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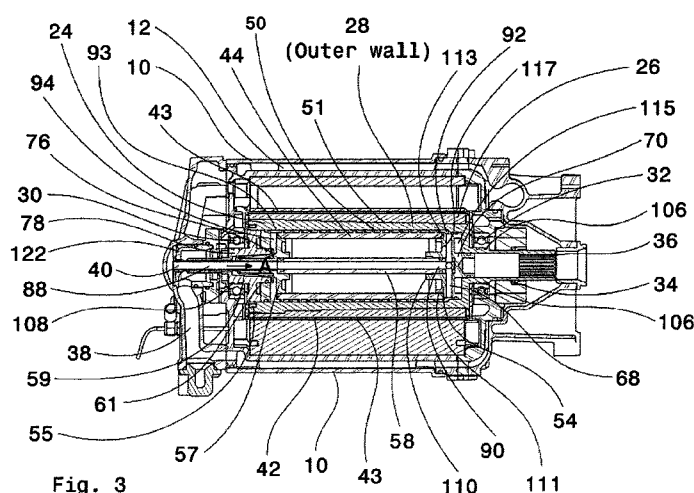


Fig. 3

(57) Abstract: The invention provides a rotary device, comprising: a stator for receiving or outputting electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises an axial fluid conduit for the flow of a coolant between a first end of the rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the axial fluid conduit and arranged in use to receive coolant from or provide coolant to the axial fluid conduit, the inner wall having one or more fluid paths for the flow of coolant, thereby to cool the rotor; and a fluid impeller arranged at the first or distal end of rotor and arranged to rotate with the rotor and impart to and/or maintain rotary movement of or remove from and/or maintain rotary movement of fluid entering or leaving the rotary device.



A Rotary Device, A Motor and a Method of Cooling a Motor

The present invention relates to a rotary device, a motor and a method of cooling a  
5 motor. The invention also relates to a generator and a method of cooling a generator.

Electric motors are used widely as a means of generating traction. However it is known  
that a problem that arises with traction motors is that significant heat can be generated  
within them. Cooling of the motor is important so as to avoid damage to thermally  
10 sensitive components within the motor. There is a desire to provide lower cost or more  
performance-dense motors. However, as will be explained below, motors that satisfy  
this desire can experience more significant heating of the rotor within the motor in normal  
operation.

15 A motor such as a three-phase synchronous motor will typically include both a stator and  
a rotor. The stator is arranged, in use, to receive electrical power so as to generate a  
varying magnetic field. The rotor, arranged coaxially within and typically enclosed by the  
stator, comprises a number of permanent magnets which, under the influence of the  
varying magnetic field, cause the rotor to rotate. Thus, by the provision of electrical  
20 power, a rotational output can be derived. Substantially the same apparatus can be  
used in a reverse order to generate electricity. In other words, if the rotor is driven by a  
rotational drive input, voltage will be generated in the stator coils.

As the demand for reduced motor mass and physical size has increased, this has  
25 inevitably led to motors in which the stator becomes hotter in use. This is due, for  
example, to a reduced copper content leading to higher resistive loss in the stator  
windings which consequently leads to the windings themselves being hotter. In a  
situation where the stator in the motor runs hotter, this generally reduces the natural  
cooling capacity of the rotor since with the stator running hotter than the rotor, there is no  
30 potential for heat loss from the rotor to the stator. This applies in particular to sealed  
enclosure motors where the rotor cannot easily be air cooled. This is typical for high  
performance liquid-cooled motors.

In addition, demand for lower manufacturing costs favour motor architectures that can lead to increased magnetic eddy current heating of the magnets and rotors. In particular the simpler the structure of, say, the permanent magnets within the motor, the greater the generated eddy currents and consequent heating can be. Conventional methods of  
5 reducing eddy current heating of rotors have included laminating the rotor and the magnets. This ensures that significant eddy currents do not have room to generate within the magnets and rotor. However, this way to address the heating problem is of reduced benefit if the stator runs at a higher temperature, since even if the amount of heat generated due to eddy currents is reduced, due to poor or negligible heat loss from  
10 the rotor to the stator, this relatively small amount of generated heat can become a problem.

In addition, if losing heat via the air gap to the stator is ineffective due to the high temperature of the stator, the remaining heat path for heat loss available to the rotor is  
15 via the shaft and bearings. This is typically a poor heat path which does not provide for significant heat transfer, so despite creating less heat by laminating the rotor, the rotor can still easily overheat due to the very poor heat loss mechanisms available.

To achieve a maximum power density motor at minimum cost, it is necessary to run the  
20 stator as hot as possible (high temperature stator materials are relatively inexpensive) and the rotor as cool as possible so as to keep magnet costs to a minimum.

The problem of how to effectively cool a motor has been around for some time and various solutions have been suggested.

25 In US-A-7,579,725 (Zhou et al) a rotor assembly cooling system is described in which a portion of a rotor shaft is hollow and includes an open end and a closed end. A coolant feed tube is rigidly attached to the rotor shaft. Thus, the shaft and the feed tube are caused to rotate at the same rate. Coolant is pumped through the feed tube until it exits  
30 the end of the feed tube and flows against the inside surface of the closed end of the rotor shaft causing the coolant to change direction and flow back through the coolant flow region. Fluid is therefore caused to flow in the space between the outer surface of the feed tube and the inner surface of the hollow rotor shaft. A continuous helical member is provided in the form of a continuous support strut which helically wraps

around the feed tube and couples it to the shaft. Due to the helical shape of the member, coolant is actively pumped in the region separating the feed tube from the shaft, thus ensuring continuous coolant flow to the rotor assembly. US-A-7,489,057 is a related patent to Zhou.

5

In US-A-3,260,872 (Potter) an oil cooled generator is provided. Here, a flow of coolant oil is provided via an opening. The coolant oil then flows through helical paths before entering the axial shaft of the generator rotor. The fluid passes towards the end of the rotor where it is reflected from the inner surface of the rotor housing and passes back  
10 through further helical paths. Eventually, the coolant passes out of the device. Accordingly, an oil cooled generator is provided in which the helical path is used to control the flow of cooling oil and in which the fluid feed tube rotates with the rotor.

Other examples of fluid-cooled motors or generators include those as described in

15 US-A-4,647,805, US-A-5,589,720, WO-A-90/09053, DE-A-19913199, US-A-4,692,644, US-A-8,022,582, US-A-2001/0308071, US-A-3,521,094, US-A-3,060,335, US-A-3,240,967, US-A-4,350,908, US-A-5,424,593, GB-A-16979, GB-A-2483122 and DE-A-3622231.

20 According to a first aspect of the present invention, there is provided a rotary device, comprising: a stator for receiving or outputting electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises conduit having an axial component for the  
25 flow of a coolant between a first end of the rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the axial fluid conduit and arranged in use to receive coolant from or provide coolant to the axial fluid conduit, the inner wall having one or more fluid paths for the flow of coolant, thereby to cool the rotor; and a fluid impeller arranged at the first or  
30 distal end of rotor and arranged to rotate with the rotor and impart rotary movement to or remove rotary movement from fluid entering or leaving the rotary device.

;

A rotary device is provided. The rotary device could function as a motor or a generator. As a motor, electrical power is provided to the stator which generates a changing magnetic field and causes rotation of the rotor by interaction with the magnets thereon. In use as a generator, the rotor is driven round which generates power in the stator by virtue of the varying magnetic field to which it is exposed. An impeller is provided arranged to rotate with the rotor and impart and/or maintain rotary movement to or remove rotary movement from fluid entering or leaving the rotary device. This means that pressure losses are avoided in cooling fluid flowing through the rotary device. An axial fluid conduit is provided which enables fluid to flow in a generally axial direction, i.e. from one end of the rotor to the other and/or back again. The axial fluid conduit is preferably arranged centrally such that fluid can flow through it in a central longitudinal axial position. In another example, the axial fluid conduit or conduits are arranged at some radial distance from the central longitudinal axis of the rotor.

According to a second aspect of the present invention, there is provided a rotary device, comprising: a stator for receiving or outputting electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises an axial fluid conduit for the flow of a coolant between a first end of the rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the axial fluid conduit and arranged in use to receive coolant from or provide coolant to the axial fluid conduit, the inner wall having one or more tortuous paths for the flow of coolant, thereby to cool the rotor; and a fluid impeller arranged at the first or distal end of rotor and arranged to rotate with the rotor and impart rotary movement to or remove rotary movement from fluid entering or leaving the rotary device.

A rotary device is provided. The rotary device could function as a motor or a generator. As a motor, electrical power is provided to the stator which generates a changing magnetic field and causes rotation of the rotor by interaction with the magnets thereon. In use as a generator, the rotor is driven round which generates power in the stator by virtue of the varying magnetic field to which it is exposed. An impeller is provided

arranged to rotate with the rotor and impart and/or maintain rotary movement to or remove rotary movement from fluid entering or leaving the rotary device. This means that pressure losses are avoided in cooling fluid flowing through the rotary device. One or more tortuous paths are provided on the inner wall for the flow of coolant. These  
5 provide a means by which fluid can be made to cover a significant proportion of the surface of the inner thereby ensuring good thermal contact of the fluid with a significant part of the rotor.

In one example, the impeller is arranged to guide the fluid towards the rotor axis for  
10 removal from the motor or radially outwardly towards the one or more tortuous paths. This is particularly useful in an example in which fluid flows (in one direction of flow) from an initially central axial position, along the length of the rotor, radially outwards to flow along the tortuous paths and then is brought back in to an axial position. The impeller in  
15 this example provides a continuous conduit for the fluid whilst not allowing the fluid to flow rotationally relative to the impeller so that when the fluid is brought back to an axial position it has had removed from it its rotational movement. With fluid flowing in the opposite direction the impeller provides a means by which the fluid can be accelerated rotationally without introducing any rotational velocity relative to the rotor.

20 In one example, the impeller is a unitary moulded component having guide ribs to guide coolant.

In one example, the impeller ribs are curved.

25 In one example, the impeller ribs are curved with varying curvature.

In one example, the impeller ribs are straight.

In one example, the impeller ribs are formed by drillings, such as cylindrical drillings..

30

In one example, the coolant enters and leaves the rotor at the same axial end thereof.

In one example, the coolant enters and leaves the rotor axially.

In one example, the coolant enters the rotor axially and leaves the rotor radially.

In one example, the coolant enters the rotor radially and leaves the rotor axially.

- 5 In one example, the stator has a labyrinthine path defined therein for the flow of coolant fluid.

In one example, the magnets are staggered or rotationally offset varying with axial displacement along rotor.

10

- According to a third aspect of the present invention, there is provided a motor for generating rotary power, the motor comprising: a stator for receiving electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon so that in response to the stator receiving the electrical power, the rotor is
- 15 caused to rotate, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant between a first end of the rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits at the second distal end of the rotor, the conduits being fluidly coupled to the central fluid
- 20 conduit and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant, thereby to cool the rotor.

- In one example, the rotor has a cylindrical body with one or more tortuous paths
- 25 arranged thereon. In other words, the inner wall is cylindrical. Upon application of power to the stator, e.g. application of a voltage to the stator, the rotor is caused to rotate. The tortuous paths guide the coolant on the surface of the cylindrical body thus ensuring good coverage of the cylindrical body by the coolant. Furthermore, radial fluid conduits are provided to guide the coolant from an axial position within the rotor to the
- 30 paths on the external surface of the cylindrical body (or in the opposite direction depending on direction of fluid flow). The use of radial conduits in this way ensures that the fluid is delivered conveniently to (or received from) the paths for onward propagation. The combination of the radial conduits and the tortuous paths provides an effective and efficient way to enable cooling of the rotor to be achieved. Furthermore, the use of

conduits for the fluid ensures that the fluid can be delivered to or received from, the tortuous paths without sudden changes in relative velocity between the rotor parts and the fluid, thus minimising resistance to the flow of coolant.

- 5 One further advantage of the use of radial conduits is that fluid is permitted to be transferred from the central axis to the outside cylinder close to the heat source and back again (or vice versa) with relatively low (if any) pressure loss.

10 In addition, the tortuous paths provided on the surface of the cylindrical body ensure that the fluid flows at relatively high velocity, i.e. higher than it would without the paths. The use of relatively high velocity fluid flow means that there is good heat transfer into the fluid. The use of tortuous paths rather than straight, narrow paths as a means to generate high velocity can be advantageous in terms of resistance to blockage and required manufacturing tolerances, although straight paths can also be used as  
15 discussed below..

Furthermore, the flow of fluid over the cylindrical surface ensures that the coolant is located close to the source of the heat (the magnets) and so heat transfer from the source is managed efficiently.

20

In one example, the tortuous paths are defined by guide ribs on or grooves in the inner wall.

In one example, the ribs or grooves are helical.

25

In one example, the angle of helical ribs or grooves is within a certain range.

In one example, the inner wall is cylindrical such that the rotor housing is hollow.

- 30 In one example, the motor comprises a fluid inlet and a fluid outlet, wherein the fluid outlet is at a greater radius than the fluid inlet.

In one example, the number of ribs or grooves is the same as the number of radial fluid conduits.



In one example, the number of ribs or grooves is 4.

5 In one example, the one or more radial conduits is or are formed as drillings or bores in an end cap fixedly mounted to the inner wall.

In one example, the central fluid conduit and the one or more radial fluid conduits are formed as a unitary component.

10 In one example, the one or more radial fluid conduits is or are curved.

In one example, the central fluid conduit acts as a rotor shaft and has a first end mounted in a bearing at a first end of rotor and second end mounted in a bearing at a second distal end of the rotor.

15 In one example, the hollow cylinder comprises a sealed air-filled cavity under a heat transfer zone within the motor.

20 In one example, the motor comprises a fluid impeller arranged at the first end of rotor to receive coolant from or provide coolant to the spiral ribs and guide the fluid towards the rotor axis for removal from the motor or radially outwardly towards the spiral ribs.

In one example, the impeller is a unitary moulded component having guide ribs to guide coolant.

25 In one example, the impeller ribs are curved.

In one example, the impeller ribs are curved with varying curvature.

30 In one example, the impeller ribs are straight.

In one example, the coolant enters and leaves the rotor at the same axial end thereof.

In one example, the coolant enters and leaves the rotor axially.

In one example, the coolant enters the rotor axially and leaves the rotor radially.

In one example, the coolant enters the rotor radially and leaves the rotor axially. It will  
5 be appreciated that fluid flow can be provided in any desired direction within the rotor. In  
one example, the fluid is provided radially and taken from the rotor after its passage  
through it, from the same end of the rotor. In another example, the fluid is provided  
axially at one end and leaves radially at the other. In another example fluid is provided  
radially at one end and leaves radially at the opposite end. In the example where fluid  
10 leaves from a different end from which it is input, it is typically fed directly into the  
tortuous paths for a single pass down the rotor before it leaves at the second end.

In one example, the stator has a labyrinthine path defined therein for the flow of coolant  
fluid.

15

In one example, the magnets are staggered or rotationally offset varying with axial  
displacement along rotor.

According to a fourth aspect of the present invention, there is provided an electricity  
20 generator, comprising: a stator having electrical contacts for outputting generated power;  
a rotor arranged coaxially within the stator and having one or more magnets arranged  
thereon, the rotor having a drive input for receiving a rotary input so that in response to  
the rotor being driven, electrical power is generated in the stator; the rotor comprising a  
housing having an inner wall, the magnets being arranged around the housing, and  
25 wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant  
between a first end of the rotor and a second distal end of the rotor; the rotor further  
comprising radial fluid conduits at the second distal end of the rotor, fluidly coupled to  
the central fluid conduit and arranged in use to receive coolant from or provide fluid to  
the central fluid conduit, the inner wall having plural tortuous paths for the flow of  
30 coolant, thereby to cool the rotor.

According to a fifth aspect of the present invention, there is provided a method of cooling  
a rotor in a motor for generating rotary power, the method comprising: in a motor having  
a stator for receiving electrical power, a rotor arranged coaxially within the stator and

having one or more magnets arranged thereon, providing the rotor with a cylindrical rotor housing having an inner wall, the magnets arranged around the housing, and also providing the rotor with a central fluid conduit for the flow of a coolant axially between a first input end of the rotor and a second distal end of the rotor; and providing the rotor  
5 with one or more radial fluid conduits at the second distal end of the rotor, fluidly coupled to the central fluid conduit and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant, thereby to cool the rotor.

10 In one example, the method comprises providing coolant to the central fluid conduit such that the coolant is caused to flow into the radial conduits and along the tortuous paths to cool the rotor.

According to a sixth aspect of the present invention, there is provided a motor for  
15 generating rotary power, the motor comprising: a stator for receiving electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon so that in response to the stator receiving the electrical power, the rotor is caused to rotate, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid  
20 conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor; the rotor further comprising an end member arranged at the second distal end of the rotor having radial fluid conduits fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the inner wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant  
25 from the second distal end to the first input end, thereby to cool the rotor.

In one example, the rotor has a cylindrical body with plural tortuous paths arranged thereon. Instead of tortuous paths, the fluid paths could instead be straight and axially aligned in any desired manner. What matters is that the fluid paths cover a significant  
30 proportion of the inner wall. . Upon application of power to the stator, e.g. application of a voltage to the stator, the rotor is caused to rotate. A cylindrical inner wall can be provided and the fluid paths guide the coolant on the surface of the cylindrical body thus ensuring good coverage of the cylindrical body by the coolant. It is preferred that the fluid paths cover at least 35%, of the surface of the inner wall. More preferably the fluid

paths are arranged to cover a majority of the surface area of the inner wall, e.g. at least 50%, and even more preferably at least 75% of the surface area of the inner wall. One convenient way by which such surface coverage can be achieved is with the use of tortuous paths which is therefore preferred.

5

It may also be provided that, in use, the minimum flow rate of fluid within the fluid paths 50 is 0.5m/s.

10

Furthermore, radial fluid conduits are provided to guide the coolant from an axial position within the rotor to the paths on the external surface of the cylindrical body. The use of radial conduits in this way ensures that the fluid is delivered conveniently to the paths for onward propagation along the cylindrical wall. The combination of the radial conduits and the tortuous paths provides an effective and efficient way to enable cooling of the rotor to be achieved. Furthermore, the use of conduits for the fluid ensures that the fluid 15 can be delivered to, and returned from the tortuous paths without sudden changes in relative velocity between the rotor parts and the fluid, thus minimising resistance to the flow of coolant.

20

One further advantage of the use of radial conduits is that fluid is permitted to be transferred from the central axis to the outside cylinder close to the heat source and back again with relatively low (if any) pressure loss.

25

In addition, the tortuous paths provided on the surface of the cylindrical body ensure that the fluid flows at relatively high velocity, i.e. higher than it would without the paths. The use of relatively high velocity fluid flow means that there is good heat transfer into the fluid. The use of tortuous paths rather than straight, narrow paths as a means to generate high velocity is advantageous in terms of resistance to blockage and required manufacturing tolerances.

30

Furthermore, the flow of fluid over the cylindrical surface ensures that the coolant is located close to the source of the heat (the magnets) and so heat transfer from the source is managed efficiently.

In one example, ribs are provided to define the tortuous paths. The ribs are preferably spiral. This ensures that full coverage of the cylindrical surface with coolant can be achieved, which in turn ensures that heat transfer from the rotor can be performed effectively.

5

In one example, the angle of ribs, i.e. the spiral angle with respect to the longitudinal dimension of the rotor is within a defined range so as to ensure good coverage of the rotor cylindrical wall and a fast fluid flow rate for good heat transfer.

10 In one example a 4 start helical thread pattern is used, which, together with the width of flow passage or pitch, yields 10 degrees as a helix angle. The width and height of passage was determined by the target flow area, which in turn results from a 2m/s target velocity, consistent with good heat transfer without excessive pressure drop. In this example, a flow area of 48mm<sup>2</sup> is provided. Similar cooling performance may be  
15 achieved with 3 or 6 radial drillings and a helix angle in the range 5 to 30 degrees. Thus, it is preferred in general that the angle of helical ribs or grooves is in the range of 5 to 30 degrees.

In one example, the cylindrical rotor housing is hollow. This is particularly advantageous  
20 since it ensures that a rotor can be provided in the motor, wherein the rotor has low inertia and mass. This is important in terms of being able to start and stop the motor, and more generally reduces the required power to accelerate or decelerate the motor.

In one example, the magnets are staggered or rotationally offset varying with axial  
25 displacement along rotor. This enables an optimal response to the varying field generated by the coils within the stator and reduces the magnetic-field-induced harmonic distortion in the driving A/C waveform.

In one example, the number of paths or ribs is the same as the number of radial fluid  
30 conduits. This enables a one-to-one correspondence to be established between the conduits and the paths which provides for efficient passing of the coolant from the radial conduits to the paths.

In one example, the number of tortuous paths ribs is 4 (the number of ribs will correspond). This provides good coverage of the cylindrical surface of the rotor whilst being easy to manufacture.

- 5 In one example, the radial conduits are formed as drillings or bores in the end member. This is a particularly preferred arrangement since it is easy to manufacture. It is envisaged that where the central fluid conduit connects to the end member drilling may extend into the central fluid conduit too so as to enable the fluid to leave from the cylindrical outer wall of the central fluid conduit directly into the drillings or bores within  
10 the end member.

- In one example, the central fluid conduit and end member (including the radial fluid conduits) are formed as a unitary component. This reduces part count of the motor as a whole and ensures good connection between the central fluid conduit and end member.  
15

- In one example, the central fluid conduit acts as a rotor shaft and has a first end mounted in bearing at first end of rotor and second end mounted in bearing at distal end, wherein the rotor shaft extends into and is supported by the bearing.
- 20 In one example, the hollow cylinder comprises a sealed air-filled cavity. The air filled cavity is arranged within the rotor under the heat transfer zone. The use of an air-filled cavity minimises inertia and thereby reduces the power required to start, stop, accelerate or decelerate the motor.

- 25 In one example, the motor comprises a fluid impeller arranged at the first end of rotor to receive coolant from the spiral ribs and guide the fluid towards the rotor axis for removal from the motor. This is a particularly advantageous feature since the removal of whirl from the coolant as it leaves the motor means that pressure loss is avoided and so no high pressure pump is required to pump the coolant through the motor.

- 30 In one example, the impeller is a unitary moulded component having guide ribs to guide coolant. This enables the benefits of the impeller to be achieved with minimal additional part count. It also means that the impeller can in practice be a simple moulded component within the motor assembly.

In one example, the impeller ribs are curved, which provides for a smooth and gentle removal of whirl from the received coolant. In the case where the impeller is a simple moulded component the provision of appropriately shaped ribs is easy to achieve.

5

In one example, the impeller ribs are curved with varying curvature. The use of a gradually varying curvature in the ribs allows the control of the removal of whirl to be more accurately achieved.

10 In one example, the stator has a labyrinthine path defined therein for the flow of coolant fluid. This enables the stator to be kept cool as well. In one example, the coolant fluid path within the stator and the coolant fluid path within the rotor are a continuous path for fluid. This means that a single fluid cycle can be used to cool the rotor and stator of the motor, i.e. the entire motor. In one example, a coolant flow rate of 15l/min is specified to  
15 cool a motor of greater than 100kW output and overall package volume of 8 litres.

In one example, the fluid inlet to the rotor and outlet from the rotor are at different radii. In combination with the low pressure losses achievable with the use of the radial conduits, this means that the motor can effectively self-pump. This is because if the  
20 outlet is at a larger radius than the inlet, then the resultant change in radius over the entire fluid path within the motor (i.e. from inlet to outlet) is in the direction that is forced by the rotation of the rotor. In other words, the rotor itself acts as centrifugal pump which can obviate the need for an additional coolant pump.

25 According to a seventh aspect of the present invention, there is provided an electricity generator, comprising: a stator having electrical contacts for outputting generated electricity; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor having a drive input for receiving a rotary input so that in response to the rotor being driven, a voltage is generated in the stator; the rotor  
30 comprising a cylindrical rotor housing having a cylindrical wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor; the rotor further comprising an end member arranged at the second distal end of the rotor having radial fluid conduits fluidly coupled to the central

fluid conduit and arranged in use to receive coolant from the central fluid conduit, the cylindrical wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.

