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(54) OIL RESISTANCE TEST METHOD AND OIL RESISTANCE TEST APPARATUS

ÖLBESTÄNDIGKEITSPRÜFVERFAHREN UND ÖLBESTÄNDIGKEITSPRÜFVORRICHTUNG

PROCÉDÉ DE TEST DE RÉSISTANCE À L'HUILE ET APPAREIL DE TEST DE RÉSISTANCE À L'HUILE

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Description

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The present disclosure relates to oil resistance test methods and oil resistance test apparatuses for electronic devices.

Description of the Background Art

[0002] A fluoro-resin material or metal is often used for an exposed portion of an electronic device in order to increase oil resistance and the like. A detection switch disclosed in Japanese Utility Model Laying-Open No. 1-170929 (PTD 1), for example, includes: a tube case made of fluoro-resin and opened at one end; a cover body made of fluoro-resin for closing this case opening; and a cable connected to a detection element at the tip and having a sheath made of fluoro-resin. The cover body is welded to the cable in the vicinity of the detection element, with the cable extending through the cover body. The tube case is provided with the detection element inserted therein, and is sealed with the cover body welded to the opening.

[0003] EP2774963A1 discloses a cable coating material, coated cable, and electronic device.

[0004] US2012074968A1 discloses a method for sulfur-based corrosion testing.

[0005] US2012103655A1 discloses an oil resistant electronic device and method for manufacturing same.

SUMMARY OF THE INVENTION

[0006] In developing a variety of electronic devices such as a sensor for use in a machine tool and the like, it is important to evaluate how oil resistant these electronic devices are to a cutting oil in the actual use environment. Although an accelerated evaluation test needs to be conducted in order to efficiently evaluate the oil resistance, specific conditions under which the accelerated evaluation test should be conducted have not been clearly established.

[0007] An object of the present disclosure is to provide an oil resistance test method and an oil resistance test apparatus for determining the life of an electronic device with respect to a cutting oil.

[0008] According to a first aspect of the present invention there is provided an oil resistance test method for an electronic device as specified in claim 1.

[0009] Using the water-soluble cutting oil as described above can facilitate swelling, contraction and decomposition of the resin material, thereby reducing a test time of an accelerated test.

[0010] The at least one type of resin material may include one or more types of resin materials each having an ester group. In this case, the test temperature is pref-

erably set based on a resin material having the lowest glass transition temperature among the one or more types of resin materials each having an ester group. When such a resin material having an ester group and a low glass transition temperature is included, a low test temperature needs to be set in order to avoid rapid degradation of the resin material.

[0011] In the first aspect of the present invention, in a first alternative option determining whether or not the electronic device has been degraded includes determining whether or not an insulation resistance value of the electronic device has become equal to or less than a reference value. The degradation of the electronic device can be readily determined by the measurement of the insulation resistance in this manner. It is noted that an electronic device as used herein means, when a cable is directly connected to a body portion (that is, when a cable is directly mounted to a body portion without a connector provided on the body portion interposed therebetween), not only the body portion but the entirety including the cable directly connected to the body portion.

[0012] In the first aspect of the present invention, in a second alternative option determining whether or not the electronic device has been degraded includes measuring an electrical characteristic of the electronic device in an energized state. The degradation of the electronic device can be readily determined by the determination of whether or not the electronic device operates normally in this manner.

[0013] Preferably, the oil resistance test method further includes, when it is detected that the electronic device has been degraded, determining which one of a plurality of divided portions of the electronic device has been degraded by measuring insulation resistance of each portion of the plurality of portions.

[0014] In the first aspect of the present invention, an estimated value of the life is calculated by multiplying the total immersion time by a predetermined acceleration factor. Here, the acceleration factor is calculated, using first and second electronic devices of an identical design, by a ratio between a time until the first electronic device is degraded in an actual use environment, and a total immersion time of the second electronic device in the cutting oil until the second electronic device is degraded at a part identical to a degraded part of the first electronic device in the atmosphere of the test temperature. In this manner, in order to properly conduct an accelerated test, it is required to confirm that the same phenomenon as that in the actual use environment is reproduced in the accelerated test, and the acceleration factor is determined after this reproducibility has been confirmed.

[0015] According to a second aspect of the present invention there is provided an oil resistance test apparatus for an electronic device as specified in claim 4.

[0016] According to the configuration of the oil resistance test apparatus described above, the insulation resistance can be measured while the electronic device to be tested is simultaneously immersed in the cutting oil in

the constant temperature oven.

[0017] The foregoing and other objects, features, aspects and advantages of the present invention will become more apparent from the following detailed description of the present invention when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018]

Fig. 1 is a diagram schematically showing an overall configuration of an oil resistance test apparatus.

Fig. 2 is a diagram showing an external appearance of a proximity sensor.

Fig. 3 is a diagram showing a relationship between resin materials and settable test temperatures in table form.

Fig. 4 is a flowchart showing the procedure of an accelerated test.

Fig. 5 is a diagram illustrating a method of measuring insulation resistance of an enclosure.

Fig. 6 is a diagram illustrating a method of measuring insulation resistance of a cable between the enclosure and a connector.

Fig. 7 is a diagram illustrating a method of measuring insulation resistance of the connector.

Fig. 8 is a diagram illustrating a method of measuring insulation resistance of the cable between the connector and an insulation resistance meter.

Fig. 9 is a flowchart showing the procedure of determining an acceleration factor.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0019] Embodiments will be described below in detail with reference to the drawings. It is noted that the same or corresponding parts are designated by the same reference signs, and description thereof will not be repeated.

[General Configuration of Oil Resistance Test Apparatus]

[0020] Fig. 1 is a diagram schematically showing an overall configuration of an oil resistance test apparatus. Referring to Fig. 1, an oil resistance test apparatus 10 includes a constant temperature oven 11, a container 13 with a cover 14 for containing a cutting oil 15, an insulation resistance meter 17, and a controller 18. A front door portion of constant temperature oven 11 is not shown in Fig. 1.

[0021] Container 13 with cover 14 is installed in constant temperature oven 11. A cutting oil of Type A1 of the JIS standard K2241 is used as cutting oil 15 (the reason for which will be described later).

[0022] An electronic device to be subjected to an accelerated test is immersed in cutting oil 15. Although a proximity sensor 100 is described as an example of the

electronic device in Fig. 1, electronic devices in which oil resistance becomes an issue are not limited to proximity sensor 100. Oil resistance to an cutting oil also becomes an issue in a limit switch, a displacement sensor, and a communication device for use in a machine tool, for example.

[0023] Fig. 2 is a diagram showing an external appearance of proximity sensor 100. Referring to Fig. 2, proximity sensor 100 includes an approximately cylindrical enclosure 110 made of metal, a sensing unit assembly 120 attached to a tip end portion of approximately cylindrical enclosure 110, a clamp 150 made of resin and attached to a base end portion of enclosure 110, and a cable 132 fixed to this clamp 150 through a joint interposing member (not shown). An electronic circuit is implemented in enclosure 110. It is noted that cable 132 may be structured such that a plurality of cables 132 are coupled via a connector 160, as shown in Fig. 1 (connector 160 is not needed in the case of a single cable 132).

