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(54) Title: SPATIAL LIGHT MODULATOR SYSTEM <div style="text-align: center;"> </div> (57) Abstract <p>A display projection apparatus comprising a light source, means for splitting light from the source into different color component beams, and a plurality of deformable mirror device spatial light modulators, characterised in that the light paths to said splitting means and modulators are provided as a single prism assembly to which said modulators are mounted.</p>		

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- 1 -

SPATIAL LIGHT MODULATOR SYSTEM

This invention relates to a spatial light modulator system. Particularly, but not exclusively, this invention relates to a projection system in which a projected display is formed by modulating light from a light source by a spatial light modulator device, and then projecting the modulated light on to a display area. Particularly, but not exclusively, the invention relates to a color spatial light modulator system in which beams having different color content are reflected from different spatial light modulator devices each driven in accordance with a different video signal, and the modulated beams are combined to form a single projected color display.

A spatial light modulator is an optical component which is controllable to modulate an incident light beam. A relatively old example is the eidophor, a layer of oil scanned by a cathode ray. One class of spatial light modulators is active matrix devices, comprising a matrix of individually addressed pixel light valves or modulators; the liquid crystal modulator array described in, for example, EP 0401912 is one modulator array of this type. In EP 0401912, a liquid crystal matrix is provided in a light path to

- 2 -

variably transmit, and hence amplitude modulate, the incident light beam (without altering its path or optical axis). Another example of such an active matrix comprises an array of the tiltable mirror devices, for example the deformable mirror device (DMD) described in, for example, US 4856863, US 4615595, and US 4596992.

Such devices comprise miniature mirrored cantilever beam elements carrying electrodes so as to be electrostatically deflectable between two positions. The extent of the deflection can be controlled by the applied electrostatic potential to provide variable degrees of reflection, or the device can be operated in a binary manner by applying predetermined electrostatic potentials to switch between discrete deflection states. It thus angularly deflects the incident light beam and hence changes the optical axis of the light beam.

Using an array of such devices, each individually addressable, a two dimensional image can be reproduced by exposing the array to an incident light beam, modulating the incident beam by controlling the individual mirror devices from a picture signal, and

- 3 -

collating the beam reflected in a particular direction. The small size and fast switching times of devices of the kind described in the above mentioned patents makes them usable at video picture data rates, enabling the display of television or video moving images on a display screen onto which the collated beam is projected.

The incident beam is not scanned, as is an electron beam, but illuminates the entire device. In order to display a color image, therefore, it is necessary to provide three separately illuminated deflector arrays, one controlled responsively to each primary color or primary color combinations, and to optically combine the modulated beams reflected from each device onto a single optical display.

One example of an application of such a system is in large scale displays as disclosed in our earlier International Applications WO91/15843, WO91/15923, PCT/GB92/00002, and PCT/GB92/00132 (all of which are incorporated herein by reference).

- 4 -

Various optical systems for spatial light modulator projectors are known from, for example, EP 0401912, EP 0363763 and EP 0450952. A projection system which includes liquid crystal arrays is described in EP 5 0395156. In this system, a lenticular array arrangement of a type also known from, for example, US 3296923 is adopted in which light from a light source is made parallel and directed through a first array of lenslets, each rectangular in cross section and curved 10 on one face, from which the light is directed through a second array of such lenslets, the spacing and curvature of the lenslets being such that each of the first lenslets focuses light into the center of a corresponding lenslet in the second array, and then 15 light from the second array is directed through a concentrating lens and thence onto a spatial light modulator array.

The effect of this arrangement is that the initially 20 circular beam of light is transformed into an array of rectangular sub images by the lenticular arrays, which are then combined by a concentrating lens into a single rectangular uniform beam of light suitable for illuminating a rectangular modulator; the 25 transformation from a circular beam to a uniform

- 5 -

rectangular beam is achieved without loss of optical power. EP 0395156 is incorporated herein by reference in its entirety.

5 The present invention provides, in one aspect, a lenticular reflective array. The array may be curved. Particularly, the reflectors of the array are each concave, so as to concentrate the light. This aspect of the invention is particularly advantageously
10 employed in a spatial light modulator projection system, since by folding the optical path the overall size of the projector can be kept small. Particularly advantageously, the lenticular lens/mirror combination is provided as a surface of a prism.

15 In another aspect, the invention provides a spatial light modulator system including a spatial light modulator device of the type in which incoming light is modulated in different angular directions depending
20 upon the picture signal applied to the modulator device, further comprising means for absorbing the unwanted light. Advantageously, the means comprises a black glass layer or the like. Particularly advantageously, the absorber converts the light into

- 6 -

heat and there is provided a heat sink for carrying the heat away.

In another aspect, the invention provides a spatial
5 light modulator display system in which the light beam
is filtered, prior to reaching the spatial light
modulator or modulators, to remove non visible
components thereof (particularly infrared, and
advantageously also ultraviolet). This prevents
10 overheating or chemical degradation of the optical,
mechanical or electrical component of the system.

Preferably, the filter comprises a reflecting coating
in the path of the light; advantageously, the
15 reflecting coating is provided on a diverging surface,
or is otherwise arranged such that rejected radiation
does not reflect back into the spatial light modulator
device again.

20 Preferably, the invention is provided for use with
spatial light modulator displays of the DMD type and
the optical arrangement is generally as described in
our Application No. PCT/GB92/00132.

- 7 -

Other aspects and preferred embodiments of the invention are as described or as claimed hereafter.

5 The invention will now be illustrated, by way of example only, with reference to the accompanying drawings in which;

10 Figure 1 shows schematically the structure of a spatial light modulator array device in an embodiment of the invention;

Figure 2 shows schematically the optical illumination of a portion of the device of Figure 1;

15 Figure 3 shows a diagrammatic perspective view of a color optical projection display system incorporating the array of Figures 1 and 2;

20 Figure 4a shows a scaled plan view of an optical assembly for use in the system of Figure 3;

Figure 4b shows a corresponding side elevation; and

- 8 -

Figure 4c shows a corresponding end elevation;

Figure 5a shows a plan view corresponding to Figure 4a
of the projection system of Figure 3 including the
5 assembly of Figure 4, and;

Figure 5b shows a corresponding side elevation;

Figures 6a and 6b correspond to Figures 5a and 5b with
10 the omission of the projecting lens, and show a second
embodiment of the invention;

Figures 7a and 7b correspond to Figures 6a and 6b and
show a third embodiment of the invention;

15

Figure 8 corresponds to Figure 7b and shows a fourth
embodiment of the invention;

Figures 9a and 9b correspond to Figures 6a and 6b and
20 show a fifth embodiment of the invention;

Figures 10a and 10b correspond to Figures 6a and 6b
and show a sixth embodiment of the invention; and

- 9 -

Figures 11a and 11b correspond to Figures 6a and 6b and show a seventh embodiment of the invention.

Referring to Figure 1, a deformable mirror device
5 array for use in the invention comprises an array of
typically $m \times n$ deflectable mirror devices; typically,
on the order of 500×500 devices for a low resolution
display or 2000×2000 devices for a high resolution
display. The array 20 is connected to an addressing
10 circuit 22 which receives the color signal from the
circuit 14, and addresses each of the respective
reflectors $M_{11} - M_{mn}$, as described in our earlier
International application number PCT/GB92/00002 dated
4 January 1992 (Agents ref. 3203299, incorporated
15 herein by reference). Each reflector is thus operated
between one of two reflection states corresponding to
different reflector positions; an "on" state in which
reflected light is directed in a first path 24a and an
"off" state in which light is directed in a second
20 path 24b. The second path 24b is disposed to lie away
from subsequent optical components of the system.
Thus, when viewed along the "on" path 24a, at an
instant, the array 20 displays a two dimensional
image, those modulators which are set to a first

- 10 -

deflection state appearing bright and those which are set to a second deflection state appearing dark.

