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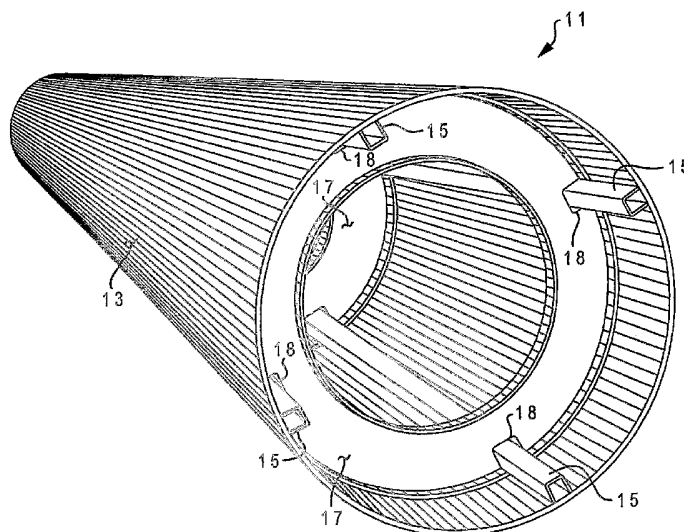
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(54) Title: CONTACT STIFFENERS FOR STRUCTURAL SKINS



(57) Abstract: An internal stiffening member of varying configurations in which the stiffening elements support the skin using a compression-only load path is disclosed. In the preferred embodiment, the stiffening element has a peripheral edge that is adapted to be press fit into contact with the skin. The stiffening member may be held in place by various retention devices. Another configuration is a slip-in rib having a flange with a peripheral channel in which a filler material is disposed. The rib is inserted into an assembled structural box beam, and the filler material is used to fill any gaps between the slip-in rib and the interior surface of the structural box beam. The filler material is preferably an expandable material, such as an expandable foam-type material. However, in situations where a slip-in rib forms a primary structural rib, the filler material is preferably a structural adhesive or liquid shim material. A solid adhesive or filler would not crush under the clamping forces from fasteners or bolts at localized fitting attachments.

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CONTACT STIFFENERS FOR STRUCTURAL SKINS

Technical Field

The present invention relates to structural skin. In particular, the present invention relates to methods and apparatuses for stiffening structural skin.

5 Description of the Prior Art

Structural skin is often used in manufacturing large parts, such as aircraft wing torque boxes, fuselages or control surface structures. This type of structure utilizes thin skins that would not be stable under bending and torsion loads that produce significant shear or compression in the walls. This type of construction is typical of most aerospace structures including wings, fuselages, control surfaces, tail booms, etc. Structural skins can be made thinner, and are, therefore, more weight efficient, when internal stiffening elements are used. A rib, for example, is a structural stiffening element that is disposed perpendicular to the longitudinal axis of a box beam, i.e., the rib lies in a cross-sectional plane of the beam structure. Ribs serve a variety of purposes in thin-skinned structure, including: (1) to provide support for the skin/skin stringer or spar panels against catastrophic buckling; (2) to maintain shape and contour of the skin; (3) to provide stiffness at major load introduction points; (4) to distribute concentrated loads into surrounding thinner structure; (5) to provide a shear redistribution path in the case of failure of any structural elements; and (6) to distribute pressure into the skin. These ribs are typically located at major load introduction points. In most instances, the entire rib is used to react loads; however, in some instances only certain regions of the rib is used to react loads. In addition, some ribs do not have any load introduction points, but react internal pressure loads.

25 Assembly of these structural box beams can be very complex, often with very tight tolerances required. As the number of parts is reduced, the manufacturing tolerances become even more critical, because there are fewer joints where variances can be accommodated. The installation of fasteners into these box beams

presents additional difficulties, including limited access to small interior spaces and complicated sealing requirements.

One-piece closed cell structures can economically be produced with a variety of methods, including filament winding, automated tape placement, resin transfer molding, and others. However, these assembly-tolerance issues often preclude the use of one-piece closed-cell torque box structures with secondarily attached internal ribs, i.e., slipped-in ribs. Because of the reduction in part count and assembly labor associated with consolidating the torque box skins into a single part, a substantial cost savings could be realized if the assembly tolerance issues could be overcome. Several composite fabrication technologies are available to economically produce such a joint-free torque-box structure, including filament winding, automated tape placement, resin transfer molding, and others. Practical application of one-piece, jointless torque box structures has been limited because of the difficulty of installing the internal stiffening ribs. A rib installation design that allowed for large assembly tolerances and the resulting gaps between the rib and the torque box skins would enable more widespread application of these cost-saving technologies.

Summary of the Invention

There is a need for a skin stabilization system that allows for a contact-only element in one of the two primary directions for skin stability. There is also a need for a stabilization element installation design that allows for large assembly tolerances and the resulting gaps between skin and the skin stabilization element, thereby reducing the fabrication cost of assembled structures.

Therefore, it is an object of the present invention to provide a structural stiffened skin in which the stiffening elements support the skin using a compression-only load path.

This object is achieved by providing a slip-in rib, or other stiffening member, of varying configurations in which the stiffening elements support the skin using a compression-only load path. In the preferred embodiment, the stiffening element has a peripheral edge that is adapted to be press fit into contact with the skin. The

stiffening member may be held in place by various retention devices. Another configuration is a slip-in rib having a flange with a peripheral channel in which a filler material is disposed. The rib is inserted into an assembled structural box beam, and the filler material is used to fill any gaps between the slip-in rib and the interior surface of the structural box beam. The filler material is preferably an expandable material, such as an expandable foam-type material. However, in situations where a slip-in rib forms a primary structural rib, the filler material is preferably a structural adhesive or liquid shim material. A solid adhesive or filler would not crush under the clamping forces from fasteners or bolts at localized fitting attachments.

The present invention provides significant advantages, including: (1) costs associated with manufacturing closed-box structures are reduced due to relaxed tolerances and the ability to reduce part count; (2) failure of the rib/box bond is not a significant structural concern, because shear transfer through the rib/box bond is a secondary load path; (3) tolerance build-up is accommodated, because the slip-in ribs can be bonded in place as one-piece ribs; and (4) manufacturing labor is reduced, because fastener installation is reduced or eliminated.

Additional objectives, features, and advantages will be apparent in the written description that follows.

Brief Description of the Drawings

The novel features believed characteristic of the invention are set forth in the appended claims. However, the invention itself, as well as, a preferred mode of use, and further objectives and advantages thereof, will best be understood by reference to the following detailed description when read in conjunction with the accompanying drawings, wherein:

Figure 1 is a perspective view of a conical tail boom of an aircraft having stiffening members according to the present invention;

Figure 2 is a longitudinal cross-sectional view of the tail boom of Figure 1 showing several types of stiffening members according to the present invention installed therein;

5 Figure 3 is an exploded perspective view of a box beam structure having a slip-in rib according to the present invention;

Figure 4 is an exploded top view of the box beam structure having a slip-in rib of Figure 3 showing the installation location of the slip-in rib;

Figure 5 is a cross-sectional view of the box beam structure having a slip-in rib of Figure 4 taken at V-V;

10 Figure 6 is a cross-sectional view of the box beam structure having a slip-in rib of Figure 5 taken at VI-VI;

Figures 7A and 7B are alternate embodiments of the box beam structure having a slip-in rib according to the present invention;

15 Figure 8 is another alternate embodiment of the box beam structure having a slip-in rib according to the present invention;

Figure 9 is another alternate embodiment of the box beam structure having a slip-in rib according to the present invention; and

Figure 10 is a perspective view of the slip-in ribs of Figures 8 and 9.

