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(54) Title: FABRIC SOFTENER COMPOSITION HAVING IMPROVED DISPENSING PROPERTIES

(57) Abstract: The present invention relates to thickened liquid fabric softener compositions as well as the methods of making and using same. Such thickened, structured liquid fabric softener compositions comprise a quaternary ammonium ester fabric softening active and cellulose fibers. Such fabric softener compositions provide softening benefits, phase stability, and easy dosing that are desired by consumers while minimizing the formation of dispenser residues.

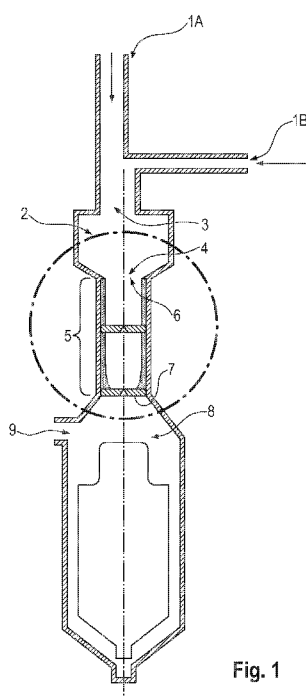


Fig. 1

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FABRIC SOFTENER COMPOSITION HAVING IMPROVED DISPENSING PROPERTIES

FIELD OF THE INVENTION

The invention is directed to fabric softener compositions comprising cellulose fibers.

BACKGROUND OF THE INVENTION

5 Fabric softener compositions provide benefits to treated fabrics, particularly in the last rinse phase of the laundry cycle, after the addition of the detergent composition. Such benefits include fabric softening, provided by the incorporation of fabric softener actives. To provide a rich appearance, improve the dosing experience, and to improve the phase stability of such fabric softener compositions, rheology modifiers are typically added.

10 In general, the fabric softener composition is mixed with the rinse water of the last rinse phase by dosing such composition into the fabric softener compartment of the dispenser of a washing machine. However, especially a thickened, structured fabric softener composition having a yield stress to improve phase stability may partially remain as a residue in the dispenser, and hence not be fully dispersed into the rinse water. As a result, the fabric softener
15 composition only partially gets in contact with the fabrics and hence the benefits are reduced. In addition to a partial loss in benefits, consumer dissatisfaction is created because such fabric softener residues make the dispenser look dirty and can even lead to the formation of malodor and hence requires additional cleaning of the washing machine dispenser. Lowering the level of rheology modifier to avoid dispenser residues negatively affects the rich appearance and dosing
20 experience and may lead to phase instabilities over time.

Hence, there is still a need for a thickened, structured, but still pourable liquid fabric softener composition comprising a fabric softening active with less tendency to leave residues in the washing machine dispenser.

25 WO2008/076753 (A1) relates to surfactant systems comprising microfibrinous cellulose to suspend particulates. WO2008/079693 (A1) relates to a cationic surfactant composition comprising microfibrinous cellulose to suspend particulates. WO2011/056956 relates to aqueous compositions comprising surfactants, microfibrinous cellulose, water, and alkaline earth metal ions. WO03085074 (A1) discloses a detergent composition comprising cationic surfactant,

perfume, and microfibrinous cellulose. WO2015/006635 relates to structured fabric care compositions comprising a fabric softener active and microfibrillated cellulose. WO03/062361 (A1) discloses liquid fabric conditioners comprising cellulose fibers and esterquats.

WO2008057985 (A1) relates to surfactant thickened systems comprising microfibrinous cellulose and methods of making same. WO2010003860 relates to liquid cleansing compositions comprising microfibrinous cellulose suspending polymers.

SUMMARY OF THE INVENTION

The present invention relates to thickened, structured liquid fabric softener compositions comprising a quaternary ammonium ester fabric softening active and cellulose fibers. The present invention further relates to a method for softening fabrics and to the use of cellulose fibers in a liquid fabric softener composition. The compositions of the present invention provide improved dispensability and dispenser appearance while still providing a rich appearance.

BRIEF DESCRIPTION OF THE DRAWINGS

While the specification concludes with claims particularly pointing out and distinctly claiming the invention, it is believed that the invention will be better understood from the following description of the accompanying figures in which like reference numerals identify like elements, and wherein:

Figure 1 details the apparatus A (see Methods).

Figure 2 details the orifice component 5 of Apparatus A (see Methods).

Figure 3 details the Apparatus B (see Methods).

DETAILED DESCRIPTION OF THE INVENTION

Definitions

As used herein, the articles including “a” and “an” when used in a claim, are understood to mean one or more of what is claimed or described.

As used herein, the terms “include”, “includes” and “including” are meant to be non-limiting.

Unless otherwise noted, all component or composition levels are in reference to the active portion of that component or composition, and are exclusive of impurities, for example, residual solvents or by-products, which may be present in commercially available sources of such components or compositions. For example, it is known that quaternary ammonium esters typically contain the following impurities: the monoester form of the quaternary ammonium ester, residual non-reacted fatty acid, and non-quaternized esteramines.

All percentages and ratios are calculated by weight unless otherwise indicated. All percentages and ratios are calculated based on the total composition unless otherwise indicated.

All ratios are calculated as a weight/weight level of the active material, unless otherwise specified.

All measurements are performed at 25°C unless otherwise specified.

It should be understood that every maximum numerical limitation given throughout this specification includes every lower numerical limitation, as if such lower numerical limitations were expressly written herein. Every minimum numerical limitation given throughout this specification will include every higher numerical limitation, as if such higher numerical limitations were expressly written herein. Every numerical range given throughout this specification will include every narrower numerical range that falls within such broader numerical range, as if such narrower numerical ranges were all expressly written herein.

The liquid fabric softener composition

As used herein, “liquid fabric softener composition” refers to any treatment composition comprising a liquid capable of softening fabrics e.g., clothing in a domestic washing machine. The composition can include solids or gases in suitably subdivided form, but the overall composition excludes product forms which are non-liquid overall, such as tablets or granules. The liquid fabric softener composition preferably has a density in the range from 0.9 to 1.3 g.cm⁻³, excluding any solid additives but including any bubbles, if present.

Aqueous liquid fabric softening compositions are preferred. For such aqueous liquid fabric softener compositions, the water content can be present at a level of from 5% to 97%, preferably

from 50% to 96%, more preferably from 70% to 95% by weight of the liquid fabric softener composition.

The pH of the neat fabric softener composition (see Methods) is typically acidic to improve hydrolytic stability of the quaternary ammonium ester softening active and may be from pH 2.0 to 6.0, preferably from pH 2.0 to 4.5, more preferably from 2.0 to 3.5.

To maintain phase stability of the fabric softener composition, the dynamic yield stress (see Methods) at 20°C of the fabric softener composition is from 0.001 Pa to 1.0 Pa, preferably from 0.002 Pa to 0.9 Pa, more preferably from 0.005 Pa to 0.8 Pa, even more preferably from 0.010 Pa to 0.5 Pa. On the one hand, absence of a dynamic yield stress may lead to phase instabilities, especially when the fabric softener composition comprises encapsulated benefit agents or particles. On the other hand, very high dynamic yield stresses may lead to undesired air entrapment during filling of a bottle with the fabric softener composition.

To provide a rich appearance while maintaining pourability of the fabrics softener composition, the viscosity (see Methods) of the fabric softener composition is from 200 mPa.s to 1000 mPa.s, preferably from 250 mPa.s to 900 mPa.s, more preferably from 300 mPa.s to 800 mPa.s, even more preferably from 350 mPa.s to 700 mPa.s at 20°C.

The liquid fabric softener composition may comprise adjunct ingredients suitable for use in the instant compositions and may be desirably incorporated in certain aspects of the invention, for example to improve the aesthetics of the composition as is the case with pigments and dyes. Moreover, liquid fabric softener compositions comprising unsaturated quaternary ammonium ester softening actives are subject to some degree of UV light and/or oxidation which increases the risk on yellowing of the fabric softener composition as well as yellowing of treated fabrics. However, especially in the presence of a dye any dispenser residue becomes more apparent. The liquid fabric softener composition may comprise from 0.0001% to 0.1%, preferably from 0.001% to 0.05% of a dye by weight of the composition. Suitable dyes are selected from the list comprising bis-azo dyes, tris-azo dyes, acid dyes, azine dyes, hydrophobic dyes, methane basic dyes, anthraquinone basic dyes, and dye conjugates formed by binding acid or basic dyes to polymers.

The quaternary ammonium ester softening active

The liquid fabric softener composition of the present invention comprises from 3.0% to 20% of a quaternary ammonium ester softening active (Fabric Softening Active, "FSA") by weight of the composition. In preferred liquid fabric softener compositions, the quaternary ammonium ester softening active is present at a level from 4.0% to 18%, more preferably from 5.0% to 15%, even more preferably from 7.0% to 12% by weight of the composition. The level of quaternary ammonium ester softening active may depend of the desired concentration of total softening active in the composition (diluted or concentrated composition) and of the presence or not of other softening active. The risk on dispenser residues is especially present with high FSA concentration. On the other hand, at very high FSA levels, the viscosity may no longer be stable over time.

