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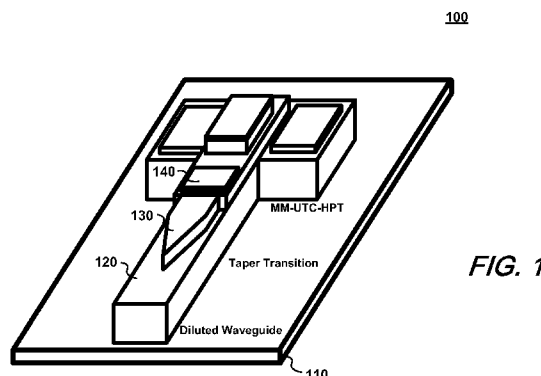
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(54) Title: OPTOELECTRONIC RECEIVER



(57) Abstract: An optoelectronic receiver and associated method of operation. The receiver comprises an optical waveguide, an electrical waveguide and one or more phototransistor amplifiers opto-electrically connecting the optical waveguide to the electrical waveguide.

OPTOELECTRONIC RECEIVER

FIELD OF DISCLOSURE

5 This disclosure relates generally to the field of optical communications and in particular to optoelectronic receivers.

BACKGROUND OF DISCLOSURE

10 Optoelectronic receivers are an essential component of contemporary optical communications systems and a variety of types have been developed and deployed. Of these types, optoelectronic receivers which employ avalanche photo detector (APD) technologies generally exhibit high sensitivity but poor power-handling capabilities. Optoelectronic receivers which employ pin photo detector technologies typically require an optical pre-amplifier or electronic amplifier to boost input signal
15 levels which unfortunately generates noise and signal delays.

SUMMARY OF DISCLOSURE

20 An advance is made in the art by an integrated InP heterojunction phototransistor-amplifier (HPT-amplifier) optoelectronic receiver and associated methods.

BRIEF DESCRIPTION OF THE DRAWING

 A more complete understanding of the disclosure may be realized by reference to the accompanying drawing in which:

25 **FIG. 1** is a perspective view of a simplified schematic diagram of an integrated traveling-wave uni-travel-carrier heterojunction phototransistor (TW-UTC-HPT) according to an aspect of the present disclosure;

FIG 2 is a simplified schematic of an InP UTC-HPT Receiver optoelectronic integrated circuit (OEIC) according to an aspect of the present disclosure;

30 **FIG 3** is a cross-sectional schematic of an exemplary HPT with underlying waveguide according to an aspect of the present disclosure;

FIG 4 is a schematic of a single-ended OEIC according to an aspect of the present disclosure;

FIG 5 is a schematic of a single-ended cascade UTC-HPT amplifier stage as employed in the embodiment of **FIG 4**;

5 **FIG 6** is a schematic of a balanced traveling wave UTC-HPT OEIC according to an aspect of the present disclosure;

FIG 7 is a schematic of a differential cascade HPT amplifier stage as employed in the embodiment of **FIG 6**; and

10 **FIG 8** is a schematic of a simplified multi-wavelength UTC-HPT OEIC according to an aspect of the present disclosure.

DESCRIPTION OF EMBODIMENTS

The following merely illustrates the principles of the various embodiments. It will thus be appreciated that those skilled in the art will be able to devise various
15 arrangements which, although not explicitly described or shown herein, embody the principles of the embodiments and are included within their spirit and scope.

Furthermore, all examples and conditional language recited herein are principally intended expressly to be only for pedagogical purposes to aid the reader in understanding the principles of the embodiments and the concepts contributed by the
20 inventor(s) to furthering the art, and are to be construed as being without limitation to such specifically recited examples and conditions.

Moreover, all statements herein reciting principles, aspects, and embodiments of the invention, as well as specific examples thereof, are intended to encompass both structural and functional equivalents thereof. Additionally, it is intended that such
25 equivalents include both currently known equivalents as well as equivalents developed in the future, i.e., any elements developed that perform the same function, regardless of structure.

Thus, for example, it will be appreciated by those skilled in the art that the diagrams herein represent conceptual views of illustrative structures depicting the
30 principles of the embodiments.

Turning now to **FIG 1** there is shown a perspective view of a simplified integrated multi-mode uni-travel carrier heterojunction photo-transistor (MM-UTC-HPT) assembly **100** according to an aspect of the disclosure. More specifically, the

MM-UTC-HPT assembly includes a substrate **110** onto which is integrated a diluted waveguide **120** which directs received optical signals (not specifically shown) into a tapered transition region **130** for reception and detection by a MM-UTC-HPT **140**.

In this embodiment shown, the base-collector junction of the HPT employs a uni-carrier design using a thin waveguide base region to detect optical signals and uses electron carriers for amplification and transport of detected optical signals. The diluted waveguide **120** and spot-size converter are integrated with the HPT thereby enhancing coupling efficiency to an optical fiber (not specifically shown) while delivering high optical power with low guiding loss. As will be described, mm-wave high power optoelectronic receivers may advantageously be produced when MM-UTC-HPTs are integrated with other high-speed HBTs.

Uni-Travel-Carrier photodiodes – as generally employed in embodiments according to the present disclosure – may utilize a very thin p+ absorption region in a reversed-biased photodiode in which photo-generated holes as majority carriers respond very fast within dielectric relaxation time, while photo-generated electrons drift quickly through thick depletion regions. Advantageously, UTC photodiodes exhibit a high cut-off frequency up to 325 GHz while accepting very high power optical signals. (See, for example, T.Ishibaashi et al., “Uni-traveling-carrier photodiodes”, *Tech. Dig. Ultrafast Electronics and Optoelectronics*” Opt. Soc. Amer., Washington, D.C., 166-168, 1997; Ito et al., “InP/InGaAs Uni-Traveling-Carrier Photodiode with 310 GHz Bandwidth”, *Electronics Letters*, v.36, pp.1809-1810, 12 OCT 2000).

