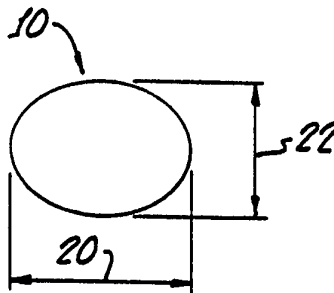




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(54) Title: HIGH REFRACTIVE INDEX HYDROGELS AND USES THEREOF



(57) Abstract

Optically transparent, high refractive index hydrogels are provided. Expansile hydrogel intraocular lenses (10) are fabricated from the hydrogels by heating them above their elastic deformation temperatures and deforming them into an elongated configuration having at least one reduced dimension (20) suitable for insertion through a small surgical incision. The lenses are allowed to cool in this configuration and retain the deformed shape prior to surgical implantation. Following implantation the lenses hydrate into an enlarged elastic form reassuming the original lens configuration of full capsule size.

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HIGH REFRACTIVE INDEX HYDROGELS AND USES THEREOF

BACKGROUND OF THE INVENTION

This application is a continuation-in-part of
Application Serial No. 07/951,775, filed September 28,
5 1992.

Field of the Invention

The present invention relates generally to hydrogels.
In one of its more particular aspects this invention
10 relates to optically transparent high refractive index
hydrogels useful for fabricating articles such as lenses,
especially intraocular lenses suitable for implantation
using small incision surgical techniques. More
particularly, the present invention involves hydrogel
15 intraocular lenses and methods for their deformation in a
dehydrated state to a size which is sufficiently reduced
for their small incision implantation following cataract
surgery. Subsequent to surgical implantation, the
deformed lenses hydrate within the ocular environment to
20 full sized lenses.

Description of Related Art

Since the early 1940's optical devices in the form of
intraocular lenses have been utilized to replace the
25 natural physiological crystalline ocular lens in humans
and other mammals. Typically, the intraocular lens is
implanted within the ocular environment immediately after
surgically removing the natural lens which has become
opaque or otherwise damaged by cataract formation or
30 injury. For decades the most prevalently utilized
materials for forming intraocular lenses were acrylates or

methacrylates and particularly polymethylmethacrylate, a rigid, glassy polymer.

More recently developed surgical techniques and improved instrumentation have made it possible to remove
5 the opaque or damaged natural lens through incision sizes as small as 2 - 3 mm. This contrasts sharply with earlier methods which involved forming incisions up to 9 or 10 mm in length in order to remove the natural lens and insert the intraocular lens. Because small incision surgery is
10 much less traumatic for patients and decreases complications and healing time, this technique has become the method of choice for a large number of ophthalmic surgeons.

Since full-size intraocular lenses have diameters in
15 the range of 8-13 mm, far exceeding the 2 - 3 mm incision size, the standard rigid polymethylmethacrylate lenses are not suitable for direct implantation through the reduced incision sizes. Thus, a number of different intraocular lens designs and materials have been developed for use in
20 connection with small incision surgical techniques. One approach utilizes the concept of preparing lenses from elastomeric materials such as silicones and thermoplastic polymers. Prior to surgically inserting the elastomeric lens, the surgeon rolls or folds the lens so that it is
25 reduced in size for passing into the eye through a smaller incision. Once placed within the eye, the lens unfolds or unrolls to its full size.

One problem associated with these elastomeric lenses is the possibility that permanent deformation or crease
30 marks may occur when the lens is folded or rolled. This is especially a concern at the center of the lens optical zone where most of the rolling or folding deformation takes place.

Another approach to providing a small incision
35 intraocular lens is suggested in U.S. Patent No. 4,731,079. This reference discloses an intraocular lens

formed of a polymer having a softening (or glass transition) temperature less than 42°C and preferably about body temperature. The lens can be heated to above its softening temperature and deformed by compression or elongation to reduce at least one dimension. Then, by cooling the lens at a temperature substantially below its softening temperature, the lens will remain in the deformed configuration until it is warmed. Ophthalmic surgeons can implant the deformed lens and once the lens warms to body temperature it returns to its original configuration.

A major problem associated with these intraocular lenses is the restricted number of polymers available for preparing the lenses. Polymethylmethacrylate has a glass transition temperature above 100°C and thus cannot be used to form these lenses. Most acrylates and methacrylates have similarly high glass transition temperatures. Though formulating the lenses with plasticizers will lower the glass transition temperature, the presence of plasticizers in intraocular lenses is generally unacceptable to most surgeons because of potential leaching problems. Alternatively, water is a suitable plasticizer. However, only small amounts of water, typically less than 10%, can be utilized in the polymers to place the glass transition in the appropriate range. Thus, typical hydrogels which have much higher amounts of water are not suitable for fabricating the deformable lenses.

An additional drawback with this suggested small incision intraocular lens is the added degree of surgical complexity required to deform the lens into its small incision configuration. The lenses are disclosed in U.S. Patent No. 4,731,079 as being packaged in a form that requires the implanting surgeon to warm, deform, and cool the lens immediately prior to its implantation. This procedure is considerably more involved than traditional lens implantation techniques.

Another suggested approach for small incision lens implantation involves implanting hydrogel intraocular lenses in their smaller dehydrated state. Once the implanted dehydrated lens is secured within the eye it reportedly hydrates and swells in the aqueous ocular environment. A significant problem associated with this approach is the large amount of swelling required to produce an effective lens diameter. In order to fully swell the lens from a diameter of about 3 mm to about 6 mm the lens must swell 8 times by volume. This translates to a lens which is 85% water. For larger full sized intraocular lenses the swell volume is much higher. Since most hydrogels are structurally very weak at these high water contents, many surgeons are reluctant to implant them. Also, these high water content hydrogels have very low refractive indices, n_p^{20} of around 1.36 and in order to achieve suitable refractive powers the hydrogel lens must be thicker in the optic portion. As a result, a dehydrated hydrogel intraocular lens that will fit through a desirably small incision will not swell to a sufficiently large hydrated size to effectively function as an intraocular lens. This problem is compounded if larger, full size intraocular lenses that have optic diameters greater than 6 mm are desired. In order to produce a hydrated lens having a sufficient optic diameter the dehydrated hydrogel lens must be larger than desirable for a small incision implantation procedure.

Alternatively, U.S. Patent No, 4,919,662 suggests rolling or folding hydrogel intraocular lenses in their elastic hydrated form, and then dehydrating the lenses at lower temperatures to fix the rolled or folded lens configuration at a size suitable for small incision implantation. Once implanted, these lenses hydrate and swell to the original lens configuration. This method has the disadvantage of requiring the handling of fully hydrated lenses during the deforming process.

Unfortunately, hydrated lenses have relatively weak tear strengths and handling the lenses causes frequent tearing damage.

U.S. Patent No. 4,813,954 discloses expansile hydrogel intraocular lenses which are formed by simultaneously deforming and dehydrating hydrogel intraocular lenses prior to implanting the lenses in their dehydrated state. Lenses subjected to this treatment swell to about 180% of their reduced size. For example, lenses deformed or compressed to a diameter of 3.2 mm will swell to only about 5.8 mm. Thus, while providing some advantages over simply implanting dehydrated lenses, the method and lenses described in U.S. Patent No. 4,813,954 do not result in full sized implanted intraocular lenses of over 8 mm.

As those skilled in the art will appreciate, each of these prior art small incision lens approaches requires an intraocular lens having generally circular, radially extending flange-type haptics as opposed to traditional filament style haptics. This is because the hydrogel materials do not have sufficient strength to stabilize the lens optics when shaped in conventional filament haptic forms. Thus, it is desirable to utilize lenses having full sized optics with diameters greater than the traditional 6 mm known in the art in order to provide lenses that stably remain in position following implantation.

Accordingly, it is an object of the present invention to provide expansile hydrogel intraocular lenses suitable for small incision implantation.

It is an additional object of the present invention to provide full sized expansile hydrogel intraocular lenses and methods for their production.

It is another object of this invention to provide high refractive index hydrogels which are particularly

adapted for use in producing lenses such as soft contact lenses and expansile hydrogel intraocular lenses.

It is further an object of the present invention to provide methods for fabricating small incision expansile hydrogel intraocular lenses which are suitable for packaging and storing in their reduced size.

SUMMARY OF THE INVENTION

The present invention accomplishes the above-mentioned objectives by providing hydrogels which are optically transparent and have high refractive indices. Such hydrogels can be used for preparing expansile hydrogel intraocular lenses as well as soft contact lenses and other articles. The expansile hydrogel intraocular lenses, in their dehydrated form, are suitably sized for small incision implantation. Unlike many prior art expansile hydrogel intraocular lenses which, when dehydrated and suitably sized for small incision implantation, hydrate within the ocular environment to undesirably small lens sizes, the intraocular lenses of the present invention hydrate and swell to full sized intraocular lenses.

Generally speaking, the methods of the present invention involve deforming dehydrated hydrogel intraocular lenses under elevated temperatures and then freezing the deformed lenses in their dehydrated configuration. The lenses retain their deformed configuration until they are exposed to conditions under which the material becomes rubbery or elastic. These reformation conditions include exposing the lens to elevated temperatures or hydrating the lens material to form the hydrogel.

