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(54) **COMPOSITE LAMINAE HAVING THERMAL MANAGEMENT FEATURES AND THERMAL MANAGEMENT APPARATUSES COMPRISING THE SAME**

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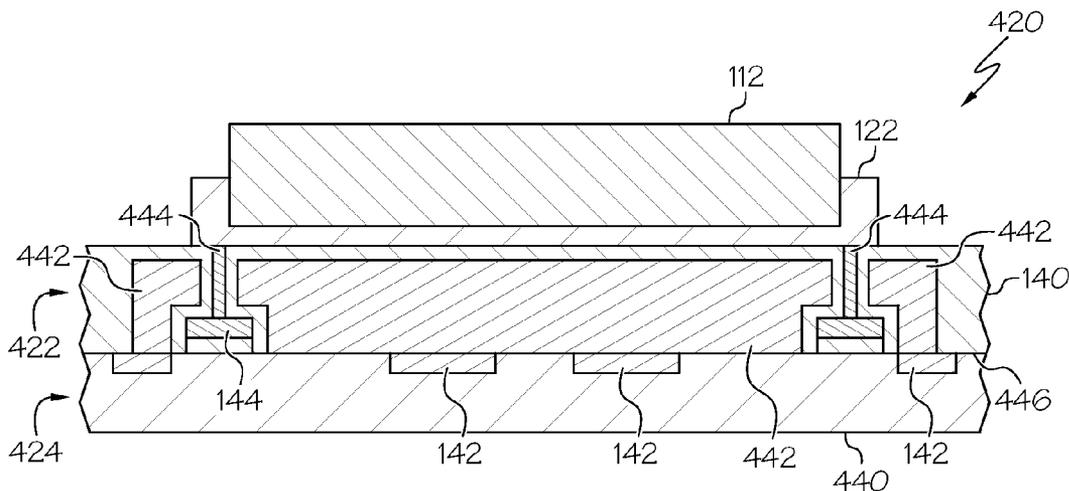
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(60) Provisional application No. 61/816,917, filed on Apr. 29, 2013.

(57) **ABSTRACT**

Heat transfer management apparatuses according to the present disclosure includes a composite lamina having an insulator substrate and a thermal conductor at least partially embedded in the insulator substrate, a temperature-sensitive component coupled to the composite lamina, and a temperature-insensitive component coupled to the composite lamina and positioned distally from the temperature-sensitive component. The temperature-insensitive component produces heat during operation. The thermal conductor and the insulator substrate are arranged into a targeted heat transfer region proximate to the temperature-sensitive component and a bulk region proximate to the temperature-insensitive component. The targeted heat transfer region and the bulk region are in thermal continuity with one another.



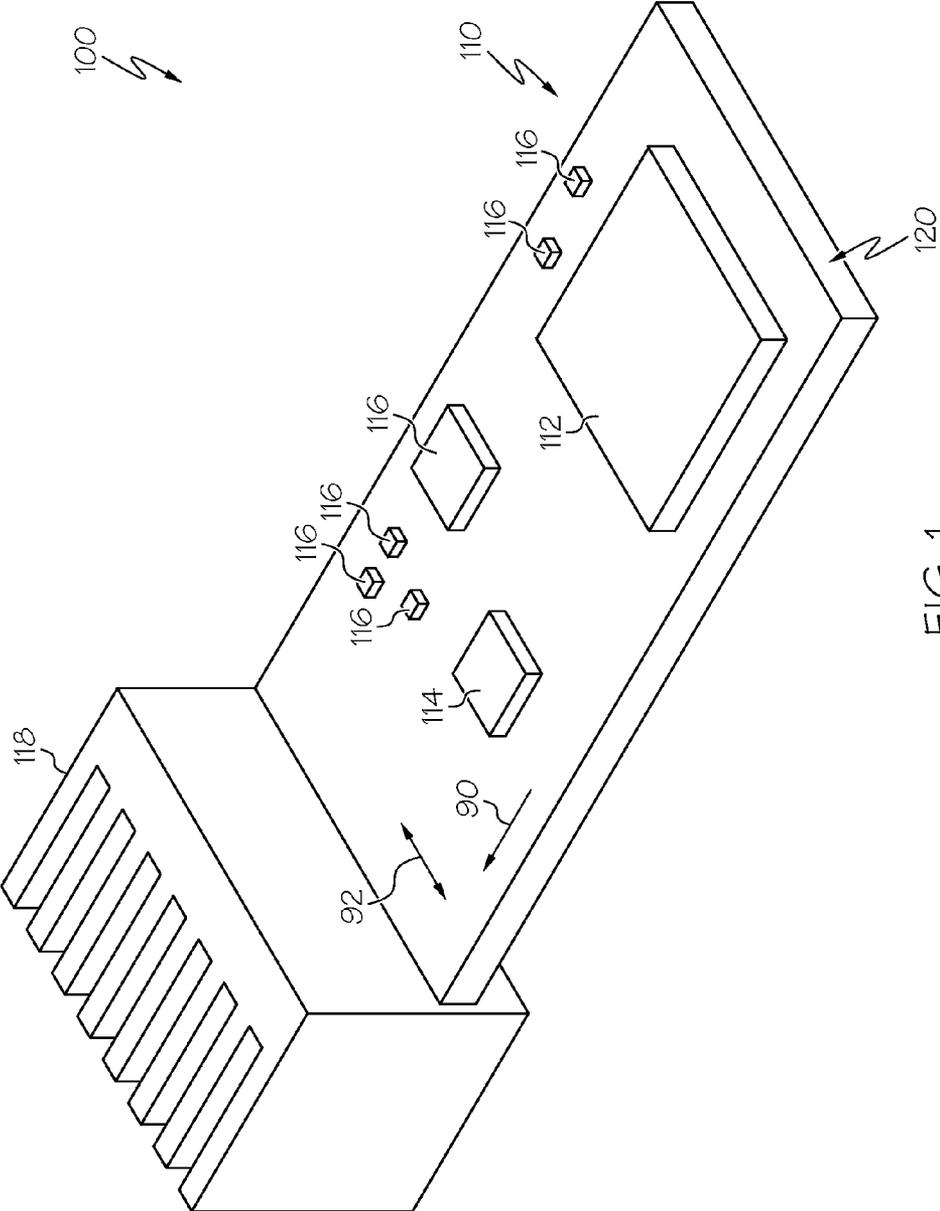
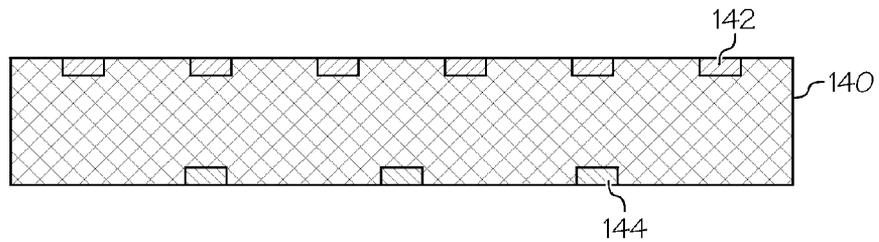
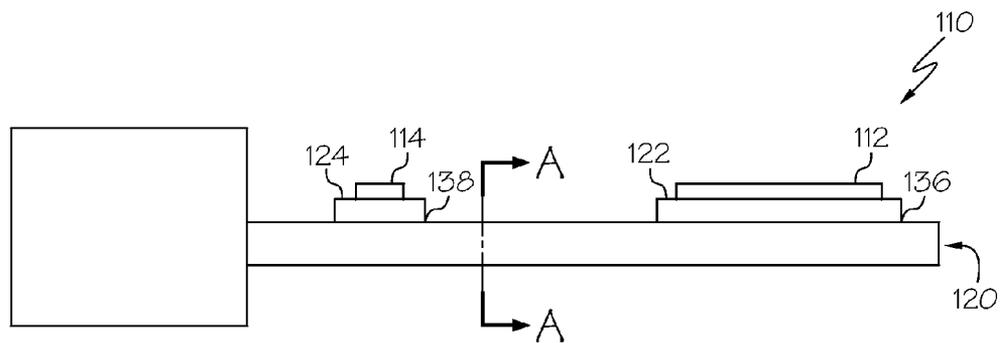
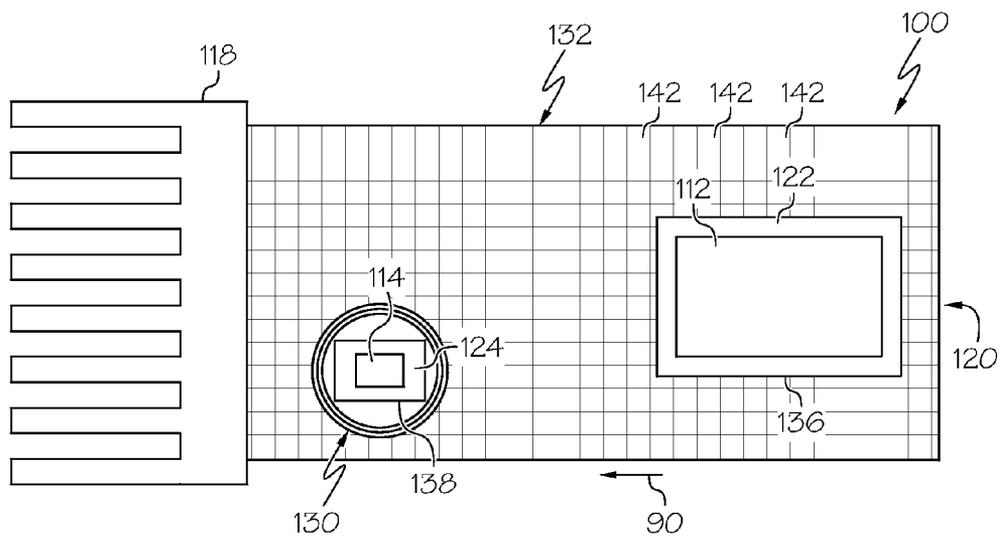