Suitable quaternary ammonium ester softening actives include but are not limited to, materials selected from the group consisting of monoester quats, diester quats, triester quats and mixtures thereof. Preferably, the level of monoester quat is from 2.0% to 40.0%, the level of diester quat is from 40.0% to 98.0%, the level of triester quat is from 0.0% to 25.0% by weight of total quaternary ammonium ester softening active.

Said quaternary ammonium ester softening active may comprise compounds of the following formula:



wherein:

m is 1, 2 or 3 with proviso that the value of each m is identical;

each R^1 is independently hydrocarbyl, or branched hydrocarbyl group, preferably R^1 is linear, more preferably R^1 is partially unsaturated linear alkyl chain;

each R^2 is independently a C_1 - C_3 alkyl or hydroxyalkyl group, preferably R^2 is selected from methyl, ethyl, propyl, hydroxyethyl, 2-hydroxypropyl, 1-methyl-2-hydroxyethyl, poly(C_{2-3} alkoxy), polyethoxy, benzyl;

each X is independently $(CH_2)_n$, $CH_2-CH(CH_3)-$ or $CH-(CH_3)-CH_2-$ and

each n is independently 1, 2, 3 or 4, preferably each n is 2;

each Y is independently $-O-(O)C-$ or $-C(O)-O-$;

A- is independently selected from the group consisting of chloride, methyl sulfate, and ethyl sulfate, preferably A- is selected from the group consisting of chloride and methyl sulfate;

with the proviso that when Y is -O-(O)C-, the sum of carbons in each R¹ is from 13 to 21,
5 preferably from 13 to 19.

In preferred liquid fabric softener compositions the iodine value of the parent fatty acid from which the quaternary ammonium fabric softening active is formed is from 0 to 100, more preferably from 10 to 60, even more preferably from 15 to 45.

Examples of suitable quaternary ammonium ester softening actives are commercially available from KAO Chemicals under the trade name Tetranyl AT-1 and Tetranyl AT-7590, from Evonik under the tradename Rewoquat WE16 DPG, Rewoquat WE18, Rewoquat WE20, Rewoquat WE28, and Rewoquat 38 DPG, from Stepan under the tradename Stepantex GA90, Stepantex VR90, Stepantex VK90, Stepantex VA90, Stepantex DC90, Stepantex VL90A.

These types of agents and general methods of making them are disclosed in U.S.P.N. 4,137,180.

10 Cellulose fibers:

Cellulose fibers of use in the present invention thicken, and structure the fabric softener composition while at the same time surprisingly help to minimize the formation of dispenser residues.

The composition of the present invention comprises cellulose fibers, preferably from
15 0.01% to 5.0 %, more preferably 0.05% to 1.0%, even more preferably from 0.10% to 0.75% of cellulose fibers by weight of the composition.

By cellulose fibers it is meant herein cellulose micro or nano fibrils. The cellulose fibers can be of bacterial or botanical origin, i.e. produced by fermentation or extracted from vegetables, plants, fruits or wood. Cellulose fiber sources may be selected from the group
20 consisting of citrus peels, such as lemons, oranges and/or grapefruit; fruits, such as apples, bananas and/or pear; vegetables such as carrots, peas, potatoes and/or chicory; plants such as bamboo, jute, abaca, flax, cotton and/or sisal, cereals, and different wood sources such as

spruces, eucalyptus and/or oak. Preferably, the cellulose fibers source is selected from the group consisting of wood or plants, in particular, spruce, eucalyptus, jute, and sisal.

The content of cellulose in the cellulose fibers will vary depending on the source and treatment applied for the extraction of the fibers, and will typically range from 15% to 100%, preferably above 30%, more preferably above 50%, and even more preferably above 80% of cellulose by weight of the cellulose fibers.

Such cellulose fibers may comprise pectin, hemicellulose, proteins, lignin and other impurities inherent to the cellulose based material source such as ash, metals, salts and combinations thereof. The cellulose fibers are preferably non-ionic. Such fibers are commercially available, for instance Citri-Fi 100FG from Fiberstar, Herbacel® Classic from Herbafood, and Exilva® from Borregaard.

The cellulose fibers may have an average diameter from 10 nm to 350 nm, preferably from 30 nm to 250 nm, more preferably from 50 nm to 200 nm.

15 Non-ionic surfactants

The fabric softener composition may comprise from 0.01% to 5%, preferably from 0.1% to 3.0%, more preferably from 0.5% to 2.0% of non-ionic surfactant based on the total fabric softener composition weight. Non-ionic surfactants help to effectively disperse perfume into the fabric softener composition and improve the overall dispersability of the fabric softener composition into water.

In preferred liquid fabric softener compositions the non-ionic surfactant is an alkoxyated non-ionic surfactant, preferably an ethoxylated non-ionic surfactant. Preferably the alkoxyated non-ionic surfactant has an average degree of alkoxylation of at least 3, preferably from 5 to 100, more preferably from 10 to 60.

25 Preferably ethoxylated non-ionic surfactant, more preferably an ethoxylated non-ionic surfactant having a hydrophobic lipophilic balance value of 8 to 18.

Examples of suitable non-ionic surfactants are commercially available from BASF under the tradename Lutensol AT80 (ethoxylated alcohol with an average degree of ethoxylation of 80 from BASF), from Clariant under the tradename Genapol T680 (ethoxylated alcohol with an

average degree of ethoxylation of 68), from Sigma Aldrich under the tradename Tween 20 (polysorbate with an average degree of ethoxylation of 20), from The Dow Chemical Company under the tradename Tergitol 15-S-30 (ethoxylated branched alcohol with an average degree of ethoxylation of 30).

5

Dispersed perfume

The liquid fabric softener composition of the present invention may comprise a dispersed perfume composition to provide a pleasant smell. By dispersed perfume we herein mean a perfume composition that is freely dispersed in the fabric softener composition and is not encapsulated. A perfume composition comprises one or more perfume raw materials. Perfume raw materials are the individual chemical compounds that are used to make a perfume composition. The choice of type and number of perfume raw materials is dependent upon the final desired scent. In the context of the present invention, any suitable perfume composition may be used. Those skilled in the art will recognize suitable compatible perfume raw materials for use in the perfume composition, and will know how to select combinations of ingredients to achieve desired scents.

Preferably, the level of dispersed perfume is at a level of from 0.1% to 10.0%, preferably from 0.5% to 7.5%, more preferably from 0.8% to 5.0% by total weight of the composition.

The perfume composition may comprise from 2.5% to 30%, preferably from 5% to 30% by total weight of perfume composition of perfume raw materials characterized by a logP lower than 3.0, and a boiling point lower than 250°C.

The perfume composition may comprise from 5% to 30%, preferably from 7% to 25% by total weight of perfume composition of perfume raw materials characterized by having a logP lower than 3.0 and a boiling point higher than 250°C. The perfume composition may comprise from 35% to 60%, preferably from 40% to 55% by total weight of perfume composition of perfume raw materials characterized by having a logP higher than 3.0 and a boiling point lower than 250°C. The perfume composition may comprise from 10% to 45%, preferably from 12% to 40% by total weight of perfume composition of perfume raw materials characterized by having a logP higher than 3.0 and a boiling point higher than 250°C.

10 Particles

The liquid fabric softener composition of the present invention may also comprise particles. The liquid fabric softener composition may comprise, based on the total liquid fabric softener composition weight, from 0.02% to 10%, preferably from 0.1% to 4%, more preferably from 0.25% to 2.5% of particles. Said particles include beads, pearlescent agents, benefit agent encapsulates, and mixtures thereof.

Encapsulated benefit agent:

The liquid fabric softener composition may comprise from 0.05% to 10%, preferably from 0.05% to 3.0%, more preferably from 0.05% to 2.0% by weight of encapsulated benefit agent. The benefit agent is selected from the group consisting of perfume composition, moisturizers, a heating or cooling agent, an insect/moth repellent, germ/mould/mildew control agents, softening agents, antistatic agents, anti-allergenic agents, UV protection agents, sun fade inhibitors, hueing dyes, enzymes and combinations thereof, color protection agents such as dye transfer inhibitors, bleach agents, and combinations thereof. Perfume compositions are preferred.

The benefit agent is encapsulated, for instance, as part of a core in one or more capsules. Such cores can comprise other materials, such as diluents, solvents and density balancing agents.

The capsules have a wall, which at least partially, preferably fully surrounds the benefit agent comprising core. The capsule wall material may be selected from the group consisting of melamine, polyacrylamide, silicones, silica, polystyrene, polyurea, polyurethanes, polyacrylate based materials, polyacrylate esters based materials, gelatin, styrene malic anhydride, polyamides, aromatic alcohols, polyvinyl alcohol, resorcinol-based materials, poly-isocyanate-based materials, acetals (such as 1,3,5-triol-benzene-gluteraldehyde and 1,3,5-triol-benzene melamine), starch, cellulose acetate phthalate and mixtures thereof.