More particularly, the present invention provides methods for fabricating intraocular lenses suitably sized for small incision insertion by first providing a dehydrated intraocular lens having small dehydrated

dimensions and formed of hydrogel forming polymer having an elastic deformation temperature, preferably above ambient or room temperature. The next step includes deforming the dehydrated intraocular lens at a temperature at least as high as the elastic deformation temperature to provide a deformed configuration with at least one of the dehydrated dimensions being sufficiently reduced to move the dehydrated and deformed lens through a small, typically 3 to 4 mm surgical incision. Finally, allowing the deformed and dehydrated intraocular lens to cool to a temperature sufficiently below the elastic deformation temperature freezes the deformed dehydrated intraocular lens in this small incision implantation deformed configuration.

Advantageously, once the lenses of the present invention are implanted within an aqueous physiological environment, the lenses hydrate and swell to effectively full sized lenses having diameters of over 6 to 8 mm or more. Following hydration the lenses also become elastic and acquire shape memory characteristics due to the elevated amount of water incorporated within the hydrogel material. This shape memory characteristic of the hydrated lenses makes it possible to perform the lens deformation processes using any of a variety of deformation techniques, including radial compression and tensile elongation without impacting the ability of the lenses to reform to their desired post-implantation configurations.

Exemplary hydrogel forming materials suitable for fabricating the expansile intraocular lenses of the present invention may be any polymer, copolymer, or polymer blend which is biocompatible and hydrates to a hydrogel having a hydrated equilibrium water content of at least 20%. Such materials include copolymers formed of at least one hydrophilic or water soluble monomer and one hydrophobic monomer. Particularly preferred are

cross-linked polymers and copolymers of heterocyclic aromatic compounds such as 3-vinylpyridine, 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine and 2-methyl-5-vinylpyrazine. Copolymers of two or more of these comonomers or copolymers of one or more of these comonomers with N-vinylimidazole or other non-aromatic heterocyclic compounds cross-linked with, for example, diethylene glycol diacrylate, tetraethylene glycol diacrylate, or 1,4-diacryloylpiperazine, have refractive indices, n_p^{20} , ranging from 1.560 to 1.594 in the dry state. They hydrate to a hydrated equilibrium water content ranging from about 57% to 90%.

The relative amount of the various monomers used to produce the hydrogel forming materials will depend upon the desired final water content, the desired refractive index, and the amount of material elasticity required to deform the lens above the desired elastic deformation temperature. The hydrogel materials also should have sufficient resiliency at their deformation temperatures to prevent permanent stretching or cracking during and after the deforming process, as known in the art.

Similarly, the shapes and dimensions of intraocular lenses suitable for deforming and implanting according to the present invention should be such that the lenses will withstand the physical deformation process and hydrate to effective post implantation configurations.

For example, full sized disc shaped lenses having bi-convex, plano-convex, or concavo-convex cross-sectional configurations and generally smooth, circular peripheral contact areas are suitable due to their generally symmetrical configuration. This configuration easily deforms to the desired small incision shape and hydrates to an appropriate full size lens configuration with minimal insertion and placement difficulty due to its symmetry. Similarly, disc shaped lenses having radially extending flange type haptics also may be utilized to

practice the present invention. As those skilled in the art will appreciate, the outer periphery of the lens need not be continuous, as long as it is reasonably symmetrical and of sufficient physical dimension to provide a stable lens supporting structure. For ease of manufacturing, bi-convex full sized or radial flange haptic styles are preferred.

Further objects, features and advantages of the expansile hydrogel intraocular lenses of the present invention, as well as a better understanding thereof, will be afforded to those skilled in the art from a consideration of the following detailed explanation of exemplary embodiments when taken in connection with the following drawings.

15

BRIEF DESCRIPTION OF THE DRAWINGS

Figs. 1a and b, respectively, illustrate an isometric view and an associated cross-sectional view of an exemplary small incision, full sized bi-convex, disc shape expansile hydrogel intraocular lens in its dehydrated form prior to deformation.

Figs. 2a and b, respectively, illustrate an isometric view and an associated cross-sectional view of the exemplary small incision, full sized bi-convex, disc shape expansile hydrogel intraocular lens of Fig. 1 following deformation in accordance with the teachings of the present invention.

Figs. 3a and b, respectively, illustrate an isometric view and an associated cross-sectional view of the exemplary small incision, full sized bi-convex, disc shape expansile hydrogel intraocular lens of Figs. 1 and 2 following hydration and swelling reformation into its full sized post-implantation configuration.

Fig. 4 is a graphical representation of the hydration characteristics of an exemplary, 2,3-dihydroxypropylmethacrylate (DHPMA) lens forming

polymer illustrating the percent water up-take at room temperature over time and the equilibrium water content upon hydration.

Fig. 5 is a graphical representation of the hydration characteristics of an exemplary tetraethylene glycol diacrylate (TEGDA) cross-linked N-vinylpyrrolidone (NVP) lens forming copolymer illustrating the percent water up-take at room temperature over time and the equilibrium water content upon hydration.

Fig. 6 is a graphical representation of the hydration characteristics of an exemplary cross-linked N-vinylsuccinimide (NVS) lens forming copolymer illustrating the percent water up-take at room temperature over time and the equilibrium water content upon hydration.

Fig. 7 is a graphical representation of the hydration characteristics of an exemplary NVP and N-(3-picolyl)methacrylamide (PIMA) lens forming copolymer illustrating the percent water up-take at room temperature over time and the equilibrium water content upon hydration.

Fig. 8 is a graphical representation of the hydration characteristics of an exemplary vinylpyrazine (VPZ) lens forming polymer illustrating the percent water up-take at room temperature over time and the equilibrium water content upon hydration.

DETAILED DESCRIPTION OF EXEMPLARY EMBODIMENTS

Broadly, the present invention provides methods for deforming or substantially reducing the size of shaped articles formed of polymer which is capable of subsequent swelling and expansile reformation in suitable fluids. These shaped polymeric articles can be deformed to a substantially reduced size while in the polymer's dry unswelled state known as its xerogel form. Then, once exposed to an appropriate fluid, the polymeric articles

swell in all dimensions, returning to their original shape and a substantially increased size.

Because the methods of the present invention advantageously provide reduced sized deformed articles
5 which swell to larger reformed volumes, they are particularly useful for preparing expansile intraocular lenses for implanting within the eye using small incision surgical techniques. The advantageously high swelling ratios allow the lenses to be configured for small
10 incision insertion into the eye where the lenses hydrate and swell to full sized hydrogel intraocular lenses. Those skilled in the art will appreciate, however, that the methods of the present invention are suitable for other uses where polymeric articles capable of swelling to
15 larger dimensions have utility.

The present invention is based upon the discovery that the hydrated elastic properties and shape memory properties of polymers which swell in the presence of fluids can be utilized to prepare deformable polymeric
20 articles having specific, reduced dimensions yet which provide large swell volumes and shape reformation characteristics. That is, the present invention involves exposing a hydrogel article in its dehydrated state to thermal conditions under which the dehydrated article is
25 elastic, and then deforming and freezing the article in its deformed configuration. The result is a dehydrated and deformed polymeric article, which, following hydration, displays substantially increased swell volumes and dimensions.

30 More particularly, an exemplary embodiment of the present invention provides methods for fabricating intraocular lenses suitably sized for small incision insertion by first providing a dehydrated intraocular lens having at least one desirably small dehydrated dimension
35 and formed of hydrogel forming polymer having an elastic deformation temperature. Preferably, the elastic

deformation temperature is sufficiently high to be above ambient or room temperature. The next step includes deforming the dehydrated intraocular lens at a temperature at least as high as the elastic deformation temperature to provide a deformed configuration with at least one of the dehydrated dimensions being sufficiently reduced to move the dehydrated and deformed lens through a 3 to 4 mm surgical incision. Finally, allowing the dehydrated and deformed intraocular lens to cool to a temperature sufficiently below the elastic deformation temperature freezes the deformed dehydrated intraocular lens in its deformed configuration. The resulting expansile small incision intraocular lens is capable of swelling to a full sized hydrogel intraocular lens upon exposure to an aqueous environment such as an ocular physiological environment; yet, in its deformed state the intraocular lens has beneficially small dimensions suitable for contemporary small incision implantation techniques.

In accordance with the processes of the present invention, deforming the dehydrated intraocular lenses can be accomplished by any method which reduces the profile of the lens in at least one dimension. For example, a dehydrated lens can be compressed by applying pressure from its outer circumference inward. Vise clamps fitted with circular shaped fixtures can be utilized for this purpose. This method results in a reduced cross-sectional lens diameter and increased lens thickness, preferably on the order to 1 to 3 mm.

An alternative deforming method includes elongating or stretching the lens using tensile forces. Tweezers, forceps or other clamping tools can be utilized for this purpose wherein the lens is grasped at diametrically opposed positions about its periphery and stretched into an elongated, lozenge shape having an appropriately reduced cross-sectional diameter. Alternative deforming methods include rolling or folding the lenses to reduce

their cross-sectional profiles. Exemplary methods for rolling or folding include those used to roll and fold elastomeric lenses such as those formed of silicones, as known in the art.