Referring to Figure 2, the angle through which each reflector is deflected between the two states is relatively small and thus, in order to achieve good discrimination between the two states the incident light beam from the source 16 is directed towards the array 20 at an angle α (from the normal to the display) of around 20 degrees. When an individual reflector device M is lying parallel to the plane of the array 20, the incident beam is reflected at a corresponding angle of 20 degrees to the normal along path 24b, but when the control signal from the addressing circuit 22 sets the deflector M into a second deflection state at an angle to the plane of the array 20, the incident beam is reflected out along the normal angle to the array on the path 24a.

Referring to Figure 3, a white light source 16 comprising a high power lamp generates light along an incident light path which is for example in a plane normal to that of a display screen 4. For example, the light source 16 may be positioned above the display screen 4. A planar deformable mirror display

- 11 -

device 20b is positioned spaced apart from and in a plane parallel to the screen 10, and the light source 16 is arranged to illuminate the array 20b at an angle of 20 degrees to its normal axis. The array 20b is
5 arranged to deflect the incident beam to illuminate the screen 10 via a projection lens 40.

Positioned within the path of the incident and deflected rays are a pair of splitter/combiner mirrors
10 30a/18b, 30b/18a which are at an inclination, rotated about the vertical axis relative to the plane of the screen by some angle (typically between 20 and 70 degrees, and preferably 45 degrees) such as to reflect the incident beam to further deformable mirror
15 deflector arrays 20a, 20c.

The arrays 20a, 20c are positioned at a distance such that the optical path traversed from each array 20a - 20c to the screen 10 is the same. The first
20 splitter/combiner mirror reflects a blue light component beam to a deformable mirror display array 20a which is modulated in response to the blue color component of the picture to be displayed. Consequently, the reflected beam is deflected
25 vertically by 20 degrees but is substantially

- 12 -

horizontally unmodified. The splitter 30a transmits red and green wave length components substantially unattenuated.

5 The second splitter 30b reflects red wave lengths to a second deformable mirror device array 20c which is modulated in response to the red color component signal of the picture to be reproduced and consequently deflected 20 degrees vertically. The
10 second splitter 30b allows the green optical wave lengths to pass substantially unattenuated, to be deflected by a third deformable mirror device array 20b responsive to the green color component signal of the picture to be reproduced.

15 The modulated green beam passes unattenuated back through both splitter/combiners through the projection lens 10 and onto the screen 4. At the first splitter/combiner reached, 18a, the modulated beam
20 from the red digital mirror device array 20c is reflected into the same path as the modulated green beam and at the second splitter/combiner 30a/18b the modulated signal from the blue digital mirror device array is reflected back into the same path so that the

- 13 -

signal at the projection lens 1 comprises the recombined color signals.

Referring to Figure 4, the mounting of the DMD devices
5 20a-20c and the splitter/combiner mirror surfaces 30a, 30b is improved by providing a prism assembly 4 integrating the paths to the components. The prism comprises an input portion 4a, to which the beam from the light source 16 is coupled, having at its other
10 end an angled reflecting surface 5 (for simplicity, a 45 degree reflecting surface) redirecting the light beam to a second reflecting surface 6 (again, conveniently at 45 degrees). As shown, the light beam is therefore bent back on itself through a prism
15 portion 4d. An inner prism reflective surface 7 comprises a dichroic splitting/combining surface layer, which reflects blue light and transmits other bands. The reflected blue light passes up an inclined prism portion 4b. At the end face of the prism
20 portion 4b in use carries a DMD device modulated for blue light. The surface 7 thus corresponds to the selective mirror 30a of Figure 3.

- 14 -

Beyond the splitter/combiner 7, a second dichroic splitter/combiner surface 8 within the prism is positioned; this surface reflects red light down an inclined prism portion 4c on the end face of which a
5 DMD device controlled in dependence upon a red video picture signal is located.

Green light will thus pass through both the surfaces 7 and 8.

10

A reflective surface 12 (comprising, for example, a total internal reflection surface within the prism or a mirrored surface therein) directs the remaining transmitted green light out of the prism to the
15 position 9a of a third DMD device controlled in dependence upon the red component of a picture.

Mounting brackets 17a, 17b are provided at the front face 19 of the prism; the brackets are to mount the
20 prism assembly to the projection lens assembly 10.

The reflecting surfaces 5 and 6 are arranged to direct the rays from the lamp 16 downwardly at an angle of 20 degrees, for the reasons discussed in our earlier
25 Patent Application PCT/GB92/00132. The splitting/

- 15 -

combining surfaces 7 and 8 are inclined at a vertical angle of 10 degrees for reasons discussed in that earlier application, and incorporated herein by reference. The reflecting surface 12 is provided because in the arrangement shown in Figure 3, the modulated beams from the modulator arrays 20a, 20c are each reflected by a combined surface whereas that from the modulator 20b is transmitted, and hence the "handedness" of the green image is reversed relative to that of the other two; although it is possible to provide a modulator device 20b which operates in the opposite sense to the other two, it is preferred to provide a further reflection in the path to the green device 20b.

15

In between the portion of the prism 4d bounded by the reflected surface 12, and from which the portions 4b, 4c branch and the prism portion 4a, a layer 11 of black glass is provided at the boundary with portion 4d and, on the other face of the black glass layer, a copper heat sink 13 is bonded; the heat sink 13 projects out to mount to additional external heat sink components (not shown).

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- 16 -

The prism 4 is made of any convenient optical glass; for example, BK7 optical crown glass. The black glass layer 11 has a refractive index matched to that of the prism 4; in the above example, the black glass layer
5 may be type NG1 available from Schott.

Referring to Figure 5, the lamp 16 may comprise a Xenon arc lamp 1 positioned at the focus of a reflector 2 (for example a parabolic reflector,
10 although an ellipsoidal reflector might be used), which collects the rearward light from the lamp 1. The beam from the reflector 2 is directed through a condenser lens system 3 into the prism 4. The light from the lamp 1 and reflector 2 may contain
15 substantial power in the infrared and ultraviolet frequency bands; the former is undesirable because it heats the optical components, leading to potential misalignment and possibly adversely affecting the mechanical properties of the assembly and the
20 electrical properties of the DMD devices. The latter is undesirable because the prism assembly may comprise a number of components cemented together with an adhesive which the ultraviolet radiation may degrade.

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- 17 -

Accordingly, in an embodiment of the invention, the front convex surface 3a of the condenser lens 3 is coated with a coating which transmits visible light but reflects infrared and/or ultraviolet; the
5 advantage of providing the coating on the convex surface 3a is that the unwanted radiation is diffused rather than being focused back on to the lamp 1 and reflector 2, which might otherwise overheat.

10 Preferably, the front surface 15 of the prism 4 is also coated with a filter coating to further reduce the level of infrared and/or ultraviolet unwanted frequencies; these are then reflected back into the lens 3, from which they are diffused by the lens
15 coating 3a. Examples of such infrared and/or ultraviolet reflecting coatings are well known.

The light beam from the lamp assembly 16 comprises a generally circular section beam, whereas it is desired
20 to illuminate each of the DMD devices 20a-20c with a uniform rectangle of light. In one embodiment the surfaces 5, 6 accordingly provide reflecting apertures, surrounded by light absorbing regions of black glass of the above described type and backed by
25 copper heat sinks (not shown). The shape of the

- 18 -

reflecting apertures 5, 6 is not precisely rectangular; each shape is four sided each side being an interpolation between a straight line and a circular arc, in dependence upon the relative distances to the DMD device and the light source, so that the sides of the aperture on the surface 5 are more curvilinear than those on the surface 6 which is nearer to the DMD device. The appropriate shapes are readily derived by considering the ray paths through the prism assembly to each DMD from the lamp 16. The reflective apertures may further be arranged to absorb or transmit unwanted IR or UV wavelengths.

Each DMD device 20a-20c is typically a rectangular array with an aspect ratio corresponding to a desired television picture aspect ratio (e.g. 4:3), and if each is illuminated by a circular beam the edge of which touches the corners of the rectangle, 36% of the light from the beam does not illuminate the rectangle; by providing light absorbing regions on the reflecting surfaces 5, 6, the power in this unwanted light is absorbed prior to reaching the vicinity of the DMD devices and consequently does not cause unwanted heating of the electronic or optical components.