Description of the Preferred Embodiment

20 A curved structural skin can be stabilized with circumferential stiffening elements, such as frames or ribs, or longitudinal stiffening elements, such as longerons, stringers, or caps. The present invention represents the basic discovery that the internal support mechanism for reacting buckling and retaining shape in structural skin can perform functionally through compressive load transfer only. In
25 other words, the structural attachment of internal stiffening elements to the skin and

other frame elements is redundant and unnecessary. As such, either type of stiffening element can be allowed to float relative with the skin using compression-only "contact" support, provided the stiffening element is trapped or supported by the attached or integral stiffening elements in the other primary direction.

5 The present invention is useful over a wide range of industries, and provides valuable benefits and advantages in any application in which it is desirable to internally support a structural skin. Although the present invention is described herein with reference to certain aircraft applications, it will be appreciated that the methods and apparatuses of the present can be used in many different applications.

10 Non-linear finite element analysis of box beam structures has shown that ribs with only enough structural connection to hold them in place are quite effective in supporting skins against initial buckling, and in allowing load redistribution to occur in post-buckled skins. The reason for this is that in order for the beam cross-section to deform when a panel buckles, for example, the members supporting the edges of
15 that panel must move toward one another. This collapsing deformation is resisted by internal ribs, which prevent the edge members from moving toward one another. The ribs react collapsing deformations in compression, so no shear attachment to the skins or spars is required. The rib perimeter bond can then be considered very
20 damage tolerant, because local discontinuities and damage do not impact the performance of the rib.

 The more general case of a large aircraft fuselage skin panel stiffened using snapped-in contact sticks between frames has also been demonstrated using nonlinear finite element analysis. The slip-in sticks function adequately as stringers to prevent global buckling and fuselage collapse under shear and compression
25 loading. In this application, the frames, which are analogous to the ribs in a torque box structure, are fixed while the stringers are not directly attached to the skins. Thus, like the slip-in rib example, this demonstrates the basic premise that stiffening elements using contact or compression-only load paths are structurally adequate for thin-skinned structures when used in one of the two orthogonal stiffening
30 orientations.

In the aircraft applications described herein, the present invention is a means of supporting the skin/skin stringer or spar panels against catastrophic buckling, and for maintaining the shape and contour of a structural box beam, such as aircraft wing torque boxes or control surface structures. In its broadest sense, the subject invention covers two main concepts: (1) that structural stiffening elements can be installed into assembled thin-skinned structures without fasteners or shims; and (2) that the structural attachment of these stiffening elements to the skins of the structural box beam and spars is redundant and not necessary.

Referring to Figures 1 and 2 in the drawings, the preferred embodiment of a contact stiffener for structural skin according to the present invention is illustrated. This preferred embodiment will be described with reference to a conical tail boom 11 for an aircraft. Tail boom 11 includes a skin 13 that is supported longitudinally by a plurality of elongated spaced apart longerons 15 and circumferentially by a plurality of slip-in ribs 17. Skin 13 is made with using a number of methods, including filament winding, braiding, fiber placement, or hand lay-up with either prepreg, thermoset or thermoplastic, or resin infusion methods, such as resin transfer molding, or variations, such as pultrusion, extrusion, or roll forming from metallic or composite sheets or panels of fiber composite laminates. Longerons 15 are co-cured or integral with skin 13. Slip-in ribs 17 include castellations 18 to fit around longerons 15. It will be appreciated that in some applications it may be desirable that a clearance exist between the top and sides of castellations 18 and longerons 15, as the primary load transfer is in compression between the interior surface of skin 13 and the peripheral edges of slip-in rib 17 that are in contact therewith.

Slip-in ribs 17 are simply inserted through the large end opening of conical tail boom 11 and pressed into place. The peripheral edges of slip-in ribs 17 are press fit into contact with the interior surface of skin 13. Thus, there is no need for any filler between the peripheral edges of slip-in ribs 17 and the interior surface of skin 13 to account for tolerances. In most applications, slip-in ribs 17 are held in place by retention means, such as snap-in clips, springs, or detent devices.

Slip-in ribs 17 may have a wide variety of shapes and configurations. Four possible configurations are shown in Figure 2. Slip-in rib 19 is a solid plug, slip-in rib 21 has a C-channel configuration with a solid web portion 27. Slip-in rib 23 has an open C-channel configuration with a central aperture or truss structure 29, and slip-in rib 25 has an open I-beam configuration having a central aperture or truss structure 31. It will be appreciated that these and other configurations may be used depending various factors, such as the location of the rib, the need to pass other components through the rib, and the load requirements. In an alternate version of this embodiment, tail boom 11 is formed by a flat skin with longitudinal stiffeners wrapped into a conical shape to form a tailboom structure.

Referring now to Figures 3 and 4 in the drawings, a structural box beam 111 according to the present invention is illustrated. Box beam 111 is a one-piece, thin-walled hollow structure having walls 113, 115, 117, and 119. Walls 113 and 115 form upper and lower surfaces of box beam 111, and walls 117 and 119 form side walls of box beam 111. As is shown, walls 113, 115, 117, and 119 may include additional material at corners 114, 116, 118, and 120 to provide longitudinal stiffness to box beam 111, if desired.

Box beam 111 is internally supported by at least one slip-in rib 121. Slip-in rib 121 has an internal web portion 123 and a peripheral flange portion 125. Although web portion 123 has been shown as a solid plate member, it should be understood that web portion 123 may include apertures and/or a truss arrangement (not shown) that would allow cables, wiring, and other component parts to pass longitudinally through box beam 111. Flange portion 125 includes a recessed channel 127 that extends along the periphery of slip-in rib 121. Web portion 123 and flange portion 125 cooperate to allow slip-in rib 121 to function as an I-beam. This configuration allows slip-in rib 121 to be very strong in compression, which the primary functional load transfer path of the present invention.

Walls 113, 115, 117, and 119 are typically integrally formed by filament winding, braiding, fiber placement or hand lay-up with either prepreg or resin infusion methods such as resin transfer molding, or variations such as, pultrusion, or

extrusion, or roll forming from metallic sheets or panels of fiber composite laminates, and slip-in ribs 121 are preferably fabricated from either a metallic or non-metallic fiber filled machining-tolerant plate material. Compression or injection molding or reaction injection molding may also be used to produce net molded ribs. However, it will be appreciated that walls 113, 115, 117, and 119 and slip-in ribs 121 may be formed from other suitable materials, depending upon load, assembly, and application requirements.

In conventional box beam structures, walls 113, 115, 117, and 119 cannot be integrated or pre-assembled without attaching the internal ribs and other support structures. One major benefit of the present invention is that walls 113, 115, 117, and 119 can be integrally produced or assembled prior to installation of the internal support network. This is because slip-in ribs 121 are configured to facilitate installation into an integral or one piece box beam 111.

