US008848937B2

(12) **United States Patent**
Inoue et al.

(10) **Patent No.: US 8,848,937 B2**
(45) **Date of Patent: Sep. 30, 2014**

(54) **ACTIVE NOISE CONTROL APPARATUS**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

(21) Appl. No.: **13/894,149**

(22) Filed: **May 14, 2013**

(65) **Prior Publication Data**

US 2013/0315409 A1 Nov. 28, 2013

(30) **Foreign Application Priority Data**

May 22, 2012 (JP) 2012-116321

(51) **Int. Cl.**
A61F 11/06 (2006.01)
G10K 11/16 (2006.01)
G10K 11/178 (2006.01)

(52) **U.S. Cl.**
CPC ***G10K 11/16*** (2013.01); *G10K 2210/121* (2013.01); *G10K 2210/511* (2013.01); *G10K 2210/3039* (2013.01); *G10K 2210/12821* (2013.01); *G10K 2210/503* (2013.01); ***G10K 11/1784*** (2013.01)
USPC **381/71.1**

(58) **Field of Classification Search**
CPC G10K 11/1788; G10K 11/178; G10L 21/0208; G10L 2021/02165; H04R 5/005
USPC 381/86, 94.1–94.4, 71.1–71.5, 381/71.11–71.14
See application file for complete search history.

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(57) **ABSTRACT**

An active noise control apparatus includes a first active noise controller for generating a first canceling signal for a first noise type, a second active noise controller for generating a second canceling signal for a second noise type that is different from the first noise type, a mixer for mixing the first canceling signal and the second canceling signal into a mixed canceling signal, a canceling sound output unit for outputting a canceling sound based on the mixed canceling signal, and an amplitude suppressor for suppressing the amplitude of the second canceling signal depending on the amplitude of the first canceling signal.

7 Claims, 9 Drawing Sheets

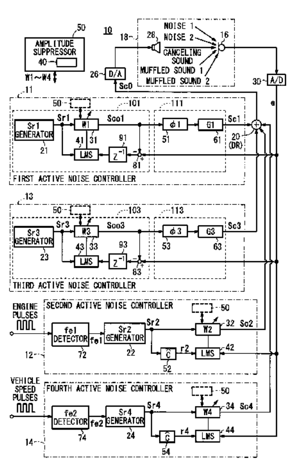
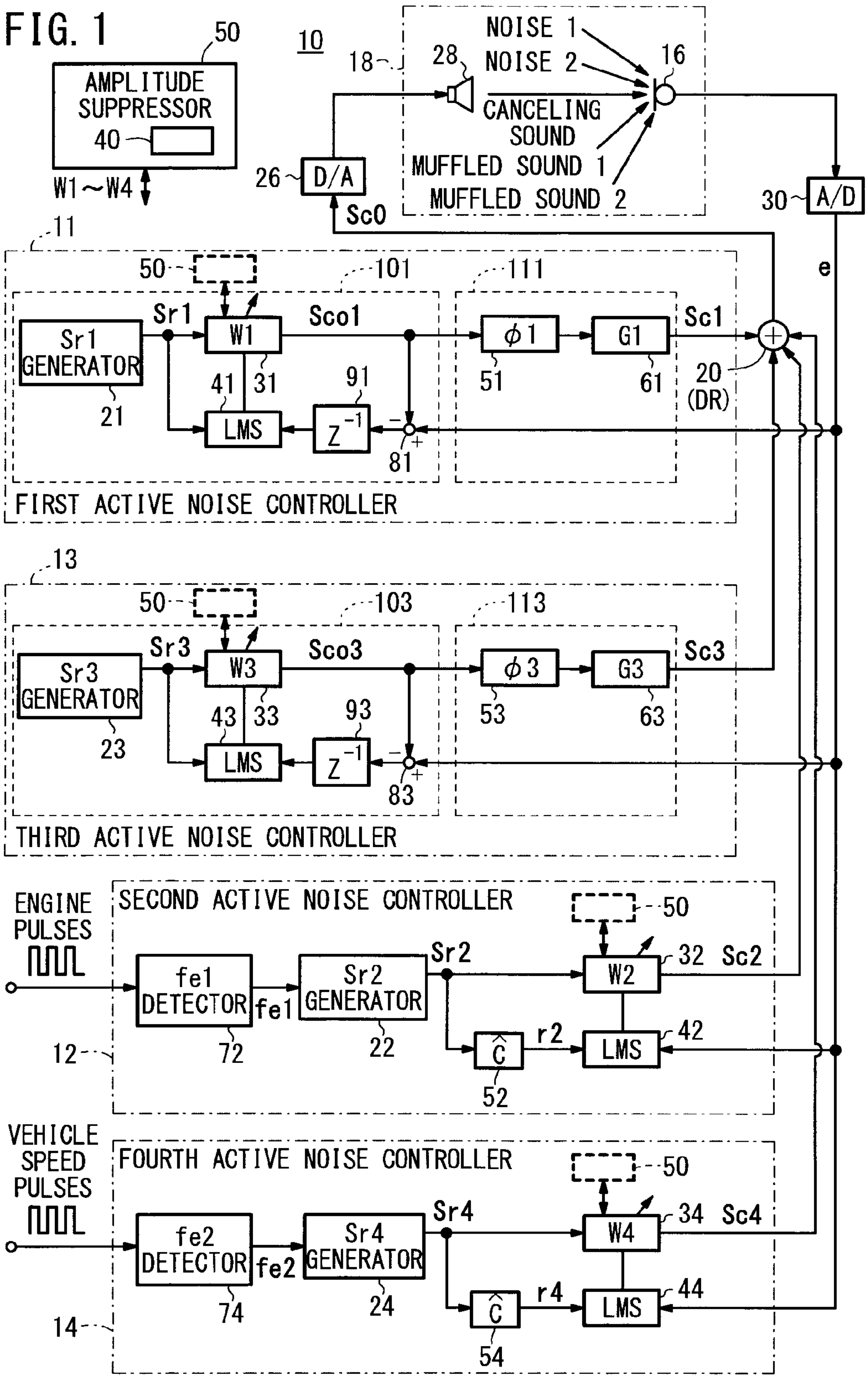


FIG. 1



50
AMPLITUDE SUPPRESSOR
40
W1～W4
10
18
28
NOISE 1
NOISE 2
CANCELING SOUND
MUFFLED SOUND 1
MUFFLED SOUND 2
16
26
D/A
Sc0
30
A/D
e
11
50
101
111
Sr1
Sr1 GENERATOR
21
W1
31
41
Sco1
LMS
Z^-1
91
81
φ1
51
G1
61
Sc1
20 (DR)
FIRST ACTIVE NOISE CONTROLLER
13
50
103
113
Sr3
Sr3 GENERATOR
23
W3
33
43
Sco3
LMS
Z^-1
93
83
φ3
53
G3
63
Sc3
THIRD ACTIVE NOISE CONTROLLER
ENGINE PULSES
SECOND ACTIVE NOISE CONTROLLER
fe1 DETECTOR
72
fe1
Sr2 GENERATOR
22
Sr2
50
W2
32
Sc2
C^
52
r2
LMS
42
12
VEHICLE SPEED PULSES
FOURTH ACTIVE NOISE CONTROLLER
fe2 DETECTOR
74
fe2
Sr4 GENERATOR
24
Sr4
50
W4
34
Sc4
C^
54
r4
LMS
44
14

FIG. 2

40

PRIORITY LEVEL	ACTIVE NOISE CONTROLLER	CANCELING SIGNAL	FILTER COEFFICIENT
1	11	Sc1 (ROAD NOISE 1)	W1
2	13	Sc3 (ROAD NOISE 2)	W3
3	12	Sc2 (MUFFLED ENGINE SOUND 1)	W2
4	14	Sc4 (MUFFLED PROPELLER SHAFT SOUND 2)	W4

FIG. 3

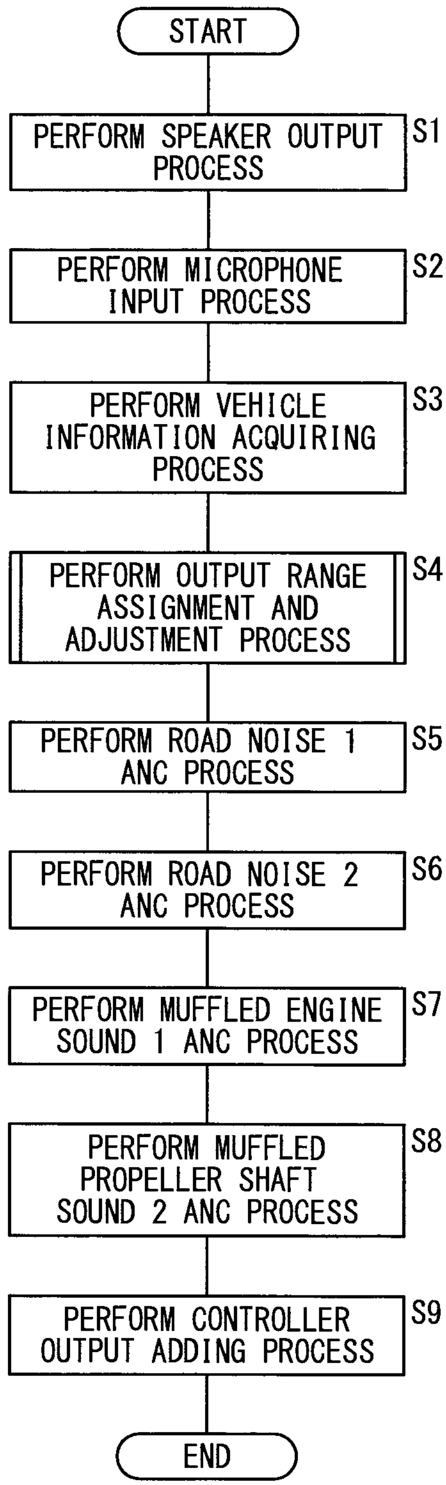

START
PERFORM SPEAKER OUTPUT PROCESS
S1
PERFORM MICROPHONE INPUT PROCESS
S2
PERFORM VEHICLE INFORMATION ACQUIRING PROCESS
S3
PERFORM OUTPUT RANGE ASSIGNMENT AND ADJUSTMENT PROCESS
S4
PERFORM ROAD NOISE 1 ANC PROCESS
S5
PERFORM ROAD NOISE 2 ANC PROCESS
S6
PERFORM MUFFLED ENGINE SOUND 1 ANC PROCESS
S7
PERFORM MUFFLED PROPELLER SHAFT SOUND 2 ANC PROCESS
S8
PERFORM CONTROLLER OUTPUT ADDING PROCESS
S9
END

