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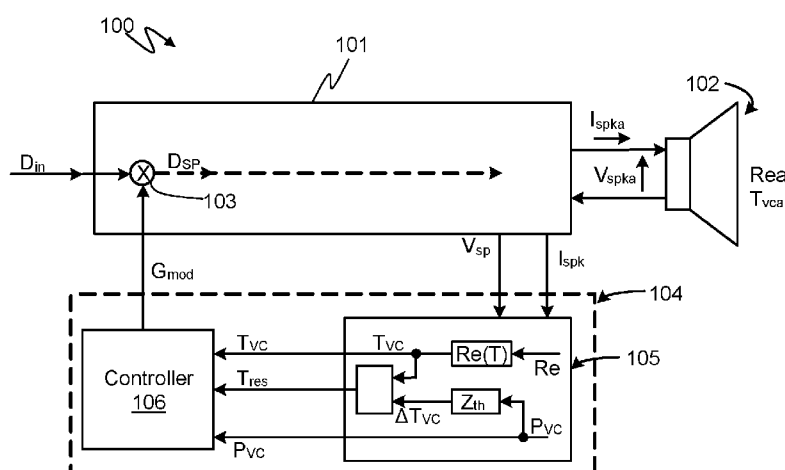


Figure 1

(57) Abstract: This application relates to methods and apparatus for thermal protection of a loudspeaker (102). A controller (106) is configured to generate a control signal (G_{mod}) for modulating the gain of a signal processing chain (101) that drives the loudspeaker. The controller is configured such that the control signal is generated as a function of each of: an indication of voice coil temperature of the loudspeaker (T_{vc}); an indication of power dissipation in the voice coil of the loudspeaker (P_{vc}); and an indication of a reservoir temperature (T_{res}) of a thermal reservoir for heat flow from the voice coil. The reservoir temperature may be an ambient temperature of the environment or a temperature of a component of the loudspeaker or apparatus that acts as a heat sink.



Loudspeaker Protection Circuitry and Methods

This invention relates to methods and apparatus for protecting loudspeakers, and especially to methods and apparatus for detecting the ambient or magnet temperature of a loudspeaker to control the drive signal supplied to the loudspeaker so as to avoid voice coil over-temperature.

A number of different products include audio circuitry, such as an audio amplifier, together with one or more loudspeakers and/or connections for driving one or more loudspeakers of a peripheral apparatus such as a headset. In some instances the loudspeaker(s) chosen will be robust enough and large enough to handle the maximum power level at which the amplifier could drive signals continuously into it, even under the worst case environmental conditions, for instance maximum supply voltage, maximum ambient temperature etc. However having robust enough loudspeakers is not always economical, and for portable devices in particular the desire is typically to make the speaker as small and light as possible. This can potentially lead to the audio drive circuitry overloading the loudspeaker. One particular problem is thermal overload of the loudspeaker.

A typical loudspeaker comprises a diaphragm which is driven by a voice coil supported relative to a magnet. In use, typically, an analogue audio drive signal is applied to the voice coil to drive the loudspeaker. High levels of audio signal may give rise to high current levels in the voice coil, which may cause it to heat up due to ohmic losses associated with the electrical resistance of the coil. Excessive voice coil temperature may give rise to reliability problems, for example the glue attaching component parts of the mechanism may soften or melt, or the permanent magnet may be demagnetised or the ferro-magnetic properties of the core may degrade.

The audio amplifier circuitry may therefore be controlled by thermal protection control circuitry to limit the output power it can deliver to the loudspeaker so that the maximum power dissipated in the voice coil does not cause the voice coil temperature to exceed some specified safe limit.

However the maximum power that may be allowed to be dissipated in the voice coil will be dependent on the ambient temperature. It will be appreciated that heat generated in the voice coil will flow to the surrounding environment via various thermal paths (with associated thermal resistances) to the environment which will be at an ambient
5 temperature. At a hot ambient temperature, less power can be dissipated before the voice coil temperature rises to a maximum limit compared to a cooler ambient. The output power limit may thus be set to a value appropriate for a maximum likely or specified temperature. However this does mean that the output power may be unnecessarily limited when operating with a more usual or even unusually low ambient
10 temperature.

To mitigate this, the voice coil temperature may be sensed and the power applied adjusted to control the measured coil temperature. However the gain of the control loop is preferably designed to be low, to avoid sudden audible changes in power level. Thus
15 the maximum power is still somewhat dependent on other influences such as ambient temperature variations, and may still be less than the maximum actually allowable.

Embodiments of the present invention provide methods and apparatus for speaker protection that at least mitigate at least some of the above mentioned disadvantages.

20

Thus according to the present invention there is provided a system for thermal protection of a loudspeaker comprising:

- a controller configured to generate a control signal for modulating the gain of a signal processing chain driving said loudspeaker,
- 25 wherein said controller is configured such that the control signal is generated as a function of each of:
 - an indication of voice coil temperature of the loudspeaker;
 - an indication of power dissipation in the voice coil of the loudspeaker; and
 - an indication of a reservoir temperature of a thermal reservoir for heat flow from
30 the voice coil.

In some embodiments the controller comprises a power limit module configured to determine an allowed power function of an allowed power dissipation with voice coil temperature based on said indication of a reservoir temperature. The controller may

also comprise a gain calculation module configured to determine a gain setting based on the indication of voice coil temperature, the indication of power dissipation in the voice coil and the allowed power function. The control signal may be based on the gain setting.

5

The power limit module may be configured to determine the allowed power function such that the allowed power dissipation at a maximum allowed temperature of the voice coil depends on said indication of a reservoir temperature. The power limit module may be configured to determine the allowed power function such that the
10 allowed power dissipation at the maximum allowed temperature corresponds to a power dissipation that leads to a substantially steady state temperature of the voice coil at the relevant reservoir temperature.

In some embodiments the power limit module may be configured to determine the
15 allowed power function for a voice coil temperature range between a threshold temperature and said maximum allowed temperature. The allowed power function between the threshold temperature and said maximum allowed temperature may correspond to at least one of: an S-shaped curve, a polynomial curve, a Bezier curve; or a spline curve.

20

The power limit module may be configured to determine the allowed power function such that for any voice coil temperature below a the threshold temperature no limit on allowed power is applied.

25 In some embodiments the power limit module may be configured to determine the allowed power function such that the allowed power dissipation at the threshold temperature is based on the indication of power dissipation in the voice coil of the loudspeaker.

30 In some embodiments the gain calculation module may be configured to determine the gain setting based on an allowed power dissipation determined according to the allowed power function and the indication of power dissipation in the voice coil. The gain calculation module may be configured to determine the gain setting according to a gain control transfer function. The gain control transfer function may vary the gain

setting from a first gain setting at a first value of power dissipation in the voice coil of the loudspeaker to a second gain setting at a second value of power dissipation in the voice coil, wherein the first gain setting corresponds to a maximum gain setting and the second gain setting corresponds to a lower gain setting. The second value of power
5 dissipation in the voice coil may correspond to the allowed power dissipation and the second gain setting corresponds to a gain setting that would lead to a power dissipation substantially equal to the allowed power dissipation if an input signal to the signal processing chain driving said loudspeaker was at a maximum level.

10 In some embodiments the system may comprise an estimation module configured to determine the indication of reservoir temperature based on said indication of power dissipation of the voice coil. The estimation module may comprise a temperature rise module configured to determine an estimated temperature rise based on the indication of power dissipation of the voice coil and a thermal impedance model of a thermal path
15 between the voice coil and the thermal reservoir; and a reservoir temperature estimation module configured to determine the indication of reservoir temperature based on the indication of voice coil temperature and the estimated temperature rise.

The estimation module may comprise at least one input for receiving a first signal
20 indicative of voltage applied to the voice coil of said loudspeaker and a second signal indicative of current flowing in said voice coil and is configured to determine said indication of temperature of the voice coil and said indication of power dissipation in the voice coil based on said first and second signals; wherein at least said estimate of temperature is based on an estimate of resistance of said voice coil which is
25 determined based on said first and second signals. The estimation module may be configured to determine the estimate of voice coil resistance based on: the difference between the value of said estimated voice coil resistance and a reference resistance value at a known temperature; and a temperature coefficient for the loudspeaker voice coil.

30

In some embodiments the estimation module may be configured to determine the indication of power dissipation based on said estimated voice coil resistance and the second signal indicative of current flowing in said voice coil. The estimation module may be configured to determine the estimate of power dissipation by multiplying said

estimated voice coil resistance by the square of the value of the second signal indicative of current flowing in said voice coil.

5 In some embodiments the system may comprise a temperature sensor configured to measure said indication of reservoir temperature.

10 In some embodiments the indication of a reservoir temperature may be an indication of an ambient temperature for the loudspeaker. In some embodiments the indication of a reservoir temperature may be an indication of the temperature of a component of the loudspeaker other than the voice coil. Such a component may be a magnet of the loudspeaker.

15 In embodiments with a gain control module, the gain control module may be configured to apply time domain processing to said gain setting to provide control signal. The time domain processing may comprise applying at least one of an attack time constant and a decay time constant to said gain control value to generate said control signal. The gain control module may be configured such that at least one of the attack time constant and a decay time constant is variable based on the indication of voice coil temperature.

20 In some embodiments the controller is configured to time the application of any gain changes to synchronise with zero crossings in the input signal. Additionally or alternatively the controller may be configured such that the maximum frequency of gain changes applied is maintained below a predetermined limit.

25 The system may comprise a gain element for applying a gain to the input signal. The gain element may be controlled by the controller. The controller may control the gain of the gain element based on said control signal and at least one other gain setting. The at least one other gain setting may be one of: a user controlled volume setting; a gain control setting for excursion limiting.

30

In some embodiments the controller may further comprise an excursion limiting module configured to generate a second gain setting for excursion limiting of the loudspeaker. In some embodiments the controller may be configured to generate the control signal

for modulating the gain of a first gain element in the signal processing chain and also to further modulate the gain of a second gain element in the signal processing chain based on the second gain setting. Alternatively the controller may be configured such that the control signal is further based on said second gain setting, i.e. on both the first
5 and second gain settings.

The system may comprise a signal processing chain for driving said loudspeaker. The system may also comprise the loudspeaker.

10 Embodiments also relate to an electronic apparatus comprising a system as described in any of the variants above. The apparatus may be at least one of: a portable device; a battery power device; a computing device; a communications device; a gaming device; a mobile telephone; a personal media player; a laptop, tablet or notebook
computing device.

15 In another aspect there is provided a system for thermal protection of a loudspeaker comprising a power limit block for determining an allowed power function of power dissipation against temperature for a voice coil of a loudspeaker, wherein the power limit block has an input for receiving an indication of the temperature of a thermal
20 reservoir for heat generated in the voice coil and wherein the allowed power function depends on said temperature of the thermal reservoir.

The power limit block may be configured such that the value of allowed power at a maximum temperature varies depends on said temperature of the thermal reservoir.
25 The temperature of the thermal reservoir may be an ambient temperature for the loudspeaker.

In a further aspect there is provided a thermal protection system for a loudspeaker comprising:

30 at least one input for receiving a first signal indicative of voltage applied to the voice coil of said loudspeaker and a second signal indicative of current flowing in said voice coil;
a temperature and power estimation module configured to determine:

an estimate of temperature of the voice coil based on an estimate of resistance of said voice coil which is determined based on said first and second signals;

an estimate of power dissipation in the voice coil based on said first signal, second signals and/or said estimate of resistance of said voice coil; and

- 5 an estimate of temperature of a thermal reservoir for heat produced in the voice coil based on a comparison of said estimate of temperature of the voice coil the voice coil and an estimate of rise of coil temperature based on a thermal speaker model and said estimate of power dissipation in the voice coil;

- 10 a gain controller configured to generate a gain control signal for modulating the gain of a signal processing chain driving said loudspeaker, wherein said gain control signal is generated as a function of each of said estimate of temperature of said voice coil, said estimate of power dissipation in the voice coil and said estimate of temperature of a thermal reservoir.

- 15 In a yet further aspect there is provided a system for thermal protection of a voice coil of a loudspeaker comprising: a module configured to generate an estimate of temperature of said voice coil, an estimate of power dissipation in the voice coil and an estimate of a temperature of a thermal reservoir for heat produced in the voice coil based on a voltage applied to said voice coil and a current flowing through said voice
20 coil and generate a gain control signal for modulating a gain of a signal processing chain driving said loudspeaker, wherein said gain control signal is based on said estimates of temperature of said voice coil, power dissipation in the voice coil and temperature of the thermal reservoir.

- 25 Aspects also relate to loudspeaker protection circuitry, for providing a gain control signal for controlling the gain applied to an input signal to provide a drive voltage into a loudspeaker voice coil, comprising a controller configured to:

- receive signals indicative of the voice coil current and drive voltage;
 calculate from said indicative signals, an estimate of the present voice coil temperature
30 and an estimate of the power dissipation of the voice coil, wherein at least said estimate of voice coil temperature is based on an estimate of the present voice coil resistance which is determined from said indicative signals;

 calculate the temperature of a thermal reservoir from said estimate of voice coil temperature and said power dissipation and a thermal speaker model; and

generate and output said gain control signal as a function of all three of the estimate of voice coil temperature, the estimate of power dissipation and the estimate of temperature of a thermal reference node.

- 5 In a further aspect there is provided a system for thermal protection of a loudspeaker comprising a power limit block for determining an allowed power function of allowed power dissipation for a voice coil temperature range between a lower threshold temperature and a higher threshold temperature, wherein the power limit block has an input for receiving an indication of the power dissipation in the voice coil and wherein
- 10 the allowed power function is determined such that the allowed power dissipation at the lower temperature threshold corresponds substantially to the indication of the power dissipation in the voice coil.

Embodiments of the invention will now be described, by way of example only, with

15 reference to the accompanying drawings, of which:

Figure 1 illustrates an audio apparatus having a loudspeaker protection module according to an embodiment of the invention;

- 20 Figure 2 illustrates a power and temperature extraction block according to an embodiment;

Figure 3 illustrate an electrical model of a loudspeaker;

- 25 Figure 4a and 4b illustrate example thermal models of a loudspeaker;

Figure 5 illustrates a gain controller according to an embodiment;

- Figure 6 illustrates one example of how allowed power may be controlled with voice
- 30 coil temperature for a given reservoir temperature;

Figure 7 illustrates another example of how allowed power may be controlled with voice coil temperature for a given reservoir temperature and also indicates how steady state power dissipation varies with reservoir temperature;

Figure 8 illustrates a family of allowed power curves that may be applied at different reservoir temperatures;

- 5 Figure 9 illustrates how allowed power curves may be derived based on the present power dissipation when a threshold temperature is reached;

Figures 10a to 10e illustrate examples of how gain may be controlled based on the allowed power and an indication of the present power dissipation;

10

Figure 11a and 11b illustrate flow charts of methods according to embodiments of the invention;

- 15 Figure 12 illustrates speaker driver circuitry comprising another embodiment of a thermal limiter; and

Figure 13 illustrates an apparatus having a loudspeaker protection module for thermal limiting.