- 5 As well as a motor, in one aspect there is also provided a generator. It will be appreciated that in terms of components the two are very similar. Whereas a motor is used to generate a rotary output from an electrical signal, a generator is used to generate an electrical output from a rotary input. The advantages ascribed above to the motor therefore apply also to the generator. In particular, the tortuous paths guide the
- 10 coolant on the surface of the cylindrical body thus ensuring good coverage of the cylindrical body by the coolant. The radial fluid conduits are provided to guide the coolant from an axial position within the rotor to the paths on the external surface of the cylindrical body. The use of radial conduits in this way ensures that the fluid is delivered conveniently to the paths for onward propagation along the cylindrical wall. The
- 15 combination of the radial conduits and the tortuous paths provides an effective and efficient way to enable cooling of the rotor to be achieved. Furthermore, the use of conduits for the fluid ensures that the fluid can be delivered to the start of the tortuous paths without significant turbulence being introduced to the fluid flow.
- 20 According to an eighth aspect of the present invention, there is provided a method of cooling a rotor in a motor for generating rotary power, the method comprising: in a motor having a stator for receiving electrical power, a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, providing the rotor with a cylindrical rotor housing having a cylindrical wall, the magnets arranged around the housing, and
- 25 also providing the rotor with a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor; and providing the rotor with an end member arranged at the second distal end of the rotor having radial fluid conduits fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the cylindrical wall having tortuous guide ribs to
- 30 define plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.



In one example, the method comprises providing coolant to the central fluid conduit such that the coolant is caused to flow into the radial conduits and along the tortuous paths to cool the rotor.

- 5 In a ninth aspect, there is provided a motor for generating rotary power, the motor comprising: a stator for receiving electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon so that in response to the stator receiving the electrical, the rotor is caused to rotate, the rotor comprising a cylindrical rotor housing having a cylindrical wall, the magnets being arranged around  
10 the housing, and wherein the rotor also comprises a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor; the rotor further comprising an end member arranged at the second distal end of the rotor having radial fluid conduits fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the cylindrical wall having plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to  
15 cool the rotor.

- In a tenth aspect, there is provided a method of cooling a generator, the method comprising: in a generator having a stator and a rotor arranged coaxially within the stator  
20 having one or more magnets arranged thereon and being arranged to receive a rotary drive input, providing the rotor with a rotor housing having an inner wall, the magnets arranged around the inner wall, and also providing the rotor with a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor; and providing the rotor with one or more radial fluid conduits at the second  
25 distal end of the rotor, fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the inner wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.

- 30 In an eleventh aspect, there is provided a rotary device, comprising: a stator for receiving or outputting electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant between a first end of the

rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits at the second distal end of the rotor, the conduits being fluidly coupled to the central fluid conduit and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having plural tortuous paths for the flow of  
5 coolant, thereby to cool the rotor.

According to a further aspect of the present invention, there is provided a rotary device, comprising: a stator for receiving or outputting electrical power; a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor  
10 comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises an axial fluid conduit for the flow of a coolant between a first end of the rotor and a second distal end of the rotor; the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the axial fluid conduit and arranged in use to receive coolant from or provide  
15 coolant to the axial fluid conduit, the inner wall having one or more fluid paths for the flow of coolant, thereby to cool the rotor, the fluid paths having internal surfaces that are in use, wetted by the flow of cooling fluid thereby defining a wetted surface area, wherein the total wetted surface area is at least 35% of the inner surface area of the magnets.

20 Preferably, the total wetted surface area is at least 50% of the surface area of the magnets. Preferably, the total wetted surface area is at least 75% of the surface area of the magnets. More preferably, the total wetted surface area is at least 100% of the surface area of the magnets and most preferably, the total wetted surface area is greater than 100%, e.g. at least 125% or 150%, of the inner surface area 51 of the magnets.

25 Preferably, there is provided a fluid impeller arranged at the first or distal end of rotor and arranged to rotate with the rotor and impart rotary movement to or remove rotary movement from fluid entering or leaving the rotary device.

30 All other stated advantages follow correspondingly. Where a feature has been stated above being provided "in one example", it will be appreciated that it can be provided in combination with one or more other such features in any of the stated aspects of the invention.

Embodiments of the present invention will now be described in detail with reference to the accompanying drawings, in which:

Figure 1 is a schematic representation of a traction motor as fitted onto the engine of a  
5 typical hybrid or electric vehicle;

Figure 2 is a schematic representation of a traction motor as might be provided in the system of Figure 1;

10 Figure 3 is a perspective cross section through the motor as might be provided in the motor assembly of Figure 2;

Figure 4 is a longitudinal cross section through the motor assembly of Figure 2;

15 Figure 5 is a partial vertical cross section through the motor assembly of Figure 2;

Figure 6 is a perspective longitudinal cross section through a rotor assembly;

Figure 7 is a schematic representation of a rotor from an assembly such as that shown in  
20 Figures 3 to 6;

Figure 8 is a schematic representation of a bearing journal for the rotor of Figure 7;

Figure 9 is a schematic representation of the helical rotor coolant component for use in a  
25 rotor assembly;

Figure 10 is a schematic representation of a coolant impeller for use in a motor assembly;

30 Figure 11 is a schematic representation of a rear end plug for use in a motor assembly;

Figure 12 is a schematic representation of a tube for connecting to the plug of Figure 11 for use in a motor assembly;

Figure 13 is a schematic representation of a plug for use in a motor assembly;

Figure 14 is a schematic representation of a longitudinal cross section through the rotor of a motor assembly;

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Figure 15 is a longitudinal cross section through a schematic representation of a rotor for a motor assembly;

Figure 16 shows a schematic representation of one example of an inlet tube seal;

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Figure 17 is a schematic representation of an alternative example of a rotor for use in a motor or rotary device;

Figure 18 is a schematic representation of a close-up of a section of the rotor of Figure 17, including four co-axial feed ports;

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Figure 19 is a schematic representation of a section through the rotor of Figure 17, showing four radial return ports at a shaft exit;

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Figure 20 is a schematic representation of an end portion of the rotor of Figure 17, including an inlet feed impeller device;

Figure 21 is a schematic representation of a section through four return ports from a surface helix on a rotor such as that shown in Figure 17;

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Figure 22 is a schematic representation of a section through four radial feed ports providing a liquid feed to the surface helix of the rotor of Figure 17;

Figure 23 is a schematic representation showing a section through two of four co-axial feed ports, by which liquid is fed to the surface helix of a rotor such as that shown in Figure 17;

30

Figure 24 is a schematic representation of an impeller and coupling spigot for a rotor such as that shown in Figure 17;

Figure 25 is a section showing the coolant path from an impeller to the shaft co-axial ports for a rotor such as that shown in Figure 17;

- 5 Figure 26 shows a section through the co-axial return conduits from the surface helix on a rotor such as that of Figure 17;

Figure 27 is a schematic representation of the front view showing the inlet holes which feed tangentially into impeller blades on a rotor such as that shown in Figure 17;

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Figure 28 is a section through one of the four inlet holes feeding tangentially into the impeller of Figure 27;

- 15 Figure 29 is a schematic representation of an alternative example of a rotor for use in a motor;

Figure 30 is a schematic representation of a section through the rotor of Figure 29;

- 20 Figure 31 is a view of a section through the ports from a surface helix to an outer co-axial annulus of the rotor of Figure 29;

Figure 32 is a schematic representation of a section through return ports from a surface helix to the outer co-axial annulus of the rotor;

- 25 Figure 33 is a view of a section through a coolant inlet-outlet manifold;

Figure 34 is a schematic representation of a section through a shaft assembly including the inlet-outlet manifold;

- 30 Figure 35 is a section through the radial coolant inlet conduits to the surface helix on the rotor of Figure 29;

Figure 36 is a section through the radial coolant return conduits from the surface helix on the rotor of Figure 29;

Figure 37 is a schematic representation of a section through the shaft assembly showing coolant inlets and outlets for the rotor of Figure 29.

5 Figure 1 is a view of a traction motor 2 installed on an engine 6. The traction motor 2 is arranged within a housing 4 coupled to the engine 6. Further description of the engine 6 will not be provided. It will be understood that any appropriate type of engine may be used. The housing 4 of the motor 2 is coupled to the engine 6 using connectors 8 such as bolts or rivets although the particular type of connector used is not important. The  
10 engine 6 can produce a power output either by the combustion of an appropriate fuel or by the output of the electric motor 2. Such hybrid power supply systems are known and further description will not be provided thereof. Such a power supply system is as might be provided in a "hybrid vehicle", i.e. a vehicle powered by a power system capable of providing power either from a combustion engine or from an electric motor.

15 Whereas a motor is used to generate a rotary output from an electrical signal, a generator is used to generate an electrical output from a rotary input. The description herein will be predominantly with respect to use of the device as a motor for generating rotary power, although it could be used instead as a generator of electrical power from a  
20 rotary power input. Thus, the term "rotary device" is used to cover both generators and motors.

Figure 2 shows a schematic representation of a motor (a traction motor) as might be provided in the system or engine of Figure 1.

25 The motor 2 has an outer casing 10 that would be in use arranged within the housing 4 shown in Figure 1. The basic structure of the motor and housing is that of a three phase synchronous motor comprising an outer stator including windings together with a co-axially mounted rotor including permanent magnets. In use, an AC power signal is  
30 provided to the windings such as to generate a rotating magnetic field which causes corresponding rotation of the rotor within the stator. In some examples this AC power source may be derived from a DC battery or cell assembly with the use of an interconnected inverter.

Figures 2A and 2B show views of the stator 22, with all or part of the inner casing 10 removed. The rotor can of course not be seen in these figures since it is enclosed by the stator. As can be seen, a labyrinthine path 12 is provided within the stator 22. The labyrinthine path 12 includes longitudinal path sections 14 together with turning portions 16 arranged generally at the axial ends of the stator. An inlet 18 is provided through which a coolant is caused to flow. An appropriate pump, such as an electric motor driven centrifugal pump may be used to drive coolant through the motor assembly. The fluid enters via the inlet 18 and passes up or down along each of the channels 14 along the labyrinthine path 12, changing direction in the turning portions 16, such as to cover substantially all of the external cylindrical surface of the stator 22 with coolant. Thus, a significant amount of heat transfer from the stator is enabled by the use of such a labyrinthine heat transfer fluid path.

As seen in Figure 2A a branching point 23 is provided at which the coolant flowing through the stator either continues on its path through the stator or splits and continues into the rotor as will now be explained in detail. The relative proportion of coolant that flows in each of the rotor and the stator can be controlled by a controllable valve or is determined by the relative dimensions of the various flow paths and conduits.

Once the heat transfer fluid has passed along the entire length of the labyrinthine path 12, and indeed further motor cooling paths, it exits via exit opening 20. The rotor cooling phase of its passage through the motor assembly will now be described with reference to Figure 3.

Figure 3 is a longitudinal cross section through the motor assembly of Figure 2. The motor assembly includes a stator 22 which typically comprises windings (not shown). The stator 22 is arranged within the casing 10 of the motor assembly. Arranged within the motor assembly 2 is a rotor designated generally at 24. The rotor will be described in greater detail below. As can be seen, the rotor comprises magnets 26 arranged around a rotor housing 28. The magnets are preferably permanent magnets which include materials such as dysprosium. The rotor 24 is arranged to rotate due to the interaction of the magnets 28 with the powered windings 22. Bearings 30 and 32 are provided to support rotation of the rotor 24 within the motor assembly. The magnets are

angularly displaced with respect to each other along the length of the rotor housing 24, as will be explained in greater detail below with reference to Figure 7.

The rotor housing 24 has a central shaft of rotation 34. At one end thereof, referred to  
5 herein as the “second end”, splines 36 are provided to enable rotational coupling between the rotor 24 and an output shaft (not shown). Thus, as the rotor 24 is driven due to the varying AC power signal provided to the stator 22, a rotational output can be taken from the motor assembly 2 via the shaft 34 and splines 36. At the other end of the rotor, the “first end”, a bearing journal 78 is provided for supporting the rotation of the  
10 rotor 24. The bearing journal 78 couples fixedly to the rotor housing 28. The bearing journal 78 is described in greater detail below with particular reference to Figure 8.

In Figure 3, the labyrinthine path 12 of the stator can be seen. A connecting region of the path (not shown) is arranged to provide a route from the labyrinthine path 12 to the  
15 inlet to the feed tube of the rotor, as mentioned above with reference to Figure 2A. Furthermore, an outlet 38 is provided through which coolant is routed as it leaves the rotor and connects to the output 20 seen in Figure 2B.

Before describing in greater detail the arrangement of the rotor within the motor  
20 assembly, reference is made to Figures 4 and 7 to 13 which show the rotor in isolation together with a number of its individual components. As shown primarily in Figure 4, the rotor 24 comprises an outer wrap 42. When arranged within the motor, an air gap 43 (see Figure 3) is provided between the outer wrap 42 of the rotor 24 and an inner cylindrical surface of the stator 22. Due to the cooling mechanisms provided and  
25 described herein heat transfer from the rotor to the stator via this air gap is not required.

The rotor 24 comprises an inner wall 44, which in part defines, in this example a cylinder of circular cross-section. Thus, the inner wall 44 may be referred to as a cylindrical housing. This is shown in isolation in Figure 9. It is preferred that the inner wall housing  
30 is cylindrical but other shaped housings can also be used. In this example, the inner cylindrical housing 44 comprises plural external helical ribs 46 which terminate at the ends of the rotor at rib ends 48. The ribs 46 define discrete tortuous channels (in this case helical channels) or fluid paths 50 around the outer cylindrical surface of the inner cylindrical housing 44, defined in part also by the inner cylindrical surface of the rotor



housing 28. In the example shown in Figure 9, four helical ribs 46 are provided, thereby defining four discrete tortuous paths 50 therebetween.

As mentioned above, instead of tortuous paths, the fluid paths 50 could instead be  
5 straight and axially aligned. What matters is that the fluid paths cover a significant proportion of the surface of the inner wall to ensure good thermal engagement therewith and with the magnets which they are arranged primarily to cool. Upon application of power to the stator, e.g. application of a voltage to the stator, the rotor is caused to rotate. A cylindrical inner wall can be provided and the fluid paths guide the coolant on  
10 the surface of the cylindrical body thus ensuring good coverage of the cylindrical body by the coolant. Whatever their configuration, e.g. straight, helical, tortuous etc, it is preferred that the fluid paths cover at least 35% of the surface of the inner wall. More preferably the fluid paths are arranged to cover at least 50% and even more preferably at least 75% of the surface of the inner wall. One convenient way by which such  
15 surface coverage can be achieved is with the use of helical paths which is therefore preferred. It may also be provided that, in use, in any of the embodiments or examples described, the minimum flow rate of fluid within the fluid paths 50 is 0.5m/s. In an alternative the minimum flow rate is set at 1.0m/s or 2m/s.

20 The inner wall 44 forms part of the rotor housing which is preferably hollow (whatever its cross-section) as shown in Figure 4 so as to provide a rotor with low mass and inertia. This reduces the power needed to accelerate or decelerate the rotor. Any desired number of tortuous channels could be provided. In one example there are four provided, whereas in another only a single tortuous channel is provided. The tortuous paths are  
25 shown in the example as being helical in shape. However it will be appreciated that other shapes may be used. For example it could be that the paths flow up and down the rotor similar to the flow paths of fluid in the stator as shown in and described with reference to Figure 2B.

30 Instead of (or as well as) providing ribs in the manner shown, in another example the surface of the inner cylindrical housing is planar with grooves formed in it so as to define the discrete paths for coolant. In both cases, ribs and/or grooves, tortuous paths are provided for the flow of coolant on the surface of the rotor housing. The grooves could be formed by etching or milling the surface of the inner cylindrical housing 44. The cross

sectional area of each of the tortuous paths will depend on each specific application although it is preferred that a range of 20 to 60mm<sup>2</sup> will be used.

- Instead of (or as well as) providing fluid paths 50 in the manner shown on the inner wall 44, ribs or grooves may be formed on the cylindrical inner surface of rotor housing 28, so as to again define tortuous paths 50 on an inner wall of the rotor. It should be borne in mind that, in use, with the rotor rotating, the channels or paths 50 rotate together with other components of the rotor, e.g. the magnets. It is clearly possible to provide the tortuous paths as an integrated part of the component 44, as part of the rotor housing 28, or indeed as a combination of the two. Furthermore, additional components could be provided, such as a cylindrical shell to surround and enclose (from the outside) the inner wall 44 or (from the inside) paths formed in the rotor housing 28. What matters is that one or more tortuous paths are provided on or associated with an inner wall of the rotor.
- 15 The rotor also comprises caps or end members 52 and 54 at opposite axial ends of the inner wall or cylindrical housing 44. The plugs are fixedly engaged with the inner wall 44 such that the caps and inner wall 44 rotate together. The plugs 52 and 54 are shown removed from the inner wall or cylindrical housing 44 in Figures 11 and 13, respectively.
- 20 The rotor 24 has an inlet tube 56 through which coolant enters the rotor. The inlet tube 56 is fixedly and rotationally coupled to the plugs 52 and 54. Therefore, as the rotor rotates in use, the inlet tube 56 rotates with it. The inlet tube 56 is followed by a fluid coupling member 58 (or coolant tube) which receives the fluid from the inlet tube 56. The coupling member 58 is shown in Figure 12. The coupling member 58 serves to connect the rotor caps 52 and 54 and provide a passage for coolant therebetween. The coolant tube 58 has grooves 60 and 62 which, in use, are arranged to receive seals for sealing against fluid leakage. The inlet tube 56 and coupling member 58 may be provided in combination as a unitary component. In combination either as separate components or a unitary component, they may be thought of as the coolant inlet assembly. Furthermore, the coolant inlet assembly together with the caps 52 and 54 may be provided as a unitary component.
- 25
- 30

The coolant tube 58 has a first end arranged to receive the coolant from the inlet tube 56 and a second end 64 arranged to allow the coolant to continue on its passage through

the rotor 24 and motor assembly more generally. At the second end 64 of the coolant tube 58, there are provided openings 66 (Figure 12) through which coolant exits the tube and passes on to the helical paths 50 on the external cylindrical surface of the component 44.

5

In this example, a central inlet tube 40 is provided. The axis or line of rotation of the rotor lies within the inlet tube 40. This means that when fluid is introduced to the rotor it need not have any rotational velocity already as it is at a substantially central axial position. It is preferable that the inlet to the rotor is axially central (or very close to the central axis) so as to minimise the change in velocity, and hence losses, at the entry.

10

As fluid flows down the tube 40 and then into coupling member 58 and in to radial drillings 68 it acquires rotational velocity as it moves radially further from the central axis of rotation along the drillings 68. By the time the fluid reaches the helical paths 50 it is moving rotationally at the same or substantially the same speed as the rotor.

15

As seen in Figure 11, the end cap 54 has a socket 110 arranged to receive the second end 64 of the coolant tube 58. The cap 54 also has radial bores or cross drillings 68 which define radial transmission paths from the second end 64 of the coolant tube 58 to the start of the helical paths 50. The radial bores may be straight or curved but in any event serve to provide one or more conduits from the radially inner region of the device to the radially outer region of the device. In one example, where a double helical path is provided two straight radial bores are provided to define a fluid transmission path from the second end 64 of the coolant tube 58 to the start of the helical paths 50. The number of radial bores is preferably selected to correspond to the number of helical paths 50. In some examples however, described in detail below, the number of helical paths is not the same as the number of radial bores or conduits.

20

25

The cap 54 also has an axial protrusion 115, seen clearly in Figure 3, arranged to be received within the start of the output shaft 72 from the rotor 24. The drillings 68 within the cap 54 terminate in substantially circular openings 74 which provide defined and fixed paths for the coolant from the coolant tube 58 to the helical paths 50.

30

Referring to Figure 9, an example of the inner housing 44 is shown. In this example, the housing 44 is cylindrical and has four discrete helical paths defined thereon. The

housing 44, when arranged in a rotor, is in a fixed angular relationship with the cap 54 such that the openings 74 from the bore or drillings 68 lead into a respective one of the helical paths 50. It is preferred so as to provide for a uniform coating of the coolant on the outer surface of the inner cylindrical housing 44, that at least four discrete helical paths are used. However it will be appreciated that any appropriate number could be used. In one example, three helical paths are used and the angular arrangement of the bores or drillings 68 within the cap 54 provided accordingly.

As seen in Figure 3, referring to the first end of the rotor (i.e. the end to which the inlet tube 56 is connected), an impeller 76 (described in detail with reference to Figure 10) is provided. The impeller is provided coupled to the cap 52 and within a bearing journal 78 for the rotor. The impeller 76 is arranged so as to receive the coolant that has passed through the helical paths 50 along the length of the outer cylindrical surface of the inner cylindrical housing 44. The impeller 76 serves to route the coolant back towards the central axis of the rotor and motor assembly and from there onwards to an output for regeneration. It is to be noted that the impeller is an example of a component or assembly that prevents relative angular rotation between the fluid and rotor parts when the fluid is encouraged to change its radial displacement. Indeed the conduits and/or guide vanes in the impeller both do this.

The impeller thus serves as a mechanism that ensures that the fluid that changes radius is always rotated at the same (or close to same) rotational velocity (or angular velocity or whirl velocity) as the rotor throughout its change in radius, until very close to the radius of the inlet or outlet (depending on the direction of fluid flowing through it).

Indeed, the impeller is a rotating part of the rotor that has conduits for the flow of fluid whereby rotation of the impeller causes rotation of the fluid within it. The fluid does not rotate relative to the impeller, but rotates with the impeller relative to the stator. In other words, the impeller provides a rotating fluid reaction surface and should be construed broadly in this manner. Thus, where there is a radius change for fluid passing through the rotary device, as the fluid passes through the impeller, the impeller can serve to impart or remove rotational energy from the fluid as its radius changes.

Referring to Figure 10, the impeller 76 comprises a frusto-conical housing 80 having radial flanges 82. The radial flanges 82 define openings 84 through which coolant is

arranged to flow from the exits from the helical paths 50 and via conduits 94 within cap 52, described in detail below. The impeller is shaped or provided with one or more grooves 86 to provide a controlled passage for the coolant from the conduits 94, onwards to an appropriate exit from the motor assembly. The function of the impeller is important in embodiments since it provides a controlled and effective manner to bring the coolant fluid back to a position close to the axis of rotation of the motor assembly prior to exit from the motor itself. This is important since it serves to maintain or ensure zero relative circumferential velocity (whirl) between the coolant and the rotor. This minimises pressure losses in the fluid.

Indeed, the impeller 76 functions as a means by which the fluid can increase or decrease its rotational velocity as it moves from a radially outer position, e.g. at the output from radial conduit 94, to a radially inner position at the plenum 38 from which the fluid may be removed from the device. In this example, it is to be noted that the radial distance from the axis of rotation of the inlet tube 58, is less than that of the outlet tube 98, such that the annular region 96 (see Figure 4) which defines the outlet from the rotor is radially further from the axis of rotation than the inlet tube. This is preferable as it ensures that the rotor is substantially self-pumping as the overall force on liquid as the rotor rotates pushes it through the rotor. This is analogous to a conventional gravitational syphon, in which fluid can be moved from a position of high potential energy to a position of lower potential energy even if it involves moving at some point along its journey to the position of lower potential to a position of higher potential energy than the input. In other words, once fluid is flowing along the path from the axial inlet tube 56 to the annular outlet 96 it will continue to flow as long as the rotor operates without requiring external pumping.

It will be appreciated that in general by introducing the fluid to the rotor's rotating frame of reference in a central axial direction will ensure that losses are minimised since there is no sudden rotational acceleration required of the fluid. In general, it is desired that the fluid is at all times in the same rotational frame of reference as whatever conduit it is within. So, for example, as the fluid has travelled along and approaches the end of the coupling member 58 (Figure 3) it will have had some rotation imparted to it due to the rotation of the coupling member 58. The coupling between the coupling member 58 and the radial drillings 68 is such that the fluid then moves into the drillings 68 and, from an

external viewpoint, accelerates rotationally as it passes along the drilling to the start of the helical paths 50. In other words, the fluid at the start of the drillings 68 (close to the end of the coupling member 58) has little if any tangential velocity. As it passes along the length of the drilling its tangential velocity increases (linearly with radius). However, within the drillings it simply moves along in a straight linear direction. This same effect is achieved at the inlet and outlet of the rotor with the use of the impeller 76.

The housing 80 of the impeller, as mentioned above, is preferred to have a generally angled outer surface such as to define a generally frusto-conical form. This enables a smooth deceleration of the coolant as it moves to the centre line velocity whilst avoiding the imparting of whirl to the fluid. The grooves or vanes 86 may be moulded into the body of the impeller and have a desired or appropriate shape. In one example, the vanes are straight. In another example, the vanes are curved such as to provide a gradual change in direction for coolant flowing therethrough. It is preferred that the impeller is a single unitary component with the vanes being an integrated part of it.