FIG. 4

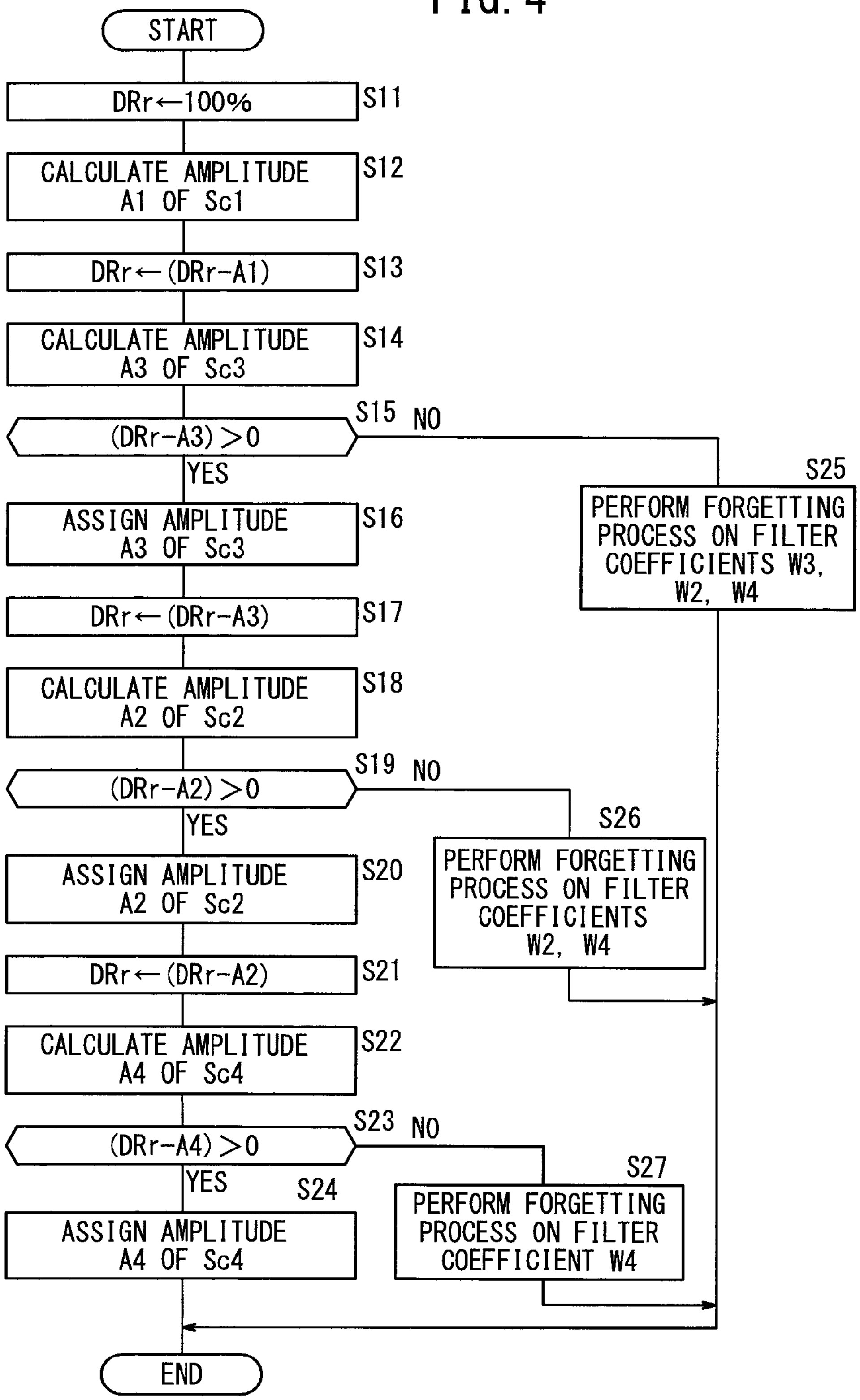

START
DRr←100%
S11
CALCULATE AMPLITUDE A1 OF Sc1
S12
DRr←(DRr−A1)
S13
CALCULATE AMPLITUDE A3 OF Sc3
S14
(DRr−A3)>0
S15
NO
YES
PERFORM FORGETTING PROCESS ON FILTER COEFFICIENTS W3, W2, W4
S25
ASSIGN AMPLITUDE A3 OF Sc3
S16
DRr←(DRr−A3)
S17
CALCULATE AMPLITUDE A2 OF Sc2
S18
(DRr−A2)>0
S19
NO
YES
PERFORM FORGETTING PROCESS ON FILTER COEFFICIENTS W2, W4
S26
ASSIGN AMPLITUDE A2 OF Sc2
S20
DRr←(DRr−A2)
S21
CALCULATE AMPLITUDE A4 OF Sc4
S22
(DRr−A4)>0
S23
NO
YES
S24
ASSIGN AMPLITUDE A4 OF Sc4
PERFORM FORGETTING PROCESS ON FILTER COEFFICIENT W4
S27
END

FIG. 5A

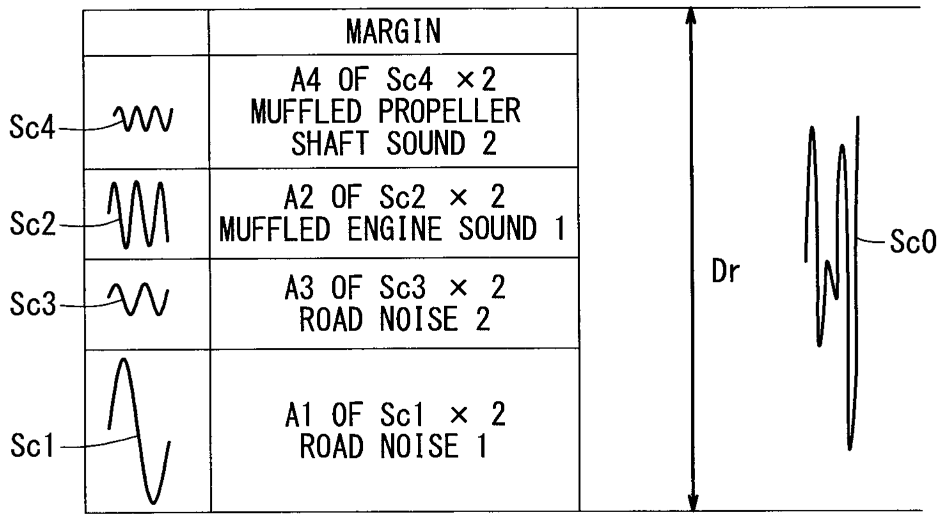

MARGIN
A4 OF Sc4 ×2 MUFFLED PROPELLER SHAFT SOUND 2
A2 OF Sc2 × 2 MUFFLED ENGINE SOUND 1
A3 OF Sc3 × 2 ROAD NOISE 2
A1 OF Sc1 × 2 ROAD NOISE 1
Sc4
Sc2
Sc3
Sc1
Dr
Sc0

FIG. 5B

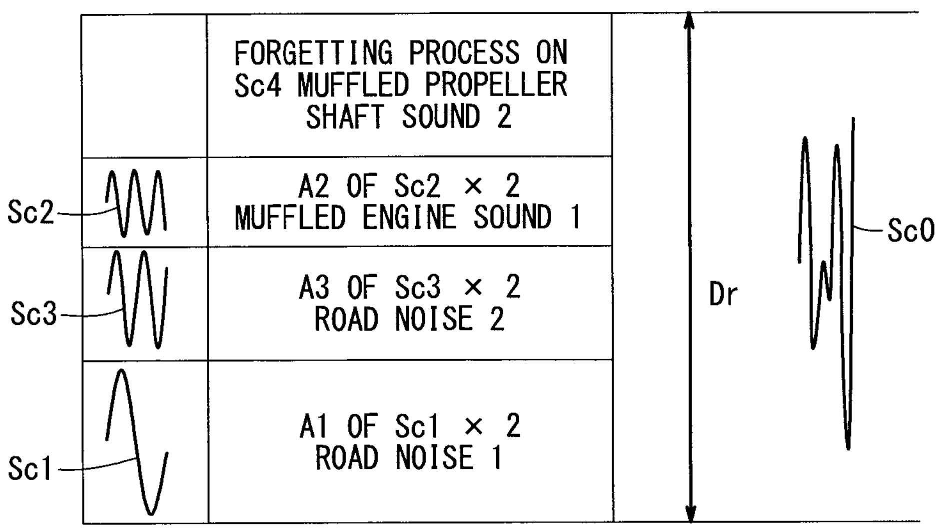

FORGETTING PROCESS ON Sc4 MUFFLED PROPELLER SHAFT SOUND 2
A2 OF Sc2 × 2 MUFFLED ENGINE SOUND 1
A3 OF Sc3 × 2 ROAD NOISE 2
A1 OF Sc1 × 2 ROAD NOISE 1
Sc2
Sc3
Sc1
Dr
Sc0