Turning now to **FIG 2** there is shown a schematic diagram of a simplified InP UTC-HPT Receiver optoelectronic integrated circuit (OEIC) **200**. The receiver **200** is fabricated onto an InP substrate **210** integrating both uni-traveling carrier photodiodes with high frequency DHBT transistors **220** advantageously resulting in a receiver exhibiting broadband detection-amplification characteristics. A diluted waveguide **230** provides direct coupling of received optical signals (not shown) into the photo-HBTs which may thereby minimize losses.

While not specifically shown in **FIG 2**, the base-collector junction of the HPT uses a thin base region for detection of optical signals while fast electrons are used as charge carriers to transport detected optical signals and high speed amplification. Operationally, the low loss InP waveguide **230** – integrated within the OEIC -

distributes optical power (with appropriate delays) to multiple HPT's **220** contained within the structure. Multiple amplifier stages comprising the UTC-HPT and HBTs are integrated with a mm-wave coplanar transmission line **240**. The transmission line **240** collects any detected and amplified electrical signals produced at each stage and
5 coherently combines them into an electrical signal output to broadband electrical output port **245**.

As compared with conventional hybrid integration of high power UTC detectors, the integrated UTC-HPT according to the present embodiment may advantageously reduce and/or eliminate lossy high-frequency interconnects of RF
10 cabling and bond wires. In addition, the single chip implementation – as already noted – provides superior gain at mm-wave frequencies as light is delivered into the intrinsic base absorption region through the integrated InP optical waveguide **230**. Guided light traversing the waveguide **230** produces photocurrent directly in the base region of the HPT **220**, bypassing high base spreading resistance in the transistor. As
15 a result, high frequency performance at mm-wave frequencies is realized.

At this point, a number of features of the OEIC shown in **FIG 2** may be appreciated by those skilled in the art. More particularly, with conventional discrete waveguide photodiode(s), the distribution of photo-generated carriers oftentimes follows an exponential decay profile along an absorption layer that leads to a high
20 density of photo-generated carriers at the waveguide front end. To facilitate high power operation, the distributed waveguide approach described herein advantageously distributes the absorption along a length of the waveguide. In a preferred embodiment, the optical absorption is distributed among a number of UTC-HPTs coupled to the embedded low loss waveguide. In this configuration, a high input
25 optical power may be more efficiently absorbed by the distributed UTC-HPTs.

Turning now to **FIG 3**, there is shown a schematic cross section of a representative HPT with underlying optical waveguide according to an aspect of the present embodiment which may be advantageously employed in the OIEC. More specifically, the HPT **300** in this example includes a semi-insulating InP single crystal
30 substrate **310**, an InGaAlAs waveguide **320** disposed upon the substrate **310** and an NPN heterojunction bipolar transistor (HPT) **330** comprising a collector **329-1**, a base **329-2**, and an emitter **329-3**, disposed upon a waveguide sub-collector **325**. The

compositions and their functions are shown in their respective layers in the structure of **FIG 3**.

Those skilled in the art will appreciate that one exemplary approach to the fabrication of structures employed according to the present disclosure involves a deep etched mesa waveguide for distributing light to the individual phototransistors. In the schematic cross section of **FIG 3**, the waveguide core may be a ~200 nm thick InGaAlAs layer having an absorption edge of about 1.3 μm .

Advantageously, cladding may be formed by InP layers. As shown in **FIG 3**, the InP substrate **310** forms a lower cladding, while an extended InP sub-collector **325** forms an upper cladding. To provide electrical isolation and to reduce any free-carrier absorption in the waveguide **320**, n-doping in the extended InP subcollector **325** may be neutralized by implant isolation regions **327**.

While various thickness(s) of the particular layers shown in **FIG 3** are possible, it will be readily understood by those skilled in the art that the thickness of the waveguide core determines the lateral confinement as well as index and that the thickness of the collector **329** will be tailored for sufficient coupling to the InGaAs absorption layer (not specifically shown in **FIG 3**) such that any disturbances elsewhere in the waveguide are reduced – as the individual waveguide provides optical input to multiple phototransistors.

As may now be understood and appreciated, a broadband low-noise amplifier is needed in the receiver of an optical transmission system to convert a relatively small photodetector current into a rather large voltage sufficient to drive successive electrical circuits, such as a demultiplexer or a clock-and-data-recovery circuit (CDR). As already noted, in the OEIC such as that shown in **FIG 2**, the input power handling is enhanced as a result of the integrated waveguide and distributed HPT gain stages, while the overall gain and broad operating frequency is enhanced through the effect of an integrated broadband traveling InP HPT pre-amplifier on the same OEIC. By delivering an optical signal directly into an intrinsic absorption region of HPT – bypassing the parasitic electrical contact of the base – such an OEIC may advantageously extend the operating frequency while exhibiting less noise than a hybrid combination of a discrete photodiode and HBT amplifier.