The location of slip-in rib 121 after installation into box beam 111 is shown in dashed lines in Figure 4. As is shown, a small clearance, or gap 131, exists between the exterior edges of flange 125 and the interior surfaces of walls 113, 115, 117, and 119. This gap allows slip-in ribs 121 to be quickly and easily inserted into the interior of box beam 111. As will be explained in more detail below, gap 131 allows slip-in ribs 121 to accommodate certain manufacturing tolerances, as well. Although only one slip-in rib 121 is shown, it will be appreciated that as many slip-in ribs 121 as are necessary to provide the desired support for box beam 111 may be installed into box beam 111. Slip-in ribs 121 may be installed from either end of box beam 111.

Referring now to Figure 5 in the drawings, box beam 111 with slip-in rib 121 installed is shown in a cross-sectional view taken at V-V of Figure 4. As is shown, it is preferred that the peripheral shape and contour of slip-in rib 121 closely match the internal shape and contour of box beam 111. This ensures that gap 131 between the exterior edges of flange 125 and the interior surfaces of walls 113, 115, 117, and 119 is generally uniform, even though manufacturing tolerances may dictate that there be a finite gap of varying size therebetween.

Referring now to Figure 6 in the drawings, box beam 111 with slip-in rib 121 installed is shown in a cross-sectional view taken at VI-VI of Figure 5. As is shown, a filler material 141 is disposed in channel 127. Filler material 141 may partially fill channel 127, fully fill channel 127, or overfill channel 127. In the preferred embodiment, the filler material 141 is an expandable foam-type adhesive that is installed in channel 127 prior to the insertion of slip-in rib 121 into the interior of box beam 111, and then activated so as to make the adhesive expand and fill channel 127 and gap 131. The process for activating expandable adhesive 141 is typically an increased temperature and or increased pressure curing process in which the temperatures and duration of curing depend upon the particular expandable adhesive used and the load and response characteristics desired. This process allows a relatively large clearance to be maintained for ease of insertion and assembly of slip-in ribs 121. Although the entire structure can be heated in a large oven to activate the expandable adhesive, local means of heat can also be used including by placing resistive heating elements or strips in proximity of the adhesive or inside or adjacent to the adhesive and passing a current through the resistive material through contacts. Resistive heating elements can be embedded into the skin lay-up adjacent to the rib and a network of contacts or wires can be routed to a point of external access. Induction heating can be employed by using magnetic material in proximity or in the adhesive and introducing a magnetic field. Induction heating can also be used with a magnetic layer embedded into the skin lay-up in proximity of the adhesive.

In Figure 6, the upper portion of channel 127 shows expandable filler material 141 prior to activation, and the lower portion of channel 127 shows expandable filler material after activation and expansion. As is shown, after expandable filler material 141 expands, channel 127 and gap 131 are filled with expandable filler material 141.

Referring now to Figures 7A and 7B in the drawings, two alternate embodiments of the present invention are illustrated. In these embodiments, the interface between flange 125 and the internal surface of walls 113, 115, 117, and 119 is modified to improve strength for loads perpendicular to the plane of slip-in rib 121. In these embodiments, filler material 141 is an expandable filler material that

may not bond with slip-in rib 121 or walls 113, 115, 117, and 119, but still provides an acceptable mechanical lock to react lateral pressure loads on slip-in rib 121.

In the embodiment of Figure 7A, a recessed groove or slot 118 is added to the interior surface of walls 113, 115, 117, and 119 opposite flange 125. Channel 127 and slot 118 are filled with filler material 141. After curing, filler material 141 forms a mechanical lock which provides longitudinal stability and helps prevent slip-in rib 121 from moving longitudinally relative to walls 113, 115, 117, and 119. In the embodiment of Figure 7B, circumferential grooves 151 are added at the bond interface to trap filler material 141 as filler material 141 expands. After curing filler material 141, grooves 151 provide longitudinal stability and help prevent slip-in rib 121 from moving longitudinally relative to walls 113, 115, 117, and 119 by means of mechanical lock.

In the embodiment of Figures 7A and 7B, the attachment between slip-in rib 121 and the interior of walls 113, 115, 117, and 119 is not critically loaded. Slip-in rib 121 can provide buckling support and shape retention through compressive load transfer only. Thus, the structural bond formed by filler material 141 is only secondary.

The foregoing discussion and the embodiments of Figures 1-7B are particularly well suited for secondary structural ribs, i.e., ribs that only react compressive loads. However, primary structural ribs require a structural adhesive bond or mechanical fastening between the rib and the box beam skins. Therefore, it is necessary to provide a means for structurally securing the rib within the box beam. This can be accomplished using either a structural adhesive or mechanical retainers.

Referring now to Figures 8-10 in the drawings, two embodiments of slip-in ribs according to the present invention that are suitable for use as both secondary and primary structural ribs are illustrated. For primary structural ribs, the rib must be bonded using a structural adhesive and/or mechanically fastened to the skin of the structural box beam in the local area of load introduction. Other regions of the primary rib can still rely on compression only contact. Although mechanical

fasteners may be used, in the preferred embodiment of the present invention, structural adhesives are used to form the bond between the slip-in rib and the skin of the box beam and fasteners are installed after this adhesive material cures as necessary.

5 As is shown, a structural box beam 211 includes a skin 213 and a slip-in rib 221. Slip-in rib 221 includes an internal web portion 223 and a peripheral flange portion 225. As with slip-in rib 121, although web portion 223 has been shown as a solid plate member, it should be understood that web portion 223 may include void spaces and/or a truss arrangement (not shown) that would allow cables, wiring, and
10 other component parts to pass longitudinally through box beam 211.

 Flange portion 225 includes a recessed channel 227 that extends along the periphery of slip-in rib 221 to receive a structural adhesive material 241. As is shown, a small clearance, or gap 231, exists between the exterior edges of flange 225 and the interior surfaces of skin 213. In these embodiments, small peripheral
15 grooves 235 may be included in both sides of flange 225 for receiving optional seal members, such as an O-rings 237. O-rings 237 help to initially seat slip-in rib 221 and help to contain adhesive 241 if required.

 In these embodiments, it is necessary to form a structural bond between slip-in rib 221 and the interior surface of skin 213. Although mechanical fasteners may
20 be used, it is preferred that structural adhesive be used to form the structural bond. One method of forming this bond is to use a self-contained displacement mechanism to force structural adhesive 241 outward into contact with the interior surface of skin 213. This method is illustrated in Figure 8. Another method of forming this bond is to inject structural adhesive 241 through apertures 243 in recessed channel 227.
25 This method is illustrated in Figure 9. It will be appreciated that there may be many other ways to form this bond that fall within the scope of the present invention. Figure 10 is a perspective view of slip-in rib 221.