FIG. 6A

Prior Art

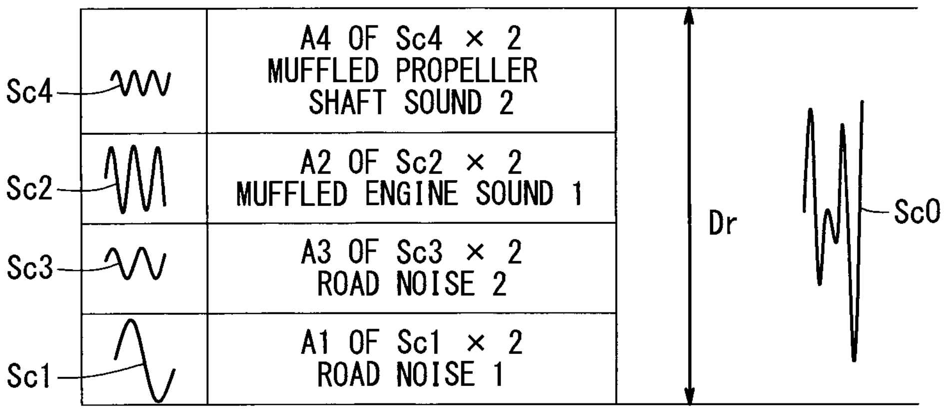


FIG. 6B

Prior Art

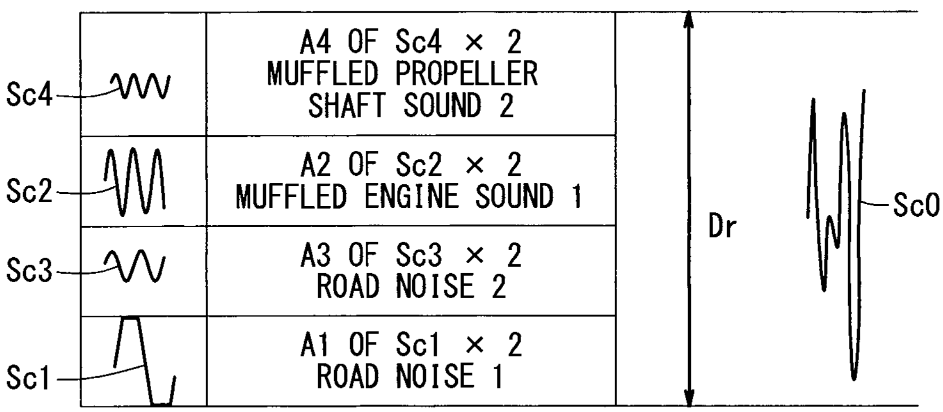


FIG. 7

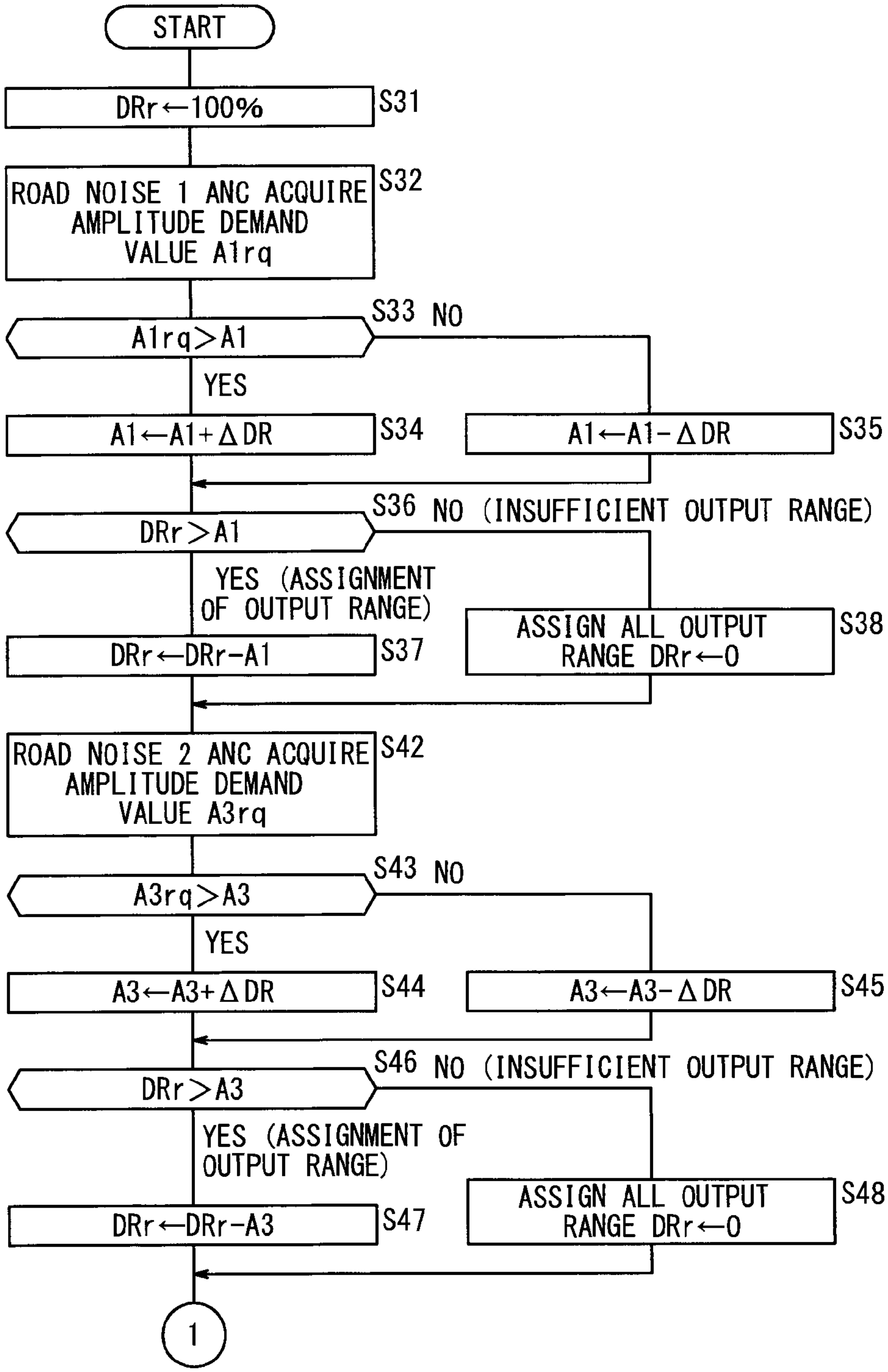

START
DRr←100%
S31
ROAD NOISE 1 ANC ACQUIRE AMPLITUDE DEMAND VALUE A1rq
S32
A1rq>A1
S33
NO
YES
A1←A1+ΔDR
S34
A1←A1-ΔDR
S35
DRr>A1
S36
NO (INSUFFICIENT OUTPUT RANGE)
YES (ASSIGNMENT OF OUTPUT RANGE)
DRr←DRr-A1
S37
ASSIGN ALL OUTPUT RANGE DRr←0
S38
ROAD NOISE 2 ANC ACQUIRE AMPLITUDE DEMAND VALUE A3rq
S42
A3rq>A3
S43
NO
YES
A3←A3+ΔDR
S44
A3←A3-ΔDR
S45
DRr>A3
S46
NO (INSUFFICIENT OUTPUT RANGE)
YES (ASSIGNMENT OF OUTPUT RANGE)
DRr←DRr-A3
S47
ASSIGN ALL OUTPUT RANGE DRr←0
S48
1

FIG. 8

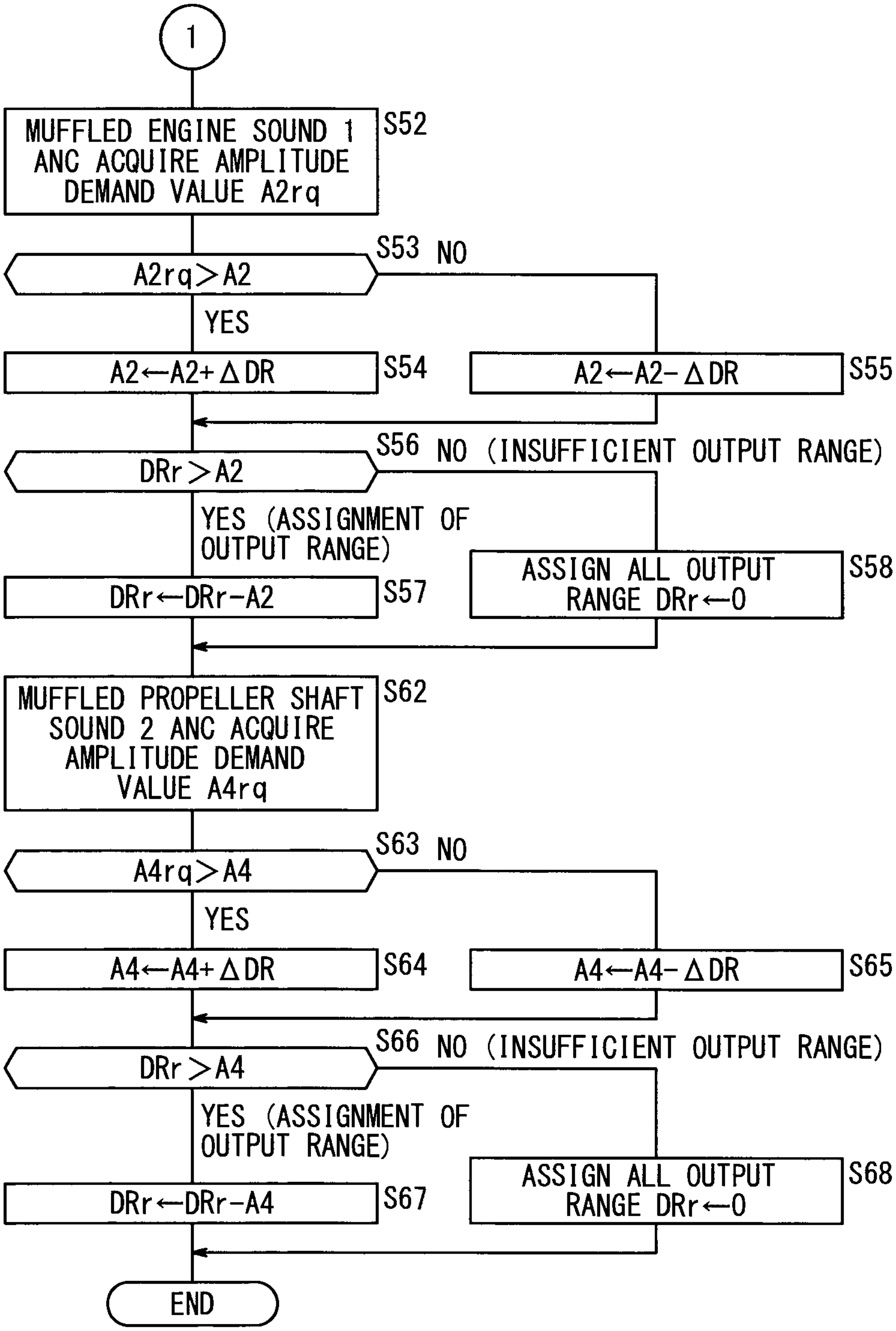
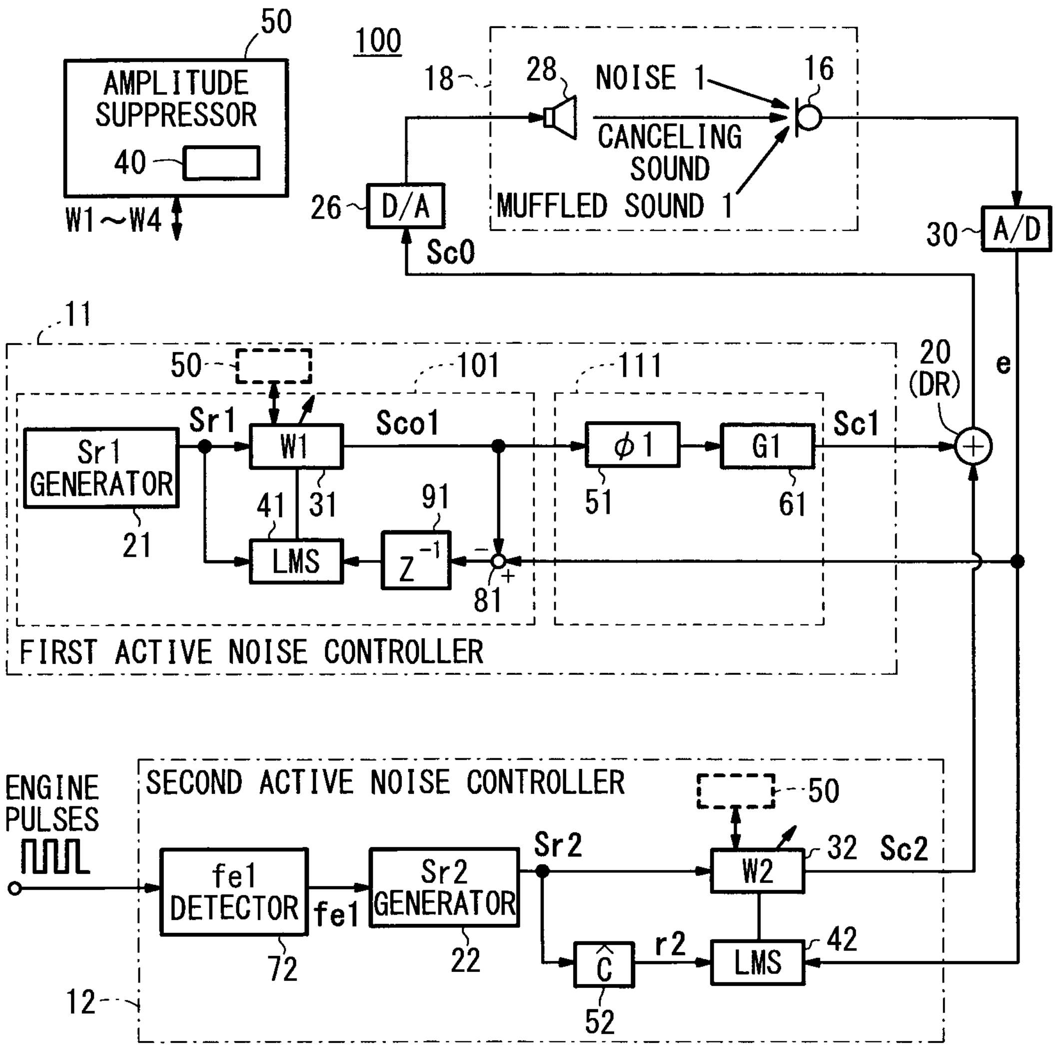

