



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁵ : G01C 19/72	A1	(11) International Publication Number: WO 92/11509 (43) International Publication Date: 9 July 1992 (09.07.92)
---	----	---

(21) International Application Number: PCT/US91/09459

(22) International Filing Date: 16 December 1991 (16.12.91)

(30) Priority data:
633,545 21 December 1990 (21.12.90) US

(71) Applicant: HONEYWELL INC. [US/US]; Honeywell Plaza, Minneapolis, MN 55408 (US).

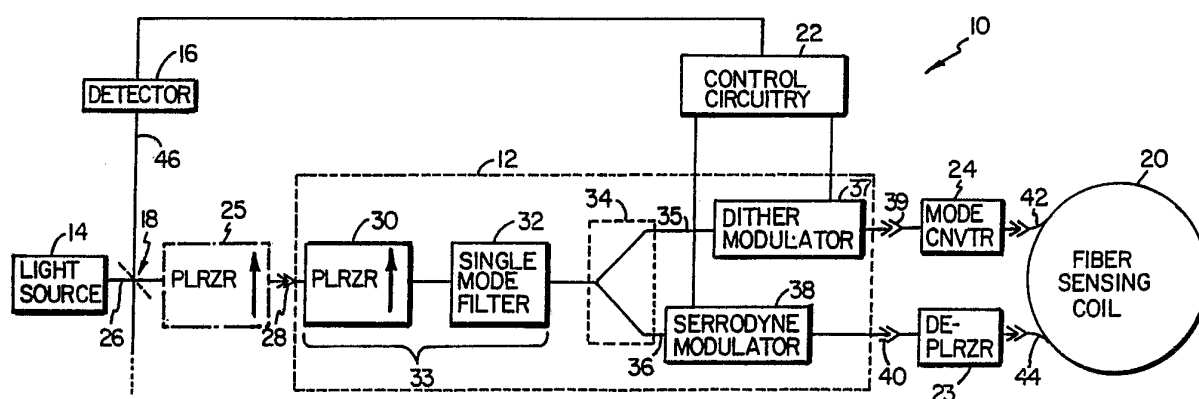
(72) Inventor: FERRAR, Carl, M. ; 114 Wildflower Road, East Hartford, CT 06118 (US).

(74) Agent: PAJAK, Robert, A.; Honeywell Inc., Honeywell Plaza, MN12-8251, Minneapolis, MN 55408 (US).

(81) Designated States: AT (European patent), BE (European patent), CA, CH (European patent), DE (European patent), DK (European patent), ES (European patent), FR (European patent), GB (European patent), GR (European patent), IT (European patent), JP, LU (European patent), MC (European patent), NL (European patent), SE (European patent).

Published
With international search report.

(54) Title: FIBER OPTIC GYRO



(57) Abstract

A low cost fiber optic gyro includes a Sagnac interferometer configured in a minimum reciprocal configuration and modified to use a 0.8 micron wavelength laser diode as the interferometer light source and 1.3 micron, single-mode fiber for the sensing coil.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	ES	Spain	MG	Madagascar
AU	Australia	FI	Finland	ML	Mali
BB	Barbados	FR	France	MN	Mongolia
BE	Belgium	GA	Gabon	MR	Mauritania
BF	Burkina Faso	GB	United Kingdom	MW	Malawi
BG	Bulgaria	GN	Guinea	NL	Netherlands
BJ	Benin	GR	Greece	NO	Norway
BR	Brazil	HU	Hungary	PL	Poland
CA	Canada	IT	Italy	RO	Romania
CF	Central African Republic	JP	Japan	SD	Sudan
CG	Congo	KP	Democratic People's Republic of Korea	SE	Sweden
CH	Switzerland	KR	Republic of Korea	SN	Senegal
CI	Côte d'Ivoire	LI	Liechtenstein	SU ⁺	Soviet Union
CM	Cameroon	LK	Sri Lanka	TD	Chad
CS	Czechoslovakia	LU	Luxembourg	TC	Togo
DE ⁺	Germany	MC	Monaco	US	United States of America
DK	Denmark				

⁺ Any designation of "SU" has effect in the Russian Federation. It is not yet known whether any such designation has effect in other States of the former Soviet Union.