Turning now to **FIG 4**, there is shown a schematic of a representative single-ended, traveling wave UTC-HPT integrated circuit **400**. As can be seen from that

figure, the circuit **400** generally comprises an optical waveguide **410**, an electrical waveguide **420**, and a number of HPT-Amplifiers **430[1]**, **430[2]**, ..., **430[n]**, opto-electrically connecting the optical and electrical waveguides. As can be appreciated such HPT-Amplifiers may be single ended UTC-HPT amplifiers of which a
5 representative simple schematic is shown in **FIG 5**.

With continued reference to **FIG 4**, those skilled in the art will readily appreciate that when optical energy **450** is introduced into the optical waveguide **410** it propagates along that waveguide. Accordingly, upon the introduction of light to an entrance to the waveguide **410** – which is shown enhanced by the application of an
10 anti-reflective coating **440** to a face of the entrance – the light so introduced propagates therealong. Accordingly, when a portion of the propagating light **450[1]** encounters a first single-ended HPT-Amplifier stage **430[1]**, an electrical current e_1 is produced in the electrical waveguide **420** through the effect of the HPT-amplifier stage **430[1]**.

Continuing with this discussion of **FIG 4**, when a remaining portion of the propagating light **450[2]** encounters a second single-ended HPT-Amplifier stage **430[2]**, an electrical current e_2 is produced in the electrical waveguide **420** through the effect of the HPT-amplifier stage **430[2]**. Similarly, when a remaining portion of the propagating light **450[n]** encounters a final single-ended HPT-Amplifier stage **430[n]**,
15 an electrical current e_n is produced in the electrical waveguide **420** through the effect of the HPT-amplifier stage **430[n]**.

One result of this photo-receiver/pre-amplifier architecture - and as can be readily appreciated by those skilled in the art – is that as the propagating light encounters successive HPT-Amplifier stages, a portion of that light is “tapped-off”
25 and results in the production of an electrical current added to that already in the electrical waveguide. Consequently, as the optical signal input to the optical waveguide gets smaller as it traverses the optical waveguide, the electrical output gets (much) larger. Consequently, the bandwidth of a device so constructed exhibits an enhanced bandwidth along with an increase in isolation between input and output.

It is notable that when describing the device shown in **FIG 4**, the phase difference of the optical signals propagating therethrough is such that the neighboring output electrical signals add to one another. In this manner, the optical phase is effectively matched to the electrical waveguide.
30

Turning now to **FIG 6**, there is shown a schematic of a balanced traveling wave UTC-HPT receiver **600**. More particularly the receiver **600** comprises a pair of optical waveguides **610[1]**, **610[2]** opto-electrically connected to a pair of electrical waveguides **620[1]**, **620[2]** via a number of differential HPT-Amplifiers **630[1]**, **630[2]**, ... **630[n]** – a representative circuit diagram of which is shown schematically in **FIG 7**.

As shown in **FIG 6**, optical energy comprising an input optical signal **650** and a local oscillator signal **675** (which may be generated by a laser – not specifically shown) is applied to the inputs of – for example - a multi-mode interference (MMI) coupler **677**. As described previously, the input coupling of the applied signals may be enhanced through the effect of one or more anti-reflective coatings **651**, **676** applied to surfaces at which the signals are received.

From the MMI coupler **677**, the input optical signals (optical signals and local oscillator signals) are directed to the optical waveguides **610[1]**, **610[2]** along which the light signals propagate. Accordingly, when a portion of the propagating light **660[1]**, **661[1]** encounters a first differential HPT-Amplifier stage **630[1]**, an electrical current e_1 is produced in the electrical waveguide **620[1]** while an electrical current \bar{e}_1 is produced in the electrical waveguide **620[2]** through the effect of the HPT-amplifier stage **630[1]**.

When the remaining portion(s) of the propagating light **660[2]**, **661[2]** encounters a second differential HPT-Amplifier stage **630[2]**, an electrical current e_2 is produced in the electrical waveguide **620[1]** while an electrical current \bar{e}_2 is produced in the electrical waveguide **620[2]** through the effect of the HPT-amplifier stage **630[2]**. Similarly, when a further remaining portion of the propagating light **660[n]**, **661[n]** encounters a final differential HPT-Amplifier stage **630[n]**, an electrical current e_n is produced in the electrical waveguide **620[1]** while an electrical current \bar{e}_2 is produced in the electrical waveguide **620[2]** through the effect of the HPT-amplifier stage **630[n]**.

Similarly to the case with the single ended device described previously – with the balanced device shown in **FIG 6** - as the optical input gets smaller, the electrical output and electrical output(OVERBAR) get (much) larger. As a result, the bandwidth of a device so constructed may exhibit an enhanced bandwidth along with an increase in isolation between input and output.

Finally turning now to **FIG 8**, there it shows a simplified schematic of an additional embodiment of a TW-UTC-HPT OEIC which may advantageously provide a multi-wavelength specificity. More particularly, the **OEIC 800** shown in **FIG 8** includes an optical waveguide **810** and an electrical waveguide **820** opto-electrically
5 connected by a plurality of photo-receiver/amplifiers **830[1]**, **830[1]**, **830[3]**, ... , **830[n]**. As with prior embodiments, optical signals input to optical waveguide **810** are detected successively by the series of cascaded photo-receivers/amplifiers **830[1]**, **830[1]**, **830[3]**, ... , **830[n]**. As discussed previously, the optical signal detected gets smaller as it propagates along the optical waveguide **810**, while the electrical output
10 signal gets larger.