20

- Figure 1** illustrates an embodiment of audio driver amplifier circuitry 100 according to an embodiment of the invention. A signal processing chain 101 receives a digital input audio signal D_{in} at an input terminal and processes it, eventually providing a signal to drive a loudspeaker 102. The input terminal may be a circuit contact such as bond pad or the like for connecting to another circuit or could simply be a node of a signal path which represents the input to the signal processing chain. For the avoidance of doubt the phrase "input terminal" as used herein includes an input node and no particular physical characteristics are implied by the word "terminal".

- 25
- 30 The signal processing chain 101 comprises a multiplier or digital gain stage 103 in the signal path and may also comprise elements such as digital filtering or other digital signal processing, digital-to-analogue convertors, and/or at least one Class D, Class AB or Class G or Class H power amplifier stage and associated modulation circuitry. The multiplier or gain stage 103 may apply a gain G_{mod} to the signal. The signal

processing chain may apply further gain G_{xx} in the signal path so that there may be will have an overall gain from the input signal D_{in} to the voltage signal V_{spka} driven into the loudspeaker proportional to G_{mod} .

- 5 It should be noted that the digital processing circuitry may comprise at least some custom-designed logic circuitry and/or may comprise a general purpose processor running appropriate code. The loudspeaker may be grounded externally and driven from a single output terminal, or both loudspeaker terminals may be connected to the signal processing chain for example where both terminals are driven in from a full-
10 bridge output stage or where the ground return current is passed through the driver circuitry as illustrated.

The signal processing chain 101 also comprises circuitry for sensing the current I_{spka} actually flowing through the voice coil of the loudspeaker. This current I_{spka} may, for
15 example, be sensed in a power supply or ground return lead, monitored in series with the load, or monitored by sensing current through or voltage across amplifier output elements.

In this embodiment circuitry in the signal processing chain provides indicative signals
20 V_{spk} and I_{spk} , indicative of the actual voice coil drive voltage V_{spka} and actual voice coil current I_{spka} respectively, to a loudspeaker protection control module 104. The loudspeaker protection control module 104 receives these indicative signals V_{spk} and I_{spk} and derives an appropriate gain control signal G_{mod} to control the digital gain stage 103 in order to modulate, i.e. reduce or increase, the gain of the signal processing
25 chain so as to modulate the signal applied to the loudspeaker to a safe level. When the indicative voltage and current signals V_{spk} and I_{spk} suggest that there is danger of thermal overload of the loudspeaker the gain applied to the input signal D_{in} is modulated such that it reduces the signal applied to the loudspeaker.

30 The loudspeaker protection control module 104 comprises power and temperature estimation module 105, which is arranged to determine, e.g. calculate, an estimate P_{vc} of the present power dissipation of the voice coil and an estimate T_{vc} of the voice coil temperature. The estimate T_{vc} of the voice coil temperature may be based on a

determination of the equivalent resistance R_e of the voice coil (which is temperature dependent according to some known function $R_e(T_{VC})$).

In this embodiment, the power and temperature estimation module 105 is also
5 arranged to determine, e.g. calculate, an estimate T_{res} of the temperature of a thermal reservoir in thermal communication with the voice coil. The estimate T_{res} of the temperature of the thermal reservoir is an indication of the temperature of a reference node that is located at or near a thermal reservoir, e.g. a heat sink, for heat generated by power dissipation in the voice coil. As noted above heat generated in the voice coil
10 may flow to the surrounding environment via various thermal paths. The surrounding environment thus acts as heat sink or thermal reservoir for heat generated in the voice coil and the estimate T_{res} may thus be an estimate of the ambient temperature of the local environment. There may however be other components of the loudspeaker, such as a heavy magnet for instance, which may function as a thermal reservoir or heat sink
15 in use, in which case the estimate T_{res} may be an estimate of the temperature of such a component, e.g. the magnet temperature. In essence the estimate T_{res} is an estimate of the temperature at the end of a thermal flow path for conducting heat away from the voice coil to the environment or a component acting as a thermal reservoir. The estimated thermal reservoir temperature T_{res} may be deduced from a comparison of the
20 measured coil temperature T_{VC} and an estimate of the coil temperature rise ΔT_{VC} based on the estimated coil power dissipation P_{VC} and on a thermal impedance model Z_{th} .

All of T_{VC} , T_{res} , and P_{VC} may thus be calculated directly or indirectly from the monitored voltage and current signals V_{spk} and I_{spk} , as explained in more detail below.

25 The loudspeaker protection control module 104 further comprises controller 106 which generates the gain control signal G_{mod} , based on, i.e. as a function of, both the voice coil power dissipation estimate P_{VC} and the voice coil temperature estimate T_{VC} and the estimated thermal reservoir temperature T_{res} .

30 In general terms, the controller 106 receives information related to the power dissipation in the voice coil as well as the temperature of the voice coil and a thermal reservoir temperature, e.g. the ambient temperature, and, based on this information, determines any gain modulation to be applied. For speaker thermal protection the gain

modulation applied will, when necessary, reduce the magnitude of the driving signal so as to reduce power dissipation. Typically therefore the gain modulation may be a modulation to reduce the overall gain. Thus if the power dissipation is relatively high and the voice coil temperature is also relatively high a gain modulation may be applied to reduce the gain applied to the input signal so as to reduce the level of power dissipation. If the power dissipation decreases and/or the voice coil temperature decreases this applied gain modulation may be at least partially removed to allow the magnitude of the drive signal to increase.

As explained in more detail below, the controller 106 may be configured to determine an allowed power limit based on the indication of voice coil temperature and the indication of the reservoir temperature, e.g. ambient temperature. The controller 106 may thence determine the value of the gain control signal, for modulating the gain applied to the drive signal voltage as a function of the indication of power dissipation in the loudspeaker and the allowed power limit. Thus a greater gain modulation may be applied the closer the estimated value of power dissipation is to the allowed power limit, and this power limit may decrease if the reservoir temperature increases. Together the estimation module 105 and controller 106 comprise loudspeaker protection control module 104.

20

Figure 2 illustrates one embodiment of a suitable estimation module, i.e. power and temperature extraction module 105.

The actual voice coil current I_{spka} may be monitored by a suitable current sensor as is well known in the art and used to derive a signal I_{spk} indicative of the coil current. In some embodiments an analogue output from the current sensor may be converted to a digital current signal I_{spk} by an analogue-to-digital convertor (ADC) 201 possibly after some pre-processing e.g. analogue filtering, amplification etc. The digital current signal I_{spk} is provided to an impedance extraction block 202.

30

The impedance extraction block 202 also receives an indication of the voltage applied to the loudspeaker, i.e. the drive voltage is monitored. In this embodiment a digital signal D_{SP} derived from a suitable point of signal processing chain 101, e.g. from the input to a digital-to-analogue convertor (DAC) 203 of the signal processing chain, may

be provided as an indication V_{spk} of the voltage of the drive signal. In other words monitoring the drive voltage may comprise monitoring the digital signal used to generate the drive signal V_{spka} . However as illustrated in figure 2 it would alternatively be possible to monitor the drive signal V_{spka} directly or via an ADC 204. It would also
 5 be possible to use the input signal D_{in} itself, i.e. the input to the signal processing chain, together with an indication of the value of the gain control signal G_{mod} and allowing for this and any other fixed or variable gain G_{xx} applied in the signal path.

The impedance extraction block 105 determines an estimate of the present resistance
 10 R_e of the voice coil, for example based on the relationship $R_e = V_{spk}/I_{spk}$, although more sophisticated known techniques such as those involving adapting coefficients of an adaptive filter receiving waveforms of V_{spk} and I_{spk} may be used if desired. **Figure 3** illustrates an electrical model of a loudspeaker voice coil. When a voltage V_{spka} is applied to the voice coil, a current I_{spka} flows. The voice coil impedance observed as
 15 defined by V_{spka}/I_{spka} comprises some inductance L_e , but at audio frequencies the ohmic resistance R_e of the coil winding may dominate.

Referring back to figure 2, the estimated value of resistance R_e may be used to determine the temperature T_{vc} of the voice coil by temperature estimation block 205.
 20 The resistance of the voice coil will have a temperature coefficient that may be known from an initial calibration step or estimated based on the type of loudspeaker used. The temperature coefficient may typically be of the order of about 4000ppm/K. The variation of the estimated resistance with respect to some reference value R_{enom} , may be used to determine an estimated temperature of the voice coil.

25 The reference coil resistance value R_{enom} may for instance be a stored nominal or test calibration value or which may be acquired in a self-calibration routine, for instance on start up. Note such a calibration would be purely an electrical measurement, at a single nominal temperature, so would not require the long measurement times of the
 30 order of the thermal time constants required for thermal impedance measurements. If the calibration value is obtained in production test (e.g. of the complete host device, or of just a flex circuit comprising the loudspeaker and associated circuitry) the ambient temperature at which this reference value is calibrated may be well controlled and known.

The estimate of voice coil resistance is also passed to power calculation block 206 which derives an estimate P_{VC} of the power dissipation of the voice coil.

- 5 The power calculation block 206, in this embodiment, determines the power dissipated using the digital representation I_{spk} of the speaker current and the determined resistance based on the relationship $P_{VC} = I_{spk}^2 \cdot R_e$. The power calculation block may calculate the power over a plurality of audio cycles, say over a few tens to hundreds of milliseconds.

10

The power dissipated in the voice coil may cause a rise ΔT_{VC} in coil temperature. This rise in temperature will depend on the thermal resistance R_{th} of a path to some thermal reservoir which can absorb the heat energy. This reservoir may be some heat sink component, or a relatively massy component such as the coil magnet, or more
 15 generally may just be the local environment at some ambient temperature. The thermal reservoir will be at a reservoir temperature T_{res} .

- Using a value of thermal resistance from the voice coil to the reservoir of R_{th} , the expected temperature rise ΔT_{VC} of the voice coil over the reservoir, e.g. ambient,
 20 temperature will be $P_{VC} \cdot R_{th}$.

The temperature of the voice coil will be given by:

$$T_{VC} = T_{res} + \Delta T_{VC} \quad (1)$$

- 25 Note that the thermal path to the reservoir, e.g. ambient, will generally include some thermal masses, and the path may be characterised by a complex thermal impedance Z_{th} rather than just a simple thermal resistance. **Figure 4a** illustrates a thermal model of a loudspeaker for thermal flow between the voice coil and a thermal reservoir, which in this model is the surrounding environment at an ambient temperature T_{amb} . The
 30 thermal mass of the voice coil is modelled by thermal capacitance C_{thvc} which is at temperature T_{VC} above a reference temperature value T_{ref} , say 300K. Assuming the reservoir temperature is not significantly changing over timescales of concern, the T_{ref} node may conveniently be sorted to T_{amb} node to simplify the model.

As mentioned above ohmic power losses can result in heating of the voice coil and thus an increase in the voice coil temperature T_{VC} . Power (modelled as thermal current) flows through a thermal resistance R_{thvc} to the adjacent magnet with thermal inertia represented by thermal capacitance C_{thm} and thence via further thermal resistance R_{thma} to the outside world, assumed to be an independently defined ambient temperature T_{amb} . It will be appreciated that this is a relatively simple model and more complex models could be developed if required, for instance including other components of the loudspeaker and/or temperature gradients within components such as the magnet. The alternative model illustrated in **Figure 4b** may also be used for convenience. It will also be appreciated that other models could be developed for flow to other components of the loudspeaker or of the device hosting the loudspeaker that may act as a thermal reservoir.

As the power of the applied signal varies, so will the rise in temperature, but with a time lag and a time-averaging time constant of possibly hundreds of milliseconds. However, assuming the thermal impedance model Z_{th} accurately reflects the coil thermal behaviour, the actual temperature rise at the voice coil will have exactly the same transient behaviour, so the difference between them will stay constant and equal to the reservoir temperature, i.e. in this model the ambient temperature. Essentially the ambient temperature acts as a ground reference voltage for the thermal equivalent circuit.

Thus referring back to Figure 3 the temperature rise ΔT_{VC} is calculated by temperature rise block 207 based on the determined power dissipation P_{VC} and a model of thermal impedance Z_{th} to the thermal reservoir. The calculated temperature rise ΔT_{VC} and the voice coil temperature T_{VC} derived from the estimated coil resistance may then be combined, e.g. by reservoir temperature estimation block 208, to provide an estimate T_{res} for the reservoir temperature. In some embodiments T_{res} may be derived by simple subtraction, i.e. via:

30

$$T_{res} = T_{VC} - \Delta T_{VC} \quad (2)$$

In other embodiments a more complex derivation may be performed, for example an iterative solution. For example the present estimate T_{VCest} of the temperature of the

voice coil, based on input power P_{VC} and estimated reservoir temperature T_{res} may be defined as:

$$T_{VCest}[i] = H_T(q^{-1}) \cdot P_{VC} + T_{res}[i] \quad (3)$$

5

where $H_T(q^{-1})$ is a discrete time model of the relevant thermal circuit, e.g. that shown in figure 4a. The next estimate of reservoir temperature may be given by:

$$T_{res}[i + 1] = T_{res}[i] + \mu \cdot (T_{VC}[i] - T_{VCest}[i]) \quad (4)$$

10

where T_{VC} is the measured voice coil temperature, i.e. the voice coil temperature as deduced from the electrical resistance. The continuous time transfer function of $H_T(q^{-1})$ may be defined, for example, by:

15

$$H = \frac{1}{\frac{1}{R_{thvc}} + s C_{thvc}} + \frac{1}{\frac{1}{R_{thm}} + s C_{thm}} \quad (5)$$

The discrete time transfer function can be defined from equation (5) using well established techniques.