1
MUFFLED ENGINE SOUND 1 ANC ACQUIRE AMPLITUDE DEMAND VALUE A2rq
S52
S53
A2rq>A2
NO
YES
A2←A2+ΔDR
S54
A2←A2-ΔDR
S55
S56
DRr>A2
NO (INSUFFICIENT OUTPUT RANGE)
YES (ASSIGNMENT OF OUTPUT RANGE)
DRr←DRr-A2
S57
ASSIGN ALL OUTPUT RANGE DRr←0
S58
MUFFLED PROPELLER SHAFT SOUND 2 ANC ACQUIRE AMPLITUDE DEMAND VALUE A4rq
S62
S63
A4rq>A4
NO
YES
A4←A4+ΔDR
S64
A4←A4-ΔDR
S65
S66
DRr>A4
NO (INSUFFICIENT OUTPUT RANGE)
YES (ASSIGNMENT OF OUTPUT RANGE)
DRr←DRr-A4
S67
ASSIGN ALL OUTPUT RANGE DRr←0
S68
END

FIG. 9


50
AMPLITUDE SUPPRESSOR
40
W1～W4
100
18
28
NOISE 1
16
CANCELING SOUND
MUFFLED SOUND 1
26
D/A
Sc0
30
A/D
11
50
101
111
20 (DR)
e
Sr1
W1
Sco1
ϕ1
G1
Sc1
Sr1 GENERATOR
21
41
31
91
51
61
LMS
Z⁻¹
81
FIRST ACTIVE NOISE CONTROLLER
ENGINE PULSES
SECOND ACTIVE NOISE CONTROLLER
50
fe1 DETECTOR
fe1
Sr2 GENERATOR
Sr2
W2
32
Sc2
72
22
C
r2
LMS
42
52
12

ACTIVE NOISE CONTROL APPARATUS

CROSS-REFERENCE TO RELATED APPLICATION

This application is based upon and claims the benefit of priority from Japanese Patent Application No. 2012-116321 filed on May 22, 2012, the contents of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to an active noise control apparatus for controlling the noise in the passenger compartment of a vehicle, and more particularly to an active noise control apparatus having a mixer for mixing canceling signals output from a plurality of active noise controllers into a mixed canceling signal.

2. Description of the Related Art

Noise types that have heretofore been known as occurring in the passenger compartments of vehicles include a muffled sound caused by the combustion of fuel by the engine (hereinafter referred to as "muffled engine sound"), a muffled sound caused by unbalanced rotation of a drive-system rotational member such as a propeller shaft while the vehicle is traveling (hereinafter referred to as "muffled propeller shaft sound"), and a noise transmitted from the road through road wheels and suspensions (hereinafter referred to as "road noise").

In order to reduce these noises, a canceling signal for canceling the muffled engine sound and a canceling signal for canceling the road noise are generated by respective active noise controllers (see Japanese Laid-Open Patent Publication No. 07-104767, Japanese Laid-Open Patent Publication No. 10-214119, Japanese Laid-Open Patent Publication No. 2009-057018, and Japanese Laid-Open Patent Publication No. 2009-292201).

In view of cost, space, and other factors, a speaker used as the music sound output unit of a music sound device in the passenger compartment is shared as a canceling sound output unit.

The canceling signal for canceling the muffled engine sound and the canceling signal for canceling the road noise are mixed or added into a mixed canceling signal by a mixer, and the mixed canceling signal is supplied to the speaker, which outputs a canceling sound.

SUMMARY OF THE INVENTION

The mixer has an output range, i.e., a dynamic range, which is limited to n bits, for example. According to the related art, the output range of the mixer is divided into a plurality of equal subranges depending on the number of canceling signals used, e.g., "m", and the subranges are assigned to the respective canceling signals and used in operation.

Active noise control apparatus according to the related art which operate in the manner described above are problematic in that if the amplitude or magnitude of a certain canceling signal becomes too large, then even though the total output range of the mixer is wide enough, the certain canceling signal tends to be clipped in the subrange to which it is assigned, resulting in a reduced noise canceling capability. In particular, the road noise is liable to change greatly in magnitude on different roads, and hence it is difficult to establish a properly predicted subrange for the road noise. Consequently, the active noise control apparatus according to the related art have room for improvement with respect to the cancelation of the road noise.

It is an object of the present invention to provide an active noise control apparatus which is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus travels, by optimizing the use of the output range of a mixer.

Noise types that can be handled by an active noise control apparatus according to the present invention include at least two noise types among a muffled engine sound, a muffled propeller shaft sound, a road noise, a wind noise that is generated by air streams that flow along the surfaces of a vehicle body, and an acceleration sound (pseudo-acceleration sound) generated and output into a passenger compartment depending on the rotational speed of an engine rotational speed.

According to the present invention, there is provided an active noise control apparatus comprising a first active noise controller for generating a first canceling signal for a first noise type, a second active noise controller for generating a second canceling signal for a second noise type that is different from the first noise type, a mixer for mixing the first canceling signal and the second canceling signal into a mixed canceling signal, a canceling sound output unit for outputting a canceling sound based on the mixed canceling signal, and an amplitude suppressor for suppressing an amplitude of the second canceling signal depending on an amplitude of the first canceling signal.

According to the present invention, since the active noise control apparatus has the amplitude suppressor that suppresses the amplitude of the second canceling signal which is input to the mixer depending on the amplitude of the first canceling signal which is input to the mixer, the active noise control apparatus is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus travels, by optimizing the use of the output range of the mixer.

If a sum of the amplitude of the first canceling signal and the amplitude of the second canceling signal is greater than a maximum output amplitude allowed by the mixer, the amplitude suppressor sets the amplitude of the second canceling signal to a difference which is produced when the amplitude of the first canceling signal is subtracted from the maximum output amplitude allowed by the mixer, preventing the amplitude of the first canceling signal from being clipped as much as possible.

If the sum of the amplitude of the first canceling signal and the amplitude of the second canceling signal is greater than a maximum output amplitude allowed by the mixer, the amplitude suppressor sets the amplitude of the second canceling signal to zero, also preventing the amplitude of the first canceling signal from being clipped as much as possible.

The first active noise controller and the second active noise controller include adaptive notch filters, respectively, and the amplitude suppressor calculates the amplitude of the first canceling signal and the amplitude of the second canceling signal based on respective filter coefficients of the adaptive notch filters. Therefore, the amplitude of the first canceling signal and the amplitude of the second canceling signal can be calculated simply.

When the first noise type represents a road noise, even if the amplitude of the first canceling signal cannot be predicted beforehand, the desired first canceling signal for generating a canceling sound for canceling the road noise is prevented from being clipped, and the active noise control apparatus is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus travels, by optimizing the use of the output range of the mixer.

According to the present invention, there is also provided an active noise control apparatus comprising a plurality of active noise controllers for generating a plurality of canceling signals respectively for a plurality of noise types, a mixer for mixing the canceling signals into a mixed canceling signal, a canceling sound output unit for outputting a canceling sound based on the mixed canceling signal, the noise types being in accordance with a noise reduction priority sequence preset therefor, and an amplitude suppressor for suppressing an amplitude of at least one of the canceling signals depending on the noise reduction priority sequence.

Since the amplitude of at least one of the canceling signals, which cancels the noise type whose priority level is lower, is suppressed by the amplitude suppressor, the amplitude of the canceling signal for canceling the noise type whose priority level is higher is prevented from being suppressed accordingly.

According to the present invention, inasmuch as the active noise control apparatus has the amplitude suppressor that suppresses the amplitude of the second canceling signal which is input to the mixer depending on the amplitude of the first canceling signal which is input to the mixer, the active noise control apparatus is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus travels, by optimizing the use of the output range of the mixer.

According to the present invention, furthermore, as the amplitude of at least one of the canceling signals, which cancels the noise type whose priority level is lower, is suppressed by the amplitude suppressor, the amplitude of the canceling signal for canceling the noise type whose priority level is higher is prevented from being suppressed accordingly.

The noise reduction priority sequence has a succession of priority levels set respectively to a road noise which is caused by resonance of suspensions and has its magnitude that varies depending on conditions of a road, a drumming noise caused by resonance of a sound field in a passenger compartment, a muffled engine sound corresponding to a rotational frequency of an engine crankshaft, and a muffled propeller shaft sound corresponding to a rotational frequency of a propeller shaft.

The amplitude suppressor may update a remaining output range of the mixer each time one of the amplitudes of the canceling signals generated respectively by the active noise controllers is assigned to the output range of the mixer in a descending order of the noise types according to the noise reduction priority sequence, and performs a forgetting process for fading out the amplitude of one of the canceling signals for the noise types which cannot be assigned within the remaining output range of the mixer.

The above and other objects, features, and advantages of the present invention will become more apparent from the following description when taken in conjunction with the accompanying drawings in which preferred embodiments of the present invention are shown by way of illustrative example.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. **1** is a block diagram showing a configuration of an active noise control apparatus according to an embodiment of the present invention;

FIG. **2** is a noise reduction priority sequence table for first through fourth active noise controllers of the active noise control apparatus according to the embodiment;

FIG. **3** is a flowchart of an operation sequence of the active noise control apparatus according to the embodiment;

FIG. **4** is a flowchart showing details of an assignment and adjustment process for an output range according to a first example, which is carried out by an amplitude suppressor;

FIGS. **5**A and **5**B are diagrams showing how the first example operates and is advantageous;

FIGS. **6**A and **6**B are diagrams showing how an active noise control apparatus according to the related art operates;

FIG. **7** is a flowchart (part **1**) showing details of a process of assigning and adjusting output ranges according to a second example, which is carried out by the amplitude suppressor;

FIG. **8** is a flowchart (part **2**) showing details of the process of assigning and adjusting output ranges according to the second example, which is carried out by the amplitude suppressor; and

FIG. **9** is a block diagram of an active noise control apparatus illustrated for an easier understanding of the configuration of the active noise control apparatus according to the embodiment, including the first and second examples, and an easier understanding of how the active noise control apparatus according to the embodiment operates and is advantageous.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Active noise control apparatus according to preferred embodiments of the present invention will be described below with reference to the accompanying drawings.

FIG. **1** shows in block form an active noise control apparatus **10** according to an embodiment of the present invention.

