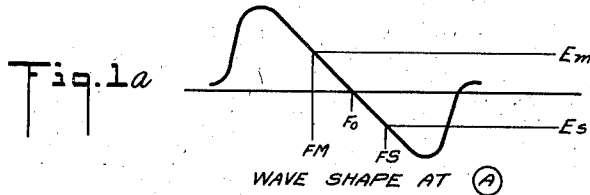
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TUNING INDICATOR FOR FREQUENCY-SHIFT CARRIER TELEGRAPH SYSTEMS

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3 Sheets-Sheet 2

IN TUNE CONDITION  
WAVE SHAPE VS FREQUENCY



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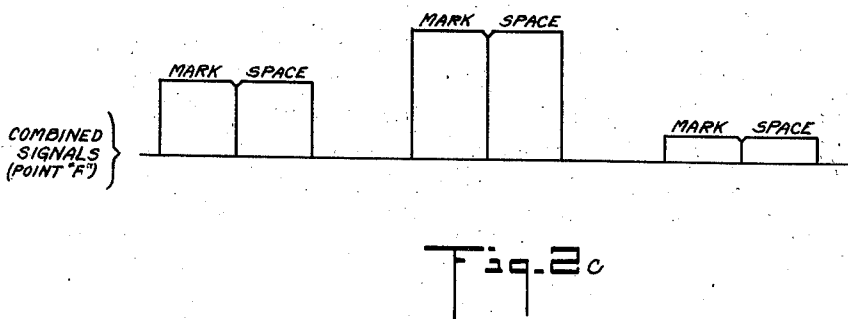
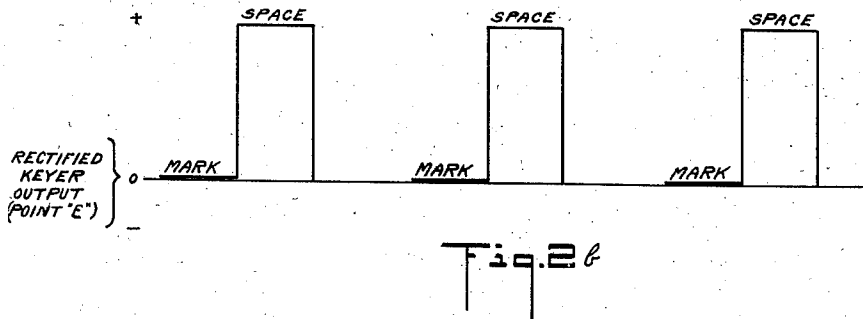
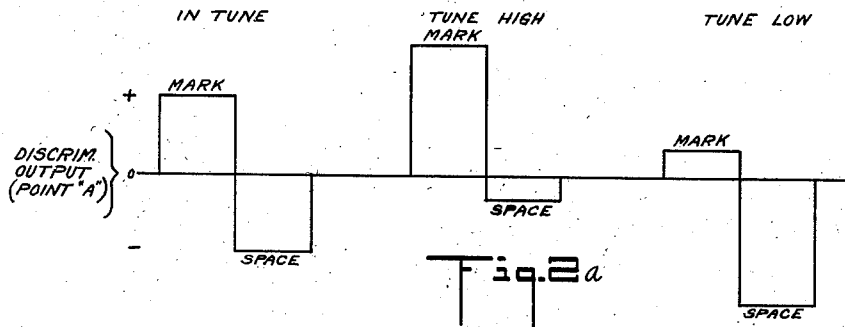
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TUNING INDICATOR FOR FREQUENCY SHIFT CARRIER TELEGRAPH SYSTEMS

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3 Sheets-Sheet 3

MARK-SPACE SIGNALS



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## UNITED STATES PATENT OFFICE

2,417,543

TUNING INDICATOR FOR FREQUENCY  
SHIFT CARRIER TELEGRAPH SYS-  
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tion of Delaware

Application January 5, 1946, Serial No. 639,262

10 Claims. (Cl. 178-66)

1

This invention relates to wave signalling systems and more particularly to improvements in the signalling systems of the frequency shift category.

A principal object of this invention is to provide an improved tuning indicator for use in controlling the "in-tune" condition of frequency shift telegraph apparatus.

A feature of this invention relates to a discriminator and detector combination having the components so correlated and connected as to provide a characteristic having a plurality of crossover points with the zero potential axis.

Another feature relates to a differential discriminator and electron tube network for use with a frequency shifted carrier wherein any out-of-tune or undesired frequency shift condition in the system results in potential changes of substantially the same magnitude and sign at both ends of the shift range.