FIG. 1



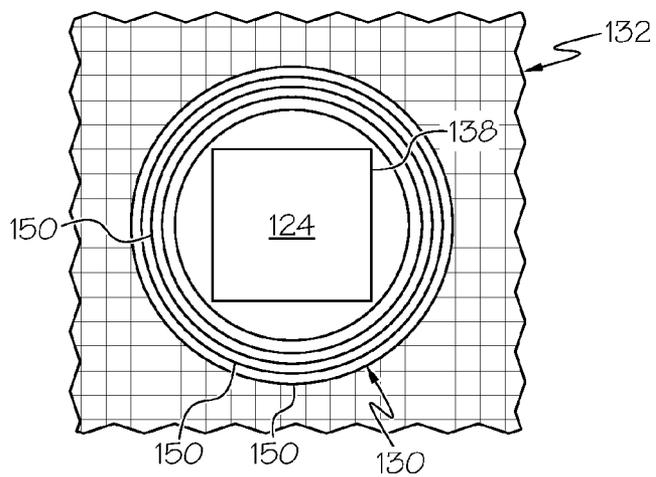


FIG. 5

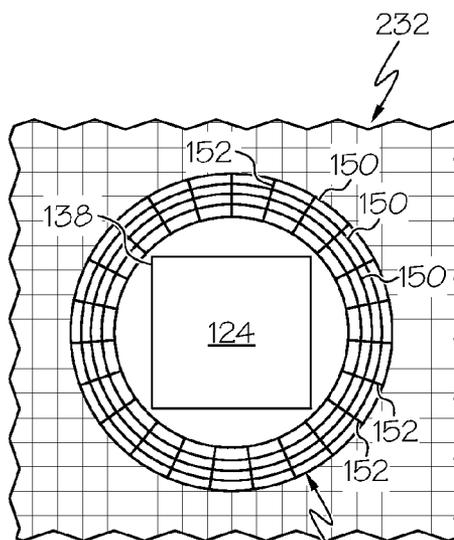


FIG. 6

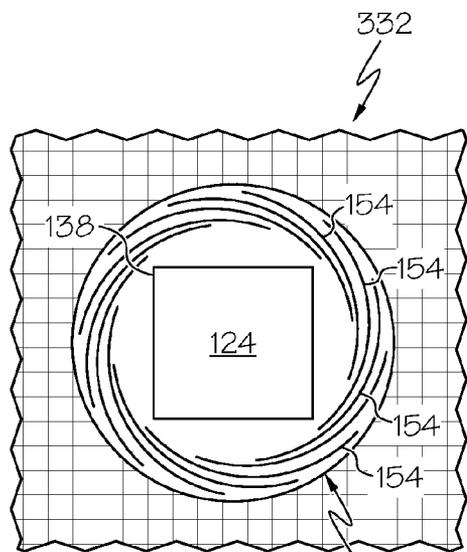
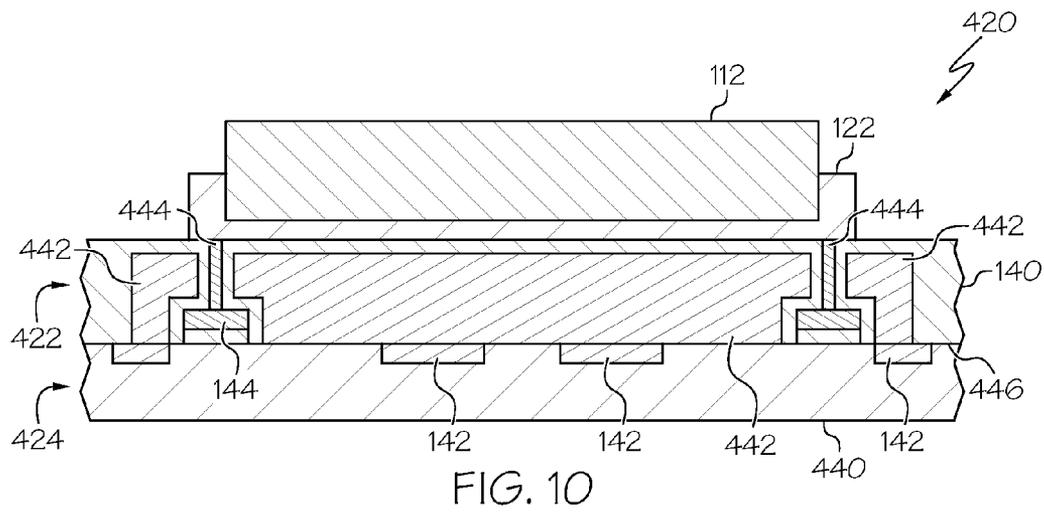
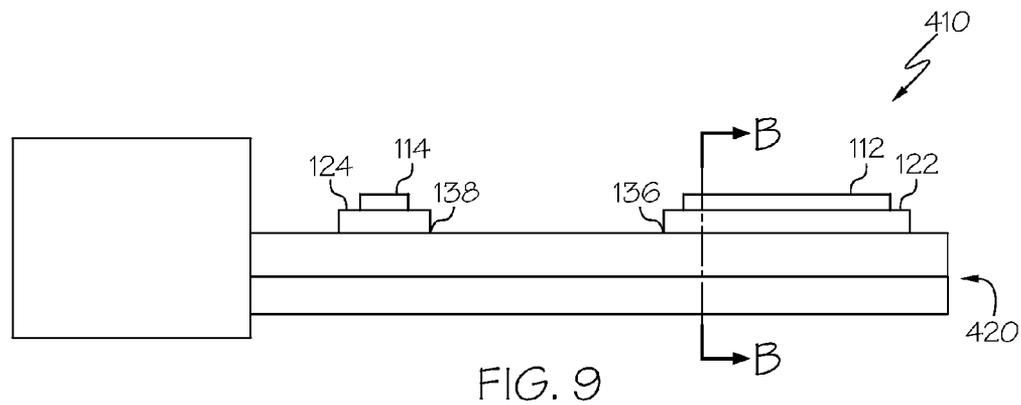
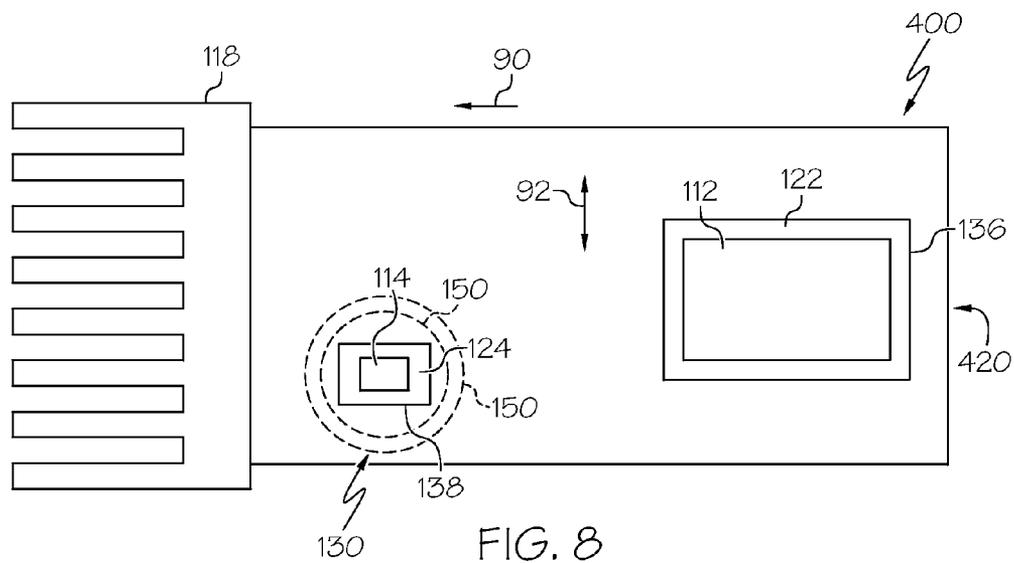