Preferably, the capsule wall comprises one or more wall material comprising melamine, polyacrylate based material and combinations thereof.

Said melamine wall material may be selected from the group consisting of melamine crosslinked with formaldehyde, melamine-dimethoxyethanol crosslinked with formaldehyde, and combinations thereof.

Said polyacrylate based material may be selected from the group consisting of polyacrylate formed from methylmethacrylate/ dimethylaminomethyl methacrylate, polyacrylate formed from amine acrylate and/or methacrylate and strong acid, polyacrylate formed from carboxylic acid acrylate and/or methacrylate monomer and strong base, polyacrylate formed from an amine
5 acrylate and/or methacrylate monomer and a carboxylic acid acrylate and/or carboxylic acid methacrylate monomer and combinations thereof.

Said polystyrene wall material may be selected from polystyrene cross-linked with divinylbenzene.

Polyurea capsules can comprise a polyurea wall which is the reaction product of the
10 polymerisation between at least one polyisocyanate comprising at least two isocyanate functional groups and at least one amine, preferably a polyfunctional amine as a cross-linking and a colloidal stabilizer.

Polyurethane capsules can comprise a polyurethane wall which is the reaction product of
15 a polyfunctional isocyanate and a polyfunctional alcohol as a cross-linking agent and a colloidal stabilizer.

Suitable capsules can be obtained from Encapsys (Appleton, Wisconsin, USA). The fabric softener compositions may comprise combinations of different capsules, for example capsules having different wall materials and/or benefit agents.

As mentioned earlier, perfume compositions are the preferred encapsulated benefit agent. The
20 perfume composition comprises perfume raw materials. The perfume composition can further comprise essential oils, malodour reducing agents, odour controlling agents and combinations thereof.

The perfume raw materials are typically present in an amount of from 10% to 95%, preferably from 20% to 90% by weight of the capsule.

25 The perfume composition may comprise from 2.5% to 30%, preferably from 5% to 30% by total weight of perfume composition of perfume raw materials characterized by a logP lower than 3.0, and a boiling point lower than 250°C.

The perfume composition may comprise from 5% to 30%, preferably from 7% to 25% by total weight of perfume composition of perfume raw materials characterized by having a logP

lower than 3.0 and a boiling point higher than 250°C. The perfume composition may comprise from 35% to 60%, preferably from 40% to 55% by total weight of perfume composition of perfume raw materials characterized by having a logP higher than 3.0 and a boiling point lower than 250°C. The perfume composition may comprise from 10% to 45%, preferably from 12% to 40% by total weight of perfume composition of perfume raw materials characterized by having a logP higher than 3.0 and a boiling point higher than 250°C.

Ratio of encapsulated benefit agent to dispersed perfume oil

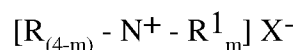
The liquid fabric softener composition may comprise a ratio of perfume oil encapsulates to dispersed perfume oil by weight of from 1:1 to 1:40, preferably from 1:2 to 1:20, more preferably from 1:3 to 1:10.

Additional Fabric Softening Active

The liquid fabric softener composition of the present invention may comprise from 0.01% to 10%, preferably from 0.1% to 10%, more preferably from 0.1% to 5% of additional fabric softening active. Suitable fabric softening actives, include, but are not limited to, materials selected from the group consisting of non-ester quaternary ammonium compounds, amines, fatty esters, sucrose esters, silicones, dispersible polyolefins, polysaccharides, fatty acids, softening oils, polymer latexes and combinations thereof.

Non-ester Quaternary ammonium compounds:

Suitable non-ester quaternary ammonium compounds comprise compounds of the formula:



wherein each R comprises either hydrogen, a short chain C₁-C₆, in one aspect a C₁-C₃ alkyl or hydroxyalkyl group, for example methyl, ethyl, propyl, hydroxyethyl, poly(C₂₋₃ alkoxy), polyethoxy, benzyl, or mixtures thereof; each m is 1, 2 or 3 with the proviso that the value of each m is the same; the sum of carbons in each R¹ may be C₁₂-C₂₂, with each R¹ being a hydrocarbyl,

or substituted hydrocarbyl group; and X^- may comprise any softener-compatible anion. The softener-compatible anion may comprise chloride, bromide, methylsulfate, ethylsulfate, sulfate, and nitrate. The softener-compatible anion may comprise chloride or methyl sulfate.

5 Non-limiting examples include dialkylenedimethylammonium salts such as dicanoladimethylammonium chloride, di(hard)tallowdimethylammonium chloride dicanoladimethylammonium methylsulfate, and mixtures thereof. An example of commercially available dialkylenedimethylammonium salts usable in the present invention is
10 Adogen® 472 and dihardtallow dimethylammonium chloride available from Akzo Nobel Arquad 2HT75.

Amines:

 Suitable amines include but are not limited to, materials selected from the group
15 consisting of amidoesteramines, amidoamines, imidazoline amines, alkyl amines, and combinations thereof. Suitable ester amines include but are not limited to, materials selected from the group consisting of monoester amines, diester amines, triester amines and combinations thereof. Suitable amidoamines include but are not limited to, materials selected from the group consisting of monoamido amines, diamido amines and combinations thereof. Suitable alkyl
20 amines include but are not limited to, materials selected from the group consisting of mono alkylamines, dialkyl amines quats, trialkyl amines, and combinations thereof.

Fatty Acid:

 The liquid fabric softener composition may comprise a fatty acid, such as a free fatty acid
25 as fabric softening active. The term “fatty acid” is used herein in the broadest sense to include unprotonated or protonated forms of a fatty acid. One skilled in the art will readily appreciate that the pH of an aqueous composition will dictate, in part, whether a fatty acid is protonated or unprotonated. The fatty acid may be in its unprotonated, or salt form, together with a counter ion, such as, but not limited to, calcium, magnesium, sodium, potassium, and the like. The term

“free fatty acid” means a fatty acid that is not bound to another chemical moiety (covalently or otherwise).

The fatty acid may include those containing from 12 to 25, from 13 to 22, or even from 16 to 20, total carbon atoms, with the fatty moiety containing from 10 to 22, from 12 to 18, or even from 14 (mid-cut) to 18 carbon atoms.

The fatty acids may be derived from (1) an animal fat, and/or a partially hydrogenated animal fat, such as beef tallow, lard, etc.; (2) a vegetable oil, and/or a partially hydrogenated vegetable oil such as canola oil, safflower oil, peanut oil, sunflower oil, sesame seed oil, rapeseed oil, cottonseed oil, corn oil, soybean oil, tall oil, rice bran oil, palm oil, palm kernel oil, coconut oil, other tropical palm oils, linseed oil, tung oil, castor oil, etc. ; (3) processed and/or bodied oils, such as linseed oil or tung oil via thermal, pressure, alkali-isomerization and catalytic treatments; (4) combinations thereof, to yield saturated (e.g. stearic acid), unsaturated (e.g. oleic acid), polyunsaturated (linoleic acid), branched (e.g. isostearic acid) or cyclic (e.g. saturated or unsaturated α -disubstituted cyclopentyl or cyclohexyl derivatives of polyunsaturated acids) fatty acids.

Mixtures of fatty acids from different fat sources can be used.

The cis/trans ratio for the unsaturated fatty acids may be important, with the cis/trans ratio (of the C18:1 material) being from at least 1:1, at least 3:1, from 4:1 or even from 9:1 or higher.

Branched fatty acids such as isostearic acid are also suitable since they may be more stable with respect to oxidation and the resulting degradation of color and odor quality.

The fatty acid may have an iodine value from 0 to 140, from 50 to 120 or even from 85 to 105.

Polysaccharides:

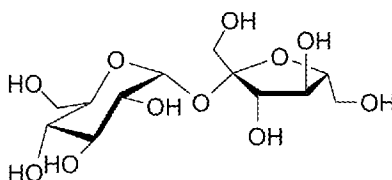
The liquid fabric softener composition may comprise a polysaccharide as a fabric softening active, such as cationic starch. Suitable cationic starches for use in the present

compositions are commercially-available from Cerestar under the trade name C*BOND[®] and from National Starch and Chemical Company under the trade name CATO[®] 2A.

Sucrose esters:

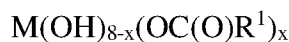
- 5 The liquid fabric softener composition may comprise a sucrose esters as a fabric softening active. Sucrose esters are typically derived from sucrose and fatty acids. Sucrose ester is composed of a sucrose moiety having one or more of its hydroxyl groups esterified.

Sucrose is a disaccharide having the following formula:



10 Alternatively, the sucrose molecule can be represented by the formula: $M(OH)_8$, wherein M is the disaccharide backbone and there are total of 8 hydroxyl groups in the molecule.

Thus, sucrose esters can be represented by the following formula:



- 15 wherein x is the number of hydroxyl groups that are esterified, whereas (8-x) is the hydroxyl groups that remain unchanged; x is an integer selected from 1 to 8, alternatively from 2 to 8, alternatively from 3 to 8, or from 4 to 8; and R^1 moieties are independently selected from C_1 - C_{22} alkyl or C_1 - C_{30} alkoxy, linear or branched, cyclic or acyclic, saturated or unsaturated, substituted or unsubstituted.