Referring again to Figure 3, the passage of the coolant through the motor will now be described. It will be assumed that the fluid has already passed through the stator cooling paths described above such that it is now at a position (23 in Figure 2A) ready to enter the rotor. Initially, the fluid enters via conduit 38 into the inlet 88 along the centre line of the motor assembly. The fluid passes axially along the rotor in the direction A until it reaches the end 90 of the coolant inlet assembly or inlet tube 58. The fluid in this example moves generally along the centreline or rotational axis of the rotor, but could depart from this position as long it generally moves from one end of the rotor to the other. For example, the coupling member could include radial deviations such that it is not simply a straight tube along the centre of the rotor. Overall though the movement of the fluid (and the conduit that carries it) from the input to the rotor to the inlets to the helical paths is axial in that it has a component that is along the axial direction of the rotor. Indeed, the helical paths themselves are axial in this example as they have an axial component for the flow of a coolant between a first end of the rotor and a second distal end of the rotor.

At this point, the fluid flows radially outwardly in the bores or drillings 68. The radial passage of the coolant fluid is aided by rotation of the rotor due to centrifugal forces. At

92 the fluid enters the helical paths and travels back along the helical paths to and for the entire length of the inner cylindrical housing 44, until it reaches openings 93 to radial conduits 94 which guide the fluid into impeller 76 and the vanes 86 therein. From here, the fluid passes along an annular or cylindrical path 96 defined by the outer surface of inlet tube 40 and the inner cylindrical surface of the protrusion 48 of the bearing journal. 5 The coolant then passes into plenum 38 such as to be removed from the motor and regenerated.

As the fluid flows along the tortuous or helical paths 50, it is in close proximity to the 10 bases of the magnets or magnet seats 28 and is thus closely thermally coupled thereto. This provides for efficient heat transfer from the magnets into the fluid.

Referring to Figure 4, the cylindrical or annular output path 96 between the outer surface of the inlet tube 56 and the inner surface of cylindrical projection 98 of the rotor bearing 15 journal 78 can be seen.

As shown in Figures 3 and 4, the fluid paths 50 have cross sections which are in these examples square or rectangular. The inner surfaces of the fluid paths 50, (square or rectangular in cross section in these examples) define what may be referred to as 20 "wetted surfaces". In some embodiments, the paths 50 are formed so as to achieve a certain wetted surface, as compared, say, to the inner surface 51 of the magnets 26. In general it is desired to maximise the wetted surfaces of the fluid paths so as to achieve an optimal amount of heat transfer to the fluid from the rotor. The inner surface 51 of the magnets within the rotor will typically define in cross section a cylinder or prism of 25 some cross-section such as a hexagonal prism, (sometimes staggered along the length of the rotor as in Figure 7). As it is typically the inner surface of the magnets through which heat passes from the stator to the fluid paths 50, the wetted surface area of the paths is in some embodiments formed to be of some size or magnitude with respect to the inner surface 51 of the magnets.

30

Preferably, the total wetted surface area of the fluid paths 50 is at least 35% or more preferably at least 50% of the inner surface area of the magnets or indeed the outer surface area of the wall 28. Preferably, the total wetted surface area is at least 75% of the surface area of the magnets. More preferably, the total wetted surface area is at

least 100% of the surface area of the magnets and most preferably, the total wetted surface area is greater than 100%, e.g. at least 125% or 150%, of the inner surface area 51 of the magnets.

5 Figure 5 shows a further example of the overall passage for fluid through the motor. As can be seen, initially, the coolant enters the rotor from the serpentine path 12 of the stator 22. The fluid passes into the inlet tube 56 along fluid feed conduit or path 100. From here, the fluid passes through the length of the coolant feed tube assembly, out through the bores or drillings 68 within the cap 54, along the helical paths 50, radially  
10 inwardly along guided conduits 52, through the impeller 76 and then through a plenum 104 and out along an output conduit 102.

The materials from which the rotor parts are preferably manufactured include appropriate metals such as steels and Aluminium. For example, the magnet seats 28 and bearing  
15 journal 78 are typically made of steel, whereas the plugs 52 and 54 and rotor cylinder 44 are typically made of Aluminium. The impeller is preferably made of a plastic material. The skilled person would be aware of the materials from which other parts of the rotor and motor assembly could be formed.

20 Figure 6 shows in slightly greater detail the output path for the coolant fluid from the rotor and motor assembly. A plenum 104 is provided which serves as a chamber to receive the fluid from the impeller 76 as described above.

Referring now to Figure 7, the rotor 24 will be described in greater detail.

25 The rotor 24 comprises seats 28 upon which are provided permanent magnets 26 (not shown in Figure 7). The rotor with the seats 28, at any point along the length of rotor, has a hexagonal cross-section. The outer surfaces of the magnets are preferably curved such that once arranged on the seats 28, the outer surface of the rotor is cylindrical, as  
30 seen in Figure 4.

It will be appreciated of course that the outer surface of grooves on the inner cylindrical housing 44 is bounded by the inner surface of the seats 28 defining a part of the rotor housing. The arrangement of the magnet on the rotor is staggered longitudinally as can



be seen in Figure 7. In other words, the substantially flat seats 28 are planar and stagger along the length of the rotor. Looking at Figure 4 for example it can be seen that each set of magnets that forms a ring on the rotor is angularly offset slightly as compared its upstream and/or downstream neighbours. As mentioned above, this  
5 reduces the magnetic-field-induced harmonic distortion in the driving A/C waveform. Indeed, this enables optimal functioning of the rotor within the motor assembly and enables smooth operation thereof in response to the energising of the coils within the stator 22. As the coils within the stator are energised by the application of AC power in a known manner, the interaction between the magnetic field thus generated and the  
10 permanent magnet, causes the rotor to rotate.

The output member 34 of the rotor can be seen clearly together with grooves 106. The grooves 106 serve to house one or more seals for the rotor within the motor assembly.

15 Figure 8 shows the bearing journal for the rotor. The bearing journal 78 includes grooves 108 which, again, are preferably used for one or more seals. The bearing journal is arranged within bearings 30 which serve to control the positioning of the rotor within the motor assembly. Referring to both Figures 3 and 8, the bearing journal will now be described in greater detail. The bearing journal comprises on one axial side, the  
20 projection 98 described above which helps to define the outlet path for the coolant from the rotor. On its other axial side there is provided a cylindrical projection 61 which has an internal region 59 of generally frusto-conical form. The internal region is sized and shaped to correspond with the outer surface of the impeller 76 such as to define, together with the grooves 86 in the impeller the paths for the coolant from the radial  
25 grooves 94 of the rotor cap 52, described below.

The bearing journal also includes an annular flange 99 having notches 109. The flange and notches provide means by which the bearing journal 78 may be fixedly coupled to the wall 28 of the rotor. Figure 3 shows how the wall 28 may be provided with recesses  
30 55 for receiving fixing elements (not shown) such as screws or rivets. As well as or instead of the notches, appropriately sized holes could be provided in the flange to receive the fixing elements.

Figures 11 and 13 show the rotor caps 52 and 54, respectively. Referring to Figure 11, the rotor cap 54 is shown which would in use be arranged at the second distal end of the rotor, i.e. the end through which fluid leaves the inlet tube 58. The rotor cap 54 includes cross drillings 68 which define the radial conduits through which the fluid passes as it moves from the inlet tube 58 to the helical paths 50. Flats 112 are provided which are preferably used to ensure that the cross drillings 68 align with the openings 66 in the distal end of the inlet tube 58. A circular rim 111 is provided which is sized to engage with the inner cylindrical surface of the cylindrical housing component 44. In addition an annular ring flat 113 is provided which engages the annular end surface 109 (see Figures 6 and 9) of the cylindrical housing component 44. An axial tubular boss 110 is provided which is sized and arranged to receive within it the end of the inlet tube 58, such that coolant that passes along the inlet tube 58 is routed through the openings 66 and onwards into the cross drillings 68. Toroidal grooves 115 and 117 (shown in Figure 3) are provided which serve to reduce the weight and inertia of the rotor cap 54 without affecting its function in other ways.

Next, referring to Figure 13, the rotor cap 52 arranged in use at the first end of the rotor will now be described in detail. As described above, the rotor cap 52 is arranged to support the impeller 76. The cap 52, comprises an axial projection 70 on which is mounted the impeller 76. In addition on the opposite axial surface of the cap 52 there is provided a cylindrical boss 57. The boss 57 has a cylindrical recess 67 sized to receive the first end of the inlet tube 58. The cylindrical recess 67 has an inner shoulder 69 which engages the end axial toroidal surface of the inlet tube 58. The projection 70 is hollow and in combination with the inlet tube 58 engaged with the shoulder 69, provides a substantially continuous conduit for coolant as it passes into the motor.

Radial grooves 94 (seen most clearly in Figure 14) provide a route for the coolant received from the helical paths 50 through the cap 52 and onwards into the impeller 76. As seen in Figure 13 and 14 circular opening 93 are provided as the inlets to the radial grooves 94. The number of grooves is selected to correspond to the number of helical paths 50 provided on the cylindrical housing component 44. Accordingly in almost all cases the number of radial grooves in the two caps 52 and 54 will be the same so as to correspond to the number of helical paths on the cylindrical housing component 44. The radial grooves are preferably straight grooves of circular cross section arranged in a

radial direction. However, in some examples, the grooves could be curved. This is seen in Figure 6 for example which shows curved grooves 94 in the caps 52 and 54. Either or both of the caps 52 and 54 could be provided with straight and/or curved radial grooves, but in all cases the grooves route fluid between a circumferential area of maximum  
5 radius and an inner central region of smaller radius.

Figures 14 and 15 show further examples of rotors for use in a motor assembly. Figure 14 shows a further example of a rotor for use in a motor assembly. As can be seen, again, a cylindrical housing component 44 is provided with end caps 52 and 54. An  
10 impeller 76 is provided between the end cap 52 and the rotor journal bearing 78. In this example, the end cap 54 includes a longitudinal drilling 114 as well as the axial cross drillings 68, described above. Thus, as fluid exits the inlet tube 58 it passes into the drillings within the cap 54 before exiting radially towards the helical paths 50 as described above. In other respects, the operation and function of the rotor will be as  
15 described above, with reference to, e.g., Figures 3 and 4. Figures 14 and 15 show clearly the fluid inlets and outlets from the rotor. As can be seen, the fluid outlet is at a larger radius than the fluid thus enabling the rotor to self-pump as a result of the centrifugal forces imparted to the fluid by rotation of the rotor.

Figure 15 shows a further embodiment. In this example, the inlet tube 58 continues into a recess 116 within the cap 54. Openings 118 are provided in the tube 58 to align with the inputs 120 to the cross drillings 68. Preferably, the openings are simple drillings within the inlet tube to allow the coolant fluid to exit radially or from the side of the inlet instead of from the end face. In other respects, the operation and arrangement of the  
20 rotor is as described above with reference to other of the figures.

Figure 16 shows a schematic representation of one example of an inlet tube seal that is preferably used at the fluid input to the motor assembly.

As can be seen, the inlet tube 56 is coupled to the plenum housing 122 via an energised face seal 124. A sealing member 126 is provided around the input to the tube 56. The sealing member is preferably formed of a low friction material such as PTFE and is provided in the form of a "top hat". The bore of the PTFE seal 124 is transition fit onto the inlet tube 56. The PTFE seal 124 has a tight fit to the inlet tube and a loose fit to the  
30

housing and is designed to seal effectively against the perpendicular face of the stationary housing 122. This permits good sealing despite any “wobble” or run-out in the shaft.

- 5 The use of the arrangement described herein enables peak component temperatures within the stator to be limited to approximately 200 degrees Centigrade. In particular examples, the component temperatures of the stator are limited to 207 degrees Centigrade. The rotor cooling, using the disclosed examples, is able to limit the peak component temperatures of the rotor wrap to within the range 160 to 210 degrees
- 10 Centigrade. Furthermore, due to the use of appropriate seals and configuration of flow paths, together with the impeller described above, the overall motor system pressure drop is limited to 0.5 or 0.4 bar, given an overall flow rate of 15 litres per minute, sufficient to cool a motor of output greater than 100kW and total package volume of 8 litres. The system is able to hold coolant without leaks at greater than 3.5 bar gauge inlet
- 15 pressure.

- The overall pressure of fluid within the outboard extremities of the rotor is dominated by the centrifugal pressure (proportional to the square of rotational speed). In one non-limiting example, this centrifugal pressure contributes an additional 17 bar when the
- 20 frequency of rotation is 18,000 rpm and the rotor flow paths are at a radius of 30mm. It is envisaged that in future using the rotor and cooling described herein speeds of up to 25,000rpm could be achieved.

- Using the described assembly, the high fluid velocity is attainable which therefore
- 25 enables good heat transfer to the coolant. This is because a higher flow rate or fluid velocity ensures that the resident time of fluid within the motor is correspondingly small. This in turn means that the fluid is continually replenished with fresh cool fluid and therefore able to receiver a higher amount of heat in unit time as well as increasing the heat transfer coefficient. Accordingly high amounts of cooling can be achieved. In one
- 30 example, more than 50% of the rotor heat has been removed using the cooling mechanism and methods described herein. Using thermochromic paint it has been determined that the rotor temperature in a motor of 8 litres overall package volume was less than 50 degrees centigrade above the coolant temperature after 10 minutes of motor operation at a power of 110 kW.

The use of the impeller also enables minimal pressure losses which therefore avoids the need for a high pressure coolant pump and complex sealing systems. Importantly, the coolant is close to the source of the heat and therefore provides for good heat transfer therefrom. Furthermore, the use of plural helical paths ensures uniform coverage of hot parts of the rotor, again, ensuring good heat transfer capability.

Last, due to the substantially hollow nature of the rotor assembly, the rotor inertia is minimised.

The disclosed embodiment would typically be used with an ethylene-glycol and water mixture, although other coolants may also be used. All or part of the coolant passes through the rotor cooling system. The coolant enters and leaves the rotor close to the rotor axis, as described above. As mentioned above, the outlet, although close to the rotor axis is at a larger radius than the inlet thus enabling the self-pumping nature of the rotor to be realised. It is preferred that, as in the enclosed embodiments, the coolant enters and leaves the rotor at the same longitudinal or axial end of the rotor. This enables a simple connection to the vehicle transmission at the other end of the rotor. In other words, since no conduits for coolant fluid need to be provided at the distal end of the rotor, the output can lead directly to an output shaft without the need to provide any fluid conduits and or corresponding seals.

A rotating sealing system is provided which prevents fluid entering the rotor cavity in the stator. This prevents fluid sheer friction losses and heat generation. A further rotating sealing system may be provided to separate inlet and outlet fluids mixing. This maximises the effectiveness of the system. It is to be noted that the cooling heat transfer occurs in the zone at significantly larger radius than the inlet and outlets. In other words, since the cooling takes place on the outer cylindrical surface of the inner cylindrical housing 44, this is at a significant radial distance from the axis of the rotor. This ensures good heat transfer (since the heat transfer is at the source of the heat) but also minimum rotor mass and inertia due to the hollow nature of the inner cylindrical housing 44.

As explained above with reference to the impeller, where radius changes are required in the cooling path, fixed barriers or drillings (i.e. the impeller) are used to maintain or guarantee zero relative circumferential velocity (whirl) between the coolant and the rotor. This minimises pressure losses in the fluid and thus obviates the need for a high  
5 pressure pump to force the coolant through the motor. In addition, a multi-start helical path for the coolant in the heat transfer zone is provided. This ensures high fluid velocity and even and substantially uniform fluid distribution. Furthermore, the component parts of the rotor housing can be made to normal manufacturing tolerances. Last, a sealed air filled cavity is provided under the heat transfer zone which minimises rotor inertia.

10 Referring again to Figures 3 to 5, in one example the cooling liquid is provided so as to flow in the opposite direction as previously described. In other words, initially, the cooling fluid passes along the annular or cylindrical path 96 defined by the outer surface of inlet tube 40 and the inner cylindrical surface of the protrusion 48 of the bearing  
15 journal. From here the fluid flows through the impeller 76 guided by the vanes 86. It then flows on to the radial conduits 94 which guide the fluid to the start of the helical path or paths around the rotor. The fluid passes along the entire length of the inner cylindrical housing 44 and eventually reaches the one or more radial drillings or bores 68 along which it flows radially inwardly to reach the conduit 58, referred to above as the "inlet  
20 tube". In this example it may be considered an "outlet tube". The fluid passes along the length of the tube 58 from the distal end towards the proximal end where it can be fed out of the device. Thus the fluid path is substantially opposite to that described above where the fluid enters the assembly via the inlet tube 58. In either usage, it may be that a pump is provided to provide additional or sufficient fluid pressure to drive the fluid in  
25 the manner described.

As described above, the radial bores may be straight or curved but in this case serve to provide one or more conduits from the radially outer region of the device to the radially inner region of the device. In one example, where a double helical path is provided two  
30 straight radial bores are provided to define a transmission path to the second end 64 of the coolant tube 58 from the end of the helical paths 50. The number of radial bores is preferably selected to correspond to the number of helical paths 50.

Figure 17 is a schematic representation of an example of a further embodiment of a rotor 138 for use in a motor.

The rotor is generally similar to that described above with reference to, for example,  
5 Figures 3 to 6. The rotor has three general sections, which are the first end section 131, the central section 133 and the second end section 135. The first and second end sections 131 and 135 generally include journal parts for engagement with rotor bearings within a motor or other rotary device. The first and second end sections 131 and 135 include a number of journal surfaces for engagement with bearings within a rotary device  
10 such as a motor or generator. For example, first end section 131 comprises generally cylindrical bearing journal 123 for engagement with a bearing (not shown). A number of annular grooves 127 are provided within which seals such as O-rings and the like will be provided to avoid or reduce fluid leakage.

15 In the example shown, the tortuous paths are defined by double helixes 130. The helixes are "double" in that a single feed inlet 132 feeds two parallel connected paths or branches 134 and 136. Liquid enters the double helix via the inlet 132 and passes along both branches 134 and 136 of the helix. By providing a helix with two parallel branches 134 and 136, increased surface coverage can be achieved for the rotor, without  
20 increasing the number of inlets correspondingly. Thus, for each of the double helixes 130 only a single inlet 132 is required. In addition, increased surface coverage can be achieved without reducing the helix angle which could slow down passage of the liquid along the tortuous paths. Return inlets 150 are provided at the second end of the central section 133 of the rotor, to receive fluid from the helical paths and direct it back through  
25 the rotor towards fluid outlets 148 in the first end section 131 described in detail below.

Figures 23 and 24 show in more detail a part longitudinal section through the first end section 131 of the rotor. A number of feed conduits 140 are provided through which a cooling liquid is fed into the rotor. The feed conduits 140 comprise parallel axial sections  
30 142 and subsequently radial sections 144 along which the fluid flows so as to reach the inlets 132 to the helical paths 130. Figure 23 shows clearly a single inlet 132 feeding two branches 134 and 136 of helical path 130. Inlets 146 to the axial sections 142 of feed conduits 140 are provided at an axial end of the rotor. In use, once liquid is fed into the rotor it will pass along the feed conduits and then along the helical paths towards the

second end section 135 of the rotor. Once there, it passes through return ports and conduits as will now be described with reference, in particular, to Figures 17, 18, 20, 24 and 26.

5 Referring to Figures 17, 18, 20 and 24, return ports 148 are provided which serve as an outlet for cooling liquid that has passed through the rotor. Cooling liquid that has passed along the helical paths 134 and 136 reaches the end of the central section 133 close to the second end 135 of the rotor and then commences its passage back towards the first end section 131.

10

Passage of the fluid through the rotor is thus as follows. Fluid is introduced via the feed conduits 140. The fluid then passes along the radial sections 144 (Figures 22 and 23) of the feed conduits 140 and on to the helical path inlets 132. From here, the fluid passes along the double helical paths 130 until it reaches the distal end of the rotor, i.e. the part of the central section 133 closest to the second end section 135. At this point, the fluid passes into return inlets 150. Radial inlet tubes or drillings 152 (Figure 21) are provided to route fluid from the return inlets 150 into one or more axial return paths 154 (see Figure 26). The radial inlet tubes or drillings are formed within the body of the rotor and again, as with the feed conduits 140, any appropriate number can be provided. Typically the number will be the same as the number of helical paths. However, where double helixes are provided as in the example shown in Figure 17, half the number of radial inlet tubes 152 will be provided. The inlet tubes 152 are arranged so as to lead to the inlets of the axial return paths 154. The inlet tubes, in the example shown are straight but as with the radial conduits 68 described above, they may be curved. It is simply required that they provide a generally radial path for the liquid to move from the helical paths to the axial return paths 154. Thus, in one example they have a generally spiral configuration leading from the inlets 150 to the axial return paths 154.

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The fluid then flows generally axially along axial return paths 154 until it reaches return ports or outlet openings 148, seen clearly in Figure 24. Thus, it will be appreciated that the flow of cooling liquid is similar to the embodiment described above with reference to Figures 1 to 16.



As shown in Figures 17 and 20 in particular, an impeller 156 is provided. The impeller 156 is coupled to the rotor and rotates with it. It serves to provide rotational velocity to the cooling liquid prior to its introduction to the feed conduits 140. It will be appreciated that in contrast to the example of, say, Figure 3, the inlets to the impeller 158 are not on the central axis of rotation of the rotor and, as the impeller will be rotating with the rest of the rotor at high rotational speeds, its inputs will be moving at some significant tangential velocity. So as ensure that fluid that enters is in the same or similar rotational frame of reference, some means such as fluid jets may be provided to impart tangential velocity to the fluid before it enters the impeller. This is described in more detail below with reference to Figures 27 and 28.

The impeller 156 has curved inlet paths 158 shown most clearly in Figure 20. Jets or inlets 157 for jets (see Figure 27) may be provided to supply the liquid to the impeller 156. The jets 157 serve to provide the liquid with some tangential (as well as axial) velocity. The blade angle of the impeller curved surfaces 158 is shallow, thus reducing or minimising losses in fluid pressure whilst still imparting desired rotational or velocity to the liquid as it passes into the rotor.

Figure 24 is a schematic representation of an impeller 156 and coupling spigots for a rotor such as that shown in Figure 17, all arranged generally at the first end section 131 of the rotor. The impeller 156 comprises impeller inlet paths 159 through which liquid passes as it enters the rotor. To ensure accurate alignment between the impeller inlet paths 159 and the axial feed conduits 140 (not shown in Figure 24) a plurality of spigots 161 are provided which engage with corresponding openings 163 in the rotor body, seen clearly in Figures 18 and 23. In this example 4 spigots 161 are provided. The spigots 161 also form end faces to close off the axial return paths 154. Thus once fluid has reached the end of axial return paths 154 it is forced out of the return ports or outlet openings 148 via engagement with the end faces of the spigots 161.

The embodiment of Figures 17 to 28 operates in a manner substantially similar to that of the embodiment described above with reference to Figures 1 to 16 and so further description will not be provided. In particular it will be appreciated that various seals and bearings are provided to enable the rotor to operate within a rotary device such as a motor or generator. These aspects will not be described in detail again.

Figures 29 to 37 show an example of a further embodiment of the rotor.

The example of Figures 29 to 37 is similar to the embodiment of Figures 1 to 17. The  
5 inlet and outlet paths, by which fluid is introduced to and removed from the rotor, are substantially parallel and co-axial with the rotor. Referring to Figure 29, a central inlet conduit 160 is provided. The outlet for the fluid that has passed through the rotor 162 is along the annular pathway surrounding the inlet conduit 160. As above, the rotor has  
10 three general sections, which are the first end section 131, the central section 133 and the second end section 135. The first and section end sections 131 and 135 generally include journal parts for engagement with rotor bearings within a motor or other rotary device and/or appropriate seals and the like.

The rotor of Figures 29 to 31 is similar to that of Figure 17 in that double helixes 164 are  
15 provided. In this example though, the inlet 166 to the helix is at the distal end of the rotor, i.e. at the end closest to the second end section 135. The fluid thus passes along the central conduit 160 until it passes radially outwards to the inlets 166. Then the fluid is forced along the helical paths 164 until it reaches the outlets 168 from the helical paths. Here, the fluid flows along radial conduits 170 and into the annular outlet path  
20 172. Figure 30 shows a section through the shaft assembly in which the central conduit 174 can be seen along which fluid is communicated to radial conduits 176 and subsequently to inlets 166.