Description

Fiber Optic Gyro

Technical Field

This invention relates to fiber optic gyros, and
5 more particularly to optical interferometer type
rotation sensors.

Background Art

Measurement of rotation rate is required in
applications ranging from robotic and ballistic missile
10 control, to aircraft and spacecraft navigation. Performance accuracy ranges from 0.001 to 0.01 degrees /
hour for Inertial Grade spacecraft/aircraft navigation
systems (10^{-3} to 10^{-4} of earth's 15 degrees/hour
rotation rate), through Moderate Grade sensing accura-
15 cies of 0.02 to 1.0 degrees/second. Intermediate Grade
performance is in the 0.1 to 10 degrees/ hour range.

Although spacecraft navigation usually relies on
spinning wheel gyros, advances in laser technology have
allowed dual laser beam gyros ("laser gyros") to be
20 used in high performance applications such as aircraft
navigation systems. The laser gyro offers fast start-
up, small size, lower cost, and most importantly the
absence of moving mechanical parts. An outgrowth of
the laser gyro is the fiber optic gyro (or "FOG"),
25 which is an alternative type
of interferometric rotation sensor.

The FOG can be smaller, more rugged, and less
costly than the laser gyro, making it ideally suited
for lower performance (Moderate and Intermediate Grade)
30 applications in the field of advanced projectiles.

2

Projectile applications for which the FOG is particularly well suited are roll attitude determination, body rate sensing, and seeker stabilization.

The FOG uses a Sagnac interferometer to measure rotation based on the principle that the transit time of an optical signal propagating through a fiber optic loop rotating about an axis perpendicular to its plane, varies with the loop rotation rate. The transit delay for two optical signals traversing the loop in opposite directions creates a Sagnac phase differential that is proportional to loop rotation rate:

$$S = \frac{2\pi L d}{\lambda * c} * \Omega \quad (\text{Equation 1})$$

where: S is the Sagnac phase difference in radians, L is the length of the fiber loop, d is the loop diameter, λ is the optical signal wavelength, c is the speed of light, and Ω is the loop rotation rate in radians/sec.

Phase detection sensitivity may be increased by modulating both optical signals with a sinusoidal phase modulator positioned at one end of the loop. The optical transit time delay causes the modulator to act on the counter circulating light beams at different times, dithering the phase difference magnitude and permitting use of sensitive AC processing to detect rotation-induced phase differences.

When counter propagating signals of unit intensity are combined interferometrically, the intensity (I) is:

$$I = 1/2 * (1 + \cos P) \quad (\text{Equation 2})$$

where P is the total phase difference (Sagnac and phase modulation).

The intensity I versus Sagnac phase difference relationship is a cosine function. At zero rotation the phase difference is zero and the signals interfere

constructively to produce a maximum intensity. Loop rotation creates a phase differential, causing the signals to destructively interfere and reduce the intensity.

- 5 Bessel expansion of the intensity expression at the modulation frequency (f) produces the rotational velocity component:

$$F = k \sin(S) \quad (\text{Equation 3})$$

$$\text{where } k = 2J_1[2A \sin(\pi f T)], \quad (\text{Equation 4})$$

- 10 and the term $2A \sin(\pi f T)$ is the dithered phase difference modulation of amplitude (A) and modulation frequency f. The coil transit time is T and, if (A) is fixed, F is maximized when $f = 1/2T$; the coil eigen-frequency.

- 15 The analog value of F can be measured directly as an indication of rotation, or the signal amplitude can be continuously nulled by a closed loop serrodyne modulator which adds an optical phase bias in opposition to the Sagnac phase difference. This is a repetitive linearly ramped phase modulator positioned at one
20 end of the fiber coil. A peak ramp amplitude of 2π radians produces an effectively constant phase difference bias between the oppositely directed beams. The ramp repetition frequency, which is proportional to the
25 phase bias amplitude, provides a measurable representation of the loop rotation rate.

- The rotation sensing accuracy critically depends on the counter propagating signals travelling identical ("reciprocal") optical paths at zero rotation rate (and
30 zero applied bias). The necessary reciprocity can be assured by arranging the optic elements in a "minimum reciprocal configuration" which requires the optical signals to pass through a common single-spatial-mode filter and a single-polarization filter when propa-
35 gating from the source to the sensing coil and from the

4

coil to the detector. This ensures that the counter propagating optical signals received by the detector will travel identical paths, associated with a single spatial mode and a single polarization, even if

5 multiple spatial modes and polarizations exist in the optical path due, for example, to fiber birefringence effects and scattering and cross-coupling between spatial modes.