As shown in FIG. **1**, the active noise control apparatus **10**, which is incorporated in a vehicle, basically includes a first active noise controller **11** for generating a first canceling signal Sc**1** to generate a canceling sound for canceling a road noise **1** having a frequency f**1**, a second active noise controller **12** for generating a second canceling signal Sc**2** to generate a canceling sound for canceling a muffled engine sound **1**, a third active noise controller **13** for generating a third canceling signal Sc**3** to generate a canceling sound for canceling a road noise **2** having a frequency f**2** which is different from the frequency f**1**, a fourth active noise controller **14** for generating a fourth canceling signal Sc**4** to generate a canceling sound for canceling a muffled propeller shaft sound **2**, and an amplitude suppressor **50** serving as an amplitude controller for controlling respective amplitudes A**1**, A**2**, A**3**, A**4** of the first, second, third, and fourth canceling signals Sc**1**, Sc**2**, Sc**3**, Sc**4** when necessary. The active noise control apparatus **10** performs a control process for silencing the road noises **1**, **2** (indicated as NOISE **1**, NOISE **2** in FIG. **1**), the muffled engine sound **1** (indicated as MUFFLED SOUND **1** in FIG. **1**), and the muffled propeller shaft sound **2** (indicated as MUFFLED SOUND **2** in FIG. **1**) in a cooperative fashion.

The first, second, third, and fourth active noise controllers **11**, **12**, **13**, **14** and the amplitude suppressor **50** are implemented by a computer or a plurality of computers, whose CPU or CPUs read and execute programs stored in a memory or memories such as ROMs in response to various input signals applied thereto, thereby acting as a function performer (also called "function performing means") for performing various functions.

The first, second, third, and fourth canceling signals Sc**1**, Sc**2**, Sc**3**, Sc**4** are mixed or added into a mixed canceling signal Sc**0** (Sc**0**=Sc**1**+Sc**2**+Sc**3**+Sc**4**) by a mixer (adder) **20** having an output range DR. Based on the mixed canceling signal Sc**0**, a D/A converter **26** supplies an output signal to a speaker (canceling sound output unit) **28** disposed in a passenger compartment space **18**. In response to the output signal from the D/A converter **26**, the speaker **28** outputs or radiates the canceling sounds for canceling the road noises **1**, **2**, the muffled engine sound **1**, and the muffled propeller shaft sound **2**.

It is to be noted that if an amplitude level which is twice (full amplitude) the amplitude (half amplitude) of the mixed canceling signal Sc**0** exceeds the output range DR of the mixer **20**, then the mixed canceling signal Sc**0** is clipped by the mixer **20**. In other words, the mixer **20** has an allowable maximum output amplitude that is one-half of the output range DR.

A microphone (error signal detector) **16** for detecting a remaining noise generated by the interference between the muffled engine sound **1**, the muffled propeller shaft sound **2**, and the road noises **1**, **2** and the canceling sounds therefor is disposed at an evaluating point (evaluating position, hearing point) in the passenger compartment space **18**.

The microphone **16** outputs an error signal e which is converted by an A/D converter **30** into a digital error signal e. The digital error signal e is supplied as an input signal to the first, second, third, and fourth active noise controllers **11**, **12**, **13**, **14**.

The first and third active noise controllers **11**, **13** for silencing the road noises **1**, **2** have respective first and third adaptive notch filters **101**, **103** functioning as bandpass filters and respective simulative transfer characteristics sections **111**, **113**.

The first adaptive notch filter **101** of the first active noise controller **11** includes a first base signal generator (Sr**1** generator) **21** for generating a first base signal Sr**1** {cosine signal cos(2πfd**1***t*) and sine signal sin(2πfd**1***t*)} in synchronism with the frequency fd**1** [Hz] of the road noise **1**, which is about a frequency of 120 [Hz], for example, inherent in the type of the vehicle, a first adaptive filter **31** for generating, from the first base signal Sr**1**, an original first canceling signal Sco**1** that is substantially equal in amplitude and phase to a component, which has the frequency fd**1** of the road noise **1**, of the error signal e at a subtrahend terminal of a subtractor **81**, and a filter coefficient updater (algorithm processor) **41**.

The filter coefficient updater **41** is supplied with the first base signal Sr**1** and a signal (e−Sco**1**) that is produced by subtracting the original first canceling signal Sco**1** from the error signal e with the subtractor **81** and delaying the difference with a 1-sample delay element **91**. The filter coefficient updater **41** updates a filter coefficient W**1** (real part+i imaginary part=Rw**1**+iIw**1**) of the first adaptive filter **31** of the first adaptive notch filter **101** based on an adaptive control algorithm for minimizing the signal (e−Sco**1**), e.g., an LMS (Least Mean Square) algorithm which is one type of steepest descent method.

The road noise **1** having the frequency fd**1** is caused by the resonance of suspensions, and has its magnitude which varies greatly depending on the conditions of the road.

The simulative transfer characteristics section **111** includes a phase shifter **51** and a gain setter (gain adjuster) **61**. The phase shifter **51** is preset to a phase shift for shifting the phase of the original first canceling signal Sco**1** having the frequency fd**1** which is input to the phase shifter **51** so that the original first canceling signal Sco**1** will be in opposite phase with the road noise **1** at the position of the microphone **16**. The gain setter **61** is set to a gain G**1** for changing the amplitude of the original first canceling signal Sco**1** shifted in phase by the phase shifter **51** so that it will become substantially equal to the amplitude of the road noise **1** at the position of the microphone **16**.

The third adaptive notch filter **103** of the third active noise controller **13** includes a third base signal generator (Sr**3** generator) **23** for generating a third base signal Sr**3** {cosine signal cos(2πfd**2***t*) and sine signal sin(2πfd**2***t*)} in synchronism with the frequency fd**2** [Hz] of the road noise **2**, which is about a frequency of 40 [Hz], for example, inherent in the type of the vehicle, a third adaptive filter **33** for generating, from the third base signal Sr**3**, an original third canceling signal Sco**3** that is substantially equal in amplitude and phase to a component, which has the frequency fd**2** of the road noise **2**, of the error signal e at a subtrahend terminal of a subtractor **83**, and a filter coefficient updater (algorithm processor) **43**.

The filter coefficient updater **43** is supplied with the third base signal Sr**3** and a signal (e−Sco**3**) that is produced by subtracting the original third canceling signal Sco**3** from the error signal e with the subtractor **83** and delaying the difference with a 1-sample delay element **93**. The filter coefficient updater **43** updates a filter coefficient W**3** (real part+i imaginary part=Rw**3**+iIw**3**) of the third adaptive filter **33** of the third adaptive notch filter **103** based on an adaptive control algorithm for minimizing the signal (e−Sco**3**), e.g., an LMS algorithm which is one type of steepest descent method.

The road noise **2** having the frequency fd**2** is a so-called drumming noise caused by the resonance etc. of the sound field in the passenger compartment, and has its magnitude which does not vary as greatly as the road noise **1**.

The simulative transfer characteristics section **113** includes a phase shifter **53** and a gain setter (gain adjuster) **63**. The phase shifter **53** is preset to a phase shift for shifting the phase of the original third canceling signal Sco**3** having the frequency fd**2** which is input to the phase shifter **53** so that the original third canceling signal Sco**3** will be in opposite phase with the road noise **2** at the position of the microphone **16**. The gain setter **63** is set to a gain G**3** for changing the amplitude of the original third canceling signal Sco**3** shifted in phase by the phase shifter **53** so that it will become substantially equal to the amplitude of the road noise **2** at the position of the microphone **16**.

Each of the second and fourth active noise controllers **12**, **14** comprises a circuit based on a feed-forward filtered-X LMS algorithm.

The second active noise controller **12** includes a rotational frequency detector (fe**1** detector) **72** comprising a frequency counter or the like for detecting a rotational frequency fe**1** of an engine crankshaft (rotational member) from an engine rotation signal (engine pulses) supplied from a fuel injection ECU (FIECU), not shown, a second base signal generator (Sr**2** generator) **22** for generating a second base signal S**2** {cosine signal cos(2πfe**1***t*) and sine signal sin(2πfe**1**t)} having a frequency equal to the rotational frequency fe**1**, a second adaptive filter **32** (second adaptive notch filter) for adjusting the phase and amplitude of the second base signal Sr**2** to generate a second canceling signal Sc**2**, a reference signal generator (filter) **52** for filtering the second base signal Sr**2** to generate a second reference signal r**2**, the reference signal generator **52** being set to simulative transfer characteristics C" and the like which simulate the transfer characteristics of the sound having the rotational frequency fe**1** (each rotational frequency fe**1** as it varies depending on the engine rotation signal) from an output terminal of the second active noise controller **12** for outputting the second canceling signal Sc**2** through the mixer **20**, the D/A converter **26**, the speaker **28**, the passenger compartment space **18** (sound field), the microphone **16**, and the A/D converter **30** to an input terminal of the second active noise controller **12**, i.e., an input terminal of a filter coefficient updater **42** to be described below, and a filter coefficient updater (algorithm processor) **42** for being supplied with the second reference signal r**2** and the error signal e and updating a filter coefficient W**2** (real part+i imaginary part=Rw**2**+iIw**2**) of the second adaptive filter **32** based on an adaptive control algorithm for minimizing the error signal e, e.g., an LMS algorithm which is one type of steepest descent method.

The noise to be canceled by a canceling sound based on the second canceling signal Sc**2** is the muffled engine sound **1** which corresponds to the rotational frequency fe**1** of the engine crankshaft.

The fourth active noise controller **14** includes a rotational frequency detector (fe**2** detector) **74** comprising a frequency counter or the like for detecting a rotational frequency fe**2** which is a harmonic of the rotational frequency of a propeller shaft (rotational member) from a vehicle speed signal (vehicle speed pulses) supplied from a vehicle speed sensor disposed near a countershaft, not shown, a fourth base signal generator (Sr**4** generator) **24** for generating a fourth base signal S**4** {cosine signal cos(2πfe**2**t) and sine signal sin (2πfe**2**t)} having a frequency equal to the rotational frequency fe**2**, a fourth adaptive filter **34** (fourth adaptive notch filter) for adjusting the phase and amplitude of the fourth base signal Sr**4** to generate a fourth canceling signal Sc**4**, a reference signal generator (filter) **54** for filtering the fourth base signal Sr**4** to generate a fourth reference signal r**4**, the reference signal generator **54** being set to simulative transfer characteristics C^ which simulate the transfer characteristics of the sound having the rotational frequency fe**2** (each rotational frequency fe**2** as it varies depending on the rotational frequency of the propeller shaft) from an output terminal of the fourth active noise controller **14** for outputting the fourth canceling signal Sc**4** through the mixer **20**, the D/A converter **26**, the speaker **28**, the passenger compartment space **18** (sound field), the microphone **16**, and the A/D converter **30** to an input terminal of the fourth active noise controller **14**, i.e., an input terminal of a filter coefficient updater **44** to be described below, and a filter coefficient updater (algorithm processor) **44** for being supplied with the fourth reference signal r**4** and the error signal e and updating a filter coefficient W**4** (real part+i imaginary part=Rw**4**+iIw**4**) of the fourth adaptive filter **34** based on an adaptive control algorithm for minimizing the error signal e, e.g., an LMS algorithm which is one type of steepest descent method.

The noise to be canceled by a canceling sound based on the fourth canceling signal Sc**4** is the muffled propeller shaft sound **2** which corresponds to the rotational frequency of the propeller shaft.