5 In order to deform the dehydrated lenses of the present invention without cracking or otherwise damaging the lens, the deforming step is performed at a temperature at which the dehydrated lens is sufficiently elastic for non-destructive deformation. More particularly, articles
10 prepared from xerogel polymers can be deformed and reduced in size to a deformed configuration without damage when the deforming step is performed at temperatures which exceed the elastic deformation temperature of the polymer used. For many polymers, the elastic deformation
15 temperature is in the same temperature region as the polymer's glass transition temperature, the temperature at which the polymer transforms from a glassy state to an elastic state. For purposes of the present invention, however, the deformation temperature and glass transition
20 temperature can be separate thermodynamic temperatures. Within the temperature region between the deformation temperature and the polymer's degradation temperature, the polymer can be deformed through the controlled application of external force. However, if the external force is
25 removed, the polymer will elastically return to its original configuration unless treated in accordance with the teachings of the present invention.

Those skilled in the art will appreciate that glass transition temperatures and polymer deformation
30 temperatures vary from polymer to polymer. Typically, polymers increase in elasticity as the temperature increases above their glass transition temperatures. Accordingly, as discussed below, suitable elastic deformation temperatures should be separately determined
35 for each type of hydrogel forming polymer used in the practice of the present invention. Preferably, the

elastic deformation temperature is above ambient temperatures and, more preferably, above about 55°C. Those skilled in the art will appreciate that elastic deformation temperatures which are above the range of
5 about 55°C allow deformed articles which are exposed to elevated temperatures during shipping and storage to maintain their deformed configuration under ambient conditions. This is because the deformed article is subjected to temperatures below those temperatures which
10 cause the deformed article to become elastic.

In accordance with the present invention, allowing the deformed dehydrated article, for example, the intraocular lens, to cool to a suitable temperature below its elastic deforming temperature prior to removing the
15 compression or elongation forces effectively freezes the deformed article in its deformed configuration. At this lower freezing temperature the dehydrated article does not require application of external forces to remain in the deformed configuration. In fact, once cooled below the
20 elastic deformation or freezing temperature, the deformed articles remain deformed until exposed to conditions under which the polymer is again elastic, at which point the articles return to their original shapes.

Typically, a suitable freezing temperature is a
25 temperature below the glass transition temperature of the hydrogel forming polymer in its xerogel form. At the lower temperature the polymer is in its plastic form as opposed to its higher temperature elastic form. In this plastic form the article has little resilience. This
30 contrasts with the elastic form where the deformed article returns to its original shape once the deformation forces are removed.

For purposes of practicing the present invention, and as mentioned above, preferred temperatures for freezing
35 the deformed articles in their deformed configuration are in the range of ambient temperatures. Thus, allowing the

heated deformed article to cool below about 30°C provides a deformed article which is frozen in its deformed configuration. This allows the deformed articles of the present invention to retain their deformed configuration
5 during storage and shipping without refrigeration or special considerations.

The articles and the hydrogel forming polymers utilized to form the articles should meet certain physical characteristics so that the articles are not damaged
10 during the deforming processes of the present invention. The polymer xerogels or dehydrated forms should have sufficient elasticity at their deforming temperatures to allow the articles to be deformed to sufficiently reduced sizes without breaking or cracking. Preferably, the
15 material from which the article is formed is not elastic at ambient temperatures, thus allowing the deformed articles to remain in a deformed configuration during storage and shipping. Additionally, where the hydrogels are used to fabricate intraocular lenses, suitable
20 polymeric materials for practicing the present invention will hydrate and swell to form hydrogels having sufficient water to exhibit elastic characteristics and shape memory properties at body temperatures, thereby enabling the lenses to reform to sizes, shapes and configurations
25 effective for their intended functions as intraocular lens implants.

Any of the polymers currently utilized to form hydrogel intraocular lenses are suitable hydrogel forming polymers for purposes of practicing the present invention.
30 Thus, commercially available hydrogel intraocular lenses can be deformed according to the processes of the present invention and then implanted utilizing small incision methodologies. Additionally, many other hydrogel forming polymers and copolymers having properties appropriate for
35 fabricating hydrogel lenses are suitable hydrogel forming polymers for practicing the present invention.

Generally, hydrogel forming polymers are cross-linked polymers of water soluble or hydrophilic monomers or copolymers of water soluble and water insoluble monomers. Because of their importance in the field of biomaterial and agriculture, hydrogels and processes for their formation are well documented in the literature. Typical hydrogel materials include homopolymers and copolymers of acrylamides, methacrylamide, acrylate and methacrylate esters having at least one hydroxyl group on the side chain, such as 2-hydroxyethyl methacrylate, hydroxyethoxyethyl methacrylate, hydroxydiethoxy methacrylate, 2,3 dihydroxypropyl methacrylate, and glycerol methacrylate. Other suitable hydrogel forming polymers include polymers and copolymers of monomers such as methoxyethylethoxyethyl methacrylate, methoxydiethoxyethyl methacrylate, methoxyethyl methacrylate, methacrylic acid, divinyl sulfone, vinyl methyl sulfone, vinyl alcohol, and vinyl acetate. Heterocyclic compounds such as N-vinyl-2-pyrrolidone and related N-alkenyl-2-pyrrolidones, N-vinyl carbazole, N-vinyl succinimide, N-(3-picolyl) methacrylamide, and N-vinylimidazole are also suitable monomers.

A preferred class of hydrogel forming polymers includes cross-linked polymers and copolymers of heterocyclic aromatic compounds such as 3-vinylpyridine, 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine and 2-methyl-5-vinylpyrazine. Copolymers of two or more of these comonomers or copolymers of one or more of these comonomers with N-vinylimidazole or other non-aromatic heterocyclic compounds cross-linked with, for example, diethylene glycol diacrylate, tetraethylene glycol diacrylate, or 1,4-diacryloylpiperazine, have refractive indices, n_D^{20} , ranging from 1.560 to 1.594 in the dry state. They hydrate to a hydrated equilibrium water content ranging from about 57% to 90%. In the nitrogen containing heterocyclic aromatic compounds the nitrogen atoms impart

hydrophilicity via hydrogen bonding with water molecules, while the delocalization of the π electrons of the aromatic rings contributes to the high refractive indices of the copolymers.

5 As pointed out above, high water content hydrogels generally have very low refractive indices, n_D^{20} . It is, therefore, unexpected to find that a cross-linked polymer of vinylpyrazine, for example, with a very high equilibrium water content of 89.2% has a refractive index
10 of 1.594. By using the high refractive index hydrogels of this invention it is possible to provide higher refractive power in a lens or other article with a much thinner optic portion than by using the low refractive index, high water content hydrogels previously available. It will be
15 appreciated by those skilled in the art that the hydrogels of the present invention can be tailored to provide a wide range of refractive indices, n_D^{20} , upwards of about 1.560 and hydrated equilibrium water contents ranging from about 20% to 90% in order to accommodate a variety of utilities.

The hydrogels of the present invention may also

include from about 0.1 wt% to about 10 wt% ultraviolet (UV) radiation absorbing compounds. Preferably, the UV absorbing compound is copolymerizable with the monomer forming the hydrogel polymer, thus becoming part of the
25 final polymer or copolymer. This feature assures that the hydrated hydrogel is optically clear, and assures that the UV absorbing compound does not leach or migrate from the article fabricated from the hydrogel, for example, from an implanted lens.

30 As noted above, hydrogel materials may not be suitable for forming intraocular lens haptics in traditional radial filament configurations due to their flexibility. Accordingly, while it is contemplated as being within the scope of the present invention to utilize
35 lenses having conventionally shaped haptics, it is preferred that the haptics be configured to account for

the physical and structural properties of the hydrogel materials. Thus, as illustrated in Fig. 1, an exemplary lens configuration suitable for practicing the present invention is a bi-convex disc shaped lens, generally indicated by reference 10. Exemplary lens 10 is shown in its dehydrated state having dimensional characteristics sufficiently reduced from that of its intended, post-implantation hydrated configuration. Thus, the outer circumferential periphery 14 of the lens 10 is intended to position lens 10 within the capsular bag of the eye following implantation and hydration. Those skilled in the art will appreciate that periphery 14 can be provided with radially extending flanges or blade type haptics (not shown) if desired. In such a configuration, lens 10 would function as the optic portion of an intraocular lens having a larger overall diameter. Thus, full size hydrogel intraocular lens implants having optic diameters of up to 10 mm and overall diameters of up to 13 mm or more can be produced utilizing the techniques of the present invention so that these lenses can be effectively reduced in size and implanted utilizing small incision surgical techniques.

More particularly, Figs. 1-3 illustrate exemplary lens configurations suitable for practicing the fabrication and deformation methods of the present invention. Figs. 1a and b illustrate the configuration of exemplary lens 10 in its dehydrated, reduced dimension form. Figs. 2a and b illustrate an exemplary deformed configuration of lens 10 having at least one dimension sufficiently small to enable the lens to be inserted through a typical small incision lens implantation procedure. Figs. 3a and b illustrate the post-implantation hydrated dimensions and configurations of lens 10.