[0024] Sensing unit assembly 120 has a structure in which a core (not shown) and a sensing coil (not shown) are contained in a coil case made of resin (not shown). Cable 132 includes a shielding material (not shown) and a sheath 130 that cover a core 131. Sheath 130 is made of a resin material such as fluororesin. Cable 132 is fixed to clamp 150 through a joint interposing member made of resin. The joint interposing member may be welded to sheath 130 of cable 132 for the purpose of sealing. Core 131 of cable 132 is electrically connected to the electronic circuit (now shown) in enclosure 110.

[0025] In the above configuration, the coil case of sensing unit assembly 120, sheath 130 of cable 132, and clamp 150 are made of resin and exposed at the outer surface of proximity sensor 100. Thus, oil resistance of these members becomes an issue.

[0026] Unlike the present embodiment, the cable may be fixed to the enclosure of the electronic device through an O ring or rubber bush, instead of clamp 150 and the joint interposing member described above. In this case, the O ring or rubber bush is exposed at the outer surface of the electronic device. Thus, oil resistance of the O ring or rubber bush becomes an issue.

[0027] Referring again to Fig. 1, the tip of a measurement cord 16A, which is one of two measurement cords 16A and 16B extending from insulation resistance meter 17, is immersed in a water-soluble cutting oil of Type A1, and the tip of the other measurement cord 16B is connected to the core of cable 132. The insulation resistance of proximity sensor 100 is measured through water-soluble cutting oil 15.

[0028] It is noted that a portion of the end (end opposite to enclosure 110) of cable 132 that is not covered with sheath 130 must be outside of container 13 with cover 14 containing the water-soluble cutting oil, in order to avoid a short circuit between measurement cords 16A and 16B.

[0029] Controller 18 detects an internal temperature of

constant temperature oven 11 by a temperature sensor 19, and performs feedback control of an output from a heater (not shown) contained in constant temperature oven 11 such that the interior of constant temperature oven 11 is equal to a user-set test temperature. Controller 18 also determines that a failure has occurred in proximity sensor 100 when a measurement value of the insulation resistance becomes equal to or less than a reference value (for example, 50 MΩ).

[0030] Although the insulation resistance of electronic device 100 to be tested is measured while electronic device 100 is simultaneously immersed in cutting oil 15 in constant temperature oven 11 in the above, the insulation resistance may be measured by taking electronic device 100 out of constant temperature oven 11 at regular time intervals. In this case, if there is no abnormality in the insulation resistance of the electronic device, electronic device 100 is put back in constant temperature oven 11 to continue the accelerated test.

[Selection of Cutting Oil]

[0031] Although a cutting oil is diluted for use in the actual use environment, a stock solution of a cutting oil is used and an electronic device to be measured is immersed in this stock solution of the cutting oil in an accelerated test. The reason for using a stock solution is because a cutting oil that has intermittently splashed on an electronic device may be potentially dried and condensed on the surface of the electronic device in the actual use environment. Further, for the reasons discussed below, a water-soluble cutting oil termed Type A1 in the JIS standard K2241 is used for the accelerated test. Type A1 refers to those "which are composed of a water-insoluble component such as mineral oil or fatty oil and a surfactant, and which exhibit a milky-white appearance when diluted with water." It is noted that there are additional Type A2 and Type A3 water-soluble cutting oils. Type A2 refers to those "which are composed of a water-soluble component alone such as a surfactant, or composed of a water-soluble component and a water-insoluble component such as mineral oil or fatty oil, and which exhibit a translucent to transparent appearance when diluted with water." Type A3 refers to those "which are composed of a water-soluble component, and which exhibit a transparent appearance when diluted with water."

[0032] In general, according to the JIS standard K2241, cutting oils are classified into Type N1 to Type N4 which are four types of water-insoluble cutting oils, and Type A1 to Type A3 which are three types of water-soluble cutting oils. Here, a cutting oil that causes quick progress of degradation of a resin member is selected for use in an accelerated test. Specifically, a cutting oil that facilitates swelling, contraction and decomposition of a resin member is selected. The degree of swelling and contraction is evaluated by a rate of weight change and/or a rate of dimensional change.

[0033] First, in terms of decomposition, the water-in-

soluble cutting oils (Types N1 to N4) are excluded because they do not cause decomposition. Next, among the water-soluble cutting oils (Types A1 to A3), the cutting oil of Type A3 is excluded because it does not contain a mineral oil which is a major contributing factor to swelling and contraction. Further, when the cutting oil of Type A1 and the cutting oil of Type A2 are compared with each other, Type A1 has a higher content of mineral oil and thus causes a higher degree of swelling and contraction. It is thus desirable to use the cutting oil of Type A1 as a cutting oil for an accelerated test. Moreover, a ratio of components in the cutting oil may be adjusted so as to maximize the effect on the resin member.

[Selection of Set Temperature (Test Temperature) of Constant Temperature Oven]

[0034] Since an electronic device is usually used in the vicinity of room temperature in the actual use environment, a test temperature for an accelerated test is set to a temperature higher than the use temperature. If a use temperature of an electronic device in the actual use environment is higher than room temperature (for example, in the vicinity of 40°C), an accelerated test temperature is again set to a temperature higher than the actual use temperature. However, it must be borne in mind that the actual accelerated test temperature has a limiting temperature depending on the resin material exposed at the outer surface of an electronic device to be tested. For example, when a particular resin material is rapidly degraded at a high temperature (for example, when the temperature of a resin material having an ester group exceeds the glass transition point), there will be a significant difference from the actual use environment. When such a material is used, therefore, a low accelerated test temperature needs to be set. Specific examples will be cited and described below.

[0035] Fig. 3 is a diagram showing a relationship between resin materials and settable test temperatures in table form. Referring to Fig. 3, when a resin material having an ester group is provided on the outer surface of an electronic device, the test temperature is set to a lower temperature than when the resin material having an ester group is not provided. This is because an ester group undergoes hydrolysis in a water-soluble cutting oil of Type A1. Specifically, in the example of Fig. 3, PBT (polybutylene terephthalate), EP (epoxy resin), and PMMA (polymethyl methacrylate) include an ester group. When these materials are exposed at the outer surface, therefore, the test temperature needs to be set to a lower temperature than when they are not exposed.

[0036] Further, when different resin materials are exposed at the outer surface depending on the portion of the electronic device, and a plurality of types of resin materials each having an ester group are exposed at the outer surface of the electronic device, the test temperature is set based on a resin material having the lowest glass transition temperature among those materials. In

the example of Fig. 3, when PBT or EP is used, the test temperature is set to 55°C, which is a value substantially equivalent to the glass transition temperatures of these materials. When only PMMA is used as a material having an ester group, the test temperature is set to 70°C in consideration of the glass transition temperature of PMMA (100°C).

[Procedure of Accelerated Test]

[0037] Fig. 4 is a flowchart showing the procedure of an accelerated test. Referring to Figs. 1 and 4, the procedure of an accelerated test of oil resistance of an electronic device will be described below.

[0038] First, electronic device 100 to be tested is immersed in cutting oil 15 (step S110). Type A1 of the JIS standard K2241 is employed as cutting oil 15. Next, the temperature of constant temperature oven 11 (test temperature) is set depending on the type of a resin material provided on the outer surface of electronic device 100 (step S120). Controller 18 controls an output from the contained heater such that the internal temperature of constant temperature oven 11 becomes equal to the set test temperature, based on a detection value from temperature sensor 19.