In practice, when the filtering is imperfect, the
10 FOG offset errors associated with residual polarization and spatial-mode-related non-reciprocity (as well as several other types of errors) may be reduced through use of a broadband, short coherence length optical source and high birefringence optic fiber in the
15 sensing coil. This makes the selected mode counter propagating waves incoherent with certain cross coupled waves.

The FOG offers the potential for good performance and low cost. Components required for FOG fabrication
20 are readily available at wavelengths near 0.8 and 1.3 microns. The longer wavelength offers the advantage of: generally lower light loss, easier coupling of components, and greatly reduced photorefractive effects in LiNbO3 integrated optic devices.

25 The selection of components, however, affects the cost/ performance tradeoff. If low cost is a primary objective, it may be difficult to choose between operation at the 1.3 micron wavelength for which communication grade fiber is readily available at low
30 cost, but the most appropriate light sources are very expensive, or operation at the 0.8 micron wavelength at which suitable inexpensive laser sources are readily available but the fiber is expensive.

Disclosure of Invention

The object of the present invention is to provide a low cost rotation sensor design for use in moderate and intermediate grade fiber optic gyros.

5 According to the present invention, a Sagnac interferometer is provided in a known minimum reciprocal configuration, including a single polarization filter and a single spatial mode filter located in the common light path between the source/detector and the
10 sensing loop, but which further includes spatial mode conversion in the sensing loop to permit use of sensing-loop fiber which may be multi-moded at the wavelength of the interferometer light source (e.g. a 1.3 micron single-mode fiber sensing coil with a 0.8
15 micron wavelength laser diode light source) to retrieve at least a minimum level of optical power from undesired spatial modes into the desired spatial mode.

In further accord with the present invention, the sensing loop single mode fiber is non-polarization
20 maintaining fiber, and the interferometer further comprises a depolarizer located in the sensing loop to prevent signal fading.

In the prior art the use of multi-mode fiber for the sensing coil fiber is usually considered inappropriate.
25 The conventional multi-mode fiber supports a large number of modes and the high degree of single-mode filtering then required to ensure reciprocity becomes impractical because it extracts and sends to the detector only a very small fraction of the available light. I have found, however, that the required
30 filtering can be incorporated without unacceptably degrading the detected light levels if the sensing loop fiber supports only a small number of modes, and if mode-conversion means in the sensing loop ensures that

a reasonable fraction of the light in any undesired modes is returned to the desired mode for detection.

These and other objects, features, and advantages of the present invention will become more apparent in
5 light of the following detailed description of a best mode embodiment thereof, as illustrated in the accompanying Drawing.

Brief Description of Drawing

The sole Drawing figure is a system block diagram
10 of a rotation sensor according to the present invention.

Best Mode for Carrying Out the Invention

As known, the minimum reciprocal configuration Sagnac interferometers yield enhanced FOG performance
15 by minimizing output errors associated with undesired polarizations and spatial modes. Prior art high performance FOG systems have typically required, in addition, the use of low coherence superluminescent diode (SLD) light sources and highly birefringent
20 (polarization preserving) sensing loop fiber to further reduce these errors. The prices, however, of the SLD and polarization preserving fiber are a significant portion of the overall sensor cost.

The present invention comprises a minimum reciprocal
25 rocal configuration Sagnac interferometer, modified to permit use of a low cost laser diode optical source (e.g., at 0.8 micron wavelength) and low cost non-polarization-preserving sensing coil fiber (e.g., fiber which is single-moded at 1.3 microns but may be moderately multi-moded at the source wavelength).
30 The minimum reciprocal configuration in combination with added components described hereinafter, produces a rotation sensor suitable for use in intermediate grade

FOGs but at a significantly lower cost than the prior art devices.

Referring to Fig. 1, an interferometer according to the present invention 10, includes an integrated optic chip (IOC) 12, a light source 14, light detection circuitry 16, an output tap 18 (which may be a directional coupler or a beam splitter), a fiber optic sensing coil 20, and control circuitry 22. As described in detail hereinafter, the present interferometer further includes a depolarizer 23 and a mode converter 24 connected between the IOC 12 and the sensing loop 20. An optional polarizer 25 (shown in phantom) may be located between the light source and the IOC.