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- 19 -

As described with reference to Figure 3, after reflection and shaping of the beam at the surfaces 5, 6 the blue component of the beam is split at the surface 7 to illuminate the blue DMD 20b, and the reflected beam from those pixels which are in the "ON" state is directed back on a path to the dichroic surface 7 of which it is to be recombined. Likewise, the beam is further split and directed to the red DMD device 20c and green DMD device 20a; in the latter case, when viewed along the prism, the effect is as if the green DMD 20a were positioned at an unreflected point 9 shown in Figure 5b. Referring to that figure, light from pixels of the green DMD device 20a is therefore transmitted back through the prism portion 4c straight to the surface 19 which the projection lens 10 abuts. However, light reflected from pixels in the "OFF" state (which, for a black picture, will comprise a substantial proportion of the entire power of the beam from the light source 16) is directed to the black glass layer 11 where it is absorbed, and its energy converted to heat which is dissipated by the heat sink 13. This arrangement is therefore of substantial benefit in reducing unwanted heating of the assembly and consequent degradation of its optical, mechanical and electrical properties.

- 20 -

The absorbing layer 11 is positioned so that radiation from pixels in the "OFF" state of the red and blue DMD devices 20b, 20c is likewise directed to the black glass layer 11. In other constructions, of course,
5 separate absorbing layers could be provided for each device.

Referring to Figure 5b, the path taken by the light from the light source 16 to the projection lens 10
10 therefore runs forward to the surface 5, sideways to the surface 6, backward to the DMD 20a (or 20b or 20c) and then forward to the projection lens 10; the path is therefore folded back on itself and distance between the projection lens 10 and each DMD device is
15 short, which allows the numerical aperture of the projection lens 10 to be high. On the other hand, the entire assembly is kept compact by the folding of the light path.

20 Referring to Figure 6, the separate condenser lens 3 can be combined with the surface 15 of the prism portion 4a; this reduces the number of optical components, and hence simplifies the task of optical alignment and slightly increases the efficiency of the
25 apparatus by reducing the number of interfaces.

- 21 -

It would equally be possible to change the shape of the reflector 2 to condense the beam from the lamp 1; the object of the condensor is to reduce the aperture of the beam from the lamp 16 to the diameter of the DMD devices.

Referring to Figure 7, in one preferred embodiment of the invention the conversion of the beam shape between a circular section from the lamp 16 and a rectangular section illuminating each of the DMD array devices is performed, as disclosed in EP 0395156 and the prior art cited therein, by providing a pair of lenslet plates 50, 51 each comprising an array of rectangular lenslets having a curved (e.g. spherical) outer surface. The integrating lens 52 of the arrangement of Figure 5 of EP 0395156 is conveniently cemented to the face 15 of the prism 4. After passing through both plates 50, 51, the beam comprises a number of uniformly illuminated rectangles, one from each of the lenslets of the array 51; the lens 52 superimposes the rectangles to integrate them into uniform rectangular light beams focused on the DMD devices. The reflector 2 is parabolic, conveniently, to produce a collimated beam falling on the plate 50 but a lens could be

- 22 -

provided to do the same job, or any of the optical arrangements of EP 0395156 could be adopted.

5 The use of an array of lenses in this way provides a relatively low loss high efficiency conversion of the round beam from the light source 16 into a uniform rectangle.

10 An alternative arrangement provides the same effect by employing rectangular lenses with crossed axes in combination.

15 Referring to Figure 8, in a preferred embodiment the complexity, and associated inefficiency and alignment difficulties, of the arrangement of Figure 7 is reduced by shaping the front surface of the prism 4 to provide the plate 50 (by grinding or molding the face, or by cementing a plate 50 to the prism). The second
20 plate 51 may be substituted by shaping the reflective face 5 of the prism as shown in Figure 8 to provide an array of rectangular concave mirrors, combining the functions of the plate 51 with the reflector 5.

- 23 -

The convergence of the beam may be produced either by an appropriately shaped reflector 2, or by providing that the lens array 50 or reflector array 51 is on a curved surface.

5

Referring to Figure 9, in an alternative arrangement, the front lenslet array 50 is also replaced, by providing second concave reflector array at the reflective surface 6. Each reflector of the array 6
10 comprises a rectangle of the same aspect ratio, but smaller, than the corresponding reflector of the array 5.

15

Referring to Figure 10, in another embodiment of the invention the converging lens 3 and lens plates 50, 51 are combined as a lenticular lens array plate 52 comprising an array of lenslets, as before. However, each lenslet in this case is provided together with (for example, provided on the face of) a prism facet
20 at a facet angle which is normal to the light path at the center of the array 52, but which increases towards the edges of the array. Thus, the light from each lenslet is tilted inwardly towards the center axis of the array 52, by an angle calculated such that
25 when the beam falls on each DMD, the rectangular light

- 24 -

beam produced by each lenslet of the array 52 is superimposed to lie on the DMD array. Thus, a single optical component is employed to replace the two lens plates and integrating lens of EP 0395156.

5

Referring to Figure 11, in a preferred embodiment of the invention, the complexity of the arrangement of Figure 10 is further reduced by integrating the plate 52 with the surface 15 of the prism. The advantages of this arrangement are discussed above with reference to Figure 6.

10

The arrays of curved reflectors shown in Figures 8 and 9 could be provided on a curved surface, to converge or diverge the beam as desired.

15

The DMD devices 20a-20c are preferably coupled to the prism 4 by a liquid (for example an oil) to reduce interface losses. They are preferably provided with position adjusting mechanisms such as those of our PCT application GB93/00172 which claims priority from our earlier British Application No. 9201810.0 (Agents ref. 3203301) incorporated herein by reference.

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- 25 -

It will be appreciated that whilst the spatial light modulators described by way of example are of the type in which tilting of the mirror devices is achieved by means of electrostatic deflection of a torsion element, the invention is also applicable to other forms of spatial light modulators comprising an array of tiltable mirror devices each effective to direct an incoming light beam to either an "on" state or an "off" state. Examples of such alternative tiltable mirror devices include devices in which the tilting of the mirror devices is achieved using piezo-electric members, and devices in which the tilting of the mirror devices is achieved using the electrostatic depression of an elastomer.

- 26 -

CLAIMS:

1. A display projection apparatus comprising a light source, means for splitting light from the source into
5 different color component beams, and a plurality of spatial light modulators each comprising an array of tiltable mirror devices, characterised in that the light paths to said splitting means and modulators are provided as a single prism assembly to which said
10 modulators are mounted.
2. An apparatus according to claim 1, in which the surface of the prism which receives light from the source is convex so as to converge the light beam onto
15 each modulator device.
3. An apparatus according to either of the preceding claims including light absorbing means positioned to absorb light directed by any of the matrix elements of
20 the modulators when said matrix element is in an "off" position.
4. Apparatus according to claim 3, in which the light absorbing means includes means for dissipating heat
25 corresponding to the light absorbed.

- 27 -

5. Apparatus according to claim 3 or claim 4, in which the light absorbing means comprises a layer mounted to a face of the prism and having a refractive index corresponding to that of the prism.

5

6. An apparatus according to claim 5, in which the layer comprises a black glass layer.

10

7. An apparatus according to any one of the preceding claims including means for filtering the beam from the light source to reject unwanted spectral components prior to entering the modulators device.

15

8. An apparatus according to claim 7, in which the filter means are such as to reject infrared components.

20

9. An apparatus according to claim 7 or 8, in which the filter means are arranged to reject ultraviolet components.

25

10. An apparatus according to any of claims 7 to 9, in which the filter means are arranged on a convex surface so as to divergently reflect said unwanted components.

- 28 -

11. An apparatus according to any of claims 7 to 10, in which the filter means are arranged so as not to refocus rejected radiation onto the light source.
- 5 12. An apparatus according to any one of claims 7 to 11 in which the filter means are arranged on a surface of the prism assembly.
- 10 13. An apparatus according to any one of the preceding claims including means positioned between the light source and the spatial light modulator, for absorbing portions of the beam which would not illuminate the spatial light modulator.
- 15 14. An apparatus according to any one of the preceding claims including an optical component comprising a surface defining an array of curved reflectors bounded by polygonal edges, the component being arranged to direct light onto the prism assembly.
- 20 15. An apparatus according to claim 14, in which the reflectors are concave.