In Figure 31 the helical paths 164 can be seen clearly terminating at outlets 168 from the  
25 helical paths leading into the radial conduits 170. Figure 32 is an end-on transverse section through the rotor showing the outlets 168 from the helical paths (also the inlets to the radial conduits 170).

Figure 33 is a schematic representation of a section through the liquid inlet-outlet  
30 manifold and Figure 34 is a schematic representation of a section through a rotor including the liquid inlet-outlet manifold of Figure 33. As can be seen, the inlet conduit 160 is able to receive coolant liquid from its open end 178. The liquid flows along inlet conduit 160 in the direction B and into the central conduit 180. Once the liquid has passed along the helical paths along the outer surface of the rotor, it returns along the

radial inlet conduits 170 seen most clearly in Figure 36. At this point, the liquid enters the annular outlet conduit and from here is removed from the assembly. As in the example above in, amongst others, Figure 3, the outlet is radially further from the axis of rotation than the fluid inlet to the rotor so that the device is self-pumping and again acts analogously to a gravitational syphon.

The inlet conduit 160, in this example, functions as the impeller since liquid fed into it will be imparted with rotational velocity as well as axial velocity. In other words, again the impeller thus serves as a mechanism that ensures fluid that enters it is rotated at the same (or close to same) rotational velocity (or angular velocity or whirl velocity) as the rotor. The inlet conduit or impeller 160 is a rotating part of the rotor that has a central axial conduit for the flow of fluid whereby rotation of the impeller causes rotation of the fluid within it.

Figure 35 shows a section through the coolant inlet port 166 to the helical paths on the rotor. Coolant received via the central conduit 180 passes along the radial conduits 176, to one of the corresponding inlets 166 and then into the helical paths 164. Various seals and the like may be provided as required to ensure efficient operation of the device. In the example of Figure 35, a seal groove 182 is provided which may receive an O-ring. The O-ring, like all other O-rings provided for operation with the rotor may be formed of an appropriate material, e.g. a rubber or elastomeric material.

Figures 36 and 37 show schematic cross sections through a part of the shaft assembly showing the liquid or coolant inlet and outlet parts. Initially, coolant is provided via inlet region 184. From there, the coolant flows in through the inlet conduit 160 and onwards through the rotor as described above. On its return, once the fluid has passed along the helical or tortuous paths described above, it passes through ports 168 and along the radial conduits 170 and from there into annular outlet 172. Then the coolant flows into radial outlet conduits 186 and subsequently to outlet 188. Again, as above, various seals 190 are provided to determine fluid flow and stop unwanted leakage.

Embodiments of the present invention have been described with particular reference to the examples illustrated. However, it will be appreciated that variations and

modifications may be made to the examples described within the scope of the present invention.

## Claims

1. A rotary device, comprising:

a stator for receiving or outputting electrical power;

5 a rotor arranged coaxially within the stator and having one or more magnets arranged thereon,

the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a conduit having an axial component for the flow of a coolant between a first end of the rotor and a second  
10 distal end of the rotor; the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the conduit having an axial component and arranged in use to receive coolant from or provide coolant to the conduit having an axial component, the inner wall having one or more fluid paths for the flow of coolant, thereby to cool the rotor;

15 at least one fluid impeller arranged at the first and/or distal end of rotor and arranged to rotate with the rotor and impart to and/or maintain rotary movement of or remove from and/or maintain rotary movement of fluid entering or leaving the rotary device.

20 2. A rotary device according to claim 1, comprising a fluid inlet to the rotary device and a fluid outlet from the rotary device, wherein the fluid outlet is at a greater radius than the fluid inlet.

25 3. A rotary device according to claim 1 or 2, in which the fluid paths of the inner wall are tortuous paths.

4. A rotary device according to any of claims 1 to 3, in which the impeller is arranged to guide the fluid towards the rotor axis for removal from the motor or radially outwardly towards the one or more tortuous paths.

30 5. A rotary device according any of claims 1 to 4, in which the coolant enters and leaves the rotor at the same axial end thereof.

6. A rotary device according to any of claims 1 to 5, in which the coolant enters and leaves the rotor axially.

7. A rotary device according to any of claims 1 to 6, in which the coolant enters the  
5 rotor axially and leaves the rotor radially.

8. A rotary device according to any of claims 1 to 7, in which the coolant enters the rotor radially and leaves the rotor axially.

10 9. A rotary device according to any of claims 1 to 8, in which the stator has a labyrinthine path defined therein for the flow of coolant fluid.

10. A rotary device according to any of claims 1 to 9, in which the magnets are staggered or rotationally offset varying with axial displacement along rotor.

15

11. A rotary device according to claim 1 to 10, in which the impeller is a unitary moulded component having guide ribs to guide coolant.

12. A rotary device according to claim 11, in which the impeller ribs are curved.

20

13. A rotary device according to claim 12, in which the impeller ribs are curved with varying curvature.

14. A rotary device according to claim 11, in which the impeller ribs are straight.

25

15. A motor for providing rotary power, the motor comprising:  
a stator for receiving electrical power;  
a rotor arranged coaxially within the stator and having one or more magnets arranged thereon so that in response to the stator receiving the electrical power, the  
30 rotor is caused to rotate,

the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant between a first end of the rotor and a second distal end of the rotor;

the rotor further comprising one or more radial fluid conduits at the second distal end of the rotor, the conduits being fluidly coupled to the central fluid conduit and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant, thereby to cool the rotor.

5

16. A motor according to claim 15, in which the tortuous paths are defined by guide ribs on or grooves in the inner wall.

17. A motor according to claim 16, in which the ribs or grooves are helical.

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18. A motor according to claim 17, in which angle of helical ribs or grooves is within a certain range.

15

19. A motor according to any of claims 15 to 18, in which inner wall is cylindrical such that the rotor housing is hollow.

20. A motor according to any of claims 15 to 19, comprising a fluid inlet and a fluid outlet, wherein the fluid outlet is at a greater radius than the fluid inlet.

20

21. A motor according to any of claims 15 to 20, in which the number of ribs or grooves is the same as the number of radial fluid conduits.

22. A motor according to claim 21, in which the number of ribs or grooves is 4.

25

23. A motor according to any of claims 15 to 22, in which the one or more radial conduits is or are formed as drillings or bores in an end cap fixedly mounted to the inner wall.

30

24. A motor according to any of claims 15 to 23, in which the central fluid conduit and the one or more radial fluid conduits are formed as a unitary component.

25. A motor according to claim 22 or 23, in which the one or more radial fluid conduits is or are curved.

26. A motor according to any of claims 15 to 25, in which the central fluid conduit acts as a rotor shaft and has a first end mounted in a bearing at a first end of rotor and second end mounted in a bearing at a second distal end of the rotor.

5 27. A motor according to claim 19, in which the hollow cylinder comprises a sealed air-filled cavity under a heat transfer zone within the motor.

28. A motor according to any of claims 15 to 27, further comprising a fluid impeller arranged at the first end of rotor to receive coolant from or provide coolant to the spiral  
10 ribs and guide the fluid towards the rotor axis for removal from the motor or radially outwardly towards the spiral ribs.

29. A motor according to claim 27, in which the impeller is a unitary moulded component having guide ribs to guide coolant.

15

30. A motor according to claim 28 or 29, in which the impeller ribs are curved.

31. A motor according to claim 30, in which the impeller ribs are curved with varying curvature.

20

32. A motor according to claim 28 or 29, in which the impeller ribs are straight.

33. A motor according any of claims 28 to 32, in which the coolant enters and leaves the rotor at the same axial end thereof.

25

34. A motor according to claim 33, in which the coolant enters and leaves the rotor axially.

30

35. A motor according to claim 34, in which the coolant enters the rotor axially and leaves the rotor radially.

36. A motor according to claim 34, in which the coolant enters the rotor radially and leaves the rotor axially.



37. A motor according to any of claims 15 to 36, in which the stator has a labyrinthine path defined therein for the flow of coolant fluid.

38. A motor according to any of claims 15 to 38, in which the magnets are staggered  
5 or rotationally offset varying with axial displacement along rotor.

39. An electricity generator, comprising:  
a stator having electrical contacts for outputting generated power;  
a rotor arranged coaxially within the stator and having one or more magnets  
10 arranged thereon, the rotor having a drive input for receiving a rotary input so that in response to the rotor being driven, electrical power is generated in the stator;  
the rotor comprising a housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant between a first end of the rotor and a second distal end of the  
15 rotor;  
the rotor further comprising radial fluid conduits at the second distal end of the rotor, fluidly coupled to the central fluid conduit and arranged in use to receive coolant from or provide fluid to the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant, thereby to cool the rotor.

20 40. A method of cooling a rotor in a motor for generating rotary power, the method comprising:

in a motor having a stator for receiving electrical power, a rotor arranged coaxially within the stator and having one or more magnets arranged thereon,  
25 providing the rotor with a cylindrical rotor housing having an inner wall, the magnets arranged around the housing, and also providing the rotor with a central fluid conduit for the flow of a coolant axially between a first input end of the rotor and a second distal end of the rotor; and providing the rotor with one or more radial fluid conduits at the second distal end of the rotor, fluidly coupled to the central fluid conduit  
30 and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant, thereby to cool the rotor.

41. A method according to claim 40, comprising providing coolant to the central fluid conduit such that the coolant is caused to flow into the radial conduits and along the tortuous paths to cool the rotor.

5 42. A motor for providing rotary power, the motor comprising:  
a stator for receiving electrical power;

a rotor arranged coaxially within the stator and having one or more magnets arranged thereon so that in response to the stator receiving the electrical power, the rotor is caused to rotate,

10 the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor;

the rotor further comprising one or more radial fluid conduits at the second distal  
15 end of the rotor, the conduits being fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.

20 43. A motor according to claim 42, in which the tortuous paths are defined by guide ribs on or grooves in the inner wall.

44. A motor according to claim 43, in which the ribs or grooves are helical.

25 45. A motor according to claim 44, in which angle of helical ribs or grooves is within a certain range.

46. A motor according to any of claims 42 to 45, in which inner wall is cylindrical such that the rotor housing is hollow.

30

47. A motor according to any of claims 42 to 46, comprising a fluid inlet and a fluid outlet, wherein the fluid outlet is at a greater radius than the fluid inlet..

48. A motor according to any of claims 42 to 47, in which the number of ribs or grooves is the same as the number of radial fluid conduits.

49. A motor according to claim 48, in which the number of ribs or grooves is 4.

5

50. A motor according to any of claims 42 to 49, in which the radial conduits are formed as drillings or bores in an end cap fixedly mounted to the inner wall.

51. A motor according to any of claims 42 to 50, in which the central fluid conduit and radial fluid conduits are formed as a unitary component.

10

52. A motor according to any of claims 42 to 51, in which the central fluid conduit acts as a rotor shaft and has a first end mounted in a bearing at a first end of rotor and second end mounted in a bearing at a second distal end of the rotor.

15

53. A motor according to claim 46, in which the hollow cylinder comprises a sealed air-filled cavity under a heat transfer zone within the motor.

54. A motor according to any of claims 42 to 53, further comprising a fluid impeller arranged at first end of rotor to receive coolant from the spiral ribs and guide the fluid towards the rotor axis for removal from the motor.

20

55. A motor according to claim 54, in which the impeller is a unitary moulded component having guide ribs to guide coolant.

25

56. A motor according to claim 54 or 55, in which the impeller ribs are curved.

57. A motor according to claim 56, in which the impeller ribs are curved with varying curvature.

30

58. A motor according to any of claims 42 to 57, in which the stator has a labyrinthine path defined therein for the flow of coolant fluid.

59. A motor according to any of claims 42 to 58, in which the magnets are staggered or rotationally offset varying with axial displacement along rotor.

60. An electricity generator, comprising:

5 a stator having electrical contacts for outputting generated power;

a rotor arranged coaxially within the stator and having one or more magnets arranged thereon, the rotor having a drive input for receiving a rotary input so that in response to the rotor being driven, electrical power is generated in the stator;

10 the rotor comprising a housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second distal end of the rotor;

15 the rotor further comprising radial fluid conduits at the second distal end of the rotor, fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.

61. A method of cooling a rotor in a motor for generating rotary power, the method comprising:

20 in a motor having a stator for receiving electrical power, a rotor arranged coaxially within the stator and having one or more magnets arranged thereon,

providing the rotor with a cylindrical rotor housing having an inner wall, the magnets arranged around the housing, and also providing the rotor with a central fluid conduit for the flow of a coolant from a first input end of the rotor axially to a second  
25 distal end of the rotor; and providing the rotor with one or more radial fluid conduits at the second distal end of the rotor, fluidly coupled to the central fluid conduit and arranged in use to receive coolant from the central fluid conduit, the inner wall having tortuous guide ribs to define plural tortuous paths for the flow of coolant from the second distal end to the first input end, thereby to cool the rotor.

30

62. A method according to claim 61, comprising providing coolant to the central fluid conduit such that the coolant is caused to flow into the radial conduits and along the tortuous paths to cool the rotor.

63. A rotary device, comprising:

a stator for receiving or outputting electrical power;

a rotor arranged coaxially within the stator and having one or more magnets arranged thereon,

5 the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises a central fluid conduit for the axial flow of a coolant between a first end of the rotor and a second distal end of the rotor;

10 the rotor further comprising one or more radial fluid conduits at the second distal end of the rotor, the conduits being fluidly coupled to the central fluid conduit and arranged in use to receive coolant from or provide coolant to the central fluid conduit, the inner wall having plural tortuous paths for the flow of coolant, thereby to cool the rotor.

64. A rotary device, comprising:

15 a stator for receiving or outputting electrical power;

a rotor arranged coaxially within the stator and having one or more magnets arranged thereon,

20 the rotor comprising a rotor housing having an inner wall, the magnets being arranged around the housing, and wherein the rotor also comprises an axial fluid conduit for the flow of a coolant between a first end of the rotor and a second distal end of the rotor;

25 the rotor further comprising one or more radial fluid conduits, the radial fluid conduits being fluidly coupled to the axial fluid conduit and arranged in use to receive coolant from or provide coolant to the axial fluid conduit, the inner wall having one or more fluid paths for the flow of coolant, thereby to cool the rotor,

the fluid paths having internal surfaces that are in use, wetted by the flow of cooling fluid thereby defining a wetted surface area, wherein the total wetted surface area is at least 35% of the inner surface area of the magnets.

30 65. A rotary device according to claim 64, wherein the total wetted surface area is at least 50% of the inner surface area of the magnets.

66. A rotary device according to claim 65, wherein the total wetted surface area is at least 100% of the inner surface area of the magnets.

67. A rotary device according to claim 66, wherein the total wetted surface area is greater than the inner surface area of the magnets.

5 68. A rotary device according to any of claims 64 to 67, in which further comprising a fluid impeller arranged at the first or distal end of rotor and arranged to rotate with the rotor and impart rotary movement to or remove rotary movement from fluid entering or leaving the rotary device.

10 69. A motor substantially as shown in and or described with reference to any one or more of Figures 1 to 37 of the accompanying drawings.

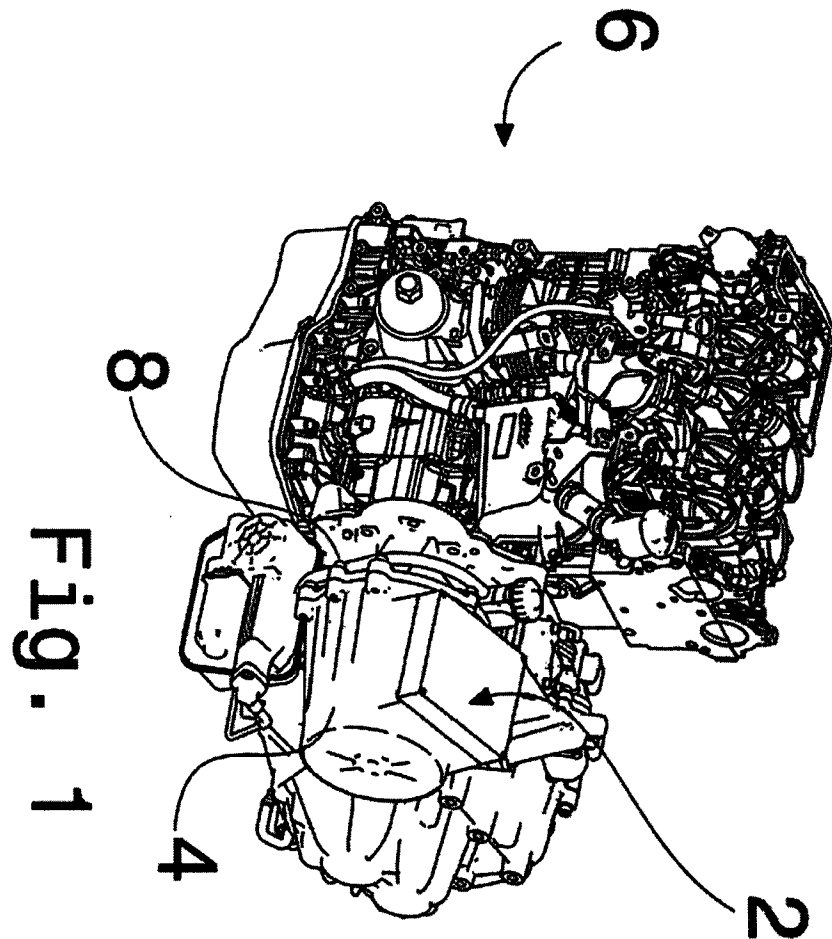
70. A generator substantially as shown in and or described with reference to any one or more of Figures 1 to 37 of the accompanying drawings.

15

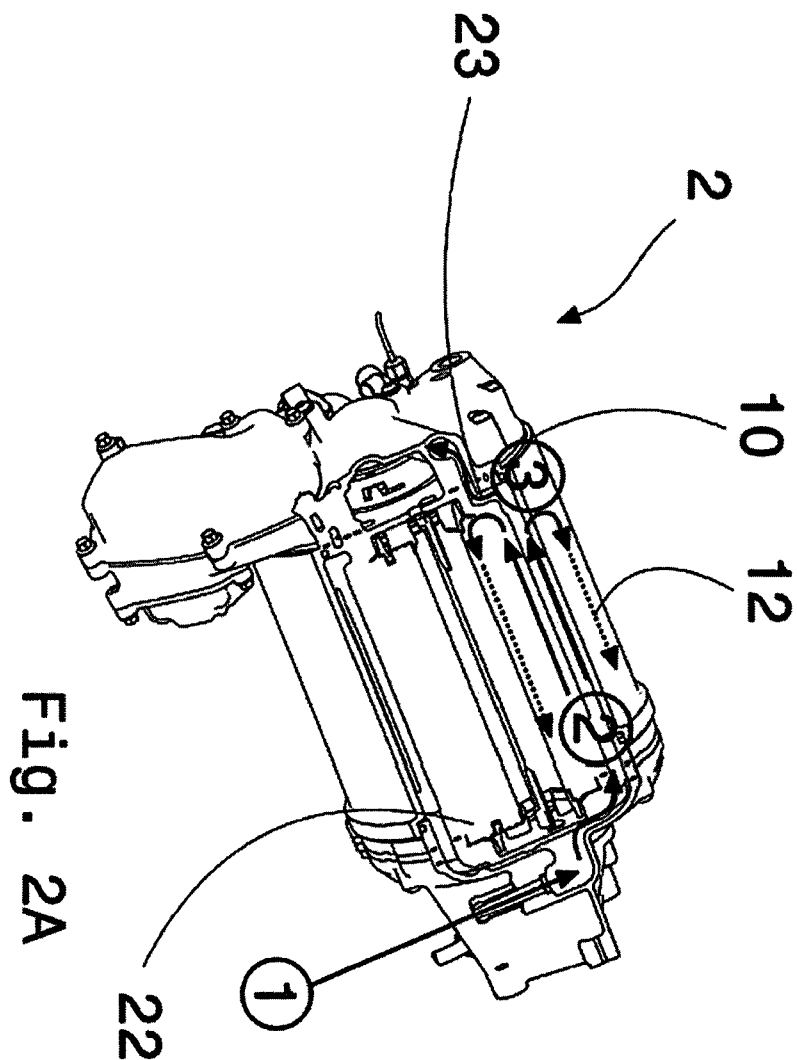
71. A method of cooling a rotor in a motor for generating rotary power, the method being substantially as shown in and or described with reference to any one or more of Figures 1 to 37 of the accompanying drawings.

20 72. A method of cooling an electricity generator or rotary device, the method being substantially as shown in and or described with reference to any one or more of Figures 1 to 37 of the accompanying drawings.

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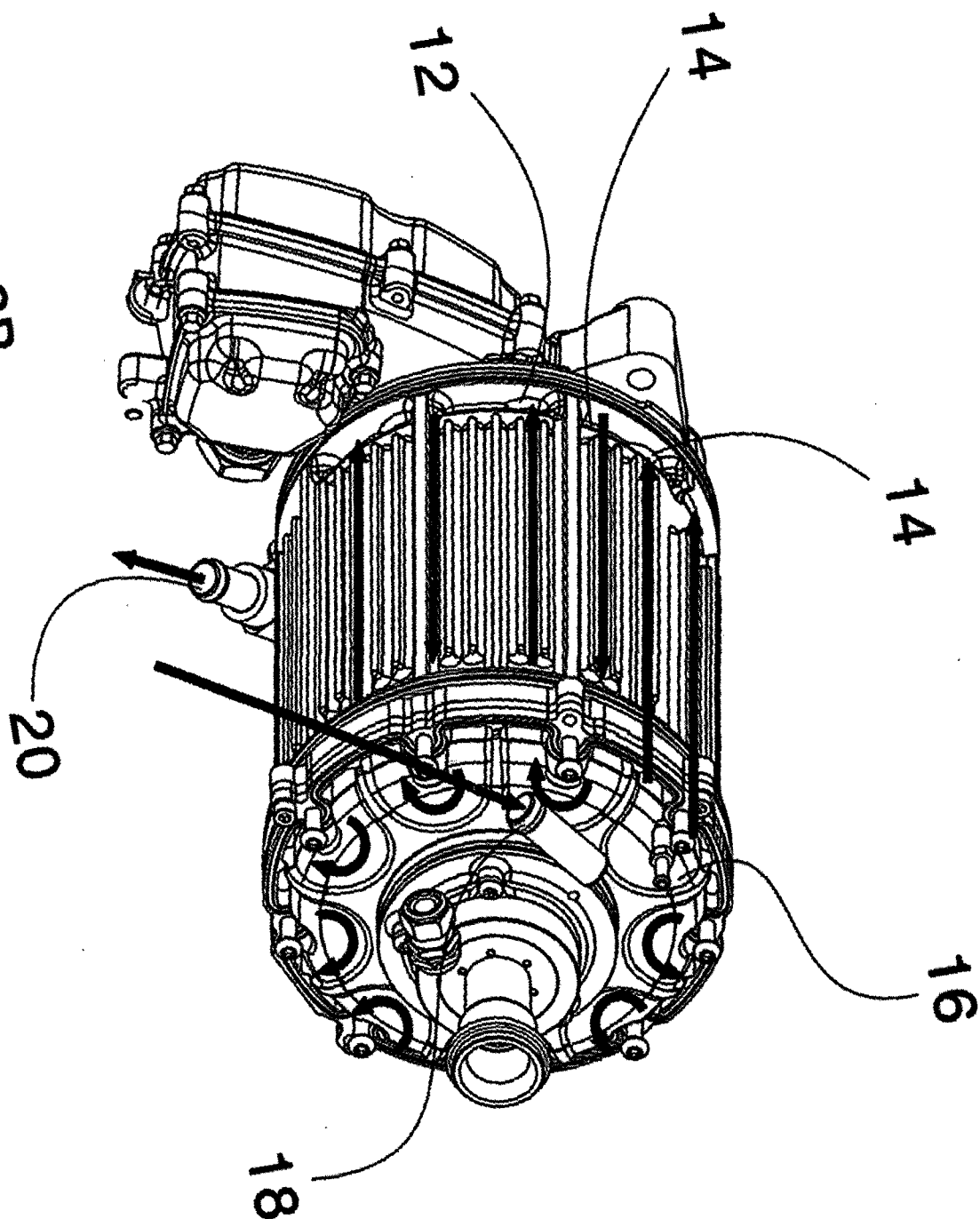
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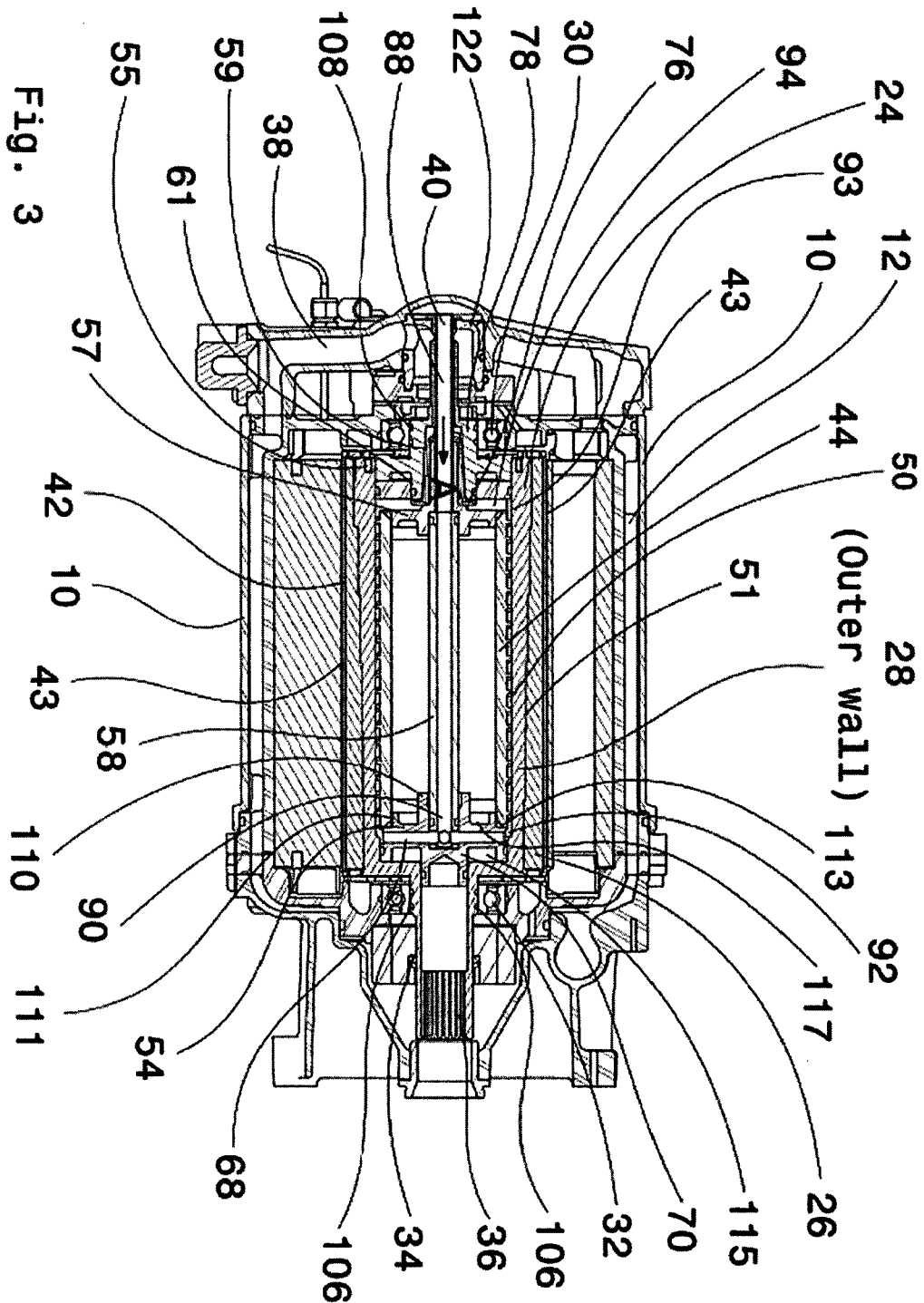