The light source 14 comprises a multi-mode low coherence (wide bandwidth) 0.8 micron wavelength laser diode. It is desirable in an interferometric FOG to use an optical source with a wide line width (low coherence) and high power coupling into an optical fiber. Superluminescent diodes (SLDs) have been used extensively in high performance FOG systems because they offer a good compromise between power coupling and line width. SLDs, however, are very expensive due to low volume production. Alternatively, multi-mode laser diodes are available with 2-3 nanometer bandwidths (about one-fifth that of SLDs but sufficient to ensure reasonably low coherence) and with coupled optical output powers approaching one milliwatt, but at less than one tenth the cost of the SLD. This type of laser diode has been selected as the best cost to performance trade-off for the interferometer light source.

The source provides the light beam on output fiber 26 to the tap 18. The tap rejects a portion of the light (e.g., 50%), which may be used for other purposes, and transmits the remainder through waveguide 28

to the IOC 12. The waveguide 28 is an optical fiber which is single-moded at the source wavelength. The IOC, which also operates single-moded at 0.8 microns, is formed using a two step proton exchange technique
5 described in a commonly owned, copending application entitled Single-Polarization, Integrated Optical Components for Optical Gyroscopes, S/N 329,121, filed March 27, 1989 by Suchoski et al.

The IOC includes a single polarization filter 30
10 and a single spatial mode filter 32 formed in a waveguide section 33. The polarization filter extinction ratio is on the order of 60 dB. The waveguide 33 is the "common path" for propagating the source optical signal to the sensing coil 20 and for guiding return
15 propagation of the interference signal from the coil to the detection circuitry 16. The spatial-mode filter ensures that only selected spatial mode light enters the sensing coil and only selected mode optical power is coupled back from the loop to the detector.

20 The filtered optical signal approaching the sensing loop is presented to a beam splitter / combiner 34, e.g. either a Y-junction or a 3 dB directional coupler, which divides the source optical signal into two equal intensity optical signals presented on
25 waveguide sections 35, 36. In the best mode embodiment a phase ("dither") modulator 37 and a serrodyne modulator 38 (each described hereinafter) are connected to the guide sections 35, 36, respectively. The modulated optical signals at IOC connections 39, 40 are presented
30 through the depolarizer 23 and mode conversion means 24 to the opposite ends 42, 44 of the sensing loop.

After circulating through the sensing loop, light returns toward the source, being combined at splitter / combiner 34 into an interference signal which then
35 proceeds back along the common path guide 33, through

the mode filter and polarizer, to tap 18 which extracts a portion (e.g., 50%) of the signal and couples it through path 44 to detection circuitry 16, the remainder of this signal being guided toward the source and effectively lost. The path 46 may be an optical fiber which may be single moded at the source wavelength. The detection circuitry may include a known PIN-diode transimpedance amplifier detection system.

In the best mode embodiment, a closed loop serrodyne modulation technique is used to measure the Sagnac phase difference. This makes the measurement insensitive to intensity variations resulting from fluctuations of the light source or from multi-mode transmission of the light through the sensing loop. The serrodyne modulator 38 applies a linear ramped phase modulation to each of the counter circulating light beams. If the ramp peak amplitude is 2π radians and the flyback is essentially instantaneous, the serrodyne modulation, acting on the two signals at different times due to optical delay in the coil, adds an effectively constant bias to the differential phase. The bias can be controlled by a servo loop within the control circuitry 22 to continuously oppose, and null, the Sagnac phase difference. The serrodyne frequency then constitutes a gyro output proportional to the loop rotation rate.

The phase modulation of the beams is provided by the dither modulator 37, which causes the interference signal amplitude to dither. This allows for AC detection of the differential phase. The dither amplitude is at a maximum when the modulation frequency is equal to the eigenfrequency of the fiber sensing coil. This modulation frequency also offers other known advantages in reducing certain types of FOG measurement errors.