- 29 -

16. An apparatus according to claim 14 or claim 15, in which the array is curved.

5 17. An apparatus according to any one of claims 14 to 16, further comprising optical means for superimposing the rays from each polygonal reflector of said array onto the prism assembly.

10 18. An apparatus according to claim 17, further comprising an array of polygonal lenses aligned with said reflective array.

15 19. An apparatus according to any one of the preceding claims including a component for producing a polygonal optical beam comprising an array of polygonal optical lenses or reflectors each said lens or reflector being combined with a prism surface, said prism surfaces being progressively tilted, relative to a point on said array, so as to superimpose the polygonal beams
20 from each said lens or reflector into a single uniform polygonal spot at a predetermined distance from the array.

- 30 -

20. An apparatus according to any one of the preceding claims including a spatial light modulator light output system, and an output lens arrangement, in which the light path from the light source via the
5 or each modulator device to the lens is folded by reflectors to reduce the physical distance to the lens, permitting a wide aperture lens.

21. A projection video apparatus which comprises an
10 active matrix spatial light modulator device, of the type in which an element of said matrix directs light in a first direction when the element is in a first state and a second direction when the element is in a second state, characterised by light absorbing means
15 positioned to absorb light directed in said second direction.

22. A video projection display system comprising a light source, a spatial light modulator for modulating
20 the beam therefrom, and means for projecting the modulated beam to a display, characterised by means for filtering the beam from the light source to reject unwanted spectral components prior to the spatial light modulator device.

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- 31 -

23. An optical component comprising a surface defining an array of curved reflectors bounded by polygonal edges.

5 24. An optical component according to claim 23 in which the reflectors are concave.

25. An optical component according to claim 23 or claim 24 in which the array is curved.

10

26. A component for producing a polygonal optical beam comprising an array of polygonal optical lenses or reflectors each said lens or reflector being combined with a prism surface, said prism surfaces being progressively tilted, relative to a point on said array, so as to superimpose the polygonal beams from each said lens or reflector into a single uniform polygonal spot at a predetermined distance from the array.

15

20

27. A spatial light modulator light output system comprising a light source, at least one spatial light modulator, and an output lens arrangement, in which the light path from the light source via the or each modulator device to the lens is folded by reflectors

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- 32 -

to reduce the physical distance to the lens,
permitting a wide aperture lens.

28. A spatial light modulator projection system
5 comprising a light source generating a beam having a
first cross section and a spatial light modulator
illuminated by the beam and having a second,
different, cross section, characterised by means
positioned between the light source and the spatial
10 light modulator, for absorbing portions of the beam
which would not illuminate the spatial light
modulator.

29. An apparatus according to claim 14, in which the
15 optical component is integral with the prism
assembly.

$1/q$

FIG.1.

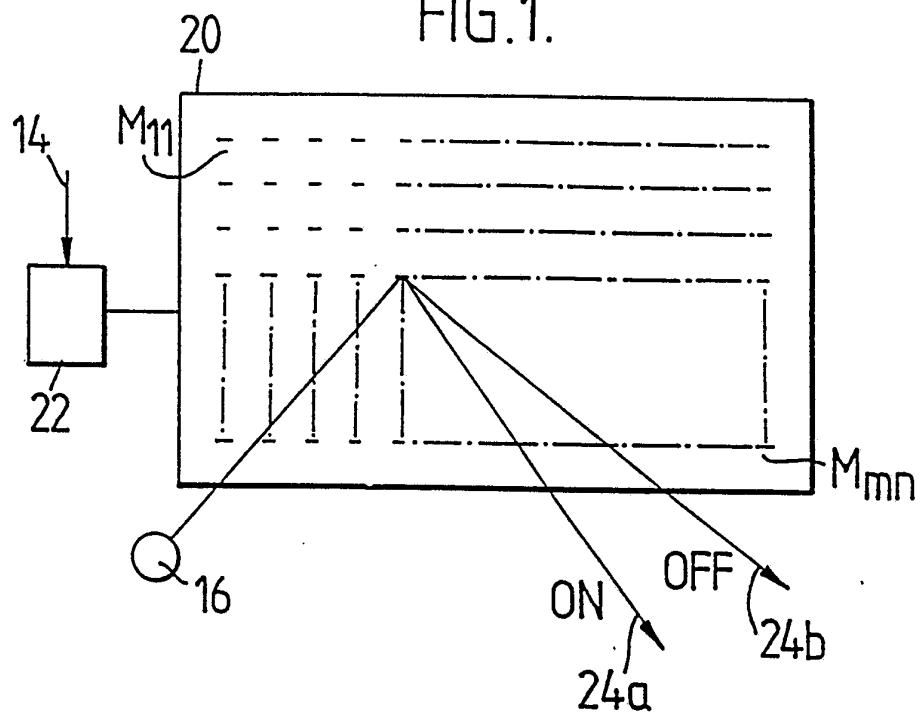
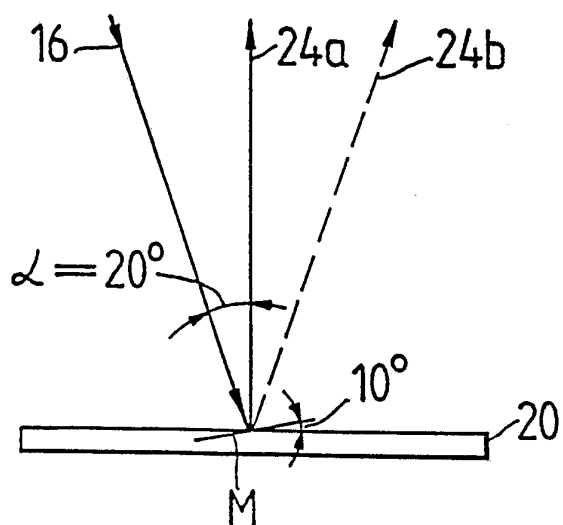
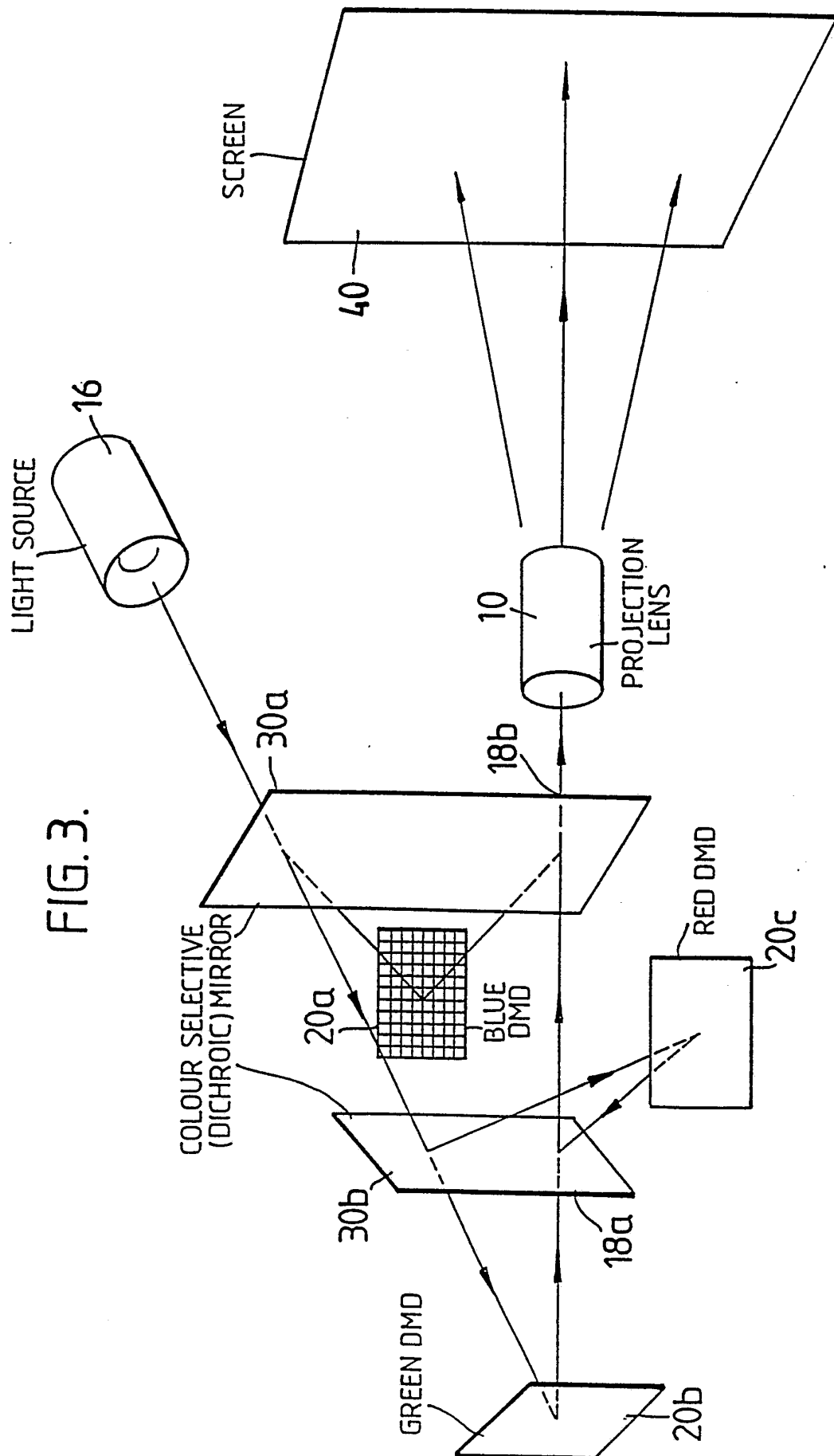