20

Equation (5) is based on the reservoir temperature being the ambient temperature. As noted previously, in some embodiments the thermal reservoir may be identified as the magnet or some other loudspeaker component with a relatively high thermal capacity. Due to its relatively high thermal mass the magnet temperature changes only slowly and thus the magnet temperature can be seen as a local ambient. Using the magnet temperature as the reservoir temperature still allows the allowed power limit to be set as will be described below and has the advantage that a simple thermal model may be used, which may simplify calculations, e.g. of the estimated reservoir temperature, especially if an iterative approach is used, and which may be more robust to modelling errors. For example the model described above with reference to equation (5) may be simplified to:

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$$H = \frac{1}{\frac{1}{R_{thvc}} + s C_{thvc}} \quad (6)$$

The estimated values of temperature and power dissipation are then passed to the controller 106. **Figure 5** illustrates one example of a suitable controller. The voice coil temperature value T_{VC} deduced from the coil resistance and the reservoir temperature T_{res} are received by a power limit block 501 which, based on the present voice coil temperature determines the maximum short term or instantaneous power dissipation level P_{all} that is permitted. This maximum allowed power value P_{all} will be determined by a desired first transfer function $f_p(T_{res}, T_{VC})$, the form of which may vary depending on the particular implementation but which will generally decrease with increasing temperature, reducing to a level at or near zero at a certain voice coil temperature limit T_{max} . In general a transfer function $f_p(T_{VC})$ between the voice coil temperature T_{VC} and allowed power P_{all} , will be selected based on the reservoir temperature.

A gain calculation block 502 receives the indication of the allowed short-term power level P_{all} and also the estimate of the present level of power dissipation P_{VC} . The gain calculation block determines a gain control value, e.g. a target gain G_{tgt} , to be applied to the input signal, depending on the estimated present power dissipation, with the aim of keeping the instantaneous power dissipated at a level which is no greater than P_{all} .

In some embodiments the target gain signal G_{tgt} may be used directly as a gain control signal. In some embodiments however a gain control block 503 may apply some time-domain processing on the target gain signal, for instance to reduce any audio artefacts caused by gain changes. For instance gain changes may only be applied when the input signal crosses zero to avoid steps introduced by gain changes applied to a non-zero part of the signal. The gain control block 503 may therefore also receive the input signal D_{in} and synchronise the gain changes with respect to zero crossings to produce the gain control signal G_{mod} .

As mentioned above in general, at a given reservoir temperature, e.g. ambient temperature, the allowed power dissipation limit, P_{all} , will reduce towards zero as the voice coil temperature T_{VC} increases towards a specified maximum voice coil temperature T_{max} for the relevant loudspeaker, which may for instance be based on a recommendation from the loudspeaker manufacturer. This aims to ensure that T_{VC} will

never exceed $T_{\max}$. However rather than reduce the gain to zero suddenly when $T_{\max}$ is reached, for instance by disabling the audio output stage, the gain is preferably gradually wound down allowing a graceful and less noticeable reduction in signal, but still fast enough relative to the thermal time constants of the speaker to avoid exceeding $T_{\max}$. For instance the gain may decrease monotonically with temperature, at least over a range between a defined threshold temperature T_{th} and $T_{\max}$.

Figure 6 illustrates an example of the transfer function between the temperature of the voice coil T_{VC} and the allowed power P_{all} for determining the maximum allowed power dissipation P_{all} in power limit block 501. The plot of P_{all} with T_{VC} shall be referred to herein as an allowed power curve. One possible form of the transfer function f_P is a linear interpolation between a threshold value P_{allth} at $T_{\text{VC}} = T_{\text{th}}$ to zero at $T_{\max}$ as illustrated by solid line 601. Alternatively a design may use a function with some convex curvature between these values such as illustrated by curve 602.

Below the threshold temperature T_{th} , the line or curve may just be continued continuously, e.g. according to line 603. In such an embodiment it will be appreciated that there is no threshold temperature as such, just a function defined over a complete anticipated range of temperature. This may lead to very high power levels being permitted by this block, but in practice this may be limited elsewhere in the system, e.g. by the finite input signal range, or the output stage's supply voltage, or some maximum current limit imposed by a speaker driver amplifier. In a different approach limiting may be applied across the whole temperature range but the local transfer function may vary above and below the temperature threshold, e.g. the gradient may change as indicated by line 604.

Alternatively, the power limit may be set to a first constant value P_{allth} below the temperature threshold T_{th} , as illustrated by line 605, especially if the threshold temperature T_{th} is a relatively low temperature compared to $T_{\max}$ such that P_{allth} is so high a power that it is rarely reached, or if the maximum power is desired to be limited for some non-thermal reason, for instance to avoid damage to the user's ears.

As a further alternative the maximum allowed power may not be limited at all below the threshold temperature T_{th} , as illustrated by line 606.

In some embodiments, rather than reduce the maximum allowed power to zero at $T_{\max}$, P_{all} may be set to a small second constant value, less than and possibly significantly less than that which is expected to cause any thermal problems, as indicated by line 5 607. This will allow the gain subsequently derived to be non-zero avoiding any complete suppression of signal. In some embodiments this may be desirable to ensure some minimum output speaker signal to allow ongoing coil resistance (i.e. temperature) monitoring. This minimum gain may also prevent noise etc. in the temperature measurement from consequently modulating the gain over a range which may be small 10 on a linear scale but noticeable on a log scale and hence give rise to audible artefacts, although it will be appreciated that this could also be handled in the time-domain function, e.g. using some fixed time-out or similar. Maintaining a small but non-zero drive signal may also be useful to avoid unwanted operation of some downstream auto-mute function in the signal processing chain.

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In addition to the linear and convex curves, an s-shaped curve can be used to transition between power levels as shown in **figure 7**. For example the transfer function or allowed power curve 701 could be defined, at least between the threshold temperature T_{th} and the maximum temperature $T_{\max}$ by a parametric curve such as:

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$$P_{\text{all}} = \frac{a}{1+b*c^{-T_{\text{VC}}}} \quad (7)$$

where a , b and c are coefficients that control the flex point, the edges of the curve and its slope. Various other curves, for example polynomials, Bezier or spline curves could 25 alternatively be used to define the variation in allowed power between at least the threshold temperature and the maximum temperature.

The advantage of the s-shaped or similar curve is to enable different behaviours of the thermal limiter, depending on whether the current temperature is closer to T_{th} or to $T_{\max}$, 30 whilst allowing a smooth power transition as temperature changes.

It will therefore be appreciated that, at least when the gain of the gain element 103 of the signal processing chain is being modulated by the digital gain stage 103 in response to the controller 106, the power dissipated in the voice coil of the loudspeaker

will be limited to the maximum allowed power limit P_{all} , such as defined by the maximum allowed power curve 701 illustrated in figure 7.

Consider for instance that the loudspeaker voice coil is driven continuously with a relatively high amplitude drive signal. Below the temperature threshold there may in effect be no power limiting and thus there may be a relatively significant amount of power dissipation in the voice coil, leading to heating of the voice coil. The voice coil temperature may increase until it reaches the temperature threshold T_{th} , say 65°C for example. If the power dissipation continues the temperature of the voice coil may continue to increase. The allowed power dissipation may then be reduced leading to a gain modulation to reduce the drive signal supplied to the loudspeaker.

As noted above however the variation in temperature of the voice coil depends on the power dissipated P_{VC} and the thermal resistance R_{th} of the flow path to the thermal reservoir, e.g. the surrounding environment. Thus as long as the power dissipation is greater than a steady state value P_{ss} given by $P_{ss} = (T_{VC} - T_{res})/R_{th}$ then the voice coil temperature will continue to increase. If however the power dissipation drops below this steady state level of power dissipation the voice coil temperature will start to drop as more heat flows to the reservoir than is dissipated due to the driving signal.

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Figure 7 illustrates how the steady state power dissipation P_{ss} varies with temperature for a range of different reservoir temperatures, as indicated by the various dashed lines. It can be seen that the plot of steady state power dissipation will intersect with this particular allowed power curve at an intersection point 702 that varies with reservoir, i.e. ambient temperature.

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If therefore a loudspeaker is being driven and gain modulation is applied as the threshold temperature is reached the power dissipated will be limited to the allowed power limit. Initially the limited power dissipation will be above the steady state level and thus the voice coil will continue heating. As long as the input signal level does not drop significantly the temperature and power dissipated in the loudspeaker will thus follow the allowed power curve 701 with increasing temperature until the relevant intersection point 702 is reached. At this point the heat input to the voice coil by the

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power dissipation is matched by the heat flowing out towards the thermal reservoir and the voice coil temperature will thus stabilise at a constant temperature.

It can be seen however for this particular allowed power curve 701 the steady state
5 power dissipation and thus the steady state voice coil temperature is reached at a temperature below the maximum allowed temperature $T_{\max}$. Figure 7 also shows the points of intersection 703 between the plots of steady state power dissipation and the maximum allowed temperature $T_{\max}$. It can be seen that for each of the reservoir temperatures the intersection of the steady state power dissipation and this allowed
10 power curve 701 occurs at a lower allowed power than would be the case at the maximum allowed temperature and it can further be seen that for this particular allowed power curve 701 the difference is greater with decreasing reservoir temperature. This illustrates that were an allowed power limit to be used independently of reservoir temperature, e.g. ambient temperature, the result would be that in at least some use
15 cases a greater degree of power limiting may be applied than may be necessary to maintain the voice coil temperature within an acceptable limit.

Embodiments of the invention may thus vary the allowed power curve, i.e. the transfer function between voice coil temperature T_{VC} and the allowed power limit P_{all} based on
20 an indication of reservoir temperature $T_{res.}$, e.g. the estimated reservoir temperature. In some embodiments the allowed power curve is varied with reservoir temperature T_{res} such that the steady state power dissipation leading to a steady state voice coil temperature corresponds to the maximum allowed temperature $T_{\max}$.

25 The power limit block 501 may thus determine a suitable allowed power curve, i.e. a suitable transfer function $f_p(T_{VC})$ to be applied based on the estimated reservoir temperature $T_{res.}$ In some embodiments the power limit block may comprise a series of stored transfer functions or allowed power curves to be applied at a given reservoir temperature or range of reservoir temperatures. In some embodiments however a
30 transfer function may be adapted in a known way based on the reservoir temperature, for instance the various coefficients used to define the allowed power curve between the threshold and maximum temperature values may be adjusted based on the reservoir temperature. In some embodiments a look-up table or similar may simply

contain an indication of the allowed power P_{all} for a given voice coil temperature T_{VC} and reservoir temperature T_{res} .

As mentioned the allowed power curves may be designed so that that the allowed
5 power dissipation is substantially equal to a steady state power dissipation at the maximum allowed temperature. This may be notionally determined by the point of intersection of a plot of steady state power dissipation with the allowed power curve.

Figure 8 illustrates one example of a family of allowed power curves 801, i.e. transfer
10 functions of voice coil temperature T_{VC} with allowed power limit P_{all} for a number of different reservoir temperatures. In each case the relevant allowed power curve is arranged to intersect with a plot of steady state power dissipation at the maximum allowed temperature T_{max} .

15 The steady state power dissipation will depend on the type of loudspeaker. The gradient of this plot with increasing voice coil temperature depends on the thermal resistance of the flow path for heat flow from the voice coil to the thermal reservoirs, with the reservoir temperature influencing the amount of offset. This will depend on the components of the loudspeaker but the thermal resistance may be similar for similar
20 types of loudspeaker. The allowed power curves for the loudspeaker will thus be chosen for the particular loudspeaker or class of loudspeaker.

It should be noted that the allowed power limit may be defined based on heat flow to the surrounding environment and thus the reservoir temperature may be the ambient
25 temperature and the thermal impedance model will model heat flow to the surrounding atmosphere. In some embodiments however, as noted above, the thermal reservoir may be identified as the magnet or some other loudspeaker component with a relatively high thermal capacity, which as noted above may simplify the thermal model used.

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It can therefore be seen in figure 8 that the allowed power curves vary from a certain allowed power P_{all-th} at the threshold temperature to an allowed power $P_{all-max}$ at the maximum temperature. The allowed power $P_{all-max}$ at the maximum temperature varies

with the estimate of reservoir temperature and may be defined with respect to the steady state power dissipation at that reservoir temperature.

The allowed power at the threshold temperature may be chosen to ensure that any
5 necessary gain reduction happens in time as the voice coil temperature increases to avoid overheating. In embodiments where no gain limiting is applied below the threshold temperature the allowed power at the threshold temperature may be chosen with a view to minimizing any audible artefacts due to sudden changes when the temperature threshold is reached.

10 If no power limiting is applied before the temperature threshold is reached then three different scenarios can be envisaged. First at the time that the voice coil temperature reaches the threshold temperature the present actual power dissipation may substantially correspond to the allowed power dissipation P_{all-th} . In this case there may
15 initially be no gain reduction applied and, assuming a constant input signal, as temperature increases, an increasing gain reduction is applied so that the power dissipated P_{VC} gradually decreases according to the power allowed curve, without any initial step. This is the optimal scenario because the thermal limiter becomes active exactly when expected, when the estimated voice coil temperature T_{VC} reaches the
20 threshold temperature T_{th} and the resulting change in volume is inaudible.

It may be the case however that at the time that the threshold temperature is reached the actual power being dissipated in the voice coil P_{VC} is greater than the allowed power limit, P_{all-th} . In this case there will be an initial reduction in gain which could be
25 relatively abrupt and which could therefore result in an abrupt change in volume which is noticeable by a listener. This may be mitigated by using a relatively slow time constant for a change of gain but this could potentially reduce the ability of the loudspeaker protection circuitry to prevent overheating as the actual power dissipation could then remain above the allowed power limit for a relatively long period of time.

30 Varying the time constant with voice coil temperature is possible but still runs the risk of overheating and/or an abrupt change of gain once the time constant becomes fast enough.

The third scenario is that the actual power dissipation is less than the allowed power limit at the point at which the voice coil temperature reaches the threshold temperature. In this instance at the point that the threshold temperature is reached there would be no need for any gain reduction and the power dissipation P_{VC} is below the allowed limit $P_{all=th}$. In this case no gain reduction may be applied until the voice coil temperature reaches has increased such that the allowed power limit P_{all} has dropped to the present power dissipation. The gain will then start to be reduced but in this case the gain changes may start to occur too late to prevent overheating if the voice coil temperature is near the maximum temperature at this point, especially if slow time constants are associated with a change in gain to avoid the abrupt changes discussed previously.