[0039] Next, heating of electronic device 100 by constant temperature oven 11 is started by placing container 13 with cover 14 containing cutting oil 15 in constant temperature oven 11 together with electronic device 100 (step S130). Further, in the case of the apparatus configuration of Fig. 1, the insulation resistance of electronic device 100 is measured while an accelerated test of oil resistance of electronic device 100 is conducted in an atmosphere of the test temperature (step S140). In contrast to this, the insulation resistance of electronic device 100 may be measured by taking electronic device 100 out of constant temperature oven 11 at regular time intervals.

[0040] When the insulation resistance is equal to or less than the reference value (for example, 50 MΩ) as a result of the insulation resistance measurement described above (YES in step S150), it is determined that a failure or degradation has occurred in electronic device 100. Here, instead of measuring the insulation resistance, it may be determined whether or not electronic device 100 operates normally when actually energized.

[0041] Here, whether or not electronic device 100 operates normally can be determined based on the following criteria. When the electronic device is a sensor, for example, whether or not the electronic device operates normally is determined based on whether or not a detection value varies. When the electronic device is a switch, whether or not the electronic device operates normally is determined based on whether or not a contact operates properly in response to an input. When the electronic device is a communication device such as an RFID (Radio Frequency Identifier), whether or not the electronic device operates normally is determined based on wheth-

er or not the communication device is communicating properly. When the electronic device includes an IO (Input/Output) terminal, whether or not the IO terminal operates normally is determined based on whether or not an internal circuit functions normally. In this manner, the degradation of electronic device 100 can also be determined by measuring the electrical characteristics of electronic device 100 other than the insulation resistance.

[0042] Next, when the degradation of electronic device 100 is detected, a degraded portion identified (step S160). Specifically, it is determined which portion has been degraded by measurement of insulation resistances of a plurality of portions.

[0043] Figs. 5 to 8 are diagrams illustrating methods of measuring insulation resistances of enclosure 110, cable 132 between enclosure 110 and connector 160, connector 160, and cable 132 between connector 160 and insulation resistance meter 17, respectively. As shown in Figs. 5 to 8, electronic device 100 includes enclosure (sensor body) 110 and cable 132 fixed to enclosure 110, where cable 132 has two parts which are connected via connector 160.

[0044] Referring to Fig. 5, when measuring the insulation resistance of only enclosure (sensor body) 110, only enclosure (sensor body) 110 is immersed in water 21 contained in a container 20. In this state, the tip of measurement cord 16A of insulation resistance meter 17 is immersed in the water, and the tip of measurement cord 16B is connected to the core of cable 132. The insulation resistance of only enclosure (sensor body) 110 can thereby be measured through the water. It is noted that a conductive liquid may be used instead of the water in the insulation resistance measurement described above.

[0045] When the cable is not directly connected to the enclosure of the electronic device (that is, when the cable is not included in the electronic device), the enclosure of the electronic device is provided with a connector to which the cable can be connected. By attaching a connector pairing with this connector provided on the enclosure to the tip of measurement cord 16B extending from insulation resistance meter 17, the enclosure and measurement cord 16B can be electrically connected to each other to measure the insulation resistance of only the enclosure. Alternatively, the enclosure and measurement cord 16B may be electrically connected to each other through a cable attached at one end to a connector pairing with the connector provided on the enclosure.

[0046] Referring to Fig. 6, when measuring the insulation resistance of cable 132 between enclosure 110 and connector 160, the appropriate portion is immersed in the water. In this state, the tip of measurement cord 16A of insulation resistance meter 17 is immersed in the water, and the tip of measurement cord 16B is connected to the core of cable 132. It is noted that when the cable is not directly connected to the enclosure of the electronic device (that is, when the cable is not included in the electronic device), the measurement step of Fig. 6 is skipped.

[0047] Referring to Fig. 7, when measuring the insula-

tion resistance of connector 160, the tip of measurement cord 16A of insulation resistance meter 17 is brought into contact with connector 160 while being immersed in the water. The tip of measurement cord 16B is connected to the core of cable 132. It is noted that when the electronic device is not provided with connector 160, the measurement step of Fig. 7 is skipped.

[0048] Referring to Fig. 8, when measuring the insulation resistance of cable 132 between connector 160 and insulation resistance meter 17, the appropriate portion is immersed in the water. In this state, the tip of measurement cord 16A of insulation resistance meter 17 is immersed in the water, and the tip of measurement cord 16B is connected to the core of cable 132. It is noted that when the cable is not directly connected to the enclosure of the electronic device (that is, when the cable is not included in the electronic device), the measurement step of Fig. 8 is skipped.

[0049] Referring again to Fig. 4, when the degradation of electronic device 100 is detected, the life of the oil resistance of electronic device 100 in the actual use environment is estimated based on a total value of immersion time of electronic device 100 in cutting oil 15 until that point in time (step S170). Specifically, an estimated value of the life of electronic device 100 can be calculated by multiplying the total value of immersion time by a predetermined acceleration factor. The procedure of determining the acceleration factor is described next.

[Procedure of Determining Acceleration Factor]

[0050] Fig. 9 is a flowchart showing the procedure of determining the acceleration factor. A plurality of electronic devices (first to third electronic devices hereinafter) of the same design are used in determining the acceleration factor.

[0051] First, in the actual use environment, a degradation time (for example, an amount of time until the insulation resistance becomes equal to or less than the reference value) and a degraded portion of the first electronic device are detected (step S210). The methods described with reference to Figs. 5 to 8 are used to detect the degraded portion.

[0052] Next, a degradation time and a degraded portion of the second electronic device are detected by an accelerated test (atmosphere of higher temperature than in the actual use environment, immersion in a cutting oil of Type A1) (step S220). The same method as that in step S210 is used to detect the degradation time and degraded portion.

[0053] Next, it is determined whether or not the degraded portion is the same between in the actual use environment and in the accelerated test (step S230). When the degraded portion differs between them (NO in step S230), the test temperature for the accelerated test is changed to a lower temperature (step S240), and the accelerated test (step S220 described above) is conducted again using the third electronic device.

[0054] When the degraded portion is the same between in the actual use environment and in the accelerated test, on the other hand, an acceleration factor (L1/L2) is determined from an elapsed time (L1) before the degradation of electronic device 100 in the actual use environment and a total immersion time (L2) in the cutting oil in the accelerated test (step S250). In this manner, in order to properly conduct the accelerated test, it is required to confirm that the same phenomenon as that in the actual use environment is reproduced in the accelerated test, and the acceleration factor (L1/L2) is determined after this reproducibility has been confirmed.

[Advantageous Effects]

[0055] According to the above embodiment, the cutting oil of Type A1 of the JIS standard K2241 is used in the accelerated test, thus allowing the accelerated test to be conducted efficiently. Further, the test temperature for the accelerated test is set depending on the resin material used for the electronic device to be tested, so that the same phenomenon as that in the actual use environment can be reproduced in the accelerated test, thus allowing the acceleration factor to be set appropriately.

[0056] Although the embodiments the present invention have been described, it should be understood that the embodiments disclosed herein are illustrative and non-restrictive in every respect. The scope of the present invention is defined by the terms of the claims, and is intended to include any modifications within the scope of the claims.