FIG. 7



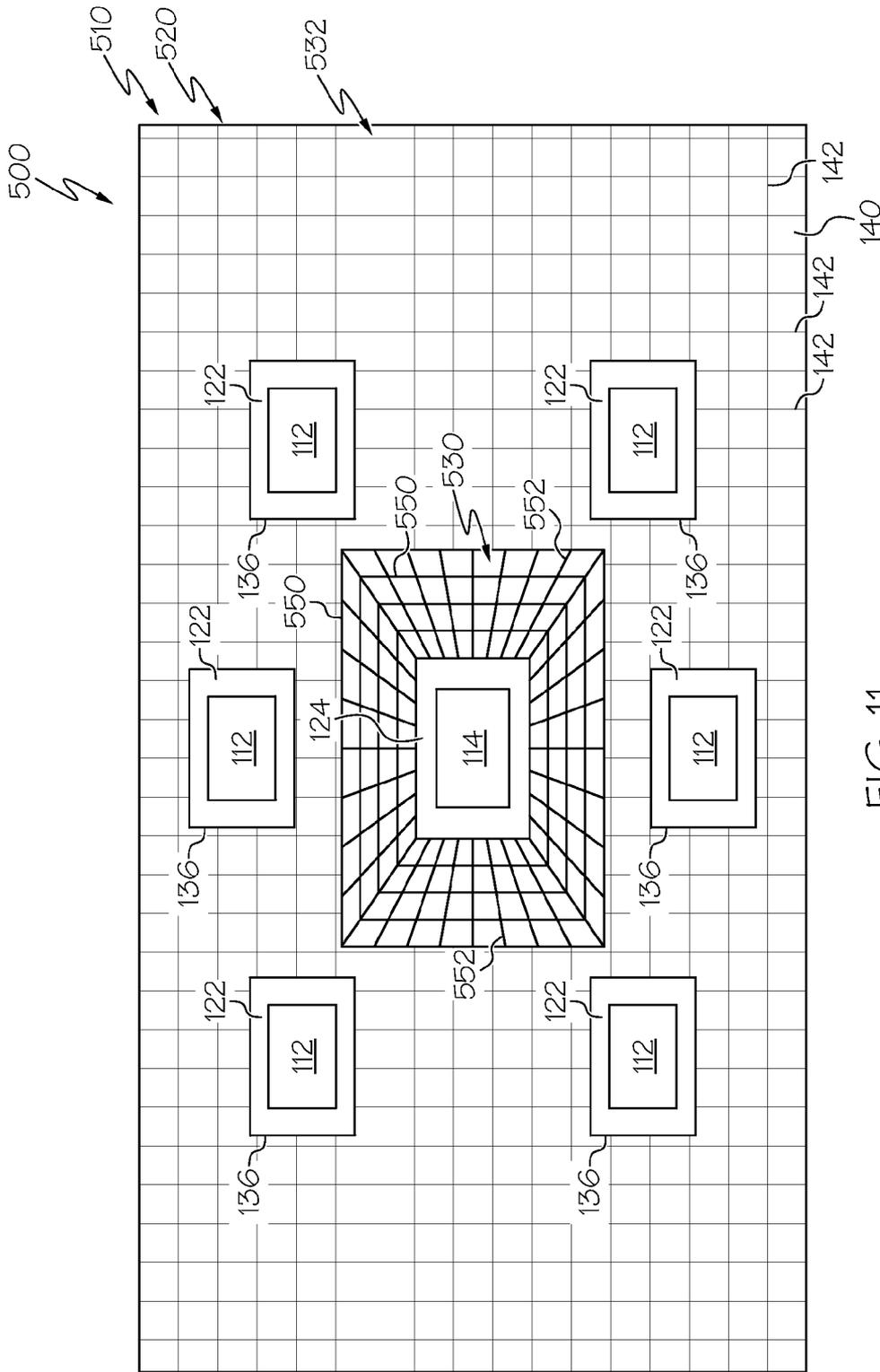


FIG. 11

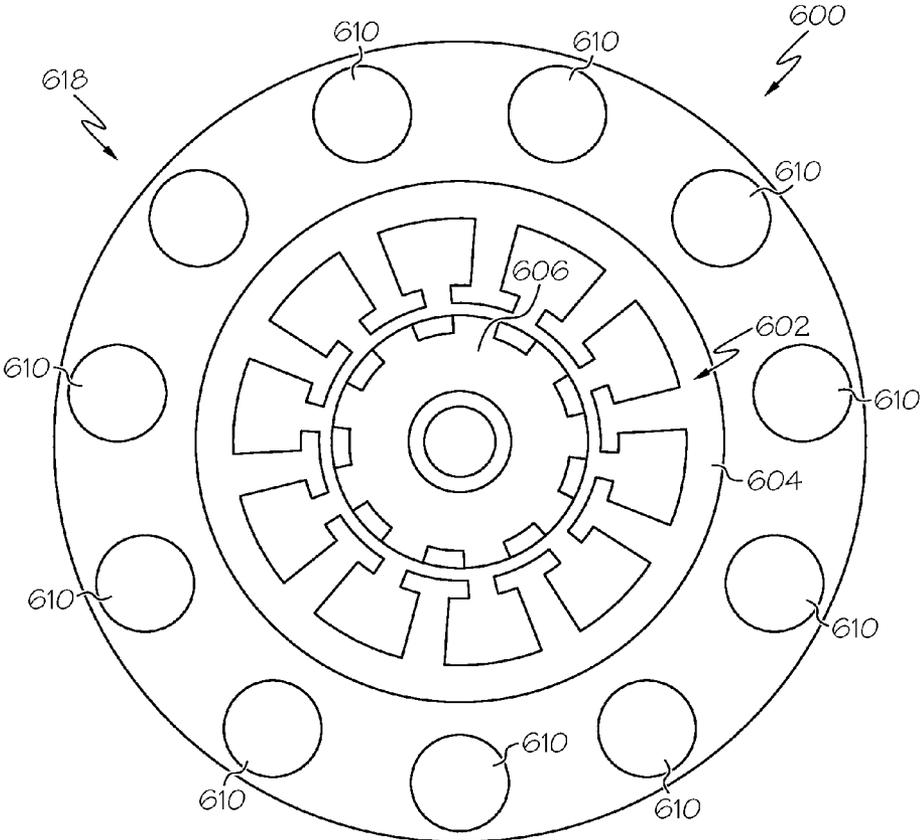


FIG. 12

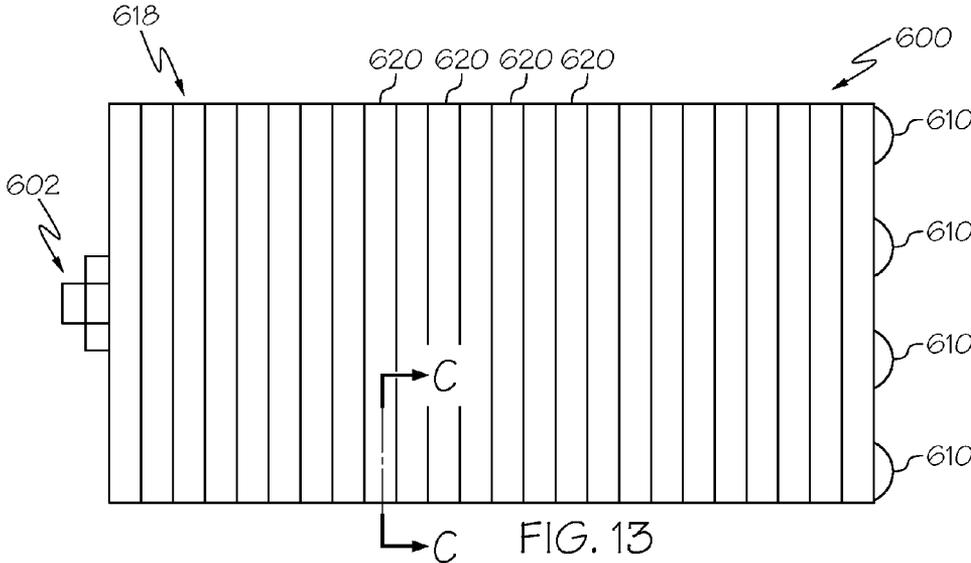
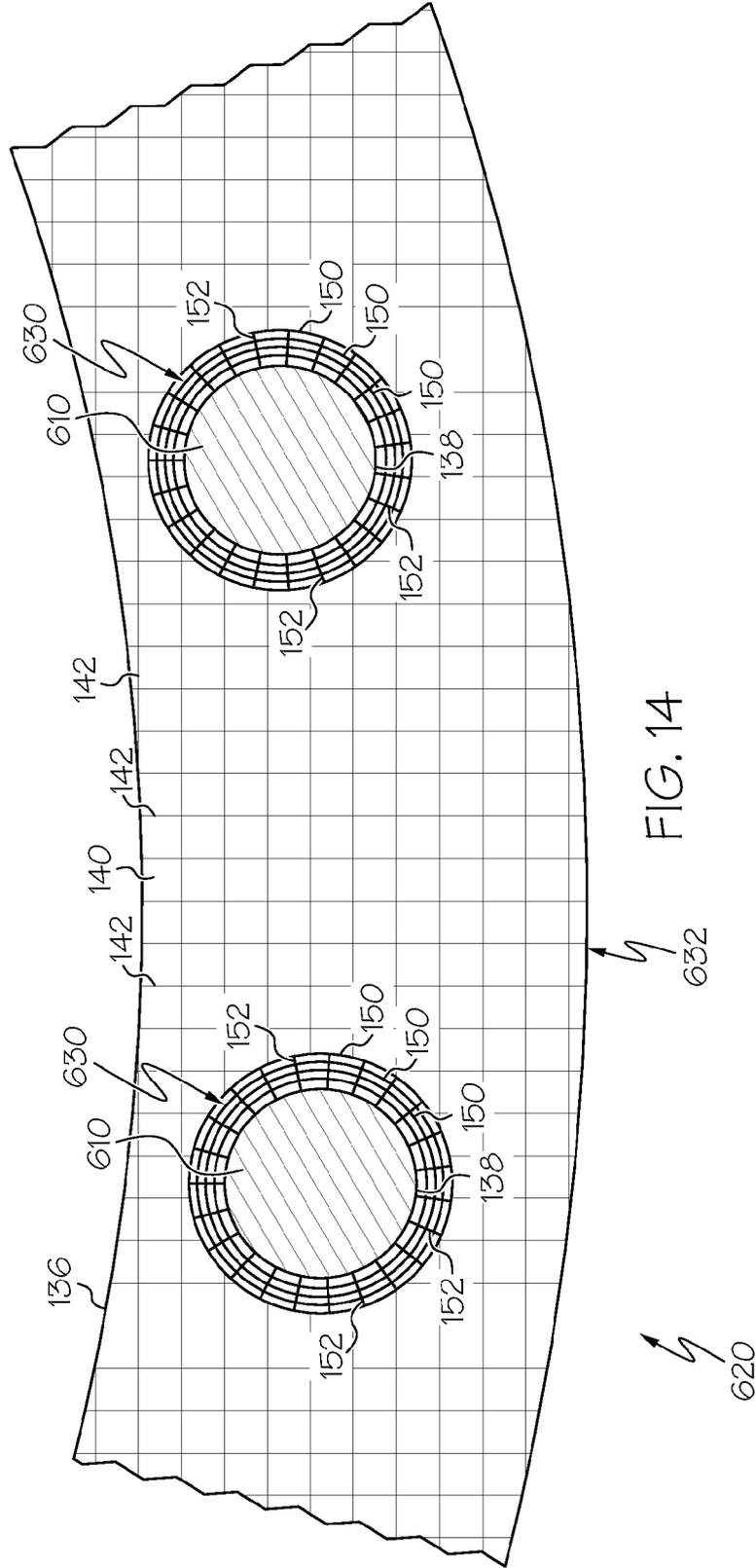