Notably, the exemplary configuration shown in **FIG 8** includes photo-receiver/amplifiers (PRA) that are more or less selective to particular wavelengths of light than their neighbors. More particularly, PRA **830[1]** is shown selective to λ_1 , while selective PRA's **830[2]**, **830[3]**, ..., **830[n]** are shown as selective to λ_2 , λ_3 , ..., λ_n , respectively. Of course, in an actual embodiment the particular selectivity may be
15 ordered/repeated/selected as desired.

At this point, while we have discussed and described the invention using some specific examples, those skilled in the art will recognize that our teachings are not so limited. Accordingly, the invention should be only limited by the scope of the claims
20 attached hereto.

We Claim:

1. An optoelectronic apparatus comprising:
 - an optical waveguide;
 - an electrical waveguide; and
 - one or more phototransistor-amplifiers opto-electrically connecting the optical waveguide to the electrical waveguide.
2. The optoelectronic apparatus of claim 1, wherein the one or more phototransistors-amplifiers are wavelength-specific.
3. The optoelectronic apparatus of claim 1, wherein the one or more phototransistor-amplifiers are optically coupled to the optical waveguide and electrically coupled to the electrical waveguide.
4. The optoelectronic apparatus of claim 1, wherein said optical waveguide is configured to guide optical radiation along a propagation axis therein and said phototransistor-amplifiers are positioned such that they may individually receive a portion of the optical radiation.
5. The optical apparatus of claim 4, wherein said phototransistor-amplifiers are positioned such that an electrical output current produced by each is additive to an output current available at the electrical waveguide.
6. The optical apparatus of claim 4, wherein said phototransistor-amplifiers comprise an emitter region, a base region, a collector region and a subcollector region overlying said waveguide which in-turn is disposed upon a substrate.
7. The optical apparatus of claim 6, wherein said phototransistor-amplifiers further comprise a tapered transition region for guiding light from the waveguide into the phototransistor.

8. A method for receiving an optical signal comprising the steps of:
 - receiving the optical signal into an optical waveguide such that it is guided therein;
 - detecting a portion of the guided optical signal through the effect of a phototransistor-amplifier optically coupled to the optical waveguide and producing an electrical current in an electrical waveguide in response; and
 - detecting a remaining portion of the guided optical signal through the effect of another phototransistor amplifier optically coupled to the optical waveguide and producing additional electrical current in the electrical waveguide in response.
9. The method of claim 8 wherein said electrical currents are combined with one another such that an overall output electrical current is produced which is substantially equal to the sum of all the individual electrical currents produced.
10. The optical apparatus of claim 8 wherein said phototransistor amplifiers are wavelength specific and the electrical current produced is indicative of a first wavelength component of the optical signal while the additional electrical current produced is indicative of a second wavelength component of the optical signal