Claims

1. An oil resistance test method for an electronic device (100), with at least one type of resin material provided on at least a portion of an outer surface of the electronic device (100), the oil resistance test method comprising:

setting a test temperature;
immersing the electronic device (100) in a water-soluble cutting oil (15) in an atmosphere of the test temperature, the cutting oil (15) containing a mineral oil and a surfactant and exhibiting a milky-white appearance when diluted with water; and

determining, based on an electrical characteristic of the electronic device (100), whether or not the electronic device (100) has been degraded by the cutting oil (15), wherein determining whether or not the electronic device (100) has been degraded includes:

determining whether or not an insulation resistance value of the electronic device (100) has become equal to or less than a refer-

ence value, or
measuring an electrical characteristic of the
electronic device (100) in an energized
state;

characterized in that the method further comprises:

estimating, based on a total immersion time
of the electronic device (100) in the cutting
oil (15) until degradation of the electronic
device (100) is detected, a life of the elec-
tronic device (100) with respect to oil resist-
ance,

wherein an estimated value of the life is cal-
culated by multiplying the total immersion
time by a predetermined acceleration fac-
tor, and

wherein the acceleration factor is calculat-
ed, using first and second electronic devic-
es (100) of an identical design, by a ratio
between a time until the first electronic de-
vice is degraded in an actual use environ-
ment, and a total immersion time of the sec-
ond electronic device in the cutting oil (15)
until the second electronic device is degrad-
ed at a part identical to a degraded part of
the first electronic device in the atmosphere
of the test temperature.

2. The oil resistance test method according to claim 1,
wherein

the at least one type of resin material includes
one or more types of resin materials each having
an ester group, and

the test temperature is set based on a resin ma-
terial having the lowest glass transition temper-
ature among the one or more types of resin ma-
terials each having an ester group.

3. The oil resistance test method according to claim 1
or 2, further comprising, when it is detected that the
electronic device (100) has been degraded, deter-
mining which one of a plurality of divided portions of
the electronic device (100) has been degraded by
measuring insulation resistance of each portion of
the plurality of portions.

4. An oil resistance test apparatus (10) for an electronic
device (100), comprising:

a constant temperature oven (11);

a container (13) provided in the constant tem-
perature oven (11), for containing a water-solu-
ble cutting oil (15) in which the electronic device
(100) is to be immersed;

an insulation resistance meter (17) for measur-

ing insulation resistance of the electronic device
(100) through the water-soluble cutting oil (15);
and

a controller (18) for controlling a temperature of
the constant temperature oven (11) to be con-
stant,

wherein the controller (18) is configured to de-
termine whether or not the insulation resistance
of the electronic device (100) has become equal
to or less than a reference value,

wherein at least one type of resin material is pro-
vided on at least a portion of an outer surface of
the electronic device (100),

wherein the water-soluble cutting oil (15) con-
tains a mineral oil and a surfactant and exhibits
a milky-white appearance when diluted with wa-
ter,

characterised in that

the controller (18) is configured to estimate a life
of the electronic device (100) with respect to oil
resistance, based on a total immersion time of
the electronic device (100) in the water-soluble
cutting oil (15) until the insulation resistance of
the electronic device (100) becomes equal to or
less than the reference value,

wherein the controller (18) is configured to cal-
culate an estimated value of the life by multiply-
ing the total immersion time by a predetermined
acceleration factor,

wherein the acceleration factor is equal to a val-
ue of a ratio between a time until it is determined
that a first electronic device (100) has been de-
graded in an actual use environment based on
insulation resistance of the first electronic device
becoming equal to or less than the reference
value, and a total immersion time of a second
electronic device (100) in the cutting oil (15) until
it is determined that the second electronic device
has been degraded at a part identical to a de-
graded part of the first electronic device in an
atmosphere of the test temperature, and
wherein the first and second electronic devices
(100) are electronic devices of an identical de-
sign.

5. The oil resistance test apparatus (10) for an elec-
tronic device (100) according to claim 4, wherein

the at least one type of resin material includes
one or more types of resin materials each having
an ester group, and

the controller (18) is configured, during a test of
oil resistance of the electronic device (100), to
control the temperature of the constant temper-
ature oven (11) to be equal to a test temperature
determined based on a resin material having the
lowest glass transition temperature among the
one or more types of resin materials each having

an ester group.

Patentansprüche

1. Ölbeständigkeitsprüfverfahren für eine elektronische Vorrichtung (100) mit zumindest einem Typ von Harzmaterial, das auf zumindest einem Abschnitt einer Außenoberfläche der elektronischen Vorrichtung (100) bereitgestellt ist, wobei das Ölbeständigkeitsprüfverfahren Folgendes umfasst:

das Einstellen einer Prüftemperatur;
 das Eintauchen der elektronischen Vorrichtung (100) in ein wasserlösliches Schneidöl (15) in einer Umgebung der Prüftemperatur, wobei das Schneidöl (15) ein Mineralöl und ein Tensid enthält und ein milchig-weißes Erscheinungsbild aufweist, wenn es mit Wasser verdünnt wird; und
 das Ermitteln auf Grundlage einer elektrischen Eigenschaft der elektronischen Vorrichtung (100), ob die elektronische Vorrichtung (100) durch das Schneidöl (15) beeinträchtigt wurde, wobei das Ermitteln, ob die elektronische Vorrichtung (100) beeinträchtigt wurde, Folgendes umfasst:

das Ermitteln, ob ein Isolationswiderstandswert der elektronischen Vorrichtung (100) kleiner oder gleich einem Referenzwert geworden ist, oder
 das Messen einer elektrischen Eigenschaft der elektronischen Vorrichtung (100) in einem mit Energie versorgten Zustand;
dadurch gekennzeichnet, dass das Verfahren ferner Folgendes umfasst:

das Schätzen auf Grundlage einer Gesamteintauchdauer der elektronischen Vorrichtung (100) in dem Schneidöl (15) bis zur Detektion der Beeinträchtigung der elektronischen Vorrichtung (100) einer Lebensdauer der elektronischen Vorrichtung (100) in Bezug auf die Ölbeständigkeit,
 wobei ein Schätzwert der Lebensdauer durch Multiplizieren der Gesamteintauchdauer mit einem vorbestimmten Beschleunigungsfaktor berechnet wird, und
 wobei der Beschleunigungsfaktor wie folgt berechnet wird: unter Verwendung einer ersten und einer zweiten elektronischen Vorrichtung (100) mit identischem Schaltungsentwurf anhand eines Verhältnisses zwischen einer Zeit bis zur Beeinträchtigung der

ersten elektronischen Vorrichtung in einer tatsächlichen Einsatzumgebung und einer Gesamteintauchdauer der zweiten elektronischen Vorrichtung in das Schneidöl (15), bis die zweite elektronische Vorrichtung an einem Teil, der mit einem beeinträchtigten Teil der ersten elektronischen Vorrichtung identisch ist, in der Umgebung der Prüftemperatur beeinträchtigt ist.

2. Ölbeständigkeitsprüfung nach Anspruch 1, wobei

der zumindest eine Typ von Harzmaterial eine oder mehrere Typen von Harzmaterialien umfasst, die jeweils eine Estergruppe aufweisen, und
 die Prüftemperatur auf Grundlage eines Harzmaterials festgelegt wird, das unter dem einen oder den mehreren Typen von Harzmaterialien, die jeweils eine Estergruppe aufweisen, die niedrigste Glasübergangstemperatur aufweist.