In some embodiments therefore the allowed power limit at a threshold temperature may also be varied based on an estimate of the power dissipation of the voice coil P_{VC} . Thus for example if no power limiting is applied below a threshold temperature then when the threshold temperature is reached an allowed power curve may be defined that starts at the threshold temperature T_{th} at an indication of the present power dissipation in the voice coil. This may for instance be the last estimated power dissipation value or the maximum of average of the last n estimated values. The allowed power curve may then be defined between the determined value of P_{all-th} and an allowed power at the maximum temperature, i.e. $P_{all-max}$. As mentioned above the allowed power at the maximum temperature, i.e. $P_{all-max}$ may be arranged to vary depending on the estimate of reservoir temperature and in some embodiments may be set at a level that leads to a steady state power dissipation at the maximum temperature at the present reservoir temperature T_{res} .

Figure 9 illustrates how the defined allowed power curve may vary based on the estimate of voice coil power dissipation when the threshold temperature is reached. Figure 9 illustrates how the allowed power curves for different starting power dissipation at one particular reservoir temperature. Any desired type of curve, e.g. linear, S-shaped, polynomial, can be used for the power allowed curve which may be defined based on the determined estimates of voice coil power dissipation P_{VC} and reservoir temperature T_{res} . Alternatively, several predefined P_{all} curves, with different ends point P_{all-th} and $P_{all-max}$, can be stored in memory and the most appropriate curve

can be derived from the available set and/or a curve derived by interpolation between stored curves.

It should be noted that the idea of defining an allowed power curve of allowed power against voice coil temperature where the allowed power at a threshold temperature varies with an indication of estimated power dissipation represents a further novel aspect of the invention. This aspect may be applied together with using an estimate of reservoir temperature to define the allowed power curve or transfer function or may in some examples be applied without an estimate of reservoir temperature. In such examples the starting point of the allowed power curve P_{all-th} may thus vary with the estimate of power dissipation in the voice coil P_{VC} but the allowed power at the maximum allowed temperature $P_{all-max}$ may be set with regard an assumed worst case ambient temperature.

One or more of the parameters for defining the transfer function, e.g. the allowed power curve, such as P_{allth} , T_{th} , and T_{max} may be fixed in hardware or stored in a suitable non-volatile memory. Suitable values may be set in chip manufacture or in subsequent end-user device manufacturing. In some instances the control circuitry may be associated with the audio drive circuitry but may read one or more parameter values from a memory associated with the loudspeaker. In some embodiments at least some of these parameters may be configurable and may vary during use, for example controlled by a control input (not shown). For example if a temperature-independent value of P_{allth} is used below the threshold temperature T_{th} and this value is set at least partly for user ear protection, it may be set to decrease over time as the monitored period of exposure increases.

As mentioned the gain calculation block 502 receives the determined maximum allowed power level and determines the target gain G_{tgt} based on the current estimated power dissipation according to a second transfer function $G_{tgt} = f_G(P_{VC}, P_{all})$.

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Figure 10 illustrates how the target gain value may be adjusted in accordance with the estimated power dissipation P_d for different values of the maximum allowed power P_{all} . The target gain G_{tgt} may be set to reduce from some nominal value G_{nom} with increasing values of P_{VC} . The nominal gain value could be defined consistently with

the gain of other elements of the system to provide the required gain between output power of the drive signal and the input audio signal, e.g. the digital input signal D_{in} . The nominal gain value may be regarded as unity if other gains in the signal processing chain are defined appropriately.

5

Figure 10a illustrates that the target gain G_{tgt} could be defined as a linear interpolation from a nominal gain G_{nom} at zero power (or power dissipation below a threshold) to zero gain at P_{all} , i.e. $G_{tgt} = G_{nom} \cdot (1 - P_{VC}/P_{all})$. Line 1001 illustrates this interpolation for a first value of P_{all} , i.e. at a first voice coil temperature T_1 . If the temperature of the voice coil increases over time, to say T_2 then P_{all} will decrease to $P_{all}(T_2)$. This will lead to a steeper gradient in the decrease from G_{nom} to zero as illustrated by curve 1002.

Instead of a linear interpolation between G_{nom} and zero (for a given value of P_{all}) a more aggressive curve with convex curvature could be employed to allow more power at intermediate temperatures, as illustrated by curve 1003. For example a transfer function of the form $G = G_{nom} \cdot \sqrt{1 - P_{VC}/P_{all}}$ could be used to give a linear interpolation of power gain rather than voltage gain.

If the value of P_{all} is at a maximum value, for instance P_{all-th} , the gain adjustment may just be disabled, i.e. set to the nominal value G_{nom} . In effect this means that the target gain is set to its nominal or maximum value, for voice coil temperatures which are less than the threshold temperature, i.e. when $T_{VC} < T_{th}$.

The gain curves illustrated in figure 10a render it impossible to drive the voice coil to dissipate in excess of P_{all} : a near-infinite amplitude input signal would be attenuated by an almost-zero gain to limit the power to P_{all} . However this means that in practice the power will be limited to significantly less than P_{all} for any realistic input signal.

Figure 10b illustrates a modulation of the target gain G_{tgt} which applies a nominal gain G_{nom} for power dissipation below a threshold P_{TH} and then linearly decreases to zero at the maximum allowed power P_{all} . This is represented by the gain control plot 1004. Figure 10b also illustrates however that the actual voice coil power dissipation for a given input signal will depend parabolically on the applied voltage gain modulation G_{tgt} , as illustrated by curve 1005 which shows how the dissipated voice coil power P_{VC}

varies with target gain value for a constant input signal power P_{in} , e.g.

$P_{VC} = G_{tgt}^2 * G_{xx} * P_{in}$. Thus for a given input signal, the system will settle at an equilibrium gain G_{eq} and power dissipation P_{eq} corresponding to the intersection of this curve 1005 with the plot 1004 representing the designed dependence of gain on
 5 estimated power dissipation. The maximum power delivered may thus be substantially less than P_{all} .

In some embodiments therefore, as illustrated in **Figure 10c**, the gain control transfer function may be designed such that the applied gain G_{tgt} is not zero, but instead is
 10 some value G_{eq} consistent with attenuating the output power dissipation to equal or less than P_{all} for even the maximum possible input signal (generally limited by the dynamic range of upstream circuitry, or in some embodiments may be subject to controlled clipping) and the maximum gain G_{xx} applied in the rest of the signal path. Figure 10c thus shows that the target gain G_{tgt} may vary according to a transfer
 15 function, illustrated by plot 1006, such that the gain is at the nominal value if the power dissipation is below a threshold and then varies, linearly in this example, to the value G_{eq} at P_{all} . The value of G_{eq} is defined with respect to the power dissipation of the maximum possible input signal P_{inmax} and the gains along the signal processing chain. Thus if the input signal is the maximum possible the target gain may be reduced until
 20 the target gain is at a level that ensures that the voice coil power dissipation P_{VC} is substantially equal to (or just below) the maximum allowed power dissipation P_{all} .

As illustrated in **Figure 10d**, if a smaller signal than the maximum P_{inmax} is applied, then the actual dissipated power for a given target gain will be lower than would be the case
 25 for the maximum input signal. Thus the intersection between the gain control function 1006 and the relationship of dissipated power with target gain would be at a target gain G_{eqy} corresponding to a power dissipation P_{VCy} , which would be lower than the maximum allowed power P_{all} . However the reduced output power P_{VCy} will tend to lead to a reduction in the voice coil temperature, which will tend to result in an increased
 30 value of P_{all} , say P_{allTx} , resulting in a change in the gain control transfer function, as illustrated by plot 1007 in **figure 10e**. The target gain and output power will thus tend to increase to a new equilibrium point (G_{eqx} , P_{VCx}) closer to the original P_{all} .

For simplicity the gain control curve has been illustrated as a linear voltage gain versus power dependence. As noted above with respect to curve 1003 in Figure 10a, other dependencies are possible, for instance the voltage gain may vary as the reciprocal of the estimated power dissipation or as the square root of the reciprocal. The
5 dependency may alternatively follow some S-shape characteristic.

It will again be appreciated that changes in the power dissipated can occur over relatively quick timescales and can occur faster than the time constant of temperature change of the voice coil or magnet. Thus for rapid changes of the dissipated power the
10 value of P_{all} may be substantially unchanging and thus the particular target gain vs. dissipated power function will be substantially fixed. Over a longer timescale however the voice coil temperature may change and thus the particular gain vs. power profile may also vary. This could lead to a change in gain being applied some time after the input signal level has stabilised.

15 It will be appreciated that the discussion with reference to figures 10a to 10e has focussed on generating a gain control value which is a target gain setting for thermal protection, i.e. a value corresponding to the gain to be applied. Thus the target gain drops with increasing values of power dissipation P_{VC} . Equivalently however the gain
20 control value could be a gain modulation value, indicating the magnitude of the modulation to the nominal gain setting, which would increase with power dissipation.

It can therefore be seen that in general the speaker protection module of embodiments of the present invention generates a control signal for modulating the gain applied to an
25 input audio signal used to drive a loudspeaker based on a measure or estimate of the present voice coil temperature of the loudspeaker, an indication of the power dissipation in the loudspeaker and also an indication of the temperature of a thermal reservoir to which heat generated in the voice coil flows. The gain applied may vary in accordance with changes in the power dissipated in the loudspeaker (at least with a
30 range of expected operating temperature) and the amount of change of gain resulting from a given change in power dissipation depends on the voice coil temperature (via the P_{all} dependence).

The indication of the temperature of a thermal reservoir may be determined or estimated using a suitable thermal impedance model as described above, e.g. by estimation of the voice coil temperature and changes in the voice coil temperature with power dissipation. However it would be possible to determine the indication of
5 reservoir temperature via some suitable temperature sensor, which may also be used for other monitoring purposes, and adjust the allowed power based on a measure of reservoir temperature.

It should be noted that gain factors described above are defined as voltage gain
10 factors, suitable for applying to the signal as a simple multiplication, rather than power gain (i.e. the square of a voltage or digital signal gain) even though defined with respect to a power variable. In some embodiments the gain control signal may be generated as a non-linear gain value, for example representing the required gain in decibels or such like coupled to a gain stage 103 configured suitably.

15 In some embodiments the gain control for thermal protection may be combined with a gain control applied for user volume control. Thus gain element 103, e.g. a digital multiplier, may be arranged to apply a gain modulation to the input signal that applies any user volume controller gain along with any gain modulation for thermal protection
20 (and/or any other required gain modulation such as for excursion limiting or ear protection). The gain controller 106 may therefore also receive an additional gain control signal, such as a user volume control signal. In some embodiments the nominal gain value G_{nom} may be modulated by such a user volume control signal to become a new value G_{adj} . This may scale the whole characteristic vertically such that
25 the gain is maintained at G_{adj} until the threshold P_{all-th} is reached and then reduced down to zero (or to the defined small non-zero level) at some maximum value $P_{all-max}$. In some embodiments however the gain may be maintained equal to G_{adj} until it intercepts the previous nominal interpolation function thus avoiding the need for any signal attenuation until higher power levels.

30 As mentioned above a gain control block 503 may apply some time-domain processing on the target gain signal to improve the implementation of the required gain change. It will be appreciated that a change in gain could in some instance lead to an audible

artefact in the audio and the time-domain processing may aim to reduce or eliminate such artefacts.

Such time domain processing may include zero-crossing detection of the input signal
5 D_{in} . For instance gain changes may only be applied when the input signal crosses zero to avoid steps introduced by gain changes applied to a non-zero part of the signal.

The time domain processing may additionally or alternatively comprise applying decay
10 time constants to limit the rate of change of any gain reductions applied to the signal so as to reduce any audible artefacts. Such decay time constants may be longer than audio signal time constants but shorter than any thermal time constants.

The time domain processing may additionally or alternatively comprise applying attack
15 time constants to limit the rate of change of any gain increases applied to the signal, e.g. as the voice coil cools down following a reduction in the amplitude of the drive signal (possibly due to a reduced input signal and/or a reduction in gain being applied). Such attack time constants may be longer than audio signal time constants. They may be longer than at least one of the thermal time constants. This may reduce possible thermal oscillations and consequent unnecessary or avoidable gain modulations.

20 As noted above however using an estimate of the present power dissipation P_{VC} to define an allowed power curve may reduce the likelihood of an abrupt change in gain that may be noticeable to a listener whilst reducing the need for slow attack time constants that may increase the risk of overheating.

25 As noted briefly above such gain profile could be variable and change, for example, based on the current voice-coil temperature. For instance, if the temperature of the voice-coil increases and exceeds the threshold temperature T_{th} because of a signal being applied to the speaker, the thermal limiter, i.e. the loudspeaker protection
30 system, will start to apply a gain reduction to reduce the output power. Initially the thermal limiter can be configured to use a relatively long attack time so as to apply a relatively gradual change in signal level as the temperature crosses T_{th} . However if the voice-coil temperature continues to rise above T_{th} and is approaching T_{max} , a fast attack time can be implemented to ensure that the power dissipation is reduced more quickly

so as to prevent the temperature from exceeding the maximum allowed level. A similar approach can be used to set different hold and release times.

By using variable time constants, it is possible to satisfy the requirements of protection, whilst at the same time maximising loudness and reducing the chance of gain changes resulting in a noticeable jump in sound level. While in a safer temperature zone, the attack times can be slower and the release faster to maximize the output power while reducing the perceived gain variation. If the temperature is closer to $T_{\max}$, the attack can be faster and the release slower to guarantee that only the allowed amount of power is driven into the system.

Additionally or alternatively the gain control 503 may be arranged to apply time-outs or minimum intervals between gain updates, to limit the maximum frequency of gain changes and hence any audio artefacts.

As mentioned above if there is no or little output power it may be difficult to obtain an accurate estimate of coil temperature, in which case a time-out may be imposed before the gain is recovered enough to obtain a revised temperature estimate.

As mentioned above, the various parameters of the power limit block 501 may be fixed in hardware or stored in memory and/or may be configurable in use. Likewise the parameters of the gain calculation block and gain control block may similarly be fixed in hardware or non-volatile memory and may be set in chip or end-user device manufacturing. One or more parameters may vary during use, e.g. controlled by a further control input. The calculation of functions f_P , f_G may be implemented via look-up tables or by customised or programmable processing hardware implementing the desired algebraic formulae.