A further feature relates to a discriminator and electron tube network for providing a sawtooth over-all relation between input frequency and output potential.

A still further feature relates to the limiting tone keyer network whereby the adverse effects of bias variations caused by detuning of the incoming signals and those caused by noise are substantially reduced.

A still further feature relates to the novel organization, arrangement and relative interconnection of parts which cooperate to provide an improved tuning control circuit for carrier frequency shift receiver systems.

Other features and advantages not particularly enumerated will be apparent after a consideration of the following detailed descriptions and the appended claims.

In the drawing which represents one preferred embodiment,

Fig. 1 shows in schematic form, a frequency shift control and tuning indicator arrangement embodying the inventive features.

Figs. 1a to 1f are diagrams explanatory of the wave forms present at corresponding points in the embodiment shown in Fig. 1.

Figs. 2a, 2b and 2c represent the mark and space signals for different conditions of tuning.

When signalling is effected by frequency shifting of a radio carrier, the radiated wave in the case of telegraph transmission consists of a marking frequency and a spacing frequency. When such systems are provided with automatic frequency control or tuning indicators to keep the apparatus in the "in-tune" condition, separate control channels are required for the two condi-

2

tions corresponding respectively to mark and space. This has been necessary because of the frequency versus voltage characteristics of the usual discriminators. The conventional discriminators have only a single crossover with the zero output axis, regardless of whether the system is in tune or out of tune, and this crossover point corresponds to the mean frequency of the limits between which the carrier is shifted for mark and space. When the frequency of the carrier drifts, it is manifested by a change in detected output. With respect to the reference potential axis the detected output will increase during one of the keying signals and decrease during the other keying signal for a condition of mistuning. Since the transmitted wave may rest on either the mark or space condition for indefinite time intervals, any tuning indicator or automatic frequency control device must respond equally to either condition. This invention provides apparatus having the necessary equal change output at the mark and space frequency, regardless of the amount of frequency drift or out-of-tune condition. The discriminator and rectifier combination has an over-all characteristic in which their two points of crossover with the zero voltage axis and output potentials vary by the same amount in polarity for a given change in tuning of the receiving apparatus.

I have disclosed in my prior application Serial No. 615,838, filed September 12, 1945, a frequency discriminator and detector arrangement having the necessary equal change of output at the mark and space frequencies. My prior application requires a special form of electronic or electromagnetic switch for controlling the required tuning indications. The present invention is in the nature of an improvement on and simplification of the system of my prior application. In the present invention no electronic or electromagnetic switches are required and instead of using an electronic limiter to produce a voltage which eventually causes a shift of the space signal, a rectified tone keyed signal is used to produce the same result. In practice, a tone keyer is usually incorporated in the terminal equipment and may also be used to provide a source of D. C. voltage which may be utilized in shifting one portion of the discriminator characteristic.

Referring more particularly to Fig. 1, the received telegraph signals are applied across terminals 1, these signals being received from any well-known source of frequency shifted carrier waves such as a frequency shift telegraph transmitter. If the carrier wave has a mean frequency of  $F_0$  it may be shifted in one direction to a frequency

$F_m$  to represent a mark signal, and in the opposite direction to a frequency of  $F_s$  to represent a space signal. This carrier wave may be received by any well-known radio receiver and the output of this receiver fed to terminals 1. For a detailed description of a typical carrier frequency shifting arrangement, reference may be had to application Serial No. 498,278, filed August 12, 1943.

Energy is fed from terminals 1 through audio transformer 3 into any well-known balanced frequency discriminator network 4. The frequency versus output voltage characteristic of this discriminator is shown in Fig. 1a.  $F_m$  indicates a "mark" voltage at the discriminator output,  $F_0$  the mean frequency voltage, and  $F_s$  the "space" voltage. This characteristic shows a substantially linear change in output voltage with frequency over the frequency range between the positive and negative peaks. This balanced differential frequency discriminator comprises dual diode tube 5, coupling condenser 6, tuning condenser 7, by-pass condensers 8 and 9, and equal load resistances 10 and 11 connected in balanced relationship to secondary 12 of transformer 3.

In order to determine when the input to terminals 1 is in proper tune with respect to the mean frequency of the shifted carrier wave, a potentiometer 12 is connected across the output of the discriminator network 4. It is the purpose of dual diode tube 13 which is connected to potentiometer 12, to separate the positive and negative portions above the mean frequency  $F_0$  of the discriminator characteristic shown in Fig. 1a. This is necessary because a change in the mean transmitted frequency  $F_0$  or in the tuned condition of the receiver supplying energy to terminals 1 will cause the original mark and space frequencies to be represented by respective voltages of different magnitudes. After these positive and negative portions are separated by tube 13 and its associated circuit, they are later combined thereby creating a new characteristic which exhibits exactly the same mark and space voltage for any condition of receiver tuning. The separated negative portion appears across resistor 14 while the separated positive portion appears across resistor 15. These separated portions are shown in Figs. 1b and 1c respectively.