100

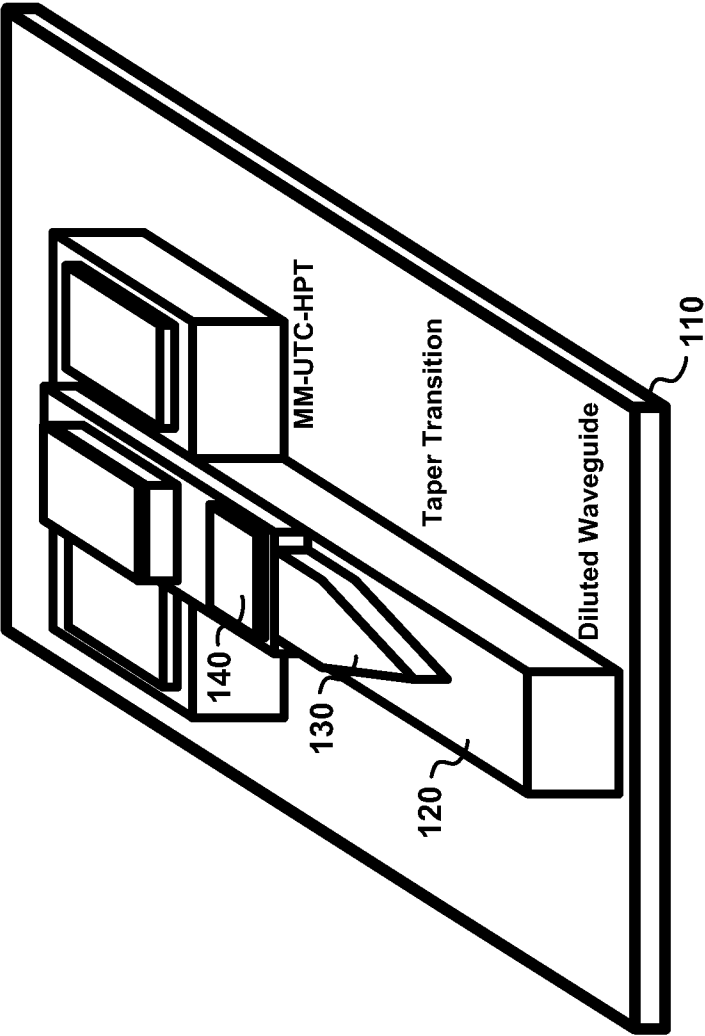


FIG. 1

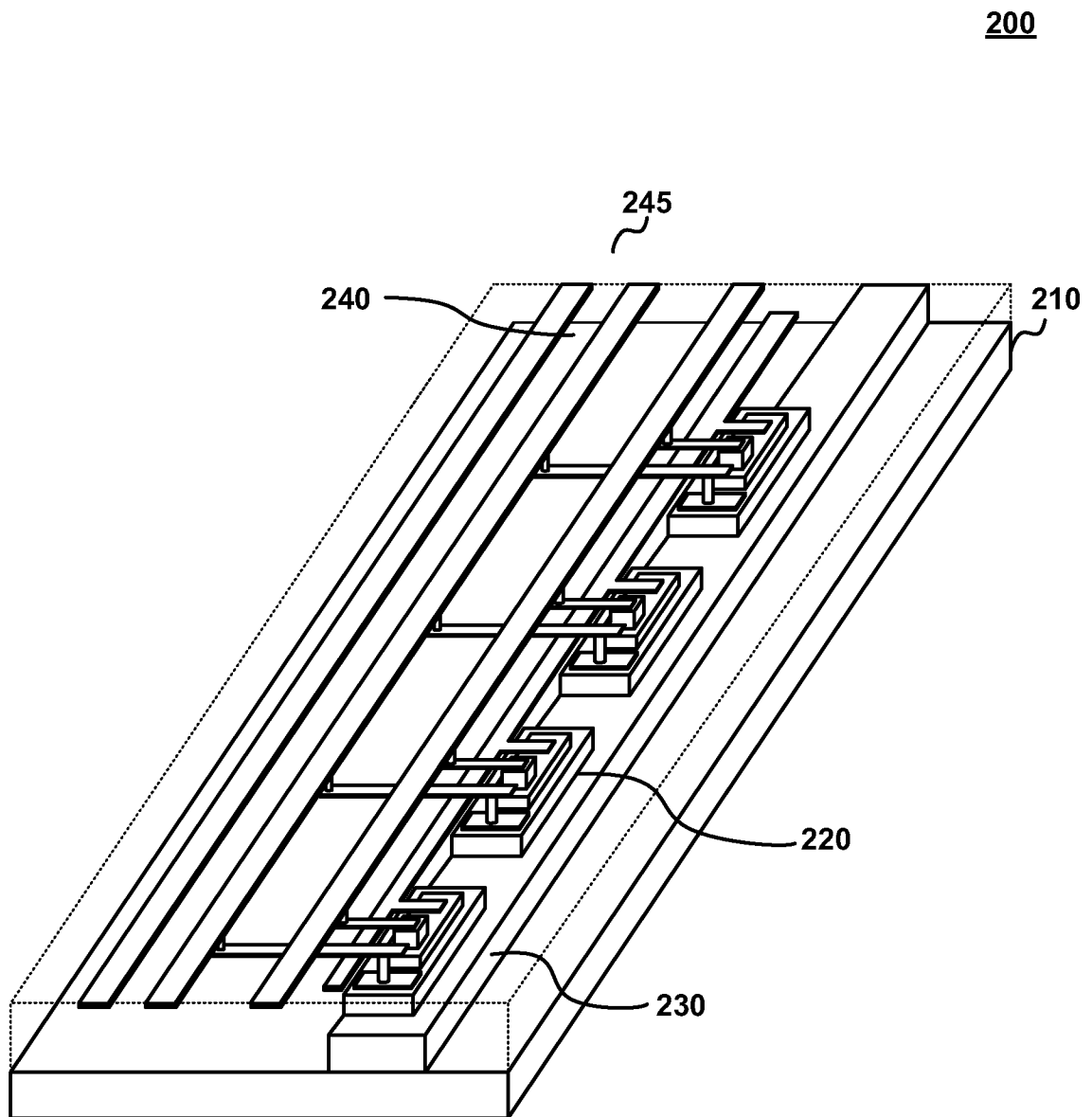