3. Ölbeständigkeitsprüfung nach Anspruch 1 oder 2, die ferner Folgendes umfasst:

bei Detektion der Beeinträchtigung der elektronischen Vorrichtung (100) das Ermitteln, welcher aus einer Vielzahl unterteilter Abschnitte der elektronischen Vorrichtung (100) beeinträchtigt wurde, durch Messen eines Isolationswiderstands jedes Abschnitts der Vielzahl von Abschnitten.

4. Ölbeständigkeitsprüfvorrichtung (10) für eine elektronische Vorrichtung (100), welche Folgendes umfasst:

einen Konstanttemperaturofen (11);
 einen Behälter (13), der in dem Konstanttemperaturofen (11) bereitgestellt ist, um ein wasserlösliches Schneidöl (15) zu enthalten, in das die elektronische Vorrichtung (100) einzutauchen ist;
 eine Isolationswiderstandsmessvorrichtung (17) zur Messung des Isolationswiderstands der elektronischen Vorrichtung (100) durch das wasserlösliche Schneidöl (15); und
 eine Steuerung (18), um zu steuern, dass die Temperatur des Konstanttemperaturofens (11) konstant ist,
 wobei die Steuerung (18) ausgelegt ist, um zu ermitteln, ob der Isolationswiderstand der elektronischen Vorrichtung (100) kleiner oder gleich einem Referenzwert geworden ist,
 wobei zumindest ein Typ von Harzmaterial auf zumindest einem Abschnitt einer Außenoberfläche der elektronischen Vorrichtung (100) bereitgestellt ist,
 wobei das wasserlösliche Schneidöl (15) ein Mi-

neralöl und ein Tensid umfasst und ein milchig-weißes Erscheinungsbild aufweist, wenn es mit Wasser verdünnt wird,

dadurch gekennzeichnet, dass

die Steuerung (18) ausgelegt ist, um eine Lebensdauer der elektronischen Vorrichtung (100) in Bezug auf die Ölbeständigkeit auf Grundlage einer Gesamteintauchdauer der elektronischen Vorrichtung (100) in dem wasserlöslichen Schneidöl (15), bis der Isolationswiderstand der elektronischen Vorrichtung (100) kleiner oder gleich dem Referenzwert geworden ist, zu schätzen,

wobei die Steuerung (18) ausgelegt ist, um einen Schätzwert der Lebensdauer durch Multiplizieren der Gesamteintauchdauer mit einem vorbestimmten Beschleunigungsfaktor zu berechnen,

wobei der Beschleunigungsfaktor gleich einem Wert eines Verhältnisses zwischen einer Zeit, bis zu der ermittelt wird, dass eine erste elektronische Vorrichtung (100) in einer tatsächlichen Einsatzumgebung auf der Grundlage eines Isolationswiderstands der ersten elektronischen Vorrichtung kleiner oder gleich dem Referenzwert geworden ist, und einer Gesamteintauchdauer einer zweiten elektronischen Vorrichtung (100) in das Schneidöl (15), bis ermittelt wird, dass die zweite elektronische Vorrichtung an einem Teil, der mit einem beeinträchtigten Teil der ersten elektronischen Vorrichtung identisch ist, in einer Umgebung der Prüftemperatur beeinträchtigt ist, und

wobei die erste und die zweite elektronische Vorrichtung (100) elektronische Vorrichtungen mit einem identischen Schaltungsentwurf sind.

5. Ölbeständigkeitsprüfvorrichtung (10) für eine elektronische Vorrichtung (100) nach Anspruch 4, wobei

der zumindest eine Typ von Harzmaterial einen oder mehrere Typen von Harzmaterialien umfasst, die jeweils eine Estergruppe aufweisen, und

die Steuerung (18) ausgelegt ist, um während einer Prüfung der Ölbeständigkeit der elektronischen Vorrichtung (100) die Temperatur des Konstanttemperaturofens (11) so zu steuern, dass sie gleich einer Prüftemperatur ist, die auf Grundlage eines Harzmaterials ermittelt wird, das die niedrigste Glasübergangstemperatur von dem einen oder den mehreren Typen von Harzmaterialien aufweist, die jeweils eine Estergruppe aufweisen.

Revendications

1. Procédé de test de résistance à l'huile destiné à un dispositif électronique (100), avec au moins un type de résine prévu sur au moins une partie d'une surface externe du dispositif électronique (100), le procédé de test de résistance à l'huile comprenant :

la définition d'une température de test ;

l'immersion du dispositif électronique (100) dans une huile de coupe soluble dans l'eau (15) dans une atmosphère de la température de test, l'huile de coupe (15) contenant une huile minérale et un tensioactif et présentant une apparence blanc laiteux lorsqu'elle est diluée avec l'eau ; et

la détermination, sur la base d'une caractéristique électrique du dispositif électronique (100), du fait que le dispositif électronique (100) ait été dégradé ou non par l'huile de coupe (15), dans lequel la détermination du fait que le dispositif électronique (100) ait été dégradé ou non comprend :

la détermination du fait qu'une valeur de résistance d'isolation du dispositif électronique (100) soit devenue ou non égale ou inférieure à une valeur de référence, ou la mesure d'une caractéristique électrique du dispositif électronique (100) dans un état sous tension ;

caractérisé en ce que le procédé comprend en outre :

l'estimation, sur la base d'une durée totale d'immersion du dispositif électronique (100) dans l'huile de coupe (15) jusqu'à ce que la dégradation du dispositif électronique (100) soit détectée, d'une durée de vie du dispositif électronique (100) par rapport à la résistance à l'huile,

dans lequel une valeur estimée de la durée de vie est calculée en multipliant la durée totale d'immersion par un facteur d'accélération prédéterminé, et

dans lequel le facteur d'accélération est calculé, à l'aide d'un premier et d'un second dispositifs électroniques (100) de conception identique, par un rapport entre une durée jusqu'à ce que le premier dispositif électronique soit dégradé dans un environnement d'utilisation réel et une durée totale d'immersion du second dispositif électronique dans l'huile de coupe (15) jusqu'à ce que le second dispositif électronique soit dégradé au niveau d'une partie identique à une partie dégradée du premier dispositif