FIG.2.



2/9



3/9

FIG. 4a.

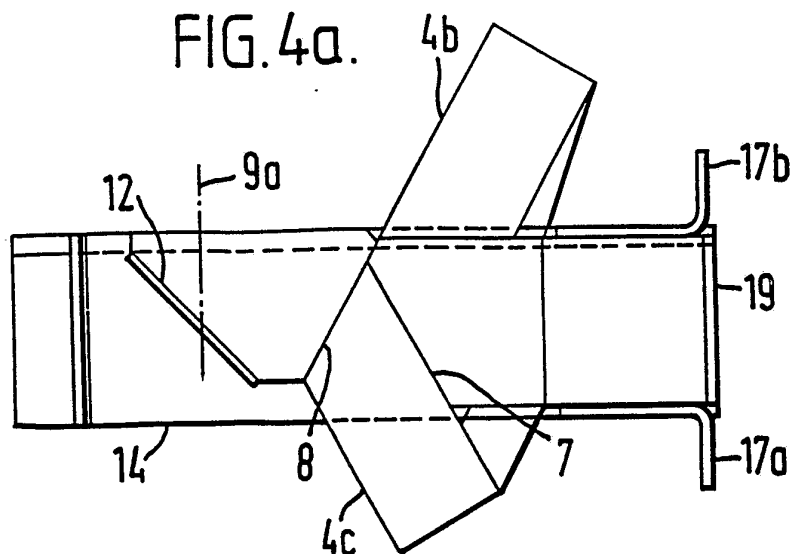


FIG. 4b.

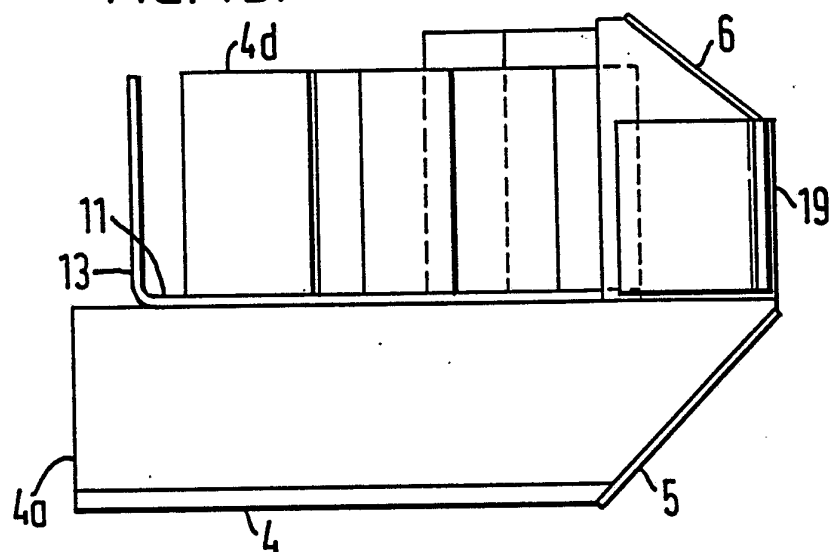
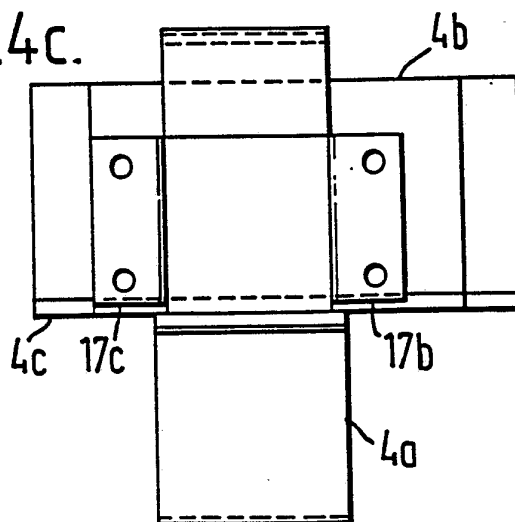


FIG. 4c.



4/9

FIG. 5a.