FIG. 13



COMPOSITE LAMINAE HAVING THERMAL MANAGEMENT FEATURES AND THERMAL MANAGEMENT APPARATUSES COMPRISING THE SAME

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the benefit of U.S. Provisional Application Ser. No. 61/816,917, filed Apr. 29, 2013, the entire disclosure of which is hereby incorporated by reference.

TECHNICAL FIELD

[0002] The present specification generally relates to thermal management apparatuses and, more particularly, thermal management apparatuses incorporating a composite lamina having thermal management features.

BACKGROUND

[0003] In general, electrical components generate heat as a byproduct of the operation of the electrical components. However, an increase in generation of heat may be detrimental to performance and operation of electrical components. The heat generated by the operation of the electrical components, therefore, is rejected into the surrounding environment. In some applications, heat-sensitive electrical components may be located at positions in which heat from other electrical components adversely affects operation of the heat-sensitive electrical components.

[0004] Accordingly, thermal management apparatuses that affect the flow of thermal energy may be desired.

SUMMARY

[0005] In one embodiment, a heat transfer management apparatus includes a composite lamina having an insulator substrate and a thermal conductor at least partially embedded in the insulator substrate, a temperature-sensitive component coupled to the composite lamina, and a temperature-insensitive component coupled to the composite lamina and positioned distally from the temperature-sensitive component. The temperature-insensitive component produces heat during operation. The thermal conductor and the insulator substrate are arranged into a targeted heat transfer region proximate to the temperature-sensitive component and a bulk region proximate to the temperature-insensitive component. The targeted heat transfer region and the bulk region are in thermal continuity with one another.

[0006] In another embodiment, a composite lamina for directing heat transfer includes an insulator substrate, a thermal conductor at least partially embedded in the insulator substrate, a temperature-sensitive component mounting region, and a temperature-insensitive component mounting region. The thermal conductor and the insulator substrate are arranged into a targeted heat transfer region proximate to the temperature-sensitive component mounting region and a bulk region proximate to the temperature-insensitive component mounting region. The targeted heat transfer region and the bulk region are in thermal continuity with one another.

[0007] These and additional features provided by the embodiments described herein will be more fully understood in view of the following detailed description, in conjunction with the drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0008] The embodiments set forth in the drawings are illustrative and exemplary in nature and not intended to limit the subject matter defined by the claims. The following detailed description of the illustrative embodiments can be understood when read in conjunction with the following drawings, where like structure is indicated with like reference numerals and in which:

[0009] FIG. 1 schematically depicts a side perspective view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0010] FIG. 2 schematically depicts a top view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0011] FIG. 3 schematically depicts a side view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0012] FIG. 4 schematically depicts a front sectional view of a heat transfer management apparatus having a composite lamina shown along line A-A of FIG. 3 according to one or more embodiments shown or described herein;

[0013] FIG. 5 schematically depicts a detailed top view of a composite laminate assembly according to one or more embodiments shown or described herein;

[0014] FIG. 6 schematically depicts a detailed top view of a composite laminate assembly according to one or more embodiments shown or described herein;

[0015] FIG. 7 schematically depicts a detailed top view of a composite laminate assembly according to one or more embodiments shown or described herein;

[0016] FIG. 8 schematically depicts a top view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0017] FIG. 9 schematically depicts a side view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0018] FIG. 10 schematically depicts a front sectional view of a heat transfer management apparatus having a composite lamina shown along line B-B of FIG. 9 according to one or more embodiments shown or described herein;

[0019] FIG. 11 schematically depicts a top view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0020] FIG. 12 schematically depicts a front view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein;

[0021] FIG. 13 schematically depicts a side view of a heat transfer management apparatus having a composite lamina according to one or more embodiments shown or described herein; and

[0022] FIG. 14 schematically depicts a detailed front sectional view of a heat transfer management apparatus having a composite lamina shown along line C-C of FIG. 13 according to one or more embodiments shown or described herein.

DETAILED DESCRIPTION

[0023] Reference will now be made in detail to embodiments of heat transfer management apparatuses that include structural features that direct the flow of heat along the heat transfer management apparatuses. The heat transfer management apparatuses include a composite lamina having an insulator substrate and a thermal conductor at least partially embedded in the insulator substrate. The thermal conductor is arranged relative to electronic components positioned on the composite lamina. The thermal conductor directs the thermal energy along the composite lamina in a direction and/or at a rate that differs from the direction and/or rate of the heat flux along an isotropic substrate. By providing a composite lamina in an anisotropic arrangement, thermal energy may be directed in a direction and/or at a rate that improves operation of the electrical components coupled to the composite lamina. Various embodiments of the heat transfer management apparatuses will be described in more detail herein.

[0024] Referring now to FIG. 1, one embodiment of a heat transfer management apparatus 100 is depicted. In this embodiment, the heat transfer management apparatus 100 is a circuit board assembly 110 that includes a composite lamina 120, a temperature-insensitive component 112 coupled to the composite lamina 120, and a temperature-sensitive component 114 coupled to the composite lamina 120. In some embodiments, the composite lamina 120 may be a printed wiring board.

[0025] Embodiments according to the present disclosure may also include a plurality of electrical components 116 that are coupled to the composite lamina 120. The heat transfer management apparatus 100 may also include a heat sink 118 coupled to the composite lamina 120 that is adapted to reject thermal energy into the surrounding environment.

[0026] In the embodiment depicted in FIG. 1, the temperature-insensitive component 112 may be a power electronics device that produces heat as a byproduct of its operation. The temperature-insensitive component 112 may be a variety of electronic devices that include integrated circuits, for example, computer processing units, graphical processing units, chipsets, and the like. In some embodiments, the temperature-insensitive component 112 may be a power semiconductor device such as those utilized in power inverters, voltage rectifiers, voltage regulators, and the like. Exemplary power semiconductor devices include, but are not limited to, power insulated-gate bi-polar transistors, metal-oxide field-effect transistors, and the like. In another embodiment, the temperature-insensitive component 112 may include an electric motor or generator. In operation, the temperature-insensitive component 112 generally produces heat as a waste byproduct of the designed operative function of the temperature-insensitive component 112. The heat produced by the temperature-insensitive component 112 in the heat transfer management apparatus is generally undesired, as electrical components are conventionally susceptible to temperature malfunction or permanent failure if an over-temperature condition is realized. Nevertheless, the temperature-insensitive component 112 will continue to operate throughout a wide temperature band.

[0027] Additionally, in the embodiment depicted in FIG. 1, the temperature-sensitive component 114 may be selected from a variety of a temperature-sensitive electronic devices including, for example planar coupler, an inductor/transformer, a high-Q resonator, a detector, a current sensing resistor, a crystal oscillator, an aligned optical component, or a

human interface control button. Operation of the temperature-sensitive component 114 may be adversely affected by thermal energy that is generated by the temperature-insensitive component 112. Alternatively, in other embodiments, the temperature-sensitive component 114 may be a temperature-sensitive electronic device that operates with increased efficiency with increased thermal energy, for example a thermo-electric generator or a piezo-electric fan. In yet other embodiments, the temperature-sensitive component 114 may be a thermo-mechanical device that operates with increased efficiency with increased temperatures, for example a multi-phase heat pipe, a convective heat sink, and the like. Increased thermal energy directed to such temperature-sensitive components 114 may increase performance of the temperature-sensitive component 114. Accordingly, to manage the temperature of temperature-sensitive components 114 coupled to the composite lamina 120, the composite lamina 120 includes a plurality of heat transfer management features that modify the direction and/or intensity of the heat flux that flows along the composite lamina 120.