In the best mode embodiment the sensing coil fiber is a 1.3 micron, non-polarization preserving, single mode fiber. The fiber was selected because of its commercial availability and low cost. The cost per meter is approximately one-fifth that of non-polarization preserving single mode fiber designed to operate at 0.8 microns, and less than 1/20th the cost per meter of 1.3 micron polarization preserving (high birefringence) fiber.

Multiple modes (typically two to five) may exist in the 1.3 micron fiber when operating with 0.8 micron optical signals. In this case it is conceivable that substantially all of the selected mode optical power might become converted to an undesired mode during propagation through the loop, leaving no selected mode light for return to the detector. To prevent this it is necessary to functionally incorporate mode converter (or "mode-scrambler") means at one or both ends of the loop. This ensures that some light from any existing mode will couple into the desired mode before leaving the loop. The light so coupled will pass through the selected-mode filter 32 to the detector 16.

The mode conversion feature may be accomplished by control of the sensing coil geometry, i.e. by controlling the coil diameter and the fiber winding technique. The range of acceptable diameter values is not critical. Small diameter values tend to be associated with high winding stresses and fiber distortions which enhance the spatial mode cross coupling (scrambling). At the same time, a small diameter increases the attenuation of high order modes and so may ultimately lead to single mode transmission through the coil, obviating the need for scrambling. However too small a diameter (e.g., less than about 2 cm) may also

//

unacceptably increase the attenuation for even the desired mode.

Subject to physical packaging limits, a large diameter coil provides greater FOG sensitivity. However, a large diameter (e.g., greater than 8 cm), combined with a smooth winding technique with controlled fiber crossovers, may yield little or no spatial mode selection or conversion. In this case it may be necessary to incorporate a separate, discrete mode scrambling means comprising any one of the known scrambler configurations, such as a serpentine series of small random fiber bends at one end of the fiber coil.

In laboratory experiments using a 16 cm diameter 180 meter long random-wound coil of conventional single-mode 1.3 micron communications fiber it was found unnecessary to include a separate mode scrambler, suggesting that fiber crossovers in such a coil may provide adequate mode mixing.

The use of non-polarization-preserving single mode fiber in the best mode embodiment also increases the chance of environmentally sensitive polarization mode coupling into undesired polarizations. To prevent the possibility that all light might couple out of the desired polarization (polarization fading), the depolarizing means may be included at one or both ends of the sensing loop. When a low coherence light source is used, a depolarizer for this purpose may, for example, comprise a short length of high birefringence (polarization preserving) fiber connected with properly orientated polarization axes relative to the IOC, using methods known to those skilled in the art. The anti-fading action of the depolarizer is analogous to that of the mode scrambler described above. It ensures that some light will always return to the detector in the

12

desired polarization. However, it also ensures that a similar amount of light will return toward the detector in the undesired polarization, so the extinction ratio of the polarizer needed to block this light must be
5 higher than if substantially all returning light were in the desired polarization state.

The extinction ratio of the IOC polarization filter 30 is on the order of 60 dB. It is not now known whether larger extinction coefficients can be
10 obtained by increasing the length of the IOC waveguide 33, or whether there is a performance limit at 60 dB beyond which a single-substrate IOC polarizing filter fails to improve with length. Such a limit might result from re-entry of previously rejected light into
15 the primary waveguide.

Tests have shown, however, that polarization related errors in a Sagnac interferometer employing a proton exchanged IOC based on a lithium niobate substrate and having an effective extinction coefficient
20 of about 60 dB can be substantially reduced by inserting a supplemental polarizer just ahead of the input to the IO circuit. Polarization-related errors in the output of our experimental gyro were typically less than 10 degrees/hour equivalent rotation rate when only
25 the IOC polarizer was used. However, when a commercial prism type polarizer specified to have a 60 dB extinction coefficient was inserted ahead of the IO polarizer, the errors decreased to less than 1 degree/ hour.

Depending on the performance accuracy required for
30 a particular application, it may be preferable to include the supplemental polarizer 25, shown in series with the IOC 12 in Fig. 1. This configuration effectively separates the two polarizers and achieves enhanced polarization extinction. The supplemental
35 polarizer need not be of the prism type. It may be an

additional, separate-substrate IOC polarizing element, or any other known type of fiber polarizer.

Test results have shown that the present rotation sensor exhibits output noise and drift no larger than a few degrees/hour, indicating that gyros constructed in accordance with the above-described ideas may be useful in a variety of applications where cost is important and moderate performance levels are required.