It will be appreciated by one skilled in the art that the loudspeaker protection control module 104 may be implemented by dedicated electronic circuit components and/or by various processing elements such as a general purpose programmable digital processor or FPGA array or the like suitably programmed. For example the power and temperature extraction block 105 and/or the controller 106 may be implemented, at least partly, as software modules running on a suitable processor. The term modules

and block should therefore be read as covering both software modules or hardware modules or a mixture of both software and hardware. Any references to circuitry for these components could also mean suitable general processing circuitry.

5 Figures 11a shows a flow diagram illustrating the general method implemented by some embodiments of the invention such as described above. At step 1101 a loudspeaker protection control module receives signals V_{spk} and I_{spk} indicative of the monitored voice coil drive voltage V_{spka} and voice coil current I_{spka} . The loudspeaker protection control module 104, at step 1102, derives an indication or estimate of the
10 resistance voice coil resistance R_e . At step 1103 an estimate T_{VC} of the voice coil temperature is derived from the estimated voice coil resistance R_e . At step 1104 an estimate P_{VC} of the present power dissipation of the loudspeaker, is derived from the indicative voltage and current signals V_{spk} and I_{spk} (or optionally from at least one of these signals and also the estimated voice coil resistance R_e). At step 1105 an
15 estimate of a thermal reservoir temperature T_{res} , e.g. a thermal reference or ambient temperature, is derived from T_{VC} and P_{VC} in conjunction with a thermal impedance model Z_{th} .

A target gain control value may then be derived (step 1106) based on the voice coil
20 power dissipation estimate P_{VC} and the voice coil temperature estimate T_{VC} and the reservoir temperature estimate T_{res} . This target gain control value may be used directly as a gain control signal or optionally, at step 1107 additional processing may derive a gain control signal G_{mod} . The gain control signal may then be applied to the input signal (step 1108).

25

Figure 11b shows a flow chart illustrating some of the processing that may be applied in calculating the target gain. At step 1109 the voice coil power dissipation estimate P_{VC} and the voice coil temperature estimate T_{VC} and the ambient temperature estimate T_{amb} are received. At step 1110 an allowed maximum power P_{all} is derived based on
30 a defined function $f_p(T_{VC}, T_{res})$. The allowed power P_{all} is then used together with the voice coil power dissipation estimate P_{VC} to derive a target gain G_{tgt} (step 1111)

In some applications it may be desirable to determine an indication of the loudspeaker voice coil resistance and/or an indication of a reservoir temperature, e.g. an ambient

- temperature for other reasons. For example an estimate of impedance may be useful; for limiting the excursion of the loudspeaker. Thus at least some blocks of the power and temperature extraction block 105 may be shared with other elements of speaker protection circuitry, for example an impedance extraction block 202 such as described with respect to figure 2. **Figure 12** illustrates an embodiment of the invention where similar components to those described above are identified using the same reference numerals but where the protection module 104 also comprises an excursion controller 1201 for controlling an additional gain element 1202 in the signal processing chain.
- 10 A power and temperature extraction block 105 receives an indication of the voice coil current and the drive signal voltage (conveniently receiving the digital input signal D_{SP} input to the DAC output stage 203) as described previously. This block will determine, i.e. calculate, an estimate of the coil resistance as described above and also determine power dissipation of the voice coil and estimates of the voice coil and reservoir
- 15 temperatures. The power and temperature estimates are provided to thermal protection controller 106 to generate a gain modulation signal G_{mod} as described previously. In this embodiment however an impedance extraction block of the power and temperature extraction block 105 also extracts other impedance parameters of the voice coil for use in excursion limiting circuitry. It will be appreciated that coil
- 20 impedance varies depending on temperature and on its position with respect to the magnet etc. Excursion controller therefore receives an indication of the coil impedance and determines an appropriate gain to be applied to the audio signal by gain element 1202 to limit the excursion of the loudspeaker to within safe bounds.
- 25 It would of course be possible to integrate excursion controller 1201 and thermal protection controller 106 in a single functional block and in some embodiments a single gain control signal may be produced and used to control a single gain element.
- Embodiments have been described above in relation to a protection module for one
- 30 output speaker. Other embodiments may comprise a protection module for a plurality of output speakers, which may all receive the same input signal or in some embodiment there may be a plurality of different input signals. The protection module be configured to treat each input signal as an independent channel, or gains may be ganged, so that all gains are reduced together, based on the worst case channel.

Since actual output powers and coil temperatures are used, there is no need to assume ultra-safe values for thermal time constants etc. so less margin is needed, and each speaker can drive closer to its safe operating limits. For example if one speaker has poor thermal resistance, it would only be necessary to limit the input signals if that particular speaker is receiving a large signal.

Embodiments of the invention therefore relate to speaker protection circuitry for thermal protection of a loudspeaker, in particular to limit the voice coil temperature within safe limits by modulating the gain of the drive signal when required. In embodiments the circuitry calculates, i.e. determines, both an estimate of the power being dissipated in the loudspeaker and the present voice coil temperature to determine an acceptable power limit and reduces the gain of the drive signal based on the relative level of present power dissipation and the acceptable power limit where the acceptable power limit is determined based on an estimate of the temperature of a reservoir for heat generated in the voice coil.

Such speaker protection circuitry may be implemented in an electronic apparatus or device 1300 as illustrated in **figure 13**, for example a mobile phone. This device comprises a loudspeaker 102 which is driven from a driver circuit block 1301, which forms at least part of the signal processing chain 101. The driver circuit block 1301 receives a digital audio signal D_3 and delivers a resultant voltage V_{spka} across the speaker.

This driver circuit block 1301 may comprise a DAC (possibly oversampled e.g. delta-sigma) and analogue amplifier powerful enough to drive the impedance of the speaker. Alternatively it may comprise a Class D amplifier, either half-bridge or full-bridge, with an analogue input from a DAC, or possibly an all-digital Class D modulator. The driver signal processing chain may also possibly include analogue signal processing.

The speaker current I_{spka} is monitored to provide a signal representative of this current. An analogue current sense signal may be generated by a sense resistor which may be local to the speaker (possibly buffered locally) or co-located with the amplifier. The amplifier may be inside the speaker package or may be a more remote power amplifier, either discrete or embedded in a more complex codec. As an alternative to a sense

resistor the voltage across a MOS output transistor may be sensed to measure the current. Whilst an analogue signal for the speaker current could be provided, in some embodiments it may be preferred to provide a digital signal DI_{spk} indicative of the sensed current. The sense buffer/digitising circuitry may therefore be provided as part of the local speaker driver chip 1301. Note that where a sense resistor or the like is used for current monitoring there may be a need for some room-temperature electrical calibration of the temperature-sense resistor. Such calibration would however be rapid, of the order of milliseconds and such calibration does not require the long time constants associated with trying to determine thermal resistance from temperature versus power measurements.

The digital speaker current signal DI_{spk} is provided along with a digital signal DV_{spk} representative of V_{spka} . Where the driver circuit 1301 includes analogue processing the driver circuit may include an ADC to deliver the signal DV_{spk} , but in many cases D_3 will already be an adequate indicative signal.

A digital signal processing (DSP) 1302 block implements the speaker protection control module. The DSP block 1302 may receive a digital input audio signal D_{in} intended for the speaker 102. This could for example be an audio signal D_{in1} received from an interface 1303, for instance an RF radio/wireless interface or modem which could for example be received audio for a voice/video call and/or streaming media. At other times the input could be an audio signal D_{in2} which may be received from some data storage 1304, for instance disk storage, either mechanical or solid-state, or some other semiconductor memory. This storage may be a permanent part of device 1300 or may be attachable storage such as a memory card or USB stick or suchlike. The DSP 1302 includes a gain stage to apply gain to the input signal D_{in} and also possibly further DSP or multiplier blocks to perform further signal processing to generate the digital signal D_3 supplied to the driver block 1301.

The speaker protection control module may be implemented by software code running on the DSP 1302.

This software code may be stored in the device as firmware on some non-volatile memory 1305 e.g. EEPROM (to preserve program data when the battery becomes discharged or is removed for replacement).

- 5 The relevant software for running the loudspeaker protection module may be loaded into the DSP on power-up, which could be for example awaking of the device 1300 from a standby mode, or on start-up of the speaker driver function, e.g. on receipt of user command to start outputting sound via the loudspeaker.
- 10 A separate processor, for example an applications processor, AP, or processor core 1306 may control this start-up.

In some applications at least some audio data (e.g. ring tone, pre-recorded voice alert or the like) may be provided from the NVM 1305, either directly or via processor AP

15 1306.

As mentioned previously in some embodiments the speaker protection control module may determine the resistance of the voice coil based on a reference voice coil resistance which could be determined on device start-up. As also mentioned

20 previously in some embodiments a temperature sensor 1307 may be associated with the loudspeaker and/or host device to provide an indication of reservoir temperature T_{res} .

It will of course be appreciated that the various blocks illustrated in figure 13 or parts

25 thereof may be co-integrated with the other blocks or parts thereof or with other functions of the host device. For example the DSP 1302 and driver block 1301 may be co-integrated into an Audio Hub.

The skilled person will thus recognise that some aspects of the above-described

30 apparatus and methods, for example the calculations performed by the processor may be embodied as processor control code, for example on a non-volatile carrier medium such as a disk, CD- or DVD-ROM, programmed memory such as read only memory (Firmware), or on a data carrier such as an optical or electrical signal carrier. For many applications embodiments of the invention will be implemented on a DSP (Digital

Signal Processor), ASIC (Application Specific Integrated Circuit) or FPGA (Field Programmable Gate Array). Thus the code may comprise conventional program code or microcode or, for example code for setting up or controlling an ASIC or FPGA. The code may also comprise code for dynamically configuring re-configurable apparatus
5 such as re-programmable logic gate arrays. Similarly the code may comprise code for a hardware description language such as Verilog TM or VHDL (Very high speed integrated circuit Hardware Description Language). As the skilled person will appreciate, the code may be distributed between a plurality of coupled components in communication with one another. Where appropriate, the embodiments may also be
10 implemented using code running on a field-(re)programmable analogue array or similar device in order to configure analogue hardware

Embodiments of the invention may be arranged as part of an audio processing circuit, for instance an audio circuit which may be provided in a host device. A circuit
15 according to an embodiment of the present invention may be implemented as an integrated circuit. One or more loudspeakers may be connected to the integrated circuit in use.

Embodiments may be implemented in a host device, especially a portable and/or
20 battery powered host device such as a mobile telephone, an audio player, a video player, a PDA, a mobile computing platform such as a laptop computer or tablet and/or a games device for example. Embodiments of the invention may also be implemented wholly or partially in accessories attachable to a host device, for example in active speakers or headsets or the like.

25 It should be noted that the above-mentioned embodiments illustrate rather than limit the invention, and that those skilled in the art will be able to design many alternative embodiments without departing from the scope of the appended claims. The word “comprising” does not exclude the presence of elements or steps other than those
30 listed in a claim, “a” or “an” does not exclude a plurality, and a single feature or other unit may fulfil the functions of several units recited in the claims. Any reference numerals or labels in the claims shall not be construed so as to limit their scope. Terms such as amplify or gain include possibly applying a scaling factor of less than unity to a signal.

CLAIMS

1. A system for thermal protection of a loudspeaker comprising:
a controller configured to generate a control signal for modulating the gain of a
5 signal processing chain driving said loudspeaker,
wherein said controller is configured such that the control signal is generated as
a function of each of:
an indication of voice coil temperature of the loudspeaker;
an indication of power dissipation in the voice coil of the loudspeaker; and
10 an indication of a reservoir temperature of a thermal reservoir for heat flow
from the voice coil.
2. A system as claimed in claim 1 wherein the controller comprises;
a power limit module configured to determine an allowed power function of an
15 allowed power dissipation with voice coil temperature based on said
indication of a reservoir temperature; and
a gain calculation module configured to determine a gain setting based on the
indication of voice coil temperature, the indication of power dissipation in
the voice coil and the allowed power function,
20 wherein said control signal is based on said gain setting.
3. A system as claimed in claim 2 wherein the power limit module is configured to
determine the allowed power function such that the allowed power dissipation at
a maximum allowed temperature of the voice coil depends on said indication of a
25 reservoir temperature.
4. A system as claimed in claim 3 wherein the power limit module is configured to
determine the allowed power function such that the allowed power dissipation at
the maximum allowed temperature corresponds to a power dissipation that leads
30 to a substantially steady state temperature of the voice coil at the relevant
reservoir temperature.

5. A system as claimed in claim 2 or claim 3 wherein the power limit module is configured to determine the allowed power function for a voice coil temperature range between a threshold temperature and said maximum allowed temperature.
- 5 6. A system as claimed in claim 5 wherein the allowed power function between the threshold temperature and said maximum allowed temperature corresponds to at least one of: an S-shaped curve, a polynomial curve, a Bezier curve; or a spline curve.
- 10 7. A system as claimed in claim 5 or claim 6 wherein the power limit module is configured to determine the allowed power function such that for any voice coil temperature below a the threshold temperature no limit on allowed power is applied.
- 15 8. A system as claimed in any of claims 5 to 7 wherein the power limit module is configured to determine the allowed power function such that the allowed power dissipation at the threshold temperature is based on said indication of power dissipation in the voice coil of the loudspeaker.
- 20 9. A system as claimed in any of claims 2 to 8 wherein the gain calculation module is configured to determine the gain setting based on an allowed power dissipation determined according to the allowed power function and the indication of power dissipation in the voice coil.
- 25 10. A system as claimed in claim 9 wherein the gain calculation module is configured to determine the gain setting according to a gain control transfer function.
11. A system as claimed in claim 10 wherein the gain control transfer function varies the gain setting from a first gain setting at a first value of power dissipation in the voice coil of the loudspeaker to a second gain setting at a second value of power dissipation in the voice coil, wherein the first gain setting corresponds to a maximum gain setting and the second gain setting corresponds to a lower gain setting.
- 30

12. A system as claimed in claim 11 wherein the second value of power dissipation in the voice coil corresponds to the allowed power dissipation and the second gain setting corresponds to a gain setting that would lead to a power dissipation substantially equal to the allowed power dissipation if an input signal to the signal processing chain driving said loudspeaker was at a maximum level.
13. A system as claimed in any preceding claim comprising an estimation module configured to determine said indication of reservoir temperature based on said indication of power dissipation of the voice coil.
14. A system as claimed in claim 13 wherein the estimation module comprises:
a temperature rise module configured to determine an estimated temperature rise based on the indication of power dissipation of the voice coil and a thermal impedance model of a thermal path between the voice coil and the thermal reservoir; and
a reservoir temperature estimation module configured to determine the indication of reservoir temperature based on the indication of voice coil temperature and the estimated temperature rise.
15. A system as claimed in claim 13 or claim 14 wherein the estimation module comprises at least one input for receiving a first signal indicative of voltage applied to the voice coil of said loudspeaker and a second signal indicative of current flowing in said voice coil and is configured to determine said indication of temperature of the voice coil and said indication of power dissipation in the voice coil based on said first and second signals; wherein at least said estimate of temperature is based on an estimate of resistance of said voice coil which is determined based on said first and second signals.
16. A system as claimed in claim 15 wherein said estimation module is configured to determine said estimate of voice coil resistance based on:
the difference between the value of said estimated voice coil resistance and a reference resistance value at a known temperature; and
a temperature coefficient for the loudspeaker voice coil.