[0028] Referring now to FIGS. 2-4, the embodiment of the heat transfer management apparatus 100 depicted includes a composite lamina 120 that includes an insulator substrate 140, a thermal conductor 142 that is at least partially embedded in the insulator substrate 140, and an electrical conductor 144 that is at least partially embedded in the insulator substrate 140. The composite lamina 120 also includes at least one electronic component attachment module 122, 124, each of which are coupled to the composite lamina 120. The electronic component attachment modules 122, 124 provide an electrical connection between the respective temperature-insensitive or temperature-sensitive component 112, 114 and the electrical conductor 144 that is incorporated into the composite lamina 120. A plurality of electronic leads may extend through the insulator substrate 140 from the electronic component attachment modules 122, 124 to the electrical conductor 144 in a series of vias, as conventionally known. The electronic component attachment modules 122, 124 may secure the respective temperature-insensitive or temperature-sensitive component 112, 114 with a snap-in fit or by attachment through a locking retention collar or a thermal pad (not shown). In other embodiments, the temperature-insensitive and/or temperature-sensitive components 112, 114 may be coupled to the composite lamina 120 and placed into electrical continuity with the electrical conductor 144, for example by soldering or welding.

[0029] In the embodiment depicted in FIGS. 2-4, the composite lamina 120 includes the thermal conductor 142 and the electrical conductor 144 that are positioned to be at least partially embedded within the insulator substrate 140. The thermal conductor 142 may be selected from any of a variety of materials having high thermal conduction properties, including, for example, copper, silver, gold, and alloys thereof. The thermal conductor 142 may have a coefficient of thermal conductivity, k_c , that is greater than the coefficient of thermal conductivity of the insulating substrate, k_i , including where k_c is at least an order of magnitude greater than k_i . Similarly, the electrical conductor 144 may be selected from any of a variety of materials having high electronic conduction properties, including, for example, copper, silver, gold, and alloys thereof. The insulator substrate 140 may be selected from any of a variety of materials having low electronic conductivity, including, for example, plastics such as polypropylene, polyester, nylon, epoxy and the like, which

may be combined with carbon or glass reinforcement. In one embodiment, the insulator substrate **140** may be made from FR-4, which is a glass-reinforced epoxy. The insulator substrate **140** has a coefficient of thermal conductivity, k_c , that is less than the coefficient of thermal conductivity of the thermal conductors, k_c .

[0030] As depicted in FIGS. 2-4, the embodiment of the composite lamina **120** includes bulk region **132** having a lattice of inter-connected strands of thermal conductor **142** that is at least partially embedded along one side of the insulator substrate **140**. The lattice of the thermal conductor **142** in the bulk region **132** is generally arranged in an orientation that encourages heat generated at the temperature-insensitive component **112** to flow towards the heat sink **118**. In the depicted embodiment, the lattice includes a plurality of square-shaped cells that are defined by the thermal conductor **142**. It should be understood that various configurations of such lattices, including having various polygonal shapes, widths, depths, and lengths, may be incorporated into the composite lamina **120** without departing from the scope of the present disclosure. In the depicted embodiment, the lattice of the thermal conductor **142** includes strands that extend in the principal direction **90** from the temperature-insensitive component **112** towards the heat sink **118** and in a cross-direction **92** transverse to the principal direction **90** from the temperature-insensitive component **112** towards the heat sink **118**. By directing the thermal energy in the cross-direction **92**, an increased proportion of the thermal conductor **142** may be used to direct thermal energy to the heat sink **118**, which may increase the efficacy of the composite lamina **120** of rejecting heat from the temperature-insensitive component **112** to the heat sink **118** and into the surrounding environment.

[0031] The composite lamina **120** also includes a targeted heat transfer region **130** that is positioned proximate to the temperature-sensitive component **114**. The targeted heat transfer region **130** includes an arrangement of thermal conductor **142** that surrounds the temperature-sensitive component **114**. The thermal conductor **142** of the targeted heat transfer region **130** may be in thermal continuity with the thermal conductor **142** of the bulk region **132**, so that heat flux flows readily along the thermal conductor **142** between the bulk region **132** and the targeted heat transfer region **130**. Thermal continuity between the thermal conductor **142** of the bulk region **132** and the targeted heat transfer region **130** may be verified by evaluating electrical continuity between the bulk region **132** and the targeted heat transfer region **130** for thermal conductors **142** that are also electrically conductive. In these embodiments, the bulk region **132** and the targeted heat transfer region **130** may steer heat flux away from the temperature sensitive component **114**. The targeted heat transfer region **130** modifies the thermal conductivity and/or thermal capacitance of the composite lamina **120** at positions proximate to the targeted heat transfer region **130**, while generally maintaining the conductive heat transfer at positions located distally from the targeted heat transfer region **130**. By modifying the thermal conductivity of the composite lamina **120**, steady state heat transfer along the composite lamina **120** can be controlled. Similarly, by modifying the thermal capacitance of the composite lamina **120**, transient thermal response of the composite lamina **120** to variations in heat flux can be controlled.

[0032] Various embodiments of the targeted heat transfer region **130**, **230**, **330** are depicted in greater detail in FIGS. 5-7. While the targeted heat transfer regions **130**, **230**, **330**

depicted herein are generally circular in shape, it should be understood that embodiments of the targeted heat transfer regions **130**, **230**, **330** according to the present disclosure are not intended to be limited by geometric shape. Accordingly, various embodiments of the targeted heat transfer regions **130**, **230**, **330** may exhibit a variety of shapes and configurations. In the embodiment depicted in FIG. 5, the targeted heat transfer region **130** includes thermal management features that are defined by a composite structure of the thermal conductor **142** and the insulator substrate **140** where the thermal conductor **142** is arranged in concentric rings **150** that encapsulate a temperature-sensitive component mounting region **138**, here the second electronic component attachment module **124**. The rings **150** of the targeted heat transfer region **130** are free from intersection with one another, and are separated from one another by insulator substrate **140**. The outer-most ring **150** may be in thermal continuity with the lattice of thermal conductor **142** positioned along the insulator substrate **140** in the bulk region **132**.

[0033] The rings **150** of the targeted heat transfer region **130** direct thermal energy along the rings **150** while decreasing the heat flux through the targeted heat transfer region **130**. Accordingly, the targeted heat transfer region **130** may reduce the amount of thermal energy that flows into the temperature-sensitive component **114**. As such, the targeted heat transfer region **130** may mask the temperature-sensitive component **114** from heat flux that is otherwise directed along the composite lamina **120**. Incorporation of the targeted heat transfer region **130** may be useful in applications in which the temperature-sensitive component **114** is sensitive to the temperature at which it operates and/or time variations in temperature across the dimensions of the temperature-sensitive component **114**. The rings **150** of the targeted heat transfer region **130** may reduce the temperature drop evaluated across the targeted heat transfer region **130** in the principal direction **90** of heat flux. The reduction in temperature drop, and the corresponding reduction in heat flux directed across the targeted heat transfer region **130** may provide an amount of thermal isolation of the temperature-sensitive component **114** from the temperature-insensitive component **112**, while maintaining electrical continuity within the composite lamina **120**.

[0034] The targeted heat transfer region **130** depicted in FIG. 5 may create a generally isothermal region in the composite lamina **120** by maintaining even temperatures across the temperature-sensitive component mounting region **138** when a temperature gradient is otherwise maintained on the composite lamina **120**. The isothermal region, therefore, may be indicative of a reduce temperature variation within the targeted heat transfer region **130**, which may be beneficial for heat-sensitive electrical components that perform adversely when subjected to thermal gradients.

[0035] The thermal management features of the targeted heat transfer region **130**, here the rings **150**, may be selected so that the effective thermal conductivity of the targeted heat transfer region **130** is similar to that of the bulk region **132**. This may be evaluated by comparing the reduced average coefficient of thermal conductivity of the targeted heat transfer region **130** and the bulk region **132** (i.e., $k_b = f k_c + (1-f) k_c$), where k_b is the of the reduced average coefficient of thermal conductivity of the bulk region **132**, k is the coefficient of thermal conductivity of the thermal conductor **142**, k_c is the coefficient of thermal conductivity of the insulator substrate **140**, and f is the volume fraction of the thermal conductor **142** within the bulk region **132**). Additionally, in some embodi-

ments, the width and the depth of the rings 150 may vary relative to one another and/or along their lengths to vary the thermal capacitance of the targeted heat transfer region 130. In some embodiments, the effective thermal conductivity of the targeted heat transfer region 130 is within about 10% of the effective thermal conductivity of the bulk region 132. In other embodiments, the effective thermal conductivity of the targeted heat transfer region 130 is within about 5% of the effective thermal conductivity of the bulk region 132. In yet other embodiments, the effective thermal conductivity of the targeted heat transfer region 130 is approximately equal to the effective thermal conductivity of the bulk region 132. Minimization of the difference between the effective thermal conductivity between the targeted heat transfer region 130 and the bulk region 132 may reduce the disruption of heat flux at positions spaced apart from the targeted heat transfer region 130.