- 20 The R^1 moieties may comprise linear alkyl or alkoxy moieties having independently selected and varying chain length. For example, R^1 may comprise a mixture of linear alkyl or alkoxy moieties wherein greater than 20% of the linear chains are C_{18} , alternatively greater than 50% of the linear chains are C_{18} , alternatively greater than 80% of the linear chains are C_{18} .

- 25 The R^1 moieties may comprise a mixture of saturate and unsaturated alkyl or alkoxy moieties. The iodine value (IV) of the sucrose esters suitable for use herein ranges from 1 to 150, or from 2 to 100, or from 5 to 85. The R^1 moieties may be hydrogenated to reduce the degree of

unsaturation. In the case where a higher IV is preferred, such as from 40 to 95, then oleic acid and fatty acids derived from soybean oil and canola oil are suitable starting materials.

The unsaturated R¹ moieties may comprise a mixture of “cis” and “trans” forms the unsaturated sites. The “cis” / “trans” ratios may range from 1:1 to 50:1, or from 2:1 to 40:1, or
5 from 3:1 to 30:1, or from 4:1 to 20:1.

Dispersible Polyolefins and latexes:

Generally, all dispersible polyolefins that provide fabric softening benefits can be used as fabric softening active in the present invention. The polyolefins can be in the form of
10 waxes, emulsions, dispersions or suspensions.

The polyolefin may be chosen from a polyethylene, polypropylene, or combinations thereof. The polyolefin may be at least partially modified to contain various functional groups, such as carboxyl, alkylamide, sulfonic acid or amide groups. The polyolefin may be at least partially carboxyl modified or, in other words, oxidized.

15 Non-limiting examples of fabric softening active include dispersible polyethylene and polymer latexes. These agents can be in the form of emulsions, latexes, dispersions, suspensions, and the like. In one aspect, they are in the form of an emulsion or a latex. Dispersible polyethylenes and polymer latexes can have a wide range of particle size diameters (χ_{50}) including but not limited to from 1 nm to 100 μm ; alternatively from 10 nm to 10 μm . As
20 such, the particle sizes of dispersible polyethylenes and polymer latexes are generally, but without limitation, smaller than silicones or other fatty oils.

Generally, any surfactant suitable for making polymer emulsions or emulsion polymerizations of polymer latexes can be used as emulsifiers for polymer emulsions and latexes used as fabric softeners active in the present invention. Suitable surfactants include anionic,
25 cationic, and nonionic surfactants, and combinations thereof. In one aspect, such surfactants are nonionic and/or anionic surfactants. In one aspect, the ratio of surfactant to polymer in the fabric softening active is 1:5, respectively.

Silicone:

The liquid fabric softener composition may comprise a silicone as fabric softening active. Useful silicones can be any silicone comprising compound. The silicone polymer may be selected from the group consisting of cyclic silicones, polydimethylsiloxanes, aminosilicones, cationic silicones, silicone polyethers, silicone resins, silicone urethanes, and combinations thereof. The silicone may be a polydialkylsilicone, alternatively a polydimethyl silicone (polydimethyl siloxane or "PDMS"), or a derivative thereof. The silicone may be chosen from an aminofunctional silicone, amino-polyether silicone, alkyloxylated silicone, cationic silicone, ethoxylated silicone, propoxylated silicone, ethoxylated/propoxylated silicone, quaternary silicone, or combinations thereof.

Further Perfume Delivery Technologies

The liquid fabric softener composition may comprise one or more perfume delivery technologies that stabilize and enhance the deposition and release of perfume ingredients from treated substrate. Such perfume delivery technologies can be used to increase the longevity of perfume release from the treated substrate. Perfume delivery technologies, methods of making certain perfume delivery technologies and the uses of such perfume delivery technologies are disclosed in US 2007/0275866 A1.

The liquid fabric softener composition may comprise from 0.001% to 20%, or from 0.01% to 10%, or from 0.05% to 5%, or even from 0.1% to 0.5% by weight of the perfume delivery technology. Said perfume delivery technologies may be selected from the group consisting of: pro-perfumes, cyclodextrins, starch encapsulated accord, zeolite and inorganic carrier, and combinations thereof.

Amine Reaction Product (ARP): For purposes of the present application, ARP is a subclass or species of pro-perfumes. One may also use "reactive" polymeric amines in which the amine functionality is pre-reacted with one or more PRMs to form an amine reaction product (ARP). Typically the reactive amines are primary and/or secondary amines, and may be part of a polymer or a monomer (non-polymer). Such ARPs may also be mixed with additional PRMs to provide benefits of polymer-assisted delivery and/or amine-assisted delivery. Nonlimiting examples of polymeric amines include polymers based on polyalkylimines, such as polyethyleneimine (PEI), or polyvinylamine (PVAm). Nonlimiting examples of monomeric (non-polymeric) amines include hydroxyl amines, such as 2-aminoethanol and its alkyl substituted derivatives, and

aromatic amines such as anthranilates. The ARPs may be premixed with perfume or added separately in leave-on or rinse-off applications. A material that contains a heteroatom other than nitrogen, for example oxygen, sulfur, phosphorus or selenium, may be used as an alternative to amine compounds. The aforementioned alternative compounds can be used in combinations with amine compounds. A single molecule may comprise an amine moiety and one or more of the alternative heteroatom moieties, for example, thiols, and phosphines. The benefit may include improved delivery of perfume as well as controlled perfume release.

Deposition Aid

The liquid fabric softener composition may comprise, based on the total liquid fabric softener composition weight, from 0.0001% to 3%, preferably from 0.0005% to 2%, more preferably from 0.001% to 1% of a deposition aid. The deposition aid may be a cationic or amphoteric polymer. The cationic polymer may comprise a cationic acrylate. Cationic polymers in general and their method of manufacture are known in the literature. Deposition aids can be added concomitantly with particles or directly in the liquid fabric softener composition. Preferably, the deposition aid is selected from the group consisting of polyvinylformamide, partially hydroxylated polyvinylformamide, polyvinylamine, polyethylene imine, ethoxylated polyethylene imine, polyvinylalcohol, polyacrylates, and combinations thereof.

The weight-average molecular weight of the polymer may be from 500 to 5000000 or from 1000 to 2000000 or from 2500 to 1500000 Dalton, as determined by size exclusion chromatography relative to polyethyleneoxide standards using Refractive Index (RI) detection. In one aspect, the weight-average molecular weight of the cationic polymer may be from 500 to 37500 Dalton.

METHODS

For each method applied to a fabric softener composition, a visually homogeneous sample is used. In case the fabric softener composition is visually not homogeneous, the entire fabric softener composition is homogenized in a way to avoid air entrapment, prior to sampling to ensure representative sampling.

Method for determining viscosity and dynamic yield stress

Viscosity and dynamic yield stress are measured using a controlled stress rheometer (such as an HAAKE MARS from Thermo Scientific, or equivalent), using a 60 mm parallel plate and a gap size of 500 microns at 20°C. The viscosity and dynamic yield stress are obtained by measuring quasi steady state shear stress as a function of shear rate in the range starting from 10 s⁻¹ to 10⁻⁴ s⁻¹, taking 25 points logarithmically distributed over the shear rate range. Quasi-steady state is defined as the shear stress value once variation of shear stress over time is less than 3%, after at least 30 seconds and a maximum of 60 seconds at a given shear rate. Variation of shear stress over time is continuously evaluated by comparison of the average shear stress measured over periods of 3 seconds. If after 60 seconds measurement at a certain shear rate, the shear stress value varies more than 3%, the final shear stress measurement is defined as the quasi state value for calculation purposes. The viscosity of the fabric softener composition is defined as the measured shear stress divided by the applied shear rate of 10 s⁻¹.

Shear stress data is then fitted using least squares method in logarithmic space as a function of shear rate following a Herschel – Bulkley model:

$$\tau = \tau_0 + k\dot{\gamma}^n$$

wherein τ is the measured equilibrium quasi steady state shear stress at each applied shear rate $\dot{\gamma}$, τ_0 is the fitted dynamic yield stress. k and n are fitting parameters.

Method of determining pH of a fabric softener composition

The pH is measured on the neat fabric softener composition, using a Sartorius PT-10P pH meter with gel-filled probe (such as the Toledo probe, part number 52 000 100), calibrated according to the instructions manual.

Method for determining fabric softener active by CatSO₃ titration

The fabric softener activity is determined by cationic CatSO₃ titration as described in ISO2871.

Specifically, to a sample containing cationic fabric softener active, a mixed indicator composed of a cationic and an anionic dye is added under stirring in a water-chloroform system. The cationic fabric softener active - anionic dye complex is blue and chloroform soluble, whereas the red cationic dye remains dissolved in the aqueous phase. Upon titration with anionic surfactant (standardized sodium dodecyl sulfate, "NaLS"), the blue dye-surfactant complex in the chloroform breaks and a colorless cationic fabric softening active – anionic titrant complex is formed while the liberated blue dye migrates back into the aqueous phase. A color change from blue to grey in the chloroform layer indicates the endpoint. Excess anionic surfactant forms a complex with the red cationic dye, giving a pink to red color to the chloroform layer.