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Fig. 2B



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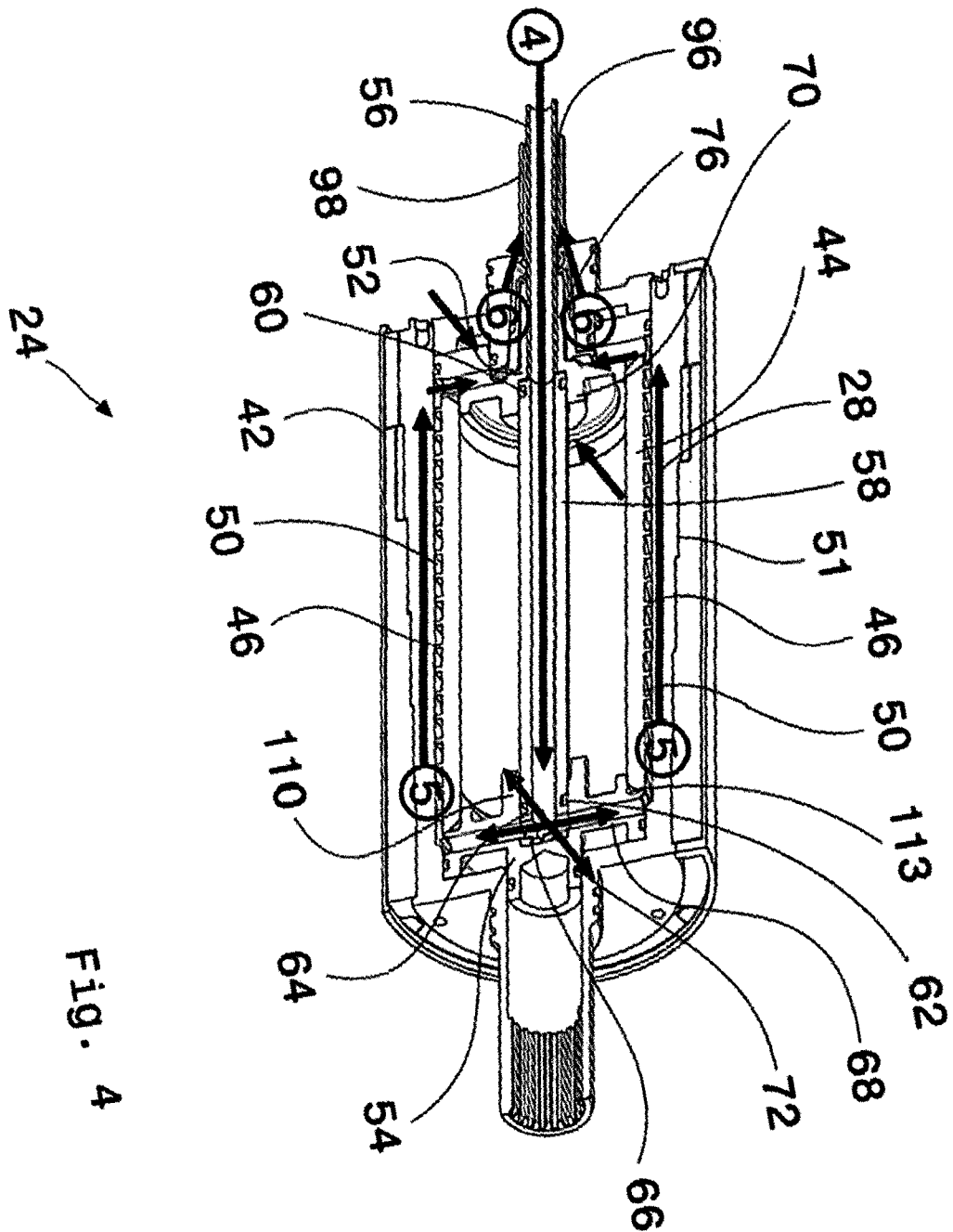
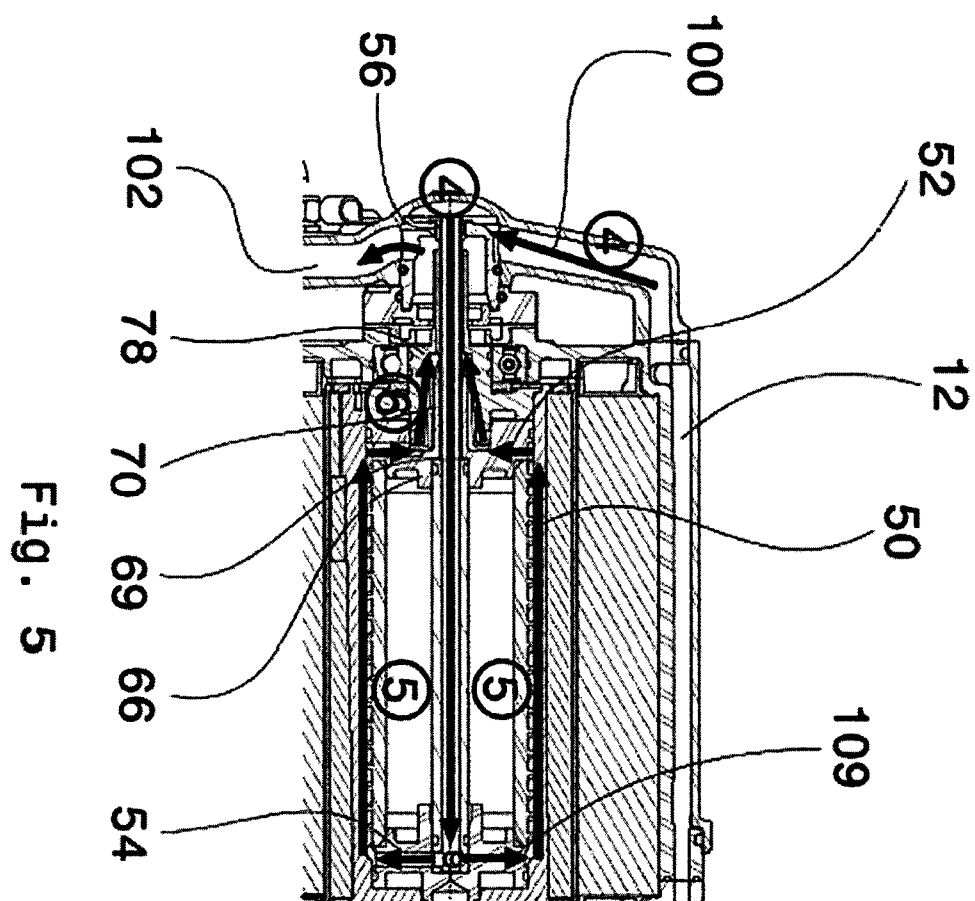


Fig. 4

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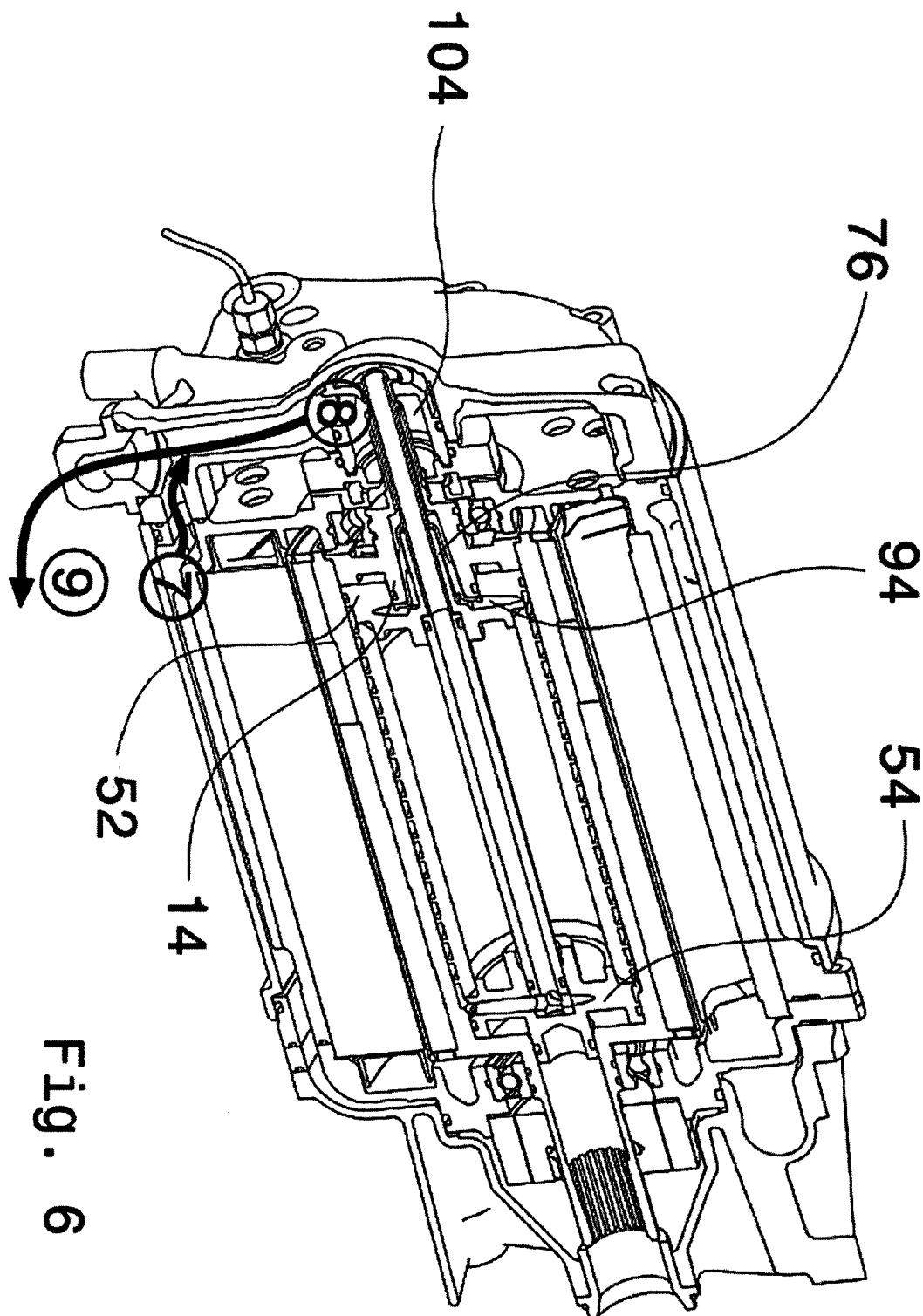
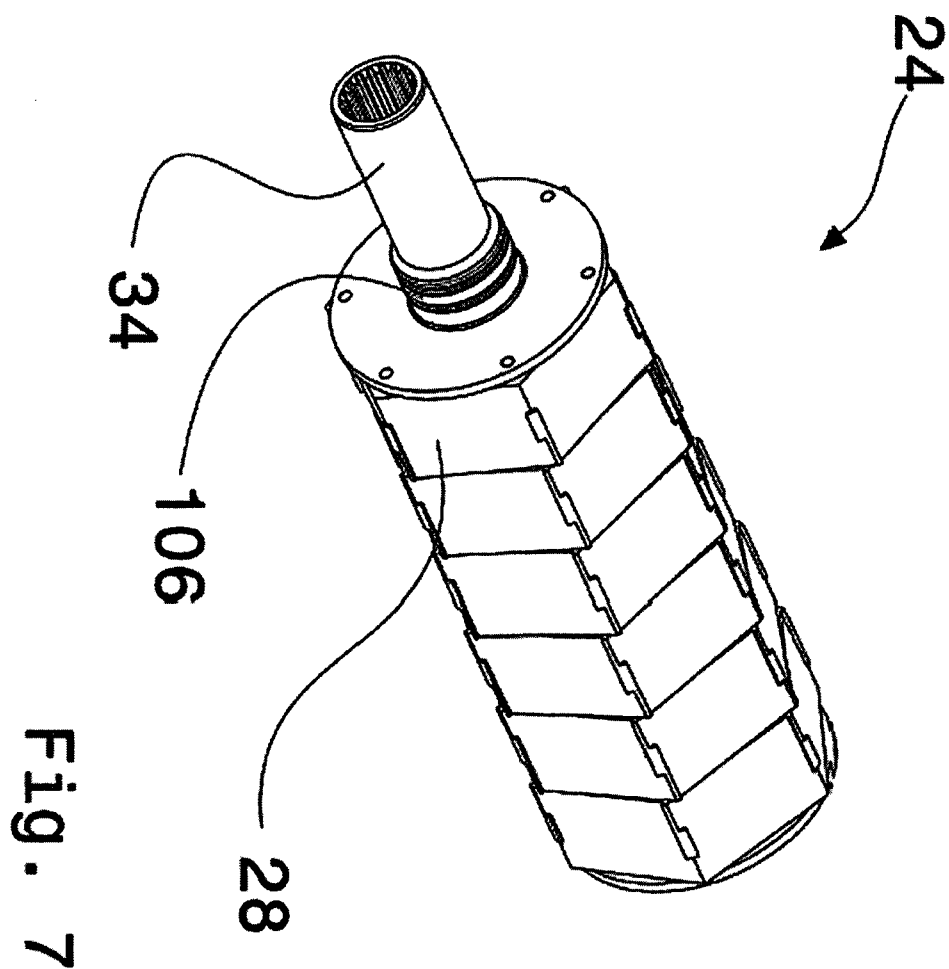
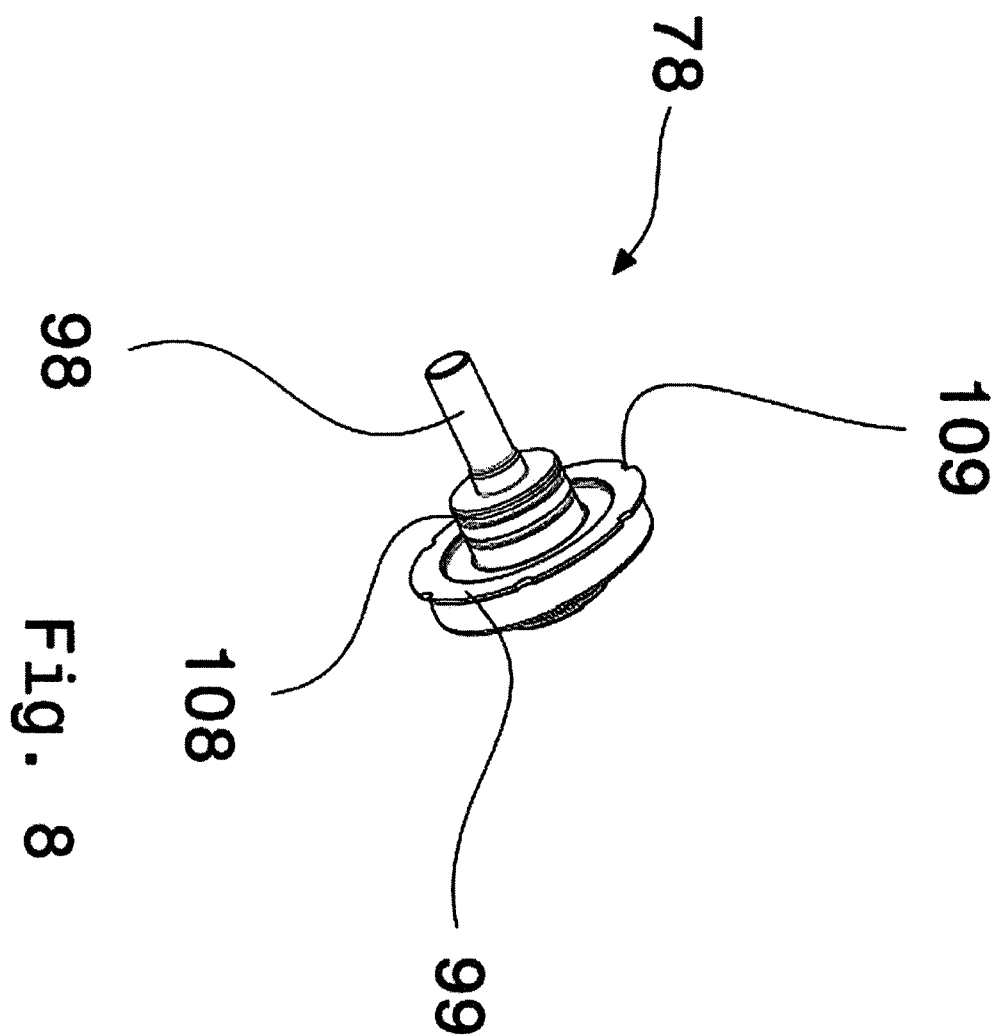


Fig. 6

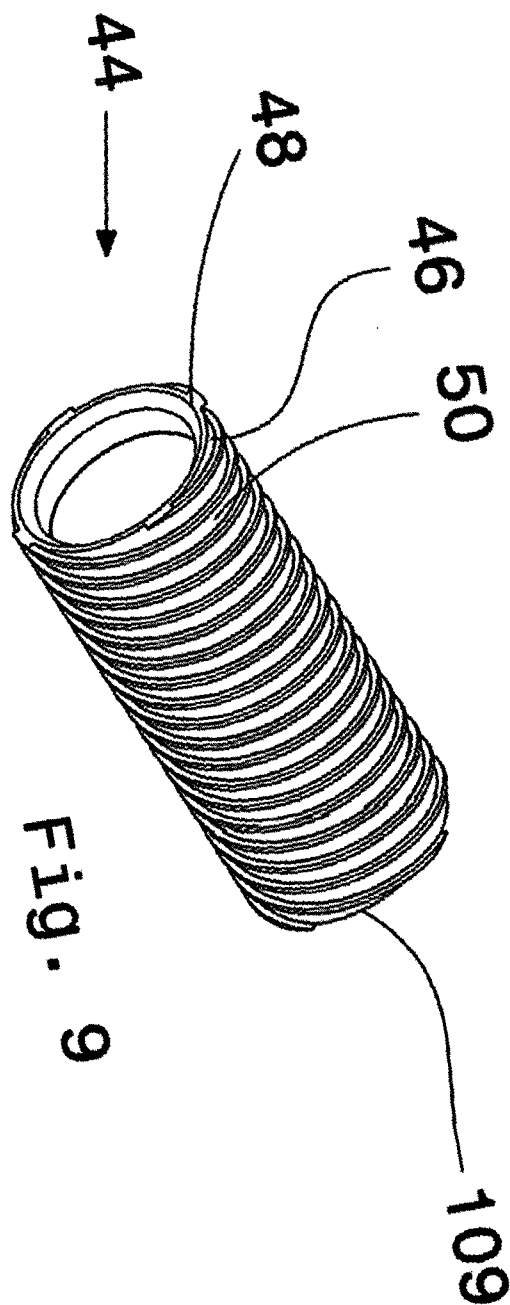
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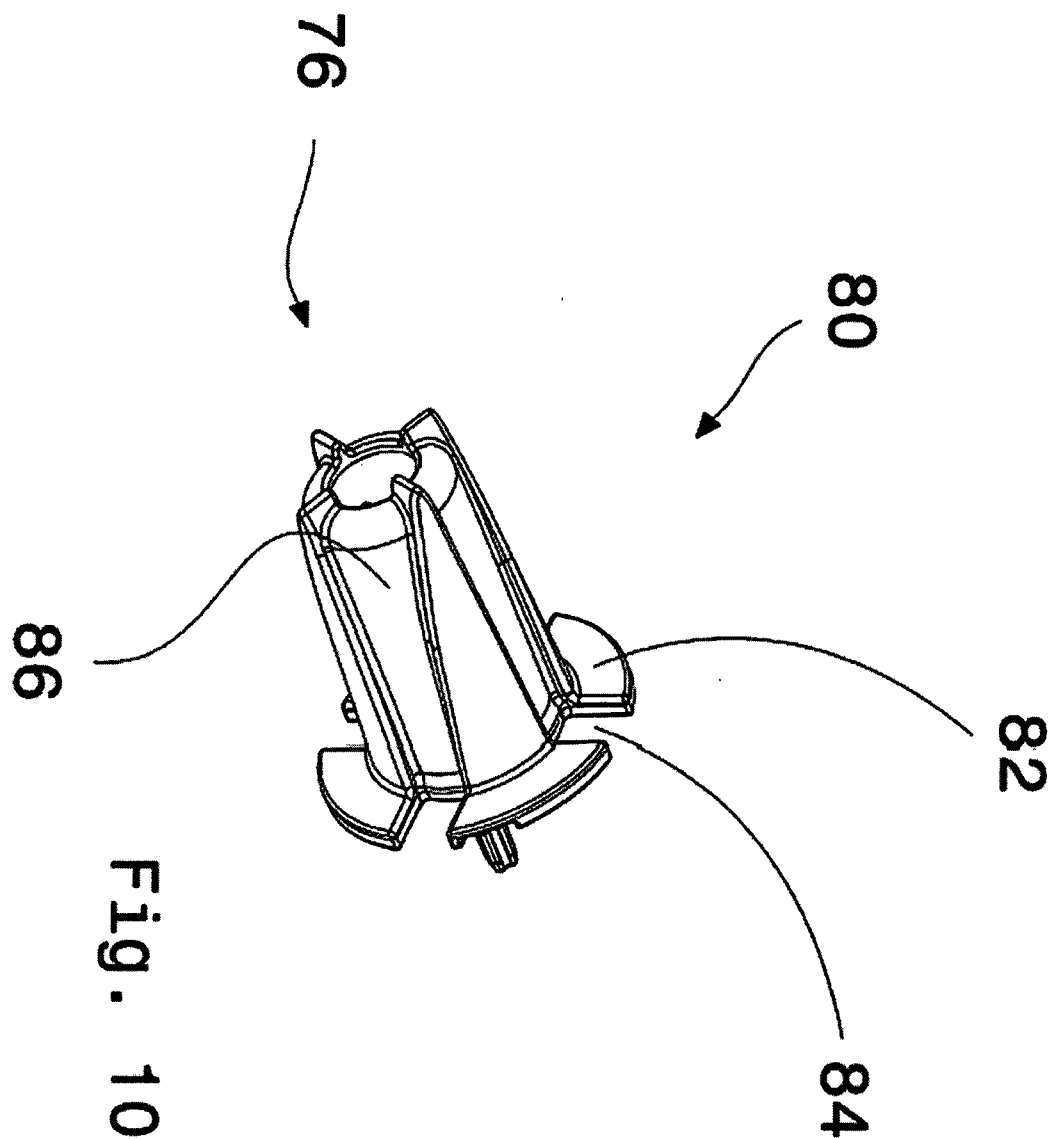