- électronique dans l'atmosphère de la température de test.
2. Procédé de test de résistance à l'huile selon la revendication 1, dans lequel
- le au moins un type de résine comprend un ou plusieurs type(s) de résines qui présentent chacun un groupe ester, et
la température de test est définie sur la base d'une résine qui présente la température de transition vitreuse la plus basse parmi le ou les type(s) de résines qui présentent chacun un groupe ester.
3. Procédé de test de résistance à l'huile selon la revendication 1 ou 2, comprenant en outre, lorsqu'il est détecté que le dispositif électronique (100) a été dégradé, la détermination de l'une d'une pluralité de parties divisées du dispositif électronique (100) qui a été dégradée, en mesurant la résistance d'isolation de chaque partie de la pluralité de parties.
4. Appareil de test de résistance à l'huile (10) destiné à un dispositif électronique (100), comprenant :
- un four à température constante (11) ;
un contenant (13) prévu dans le four à température constante (11), afin de contenir une huile de coupe soluble dans l'eau (15) dans laquelle le dispositif électronique (100) doit être immergé ;
un dispositif de mesure de résistance d'isolation (17) destiné à mesurer la résistance d'isolation du dispositif électronique (100) par le biais de l'huile de coupe soluble dans l'eau (15) ; et
un contrôleur (18) destiné à contrôler une température du four à température constante (11) afin qu'elle reste constante,
dans lequel le contrôleur (18) est configuré pour déterminer si la résistance d'isolation du dispositif électronique (100) est devenue égale ou inférieure à une valeur de référence,
dans lequel au moins un type de résine est prévu sur au moins une partie d'une surface externe du dispositif électronique (100),
dans lequel l'huile de coupe soluble dans l'eau (15) contient une huile minérale et un tensioactif et présente une apparence blanc laiteux lorsqu'elle est diluée dans l'eau,
caractérisé en ce que
le contrôleur (18) est configuré pour estimer une durée de vie du dispositif électronique (100) par rapport à la résistance à l'huile, sur la base d'une durée totale d'immersion du dispositif électronique (100) dans l'huile de coupe soluble dans l'eau (15) jusqu'à ce que la résistance d'isolation du dispositif électronique (100) devienne égale
- ou inférieure à la valeur de référence,
dans lequel le contrôleur (18) est configuré pour calculer une valeur estimée de la durée de vie en multipliant la durée totale d'immersion par un facteur d'accélération prédéterminé,
dans lequel le facteur d'accélération est égal à une valeur d'un rapport entre une durée jusqu'à ce qu'il soit déterminé qu'un premier dispositif électronique (100) ait été dégradé dans un environnement d'utilisation réel sur la base d'une résistance d'isolation du premier dispositif électronique qui devient égale ou inférieure à la valeur de référence et une durée totale d'immersion d'un second dispositif électronique (100) dans l'huile de coupe (15) jusqu'à ce qu'il soit déterminé que le second dispositif électronique ait été dégradé au niveau d'une partie identique à une partie dégradée du premier dispositif électronique dans une atmosphère de la température de test, et
dans lequel le premier et le second dispositifs électroniques (100) sont des dispositifs électroniques de conception identique.
5. Appareil de test de résistance à l'huile (10) destiné à un dispositif électronique (100) selon la revendication 4, dans lequel
- le au moins un type de résine comprend un ou plusieurs type(s) de résines qui présentent chacun un groupe ester, et
le contrôleur (18) est configuré, pendant un test de résistance à l'huile du dispositif électronique (100), pour contrôler la température du four à température constante (11) afin qu'elle soit égale à une température de test déterminée sur la base d'une résine qui présente la température de transition vitreuse la plus basse parmi le ou les types de résines qui présentent chacun un groupe ester.