The output voltage of the discriminator network 4 is also fed to the tubes 16 and 17 which comprise a limiting tone keyer. The source of audio frequency oscillations 18 represents the tone to be keyed. The output characteristic of this keyer is such that an increase in the keying wave causes a linear increase in the keyed tone output until a certain amplitude is reached beyond which an increase of the amplitude of the keying waves causes no appreciable increase in the keyed tone output. It is seen that this amplitude limiting has the effect of removing variations of signal strength, which may be due to noise components affecting the peaks thereof.

As the grids 19 and 19a of dual tubes 16 and 17 become more positive, more current flows through the cathode resistors 20 and 21. This is equivalent to having a high negative bias on the grids 22 and results in a downward modulation of the applied signals. For high positive bias on grids 19 cut-off occurs and a space is left between signals. Conversely as the grids 19 become more negative, less current flows through cathode resistors 20 and 21 and the effective bias on grids 22 increases. This results in an upward modulation of the applied signals for higher negative bias on grids 19. At a certain value

of negative bias, the tubes associated with grids 19 cut-off, thereby limiting the tone output to a fixed value which will not rise above the cut-off point of the tubes. This provides a tone output amplitude limiter.

The tone keyer output is shown in the full line wave of Fig. 1d. The dotted positions of these waves represent the variable amplitude noise variations that might be present if not one limiter were used. The keyed tone appears across the potentiometer 23 and consists of an oscillator frequency keyed on and off in accordance with the mark and space signals. The potentiometer 23 allows the desired level of keyed output to be applied to the amplifier 24.

One section of twin triode amplifier 24 is used to amplify the keyed tone voltage appearing across potentiometer 23 and deliver it to the 500 ohm keyer output terminals 25. The other triode section of amplifier 24 amplifies the keyed tone voltage and feeds it through transformer 26 to the push-pull diode rectifier 27. When the tone keyer is in the "off" condition, there is no output across the rectifier load resistance 28. When the keyer is in the "on" condition, a voltage appears across resistance 28 and has a polarity as indicated in Fig. 1e.

The positive voltage appearing across resistor 28 is in series with the negative voltage appearing across resistor 14. The resultant of these voltages is conveyed to the grid 29 of linear amplifier 30. Fig. 1e shows the shape of the resultant positive voltage wave which is made equal in value by means of potentiometer arm 14a, to the positive voltage across resistor 15. The effect of this action is to shift the negative portion of the discriminator characteristic shown in Fig. 1b in a positive direction, thereby producing the characteristic shown in Fig. 1f. This characteristic exhibits itself at the tuning meter 31 connected in the output circuit of linear amplifier 30. It will thus be seen that grid 32 is excited with a positive voltage which is independent of the tone keyer, while grid 29 is excited with an equal positive voltage which is the resultant of the voltages at point B and the rectified tone-keyed voltage appearing across resistor 28.

From Fig. 1f it is seen that  $F_m$  and  $F_s$  are of the same value. If the input to terminals 1 should drift, the resultant voltage of  $F_m$  and  $F_s$  will remain the same since these two signals equally increase or decrease with respect to the in-tune voltage  $E_t$  and their direction of change is dependent upon the direction of the input drift. The voltages applied to the linear amplifier 30 are such that the resultant current passed through the meter 31 is proportional to the voltages applied to grids 29 and 32. Since both mark and space signals  $F_m$  and  $F_s$  are of the same voltage, the same current will flow through meter 31 for the mark signal and space signal.

By calibration of meter 31, the detuning from the mean frequency  $F_0$  of the received signals at terminals 1 may be read directly from the meter scale. The current resulting from the in-tune  $E_t$  should cause one-half scale deflection of meter pointer 33, and this position should be calibrated as the zero frequency position. The pointer 33 will then indicate the amount and direction of the detuning of the received signals.

The potentiometer 12 is termed the deviation control and is adjusted to produce the voltage  $E_t$  (Fig. 1f) for any deviation within the range of the equipment. This adjustment will change

5

simultaneously the slope of each portion of the saw-tooth characteristic shown in Fig. 1f. Adjustment of potentiometer 14 compensates for numerous irregularities and enables balance of the mark and space voltages shown in Fig. 1f and appearing at meter 31.