17. A system as claimed in claim 15 or claim 16 wherein said estimation module is configured to determine said indication of power dissipation based on said estimated voice coil resistance and said second signal indicative of current flowing in said voice coil.
- 5
18. A system as claimed in claim 17 wherein said estimation module is configured to determine said estimate of power dissipation by multiplying said estimated voice coil resistance by the square of the value of said second signal indicative of current flowing in said voice coil.
- 10
19. A system as claimed in any of claims 1 to 12 comprising a temperature sensor configured to measure said indication of reservoir temperature.
- 15
20. A system as claimed in any preceding claim wherein the indication of a reservoir temperature is an indication of an ambient temperature for the loudspeaker.
- 20
21. A system as claimed in any of claims 1 to 19 wherein the indication of a reservoir temperature is an indication of the temperature of a component of the loudspeaker other than the voice coil.
- 25
22. A system as claimed in 21 wherein said component is a magnet of the loudspeaker.
- 30
23. A system as claimed in claim 2 or any claim dependent, directly or indirectly on claim 2, wherein said controller comprises a gain control module configured to apply time domain processing to said gain setting to provide control signal.
24. A system as claimed in claim 23 wherein said time domain processing comprises applying at least one of an attack time constant and a decay time constant to said gain control value to generate said control signal.
25. A system as claimed in claim 24 wherein the gain control module is configured such that at least one of the attack time constant and a decay time constant is variable based on the indication of voice coil temperature.

26. A system as claimed in any preceding claim wherein said controller is configured to time the application of any gain changes to synchronise with zero crossings in the input signal.
- 5
27. A system as claimed in any preceding claim wherein said controller is configured such that the maximum frequency of gain changes applied is maintained below a predetermined limit.
- 10
28. A system as claimed in any preceding claim comprising a gain element for applying a gain to the input signal, said gain element being controlled by said controller.
- 15
29. A system as claimed in claim 28 wherein said controller controls the gain of said gain element based on said control signal and at least one other gain setting.
30. A system as claimed in claim 29 wherein said at least one other gain setting is one of: a user controlled volume setting; a gain control setting for excursion limiting.
- 20
31. A system as claimed in any preceding claim wherein said controller further comprises an excursion limiting module configured to generate a second gain setting for excursion limiting of the loudspeaker.
- 25
32. A system as claimed in claim 31 wherein the controller is configured to generate said control signal for modulating the gain of a first gain element in the signal processing chain and to further modulate the gain of a second gain element in the signal processing chain based on the second gain setting.
- 30
33. A system as claimed in claim 31 wherein the controller is configured such that said control signal is further based on said second gain setting.
34. A system as claimed in any preceding claim comprising a signal processing chain for driving said loudspeaker.

35. A system as claimed in claim 34 comprising a loudspeaker.
36. An electronic apparatus comprising a system as claimed in any preceding claim.
- 5 37. An electronic apparatus as claimed in claim 36 wherein said apparatus is at least one of: a portable device; a battery power device; a computing device; a communications device; a gaming device; a mobile telephone; a personal media player; a laptop, tablet or notebook computing device.
- 10 38. A system for thermal protection of a loudspeaker comprising a power limit block for determining an allowed power function of power dissipation against temperature for a voice coil of a loudspeaker, wherein the power limit block has an input for receiving an indication of the temperature of a thermal reservoir for
- 15 heat generated in the voice coil and wherein the allowed power function depends on said temperature of the thermal reservoir.
39. A system as claimed in claim 38 wherein power limit block is configured such that the value of allowed power at a maximum temperature varies depends on said
- 20 temperature of the thermal reservoir.
40. A system as claimed in claim 38 or 39 wherein the temperature of the thermal reservoir is an ambient temperature for the loudspeaker.
- 25 41. A thermal protection system for a loudspeaker comprising:
at least one input for receiving a first signal indicative of voltage applied to the voice coil of said loudspeaker and a second signal indicative of current flowing in said voice coil;
a temperature and power estimation module configured to determine:
- 30 an estimate of temperature of the voice coil based on an estimate of resistance of said voice coil which is determined based on said first and second signals;

- an estimate of power dissipation in the voice coil based on said first signal,
second signals and/or said estimate of resistance of said voice coil;
and
an estimate of temperature of a thermal reservoir for heat produced in the
voice coil based on a comparison of said estimate of temperature of
the voice coil the voice coil and an estimate of rise of coil temperature
based on a thermal speaker model and said estimate of power
dissipation in the voice coil;
- a gain controller configured to generate a gain control signal for modulating the
gain of a signal processing chain driving said loudspeaker, wherein said
gain control signal is generated as a function of each of said estimate of
temperature of said voice coil, said estimate of power dissipation in the
voice coil and said estimate of temperature of a thermal reservoir.
42. A system for thermal protection of a voice coil of a loudspeaker comprising:
a module configured to generate an estimate of temperature of said voice coil, an
estimate of power dissipation in the voice coil and an estimate of a
temperature of a thermal reservoir for heat produced in the voice coil based
on a voltage applied to said voice coil and a current flowing through said
voice coil and generate a gain control signal for modulating a gain of a
signal processing chain driving said loudspeaker, wherein said gain control
signal is based on said estimates of temperature of said voice coil, power
dissipation in the voice coil and temperature of the thermal reservoir.
43. Loudspeaker protection circuitry, for providing a gain control signal for controlling
the gain applied to an input signal to provide a drive voltage into a loudspeaker
voice coil, comprising a controller configured to:
receive signals indicative of the voice coil current and drive voltage;
calculate from said indicative signals, an estimate of the present voice coil
temperature and an estimate of the power dissipation of the voice
coil, wherein at least said estimate of voice coil temperature is based
on an estimate of the present voice coil resistance which is
determined from said indicative signals;

calculate the temperature of a thermal reservoir from said estimate of voice coil temperature and said power dissipation and a thermal speaker model; and

5 generate and output said gain control signal as a function of all three of the estimate of voice coil temperature, the estimate of power dissipation and the estimate of temperature of a thermal reference node.

44. A system for thermal protection of a loudspeaker comprising a power limit block for determining an allowed power function of allowed power dissipation for a
10 voice coil temperature range between a lower threshold temperature and a higher threshold temperature, wherein the power limit block has an input for receiving an indication of the power dissipation in the voice coil and wherein the allowed power function is determined such that the allowed power dissipation at the lower temperature threshold corresponds substantially to the indication of the
15 power dissipation in the voice coil.