In Fig. 1a lens 10 is shown as a circular, bi-convex lens in its dehydrated configuration having an exemplary

diameter 12 ranging from approximately 4 to 7 mm. As shown in Fig. 1b an exemplary cross-sectional thickness 16 for lens 10 ranges from approximately 2 to 4 mm.

In accordance with the teachings of the present invention, lens 10 may be deformed in its dehydrated state into an elongated configuration as illustrated in Fig. 2a. Thus, by warming dehydrated lens 10 above its elastic deformation temperature, grasping opposite edges of circumferential periphery 14 with suitable tools and pulling, lens 10 may be pulled into the lozenge shape of Fig. 2a having a long dimension 18 on the order of 8 to 10 mm and, as illustrated in Fig. 2b, a cross-sectional width 20 of approximately 2 to 4 mm and a cross-sectional height 22 of approximately 2 to 3 mm. As noted above, the lozenge shape illustrated in Fig. 2a can also be produced by applying compressive forces across diameter 12 or through rolling and folding. Regardless of the deformation technique, before the deforming forces are removed lens 10 is allowed cool below its elastic deformation temperature to its freezing temperature. This can be accomplished by placing lens 10 in an appropriately configured fixture such as a tubular holder and allowing the heated lens to cool prior to removal from the holder or clamps.

As is readily apparent from Figs. 2a and b, in its deformed configuration lens 10 can be inserted through an ocular incision on the order of 3 to 4 mm in length by presenting the reduced cross-sectional dimensions of the elongated, deformed lens and sliding the lens through the incision. Coating lens 10 with a viscoelastic material may facilitate this movement through the ocular incision. Advantageously, the deformed lens 10 illustrated in Fig. 2a and b is capable of minimizing the possibility of decentration once it is inserted in the ocular capsular bag. The ocular capsular bag has a general oval shape and the average size of the natural human lens is about 9.6 mm

x 4.3 mm. The elongated shape of deformed lens 10 causes the lens to orient itself within the bag in alignment with the shape of the capsular bag. Additionally, the length of the elongated dimension acts as an anchor to secure the
5 expansile deformed lens within the ocular capsular bag during the hydration process.

Following implantation lens 10 is allowed to hydrate and swell to an enlarged, full sized configuration as illustrated in Figs. 3a and b. As shown in Fig. 3a,
10 hydrated lens 10 has returned to its circular configuration and has enlarged to an expanded diameter 24 on the order of 8 to 10 mm. Similarly, as shown in Fig. 3b, the expanded cross-sectional thickness 26 of hydrated lens 10 is significantly larger than that of dehydrated
15 cross-sectional thickness 16 and ranges on the order of 4 to 5 mm in this exemplary embodiment.

Thus, Figs. 1-3 clearly demonstrate the dramatic reduction in at least one dimension of an expansile hydrogel lens that may be produced through the method of
20 the present invention to provide a lens implant that can be inserted through a small incision surgical technique, yet will expand to a full size hydrated implant that reforms to its original configuration. By artfully combining the elasticity of the dehydrated lenses at
25 elevated temperatures with their elastic memory behavior following hydration in combination with their swelling characteristics, the present invention provides full sized expansile hydrogel lenses that can be inserted through small surgical incisions.

30 It is also an aspect of the present invention to provide associated processes for surgically implanting such small incision intraocular lenses. An exemplary implantation process includes the steps of providing an ocular incision of less than about 4 mm in length and
35 inserting such a deformed expansile intraocular lens through the ocular incision. Following insertion the

deformed lens is allowed to hydrate and swell to an enlarged, full sized hydrogel intraocular lens having the configuration of the original reduced size lens only with enlarged dimensional characteristics.

5 Unlike prior art small incision procedures for implanting expansile intraocular lenses which are restricted to less than full sized hydrogel lenses, the processes of the present invention provide for the implantation of full sized hydrogel lenses. This is made
10 possible because the processes of the present invention utilize both the hydration swelling and elastic memory characteristics of hydrogels. Moreover, the present invention contrasts with prior art methods for preparing deformed polymeric intraocular lenses for small incision
15 implantation in that prior art processes depend upon only the temperature related elastic deformation properties of polymers. As mentioned above, the prior art deformation processes occur at physiological temperatures and elastic recovery occurs at physiological temperatures.

20 Thus, materials suitable for deforming according to prior art methods must have deformation temperatures which are close to physiological temperatures and freezing temperatures which are just below physiological temperatures. In any case, the maximum material
25 deformation temperature is only slightly above 40°C for these prior art processes. Generally, polymers having higher plasticizer content possess lower elastic deformation temperatures. Further, water incorporated in the polymer matrix of hydrogels acts as a plasticizer,
30 effectively maintaining a low elastic deformation temperature compared with the xerogel state of the polymeric material. Typical hydrogels used to fabricate ophthalmic lenses have elastic deformation temperatures which are substantially below physiological temperatures.
35 Accordingly, these hydrogels are not suitable for processing according to prior art deformation procedures

since they do not remain deformed without external forces at room temperatures.

As mentioned above, in addition to being elastic at temperatures above the elastic deformation temperature, suitable hydrogel polymers for practicing the present invention are elastic in their hydrated form. Thus, by simply hydrating the deformed hydrogel intraocular lenses of the present invention, even at temperatures less than the elastic deformation temperature, the lenses return to an elastic state and recover their original configuration. This is in addition to the substantial size increase attributed to the hydrating and swelling action.

The following examples are offered as being illustrative of the principles of the present invention and not by way of limitation.

EXAMPLE 1

A total of ten different copolymers and homopolymers were prepared and evaluated for use as exemplary hydrogel forming materials of the present invention. Table I illustrates the proportions of each component of the polymerization mixture and presents comments relating to the polymer. Each polymerization procedure was carried out by first mixing the appropriate amounts of the monomer, comonomer, cross-linker and polymerization initiator as indicated in the first column of Table I. Then each mixture was transferred to an ampoule which was pre-treated with a silicone grease mold releasing agent. Each ampoule and mixture was then attached to a vacuum system and cooled with liquid nitrogen. After the mixture was frozen by the liquid nitrogen, the mixture was evacuated by turning on the vacuum system. Once a constant pressure was achieved, the vacuum system was turned off and the mixture was allowed to thaw by warming the ampoule in a water bath. This freeze-thaw cycle was repeated three times in order to provide sufficient

mixture degassing. Finally, each mixture and ampoule were sealed under vacuum or an inert gas such as nitrogen or argon and polymerized. The polymerization temperatures and time periods varied with the particular monomers and comonomers in the polymerization mixture as indicated in the second column of Table I.

The abbreviations utilized in Table I are identified in Table II, immediately following.

10

TABLE I

	<u>MONOMERS AND COMPONENTS</u>	<u>POLYMERIZATION CONDITIONS</u>	<u>PROPERTIES</u>	<u>COMMENTS</u>
15	(1) 7 ml DHPMA 35 μ l EGDMA 7 mg AIBN	60°C/60h 110°C/24h	Clear colorless solid; clear in swollen state	Slow hydration
20	(2) 7.96 ml NVP 40 μ l TEGDA 8 mg AIBN	60°C/63h 120°C/30h	Clear colorless solid; clear in swollen state	Rapid hydration
25	(3) 7.92 ml NVP 80 μ l TEGDA 8 mg AIBN	60°C/63h 120°C/30h	Clear colorless solid; clear in swollen state	Rapid hydration
30	(4) 9.8 ml NVP 0.2 ml TEGDA 8 ml AIBN	60°C/63h 120°C/30h	Clear colorless solid; clear in swollen state	Rapid hydration IOLs made

5	<p>(5) 3.96 g NVS 40 mg TEGDA 4 mg AIBN</p>	<p>50°C/48h 80°C/48h 100°C/6h</p>	<p>Clear colorless solid; clear in swollen state</p>	<p>Low water content; intermedia te hydration rate</p>
10	<p>(6) 5.54 g NVP 1.39 g PIMA 70 mg TEGDA 7 mg AIBN</p>	<p>50°C/60h 80°C/24h 120°C/6h</p>	<p>Clear colorless solid; clear in swollen state;water content 89%</p>	<p>Intermedia te hydration rate</p>
15	<p>(7) 7.5 g NVP 7.5 g NVI 150 mg TEGDA 15 mg AIBN</p>	<p>50°C/40h 80°C/96h</p>	<p>Clear slightly yellow solid; clear in swollen state; water content 94%</p>	<p>Rapid hydration</p>
20	<p>(8) 2.4 g NVI 0.6 g 4VP 60 µl TEGDA 3 mg AIBN</p>	<p>60°C/48h 120°C/12h</p>	<p>Clear slightly yellow solid; clear in swollen state; water content 61%</p>	<p>Rapid hydration</p>
25	<p>(9) 7.5 g NVI 2.5 g 4VP 57 µl TEGDA 10 mg AIBN</p>	<p>60°C/48h 120°C/24h</p>	<p>Clear slightly yellow solid; clear in swollen state; water content 63%</p>	<p>Rapid hydration</p>
30				

5	(10) 7.5 g NVI 2.5 g 4VP 100 μ l TEGDA 10 mg AIBN	60°C/48h 120°C/24h	Clear slightly yellow solid; clear in swollen state; water content 61%	Rapid hydration
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TABLE II