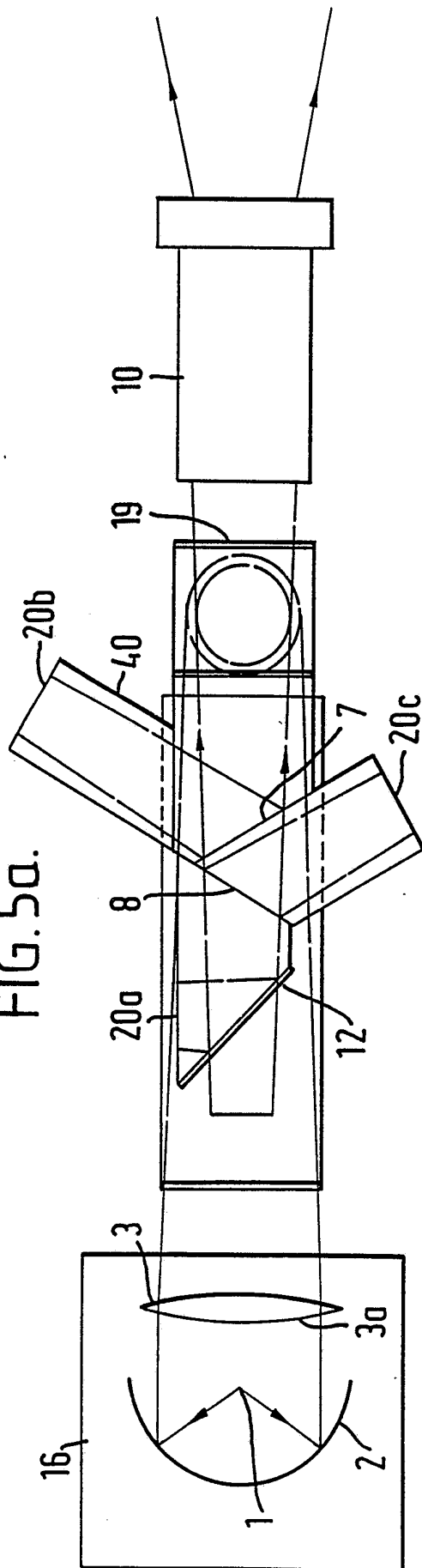
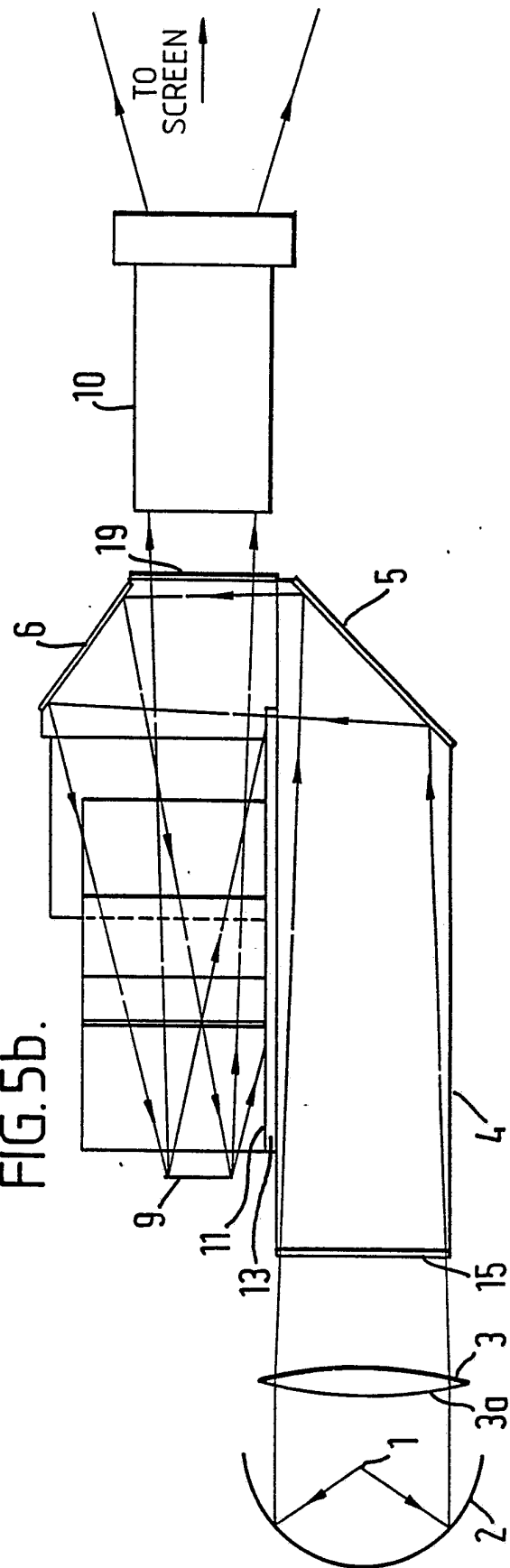


FIG. 5b.



5/9

FIG. 6a.

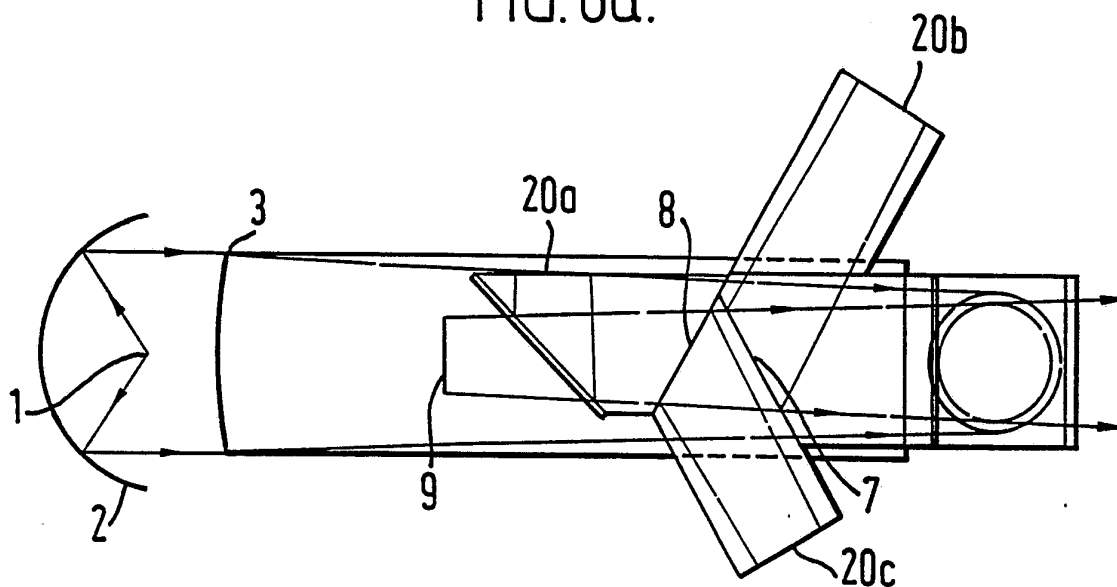
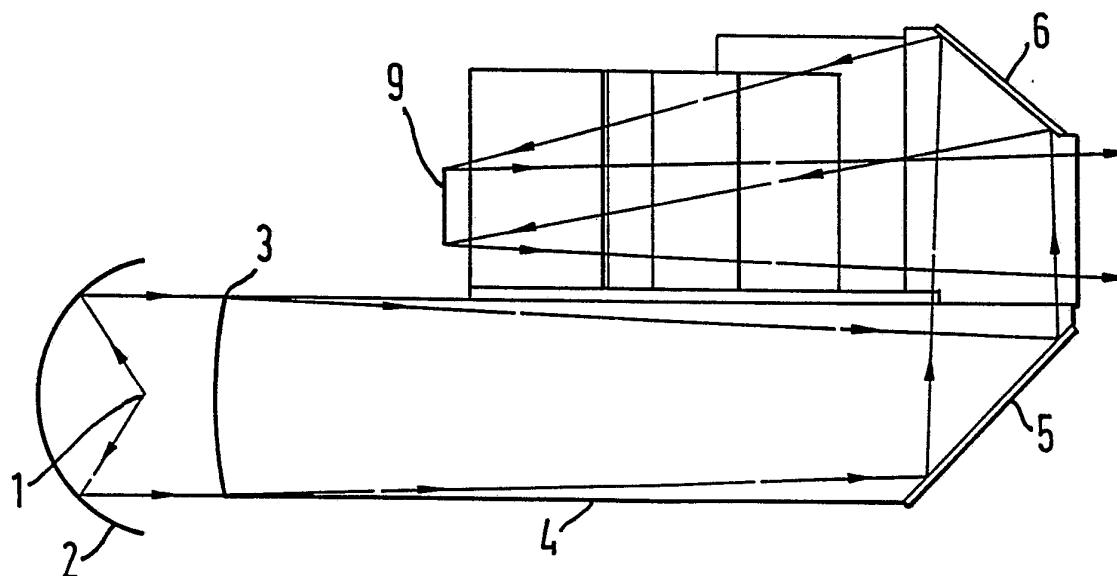


FIG. 6b.



6/9

FIG. 7a.

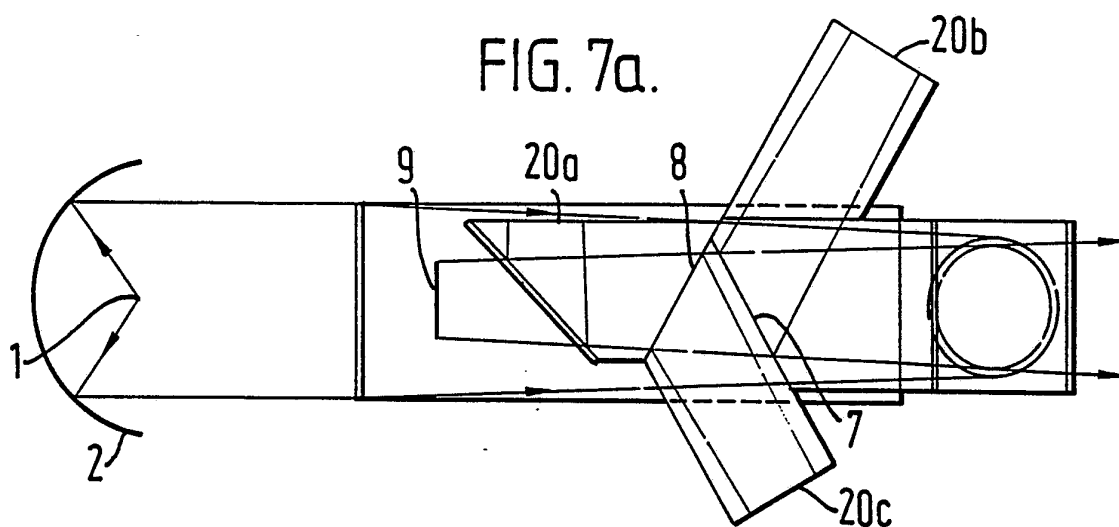


FIG. 7b.