FIG. 2

300

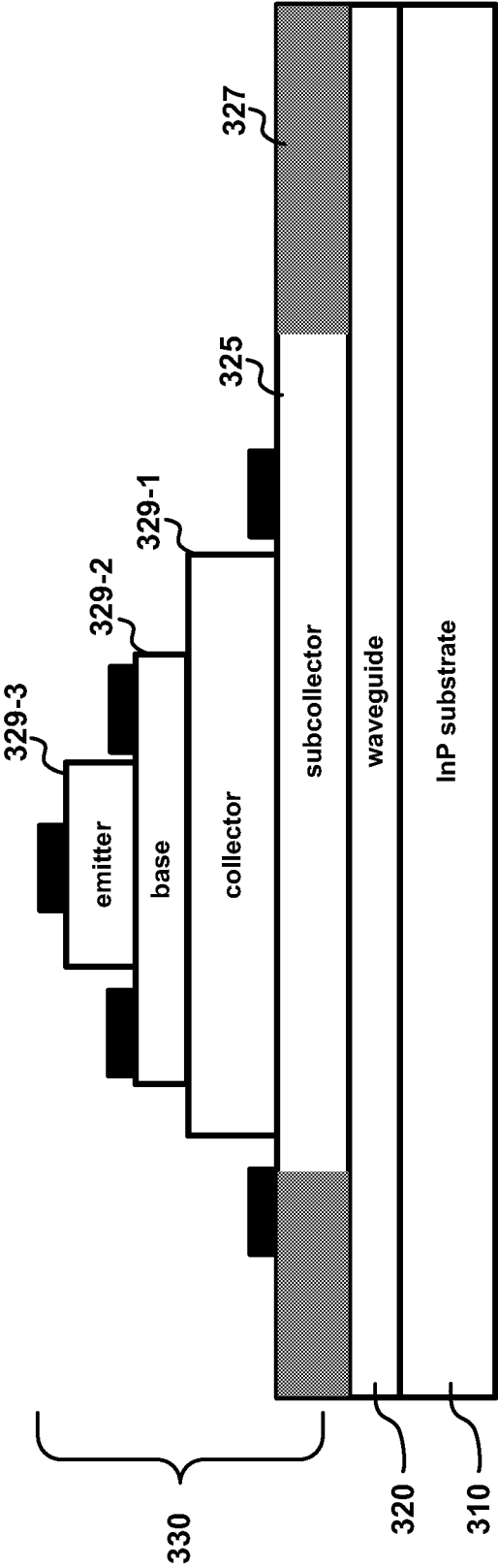


FIG. 3

400

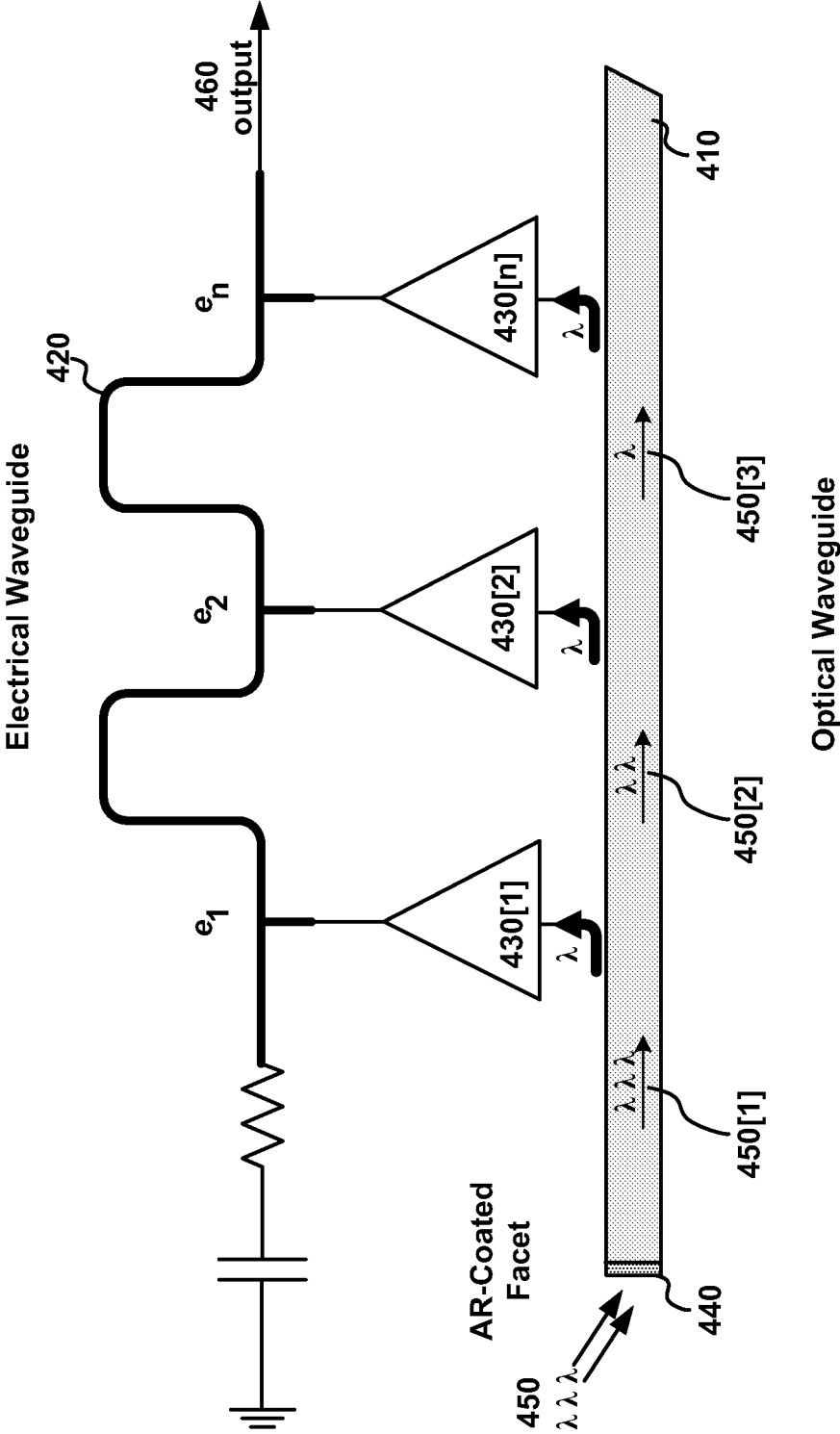