Calculation:

$$\% \text{ Cationic SO}_3 \text{ equivalent} = [(V * N)] * 0.080 * 100 / W$$

Where:

V = mL NaLS Standard Solution

N = Normality of NaLS Standard Solution

0.080 = Milliequivalent Weight of SO₃

W = Sample weight in g

Method for determining dispenser residue:

Following setup is used to simulate the final rinse cycle in the dispenser of the washing machine.

The dispenser drawer PP-T40 corresponding to a Miele Novotronic W986 washing machine is fixed in horizontal position. Then, 25 grams of the fabric softener composition is added into the fabric softener composition compartment of the dispenser drawer.

A total flow of 3.47 kg of water of 2.5 mmol/L hardness is flushed through the dispenser in 80 seconds at 20°C by using a "cylindrical nozzle" located horizontally 2.5 cm above and parallel to the dispenser compartment. Such cylindrical nozzle having a diameter of 4 cm and a length of

12.8 cm with 3 orifices of 0.5 cm diameter located corresponding to the orifices of the fabric care composition compartment of the dispenser drawer.

Rinse water containing the fabric care composition is collected in a bucket containing 5 kg of 2.5 mmol/L hardness water and homogenized with an IKA EURO-ST P VC with an R 2302 4-bladed Propeller stirrer at 450 rpm for 1 minute after water flow has finished. The total rinse water mass obtained at the end of the dispenser residue test is 8.47 kg.

The fabric softener activity, measured using CatSO₃ titration, is measured of the fabric softener composition added into the dispenser and of the rinse water.

10 Dispensing residue expressed in % is calculated as:

$$\frac{0.025 \cdot \text{CatSO}_3(\text{fabric softener composition}) - 8.47 \cdot \text{CatSO}_3(\text{rinse water})}{0.025 \cdot \text{CatSO}_3(\text{fabric softener composition})}$$

wherein

CatSO₃(fabric softener composition) is the % Cationic SO₃ Equivalent determined by CatSO₃ titration of the fabric softener composition;

15 CatSO₃(rinse water) is the % Cationic SO₃ Equivalent determined by CatSO₃ titration of the rinse water collected at the end of the dispenser residue test.

Method for determining average cellulose fiber diameter:

20 The average cellulose fiber diameter can be determined directly from the cellulose fiber raw material or from the fabric softener composition comprising cellulose fibers.

A) Cellulose fibers raw material: A cellulose fibers sample is prepared by adding 1% dry matter of cellulose fibers to water and activating it with a high pressure homogenizer (PANDA from GEA, 350 bars, 10 passes). Obtained sample is analyzed.

B) Fabric softener composition comprising cellulose fibers:

25 The fabric softener composition sample is centrifuged at 4 000 rpm for 10 minutes using a 5804 centrifuge from Eppendorf, in order to remove potential particles to avoid interference in the

measurement of the fiber size. The clarified fabric softener composition is then decanted as the supernatant. The cellulose fibers present in the fabric softener composition (supernatant) are redispersed in ethanol using an Ultra Turrax device from IKA, T25 S 25 N - 25 G - ST, at a speed of 21 000 rpm for 10 minutes. Then, sample is centrifuged at 4 000 rpm for 10 minutes using a 5804 centrifuge from Eppendorf and supernatant is removed. Remaining cellulose fibers at the bottom are analyzed. Repeat the process as many times as needed to have enough amount for the analysis.

Average cellulose fiber diameter is analysed using Atomic force microscopy (AFM). A 0.02% cellulose fiber dispersion in demineralized water is prepared, and a drop of this dispersion is deposited onto freshly cleaved mica (highest grade V1 Mica, 15x15mm – TED PELLA , INC., or equivalent). The sample is then allowed to dry in an oven at 40°C.

The mica sheet is mounted in an AFM (Nanosurf Flex AFM, ST Instruments or equivalent) and imaged in air under ambient conditions using a Si cantilever in dynamic mode with dynamic mode tip (ACTA -50 - APPNANO or equivalent). The image dimensions are 20 micron by 20 micron, and 256 points per line are captured.

The AFM image is opened using suitable AFM data analysis software (such as Mountainsmap SPM 7.3, ST Instruments, or equivalent). Each image is leveled line by line. One or more profiles are extracted crossing perpendicularly one or multiple fibers avoiding bundles of fibers, and from each profile, a distance measurement is performed to obtain the diameter of the fibers. Ten diameter measurements are performed per picture counting each fiber only once.

Three sets of measurements (sample preparation, AFM measurement and image analysis) are made. The arithmetic mean of all fibers measured in all images is the Average Cellulose Fiber Diameter.

Processes of Making the Fabric softener composition of the invention

The compositions of the present invention can be formulated into any suitable form and prepared by any process chosen by the formulator, non-limiting examples of which are described in Applicant's examples and in US 2013/0109612 A1 which is incorporated herein by reference.

The compositions disclosed herein may be prepared by combining the components thereof in any convenient order and by mixing, e.g., agitating, the resulting component combination to form a phase stable fabric care composition. A fluid matrix may be formed containing at least a major proportion, or even substantially all, of the fluid components with the fluid components being thoroughly admixed by imparting shear agitation to this liquid combination. For example, rapid stirring with a mechanical stirrer may be employed.

The liquid fabric softener compositions described herein can also be made as follows:

– Taking an apparatus A (see Figure 1) comprising:

at least a first inlet 1A and a second inlet 1B; a pre-mixing chamber 2, the pre-mixing chamber 2 having an upstream end 3 and a downstream end 4, the upstream end 3 of the pre-mixing chamber 2 being in liquid communication with the first inlet 1A and the second inlet 1B; an orifice component 5, the orifice component 5 having an upstream end 6 and a downstream end 7, the upstream end of the orifice component 6 being in liquid communication with the downstream end 4 of the pre-mixing chamber 2, wherein the orifice component 5 is configured to spray liquid in a jet and produce shear and/or turbulence in the liquid; a secondary mixing chamber 8, the secondary mixing chamber 8 being in liquid communication with the downstream end 7 of the orifice component 5; at least one outlet 9 in liquid communication with the secondary mixing chamber 8 for discharge of liquid following the production of shear and/or turbulence in the liquid, the inlet 1A, pre-mixing chamber 2, the orifice component 5 and secondary mixing chamber 8 are linear and in straight line with each other, at least one outlet 9 being located at the downstream end of the secondary mixing chamber 8; the orifice component 5 comprising at least one orifice unit, a specific example, as shown in Figure 2, is that the orifice component 5 comprises two orifice units 10 and 11 arranged in series to one another and each orifice unit comprises an orifice plate 12 comprising at least one orifice 13, an orifice chamber 14 located upstream from the orifice plate 12 and in liquid communication with the orifice plate 12; and wherein neighboring orifice plates are distinct from each other;

– connecting one or more suitable liquid pumping devices to the first inlet 1A and to the second inlet 1B;

– pumping a second liquid composition into the first inlet 1A, and, pumping a liquid fabric softener active composition into the second inlet 1B, wherein the operating pressure of the apparatus is from 2.5 bar to 50 bar, from 3.0 bar to 20 or from 3.5 bar to 10 bar the operating pressure being the pressure of the liquid as measured in the first inlet 1A near to inlet 1B. The operating pressure at the outlet of apparatus A needs to be high enough to prevent cavitation in the orifice;

– allowing the liquid fabric softener active and the second liquid composition to pass through the apparatus A at a desired flow rate, wherein as they pass through the apparatus A, they are dispersed one into the other, herein, defined as a liquid fabric softener intermediate.

– passing said liquid fabric softener intermediate from Apparatus A's outlet, to Apparatus B's (Figure 3) inlet 16 to subject the liquid fabric softener intermediate to additional shear and/or turbulence for a period of time within Apparatus B.

– circulating said liquid fabric softener intermediate within apparatus B with a circulation Loop pump 17 at a Circulation Loop 18 Flow Rate equal to or greater than said inlet liquid fabric softener intermediate flow rate in said Circulation Loop System. A tank, with or without a recirculation loop, or a long conduit may also be employed to deliver the desired shear and/or turbulence for the desired time.

– adding by means of a pump 19, piping and in-line fluid injector 20, an adjunct fluid, in one aspect, but not limited to a dilute salt solution, into Apparatus B to mix with the liquid fabric softener intermediate

– allowing the liquid fabric softener composition with the desired microstructure to exit Apparatus B 21 at a rate equal to the inlet flow rate into Apparatus B.

– passing said liquid fabric softener composition exiting Apparatus B outlet through a heat exchanger to be cooled to ambient temperature, if necessary.

– discharging the resultant liquid fabric softener composition produced out of the outlet of the process.