The amplitude suppressor **50** of the active noise control apparatus **10** monitors the amplitudes A**1**, A**2**, A**3**, A**4** of the first, second, third, and fourth canceling signals Sc**1**, Sc**2**, Sc**3**, Sc**4** based on the respective filter coefficients W**1**, W**2**, W**3**, W**4**, and adjusts the assignment of the output range DR of the mixer **20** based on the filter coefficients W**1**, W**2**, W**3**, W**4** thereby to suppress the amplitudes A**1**, A**2**, A**3**, A**4** of the first, second, third, and fourth canceling signals Sc**1**, Sc**2**, Sc**3**, Sc**4**.

The first active noise controller **11** shown in FIG. **1** which generates the canceling sound to cancel the road noise **1** having the frequency f**1** may be replaced with an active noise controller according to the so-called adaptive feed-forward technology, i.e., the circuit technology based on the feed-forward filtered-X LMS algorithm, which detects a base signal with respect to suspension vibrations with a vibration detector, outputs the detected base signal as a canceling sound from the speaker **28** through an adaptive filter, detects a remaining noise generated by the interference between the canceling sound and the road noise **1**, as an error signal with the microphone **16**, inputs a reference signal generated based on acoustic transfer characteristics (simulative transfer characteristics from the speaker to the microphone) from the base signal and the error signal, and updates the filter coefficient of the adaptive filter in order to minimize the error signal.

FIG. **2** shows a noise reduction priority sequence table **40** for the first through fourth active noise controllers **11** through **14** of the active noise control apparatus **10** according to the embodiment. The noise reduction priority sequence table **40** is set or stored in a memory of the amplitude suppressor **50**.

According to the present embodiment, a priority level **1** in the noise reduction priority sequence table **40** is set in the first active noise controller **11** which outputs the first canceling signal Sc**1** for canceling the road noise **1** whose amplitude is most difficult to predict in advance. A priority level **2** is set in the third active noise controller **13** which outputs the third canceling signal Sc**3** for canceling the road noise **2**. A priority level **3** is set in the second active noise controller **12** which outputs the second canceling signal Sc**2** for canceling the muffled engine sound **1**. A priority level **4** is set in the fourth active noise controller **14** which outputs the fourth canceling signal Sc**4** for canceling the muffled propeller shaft sound **2**.

The active noise control apparatus **10** according to the present embodiment is basically constructed as described above. Operation of the active noise control apparatus **10** will be described below.

[Overall Operation]

FIG. **3** is a flowchart of the entire operation sequence of the active noise control apparatus **10** according to the embodiment. The operation sequence shown in FIG. **3** is carried out as an interrupt routine in constant cyclic periods by the amplitude suppressor **50** and the first through fourth active noise controllers **11** through **14**.

In step S**1**, a speaker output process is performed in which the speaker **28** outputs canceling sounds for canceling the road noise **1**, the road noise **2**, the muffled engine sound **1**, and the muffled propeller shaft sound **2** into the passenger compartment space **18** based on the first through fourth canceling sounds Sc**1** through Sc**4** that are generated by the first through fourth active noise controllers **11** through **14**.

In step S**2**, a microphone input process is performed in which the microphone **16** detects a remaining noise generated by the interference between the road noise **1**, the road noise **2**, the muffled engine sound **1**, and the muffled propeller shaft sound **2** and the canceling sounds therefor as an error signal e at the evaluating point, and outputs the error signal e to the first through fourth active noise controllers **11** through **14**.

In step S**3**, a vehicle information acquiring process is performed in which vehicle information such as engine pulses and vehicle speed pulses is supplied to the second and fourth active noise controllers **12**, **14**.

In step S**4**, an assignment and adjustment process for the output range DR of the mixer **20** according to a first or second example is carried out as described in detail later.

Based on the results of the assignment and adjustment process for the output range DR of the mixer **20**, filter coefficients W**1** through S**4** are established respectively for the first through fourth active noise controllers **11** through **14**, and first through fourth canceling sounds Sc**1** through Sc**4** are generated respectively by the first through fourth active noise controllers **11** through **14** in steps S**5** through S**8** {in the flowchart shown in FIG. **3**, a road noise **1** ANC (Active Noise Control) process in step S**5**, a road noise **2** ANC process in step S6, a muffled engine sound 1 ANC process in step S7, and a muffled propeller shaft sound 2 ANC process in step S8}.

In step S9, a controller output adding process is performed in which the first through fourth canceling sounds Sc1 through Sc4 that are generated respectively by the first through fourth active noise controllers 11 through 14 are mixed or added into a mixed canceling signal sc0 by the mixer 20. Then, control goes back to step S1.

[Operation of First Example]

FIG. 4 is a flowchart showing details of an assignment and adjustment process for the output range DR of the mixer 20 according to a first example, which is carried out by the amplitude suppressor 50 in step S4.

In step S11 shown in FIG. 4, the amplitude suppressor 50 initializes a remaining output range DRr which represents a remainder of the output range DR (DRr←100 [%]).

In step S12, the amplitude suppressor 50 calculates an amplitude (amplitude demand value) A1 of the first canceling signal Sc1 at the priority level 1 based on a present filter coefficient W1 of the first adaptive filter 31 according to a following equation (1), and assigns the calculated amplitude A1 to the remaining output range DRr:

$$A1=G1\times\sqrt{\{(Rw1)^2+(Iw1)^2\}} \tag{1}$$

On the right side of the equation (1), G1 represents the gain of the gain setter 61 and $\sqrt{\{(Rw1)^2+(Iw1)^2\}}$ the magnitude of the filter coefficient W1 (W1=Rw1+i·Iw1) of the first adaptive filter 31.

In step S13, the amplitude suppressor 50 updates the remaining output range DRr according to a following expression (2):

$$DRr\leftarrow(DRr-A1) \tag{2}$$

In other words, the amplitude A1 is subtracted from the present remaining output range DRr to produce an updated remaining output range DRr.

In step S14, the amplitude suppressor 50 calculates an amplitude (amplitude demand value) A3 of the third canceling signal Sc3 at the priority level 2 based on a present filter coefficient W3 of the third adaptive filter 33 according to a following equation (3):

$$A3=G3\times\sqrt{\{(Rw3)^2+(Iw3)^2\}} \tag{3}$$

On the right side of the equation (3), G3 represents the gain of the gain setter 63 and $\sqrt{\{(Rw3)^2+(Iw3)^2\}}$ the magnitude of the filter coefficient W3 (W3=Rw3+i·Iw3) of the third adaptive filter 33.

In step S15, the amplitude suppressor 50 judges whether any remaining output range DRr of the mixer 20 is left or not according to a following inequality (4):

$$(DRr-A3)>0 \tag{4}$$

If there is left a remaining output range DRr, then the amplitude suppressor 50 assigns the amplitude A3 of the third canceling signal Sc3 to the remaining output range DRr of the mixer 20 in step S16. In step S17, the amplitude suppressor 50 updates the remaining output range DRr according to a following expression (5):

$$DRr\leftarrow(DRr-A3) \tag{5}$$

In step S18, the amplitude suppressor 50 calculates an amplitude (amplitude demand value) A2 of the second canceling signal Sc2 at the priority level 3 based on a present filter coefficient W2 of the second adaptive filter 32 according to a following equation (6):

$$A2=\sqrt{\{(Rw2)^2+(Iw2)^2\}} \tag{6}$$

On the right side of the equation (6), $\sqrt{\{(Rw2)^2+(Iw2)^2\}}$ represents the magnitude of the filter coefficient W2 (W2=Rw2+i·Iw2) of the second adaptive filter 32.

In step S19, the amplitude suppressor 50 judges whether any remaining output range DRr of the mixer 20 is left or not according to a following inequality (7):

$$(DRr-A2)>0 \tag{7}$$

If there is left a remaining output range DRr, then the amplitude suppressor 50 assigns the amplitude A2 of the second canceling signal Sc2 to the remaining output range DRr of the mixer 20 in step S20. In step S21, the amplitude suppressor 50 updates the remaining output range DRr according to a following expression (8):

$$DRr\leftarrow(DRr-A2) \tag{8}$$

In step S22, the amplitude suppressor 50 calculates an amplitude (amplitude demand value) A4 of the fourth canceling signal Sc4 at the priority level 4 based on a present filter coefficient W4 of the fourth adaptive filter 34 according to a following equation (9):

$$A4=\sqrt{\{(Rw4)^2+(Iw4)^2\}} \tag{9}$$

On the right side of the equation (9), $\sqrt{\{(Rw4)^2+(Iw4)^2\}}$ represents the magnitude of the filter coefficient W4 (W4=Rw4+i·Iw4) of the fourth adaptive filter 34.

In step S23, the amplitude suppressor 50 judges whether any remaining output range DRr of the mixer 20 is left or not according to a following inequality (10):

$$(DRr-A4)>0 \tag{10}$$

If there is left a remaining output range DRr, then the amplitude suppressor 50 assigns the amplitude A4 of the fourth canceling signal Sc4 to the remaining output range DRr of the mixer 20 in step S24. Thereafter, the assignment and adjustment process shown in FIG. 4 is ended. After steps S5 through S9 and steps S1 through S3 shown in FIG. 3 are performed, steps S11 through S24 shown in FIG. 4, which represent a subroutine of step S4, are repeated.

If it is judged in step S15 that the amplitude A3, calculated in step S14, of the third canceling signal Sc3 for canceling the road noise 2 at the priority level 2 cannot be assigned {(DRr−A3)≤0}, then a forgetting process is carried out for the filter coefficients W3, W2, W4 at the priority levels 2, 3, 4 in step S25. Specifically, a forgetting process is carried out to fade out the third, second, and fourth canceling signals Sc3, Sc2, Sc4 which generate canceling sounds using corrected filter coefficients that are produced by multiplying the filter coefficients W3, W2, W4 of the third, second, and fourth adaptive filters 33, 32, 34 of the third, second, and fourth active noise controllers 13, 12, 14, by a certain value smaller than 1, e.g., 127/128≈0.99.

Similarly, if it is judged in step S19 that the amplitude A2, calculated in step S18, of the second canceling signal Sc2 for canceling the muffled engine sound 1 at the priority level 3 cannot be assigned {(DRr−A2)≤0}, then a forgetting process is carried out for the filter coefficients W2, W4 (which have not been updated yet) at the priority levels 3, 4 in step S26. Specifically, a forgetting process is carried out to fade out the second and fourth canceling signals Sc2, Sc4 which generate canceling sounds using corrected filter coefficients that are produced by multiplying the filter coefficients W2, W4 of the second and fourth adaptive filters 32, 34 of the second and fourth active noise controllers 12, 14, by a certain value smaller than 1, e.g., 127/128≈0.99.

If it is judged in step S23 that the amplitude A4, calculated in step S22, of the fourth canceling signal Sc4 for canceling the muffled propeller shaft sound **2** at the priority level **4** cannot be assigned {(DRr−A**4**)≤0}, then a forgetting process is carried out for the filter coefficient W**4** at the priority level **4** in step S**27**. Specifically, a forgetting process is carried out to fade out the fourth canceling signal Sc**4** which generates a canceling sound using a corrected filter coefficient that is produced by multiplying the filter coefficient W**4** (which has not been updated yet) of the fourth adaptive filter **34** of the fourth active noise controller **14**, by a certain value smaller than 1, e.g., 127/128≈0.99.

FIGS. **5**A and **5**B are diagrams showing how the first example operates and is advantageous, and FIGS. **6**A and **6**B are diagrams showing how an active noise control apparatus according to the related art operates.