[0036] Referring now to FIG. 6, another embodiment of the targeted heat transfer region 230 is depicted. The targeted heat transfer region 230 includes a composite structure of the thermal conductor 142 and the insulator substrate 140 where the thermal conductor 142 is arranged in rings 150 that encapsulate a temperature-sensitive component mounting region 138, here the second electronic component attachment module 124, and a plurality of spokes 152 that extend radially between the concentric rings 150 to place the concentric rings 150 into thermal continuity with one another. While the spokes 152 depicted in FIG. 6 are arranged in a radial orientation, it should be understood that the spokes 152 may be arranged in a variety of configurations based on the requirements of the application. The outer-most ring 150 may be in thermal continuity with the lattice of thermal conductor 142 positioned along the insulator substrate 140.

[0037] The concentric rings 150 and the spokes 152 of the targeted heat transfer region 230 direct heat flux along the spokes 152 and between the rings 150 so that the heat flux through the targeted heat transfer region 230 increases as compared with the bulk region 132 of the composite lamina 120 incorporating the thermal conductor 142 and the insulating substrate 140 in the lattice-like arrangement. In this embodiment, the targeted heat transfer region 230 encapsulates the temperature-sensitive component mounting region 138, while the thermal conductor 142 in the lattice-like arrangement is positioned around the temperature-insensitive component mounting region 136 of the composite lamina 120. Accordingly, the targeted heat transfer region 230 may increase heat flux that flows into the temperature-sensitive component 114. As such, the targeted heat transfer region 230 may concentrate thermal energy towards the temperature-sensitive component 114. Incorporation of the targeted heat transfer region 230 may be useful in applications in which the temperature-sensitive component 114 performs with improved efficiency at elevated temperature gradients, for example with thermoelectric components. The spokes 152 between the concentric rings 150 of the targeted heat transfer region 230 may increase the temperature drop evaluated across the targeted heat transfer region 230 in the principal direction 90 of heat flux. The increase in temperature drop, and the corresponding increase in heat flux directed across the targeted heat transfer region 230, may provide an amount of thermal amplification of the temperature-sensitive component 114 from heat generated by the temperature-insensitive component 112, while maintaining electrical continuity within the composite lamina 120.

[0038] Referring now to FIG. 7, yet another embodiment of the targeted heat transfer region 330 is depicted. The targeted heat transfer region 330 includes a composite structure of the thermal conductor 142 and the insulator substrate 140 where the thermal conductor 142 is arranged in a plurality of spokes 154 that extend in a spiraled orientation to encapsulate a temperature-sensitive component mounting region 138, here the second electronic component attachment module 124. While the spokes 154 depicted in FIG. 7 are arranged in a spiral orientation in which the radius of the spoke 154 decreases with increasing distance from the lattice-like region, it should be understood that the spokes 154 may be arranged in a variety of configurations depending on the requirements of the application.

[0039] The spokes 154 of the targeted heat transfer region 330 direct thermal energy along the spokes 154 and away from travelling in a linear direction through the targeted heat transfer region 330 so that the thermal energy introduced to the targeted heat transfer region 330 is turned to follow the direction of the spokes 154. As such, the targeted heat transfer region 330 may direct thermal energy around the temperature-sensitive component 114, thereby turning the direction of conveyance of thermal energy within the targeted heat transfer region 330. In some embodiments, the targeted heat transfer region 330 may turn the heat flux such that the temperature drop evaluated along the interior of the targeted heat transfer region 330 proximate to the temperature-sensitive component mounting region 138 is inverted from the temperature drop evaluated along the exterior of the targeted heat transfer region 330. Incorporation of the targeted heat transfer region 330 may be useful in applications in which the temperature-sensitive component 114 performs with improved efficiency when heat flows in a particular direction. The decrease in temperature drop, and the corresponding decrease in heat flux directed across the targeted heat transfer region 330, may provide an amount of thermal isolation of the temperature-sensitive component 114 from heat generated by the temperature-insensitive component 112, while maintaining electrical continuity within the composite lamina 120.

[0040] Incorporating targeted heat transfer regions 130, 230, 330 according to the present disclosure into composite laminas 120 may allow for modifying the conductive heat transfer along the surface of the composite laminas 120. As discussed hereinabove, when embodiments of the circuit board assembly include electrical components that perform adversely when subjected to elevated temperatures or high temperature gradients, targeted heat transfer zones regions that shield the electrical component from heat flux or turn the heat flux to reduce the introduction of thermal energy to the electrical component may be desired. In these embodiments, incorporation of a targeted heat transfer zone may allow for temperature-sensitive components to be mounted to the composite lamina for electrical continuity, while minimizing any effects of elevated temperature on the temperature-sensitive electrical components. Additionally, as noted hereinabove, the targeted heat transfer zones may be configured with alternative geometric shapes to provide shape the thermal environment along the composite laminas that surround the temperature-sensitive components.

[0041] Similarly, for electrical components that operate with increased efficiency at elevated temperatures, embodiments of the circuit board assembly may incorporate targeted heat transfer regions that focus the heat flux towards the electrical component, thereby increasing the temperature sur-

rounding the electrical component. In these embodiments, the increase in temperature may improve the performance of the temperature-sensitive electrical component. Accordingly, by focusing the thermal energy towards the temperature-sensitive electrical component, improved performance of the temperature-sensitive electrical component may be realized.

[0042] Referring again to FIGS. 2-4, it should be understood that the electrical conductor 144 and the insulator substrate 140 may convey thermal energy from the temperature-insensitive component 112 towards the heat sink 118 and/or the temperature-sensitive component 114, in addition to the thermal energy that is conveyed by the thermal conductor 142. However, the thermal conductor 142 may exhibit a thermal conductivity (based on the thermal conductivity and the width and thickness of the thermal conductor 142) that is greater than the thermal conductivity of the insulator substrate 140 and the electrical conductor 144. Because the thermal conductivity of the thermal conductor 142 is greater than the insulator substrate 140 and the electrical conductor 144, a substantial portion of the thermal energy emitted by the temperature-insensitive component 112 may be directed by the thermal conductor 142. Particular designs of the composite laminas 120 according to the present disclosure may account for the location, dimensions, and the thermal conductivity of the insulator substrate 140 and the electrical conductor 144 when the position of the thermal conductor 142 is determined. Accordingly, design of the composite laminas 120 may account for both the thermal dissipation and electrical continuity requirements of the various electrical components of the circuit board assembly 110.

[0043] In some embodiments, the thermal conductor may place the temperature-insensitive component into electrical continuity with the temperature-sensitive component, so that no additional electrical conductor is required in the composite lamina. In these embodiments, the thermal conductor is configured to direct the flow of heat flux along the composite lamina while simultaneously maintaining electrical continuity between components mounted to the composite lamina including, for example, the temperature-sensitive component and the temperature-insensitive component. In such embodiments, the thermal conductor, therefore, conducts both thermal and electrical energy.

[0044] Referring now to FIGS. 8-10, another embodiment of a heat transfer management apparatus 400 is depicted. In this embodiment, the heat transfer management apparatus 400 includes a composite laminate assembly 420 having a plurality of laminae 422, 424. In the embodiment depicted in FIGS. 8-10, the composite laminate assembly 420 includes a first lamina 422 and a second lamina 424. It should be understood that composite laminate assemblies 420 according to the present disclosure may include any number of laminae based on the requirements of the particular application. The first lamina 422 includes a first electronic component attachment module 122 and a second electronic component attachment module 124 to which a temperature-insensitive component 112 and a temperature-sensitive component 114, respectively, may be coupled. The first lamina 422 of the composite laminate assembly 420 also includes a plurality of electrical conductors 144 that are at least partially embedded in the insulator substrate 140. In the depicted embodiment, the electrical conductors 144 are positioned along an interior face of the first lamina 422 opposite the first and second electronic component attachment module 122, 124. The electronic component attachment modules 122, 124 are main-

tained in electrical continuity with the electrical conductors 144. In the depicted embodiment, a plurality of electronic leads 444 extend from the first and second electronic component attachment modules 122, 124 to the electrical conductors 144 and place the first and second electronic component attachment modules 122, 124 in electrical continuity with the electrical conductors 144.

[0045] The first lamina 422 also includes an embedded thermal conductor 442. The embedded thermal conductor 442 is at least partially embedded within the insulator substrate 140 and is electrically isolated from the electrical conductor 144. In the embodiment depicted in FIGS. 8-10, the embedded thermal conductor 442 is spaced apart from the exterior face of the first lamina 422 along which the first and second electronic component attachment modules 122, 124 are positioned. The embedded thermal conductor 442 is exposed along the interior face of the first lamina 422 opposite the first and second electronic component attachment modules 122, 124.

[0046] The second lamina 424 includes an insulator substrate 440 and a thermal conductor 142 at least partially embedded in the insulator substrate 440. In the embodiment depicted in FIGS. 8-10, the thermal conductor 142 is positioned along the top face of the second lamina 424. The thermal conductor 142 may be arranged in a variety of configurations, including being positioned in a lattice, similar to that described in regard to FIGS. 2-4 above. The thermal conductor 142 is positioned to be spaced apart from the electrical conductor 144, so that the thermal conductor 142 and the electrical conductor 144 remain electrically isolated from one another. The thermal conductor 142 is placed into thermal conductivity with the embedded thermal conductor 442 of the first lamina 422.