 In the method of Figure 8, channel 227 is lined with a self-contained displacement mechanism, such as an evacuated or collapsed inflatable tubular

bladder 245. Structural adhesive 241 is then located on top of the displacement mechanism, inflatable bladder 245 in this example. Channel 227 is sized and shaped to accommodate the reduced volume of bladder 245 and additional volume to accommodate enough structural adhesive 241 to fill the interface area between slip-in rib 221 and skin 213. Bladder 245 is preferably made of a material, such as nylon, rubber, or other elastomeric material, such that when inflated or otherwise activated, structural adhesive 241 is displaced outward into contact with the interior surface of skin 213, thereby forming the structural bond between slip-in rib 221 and skin 213. Bladder 245 may then be sealed so as to remain inflated, become a sacrificial "fly-away" tool, or be extracted from channel 227 after structural adhesive 241 cures. In this embodiment, apertures 243 may be used to allow access to one or more valve stems 247 for inflating bladder 245. The use of a self-contained displacement mechanism, such as bladder 245, allows a measured or metered volume of a fluid adhesive to be dispensed. This eliminates the requirement to control adhesive volume using conventional methods, such as calendared or film adhesive.

In the method of Figure 9, slip-in rib 221 is inserted dry into place within skin 213. Then, structural adhesive 241 is injected through apertures 243, so as to flow around and fill channel 227. Channel 227 is sized and shaped to allow adhesive 241 to flow around the perimeter of slip-in rib 221 without squeezing out of flange 227. As is shown in Figure 10, apertures 243, which may be located at varying locations around flange 225, and which may be simple inspection ports, may be used to ensure that adhesive 241 has adequately filled channel 227. Structural adhesive 241 is forced into channel 227 with sufficient pressure to force structural adhesive into contact with the interior surface of skin 213, thereby forming the structural bond between slip-in rib 221 and skin 213.

It should be understood that although the embodiments of Figure 8-10 have been shown and described with continuous adhesion, it is not necessary that structural adhesive 241 form a continuous bond with skin 213. According to the present invention, only local adhesion is required. For example, portions of the interface between slip-in rib 221 and skin 213 may be treated so as to release

structural adhesive 241 at selected locations and maintain the bond at other locations.

As forth above, mechanical retainers may be used instead of structural adhesive to secure the slip-in ribs in place within the box beam. Some mechanical retainers include: shims with snap-in receivers, spring biased buttons, and leaf springs, to name a few.

The slip-in ribs of the present invention reduce the complexity of the assembly of box beam structures, particularly in applications where the number of parts has been reduced. This is because the slip-in ribs of the present invention are not directly dependent upon the number of joints where manufacturing tolerances are accommodated. Also, the installation of fasteners into box beam structure presents difficulties such as access to small interior spaces and sealing requirements. The process by which the slip-in ribs of the present invention are installed accommodates tolerance buildup, resulting in reduced part count. This reduces manufacturing labor because fastener installation is eliminated.

By using the slip-in ribs according to the present invention, the costs associated with manufacturing a closed-box structure can be reduced due to relaxed tolerances and the ability to reduce part count without incurring additional assembly cost. Because the rib/box bond is secondary, failure of the rib/box bond is not a significant structural concern as long as the rib position in the box is retained.

Using slip-in ribs that can be bonded in place with a process that accommodates tolerance build-up results in reduced part count, as installing one-piece ribs in one-piece structural box beams is possible; and manufacturing labor is reduced, as fastener installation is eliminated.

Although the present invention has been described with respect to a slip-in rib having basically the same shape and contour as the geometrical cross-section of the structural box beam, it should be understood that the concept of the present invention, i.e., the ability to internally support the box beam using compression-only load paths, may be achieved by other means, as well, including the use of rigid,

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elongated rods placed between ribs or spars, the rods not being fixed to the internal surface of the box beam. These rods resist buckling of the skins by maintaining the desired spacing between internal stiffening members.

5 It is apparent that an invention with significant advantages has been described and illustrated. Although the present invention is shown in a limited number of forms, it is not limited to just these forms, but is amenable to various changes and modifications without departing from the spirit thereof.

Claims

1. An internal stiffening member for use in supporting a thin-walled structural skin comprising:

a web portion; and

5 a peripheral flange;

wherein the internal stiffening member supports the structural skin in a compression-only load path.

2. The internal stiffening member according to claim 1, wherein the web portion and the flange have a C-channel shaped cross-sectional geometry.

3. The internal stiffening member according to claim 1, wherein the web portion and the flange have an I-beam shaped cross-sectional geometry.

4. The internal stiffening member according to claim 1, further comprising:
15 at least one aperture passing longitudinally through the web portion.

5. The internal stiffening member according to claim 1, wherein the flange is configured to contour to the shape of the interior surface of the thin-walled skin.

6. The internal stiffening member according to claim 1, further comprising:
20 a recessed channel formed in the flange.

7. The internal stiffening member according to claim 6, further comprising:
25 a filler material disposed in the flange, the filler material being adapted to fill gaps between the flange and the interior surface of the thin-walled skin.

8. The internal stiffening member according to claim 7, further comprising:
peripheral grooves disposed in the flange; and

a seal member disposed in each peripheral groove for forming a seal between the flange and the interior surface of the thin-walled skin so as to contain the filler material.

- 5 9. The internal stiffening member according to claim 7, further comprising:
a structural adhesive adapted to be forced into the recessed channel for forming a mechanical bond.
- 10 10. The internal stiffening member according to claim 7, wherein the filler material is an expandable adhesive.
- 15 11. The internal stiffening member according to claim 10, further comprising:
at least one aperture in the recessed channel for injecting the expandable adhesive.
- 20 12. The internal stiffening member according to claim 1, wherein the internal stiffening member is configured to be inserted into the interior of the thin-walled skin after the thin-walled skin is fabricated and assembled.
- 25 13. The internal stiffening member according to claim 1, wherein the web portion is solid.
14. The internal stiffening member according to claim 1, wherein the web portion includes void spaces.
- 30 15. The internal stiffening member according to claim 1, wherein the internal stiffening member forms a primary structural rib, such that a mechanical attachment is formed between the internal stiffening member and the thin-walled skin.
16. The internal stiffening member according to claim 15, wherein the mechanical attachment is enhanced using a mechanical fastener.

17. The internal stiffening member according to claim 15, wherein the mechanical attachment includes a shim.

5 18. The internal stiffening member according to claim 6, further comprising:
means for reacting loads perpendicular to the plane of the internal stiffening member.

10 19. The internal stiffening member according to claim 18, wherein the means for reacting loads perpendicular to the plane of the internal stiffening member comprises:

a recessed groove in the interior surface of the thin-walled skin opposite the flange for trapping the filler material.

15 20. The internal stiffening member according to claim 18, wherein the means for reacting loads perpendicular to the plane of internal stiffening member comprises:

peripheral grooves located at the bond interface between the flange and the interior surface of the skins for trapping the filler material.

20 21. The internal stiffening member according to claim 20, wherein the peripheral grooves are disposed in the recessed channel of the flange.

25 22. The internal stiffening member according to claim 20, wherein the peripheral grooves are disposed in the interior surface of the thin-walled skin opposite the flange.

23. The internal stiffening member according to claim 20, wherein the peripheral grooves are disposed in both the recessed channel of the flange and the interior surface of the thin-walled skin opposite the flange.