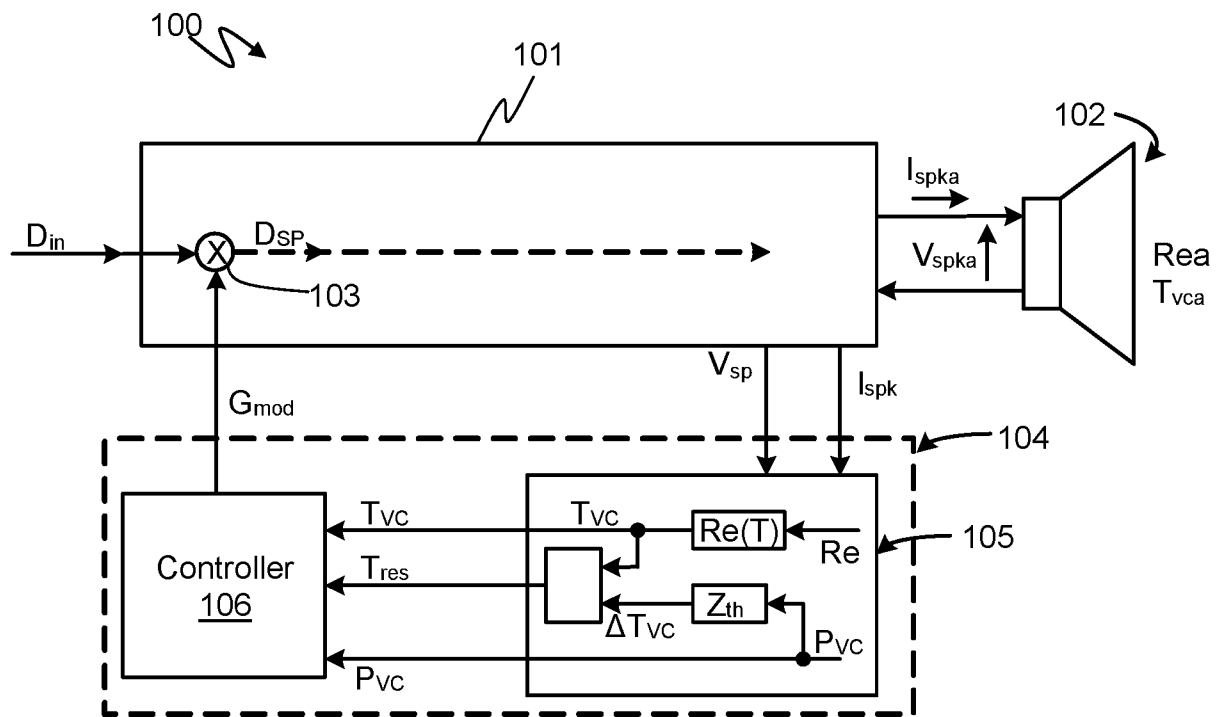


Figure 1

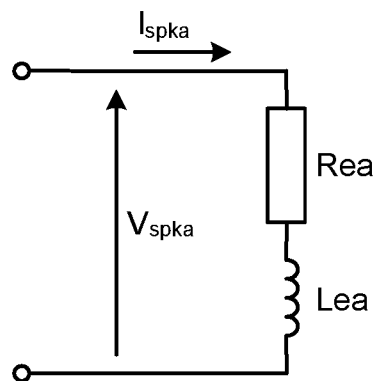


Figure 3

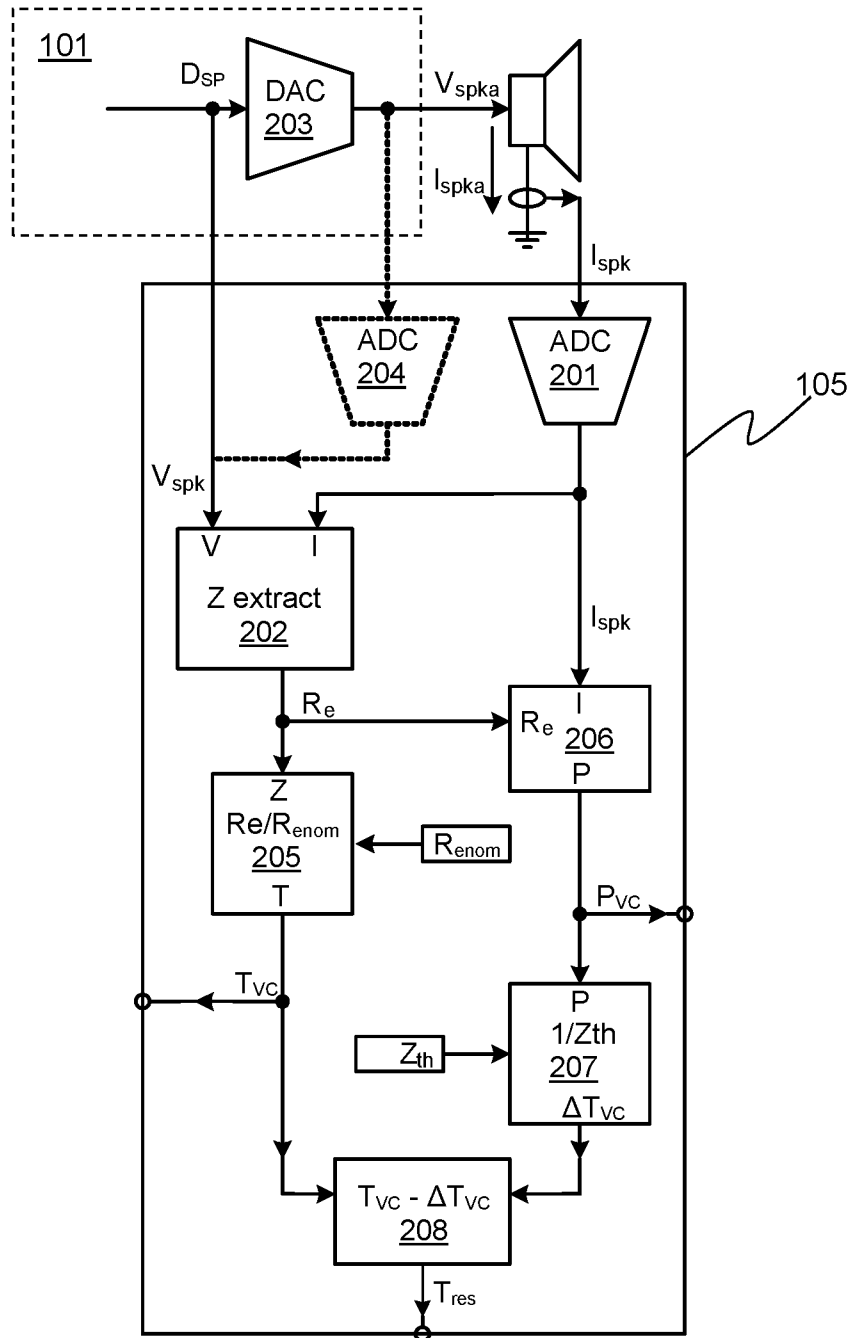


Figure 2

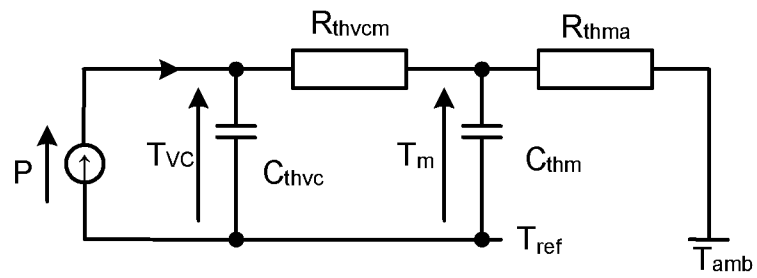


Figure 4a

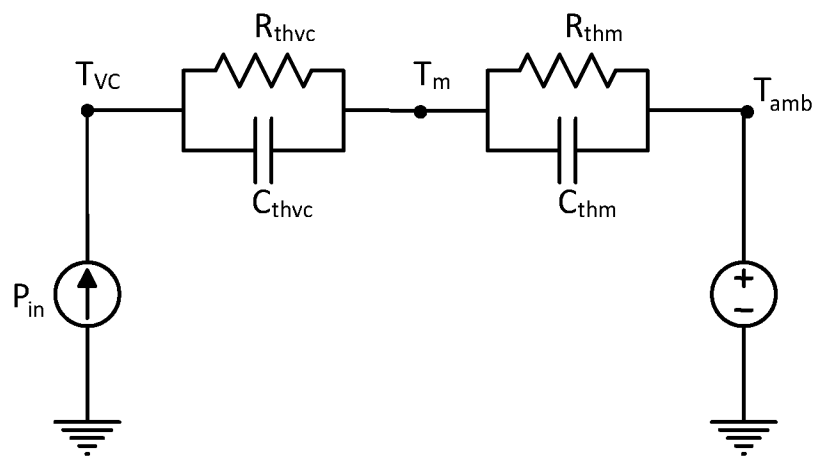


Figure 4b

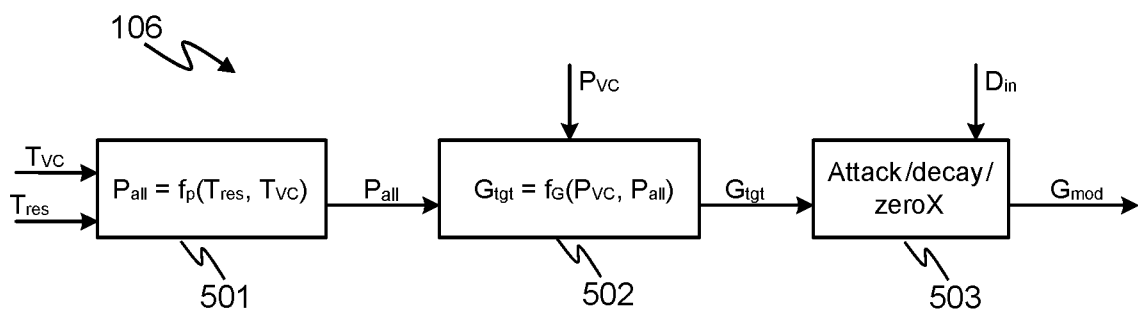


Figure 5

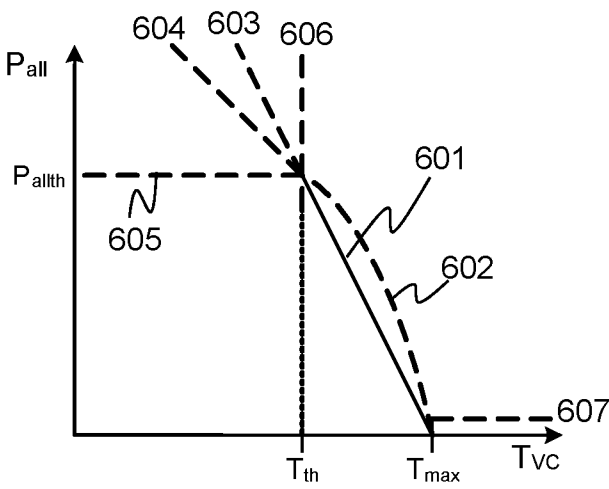


Figure 6

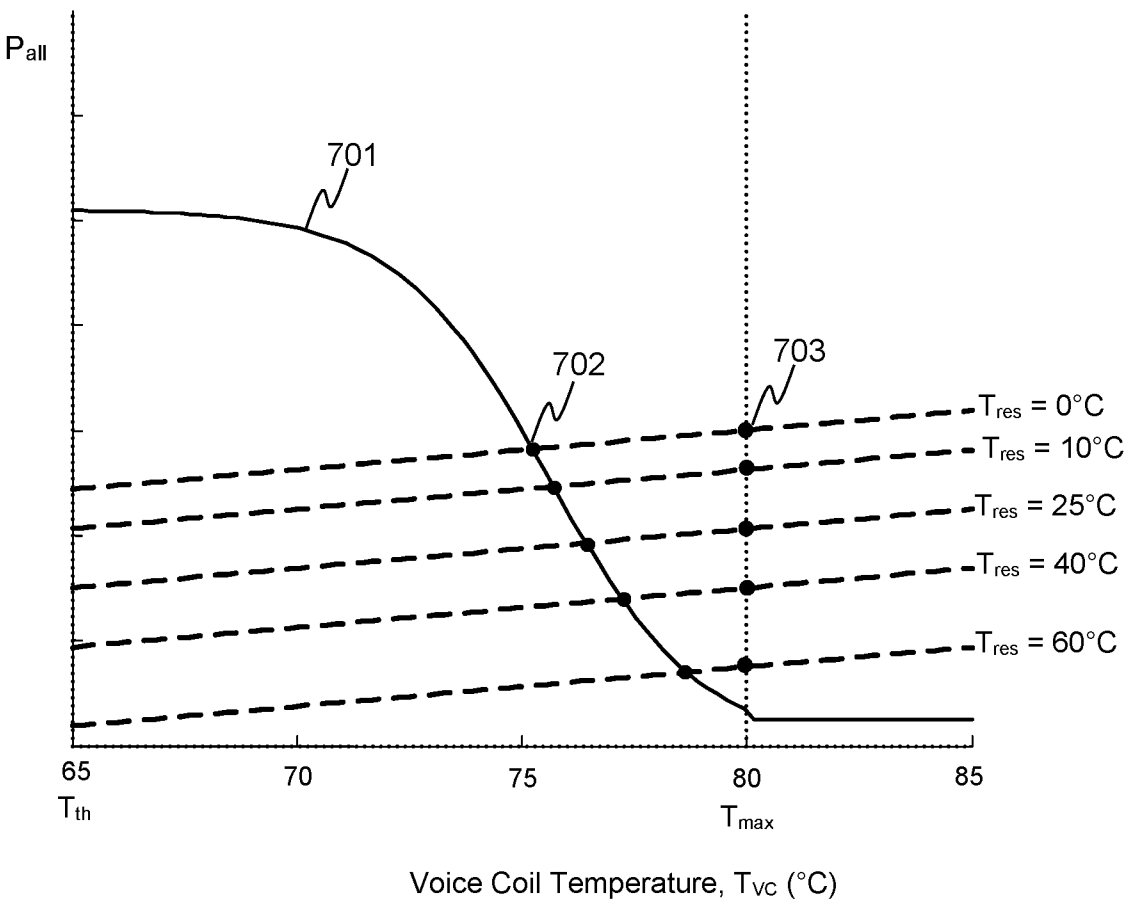


Figure 7

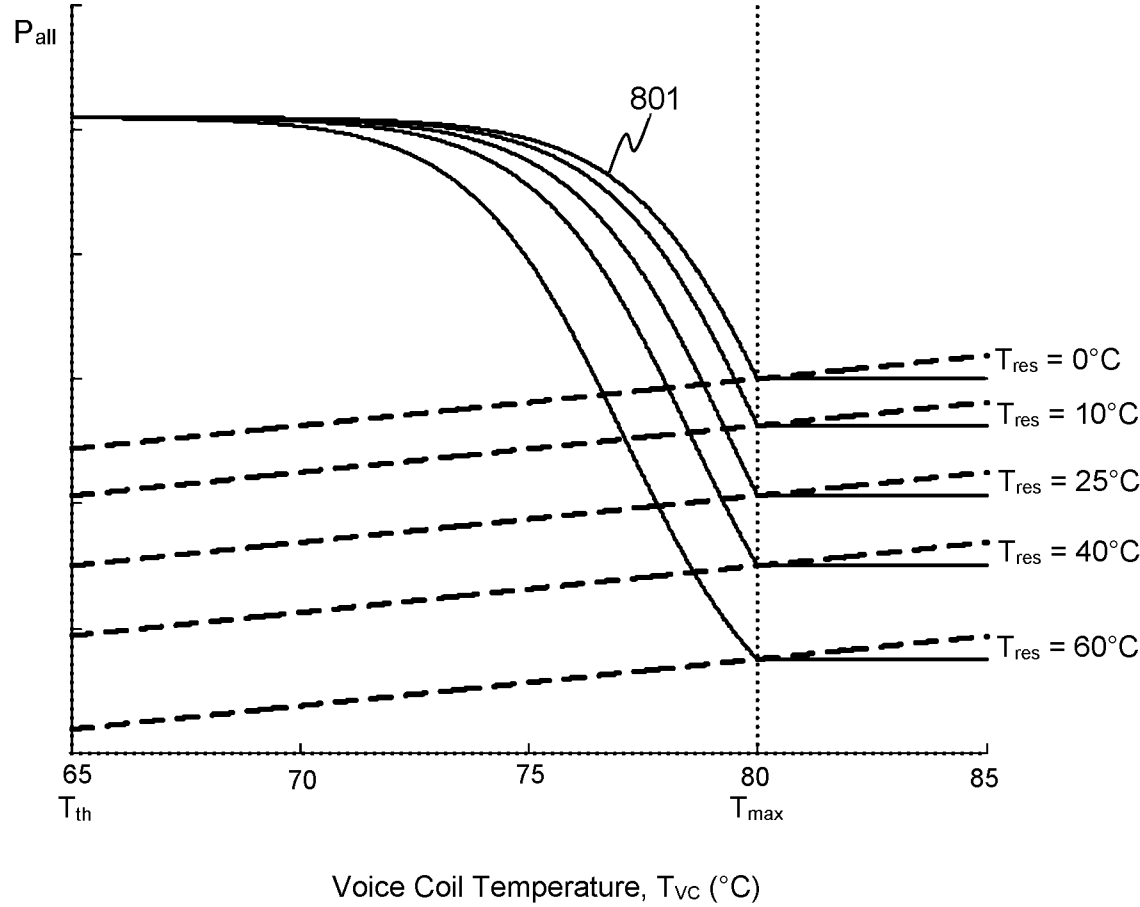


Figure 8

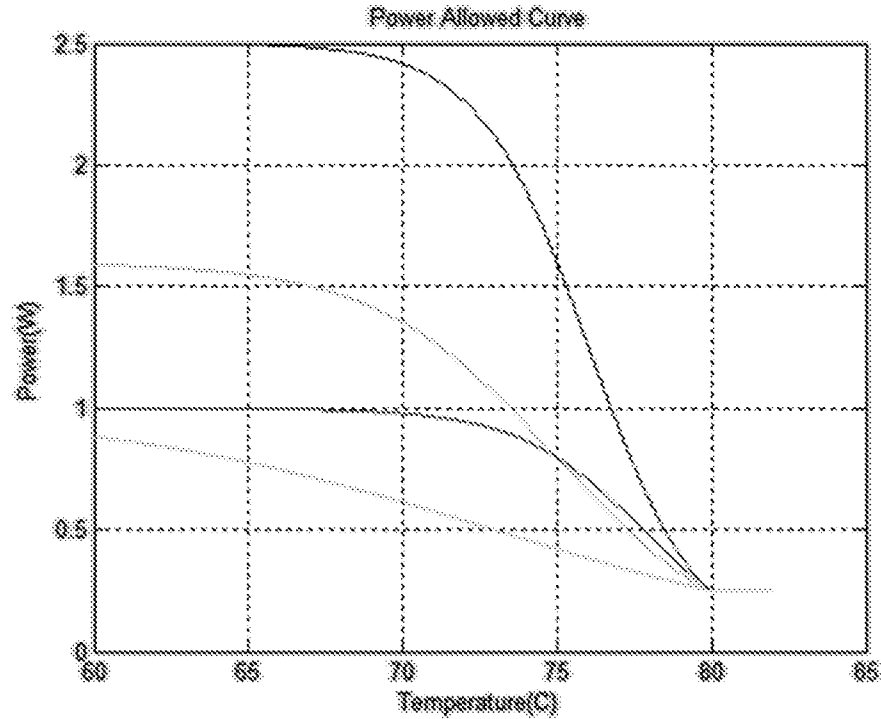


Figure 9

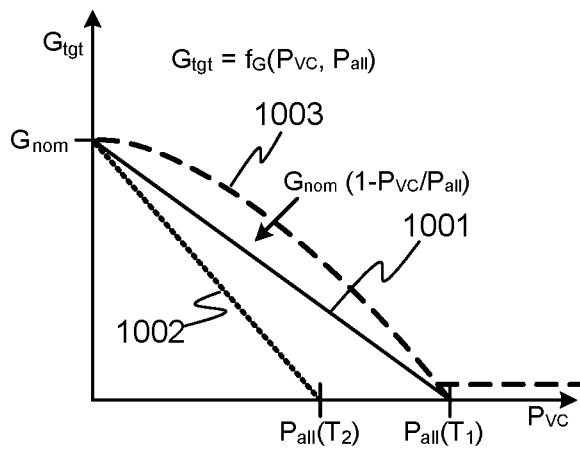


Fig. 10(a)

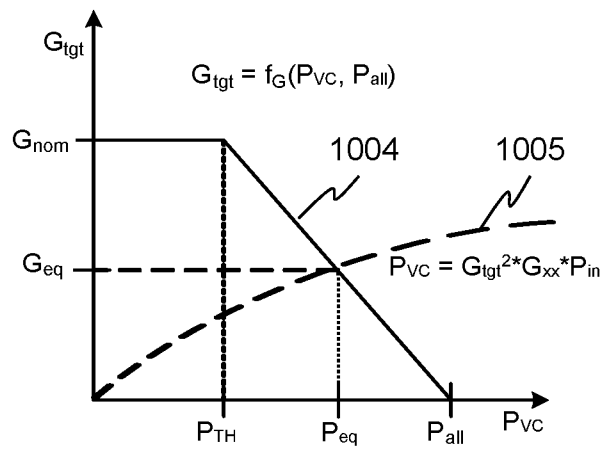


Fig. 10(b)