It should be understood that the source and sensing fiber wavelengths need not be limited to 0.8 and 1.3 microns. Any relatively short wavelength light source may be used in combination with any relatively long wavelength sensing fiber. For example, the source wavelength may range from 750 to 900 nanometers and the design wavelength of the fiber may range from 1200 to 1600 nanometers.

Similarly, although the invention has been shown and described with respect to a best mode embodiment thereof, it should be understood by those skilled in the art that the foregoing and various other changes, omissions, and additions in the form and detail thereof, may be made therein without departing from the spirit and scope of this invention.

We claim:

Claims

1. An interferometric rotation sensor, comprising:
 - optical signal source means, for providing a source optical signal;
 - 5 optical fiber sensing loop means, for providing, in the presence of loop rotation, a Sagnac phase difference between two sensing loop optical signals propagating in counter circulating paths therethrough;
 - integrated optic circuit (IOC) means, having a
 - 10 substrate with a waveguide array formed thereon, said waveguide array including a bi-directional common path section responsive to said source optical signal, said common path having a single polarization mode filter and a single spatial mode filter formed therein to pass
 - 15 select mode optical signals having a desired spatial mode and a desired polarization mode, said waveguide means further including beam splitter / combiner means for splitting said select mode optical signal received from said common path into said two sensing loop
 - 20 optical signals for counter propagation through said sensing loop means, and for combining sensing loop optical signals received from said loop into a common interference signal for return through said common path, said interference signal amplitude being
 - 25 dependent on the magnitude of said Sagnac phase difference;
 - detector means, for sensing the amplitude of said interference signal; and
 - means for coupling said source optical signal to
 - 30 said IOC means and for coupling said interference signal from said IOC means to said detector means;
 - as characterized by:
 - said optical signal source means comprising a laser diode having a source optical signal wavelength;

35 said sensing loop fiber comprising an optical
fiber which is designed for single mode operation at a
wavelength which is longer than said source wavelength,
and wherein said sensing loop fiber embodies a signal
mode conversion characteristic therein, to prevent
40 sensing loop cross coupling of all optical power from
the select spatial mode to undesired spatial modes.

2. The rotation sensor of claim 1, wherein said
sensing loop comprises a fiber coil configuration
having a fiber winding geometry which causes said
sensing loop to display inherent mode conversion
5 characteristics.

3. The rotation sensor of claim 1, wherein said
sensing loop coil configuration comprises a discrete
mode conversion element positioned at one end of said
sensing loop coil.

4. The rotation sensor of claim 3, wherein said
discrete mode conversion element comprises a serpentine
segment of fiber bends positioned at one end of the
sensing loop coil.

5. The rotation sensor of claim 1, wherein said
source wavelength is on the order of 0.8 microns and
the sensing loop optical fiber is designed to operate
at a wavelength on the order of 1.3 microns.

6. The rotation sensor of claim 1, further comprising
depolarization means, at least one, located between the
sensing loop coil and said IOC combiner / splitter, to
prevent sensing loop cross coupling of all optical
5 power from the desired polarization mode to an
undesired mode.

16

7. The rotation sensor of claim 6, wherein said depolarization means comprises a length of single mode fiber having high birefringence.