COMPONENTS	ABBREVIATION
2,3-Dihydroxypropyl methacrylate	DHPMA
15 Ethylene glycol dimethacrylate	EGDMA
2,2'-Azobisisobutyronitrile	AIBN
N-Vinylpyrrolidone	NVP
Tetraethylene glycol diacrylate	TEGDA
N-Vinylimidazole	NVI
20 N-(3-Picolyl) methacrylamide	PIMA
4-Vinylpyridine	4VP
N-Vinylsuccinimide	NVS

25 The hydration characteristics and equilibrium water contents were determined for five of the polymers and copolymers identified in Table I. Water uptake profiles were determined by placing equal size blanks of each

polymer or copolymer in deionized water and periodically weighing each sample to determine the weight increase caused by water uptake. These results were plotted to determine a water uptake profile and equilibrium hydration water content as illustrated in Figs. 4 through 7. Fig. 4 illustrates the water uptake profile of an exemplary DHPMA polymer identified as polymer 1 in Table 1. Water content was measured over a period of 14 days of hydration and stabilized at an equilibrium water content of approximately 45% to 48% following 4 days of hydration. Fig. 5 illustrates a much faster water uptake profile of a TEGDA cross-linked NVP polymer identified as polymer 4 of Table I occurring over a 7 hour period. An equilibrium water content of approximately 85% was achieved in 6 hours. A 40 hour water uptake profile of cross-linked NVS polymer (polymer 5 of Table I) is illustrated in Fig. 6 and a 24 hour water uptake profile of a cross-linked polymer of NVP and PIMA (polymer 6 of Table I) is illustrated in Fig. 7.

The following example illustrates the deformation method of the present invention utilizing a cross-linked N-Vinylpyrrolidone polymer.

EXAMPLE 2

In order to demonstrate the feasibility of the deformation method of the present invention a full sized expansile intraocular lens was prepared from polymer 4 of Table I by polymerizing a mixture of N-vinyl pyrrolidone and 2 wt% tetraethyleneglycol diacrylate with an AIBN initiator. The same general procedure described in Example 1 was utilized to prepare the mixture filled ampoule for polymerization and the polymerization process included a 72 hour cycle at 60°C and a 48 hour cycle at 120°C. After the polymerized material was cooled the ampoule was broken open and the resulting polymer rod was cut into blanks. Each blank was then machined to an

expansile intraocular lens in its dehydrated state. These blanks generally corresponded to the exemplary lens configuration 10 illustrated in Figs. 1a and b. The machined dehydrated lenses had diameters 12 ranging from approximately 4.5 to 7.1 mm and cross-sectional thicknesses 16 ranging from approximately 2.3 to 3.6 mm.

Exemplary lenses were deformed by heating a water bath to 60°C and placing a beaker of heptane in the water bath. The lenses were immersed in the warm heptane for approximately 10 seconds and simultaneously folded with a pair of tweezers. The folded lenses were then removed from the heptane and inserted into 1/16 inch I.D. silicone tubes. The tube and folded lenses were then immersed in the warm heptane for 10 - 20 seconds. The tubes and lenses were removed from the heptane and immediately rolled and squeezed between two fingers, compressing the lenses into tightly folded and elongated shapes. The elongated lenses and tubes were allowed to cool to room temperature and then the lenses were removed from the tubes. At room temperature the lenses remained in their elongated state and had a configuration similar to that illustrated in Figs. 2a and b. The long dimension 18 ranged from approximately 8 to 13 mm, the cross-sectional width 20 ranged from approximately 2 to 4 mm, and the cross-sectional height 22 ranged from approximately 1.8 to 3.0 mm.

Each lens was immersed in physiologically buffered aqueous solutions for 8-48 hours and allowed to hydrate to an equilibrium water content of about 85% by weight. The lenses were observed to expand and reform to the original configuration as illustrated in Figs. 3a and b. The enlarged reconfigured hydrated lenses had expanded diameters 24 ranging from approximately 8.5 to 9.5 mm and expanded cross-sectional thicknesses 26 of approximately 4.5 mm.

The following example illustrates the use of a cross-linked copolymer of N-vinylimidazole and 4-vinylpyridine.

5 EXAMPLE 3

Intra-ocular lenses were machined from lens blank formed of polymer 8 of Table I by polymerizing a mixture of N-vinyl imidazole, 4-vinyl pyridine (25 wt%), and tetraethyleneglycol diacrylate with an AIBN initiator.
10 The same general procedure described in Example 1 was utilized to prepare the mixture filled ampoule for polymerization and the polymerization process also included a 48 hour cycle at 60°C and a 24 hour cycle at 120°C.

15 Exemplary lenses were similar in dimensions to those described in Example 2. A typical optical resolution of the exemplary lenses in the dehydrated state was 80% as measured on a Meclab optical bench. The exemplary lenses were then deformed according to the procedures provided in
20 Example 2. After hydration in physiologically buffered aqueous solutions for about 24 hours, the deformed lenses recovered their original configurations. As measured on a Meclab optical bench, a typical optical resolution of 70% was found for the hydrated lenses. This compares
25 favorably with the 60% optical resolution minimally acceptable within the ophthalmic industry.

The following example illustrates a number of the high refractive index hydrogels of the present invention.

30 EXAMPLE 4

The general procedure described in Example 1 was followed using various combinations of heterocyclic monomers. The results, including the refractive index, n_D^{20} , of the cross-linked polymers and copolymers and the
35 equilibrium water content of the hydrated polymers, are shown in Table III.

Those abbreviations utilized in Table III not previously identified in Table II are defined in Table IV, immediately following.

5

TABLE III

	<u>MONOMERS AND COMPONENTS</u>	<u>POLYMERIZATION CONDITIONS</u>	<u>PROPERTIES</u>
10	(11) VPZ 1 g TEGDA 13 μ l AIBN 10 mg	60°C/24h 120°C/12h	Clear light brown solid; clear slightly yellow when swollen; water content 89.2%; n_D^{20} (dry)=1.594
15	(12) 4VP 2 g TEGDA 18 μ l AIBN 2 mg	60°C/48h 120°C/24h	Clear slightly yellow solid; clear colorless when swollen; water content 26.7%; n_D^{20} (dry)=1.591
20	(13) NVI 7.5 g 4VP 2.5 g TEGDA 100 μ l AIBN 10 mg DCP 10 mg	60°C/48h 120°C/48h	Clear light yellow solid; clear slightly yellow when swollen; water content 65.6%; n_D^{20} (dry)=1.563
25	(14) NVI 7.5 g 3VP 2.5 g DEGDA 71 μ l AIBN 10 mg DCP 10 mg	60°C/48h 120°C/48h	Clear slightly yellow solid; clear very slightly yellow when swollen; water content 69.7%; n_D^{20} (dry)=1.560
30	(15) MPZ 3 g DEGDA 49 μ l AIBN 9 mg DCP 6 mg	60°C/48h 120°C/48h	Clear brown solid; clear light brown when swollen; water content 77.1%; n_D^{20} (dry)=1.585

5	(16) NVI 2.2 g 3VP 1.5 g VPM 1 g DAP 92 mg AIBN 5 mg	60°C/36h 120°C/12h	Clear yellow solid; clear light yellow when swollen; water content 57.0%; $n_D^{20}(\text{dry})=1.587$
10	(17) NVI 1.4 g VPM 0.93 g 4VP 0.61 g DAP 58 mg AIBN 3 mg	60°C/36h 120°C/12h	Clear deep yellow solid; clear yellow when swollen; water content 63.0%; $n_D^{20}(\text{dry})=1.589$
15	(18) NVI 1.45 g VPM 1 g 4VP 0.66 g DEGDA 61 μl AIBN 3 mg DCP 1 mg	60°C/36h 120°C/12h	Clear yellow solid; clear very slightly yellow when swollen; water content 66.5%; $n_D^{20}(\text{dry})=1.586$
20	(19) NVI 1.46 g VPM 1 g 4VP 0.66 g DAP 30.5 mg AIBN 3 mg DCP 1 mg	60°C/36h 120°C/12h	Clear deep yellow solid; clear yellow when swollen; water content 67.9%; $n_D^{20}(\text{dry})=1.587$
25	(20) NVI 1.46 g VPM 1 g 4VP 0.66 g DEGDA 30.5 μl AIBN 3 mg DCP 1 mg	60°C/36h 120°C/12h	Clear yellow solid; clear virtually colorless when swollen; water content 69.6%; $n_D^{20}(\text{dry})=1.588$
30	(21) VPM 944 μl NVP 439 μl DEGDA 47.1 μl AIBN 0.8 mg DCP 0.8 mg	60°C/36h 135°C/4h	Clear light yellow solid; clear virtually colorless when swollen; Water content 72.0%; $n_D^{20}(\text{dry})=1.570$
35	(22) VPM 802 μl NVP 780 μl 4VP 291 μl DEGDA 52.3 μl AIBN 1 mg DCP 1 mg	60°C/36h 135°C/4h	Clear light yellow solid; clear virtually colorless when swollen; Water content 71.0%; $n_D^{20}(\text{dry})=1.563$
40			
45			

5	(23) NVI 1236 μ l VPM 607 μ l DEGDA 68.9 μ l AIBN 1 mg DCP 1 mg	60°C/36h 135°C/4h	Clear light yellow solid; clear virtually colorless when swollen; Water content 66.0%; n_D^{20} (dry)=1.570
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10

TABLE IV

10	COMPONENTS	ABBREVIATION
	Vinylpyrazine	VPZ
	Dicumyl peroxide	DCP
	Diethylene glycol diacrylate	DEGDA
15	3-Vinylpyridine	3VP
	2-Methyl-5-vinylpyrazine	MPZ
	4-Vinylpyrimidine	VPM
	1,4-Diacryloyl piperazine	DAP

20

Having thus described exemplary embodiments of the present invention, it should be noted by those skilled in the art that the disclosures herein are exemplary only and that alternatives, adaptations and modifications may be made within the scope of the present invention.