The process comprises introducing, in the form of separate streams, the fabric softener active in a liquid form and a second liquid composition comprising other components of a fabric softener composition into the pre-mixing chamber 2 of Apparatus A so that the liquids pass through

the orifice component 5. The fabric softener active in a liquid form and the second liquid composition pass through the orifice component 5 under pressure. The fabric softener active in liquid form and the second liquid composition can be at the same or different operating pressures. The orifice component 5 is configured, either alone, or in combination with some other component, to mix the liquid fabric softener active and the second liquid composition and/or produce shear and/or turbulence in each liquid, or the mixture of the liquids.

The liquids can be supplied to the apparatus A and B in any suitable manner including, but not limited to through the use of pumps and motors powering the same. The pumps can supply the liquids to the apparatus A under the desired operating pressure. In one embodiment, an '8 frame block-style manifold' is used with a 781 type Plunger pump available from CAT pumps (1681 94th Lane NE, Minneapolis, MN 55449).

The operating pressure of conventional shear and/or turbulence apparatuses is typically between 2 bar and 490 bar. The operating pressure is the pressure of the liquid in the inlet 1A near inlet 1B. The operating pressure is provided by the pumps.

The operating pressure of Apparatus A is measured using a Cerphant T PTP35 pressure switch with a RVS membrane, manufactured by Endress Hauser (Endress+Hauser Instruments, International AG, Kaegenstrasse 2, CH-4153, Reinach). The switch is connected with the inlet 1A near inlet 1B using a conventional thread connection (male thread in the pre-mix chamber housing, female thread on the Cerphant T PTP35 pressure switch).

The operating pressure of Apparatus A may be lower than conventional shear and/or turbulence processes, yet the same degree of liquid mixing is achievable as seen with processes using conventional apparatuses. Also, at the same operating pressures, the process of the present invention results in better mixing than is seen with conventional shear and/or turbulence processes.

As the fabric softener active and the second liquid composition flow through the Apparatus A, they pass through the orifices 13 and 15 of the orifice component 5. As they do, they exit the orifice 13 and/or 15 in the form of a jet. This jet produces shear and/or turbulence in the fabric softener active and the second liquid composition, thus dispersing them one in the other to form a uniform mixture.

In conventional shear and/or turbulence processes, the fact that the liquids are forced through the orifice 13 and/or 15 under high pressure causes them to mix. This same degree of mixing is achievable at lower pressures when the liquids are forced through a series of orifices, rather than one at a high pressure. Also, at equivalent pressures, the process of the present invention results in better liquid mixing than shear and/or turbulence processes, due to the fact that the liquids are now forced through a series of orifices.

A given volume of liquid can have any suitable residence time and/or residence time distribution within the apparatus A. Some suitable residence times include, but are not limited to from 1 microsecond to 1 second, or more. The liquid(s) can flow at any suitable flow rate through the apparatus A. Suitable flow rates range from 1 to 1 500 L/min, or more, or any narrower range of flow rates falling within such range including, but not limited to from 5 to 1 000 L/min.

For Apparatus B Circulating Loop System example, one may find it convenient to characterize the circulation flow by a Circulation Loop Flow Rate Ratio which is equal to the Circulation Flow Rate divided by the Inlet Flow Rate. Said Circulation Loop Flow Rate Ratio for producing the desired fabric softener composition microstructure can be from 1 to 100, from 1 to 50, and even from 1 to 20. The fluid flow in the circulation loop imparts shear and turbulence to the liquid fabric softener to transform the liquid fabric softener intermediate into a desired dispersion microstructure.

The duration of time said liquid fabric softener intermediate spends in said Apparatus B may be quantified by a Residence Time equal to the total volume of said Circulation Loop System divided by said fabric softener intermediate inlet flow rate. Said Circulation Loop Residence Time for producing desirable liquid fabric softener composition microstructures may be from 0.1 seconds to 10 minutes, from 1 second to 1 minute, or from 2 seconds to 30 seconds. It is desirable to minimize the residence time distribution.

Shear and/or turbulence imparted to said liquid fabric softener intermediate may be quantified by estimating the total kinetic energy per unit fluid volume. The kinetic energy per unit volume imparted in the Circulation Loop System to the fabric softener intermediate in Apparatus B may be from 10 to 1 000 000 $\text{g.cm}^{-1}.\text{s}^{-2}$, from 50 to 500 000 $\text{g.cm}^{-1}.\text{s}^{-2}$, or from 100 to 100 000 $\text{g.cm}^{-1}.\text{s}^{-2}$. The liquid(s) flowing through Apparatus B can flow at any suitable flow rate. Suitable inlet and outlet flow rates range from 1 to 1 500 L/min, or more, or any narrower range of flow

rates falling within such range including, but not limited to from 5 to 1 000 L/min. Suitable Circulation Flow Rates range from 1 L/min to 20 000 L/min or more, or any narrower range of flow rates falling within such range including but not limited to from 5 to 10 000 L/min. Apparatus A is ideally operated at the same time as Apparatus B to create a continuous process. The liquid fabric softener intermediate created in Apparatus A may also be stored in a suitable vessel and processed through apparatus B at a later time.

EXAMPLES

The fabric softener compositions of Examples 1-8 were prepared by first preparing dispersions of the quaternary ammonium ester softener active ("FSA") using apparatus A and B in a continuous fluid making process with 3 orifices. Coconut oil and isopropanol were added to the hot FSA at 81°C to form an FSA premix. Heated FSA premix at 81°C and heated deionized water at 65°C containing adjunct materials NaHEDP, HCl, Formic Acid, and the preservative were fed using positive displacement pumps, through Apparatus A, through apparatus B, a circulation loop fitted with a centrifugal pump. The liquid fabric softener composition was immediately cooled to 25°C with a plate heat exchanger. The total flow rate was 3.1 kg/min; pressure at Apparatus A Inlet 5 bar; pressure at Apparatus A Outlet 2.5 bar; Apparatus B Circulation Loop Flow rate Ratio 8.4; Apparatus B Kinetic Energy $18\,000\text{ g}\cdot\text{cm}^{-1}\cdot\text{s}^{-2}$; Apparatus B Residence Time 14 s; Apparatus B Outlet pressure 3 bar.

The fabric softener compositions were finished by adding the remaining ingredients provided in Table 1 below using a Ytron-Y high speed mixer operated at 20 Hz for 15-20 minutes. Table 1 shows the overall composition of Examples 1-8. In examples 5 to 8, a premix comprising 3% microfibrinous cellulose was added in a last step to the liquid fabric softener composition using a Silverson Homogenizer L5M, operating at 4 500 rpm for 5 min, to achieve a homogeneous dispersion. The preparation of the 3% premix comprising the microfibrinous cellulose was obtained by mixing the 10% aqueous cellulose fiber paste as obtained from the supplier in the non-thickened liquid fabric softener composition with an IKA Ultra Turrax high shear mixer for 10 min at 21500 rpm.

Table 1: Liquid fabric softener compositions examples 1 through 8. The examples marked with an asterisk (*) are comparative examples.

	Weight %			
	Ex. 1*	Ex. 2*	Ex. 3*	Ex. 4*
deionized water	Balance	Balance	Balance	Balance
NaHEDP	0.007	0.007	0.007	0.007
Formic acid	0.044	0.044	0.044	0.044
HCl	0.009	0.009	0.009	0.009
Preservative ^a	0.022	0.022	0.022	0.022
FSA ^b	7.6	7.6	7.6	7.6
Antifoam ^c	0.1	0.1	0.1	0.1
coconut oil	0.3	0.3	0.3	0.3
isopropanol	0.78	0.78	0.77	0.77
Encapsulated perfume ^d	0.15	0.15	0.15	0.15
dye	0.015	0.015	0.015	0.015
Cationic polymeric thickener ^e	0.15	0.20	0.28	0.35
Cellulose fibers ^f	-	-	-	-
Perfume	1.0	1.0	1.0	1.0
Dynamic yield stress	0.000 Pa	0.090 Pa	0.380 Pa	0.380 Pa
Viscosity at 10 s ⁻¹	172 mPa.s	284 mPa.s	474 mPa.s	662 mPa.s
Dispenser residue	11%	14%	34%	39%

Table 1 continued

	Weight %			
	Ex. 5	Ex. 6	Ex. 7	Ex. 8
deionized water	Balance	Balance	Balance	Balance
NaHEDP	0.007	0.007	0.007	0.007
Formic acid	0.043	0.043	0.043	0.043
HCl	0.009	0.009	0.009	0.009
Preservative ^a	0.022	0.021	0.021	0.021
FSA ^b	7.4	7.4	7.3	7.3
Antifoam ^c	0.1	0.1	0.1	0.1
coconut oil	0.3	0.3	0.3	0.2
isopropanol	0.76	0.76	0.75	0.75
Encapsulated perfume ^d	0.15	0.15	0.15	0.15
dye	0.015	0.015	0.015	0.015
Cationic polymeric thickener ^e	-	-	-	-
Microfibrinous cellulose ^f	0.22	0.27	0.34	0.36
Perfume	1.0	1.0	1.0	1.0
Dynamic yield stress	0.060 Pa	0.110 Pa	0.200 Pa	0.230 Pa
Viscosity at 10 s ⁻¹	208 mPa.s	230 mPa.s	367 mPa.s	600 mPa.s
Dispenser residue	12%	12%	6%	5%

^a Proxel GXL, 20% aqueous dipropylene glycol solution of 1,2-benzisothiazolin-3-one, supplied by Lonza.