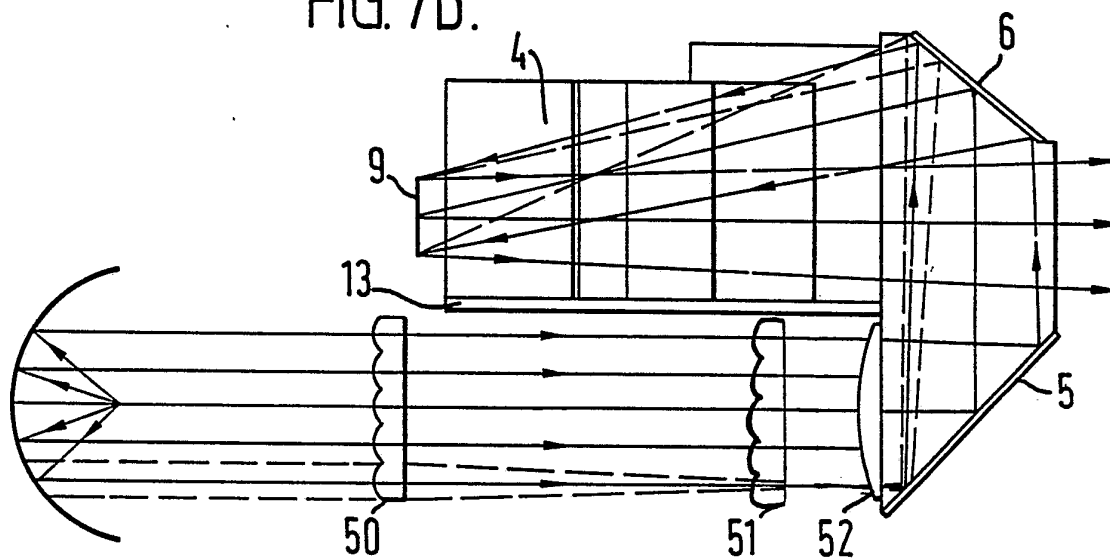
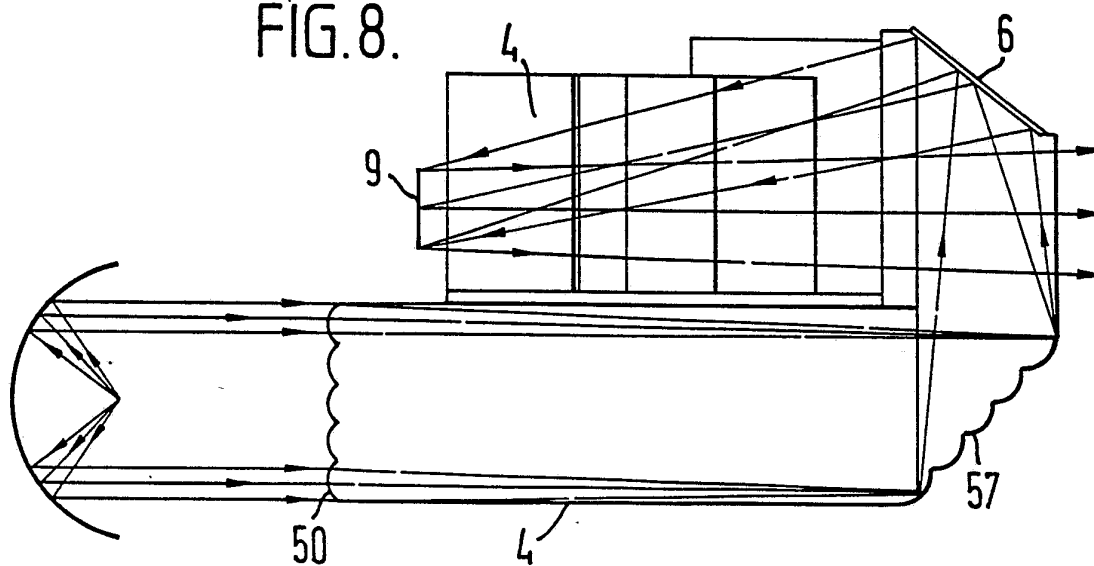


FIG. 8.



7/9

FIG. 9a.

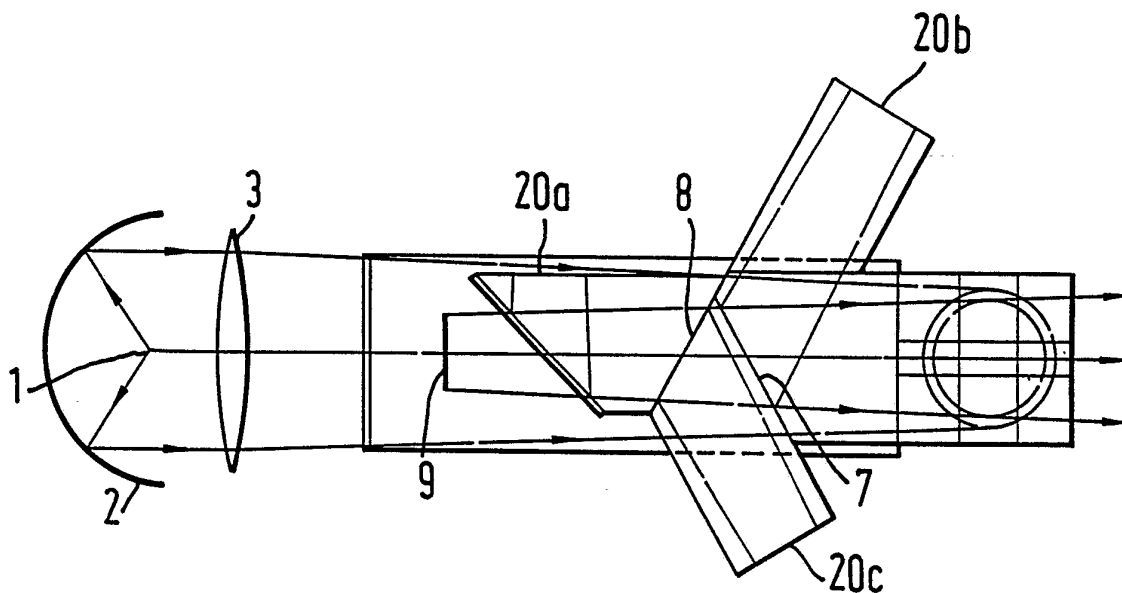
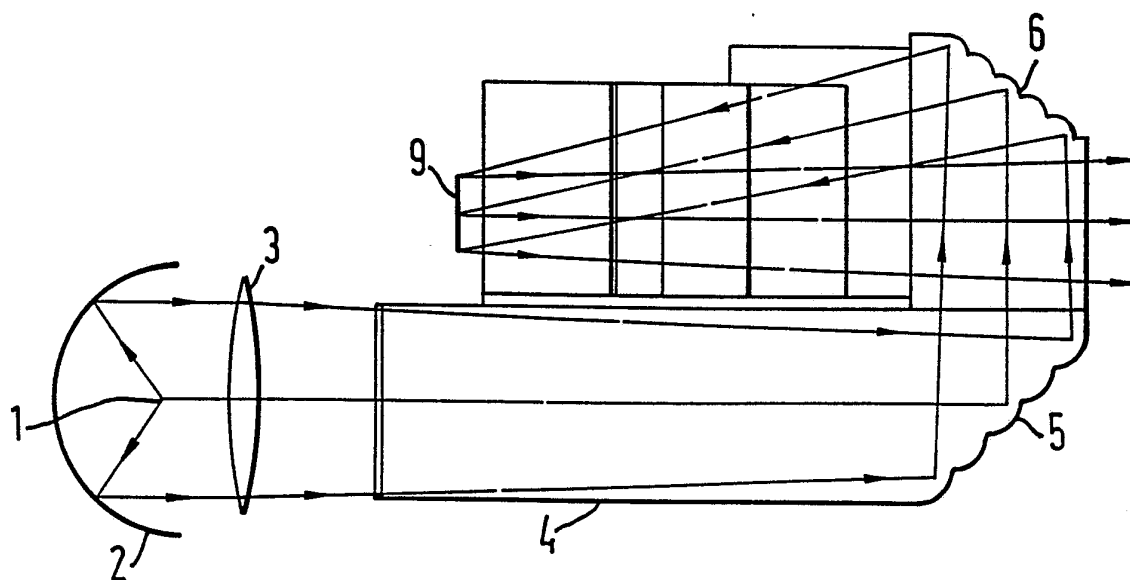