[0047] The second lamina 424 also includes a targeted heat transfer region 130 that is at least partially embedded within the insulator substrate 440 of the second lamina 424. Similar to the embodiments of the targeted heat transfer region 130 described hereinabove, the targeted heat transfer region 130 may modify the local thermal conductivity of the composite laminate assembly 420 to shape the heat flux that is directed along the composite laminate assembly 420. Embodiments of the targeted heat transfer regions 130 may shield the temperature-sensitive component 114 from thermal energy generated by the temperature-insensitive component 112 or may focus the thermal energy from the temperature-insensitive component 112 towards the temperature-sensitive component 114.

[0048] Electrical signals are conveyed to and from the temperature-insensitive component 112 through the electrical conductors 144. Heat generated by the temperature-insensitive component 112 is directed into the first lamina 422 of the composite laminate assembly 420. A substantial portion of the thermal energy generated by the temperature-insensitive component 112 is directed into the embedded thermal conductor 442 of the first lamina 422. Thermal energy is directed along the composite laminate assembly 420 from the embedded thermal conductor 442 to the thermal conductor 142 of the second lamina 424, along a thermal path towards the heat sink 118 and/or the temperature-sensitive component 114. Thermal energy from the temperature-insensitive component 112 is selectively shielded from, focused towards, or guided in relation to the temperature-sensitive component 114, based on the configuration of the targeted heat transfer region 130.

[0049] It should be understood that a variety of configurations of the multi-laminae composite laminate assembly 420

may incorporate thermal conductors **142** and electrical conductors **144** that are electrically isolated from one another so that the conveyance of heat flux along the composite laminate assembly **420** may be controlled to provide a desired effect, while maintaining electrical continuity between electrical components mounted to the composite laminate assembly **420**. Additional laminae incorporating electrical components, thermal conductors, and/or electric conductors into an insulator substrate **440** may be included in the circuit board assembly **410** so that the desired electronic assembly are able to reject heat into the surrounding environment, shielding or focusing the thermal energy towards the temperature-sensitive electronics components as required. Accordingly, it should be understood that embodiments of the composite laminate assembly **420** according to the present disclosure may be designed to account for both the thermal dissipation and electrical continuity requirements of the various electrical components of the circuit board assembly **410**. Further, the thermal conductors **142** and the electrical conductors **144** of the composite laminate assembly **420** may be separated from one another by insulator substrate **440** so that the heat flux can be selectively directed along the thermal conductor **142**, minimizing the effects of the thermal conductivity of the electrical conductors **144**.

[0050] In yet further embodiments of multi-laminae composite laminate assemblies, thermal conductors of certain layers may both provide thermal and electrical continuity to the components of the heat transfer management apparatus. In some embodiments, electrical continuity between the components of the heat transfer management apparatus may be directed to composite laminae that are spaced apart from the printed wiring board to which the components are mounted. In such embodiments, the thermal continuity and the electrical continuity between components may be maintained through alternate layers of the multi-laminae composite laminate assembly.

[0051] Referring now to FIG. 11, another embodiment of a heat transfer management apparatus **500** incorporating a composite laminate assembly **510** is depicted. In this embodiment, the composite laminate assembly **510** includes a composite lamina **520** having a plurality of electronic component attachment modules **122** and at least one second electronic component attachment modules **124**. A temperature-insensitive component **112** is attached to each of the electronic component attachment modules **122** and a temperature-sensitive component **114**, here a temperature-sensitive electrical component, is coupled to the second electronic component attachment module **124**. Similar to embodiments discussed hereinabove, the composite lamina **520** also includes a thermal conductor **542** that is at least partially embedded into an insulator substrate **540**. The thermal conductor **542** is adapted to conduct heat along its elements. In the embodiment depicted in FIG. 11, the thermal conductor **542** is arranged in to a lattice having a plurality of strands that are in thermal conductivity with one another. The thermal conductor **142** also is arranged into a targeted heat transfer region **530**. The targeted heat transfer region **530** includes a modified pattern as compared to the bulk region **532** of the thermal conductor **142**, so that the direction of heat flux in the bulk region **532** differs from that in the targeted heat transfer region **530**.

[0052] In the embodiment depicted in FIG. 11, the targeted heat transfer region **530** directs thermal energy from each of the temperature-insensitive components **112** toward the temperature-sensitive component **114**, focusing the thermal

energy from the temperature-insensitive components **112** to the temperature-sensitive component **114**. Such a configuration may be suitable for applications in which the temperature-sensitive component **114** is a temperature-sensitive electrical component that operates with increased efficiency at elevated temperatures. The configuration of the temperature-insensitive components **112**, the temperature-sensitive component **114**, and the targeted heat transfer region **530** may increase the heat flux that is directed to the temperature-sensitive component **114**.

[0053] Referring now to FIGS. 12-14, another embodiment of the heat transfer management apparatus **600** is depicted. In this embodiment, the heat transfer management apparatus **600** includes a plurality of composite laminae **620** that are coupled to one another to form a composite laminate assembly **618**. The composite laminae **620** are assembled around an electric motor **602**. The electric motor **602** includes a rotor **606** that is adapted to rotate within a stator **604**, generating a motive force of the rotor. In the depicted embodiment, the strength of the motive force is based on the amount of electricity passing through the windings (not shown) of the stator **604** and the strength of the magnetic force of the rotor **606**. As the amount of electricity passing through the windings increases, the motive force provided by the rotor **606** generally increases.

[0054] The increase in electricity passing through the windings, however, generally corresponds to an increase in the operating temperature of the electric motor **602**. To manage the temperature of the stator **604** of the electric motor **602**, the heat transfer management apparatus **600** may include a plurality of heat extraction devices **610** that draw heat flux away from the stator **604**, thereby reducing the temperature of the stator **604**. The heat extraction devices **610** may perform with increased efficiency at elevated temperatures and/or at elevated temperature gradients, so that the heat extraction devices **610** are temperature-sensitive components. In some embodiments, the heat extraction devices **610** may be, for example and without limitation, heat pipes, thermo-electric coolers, convective heat sinks, and the like.

[0055] Referring now to FIG. 14, one of the composite laminae **620** is depicted. Each of the composite lamina **620** in the composite laminate assembly **618** (as shown in FIG. 13) may include similar layouts of the thermal conductor **142** and the insulator substrate **140**. In the embodiment depicted in FIG. 14, the composite lamina **620** includes a thermal conductor **142** that is at least partially embedded in an insulator substrate **140**. The thermal conductor **142** is arranged into a bulk region **632** and a plurality of targeted heat transfer region **630**, where the conductive heat transfer coefficient of the bulk region **632** is less than the conductive heat transfer coefficient of the targeted heat transfer region **630**. In the embodiment depicted in FIG. 14, the targeted heat transfer region **630** includes a plurality of rings **150** that are arranged in a concentric relationship with one another, and a plurality of spokes **152** that are arranged in a radial relationship and interconnect the plurality of rings **150** with one another. As discussed hereinabove, the targeted heat transfer region **630** tends to focus heat flux from the temperature-insensitive component (here, the stator **604**) to direct heat flux into the heat extraction devices **610**. By increasing the heat flux across each of the targeted heat transfer regions **630**, thermal energy that is rejected from the stator **604** may be directed to the heat extraction devices **610** with high efficiency. Increasing the efficiency of heat rejection may decrease the quantity of heat

extraction devices **610** that are required to maintain the temperature of the stator **604** across the design envelope. Additionally, in this embodiment, the bulk region **632** and the targeted heat transfer region **360** of the composite laminae **620** may steer heat flux towards the heat extraction devices **610** (i.e., the temperature sensitive components). Accordingly, incorporation of the targeted heat transfer regions **630** may reduce the cost and complexity of the heat transfer management apparatus **600**.

[0056] It should now be understood that heat transfer management apparatuses according to the present disclosure may include at least one composite lamina having an insulator substrate and a thermal conductor at least partially embedded in the substrate. The thermal conductor is arranged in a targeted heat transfer region and a bulk region. The thermal conductivity of the printed circuit board is locally modified by the thermal conductor, such that heat flux flowing along the composite lamina is modified in the targeted heat transfer region as compared with the bulk region. The modification of the flow of thermal energy in the targeted heat transfer region allows for temperature sensitive components to be located on the composite lamina and perform with increased efficiency as compared to locating the temperature sensitive components on the bulk region.