30 24. The internal stiffening member according to claim 9?, further comprising:

a self-contained displacement mechanism disposed within the recessed channel for selectively displacing the filler material after the internal stiffening member has been inserted in to the interior of the structural box beam.

5 25. The internal stiffening member according to claim 24, wherein the self-contained displacement mechanism is an inflatable bladder.

26. The internal stiffening member according to claim 25, wherein the inflatable bladder is made from an elastomeric material.

10

27. The internal stiffening member according to claim 25, further comprising:
at least one aperture in the recessed channel for receiving a valve stem of the inflatable bladder.

15

28. The internal stiffening member according to claim 1, wherein the filler material only partially fills the recessed channel.

20

29. The internal stiffening member according to claim 1, further comprising:
retention means for maintaining the position of the slip-in rib, the retention means producing only secondary load paths.

30. The internal stiffening member according to claim 29, wherein the retention means comprises a mechanical fastener including a snap-in receiver.

25

31. The internal stiffening member according to claim 29, wherein the retention means comprises a spring biased button.

32. The internal stiffening member according to claim 29, wherein the retention means comprises a leaf spring.

30

33. A structural box beam comprising:
an enclosure formed by at least one thin-walled skin;

a slip-in rib adapted to be slipped into the enclosure after the enclosure is formed, the slip-in rib comprising:

a web portion;

a flange disposed around the periphery of the web portion;

5 a recessed channel formed in the flange; and

a filler material disposed in the recessed area, the filler material being adapted to fill gaps between the flange and the interior surfaces of the enclosure;

wherein the structural box beam is supported by the slip-in rib in compression only.

10 34. The structural box beam according to claim 33, wherein the filler material is an expandable adhesive.

15 35. The structural box beam according to claim 33, further comprising:
an inflatable bladder disposed within the recessed channel for selectively displacing the filler material into contact with the interior surfaces of the enclosure.

20 36. The structural box beam according to claim 33, further comprising:
apertures disposed in the recessed channel for injecting the filler material into the recessed channel.

25 37. A method of supporting a structural box beam comprising the steps of:
providing an internal support member;
inserting the internal support member into the interior of the structural box beam; and
supporting the structural box beam with the internal support member in compression only.

30 38. The method according to claim 37, wherein the step of supporting the structural box beam with the internal support member in compression only comprises the steps of:

providing a slip-in rib having a central web portion, a peripheral flange, and a recessed channel in the peripheral flange;

disposing an expandable filler material in the recessed channel;

activating the expandable filler material such that the filler material expands,
5 thereby filling gaps between the peripheral flange and the interior surface of the structural box beam.

39. An internal stiffening member for use in supporting a thin-walled structural skin comprising:

10 an internal support member; and

a peripheral contact surface disposed on the internal support member being adapted for contacting the thin-walled skin;

wherein the internal stiffening member supports the structural skin in a compression-only load path.

40. The internal stiffening member according to claim 10, further comprising:

a resistive heating element operably associated with the thin-walled skin for activating the expandable adhesive.

41. The internal stiffening member according to claim 40, wherein the resistive heating element is embedded within the thin-walled skin.

42. The internal stiffening member according to claim 10, further comprising:

a magnetic material operably associated with the thin-walled skin for
25 introducing a magnetic field for activating the expandable adhesive.