FIG. 9b.



8/9

FIG. 10a.

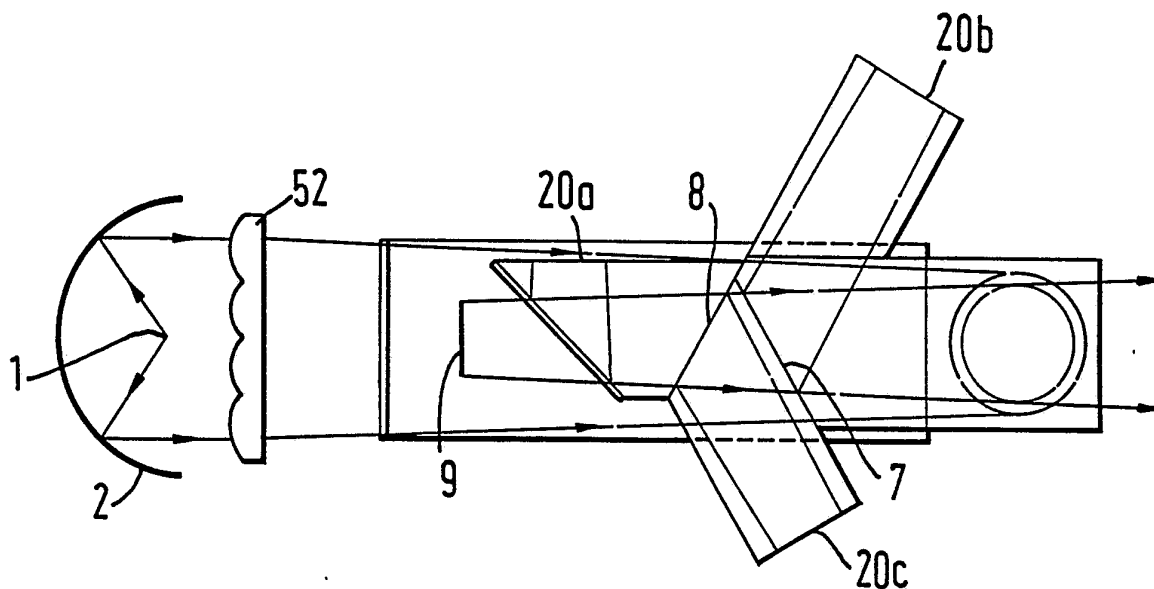
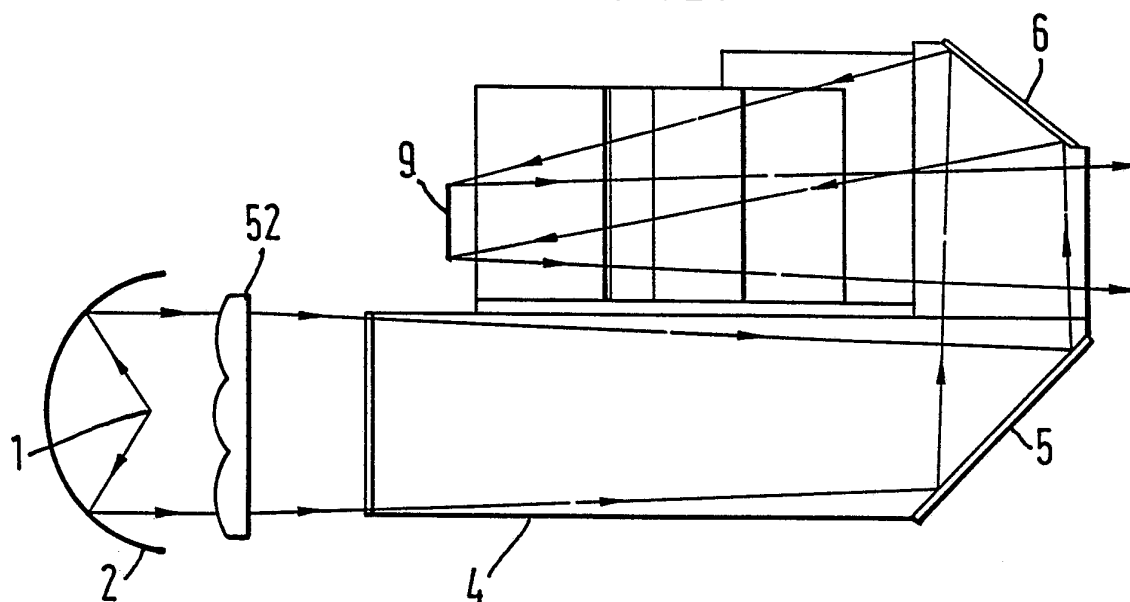


FIG. 10b.



9/9

FIG. 11a.

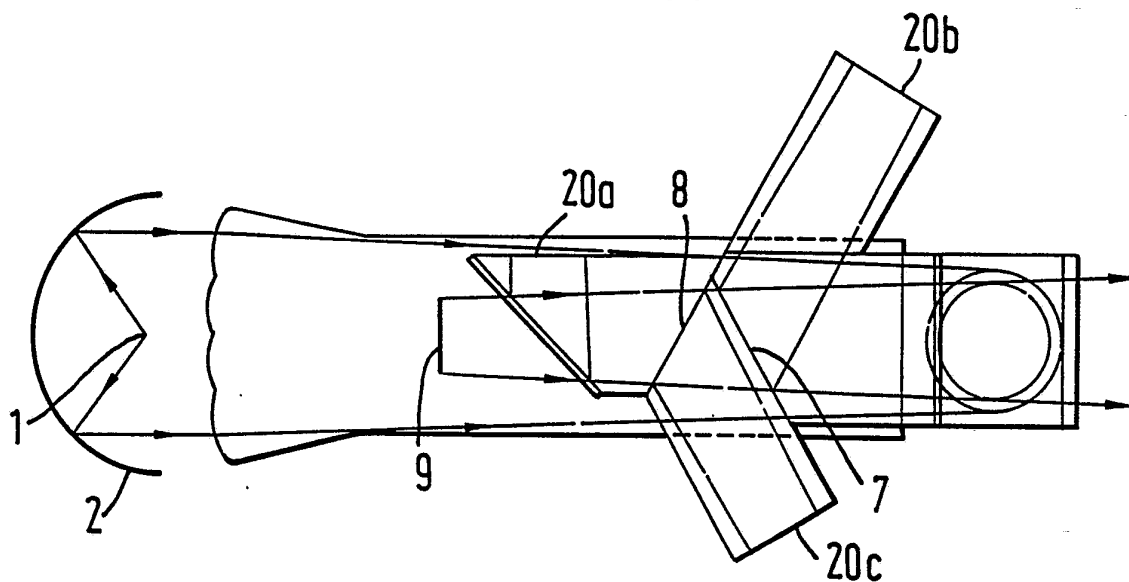


FIG. 11b.