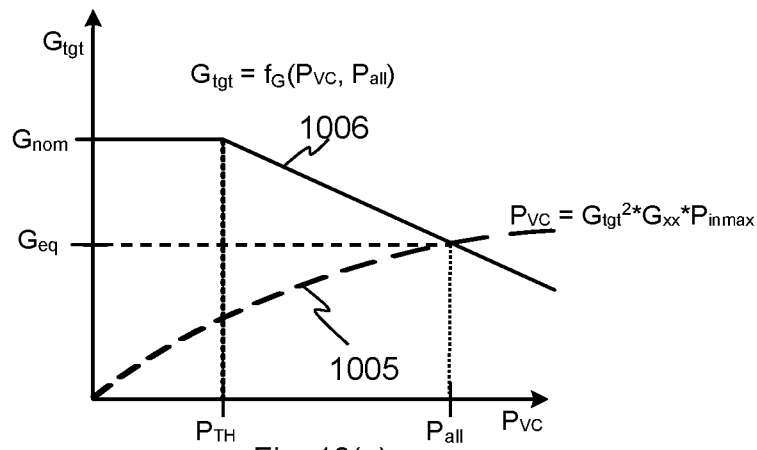


Fig. 10(c)

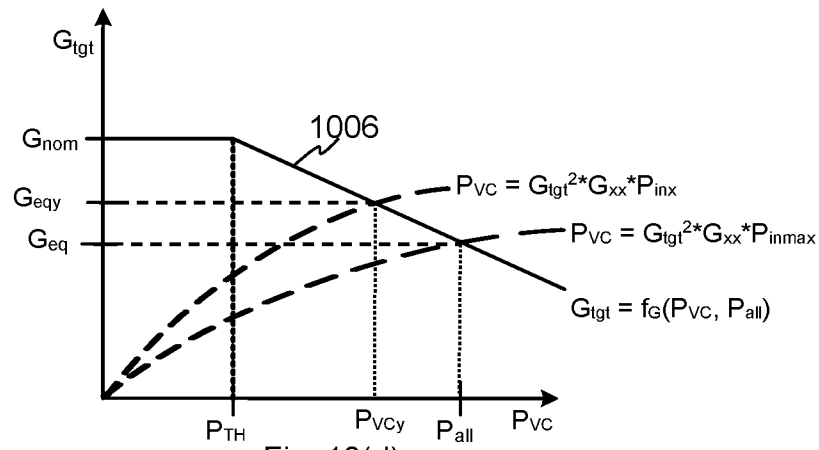


Fig. 10(d)

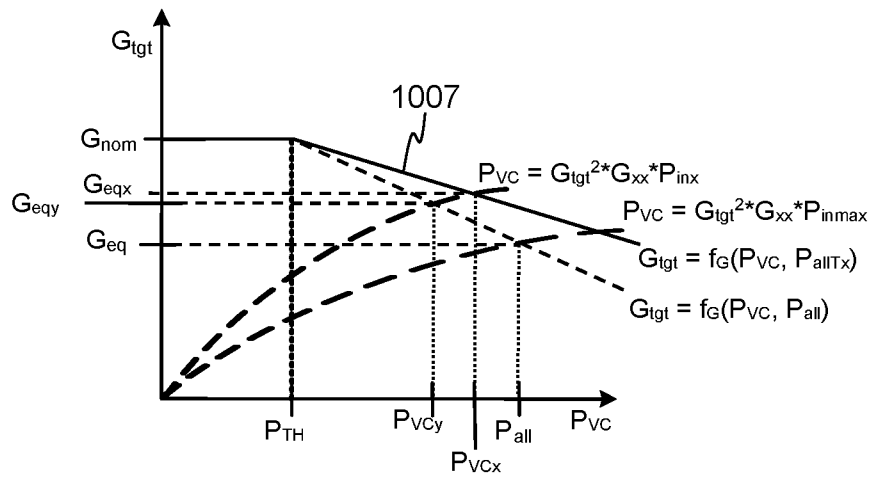


Fig. 10(e)

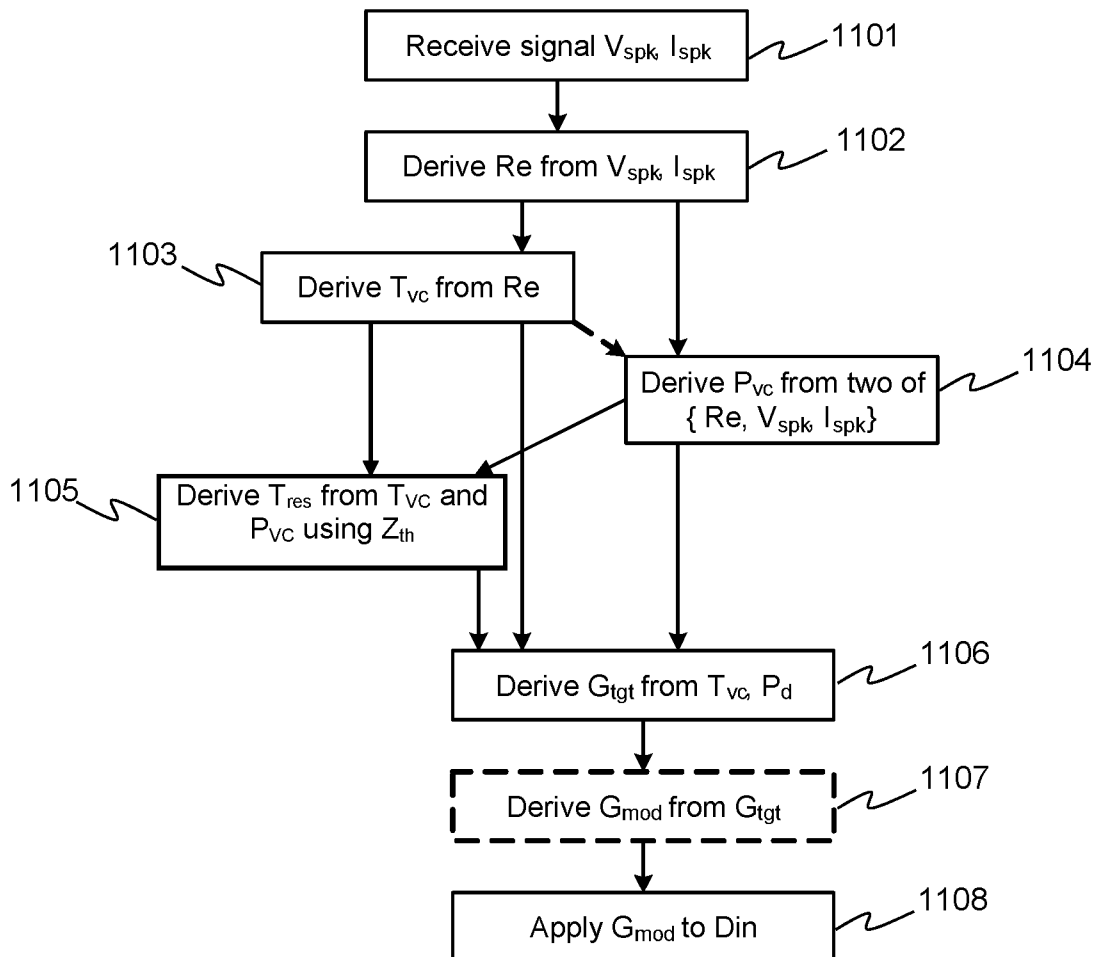


Figure 11a

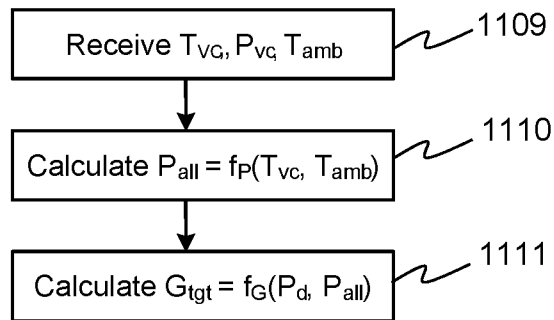


Figure 11b

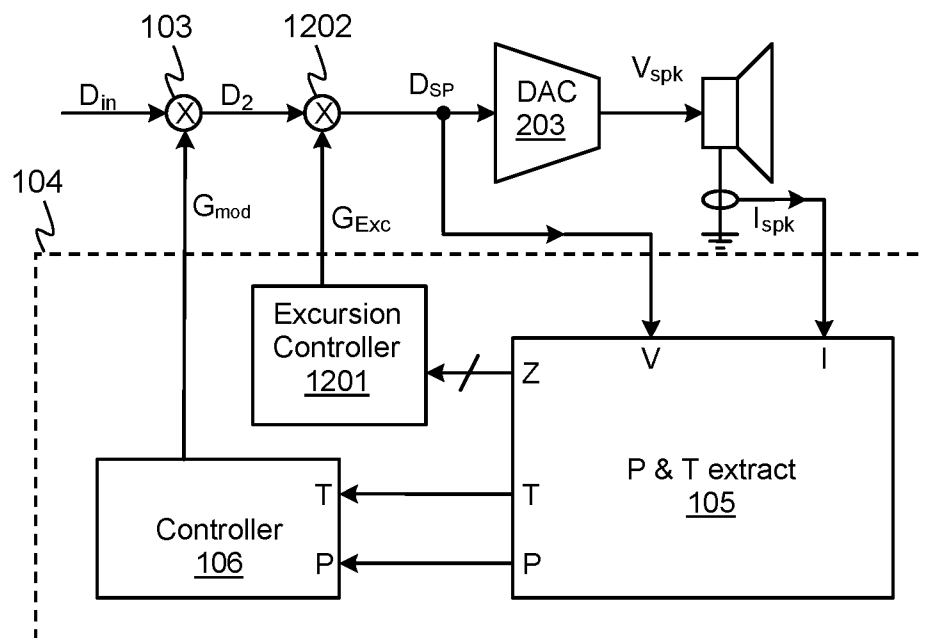


Figure 12

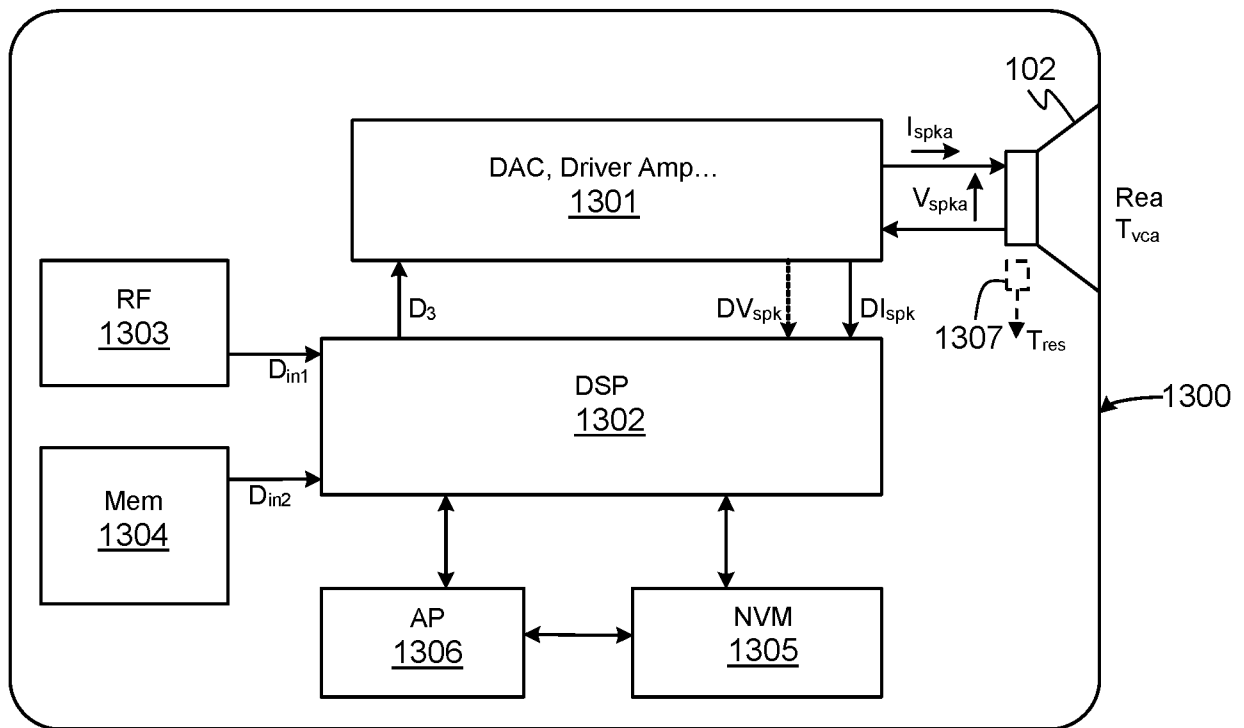


Figure 13

INTERNATIONAL SEARCH REPORT

International application No

PCT/GB2016/052927

A. CLASSIFICATION OF SUBJECT MATTER

INV. H04R29/00 H04R3/00 H03G3/30
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

H04R H03G

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	GB 2 522 449 A (WOLFSON MICROELECTRONICS PLC [GB]) 29 July 2015 (2015-07-29) the whole document	1-44
X	EP 2 800 397 A1 (SAMSUNG ELECTRONICS CO LTD [KR]) 5 November 2014 (2014-11-05) paragraphs [0020], [0034] - [0042], [0062] - [0067], [0088] - [0094]; figures 1,4,10	1-23, 34-44
X	US 2013/083928 A1 (WILLIAMS JOSEPH M [US] ET AL) 4 April 2013 (2013-04-04) paragraphs [0017], [0020] - [0027]; figures 1-6	1-21,23, 34-44
X	US 2009/257599 A1 (SAND JENSEN BJORN [DK] ET AL) 15 October 2009 (2009-10-15) paragraphs [0029] - [0036], [0050] - [0071]; figures 1,2	1-23, 34-44



Further documents are listed in the continuation of Box C.



See patent family annex.

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"O" document referring to an oral disclosure, use, exhibition or other means

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"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

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Date of the actual completion of the international search

5 January 2017

Date of mailing of the international search report

24/01/2017

Name and mailing address of the ISA/

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Authorized officer

Navarri, Massimo

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/GB2016/052927

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
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