What is claimed is:

1. A hydrogel comprising a cross-linked polymer prepared from one or more monomers selected from the group consisting of 3-vinylpyridine, 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine, and
5 2-methyl-5-vinylpyrazine.

2. The hydrogel of claim 1 wherein one or more monomers selected from the group consisting of diethylene glycol diacrylate, tetraethylene glycol diacrylate, and 1,4-diacryloylpiperazine is employed as a cross-linking
5 agent.

3. A hydrogel comprising a cross-linked polymer prepared from a mixture of monomers comprising N-vinylimidazole and at least one comonomer selected from the group consisting of 3-vinylpyridine, 4-vinylpyridine,
5 4-vinylpyrimidine, vinylpyrazine, and 2-methyl-5-vinylpyrazine.

4. A hydrogel comprising a cross-linked polymer prepared from a mixture of monomers comprising N-vinylimidazole, 4-vinylpyrimidine, and a vinyl pyridine.

5. A hydrogel comprising a cross-linked polymer prepared from a mixture of monomers comprising

N-vinylpyrrolidone and at least one comonomer selected from the group consisting of 3-vinylpyridine, 5 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine, and 2-methyl-5-vinylpyrazine.

6. A hydrogel comprising a cross-linked polymer prepared from a mixture of monomers comprising N-vinylpyrrolidone, 4-vinylpyrimidine, and a vinyl pyridine.

7. A hydrogel comprising a cross-linked polymer prepared from a mixture of monomers comprising N-vinylpyrrolidone and 4-vinylpyrimidine.

8. The hydrogel of claim 1 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

9. The hydrogel of claim 2 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

10. The hydrogel of claim 3 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

11. The hydrogel of claim 4 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

12. The hydrogel of claim 5 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

13. The hydrogel of claim 6 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

14. The hydrogel of claim 7 wherein said cross-linked polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

15. The hydrogel of claim 8 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

16. The hydrogel of claim 9 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

17. The hydrogel of claim 10 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

18. The hydrogel of claim 11 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

19. The hydrogel of claim 12 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

20. The hydrogel of claim 13 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

21. The hydrogel of claim 14 wherein said cross-linked polymer has a hydrated equilibrium water content of about 57% to 90%.

22. A process for fabricating expansile hydrogel intraocular lenses having reduced size for small incision insertion, said process comprising the steps of:

providing a dehydrated hydrogel intraocular lens
5 having dehydrated dimensions, said dehydrated hydrogel
intraocular lens being formed of a cross-linked polymer
prepared from one or more monomers selected from the group
consisting of 3-vinylpyridine, 4-vinylpyridine,
4-vinylpyrimidine, vinylpyrazine, and
10 2-methyl-5-vinylpyrazine, and having an elastic
deformation temperature;

deforming said dehydrated intraocular lens at a temperature at least as high as said elastic deformation temperature to provide a deformed configuration with at least one of said dehydrated dimensions being sufficiently reduced to move said dehydrated and deformed lens through a 4 mm surgical incision; and

allowing said deformed dehydrated intraocular lens to cool to a temperature sufficiently below said elastic deformation temperature to freeze said deformed dehydrated intraocular lens in its deformed configuration.

23. The process of claim 22 wherein one or more monomers selected from the group consisting of diethylene glycol diacrylate, tetraethylene glycol diacrylate, and 1,4-diacryloylpiperazine is employed as a cross-linking agent.

24. The process of claim 22 wherein said polymer is prepared from a mixture of monomers comprising N-vinylimidazole and at least one comonomer selected from the group consisting of 3-vinylpyridine, 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine, and 2-methyl-5-vinylpyrazine.

25. The process of claim 22 wherein said polymer is prepared from a mixture of monomers comprising N-vinylimidazole, 4-vinylpyrimidine, and a vinyl pyridine.

26. The process of claim 22 wherein said polymer is prepared from a mixture of monomers comprising N-vinylpyrrolidone and at least one comonomer selected from the group consisting of 3-vinylpyridine, 5 4-vinylpyridine, 4-vinylpyrimidine, vinylpyrazine, and 2-methyl-5-vinylpyrazine.

27. The process of claim 22 wherein said polymer is prepared from a mixture of monomers comprising N-vinylpyrrolidone, 4-vinylpyrimidine, and a vinyl pyridine.

28. The process of claim 22 wherein said polymer is prepared from a mixture of monomers comprising N-vinylpyrrolidone and 4-vinylpyrimidine.

29. The process of claim 22 wherein said polymer has a refractive index, n_p^{20} , ranging from 1.560 to 1.594 in the dry state.

30. The process of claim 23 wherein said polymer has a refractive index, n_p^{20} , ranging from 1.560 to 1.594 in the dry state.

31. The process of claim 24 wherein said polymer has a refractive index, n_p^{20} , ranging from 1.560 to 1.594 in the dry state.

32. The process of claim 25 wherein said polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

33. The process of claim 26 wherein said polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

34. The process of claim 27 wherein said polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

35. The process of claim 28 wherein said polymer has a refractive index, n_D^{20} , ranging from 1.560 to 1.594 in the dry state.

36. The process of claim 29 wherein said polymer has an equilibrium water content of about 57% to 90%.

37. The process of claim 30 wherein said polymer has an equilibrium water content of about 57% to 90%.

38. The process of claim 31 wherein said polymer has an equilibrium water content of 57% to 90%.

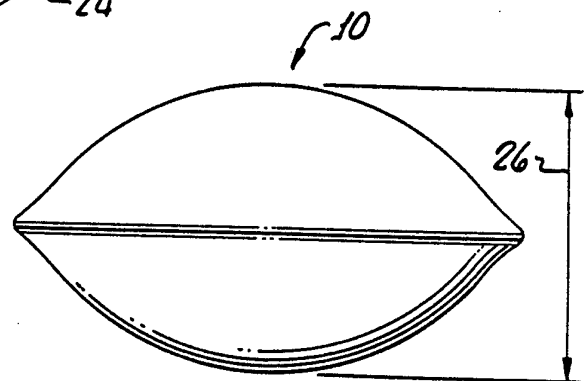
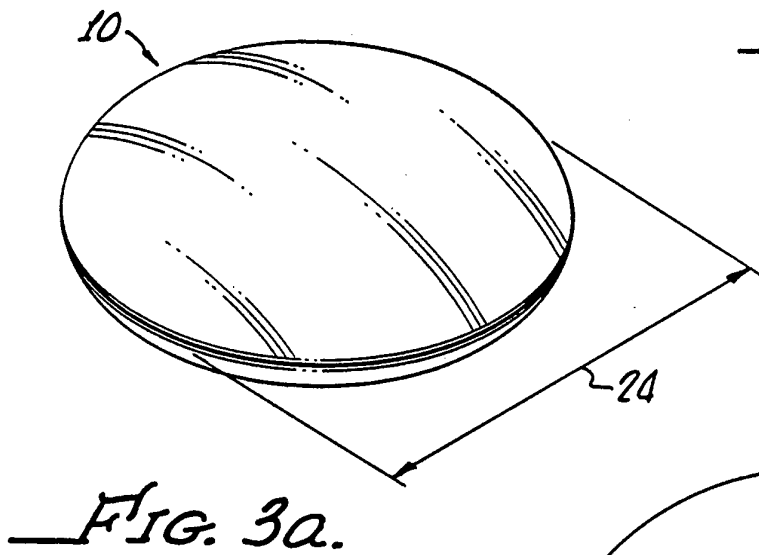
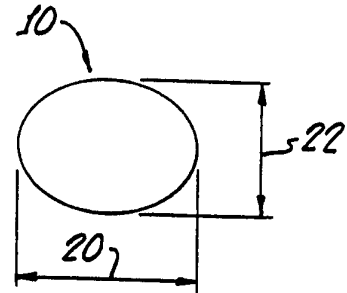
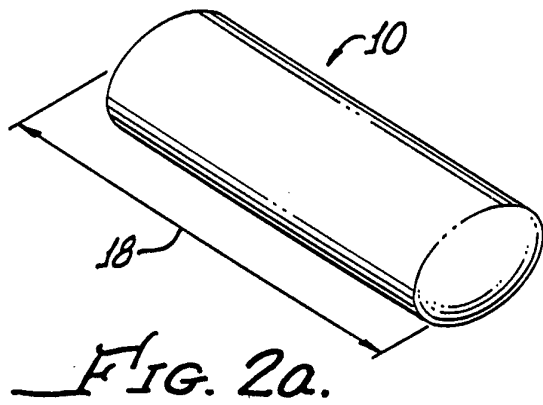
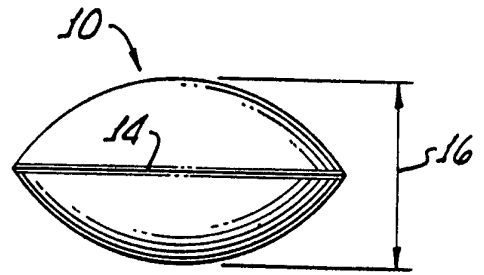
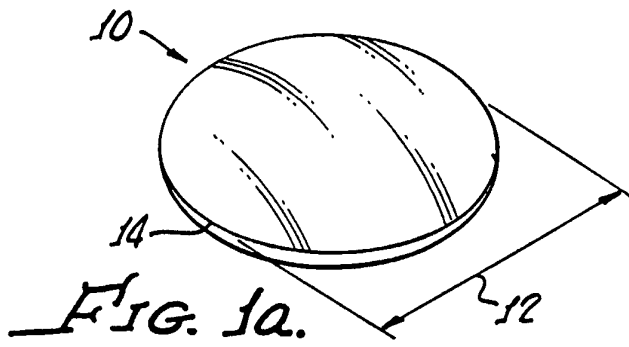
39. The process of claim 32 wherein said polymer has an equilibrium water content of about 57% to 90%.