According to the first example, as shown in FIG. **5**A, if the sum 2×(A**1**+A**3**+A**2**+A**4**) of the full amplitudes A**1**×2, A**3**×2, A**2**×2, A**4**×2 of the first, third, second, and fourth canceling signals Sc**1**, Sc**3**, Sc**2**, Sc**4** is smaller than the output range DR, then since any one of the first, third, second, and fourth canceling signals Sc**1**, Sc**3**, Sc**2**, Sc**4** is not clipped, the mixed canceling signal Sc**0** output from the mixer **20** is supplied while undistorted through the D/A converter **26** to the speaker **28**, which then output corresponding canceling sounds.

According to the first example, as shown in FIG. **5**B, if the sum 2×(A**1**+A**3**+A**2**) of the full amplitudes A**1**×2, A**3**×2, A**2**×2 of the first, third, and second canceling signals Sc**1**, Sc**3**, Sc**2** is smaller than the output range DR (step S**19**: YES), then any one of the first, third, and second canceling signals Sc**1**, Sc**3**, Sc**2** is not clipped, but output as a canceling sound. If the answer to step S**23** is negative {(DRr−A**4**)≤0}, then since a forgetting process is performed on the fourth canceling signal Sc**4**, the mixed canceling signal Sc**0** that is output from the mixer **20** from the first, third, and second canceling signals Sc**1**, Sc**3**, Sc**2** is not distorted.

According to the related art, as shown in FIG. **6**A, if each of the full amplitudes A**1**×2, A**3**×2, A**2**×2, A**4**×2 of the first, third, second, and fourth canceling signals Sc**1**, Sc**3**, Sc**2**, Sc**4** is smaller than ¼ of the output range DR, then since any one of the first, third, second, and fourth canceling signals Sc**1**, Sc**3**, Sc**2**, Sc**4** is not clipped, the mixed canceling signal Sc**0** is not distorted.

According to the related art, however, as shown in FIG. **6**B, if either one of the full amplitudes A**1**×2, A**3**×2, A**2**×2, A**4**×2 of the first, third, second, and fourth canceling signals Sc**1**, Sc**3**, Sc**2**, Sc**4**, i.e., the full amplitude A**1**×2 of the first canceling signal Sc**1** in this example, is greater than ¼ of the output range DR, then since the first canceling signal Sc**1** is clipped, the mixed canceling signal Sc**0** is distorted.

[Operation of Second Example]

FIGS. **7** and **8** are flowcharts showing details of an assignment and adjustment process for the output range DR of the mixer **20** according to a second example, which is carried out by the amplitude suppressor **50** in step S**4**. The same or presumable operation in the second example as or from the operation in the first example will be omitted or described briefly for avoiding complexity.

In step S**31** shown in FIG. **7**, the amplitude suppressor **50** initializes a remaining output range DRr which represents a remainder of the output range DR (DRr←100 [%]).

In step S**32**, the amplitude suppressor **50** calculates an amplitude demand value A**1***rq* of the first canceling signal Sc**1** at the priority level **1** based on a present filter coefficient W**1** of the first adaptive filter **31** according to a following equation (11):

$$A1rq=K1\times G1\times\sqrt{\{(Rw1)^2+(Iw1)^2\}} \tag{11}$$

where K**1** represents a margin coefficient which is preset to a certain value in the range of 2>K**1**>1. The margin coefficient K**1** is set to a value greater than 1 in order to maintain the output range DR in a next updating cycle to allow the next updating cycle to a certain extent.

In step S**33**, the amplitude suppressor **50** judges whether or not the amplitude demand value A**1***rq* is greater than a present suppressed amplitude value A**1**[A**1**=G**1**×√{(Rw**1**)²+(Iw**1**)²}] that is calculated based on the filter coefficient W**1** of the first adaptive filter **31**.

If the amplitude suppressor **50** decides that the amplitude demand value A**1***rq* is greater than the present suppressed amplitude value A**1** (step S**33**: YES), then the amplitude suppressor **50** performs a follow-up process for gradually increasing a target value to update the suppressed amplitude value A**1** according to a following expression (12) in step S**34**:

$$A1\leftarrow(A1+\Delta DR) \tag{12}$$

where ΔDR represents a fixed value to be added to slightly increase the suppressed amplitude value A**1** for the assignment of the output range DR.

If the amplitude suppressor **50** decides that the amplitude demand value A**1***rq* is not greater than the present suppressed amplitude value A**1** (step S**33**: NO), then the amplitude suppressor **50** performs a follow-up process for gradually decreasing a target value to update the suppressed amplitude value A**1** according to a following expression (13) in step S**35**:

$$A1\leftarrow(A1-\Delta DR) \tag{13}$$

In step S**36**, the amplitude suppressor **50** judges whether the updated suppressed amplitude value A**1** is smaller than a remaining output range DRr or not.

If the updated suppressed amplitude value A**1** is smaller than the remaining output range DRr (step S**36**: YES), then the amplitude suppressor **50** sets 1/G**1** of the updated suppressed amplitude value A**1** to the filter coefficient W**1** of the first adaptive filter **31** of the first active noise controller **11** for silencing the road noise **1**, and updates the remaining output range DRr according to a following expression (14) in step S**37**:

$$DRr\leftarrow(DRr-A1) \tag{14}$$

If the updated suppressed amplitude value A**1** is not smaller than the remaining output range DRr (step S**36**: NO, DRr≤A**1**), then since the output range DR is insufficient, the amplitude suppressor **50** assigns all the output range DR of the mixer **20** to the first active noise controller **11** for silencing the road noise **1**, and sets the remaining output range DRr to zero (DRr←0) in step S**38**.

Then, in step S**42**, the amplitude suppressor **50** calculates an amplitude demand value A**3***rq* of the third canceling signal Sc**3** at the priority level **2** based on a present filter coefficient W**3** of the third adaptive filter **33** according to a following equation (15):

$$A3rq=K3\times G3\times\sqrt{\{(Rw3)^2+(Iw3)^2\}} \tag{15}$$

where K**3** represents a margin coefficient which is preset to a certain value in the range of 2>K**3**>1.

The processing of each of steps S**43** through S**48** is similar to the processing of each of steps S**33** through S**38**, and will briefly be described below.

In step S**43**, the amplitude suppressor **50** judges whether or not the amplitude demand value A**3***rq* is greater than a present suppressed amplitude value A**3** [A**3**=G**3**×√{(Rw**3**)²+(Iw**3**)²}] based on the filter coefficient W**3** of the third adaptive filter **33**. If the amplitude suppressor **50** decides that the amplitude demand value A**3***rq* is greater than the present suppressed amplitude value A3 (step S43: YES), then the amplitude suppressor **50** performs a follow-up process for gradually increasing a target value to update the suppressed amplitude value A3 according to a following expression (16) in step S44:

$$A3 \leftarrow (A3+\Delta DR) \quad (16)$$

If the amplitude suppressor **50** decides that the amplitude demand value A3*rq* is not greater than the present suppressed amplitude value A3 (step S43: NO), then the amplitude suppressor **50** performs a follow-up process for gradually decreasing a target value to update the suppressed amplitude value A3 according to a following expression (17) in step S45:

$$A3 \leftarrow (A3-\Delta DR) \quad (17)$$

In step S46, the amplitude suppressor **50** judges whether the updated suppressed amplitude value A3 is smaller than the remaining output range DRr or not.

If the updated suppressed amplitude value A3 is smaller than the remaining output range DRr (step S46: YES), then the amplitude suppressor **50** sets 1/G3 of the updated suppressed amplitude value A3 to the filter coefficient W3 of the third adaptive filter **33** of the third active noise controller **13** for silencing the road noise **2**, and updates the remaining output range DRr according to a following expression (18) in step S47:

$$DRr \leftarrow (DRr-A3) \quad (18)$$

If the updated suppressed amplitude value A3 is not smaller than the remaining output range DRr (step S46: NO, DRr≤A3), then since the output range DR is insufficient, the amplitude suppressor **50** assigns all the output range DR of the mixer **20** to the third active noise controller **13** for silencing the road noise **2**, and sets the remaining output range DRr to zero (DRr←0) in step S48. If the remaining output range DRr has already been set to zero in step S38, then the filter coefficient W3 of the third adaptive filter **33** is set to zero according to a forgetting process.

Then, in step S52 shown in FIG. **8**, the amplitude suppressor **50** calculates an amplitude demand value A2*rq* of the second canceling signal Sc2 at the priority level **3** based on a present filter coefficient W2 of the second adaptive filter **32** according to a following equation (19):

$$A2rq = K2 \times \sqrt{\{(Rw2)^2+(Iw2)^2\}} \quad (19)$$

where K2 represents a margin coefficient which is preset to a certain value in the range of 2>K2>1.

The processing of each of steps S53 through S58 is similar to the processing of each of steps S33 through S38, and will briefly be described below.

In step S53, the amplitude suppressor **50** judges whether or not the amplitude demand value A2*rq* is greater than a present suppressed amplitude value A2 [$A2=\sqrt{\{(Rw2)^2+(Iw2)^2\}}$]. If the amplitude suppressor **50** decides that the amplitude demand value A2*rq* is greater than the present suppressed amplitude value A2 (step S53: YES), then the amplitude suppressor **50** performs a follow-up process for gradually increasing a target value to update the suppressed amplitude value A2 according to a following expression (20) in step S54:

$$A2 \leftarrow (A2+\Delta DR) \quad (20)$$

If the amplitude suppressor **50** decides that the amplitude demand value A2*rq* is not greater than the present suppressed amplitude value A2 (step S53: NO), then the amplitude suppressor **50** performs a follow-up process for gradually decreasing a target value to update the suppressed amplitude value A2 according to a following expression (21) in step S55:

$$A2 \leftarrow (A2-\Delta DR) \quad (21)$$

In step S56, the amplitude suppressor **50** judges whether the updated suppressed amplitude value A2 is smaller than the remaining output range DRr or not.

If the updated suppressed amplitude value A2 is smaller than the remaining output range DRr (step S56: YES), then the amplitude suppressor **50** sets the updated suppressed amplitude value A2 to the filter coefficient W2 of the second adaptive filter **32** of the second active noise controller **12** for silencing the muffled engine sound **1**, and updates the remaining output range DRr according to a following expression (22) in step S57:

$$DRr \leftarrow (DRr-A2) \quad (22)$$

If the updated suppressed amplitude value A2 is not smaller than the remaining output range DRr (step S56: NO, DRr≤A2), then since the output range DR is insufficient, the amplitude suppressor **50** assigns all the output range DR of the mixer **20** to the second active noise controller **12** for silencing the muffled engine sound **1**, and sets the remaining output range DRr to zero (DRr←0) in step S58.

If the remaining output range DRr has already been set to zero in step S38 or step S48, then the filter coefficient W2 of the second adaptive filter **32** is set to zero according to a forgetting process.

Then, in step S62, the amplitude suppressor **50** calculates an amplitude demand value A4*rq* of the fourth canceling signal Sc4 at the priority level **4** based on a present filter coefficient W4 of the fourth adaptive filter **34** according to a following equation (23):

$$A4rq = K4 \times \sqrt{\{(Rw4)^2+(Iw4)^2\}} \quad (23)$$

where K4 represents a margin coefficient which is preset to a certain value in the range of 2>K4>1.