^b N,N-bis(hydroxyethyl)-N,N-dimethyl ammonium chloride fatty acid ester. The iodine value of the parent fatty acid of this material is between 18 and 22. The material as obtained from Evonik contains impurities in the form of free fatty acid, the monoester form of N,N-bis(hydroxyethyl)-N,N-dimethyl ammonium chloride fatty acid ester, and fatty acid esters of N,N-bis(hydroxyethyl)-N-methylamine.

^c MP10[®], supplied by Dow Corning, 8% activity

^d as described in US 8,765,659, expressed as 100% encapsulated perfume oil

^e Rheovis[®] CDE, cationic polymeric thickener supplied by BASF

^f Exilva[®], microfibrinous cellulose, expressed as 100% dry matter, supplied as 10% aqueous dispersion by Borregaard

5

When the fabric softener composition partially remains as residue in the dispenser and hence is not fully mixed with the rinse water, the fabric softener composition only partially gets in contact with the fabrics and hence benefits, such as softening benefits, are reduced. Additional consumer dissatisfaction is created because such fabric softener residues make the dispenser look
10 dirty and can even lead to the formation of malodor.

Comparative examples 1 to 4 comprising increasing level of a traditional cationic polymer to thicken the composition improved the richness appearance connotation of the compositions. Furthermore, comparative examples 2 to 4 also possessed a dynamic yield stress which improves phase stability over time. However, with higher viscosity and the presence of a
15 dynamic yield stress, it became more difficult to fully dispense the fabric softener composition from the dispenser. The increasing viscosities led to increasing residues from 11% to 39%.

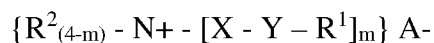
Examples 5 to 8 according to the present invention comprised increasing levels of cellulose fibers which resulted also in increasing viscosity to connote richness while all of the examples 5 to 8 comprised a dynamic yield stress. Surprisingly, because of the presence of
20 cellulose fibers the dispenser residue did not increase at higher viscosities nor in the presence of a dynamic yield stress. In fact, example 7 and 8 even showed a decrease in dispenser residue even though the viscosity and yield stress was higher than in example 5 and 6.

CLAIMS

What is claimed is:

1. A liquid fabric softener composition comprising:
 - a) from 3.0% to 20% by weight of the total composition of a quaternary ammonium ester softening active;
 - b) cellulose fibres;

wherein the viscosity measured at 10 s^{-1} at 20°C of the fabric softener composition is from 200 mPa.s to 1000 mPa.s and the dynamic yield stress at 20°C of the fabric softener composition is from 0.001 Pa to 1.0 Pa.
2. The liquid fabric softener composition according to claim 1, wherein the viscosity measured at 10 s^{-1} at 20°C of the fabric softener composition is from 250 mPa.s to 900 mPa.s, preferably from 300 mPa.s to 800 mPa.s, more preferably from 350 mPa.s to 700 mPa.s.
3. The liquid fabric softener composition according to any preceding claim, wherein the dynamic yield stress at 20°C of the fabric softener composition is from 0.002 Pa to 0.9 Pa, preferably from 0.005 Pa to 0.8 Pa, more preferably from 0.010 Pa to 0.5 Pa.
4. The liquid fabric softener composition according to any preceding claim, wherein the quaternary ammonium ester softening active is present at a level of from 4.0% to 18%, preferably from 5.0% to 15%, more preferably from 7.0% to 12% by weight of the composition.
5. The liquid fabric softener composition according to any preceding claim, further comprising a non-ionic surfactant at a level of from 0.01% to 5.0%, preferably from 0.1% to 3.0%, more preferably from 0.5% to 2.0% by weight of the composition.
6. The liquid fabric softener composition according to any preceding claim, wherein the quaternary ammonium ester softening active has the following formula:



wherein:

m is 1, 2 or 3 with proviso that the value of each m is identical;

each R^1 is independently hydrocarbyl, or branched hydrocarbyl group, preferably R^1 is linear, more preferably R^1 is partially unsaturated linear alkyl chain;
 each R^2 is independently a C_1 - C_3 alkyl or hydroxyalkyl group, preferably R^2 is selected from methyl, ethyl, propyl, hydroxyethyl, 2-hydroxypropyl, 1-methyl-2-hydroxyethyl, poly(C_{2-3} alkoxy), polyethoxy, benzyl;
 each X is independently $(CH_2)_n$, $CH_2-CH(CH_3)-$ or $CH-(CH_3)-CH_2-$ and
 each n is independently 1, 2, 3 or 4, preferably each n is 2;
 each Y is independently $-O-(O)C-$ or $-C(O)-O-$;
 A^- is independently selected from the group consisting of chloride, methylsulfate, and ethylsulfate, preferably A^- is selected from the group consisting of chloride and methyl sulfate;

with the proviso that the sum of carbons in each R^1 , when Y is $-O-(O)C-$, is from 13 to 21, preferably the sum of carbons in each R^1 , when Y is $-O-(O)C-$, is from 13 to 19.

7. The liquid fabric softener composition according to any preceding claim, wherein the cellulose fiber is present at a level of from 0.01% to 5.0 %, preferably from 0.05% to 1.0 %, more preferably from 0.10% to 0.75% by weight of the composition.
8. The liquid fabric softener composition according to any preceding claim, wherein the cellulose fiber is microfibrinous cellulose, preferably microfibrinous cellulose derived from: bacterial or botanical origin, preferably from sources selected from the group consisting of citrus peel, fruit; vegetables; plants, wood, and mixtures thereof, more preferably from wood or jute.
9. The liquid fabric softener composition according to any preceding claim, wherein the cellulose fibers have an average diameter from 10 nm to 350 nm, preferably from 30 nm to 250 nm, more preferably from 50 nm to 200 nm.
10. The liquid fabric softener composition according to any preceding claim further comprising dispersed perfume at a level from 0.1% to 10.0%, preferably from 0.5% to 7.5%, more preferably from 0.8% to 5.0% by weight of the composition.
11. The liquid fabric softener composition according to any preceding claim further comprising a dye, preferably at a level from 0.0001% to 0.1%, more preferably from 0.001% to 0.05% by weight of the composition.

12. The liquid fabric softener composition according to any preceding claim further comprising from 0.05% to 10%, preferably from 0.05% to 3.0%, more preferably from 0.05% to 2.0 % by total weight of the composition of encapsulated benefit agent, said encapsulated benefit agent is encapsulated in capsules wherein said capsules comprise a capsule wall, said capsule wall comprising wall material selected from the group consisting of melamine, polyacrylamide, silicones, silica, polystyrene, polyurea, polyurethanes, polyacrylate based materials, polyacrylate esters based materials, gelatin, styrene malic anhydride, polyamides, aromatic alcohols, polyvinyl alcohol, resorcinol-based materials, poly-isocyanate-based materials, acetals (such as 1,3,5-triol-benzene-gluteraldehyde and 1,3,5-triol-benzene melamine), starch, cellulose acetate phthalate and mixtures thereof, preferably the capsule wall comprises one or more wall material comprising melamine, polyacrylate based material and combinations thereof.
13. A method for softening fabrics comprising the steps of:
- a) adding fabrics in an automatic or semi-automatic washing machine;
 - b) dosing the liquid fabric softener composition according to any preceding claim into the fabric softener compartment of the washing machine dispenser;
 - c) rinsing fabrics in a solution containing the fabric softener composition according to any preceding claim.
14. Use of cellulose fibers in a liquid fabric softener composition to avoid dispenser residue in an automatic or semi-automatic washing machine.