While there has been here described a specific embodiment, various changes and modifications may be made therein without departing from the spirit and scope of the invention.

What is claimed is:

1. In a telegraph system for receiving a carrier frequency  $F_m$  representing a telegraph mark signal and a carrier frequency  $F_s$  representing a telegraph space signal and including a receiver for said frequencies normally tuned to produce a predetermined base potential representing a mean frequency between  $F_m$  and  $F_s$ , a balanced differential discriminator for producing mark and space voltages in response to said frequencies, rectifier means connected to said discriminator to produce positive and negative D. C. voltages corresponding to said signals, a source of sustained tone frequency, means to key said source on and off in synchronism with the received signals, means to rectify and combine a portion of the keyed output of said source with one of said D. C. voltages to produce a resultant, and a tuning control indicator which is energized by the other of said D. C. voltages and by said resultant.

2. In a telegraph system for receiving frequency shift telegraph mark and space signals, means to convert said signals into corresponding positive and negative D. C. voltages, means to key a tone source by said signals, means to rectify a portion of said keyed tone signals, a tuning control indicator, and means to control said indicator jointly by said voltages and by the rectified portion of said keyed tone.

3. A telegraph system according to claim 2 in which said means for keying said tone source includes a rectifier for producing a positive D. C. potential only when a space signal is being received, and means are provided for combining said D. C. positive potential with said negative D. C. voltage.

4. In a telegraph system, means to receive two frequencies representing respectively mark and space, a balanced discriminator and rectifier for producing respective positive and negative D. C. voltages corresponding to said signals, a source of sustained tone, means to key said source on and off under control of the output of said discriminator, means to rectify the keyed tone signal to produce a positive D. C. voltage, a pair of grid-controlled amplifier paths, means to combine said rectified tone signal with the negative D. C. voltage from said discriminator rectifier to produce a resultant, means to apply said resultant to one of said amplifiers, means to apply the positive rectified discriminator voltage to the other of said paths, and a common output circuit for the plates of both said amplifier paths, said output circuit including a tuning indicator device.

5. A telegraph system according to claim 4 in which means are provided for limiting the amplitude of the keyed tone signals.

6. A wave signalling frequency shift system including a balanced differential frequency discriminator which has a frequency versus potential characteristic having positive and negative portions symmetrical with respect to a predetermined mean frequency, a positive and negative

6

wave separating circuit, a limiting tone keyer electronic circuit connected to the output of said discriminator, a push-pull diode rectifier cooperating with said keyer, and connected to the output of said wave separating circuit whereby the positive output voltage of said rectifier is in series with the said negative output, a grid-controlled linear amplifier having the above-mentioned series positive output voltage and negative output voltage impressed upon said grid, and tuning indicator means in the output circuit of said amplifier whereby the voltage applied to said amplifier is equal to the positive voltage output of said separate circuit.

7. A claim in accordance with claim 6, wherein said tuning indicator means comprises a current meter calibrated to indicate the frequency deviation from said mean frequency.

8. In a system for receiving a frequency-shifted carrier wave and including a balanced differential discriminator, a positive and negative signal wave separating circuit connected to the output of said discriminator, a tone keyer connected to the output of said discriminator and adapted to key an oscillator frequency "on" and "off" in accordance with mark and space carrier waves, means to limit the amplitude of the keyed tones, signal amplifying means for amplifying the output of said keyer, electronic amplifier means connected to the positive output of said separating circuit, signal rectifier means connected to the negative output of said separating circuit and to said amplifier means whereby when a detuning in said frequency-shifted carrier wave occurs, the resultant voltages representing respectively the mark and space signals preserve their original ratio and are of the same relative polarity.

9. In a telegraph system for receiving a carrier frequency  $F_m$  representing a telegraph mark signal, and a carrier frequency  $F_s$  representing a telegraph space signal, and including a receiver for said carriers normally tuned to produce a predetermined base potential representing the mean frequency of said two frequencies, a balanced differential discriminator circuit cooperating with a limiting tone keyer circuit and rectifier circuit, a positive signal and negative signal separating circuit cooperating with the above-mentioned circuits, amplifier means connected to a tuning indicating meter and the output of said rectifier circuit, whereby the said negative signal separated from the said positive signal by said separating circuit is shifted in a positive direction and combined with said positive signal, thereby producing a wave having a saw-tooth section including a pair of linear sloped portions symmetrically displaced on opposite sides of said mean frequency.

10. A claim in accordance with claim 9, wherein when said system is in the in-tune condition, the current drawn by said meter from said amplifier means causes the pointer of said meter to be deflected half the scale.

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