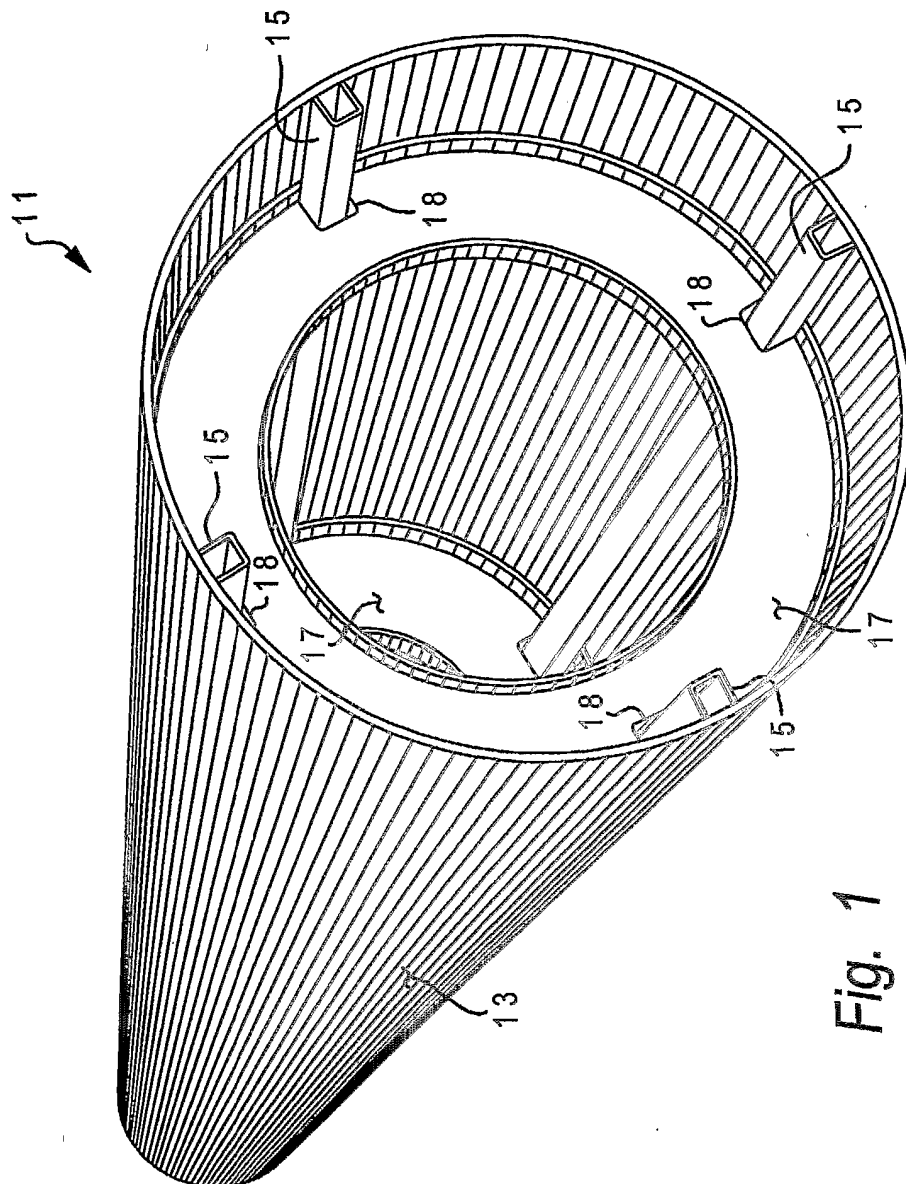


Fig. 1

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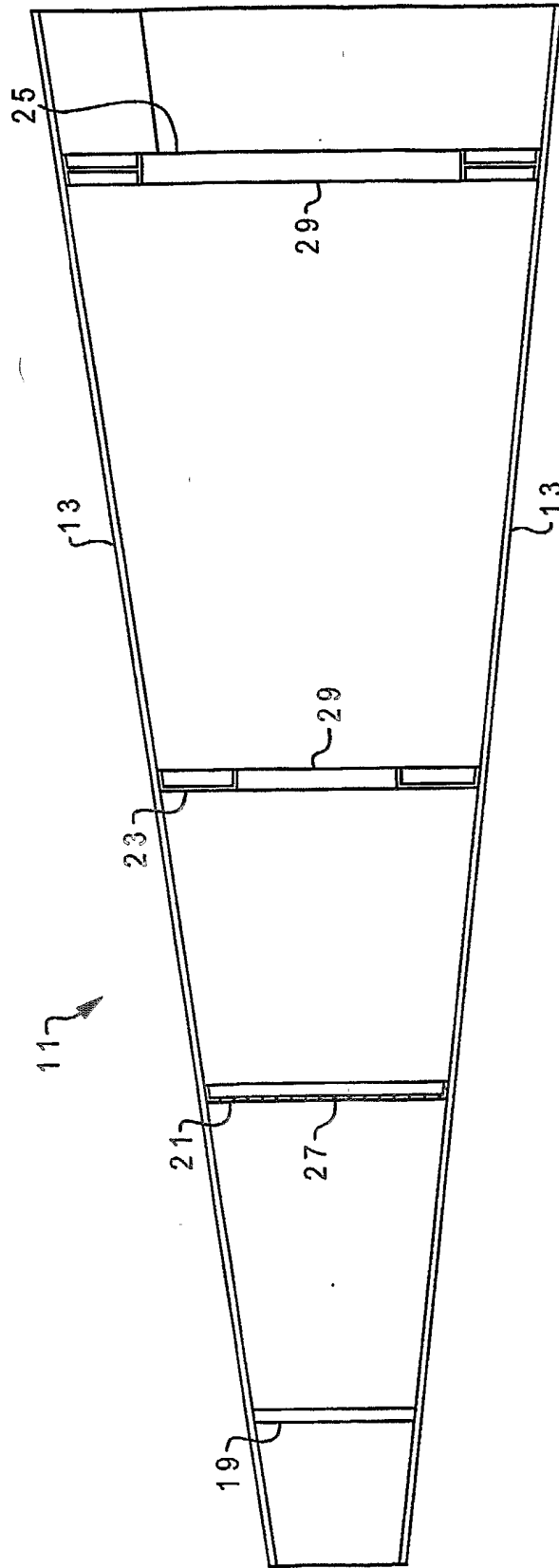