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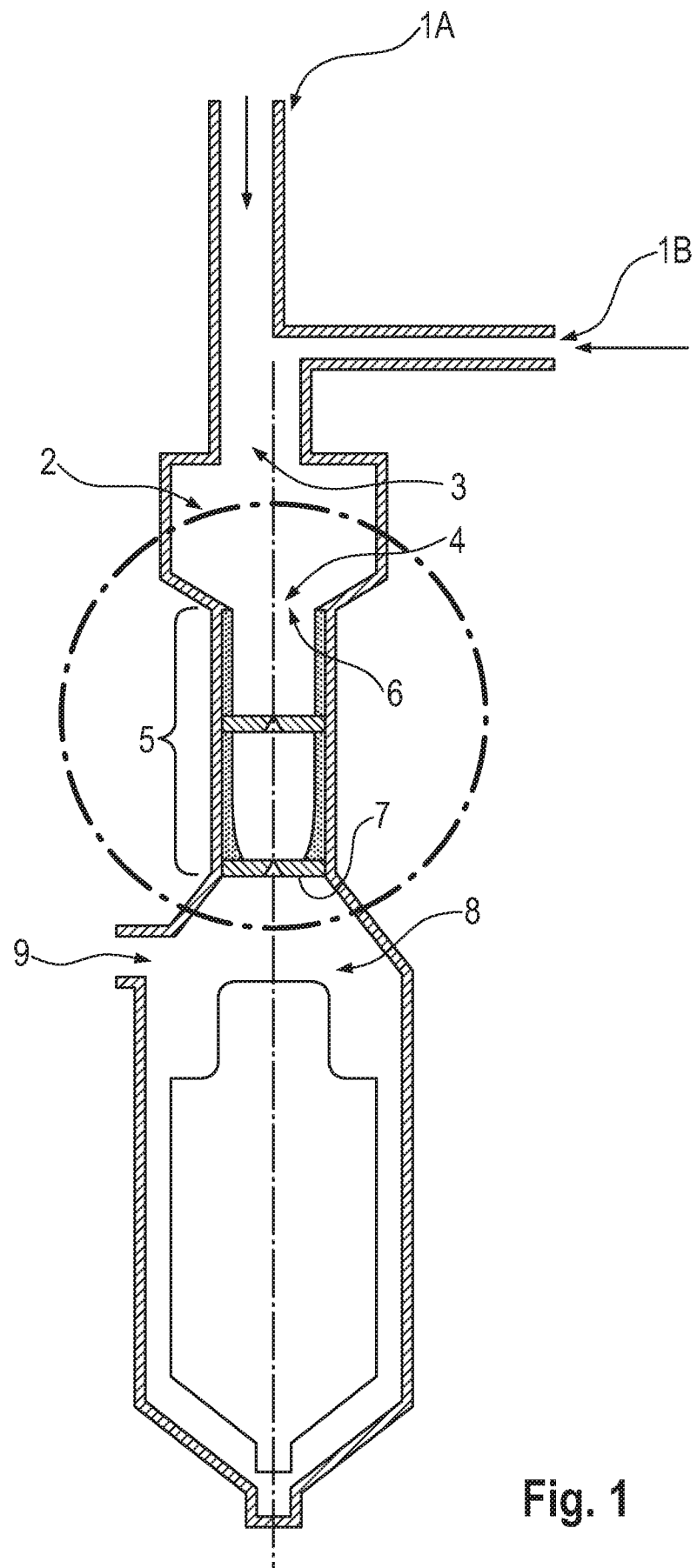


Fig. 1

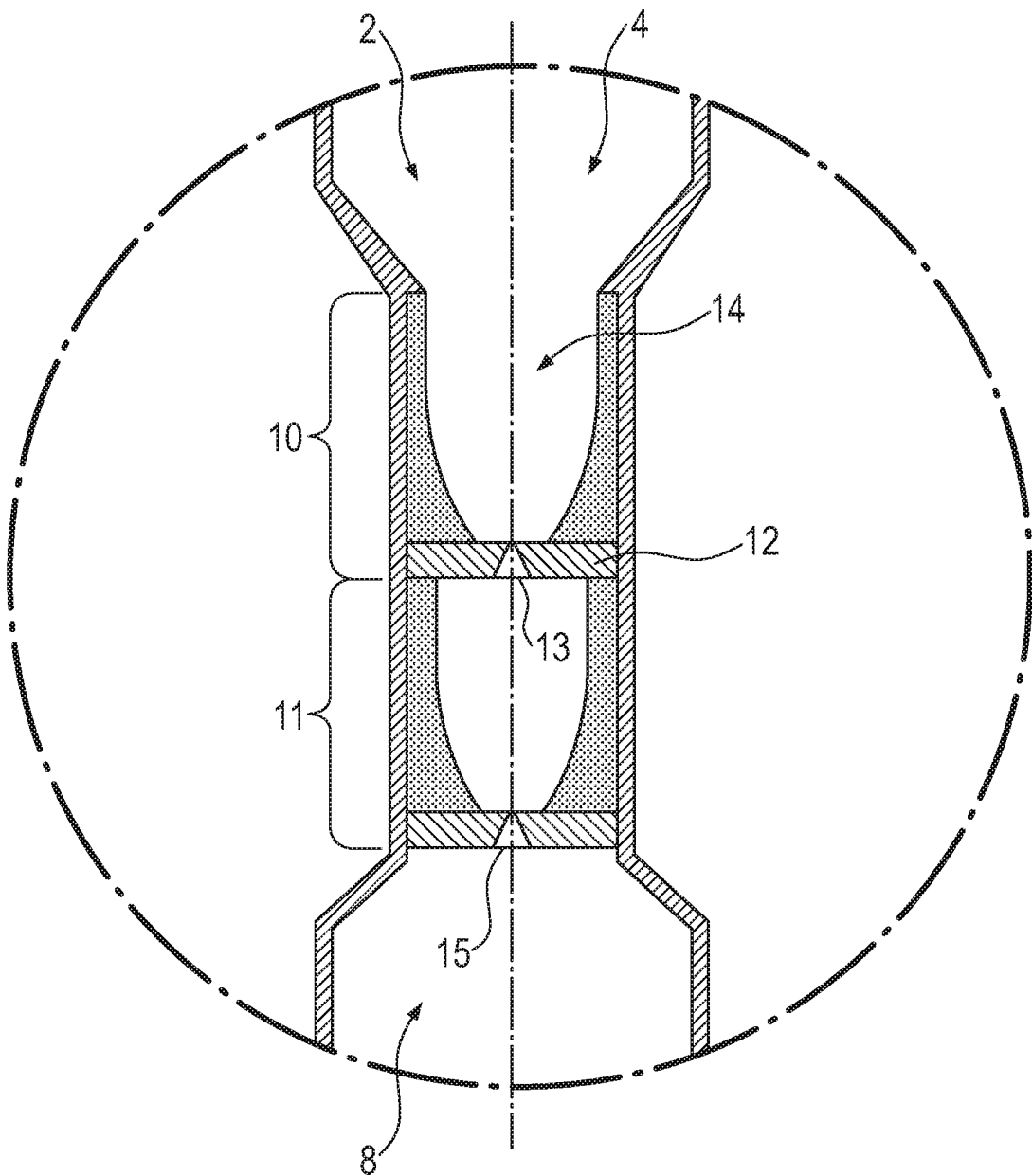


Fig. 2

Apparatus B Example
Circulation Loop System

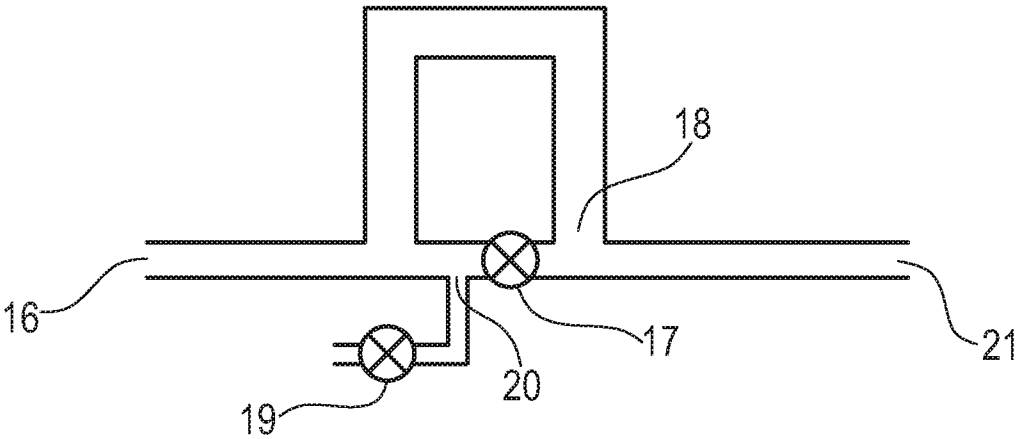


Fig. 3

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2017/065052

A. CLASSIFICATION OF SUBJECT MATTER INV. C11D1/62 C11D3/00 C11D3/22 C11D3/382 C11D17/00 ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols) C11D		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EPO-Internal, WPI Data		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 2 824 169 A1 (PROCTER & GAMBLE [US]) 14 January 2015 (2015-01-14) paragraphs [0003] - [0010]; claims 1-9; examples	1-14
A	US 2001/021692 A1 (MOHAMMADI MANSUR SULTAN [GB] ET AL) 13 September 2001 (2001-09-13) paragraphs [0001] - [0003], [0121]; claims	1-14
A	WO 2013/174603 A1 (UNILEVER PLC [GB]; UNILEVER NV [NL]; CONOPCO INC DBA UNILEVER [US]) 28 November 2013 (2013-11-28) page 2, lines 19-26 page 5, line 1 - line 11 page 18, line 15 - page 19, line 22; claims; table 1	1-14
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☒ Further documents are listed in the continuation of Box C. ☒ See patent family annex.		
* Special categories of cited documents : "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family		
Date of the actual completion of the international search 8 March 2018		Date of mailing of the international search report 22/03/2018
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016		Authorized officer Grittern, Albert

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International application No

PCT/US2017/065052

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
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