Examples

[0057] Four samples were prepared for testing to evaluate the heat transfer properties offered by the various targeted heat transfer regions discussed hereinabove. Standard coupons were made using RO4350B material as the insulator substrate, having a coefficient of thermal conductivity of 0.69 W/(m·K). The coupons had overall lengths of 115 mm and widths of 50 mm. The insulator substrate had a thickness of 508 μm . Silver-plated copper having a coefficient of thermal conductivity of 400 W/(m·K) was formed into the bulk region with a thickness of 35 μm along both the top and bottom surfaces of the insulator substrate through chemical etching, giving the printed circuit board coupon a total thickness of 578 μm . The silver-plated copper was arranged in the bulk region with a thickness of 200 μm with a plurality of square-shaped cells having a length and a width dimension of 2.5 mm. Thermal bus bars a complete distribution of silver-plated copper extending 37.5 mm from both ends of the insulator substrate were incorporated to provide even heat inflow and outflow to the region of interest, the 40 mm at the center of the coupon. A thin uniform coating of high emissivity ($\epsilon=0.96-0.98$) flat black paint, Krylon 1618, was applied to the region of interest of each coupon to facilitate accurate thermal imaging. The thermal contours on the exposed topside of each composite structure were obtained via a calibrated IR camera (FLIR SC7650) positioned directly above the test apparatus. Temperature gradients across corresponding to the inner diameter of the concentric rings having a diameter of 10 mm were measured.

[0058] Power was applied to each of the coupons with a 30 mm \times 30 mm \times 50 mm copper block heater with a center hole machined lengthwise to receive a single 120 V cartridge heater with a maximum power of 50 W. A direct-to-air thermoelectric cooler with a maximum cooling power of 11 W was positioned opposite the heaters and used as a heat sink. The testing apparatus was surrounded by insulation except for the area of interest, which was exposed to the ambient air environment.

[0059] Computer simulation models were constructed to simulate the steady-state heat transfer of each of the test cases.

Baseline

[0060] A baseline coupon was prepared with no targeted heat transfer region such that the bulk region having a plurality of square-shaped cells extended along the region of interest.

[0061] With power applied to the baseline coupon to establish a temperature differential of 35 K across the region of interest, the temperature gradient evaluated at a distance corresponding to the inner diameter of the concentric rings of the other coupons was evaluated to be $\nabla T \approx 8.3$ K/cm. In comparison, simulation modeling indicated that the temperature gradient would be $\nabla T \approx 9$ K/cm.

Sample 1

[0062] A coupon having a targeted heat transfer region corresponding to FIG. 5 having a plurality of concentric rings was produced having nine 250 μm -wide concentric copper rings, each of rings being spaced evenly apart from one another, where the outer diameter of the concentric rings was 18.5 mm and the inner diameter was 10 mm.

[0063] With power applied to the baseline coupon to establish a temperature differential of 35 K across the region of interest, the temperature gradient evaluated across the inner diameter of the concentric rings was evaluated to be $\nabla T \approx 0.22$ K/cm. In comparison, simulation modeling indicated that the temperature gradient would be $\nabla T \approx 0.86$ K/cm.

Sample 2

[0064] A coupon having a targeted heat transfer region corresponding to FIG. 6 having a plurality of concentric rings with radial spokes interconnecting the concentric rings was produced having two 250 μm -wide concentric copper rings, the outer ring having an outer diameter of 18.5 mm and the inner ring having an inner diameter of 10 mm. The sample included 90 radial spokes evenly arrayed around the concentric rings and connecting the outer ring and the inner ring. Each spoke had a thickness at the inner ring of 175 μm , the thickness increasing towards the outer ring so that each spoke traversed approximately 2°.

[0065] With power applied to the baseline coupon to establish a temperature differential of 35 K across the region of interest, the temperature gradient evaluated across the inner diameter of the concentric rings was evaluated to be $\nabla T \approx 16.7$ K/cm. In comparison, simulation modeling indicated that the temperature gradient would be $\nabla T \approx 19.5$ K/cm.

Sample 3

[0066] A coupon having a targeted heat transfer region corresponding to FIG. 7 having a plurality of spiraled spokes was produced having an outer diameter of 25 mm and an inner diameter of 10 mm. The sample included 16 equally-spaced logarithmic spiral copper spoke that wrapped approximately 300° around the inner diameter. Each spiral spoke was tapered and had a width of 177 μm at the inner diameter and 414 μm at the outer diameter.

[0067] With power applied to the baseline coupon to establish a temperature differential of 35 K across the region of interest, the temperature gradient evaluated across the inner diameter of the concentric rings was evaluated to be $\nabla T \approx 1.1$

K/cm, where the temperature gradient is negative, indicating that heat flux flowed in reverse across the targeted heat transfer region, the heat flux being effectively turned. In comparison, simulation modeling indicated that the negative temperature gradient would be $\nabla T \approx 1.9$ K/cm.

[0068] It is noted that the term “substantially” may be utilized herein to represent the inherent degree of uncertainty that may be attributed to any quantitative comparison, value, measurement, or other representation. This term is also utilized herein to represent the degree by which a quantitative representation may vary from a stated reference without resulting in a change in the basic function of the subject matter at issue.

[0069] While particular embodiments have been illustrated and described herein, it should be understood that various other changes and modifications may be made without departing from the spirit and scope of the claimed subject matter. Moreover, although various aspects of the claimed subject matter have been described herein, such aspects need not be utilized in combination. It is therefore intended that the appended claims cover all such changes and modifications that are within the scope of the claimed subject matter.

1. A heat transfer management apparatus comprising:
 a composite lamina comprising an insulator substrate and a thermal conductor at least partially embedded in the insulator substrate;
 a temperature-sensitive component coupled to the composite lamina; and
 a temperature-insensitive component coupled to the composite lamina and positioned distally from the temperature-sensitive component, the temperature-insensitive component producing heat during operation;
 wherein the thermal conductor and the insulator substrate are arranged into a targeted heat transfer region proximate to the temperature-sensitive component and a bulk region proximate to the temperature-insensitive component and the targeted heat transfer region and the bulk region are in thermal continuity with one another.

2. The heat transfer management apparatus of claim 1, further comprising a plurality of composite laminae coupled to one another to form a composite laminate assembly.

3. The heat transfer management apparatus of claim 1, wherein the temperature-sensitive component comprises a thermoelectric generator.

4. The heat transfer management apparatus of claim 1, wherein the temperature-sensitive component comprises a heat sink.

5. The heat transfer management apparatus of claim 1, wherein the composite lamina further comprises a temperature-sensitive component mounting region positioned proximate to the temperature-sensitive component.

6. The heat transfer management apparatus of claim 5, wherein the targeted heat transfer region comprises a composite structure having a plurality of thermally conductive rings that are embedded in the insulator substrate and encapsulate the temperature-sensitive component mounting region.

7. The heat transfer management apparatus of claim 5, wherein the targeted heat transfer region comprises a composite structure having a plurality of thermally conductive spokes that are embedded in the insulator substrate and spiraled around the temperature-sensitive component mounting region.

8. The heat transfer management apparatus of claim 5, wherein the targeted heat transfer region comprises a com-

posite structure having a plurality of thermally conductive spokes that are embedded in the insulator substrate and radially arrayed around the temperature-sensitive component mounting region.

9. The heat transfer management apparatus of claim 1, wherein the bulk region comprises a lattice of thermal conductor that is at least partially embedded in the insulator substrate.

10. The heat transfer management apparatus of claim 1, wherein the thermal conductor and the insulator substrate are positioned in the bulk region and the targeted heat transfer region to steer thermal flux from the temperature-insensitive component towards the temperature-sensitive component.

11. The heat transfer management apparatus of claim 1, wherein the thermal conductor and the insulator substrate are positioned in the bulk region and the targeted heat transfer region to steer thermal flux from the temperature-insensitive component away from the temperature-sensitive component.

12. The heat transfer management apparatus of claim 1, wherein the composite lamina places the temperature-sensitive component and the temperature-insensitive component in thermal continuity with one another.

13. A composite lamina for directing heat transfer comprising:

an insulator substrate;

a thermal conductor at least partially embedded in the insulator substrate;

a temperature-sensitive component mounting region; and
 a temperature-insensitive component mounting region,

wherein the thermal conductor and the insulator substrate are arranged into a targeted heat transfer region proximate to the temperature-sensitive component mounting region and a bulk region proximate to the temperature-insensitive component mounting region and the targeted heat transfer region and the bulk region are in thermal continuity with one another.

14. The composite lamina of claim 13, wherein the thermal conductor and the insulator substrate are positioned in the bulk region and the targeted heat transfer region to steer thermal flux from the temperature-insensitive component mounting region towards the temperature-sensitive component mounting region.

15. The composite lamina of claim 13, wherein the thermal conductor and the insulator substrate are positioned in the bulk region and the targeted heat transfer region to steer thermal flux from the temperature-insensitive component mounting region away from the temperature-sensitive component mounting region.

16. The composite lamina of claim 13, wherein an effective thermal conductivity of the targeted heat transfer region is within about 10% of the effective thermal conductivity of the bulk region.

17. The composite lamina of claim 13, wherein the thermal conductor places the temperature-insensitive component mounting region, the bulk region, and the targeted heat transfer region into thermal continuity with one another.

18. The composite lamina of claim 13, wherein the targeted heat transfer region comprises a plurality of thermally conductive rings that are embedded in the insulator substrate and encapsulate the temperature-sensitive component mounting region.

19. The composite lamina of claim 13, wherein the targeted heat transfer region comprises a plurality of thermally con-

ductive spokes that are embedded in the insulator substrate and spiraled around the temperature-sensitive component mounting region.

20. The composite lamina of claim **13**, wherein the targeted heat transfer region comprises a plurality of thermally conductive spokes that are embedded in the insulator substrate and radially arrayed around the temperature-sensitive component mounting region.

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