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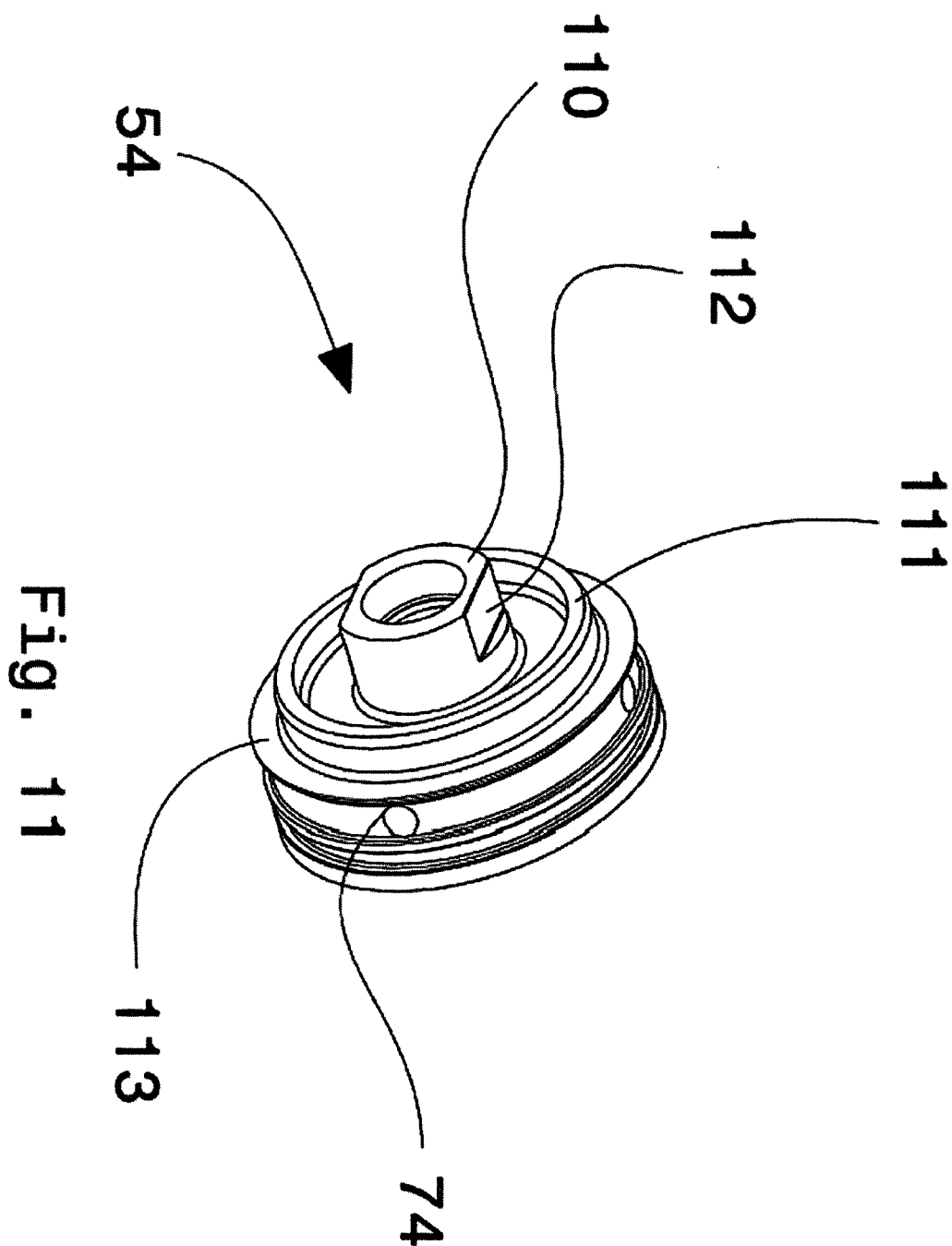




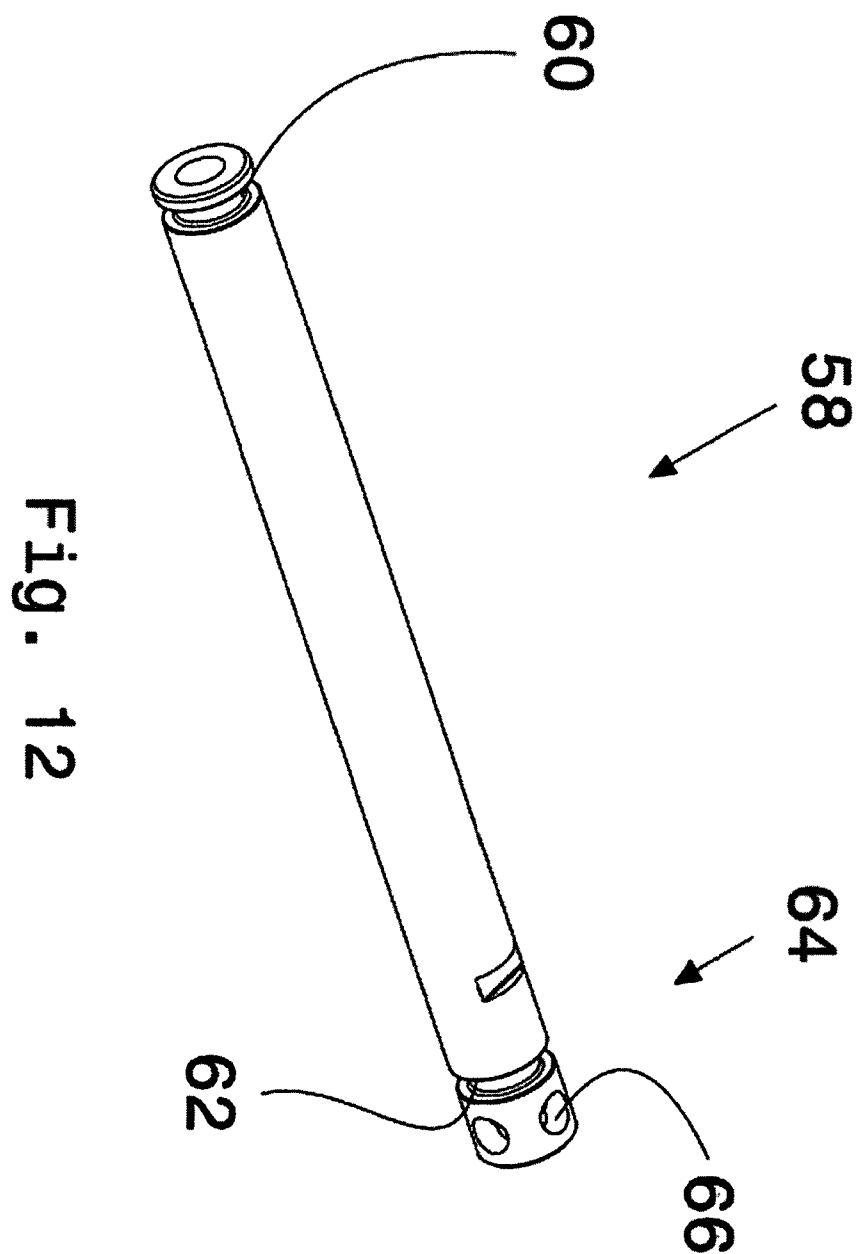
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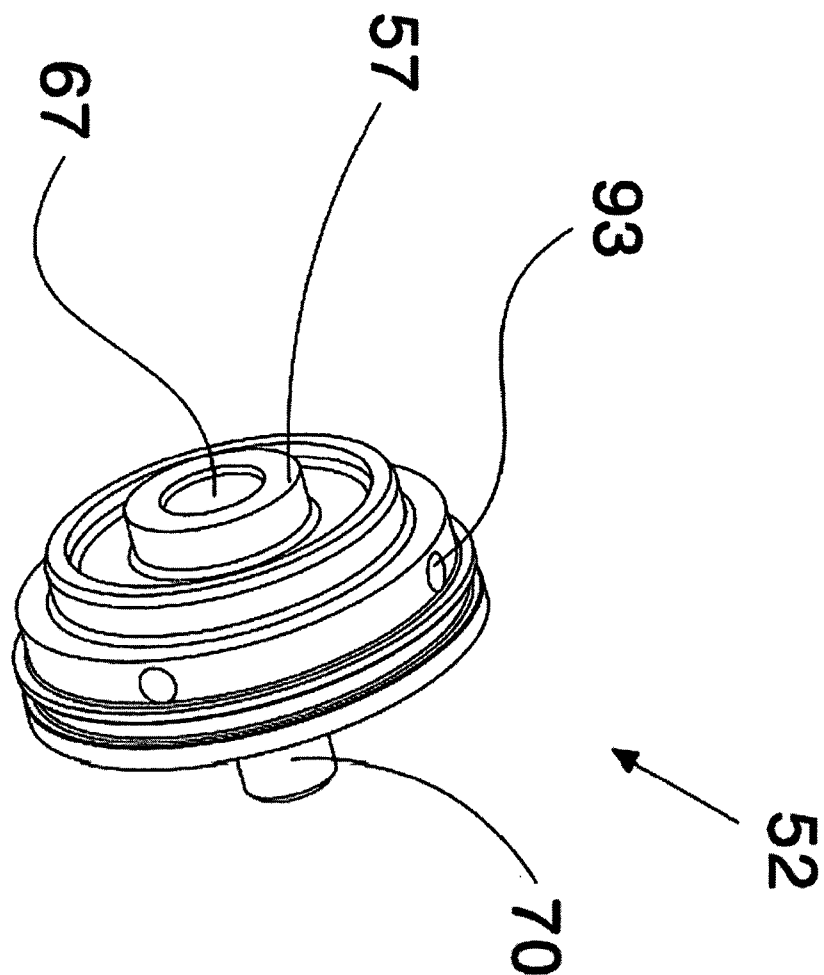


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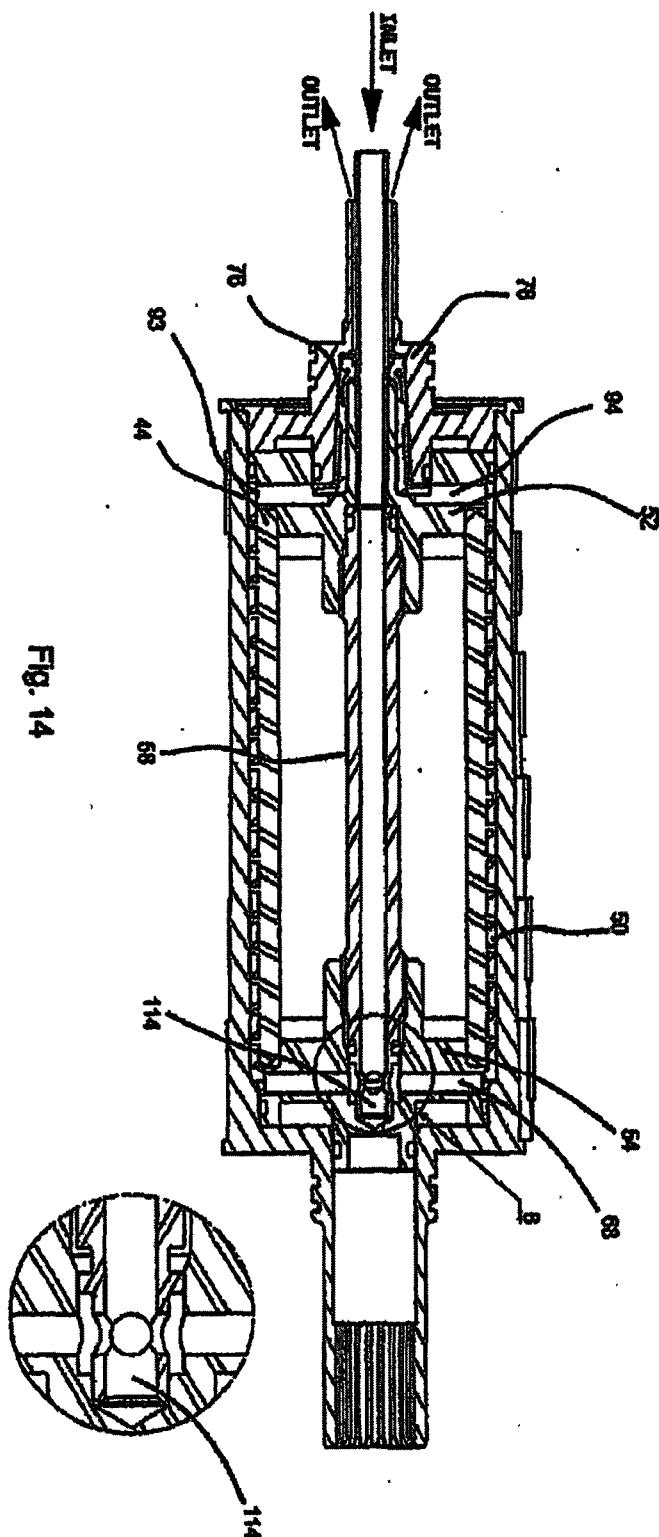


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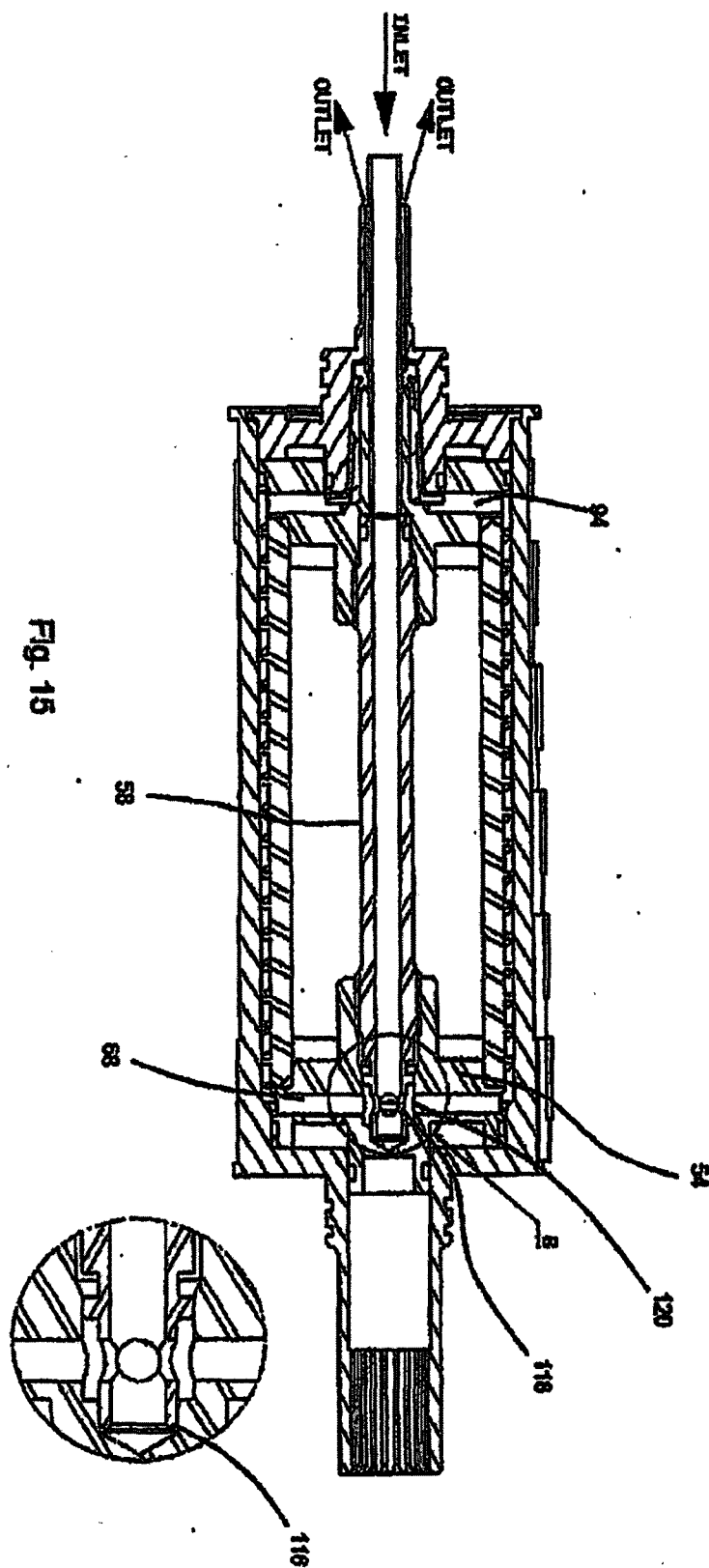
Fig. 13



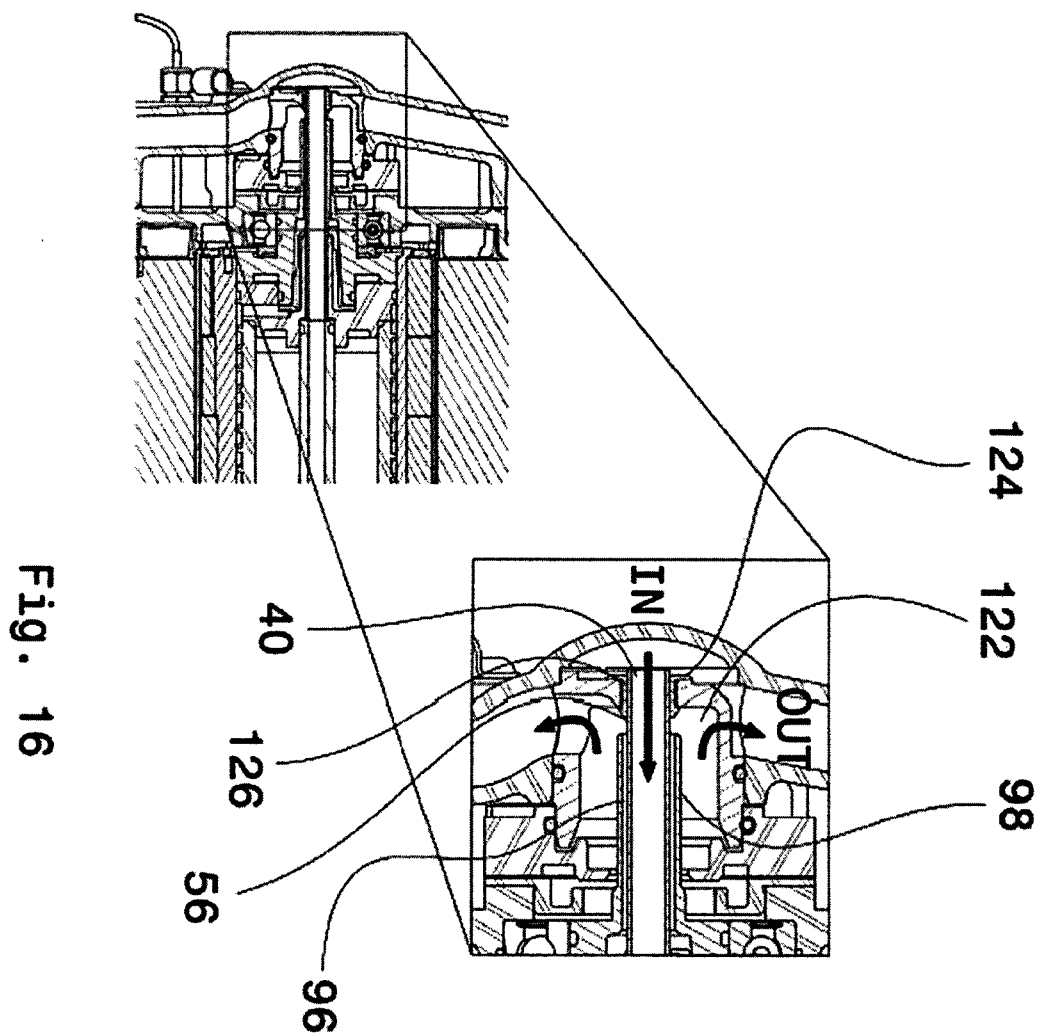
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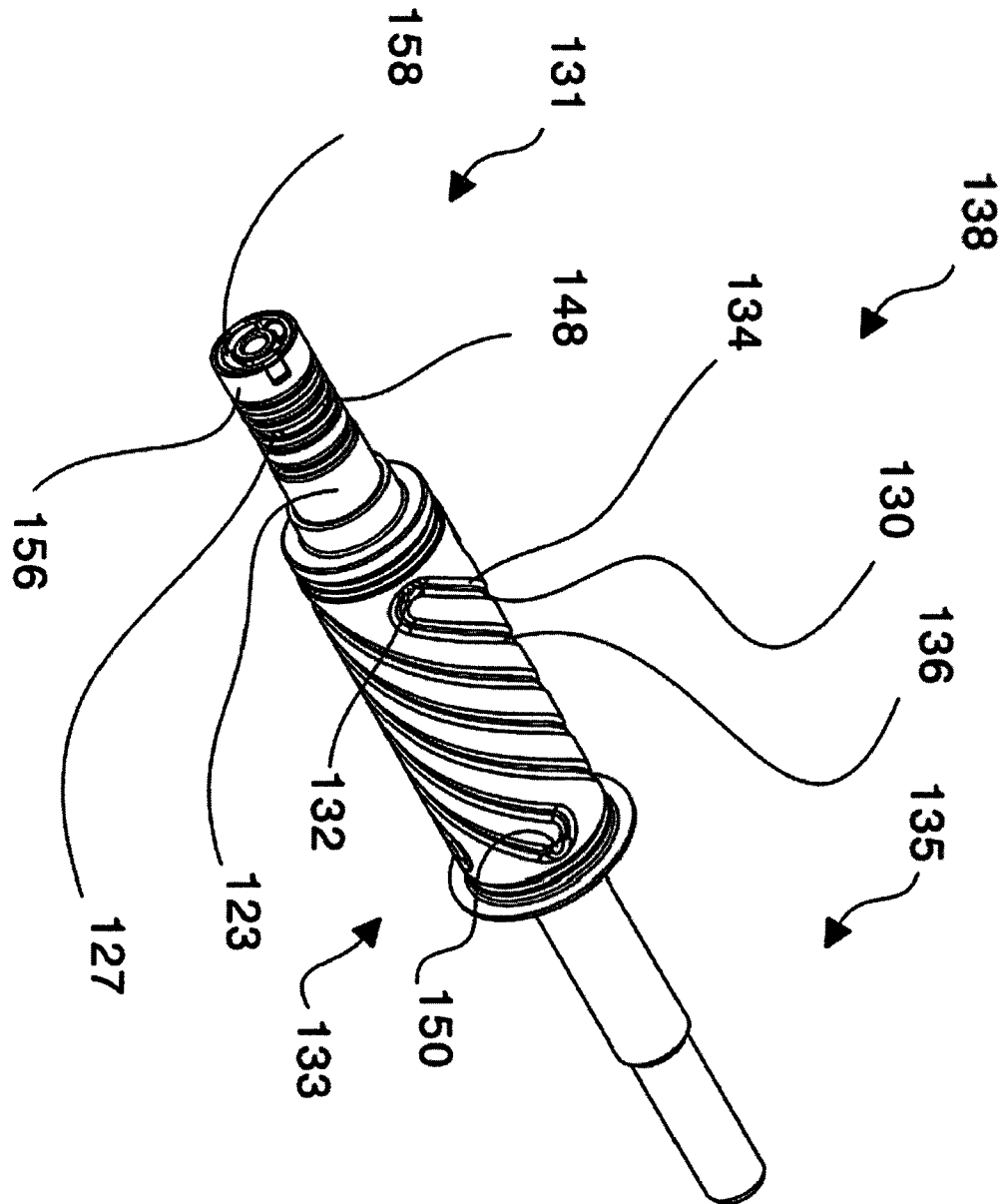