Fig. 2

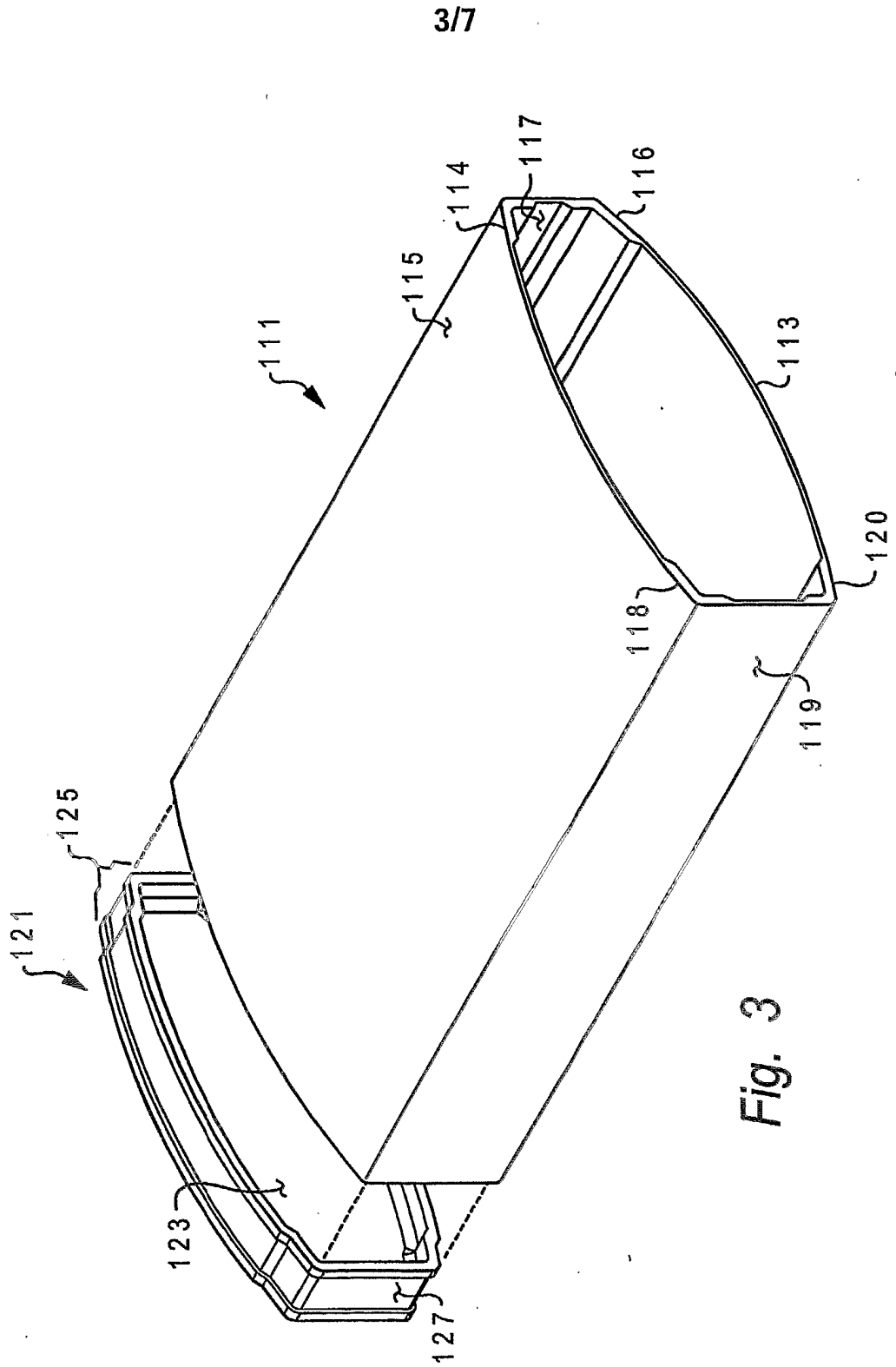


Fig. 3

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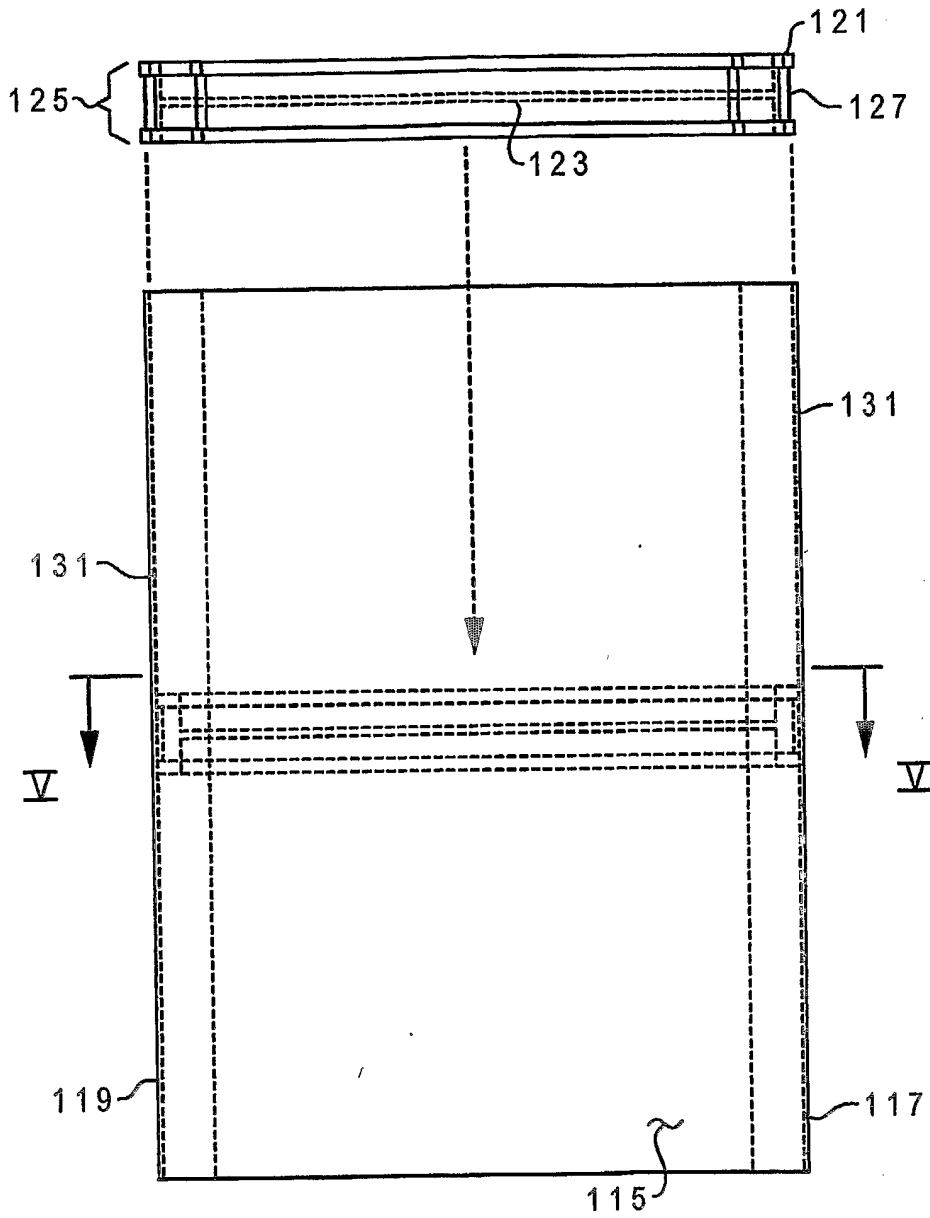


Fig. 4

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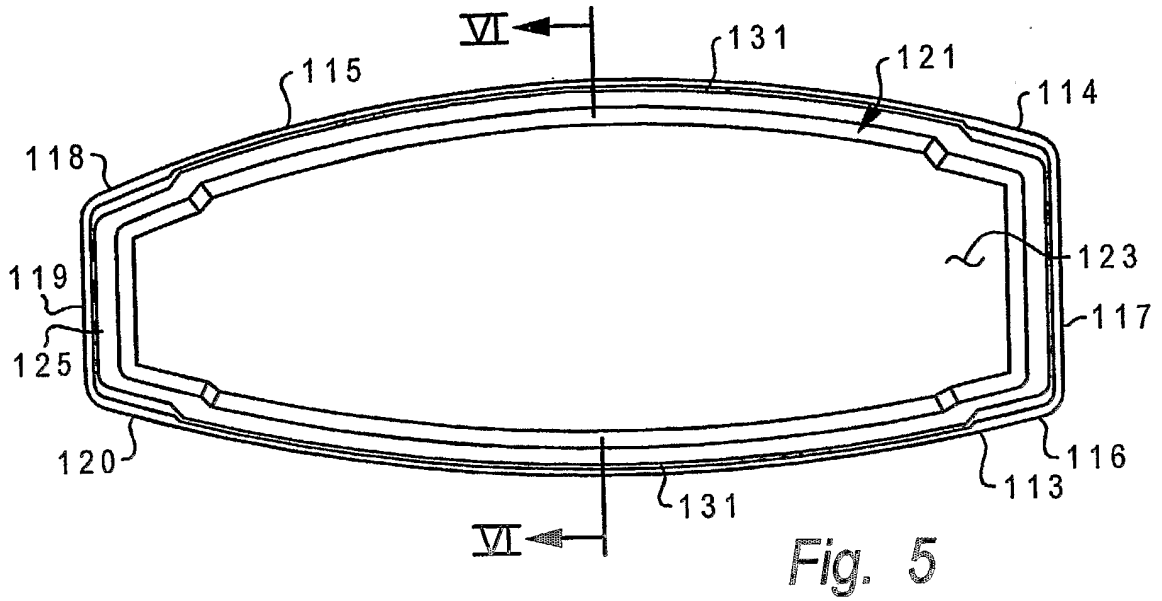


Fig. 5

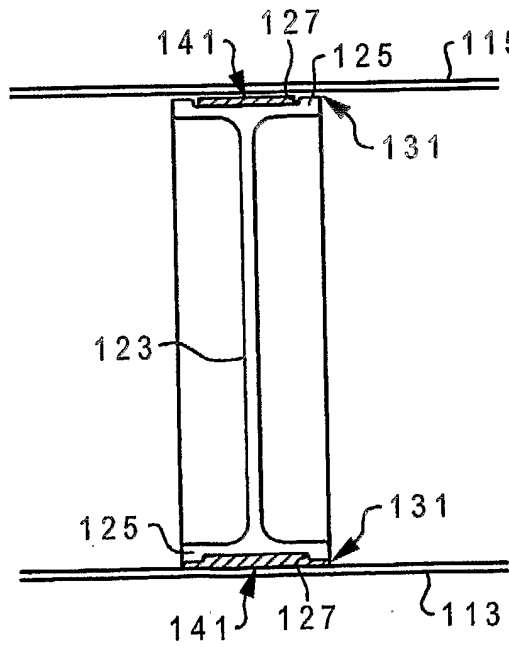


Fig. 6

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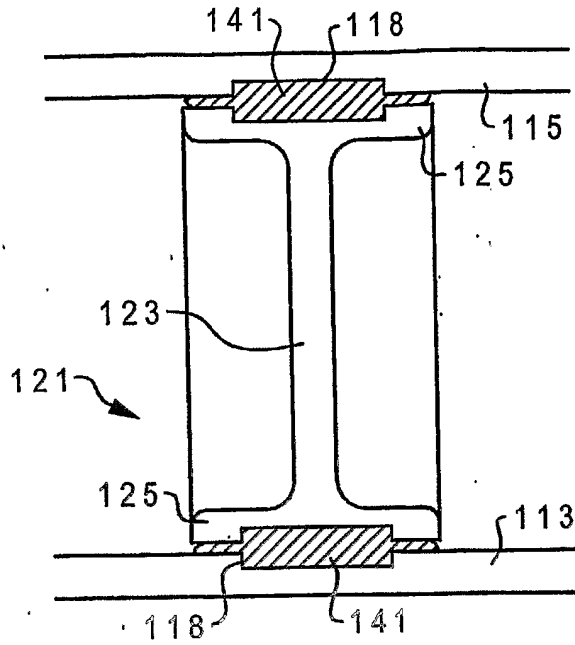