FIG.1

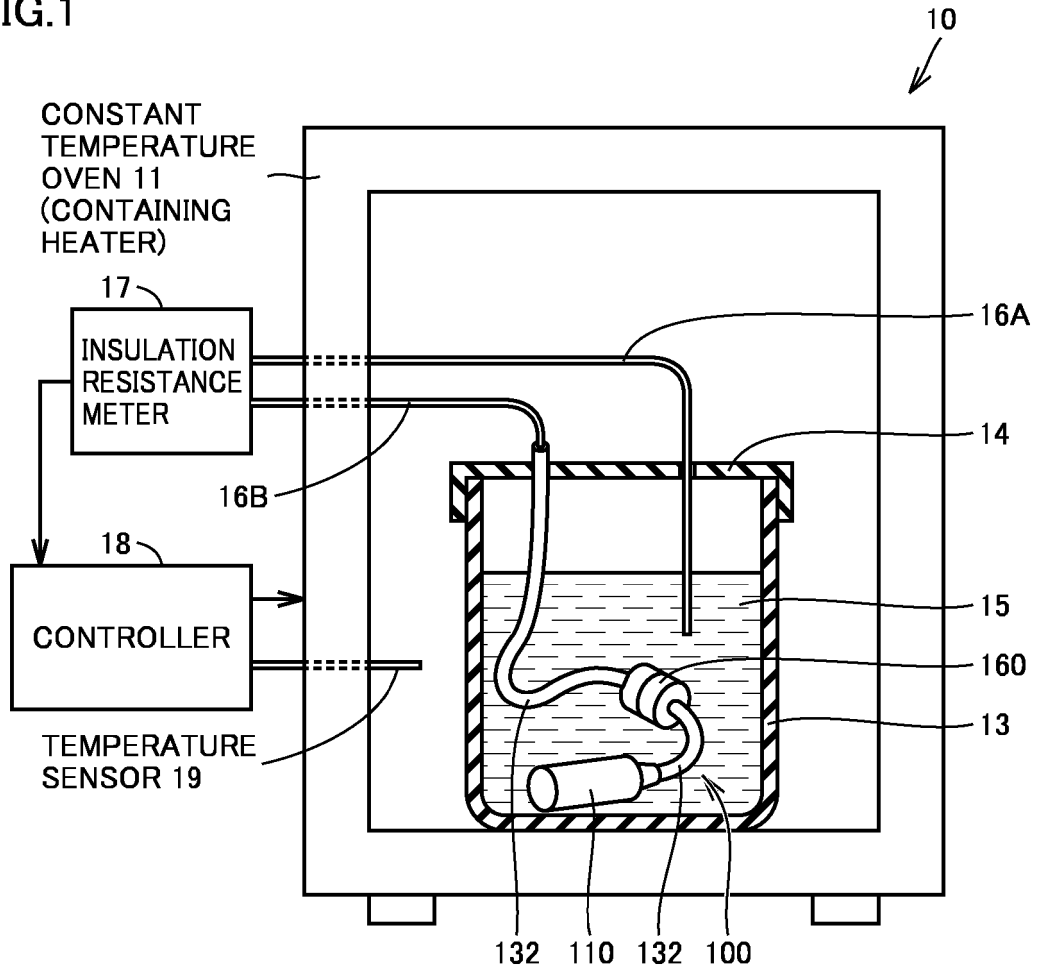


FIG.2

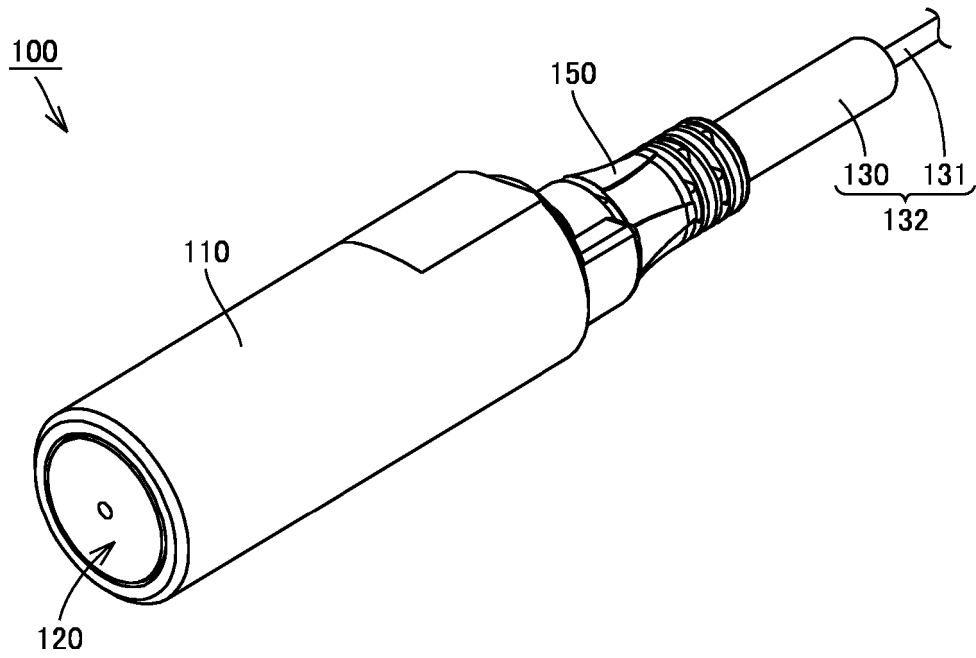


FIG.3

MATERIAL NAME	ESTER GROUP	GLASS TRANSITION POINT T _g (°C)	SETTABLE TEMPERATURE
PBT (POLYBUTYLENE TEREPHTHALATE)	PRESENT	40~60	55°C
EP (EPOXY RESIN)	PRESENT	52~100	55°C
PEI (POLYETHER IMIDE)	ABSENT	200	70°C
PMMA (POLYMETHYL METHACRYLATE)	PRESENT	100	70°C
PFA (TETRAFLUOROETHYLENE- PERFLUOROALKYL VINYL ETHER COPOLYMER)	ABSENT	75	70°C