Fig. 17



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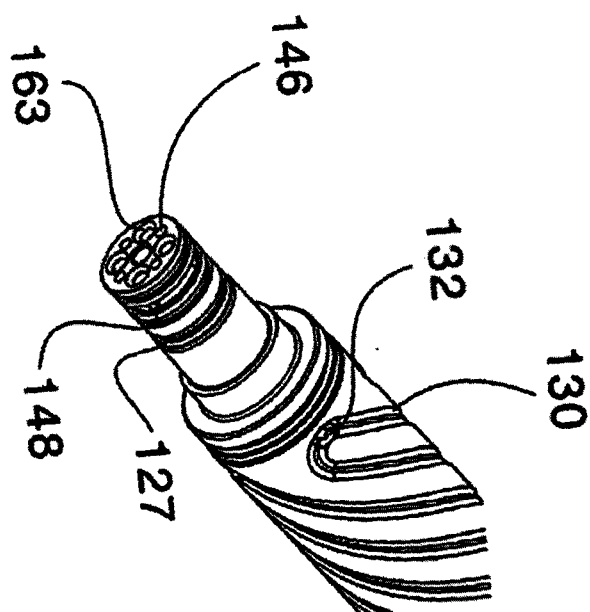
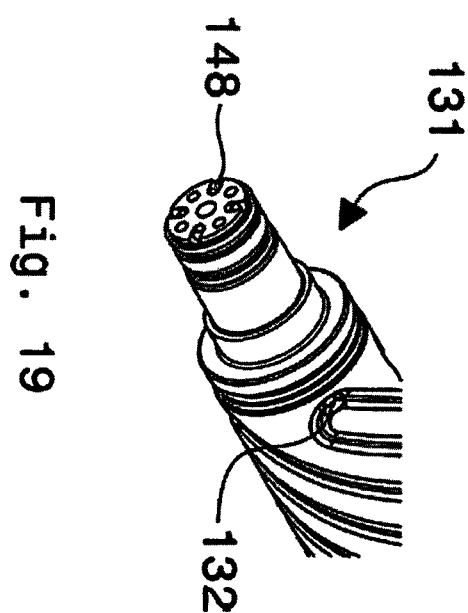
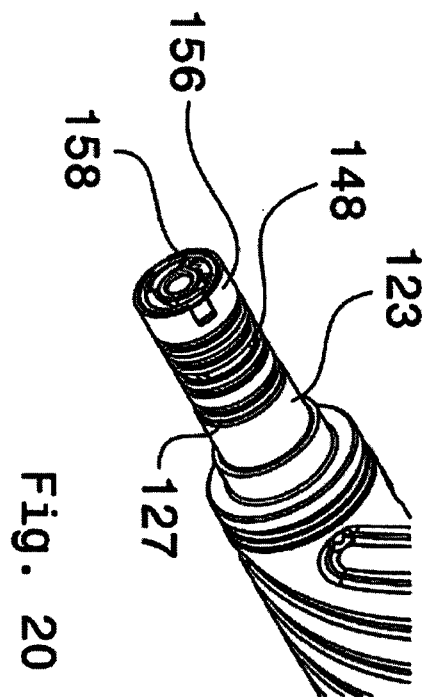


Fig. 18

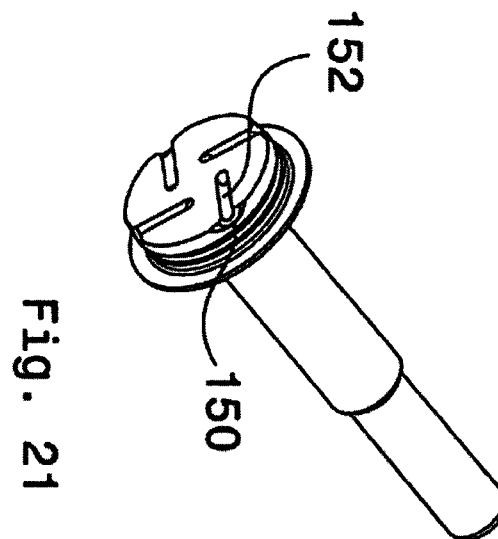
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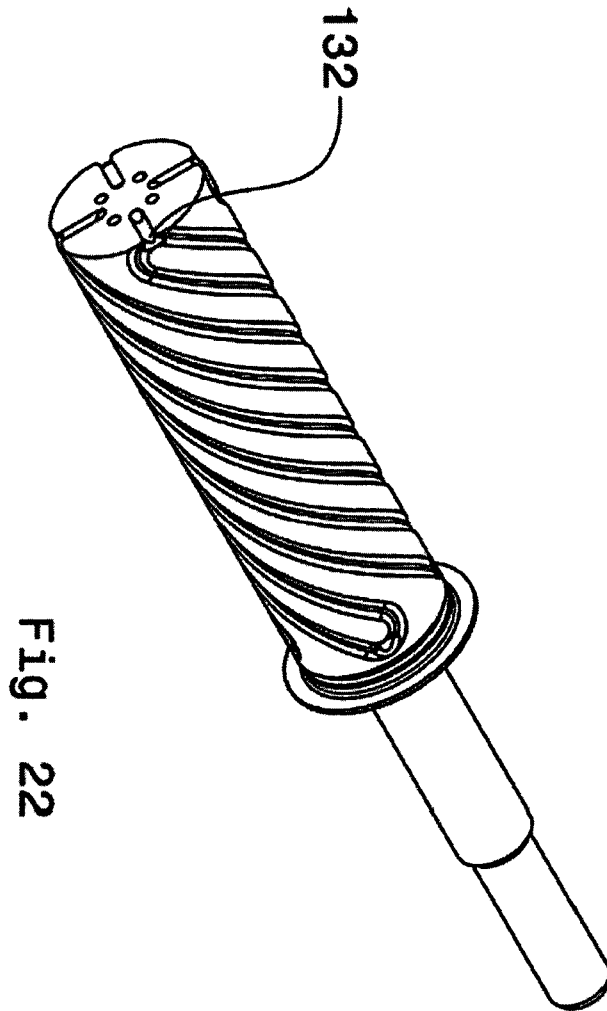
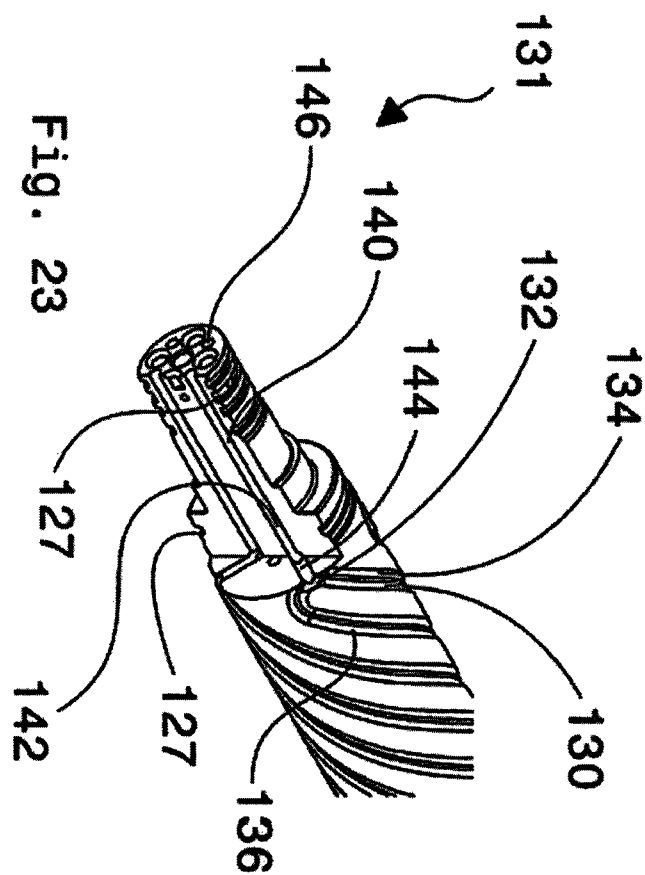


Fig. 22

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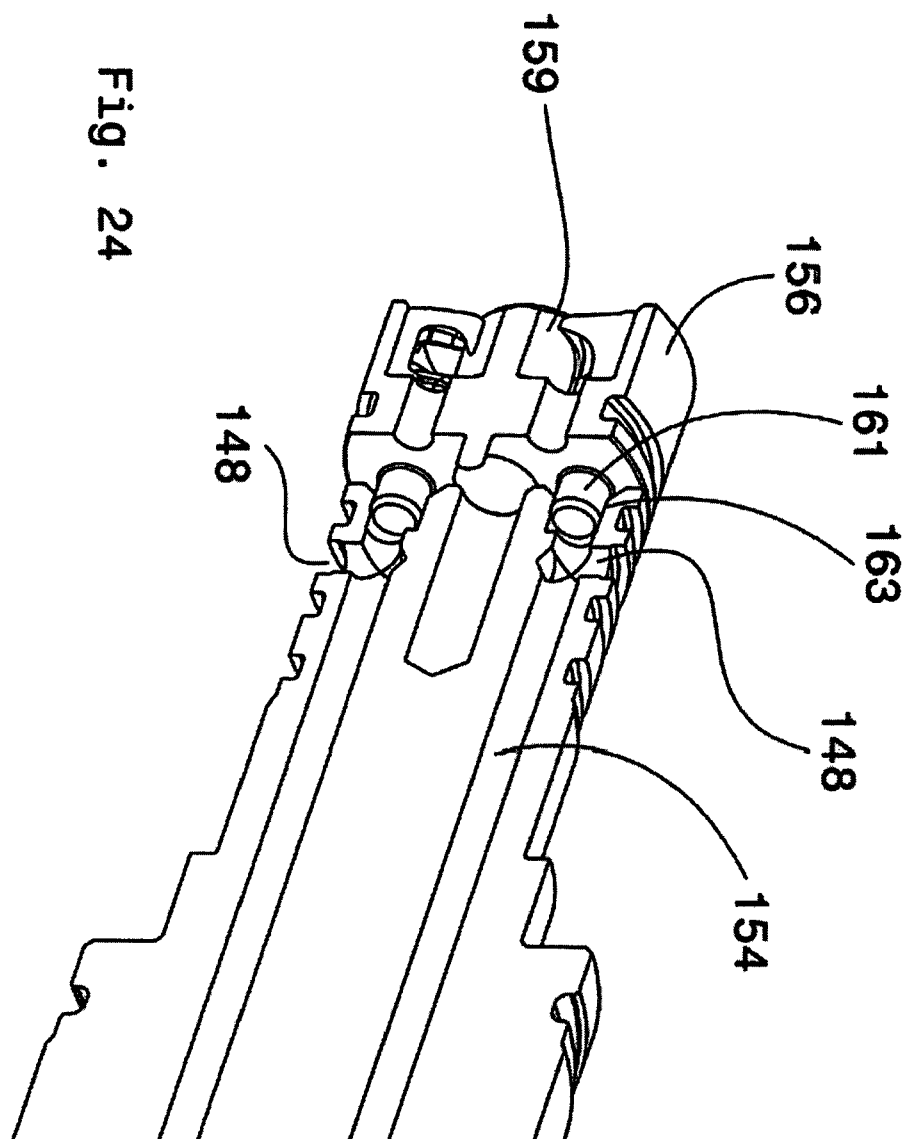
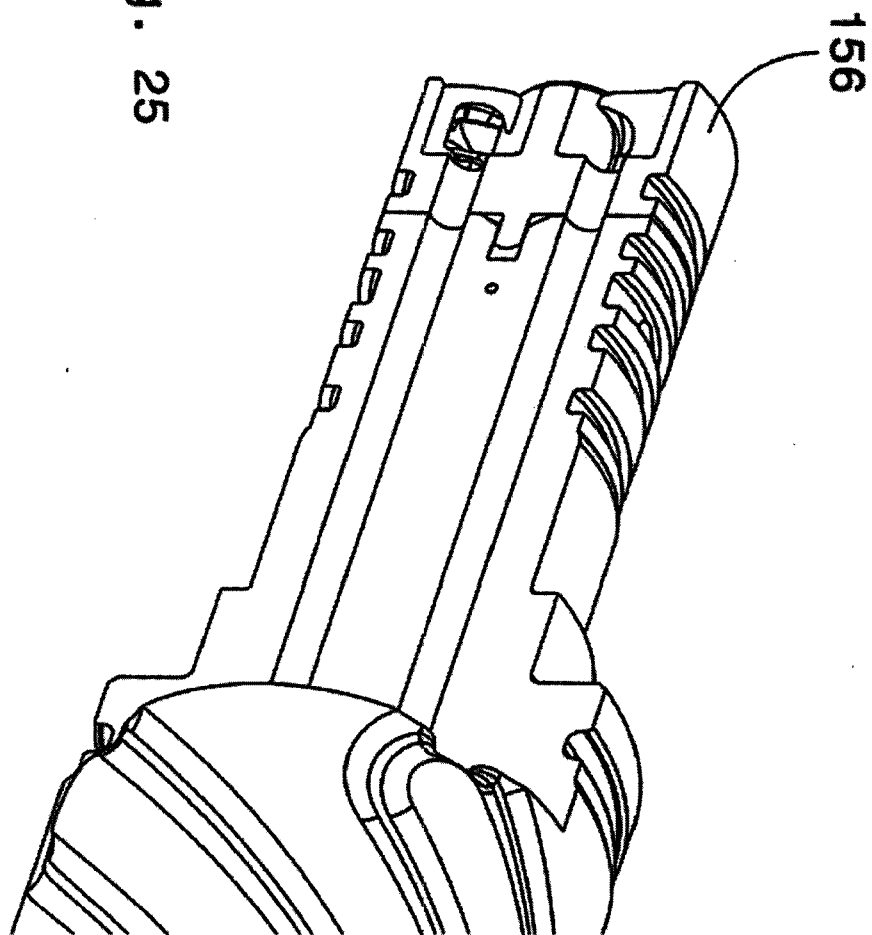


Fig. 24

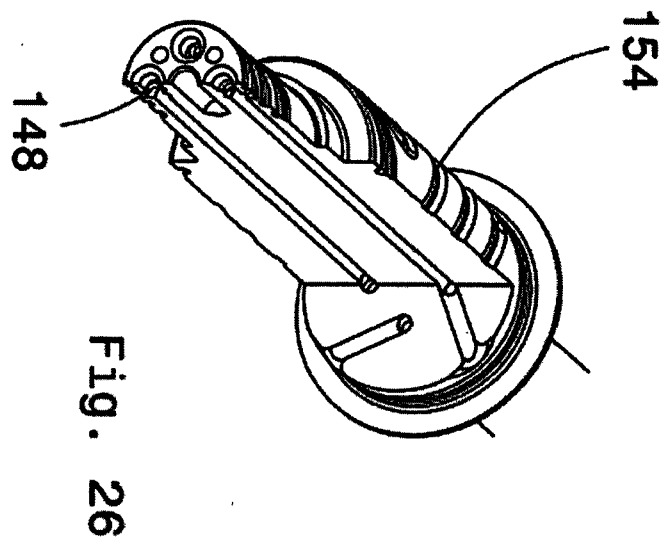
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Fig. 25



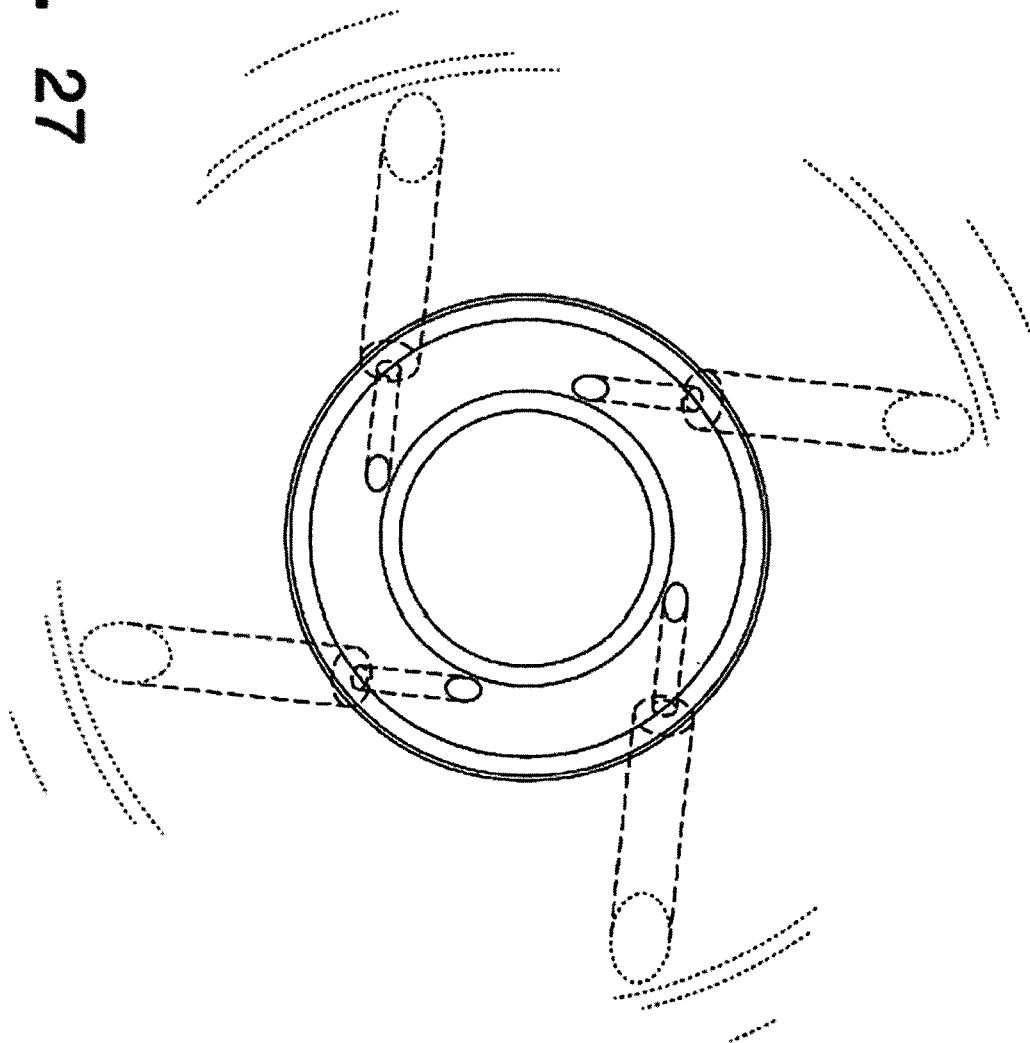


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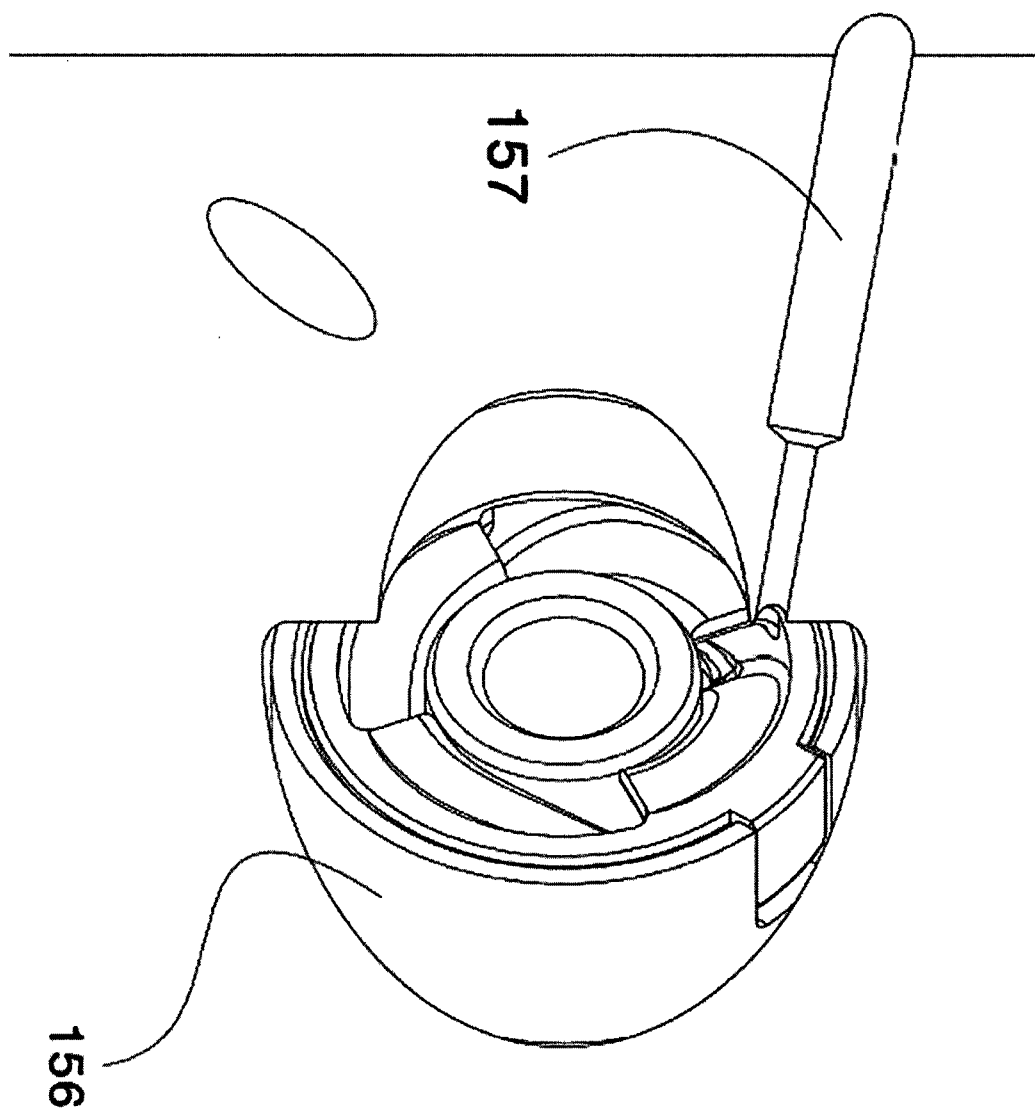
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Fig. 27