FIG. 4

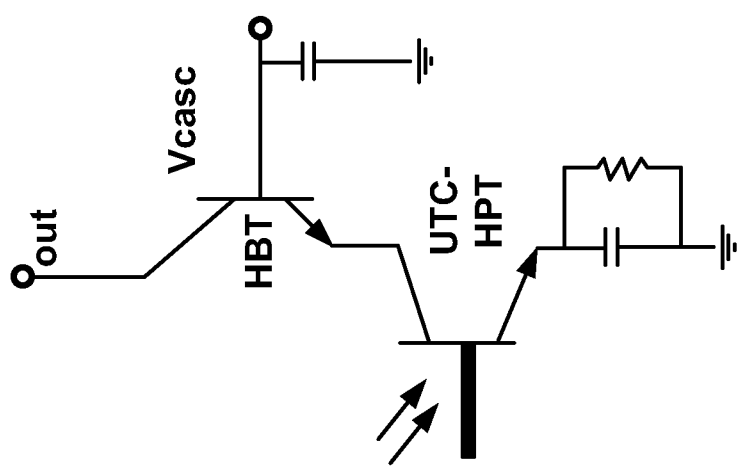
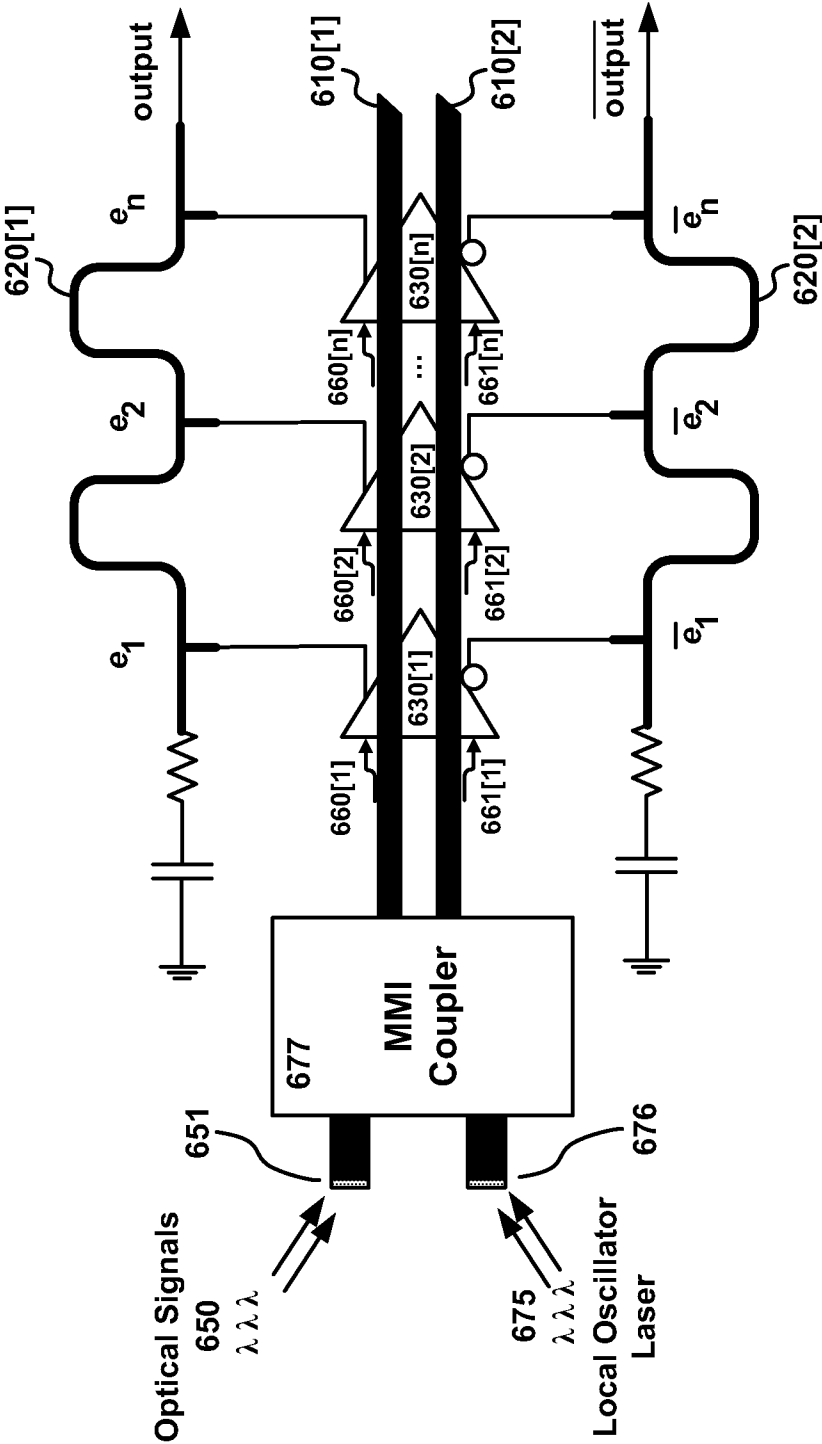