The processing of each of steps S63 through S68 is similar to the processing of each of steps S33 through S38, and will briefly be described below.

In step S63, the amplitude suppressor **50** judges whether or not the amplitude demand value A4*rq* is greater than a present suppressed amplitude value A4 [$A4=\sqrt{\{(Rw4)^2+(Iw4)^2\}}$]. If the amplitude suppressor **50** decides that the amplitude demand value A4*rq* is greater than the present suppressed amplitude value A4 (step S63: YES), then the amplitude suppressor **50** performs a follow-up process for gradually increasing a target value to update the suppressed amplitude value A4 according to a following expression (24) in step S64:

$$A4 \leftarrow (A4+\Delta DR) \quad (24)$$

If the amplitude suppressor **50** decides that the amplitude demand value A4*rq* is not greater than the present suppressed amplitude value A4 (step S63: NO), then the amplitude suppressor **50** performs a follow-up process for gradually decreasing a target value to update the suppressed amplitude value A4 according to a following expression (25) in step S65:

$$A4 \leftarrow (A4-\Delta DR) \quad (25)$$

In step S66, the amplitude suppressor **50** judges whether the updated suppressed amplitude value A4 is smaller than the remaining output range DRr or not.

If the updated suppressed amplitude value A4 is smaller than the remaining output range DRr (step S66: YES), then the amplitude suppressor **50** sets the updated suppressed amplitude value A4 to the filter coefficient W4 of the fourth adaptive filter **34** of the fourth active noise controller **14** for silencing the propeller shaft sound **2**, and updates the remaining output range DRr according to a following expression (26) in step S**67**:

$$DRr \leftarrow (DRr - A4) \quad (26)$$

If the updated suppressed amplitude value A**4** is not smaller than the remaining output range DRr (step S**66**: NO, DRr≤A**4**), then since the output range DR is insufficient, the amplitude suppressor **50** assigns all the output range DR of the mixer **20** to the fourth active noise controller **14** for silencing the propeller shaft sound **2**, and sets the remaining output range DRr to zero (DRr←0) in step S**68**.

If the remaining output range DRr has already been set to zero in step S**38** or step S**48** or step S**58**, then the filter coefficient W**4** of the fourth adaptive filter **34** is set to zero according to a forgetting process.

[Summary of the Embodiment]

The configuration and advantages of the active noise control apparatus according to the present embodiment which includes the first and second examples described above will be described with respect to an active noise control apparatus **100** shown in FIG. **9** which includes two active noise controllers, i.e., a first active noise controller **11** for silencing the road noise **1** at the priority level **1** and a second active noise controller **12** for silencing the muffled engine sound **1** at the priority level **3** (priority level **2** in FIG. **9**), for an easier understanding of the present invention.

The active noise control apparatus **100** includes a first active noise controller **11** which generates a first canceling signal Sc**1** for a first noise type, a second active noise controller **12** which generates a second canceling signal Sc**2** for a second noise type that is different from the first noise type, a mixer **20** for mixing the first canceling signal Sc**1** and the second canceling signal Sc**2** into a mixed canceling signal Sc**0**, a speaker **28** as a canceling sound output unit for outputting a canceling signal based on the mixed canceling signal Sc**0**, and an amplitude suppressor **50** for suppressing the amplitude A2 [$A2=\sqrt{\{(Rw2)^2+(Iw2)^2\}}$] of the second canceling signal Sc**2** depending on the amplitude A1 [$A1=G1\times\sqrt{\{(Rw1)^2+(Iw1)^2\}}$] of the first canceling signal Sc**1**.

Since the active noise control apparatus **100** has the amplitude suppressor **50** that suppresses the amplitude A2 of the second canceling signal Sc**2** which is input to the mixer **20** depending on the amplitude A1 of the first canceling signal Sc**1** which is input to the mixer **20**, the active noise control apparatus **100** is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus **100** travels, by optimizing the use of the output range DR (DR/2 if corresponding to the amplitude) of the mixer **20**.

If the sum (A**1**+A**2**) of the amplitude A1 of the first canceling signal Sc**1** and the amplitude A2 of the second canceling signal Sc**2** is greater than the maximum output amplitude DR/2 allowed by the mixer **20** {(A**1**+A**2**)>(DR/2)}, then the amplitude suppressor **50** sets the amplitude A2 of the second canceling signal Sc**2** to the difference that is produced when the amplitude A1 of the first canceling signal Sc**1** is subtracted from the allowable maximum output amplitude DR/2 of the mixer **20** [A**2**≤{(DR/2)−A**1**}], preventing the amplitude A1 of the first canceling signal Sc**1** from being clipped as much as possible.

If the sum (A**1**+A**2**) of the amplitude A1 of the first canceling signal Sc**1** and the amplitude A2 of the second canceling signal Sc**2** is greater than the maximum output amplitude DR/2 allowed by the mixer **20** {(A**1**+A**2**)>(DR/2)}, then the amplitude suppressor **50** sets the amplitude A2 of the second canceling signal Sc**2** to zero, also preventing the amplitude A1 of the first canceling signal Sc**1** from being clipped as much as possible.

The first active noise controller **11** and the second active noise controller **12** have the first and second adaptive notch filters **101**, **32**, respectively (through the reference numeral **32** is described as representing an adaptive filter, it may also be considered as an adaptive notch filter because it adaptively attenuates the muffled engine sound **1** having the rotational frequency fe**1**), and the amplitude A1 [$A1=G1\times\sqrt{\{(Rw1)^2+(Iw1)^2\}}$] of the first canceling signal Sc**1** and the amplitude A2 [$A2=\sqrt{\{(Rw2)^2+(Iw2)^2\}}$] of the second canceling signal Sc**2** are calculated from the respective filter coefficients W**1**, W**2** of the first and second adaptive notch filters **101**, **32**. Therefore, the amplitude A1 of the first canceling signal Sc**1** and the amplitude A2 of the second canceling signal Sc**2** can be calculated simply.

When the first noise type represents the road noise **1**, even if the amplitude A1 of the first canceling signal Sc**1** cannot be predicted beforehand, the desired first canceling signal Sc**1** is prevented from being clipped, and the active noise control apparatus **100** is capable of outputting an optimum canceling sound depending on how a vehicle that incorporates the active noise control apparatus **100** travels, by optimizing the use of the output range DR of the mixer **20**.

The active noise control apparatus **100** includes first and second active noise controllers **11**, **12** which generate a plurality of first and second canceling signals Sc**1**, Sc**2** respectively for a plurality of noise types, a mixer **20** for mixing the first and second canceling signals Sc**1**, Sc**2** into a mixed canceling signal Sc**0**, a speaker **28** as a canceling sound output unit for outputting a canceling sound based on the mixed canceling signal Sc**0**, the noise types being in accordance with a noise reduction priority sequence (the priority level of the noise type to be canceled by the first active noise controller **11** is higher than the priority level of the noise type to be canceled by the second active noise controller **12**) established therefor, and an amplitude suppressor **50** for suppressing the amplitude of at least one (whose priority level is lower) of the first and second canceling signals Sc**1**, Sc**2**, i.e., the amplitude A2 of the second canceling signal Sc**2**, depending on the noise reduction priority sequence.

Since the amplitude A2 of the second canceling signal Sc**2**, i.e., the amplitude of at least one of the canceling signals for canceling the noise type whose priority level is lower, is suppressed by the amplitude suppressor **50**, the amplitude A1 of the first canceling signal Sc**1** for canceling the noise type whose priority level is higher is prevented from being suppressed accordingly.

The present invention is not limited to the above embodiment, but may changes and modifications may be made based on the disclosure of the above description. For example, the active noise control apparatus **100** shown in FIG. **9** may be devoid of the second active noise controller **12** for canceling the muffled engine sound **1**, but may instead include an active sound effect generation controller at the priority level **2** for generating a base signal based on a signal representing detected engine vibrations, generating a control signal by changing the amplitude and phase of the base signal to produce an acceleration-dependent sound effect, and supplying the control signal via the mixer **20** to the speaker **28** to produce a sound effect (accelerating sound) in the passenger compartment space **18**, or the active noise control apparatus **10** shown in FIG. **1** may include such an active sound effect generation controller at a priority level **5**.

What is claimed is:

1. An active noise control apparatus, comprising:

a first active noise controller for generating a first canceling signal for a first noise type, the first active noise controller including a first adaptive notch filter;

a second active noise controller for generating a second canceling signal for a second noise type that is different from the first noise type, the second active noise controller including a second adaptive notch filter;

a mixer for mixing the first canceling signal and the second canceling signal into a mixed canceling signal;

a canceling sound output unit for outputting a canceling sound based on the mixed canceling signal; and

an amplitude suppressor for calculating an amplitude of the first canceling signal based on a filter coefficient of the first adaptive notch filter, calculating an amplitude of the second canceling signal based on a filter coefficient of the second adaptive notch filter, and suppressing the amplitude of the second canceling signal depending on the amplitude of the first canceling signal,

wherein if the amplitude of the second canceling signal cannot be assigned within a value range which is produced when the amplitude of the first canceling signal is subtracted from a maximum output amplitude allowed by the mixer, the amplitude suppressor decreases the filter coefficient of the second adaptive notch filter to fade out the second canceling signal.

2. The active noise control apparatus according to claim **1**, further comprising:

a plurality of active noise controllers, including the first active noise controller and the second active noise controller, for generating a plurality of canceling signals respectively for a plurality of noise types;

wherein the mixer mixes the canceling signals into a mixed canceling signal; and

the amplitude suppressor suppresses an amplitude of at least one of the canceling signals depending on a noise reduction priority sequence preset for the noise types.

3. The active noise control apparatus according to claim **1**, wherein if a sum of the amplitude of the first canceling signal and the amplitude of **1** the second canceling signal is greater than the maximum output amplitude allowed by the mixer, the amplitude suppressor sets the amplitude of the second canceling signal to a difference which is produced when the amplitude of the first canceling signal is subtracted from the maximum output amplitude allowed by the mixer.

4. The active noise control apparatus according to claim **1**, wherein if the sum of the amplitude of the first canceling signal and the amplitude of the second canceling signal is greater than the maximum output amplitude allowed by the mixer, the amplitude suppressor sets the amplitude of the second canceling signal to zero.

5. The active noise control apparatus according to claim **1**, wherein the first noise type represents a road noise.

6. The active noise control apparatus according to claim **2**, wherein the noise reduction priority sequence has a succession of priority levels set respectively to a road noise which is caused by resonance of suspensions and has its magnitude that varies depending on conditions of a road, a drumming noise caused by resonance of a sound field in a passenger compartment, a muffled engine sound corresponding to a rotational frequency of an engine crankshaft, and a muffled propeller shaft sound corresponding to a rotational frequency of a propeller shaft.

7. The active noise control apparatus according to claim **2**, wherein the amplitude suppressor updates a remaining output range of the mixer each time one of the amplitudes of the canceling signals generated respectively by the active noise controllers is assigned to the output range of the mixer in a descending order of the noise types according to the noise reduction priority sequence, and performs a forgetting process for fading out the amplitude of one of the canceling signals for the noise types which cannot be assigned within the remaining output range of the mixer.

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