Fig. 7A

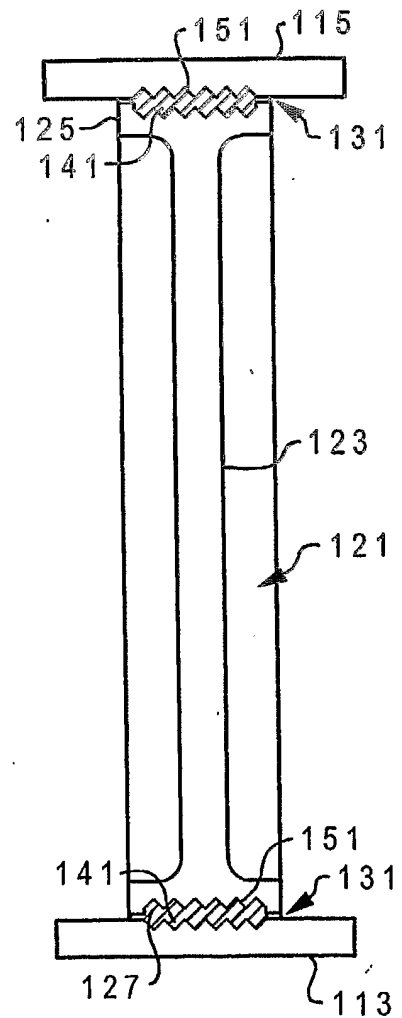


Fig. 7B

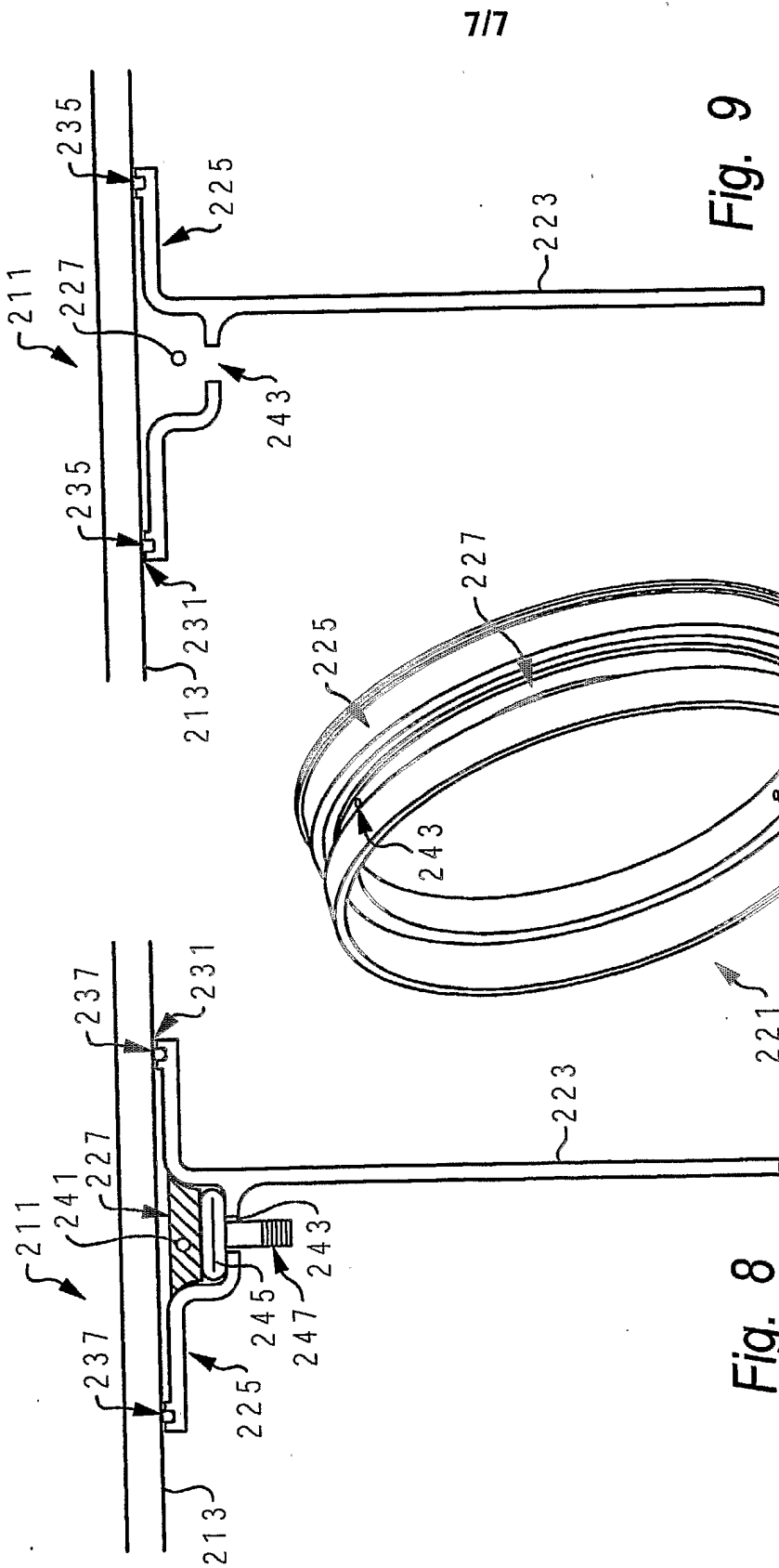


Fig. 9

Fig. 8

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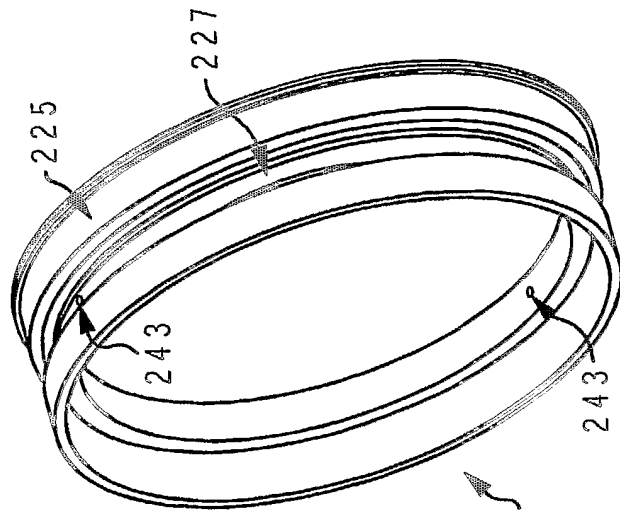


Fig. 10