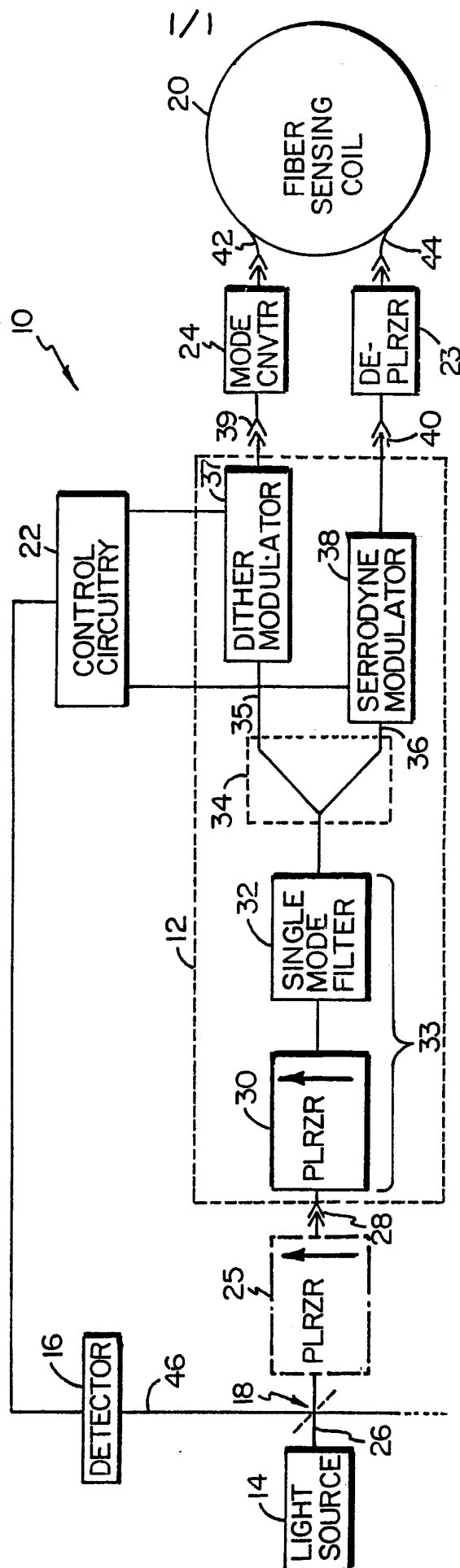
8. The rotation sensor of claim 1, further comprising:

serrodyne modulation means, for applying a linear ramped phase modulation to said sensing loop optical signals, to provide a phase bias in opposition to the Sagnac phase difference; and

control circuitry, for continuously changing the value of the serrodyne modulation frequency in dependence on said interference signal amplitude so as to cause the phase bias to continuously null the Sagnac phase difference magnitude, whereby the nulling value of the serrodyne modulation frequency is proportional to said sensing loop rotation rate.

9. The rotation sensor of claim 6, further comprising discrete polarizer means, positioned between said means for coupling and said IOC common path waveguide segment, to increase the extinction ratio of said IOC single polarization filter.

10. The rotation sensor of claim 5, wherein said source wavelength may range from 750 to 900 nanometers and the design wavelength of the sensing loop fiber may range from 1200 to 1600 nanometers.

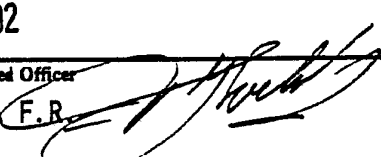


SUBSTITUTE SHEET

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 91/09459

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ⁶		
According to International Patent Classification (IPC) or to both National Classification and IPC		
Int.Cl. 5 G01C19/72		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
Int.Cl. 5	G01C	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹		
Category ¹⁰	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
Y A	US,A,4 265 541 (LECLERC ET AL.) 5 May 1981 see column 5, line 64 - column 6, line 19; figures 2,7 ---	1-3 5,10
Y	US,A,4 944 591 (MCMICHAEL) 31 July 1990 see column 3, line 49 - column 4, line 10; figure 2 ---	1,2
Y	ELECTRONICS LETTERS. vol. 16, no. 25, 4 December 1980, ENAGE GB pages 941 - 942; HOTATE ET AL.: 'rotation detection by optical fibre laser gyro with easily introduced phase-difference bias' *page 941, paragraph "experiment"* --- -/-	1,3
<p>¹⁰ Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
01 APRIL 1992	14. 04. 92	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	HOEKSTRA F.R. 	

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claim No.
A	EP,A,0 260 885 (LITTON SYSTEMS INC.) 23 March 1988 see page 22, right column, line 30 - line 37; figure 1 ---	6,7
A	IEE PROCEEDINGS J. OPTOELECTRONICS vol. 132, no. 5, October 1985, STEVENAGE GB pages 259 - 264; C.J.KAY: 'serrodyne modulator in a fibre-optic gyroscope' see the whole document ---	8

**ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.**

US 9109459
SA 55795

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report.
The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information. 01/04/92

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A-4265541	05-05-81	FR-A- 2409518 GB-A, B 2009396	15-06-79 13-06-79
US-A-4944591	31-07-90	None	
EP-A-0260885	23-03-88	JP-A- 63085313 US-A- 4997282	15-04-88 05-03-91