40. The process of claim 33 wherein said polymer has an equilibrium water content of about 57% to 90%.

41. The process of claim 34 wherein said polymer has
5 an equilibrium water content of 57% to 90%.

42. The process of claim 35 wherein said polymer has an equilibrium water content of about 57% to 90%.

1/5



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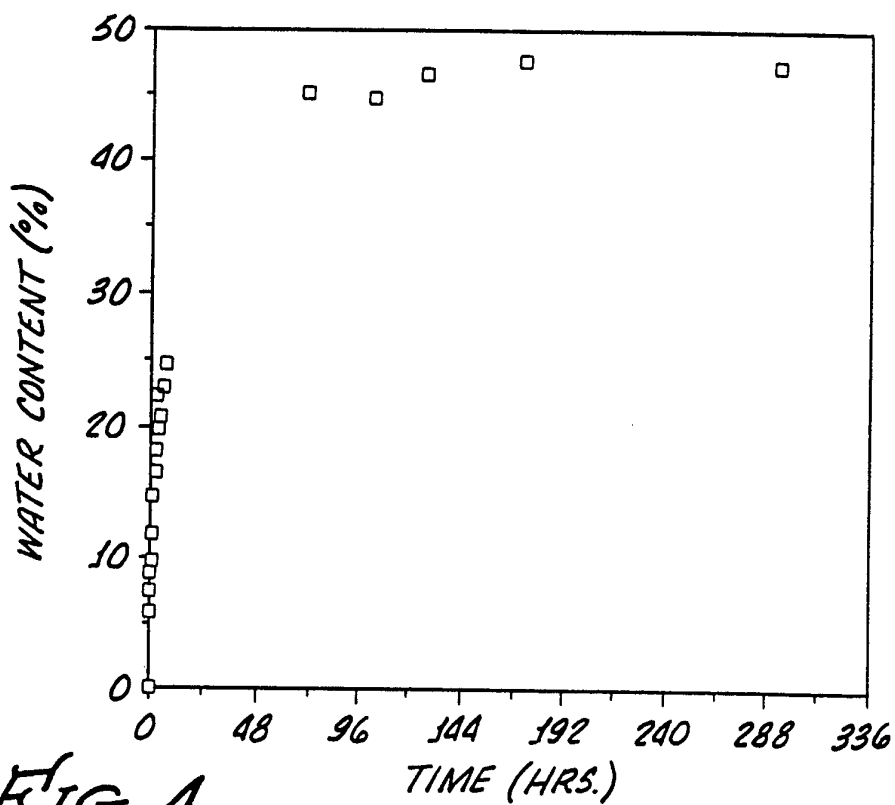


FIG. 4.

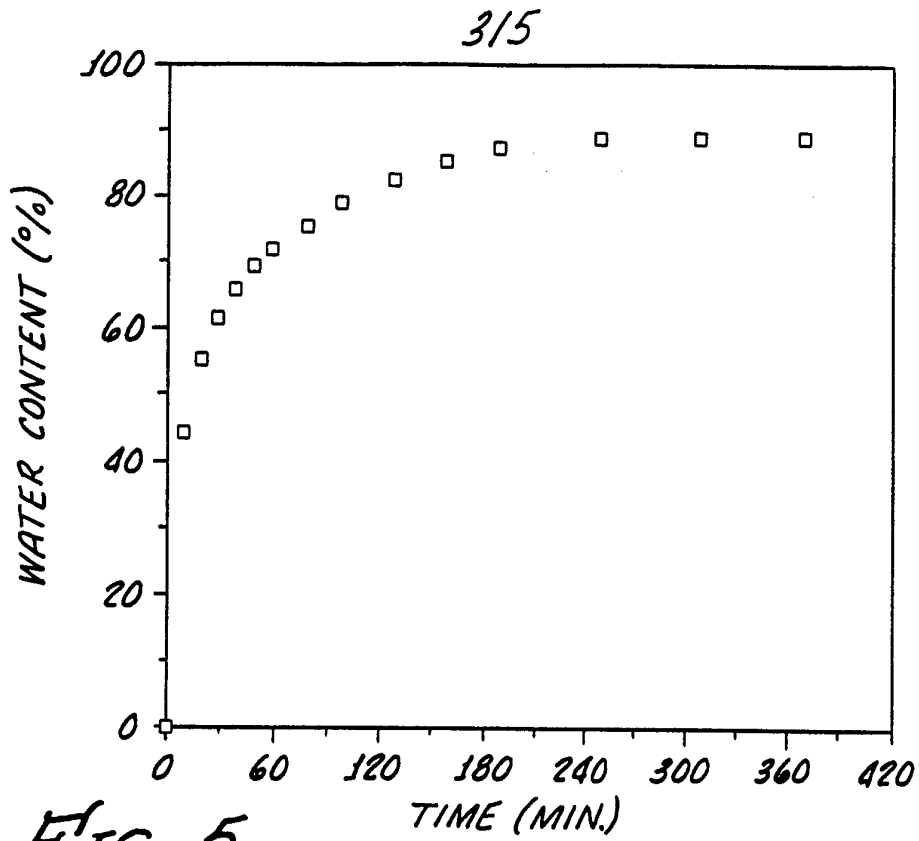


FIG. 5.

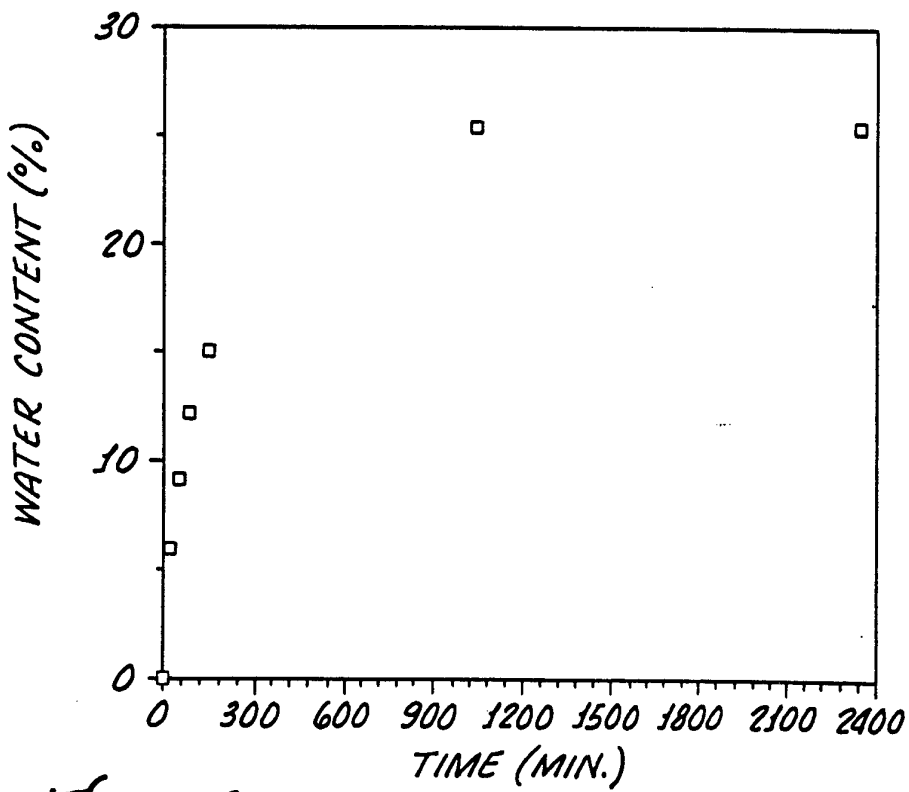


FIG. 6.