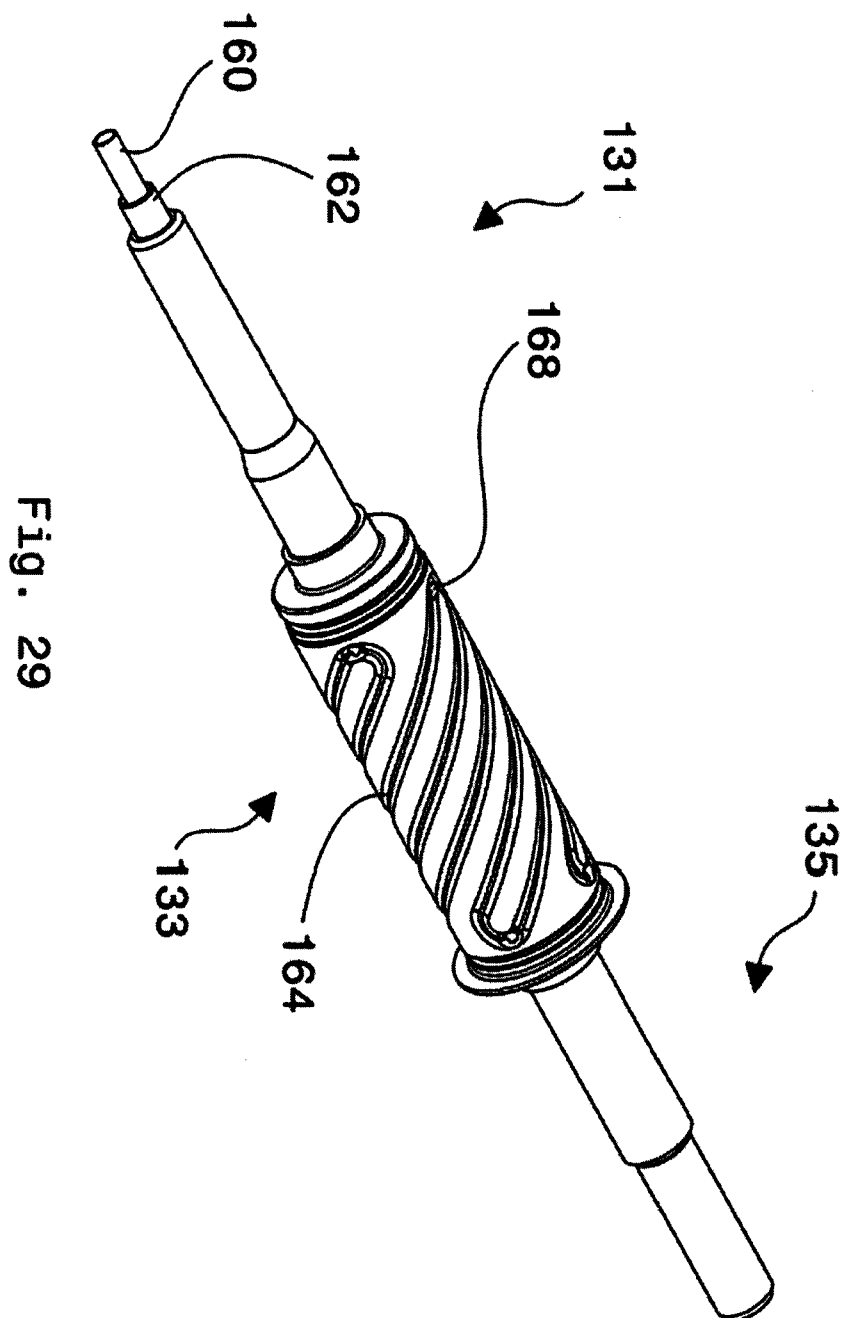


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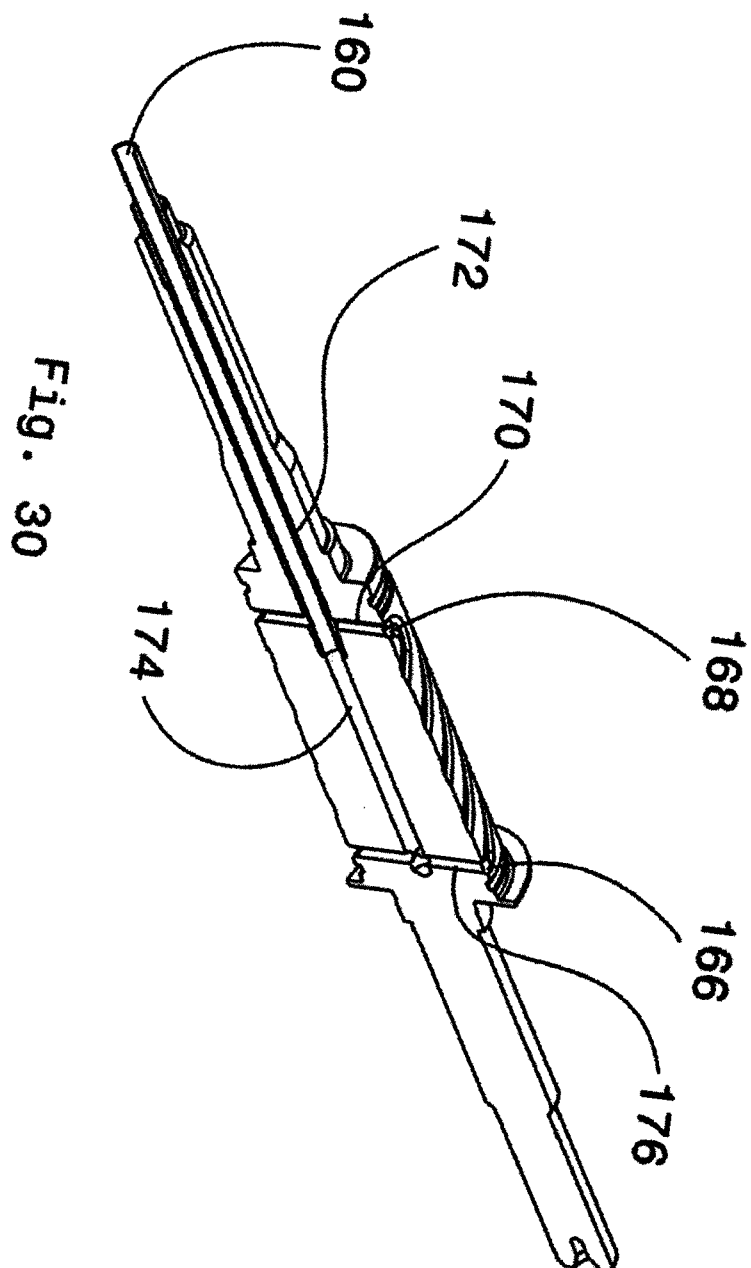
Fig. 28



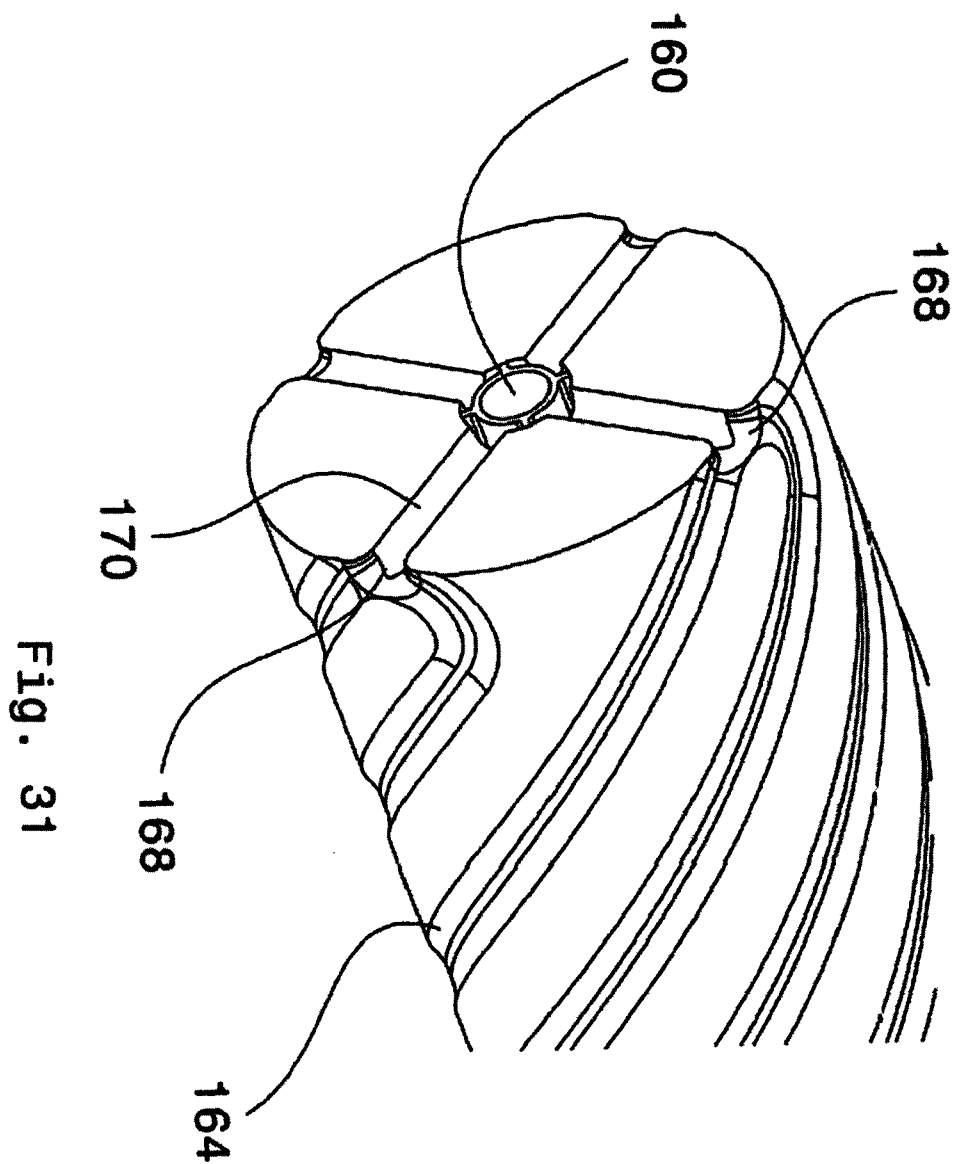
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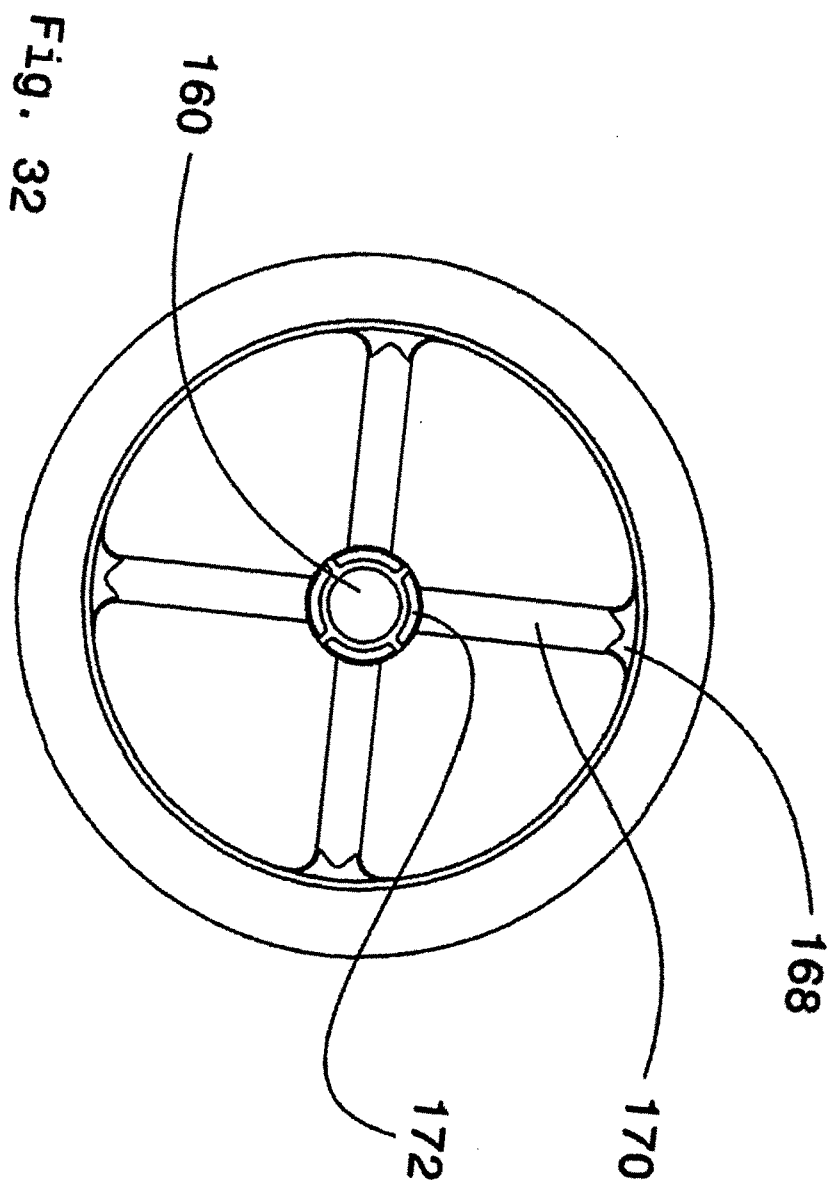
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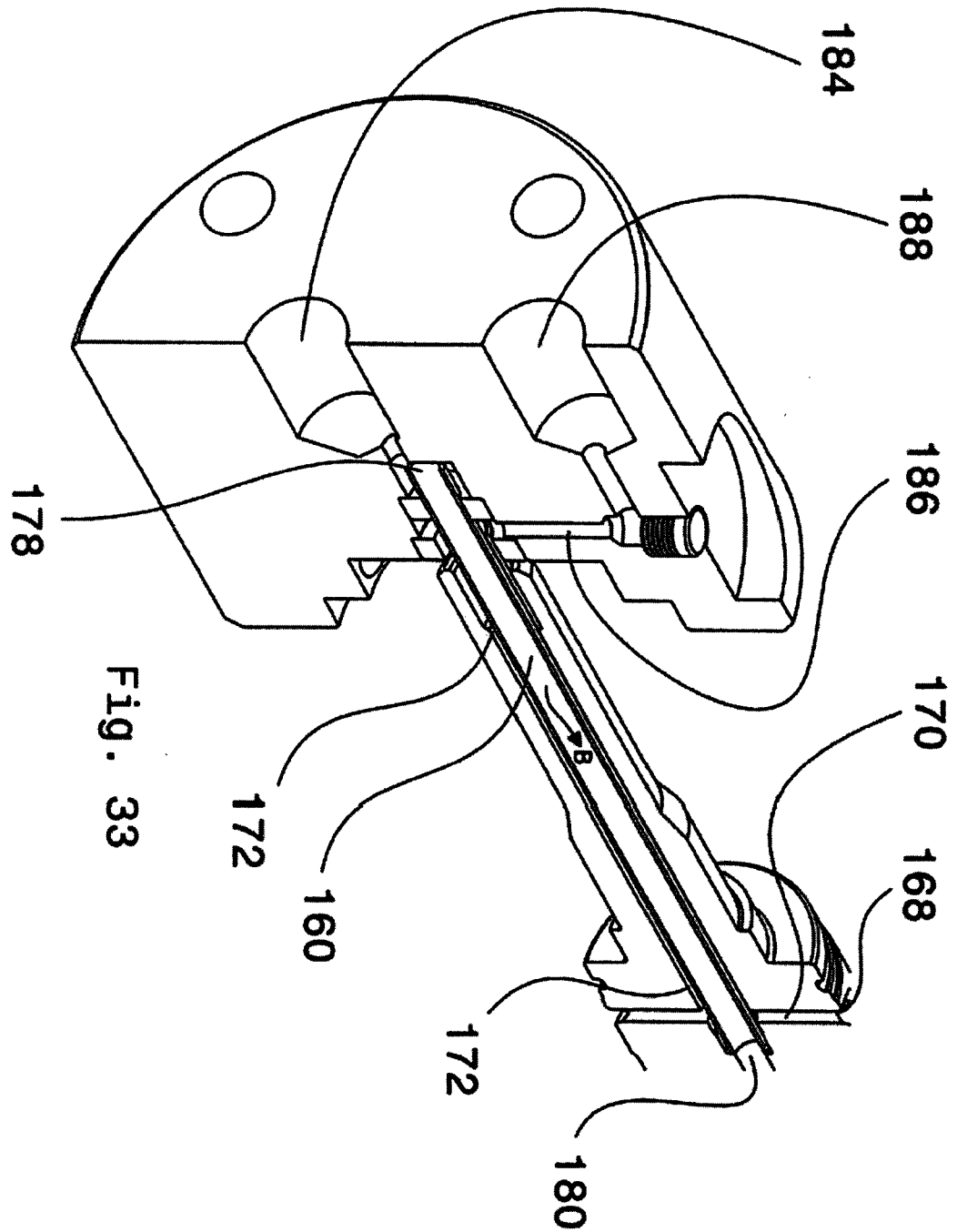
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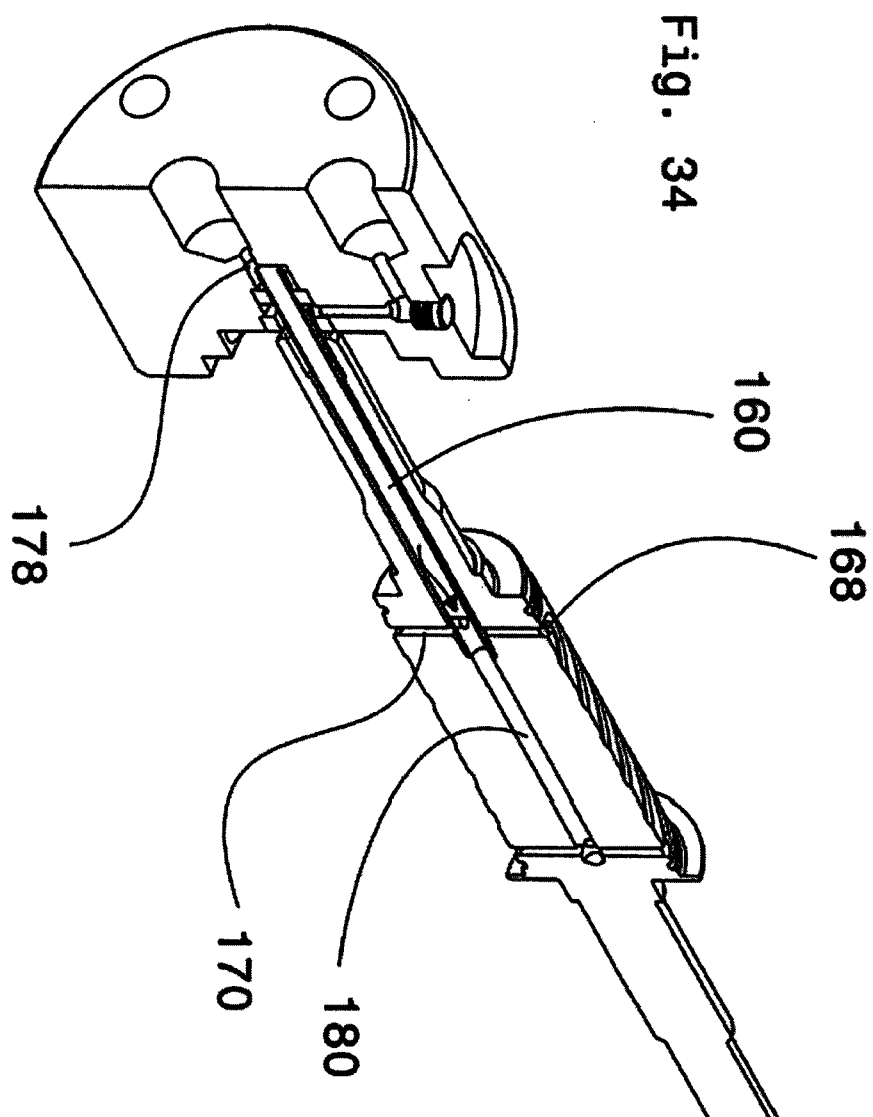


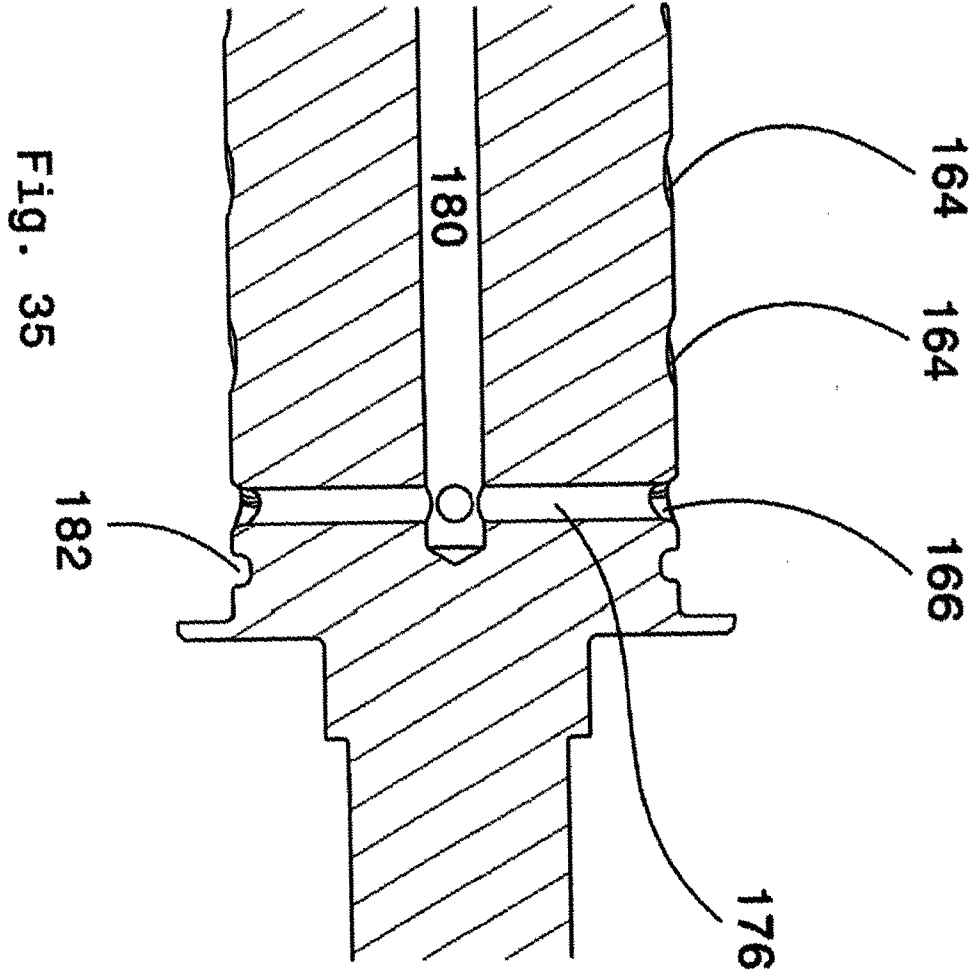
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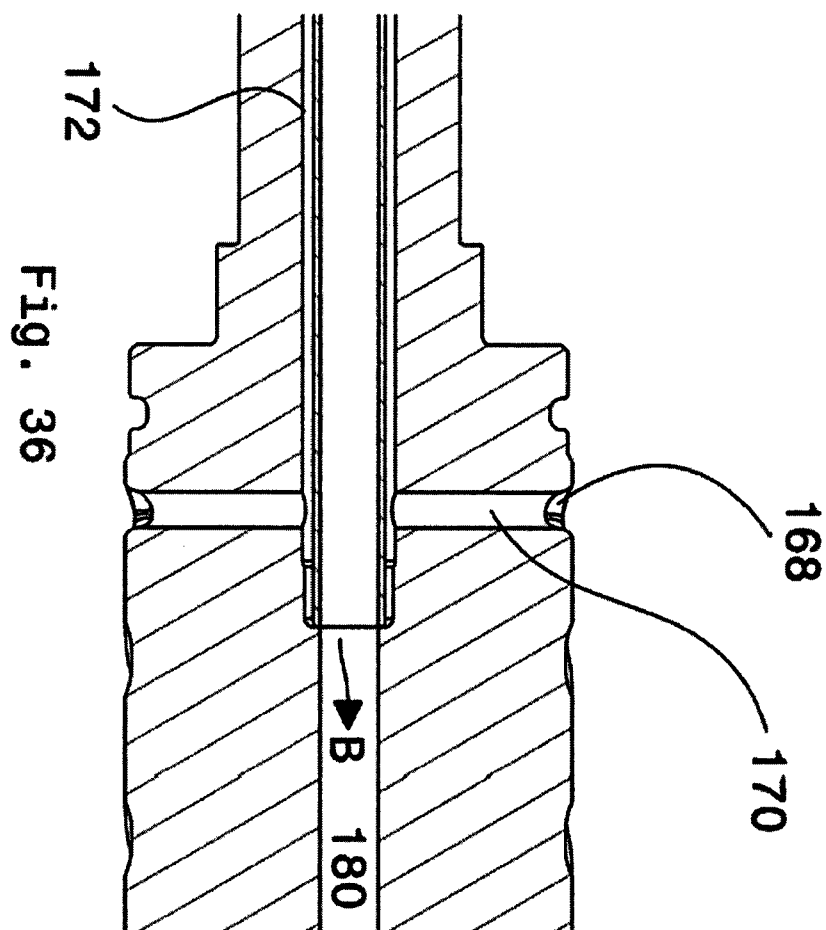


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Fig. 37