FIG.4

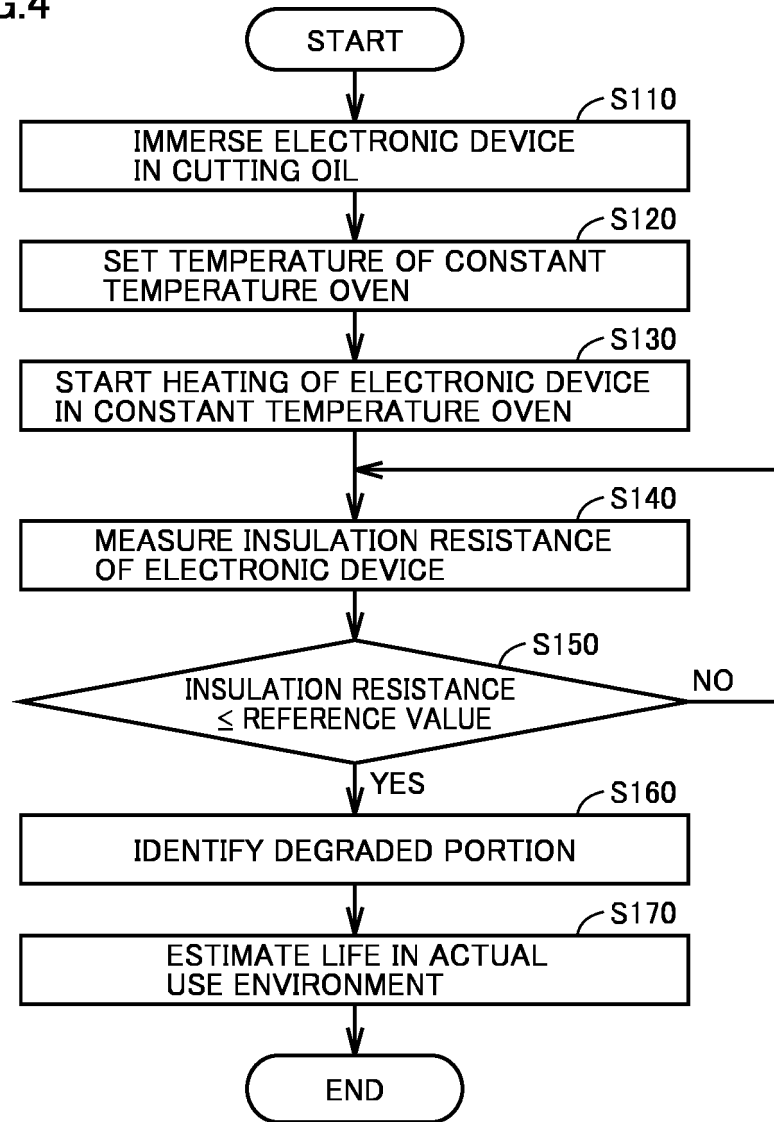


FIG.5

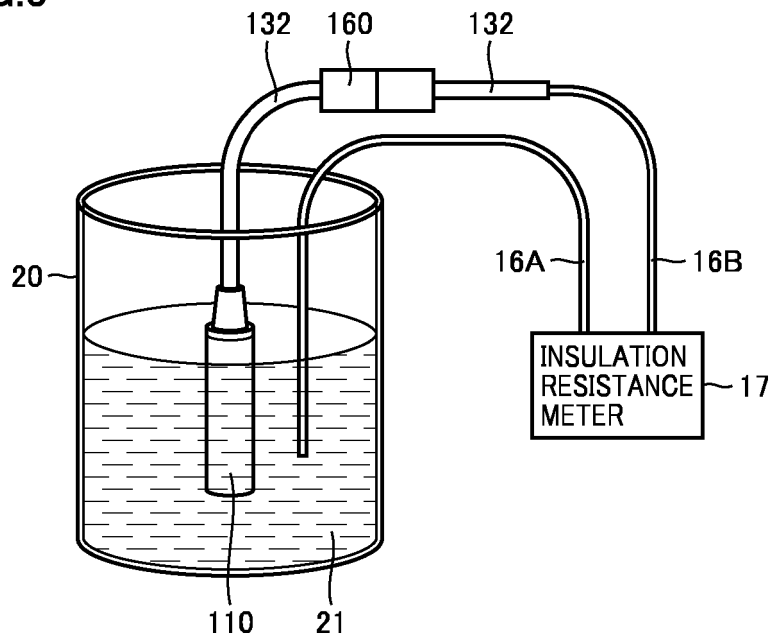


FIG.6

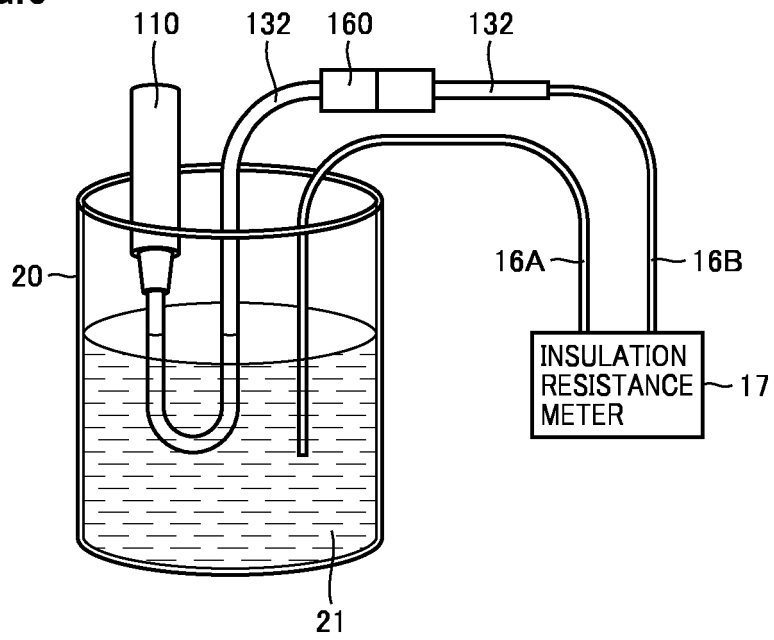


FIG. 7

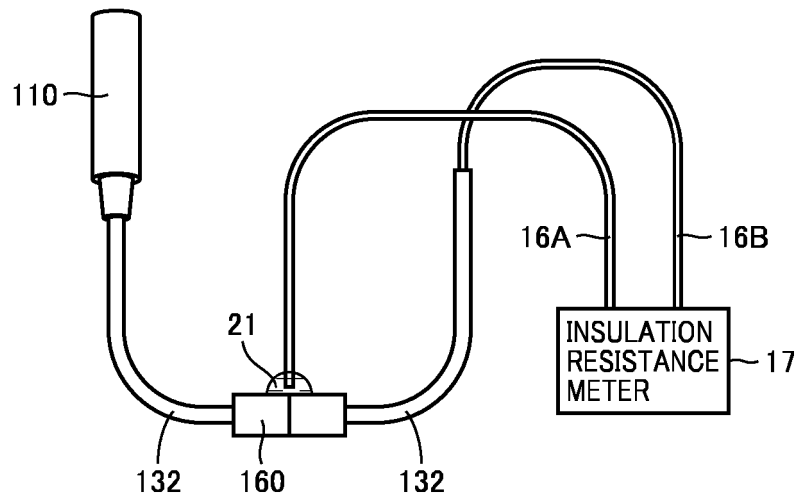


FIG.8

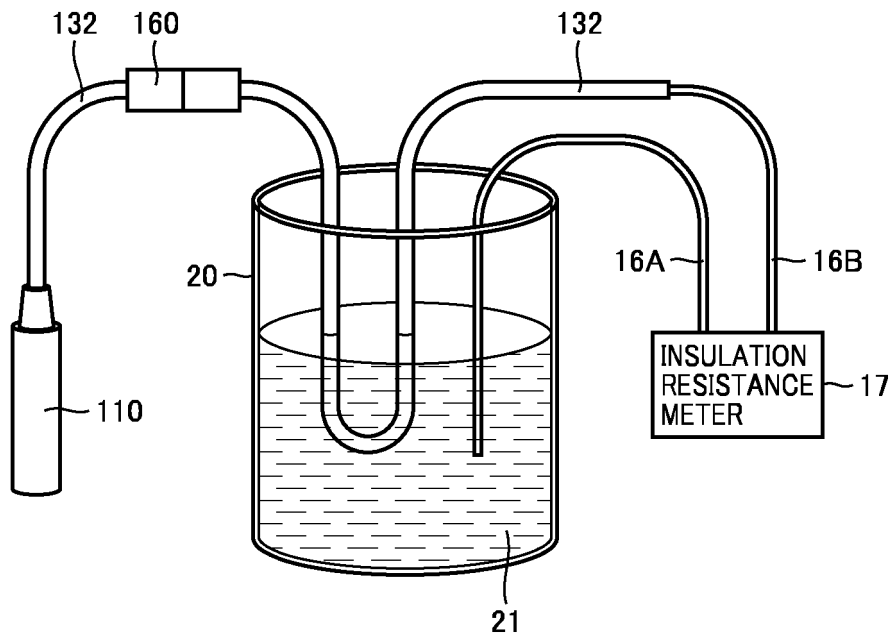
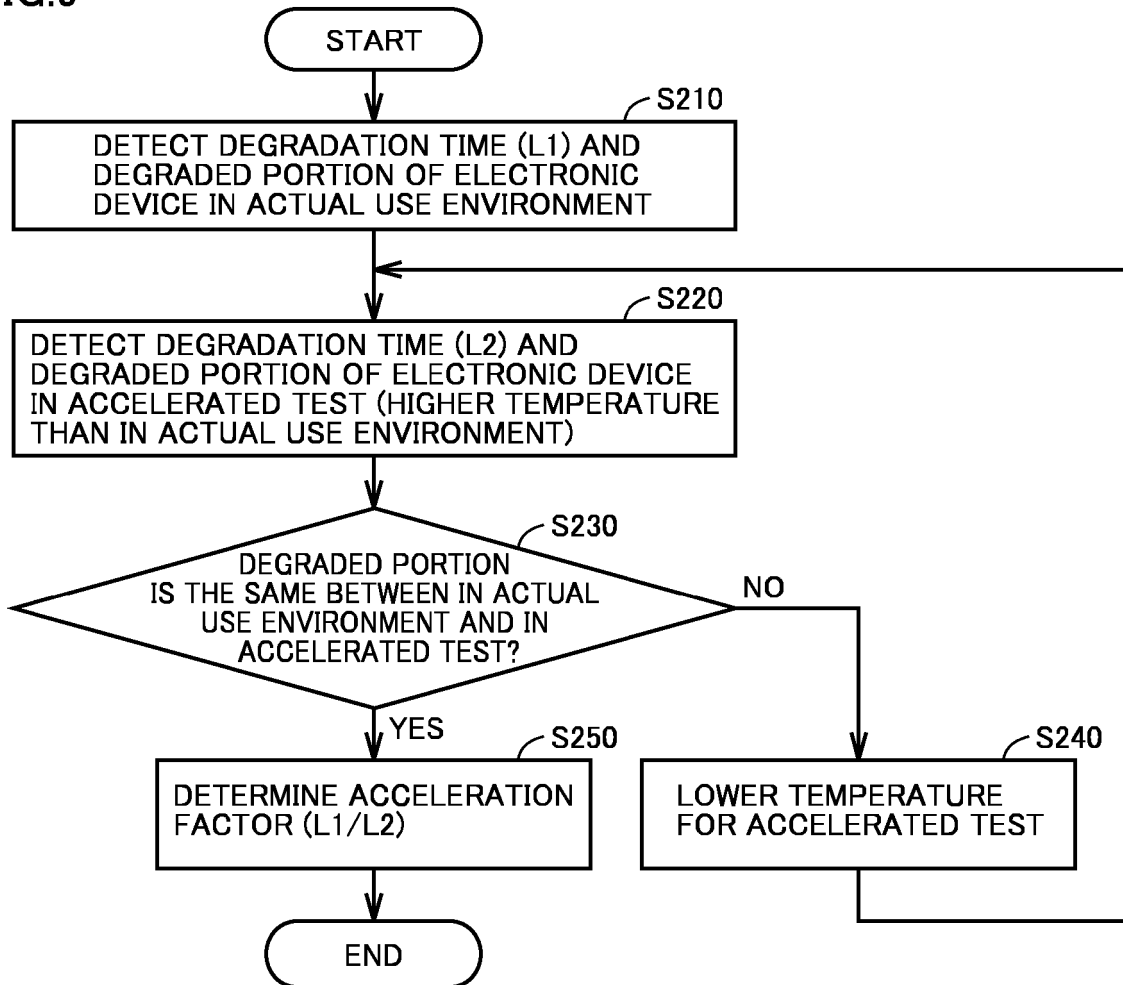


FIG.9



REFERENCES CITED IN THE DESCRIPTION

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