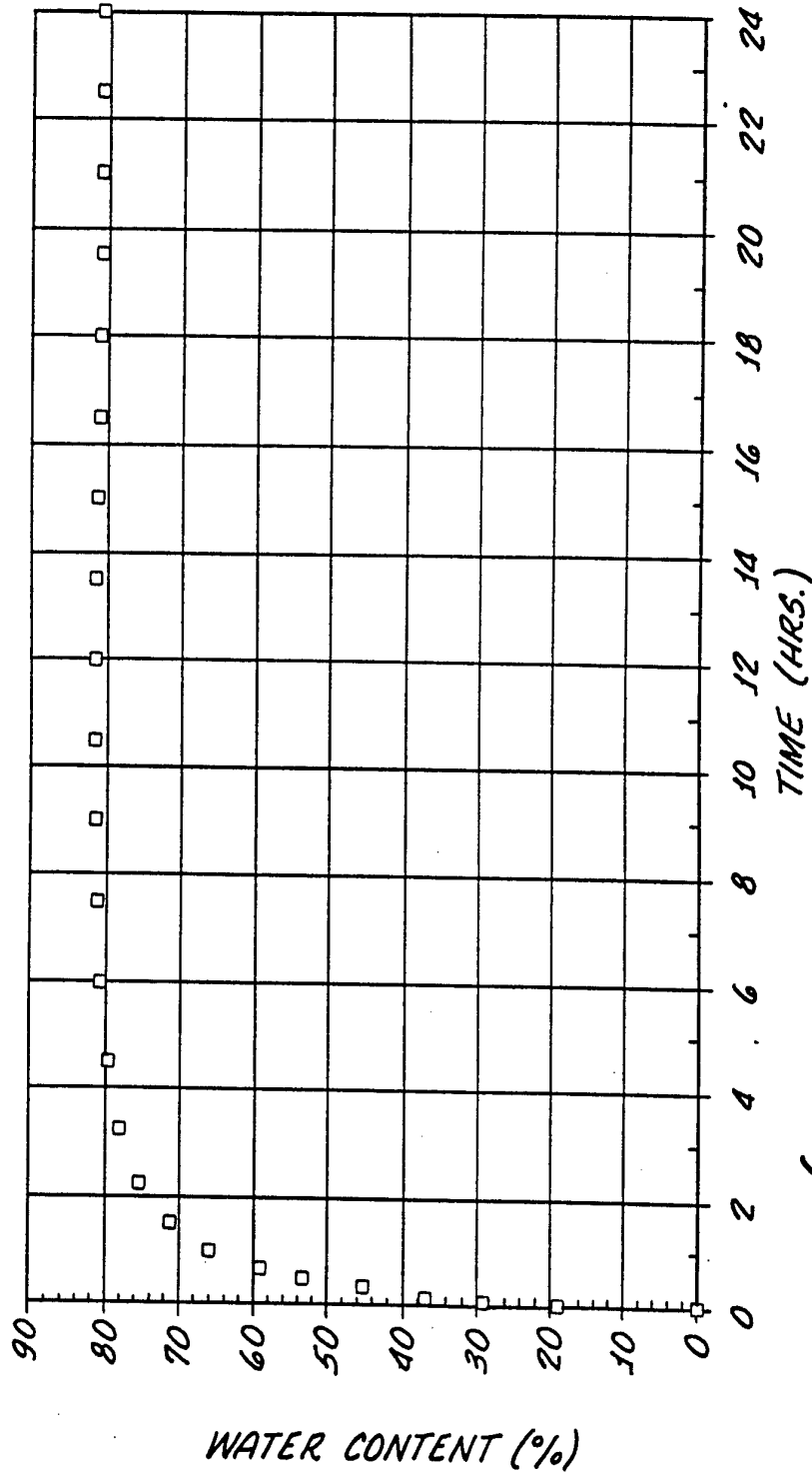


FIG. 7.

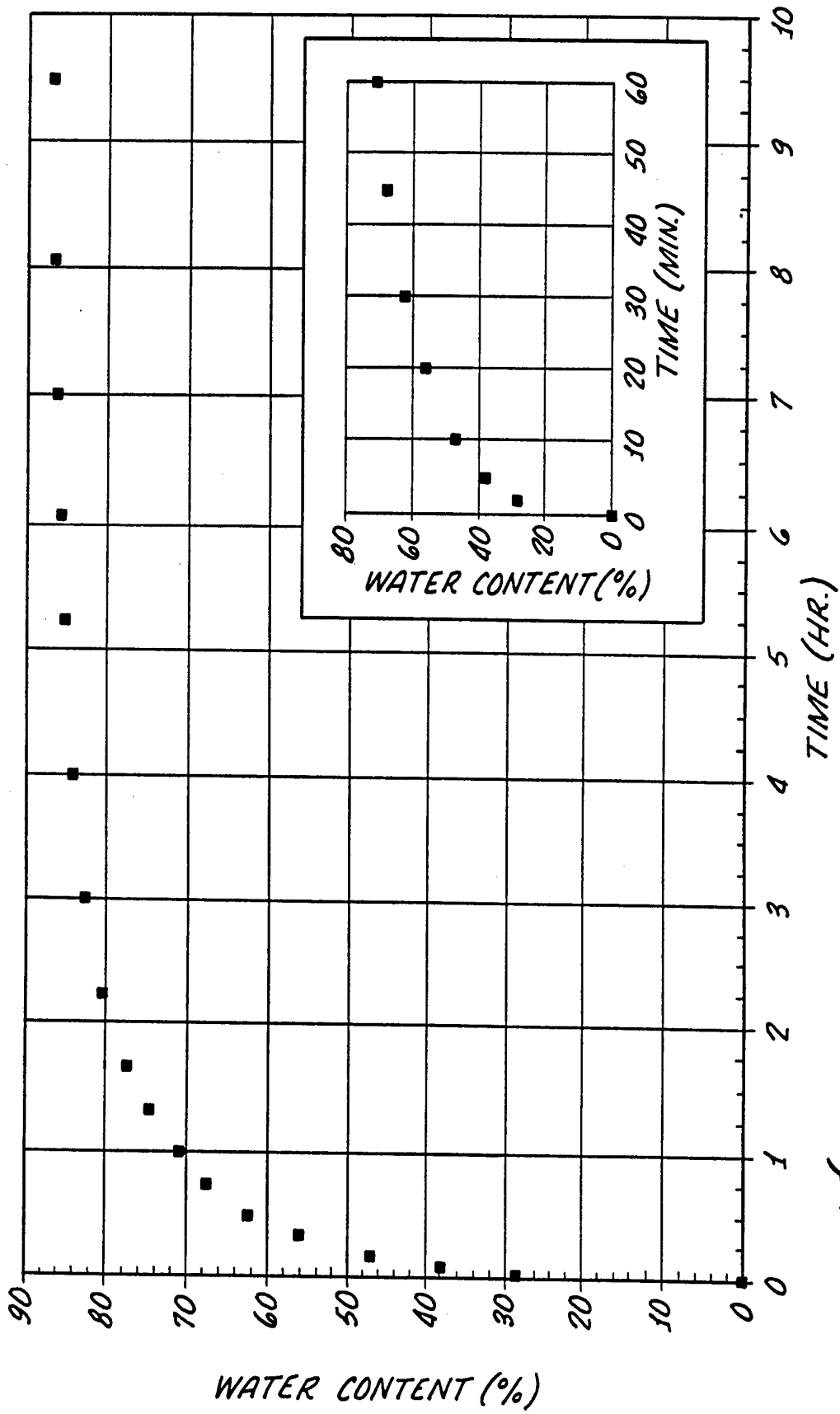


FIG. 8.

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US93/09121

A. CLASSIFICATION OF SUBJECT MATTER
 IPC(5) :B29D 11/00; C08L 39/04, 39/08; A61F 2/16
 US CL :264/1.7, 2.6, 2.7; 523/108; 524/555; 623/6
 According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
 Minimum documentation searched (classification system followed by classification symbols)
 U.S. : 264/1.7, 2.6, 2.7; 523/108; 524/555; 623/6

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X Y	US, A, 5,210,111 (GOLDENBERG ET AL) 11 MAY 1993. See col. 4, lines 6-26, col. 5, lines 11-28 and col. 6, line 58 to col. 7, line 13.	<u>1-21</u> 22-42
Y	US, A, 5,217,491 (VANDERBILT) 08 JUNE 1993. See col. 3, lines 33-55, col. 4, lines 19-55, col. 5, lines 49-68 and col. 6, lines 22-27.	22-42
Y	US, A, 4,813,954 (SIEPSE) 21 MARCH 1989. See col. 2, lines 50-60 and col. 4, lines 18-64.	22-42

Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be part of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family.
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 30 NOVEMBER 1993	Date of mailing of the international search report 11 FEB 1994
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Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. NOT APPLICABLE	Authorized officer <i>Renew award for</i> ANDREW E.C. MERRIAM Telephone No. (703) 308-2351
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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US93/09121

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US, A, 4,556,998 (SIEPSE) 10 DECEMBER 1985. See col. 4, lines 52-65 and col. 6, lines 13-59.	22-42