FIG. 5

600

Balanced Distributed Electrical Waveguide



Balanced Distributed Electrical Waveguide

FIG. 6

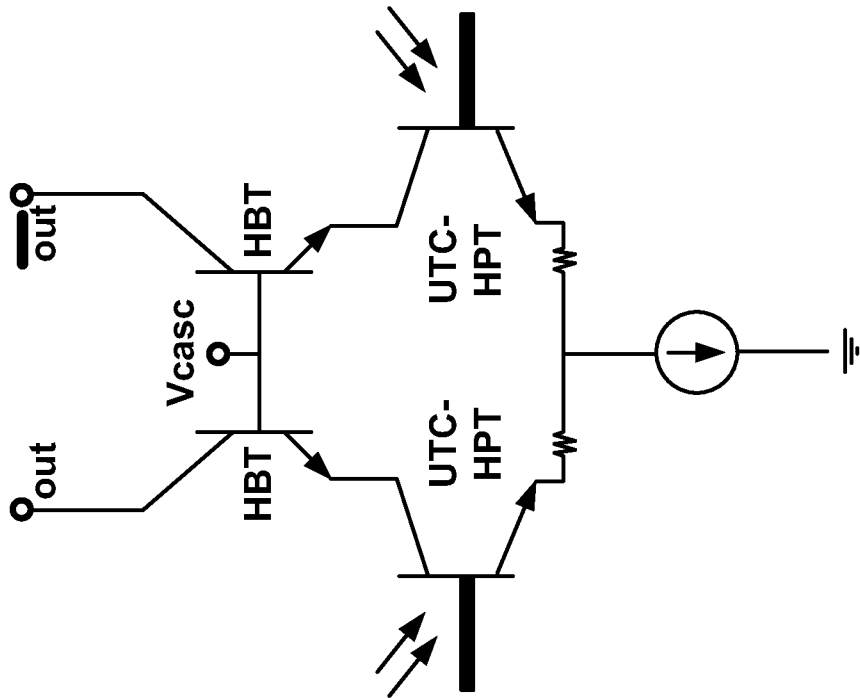


FIG. 7

800

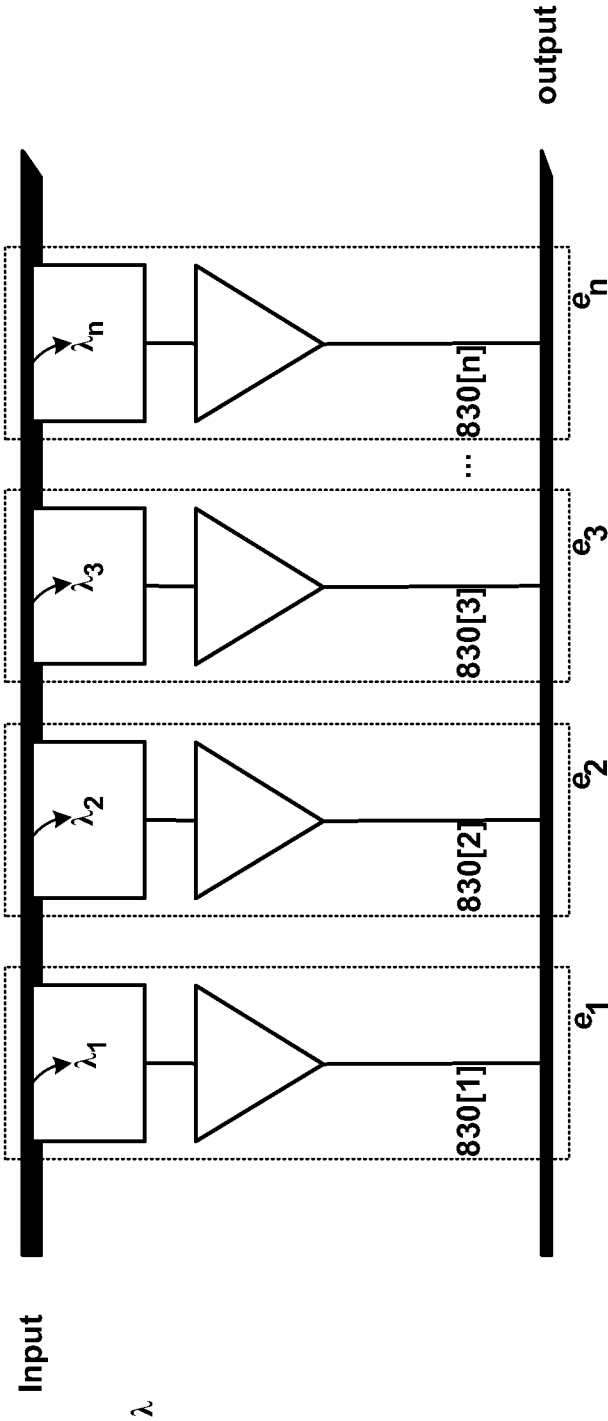


FIG. 8

INTERNATIONAL SEARCH REPORT

International application No

PCT/US2010/028205

A. CLASSIFICATION OF SUBJECT MATTER

INV. H04B10/158 G02B6/42 H01L27/14 H01L31/11
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

H04B H01L G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal, WPI Data, INSPEC

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2007/014508 A1 (CHEN YOUNG-KAI [US] ET AL CHEN YOUNG-KAI [US] ET AL) 18 January 2007 (2007-01-18)	1-4,6,7
Y	* abstract paragraphs [0002] - [0011] paragraphs [0020] - [0023] paragraphs [0032] - [0038] figures 1, 2 ----- -/--	5,8-10



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

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Date of the actual completion of the international search

18 June 2010

Date of mailing of the international search report

25/06/2010

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INTERNATIONAL SEARCH REPORT

International application No

PCT/US2010/028205

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>HOUSTON P A ET AL: "InP/InGaAs Heterojunction Phototransistors for Optoelectronic Receivers" SEMICONDUCTOR ELECTRONICS, 2004. ICSE 2004. IEEE INTERNATIONAL CONFERENCE ON, IEEE, PISCATAWAY, NJ, USA LNKD-DOI:10.1109/SMELEC.2004.1620821, 7 December 2004 (2004-12-07), pages A1-A5, XP010910225 ISBN: 978-0-7803-8658-7 the whole document</p>	1-4,6,7
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X	<p>US 2003/087466 A1 (WANG YUQI [HK] ET AL) 8 May 2003 (2003-05-08) paragraphs [0001] - [0005] paragraph [0020] paragraph [0043] figures 1, 2, 6</p>	1-4,6,7
Y	<p>CHARLES L GOLDSMITH ET AL: "Principles and Performance of Traveling-Wave Photodetector Arrays" IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES, IEEE SERVICE CENTER, PISCATAWAY, NJ, US, vol. 45, no. 8, 1 August 1997 (1997-08-01), XP011036903 ISSN: 0018-9480 the whole document</p>	5,8-10

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2010/028205

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