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(54) Title: SEPARATION SYSTEM, COMPONENTS OF A SEPARATION SYSTEM AND METHODS OF MAKING AND USING THEM

(57) **Abrégé/Abstract:**

Permeable polymeric monolithic materials are prepared in a column casing. In one embodiment, the permeable polymeric monolithic materials polymerized by the application of heat from an external source starting at a low temperature such as 40 degrees centigrade, depending on the mixture and size of the column, and continuing at a higher temperature, such as 60 degrees centigrade. The temperature at the start of the polymerization is low enough so as not to cause exothermal run-away conditions and to avoid high heat of reaction that would prevent a substantially constant temperature across the cross-section of the column. The higher temperature is used after sufficient monomer depletion has occurred and steric interference has increased so the polymerization reaction is sufficiently slow to avoid heat of reaction generation high enough to cause significant reduction in the homogeneousness of the pore sizes.



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(57) Abstract: Permeable polymeric monolithic materials are prepared in a column casing. In one embodiment, the permeable polymeric monolithic materials polymerized by the application of heat from an external source starting at a low temperature such as 40 degrees centigrade, depending on the mixture and size of the column, and continuing at a higher temperature, such as 60 degrees centigrade. The temperature at the start of the polymerization is low enough so as not to cause exothermal run-away conditions and to avoid high heat of reaction that would prevent a substantially constant temperature across the cross-section of the column. The higher temperature is used after sufficient monomer depletion has occurred and steric interference has increased so the polymerization reaction is sufficiently slow to avoid heat of reaction generation high enough to cause significant reduction in the homogeneousness of the pore sizes.

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SEPARATION SYSTEM, COMPONENTS OF A SEPARATION SYSTEM AND METHODS OF MAKING AND USING THEM

RELATED CASES

This application is a continuation-in-part of United States patent
5 application 10/607,080 filed June 25, 2003, in the names of Robert W.
Allington, Shaofeng Xie, Tao Jiang and Mingcheng Xu, for SEPARATION
SYSTEM, COMPONENTS OF A SEPARATION SYSTEM AND METHODS OF
MAKING AND USING THEM which is a continuation in part of United States
patent application 10/180,350 filed June 26, 2002, in the names of Shaofeng
10 Xie and Robert W. Allington for SEPARATION SYSTEM, COMPONENTS OF
A SEPARATION SYSTEM AND METHODS OF MAKING AND USING THEM.

BACKGROUND OF THE INVENTION

This invention relates to separation systems and their components and
15 more particularly to separation systems and components involving monolithic
permeable polymeric materials.

Monolithic macroporous materials such as for example organic
monolithic macroporous polymeric materials and monolithic silica packings are
known as components for separation systems such as chromatographic or
20 extraction systems. One class of such materials is formed as a monolithic
macroporous polymer plug or solid support produced by polymerizing one or
more monomers in a polymerization mixture that includes at least a porogen.
It is known for some polymerization mixtures, to include other materials such
as cross-linking agents, catalysts and small soluble polymers which can be

dissolved after polymerization to control the porosity, separation-effective opening size distribution and other characteristics. Moreover, the plug may be modified after being formed to add functional groups.

The plug or solid support is normally contained in a housing such as for example a chromatographic column or a pressure vessel. The portion of the housing where the plug resides acts as a reactor. In one prior art process for making monolithic columns, the polymerization mixture may be added to the column casing and polymerization initiated therein to form a macroporous polymeric plug or solid support within the walls of the column.

There are wide applications of these plugs or solid supports including gas, liquid and supercritical fluid chromatography, membrane chromatography and filtration, solid phase extraction, catalytic reactors, solid phase synthesis and others. The efficiency of the column or other container for the plug or solid support, the time required for a separation, and the reproducibility of the columns or other container for the plug or solid support are important commercial factors. The efficiency of separation systems such as chromatographic columns with porous polymer in them is related to both the selectivity of the column or other component containing the macroporous polymeric material and to zone spreading. Some of these factors are affected by molecular diffusion and velocity of the mobile phase in the plug or solid support during a separation process.

The manner in which molecular diffusion and velocity of the mobile phase affects column efficiency can be in part explained by showing the effect of these factors on Height Equivalent to Theoretical Plates (HETP), the

conventional designation of column efficiency. The van Deemter Equation shows the relationship between zone spreading, flow velocity and diffusion in terms of H (HETP) as follows:

$$H = A + B/u + Cu \text{ with low } H \text{ corresponding to high efficiency}$$

5 U= Flow velocity of the mobile phase

A=Radial Eddy Diffusion coefficient

B=Longitudinal Molecular Diffusion coefficient

C= The mass transfer coefficient

10 Molecular diffusion depends on the diffusion of the molecules but not on the packing of the bed. Eddy diffusion depends on the homogeneity of the packing of the particles.

Zone spreading from mass transfer can be minimized by using non-porous particles and porous particle with sizes smaller than 1.5 microns. However, packing with non-porous particles has extremely low surface area
15 which is detrimental to the purification process (as opposed to the analytical process) because the purification process requires high sample loading. The use of very small packed particles requires either high pressure which is difficult in most of the separation process using current instrumentation or low velocity, which can increase the time for a given separation (sometimes expressed in H
20 per minute).

The prior art separation systems that include as a component macroporous polymeric monolithic plugs or solid supports use plugs or solid supports formed from particles in the polymers that are larger than desired, less homogenous and include micropores. The large size of the particles and their

lack of homogeneity result in a lack of homogeneity in the separation-effective opening size distribution. The non-homogeneity of the sizes of the separation-effective openings and large amount of micropores in the prior art porous polymers contributes greatly to the zone spreading as shown by the van
5 Deemter Equation. The large number of micropores contributes to zone spreading by capturing sample and retaining it for a time. This may be stated conventionally as the non-equilibrium mass transfer in and out of the pores and between the stationary phase and the mobile phase.

The prior art plugs or solid supports formed of porous polymers have
10 lower homogeneity of the separation-effective opening sizes, less desirable surface features and voids in their outer wall created by wall effect and thus higher zone spreading and lower efficiency than desired in separation systems.

The prior art also fails to provide an adequate liquid mixture to a problem related to shrinkage that occurs during polymerization and shrinkage that
15 occurs after polymerization in some prior art porous polymers. The problem of shrinkage during polymerization occurs because monomers are randomly dispersed in the polymerization liquid mixture and the polymers consist of orderly structured monomers. Therefore, the volume of the polymers in most of the polymerization is smaller than the volume of the mixed monomers. The
20 shrinkage happens during the polymerization in all of the above preparation processes. One of the problems with shrinkage after polymerization occurs because of the incompatibility of a highly hydrophilic polymer support with a highly hydrophilic aqueous mobile phase or other highly polar mobile phase such as for example, a liquid mixture having less than 5-8 percent organic

solvent content.

Shrinkage of the porous polymeric materials used in separation systems and their components during polymerization results in irregular voids on the surface of the porous polymers and irregularity of the separation-effective opening sizes inside the polymer, which are detrimental to the column efficiency and the reproducibility of the production process. One reason the column efficiency is reduced by wall effect is that wall effect permits the sample to flow through the wall channels and bypass the separation media. One reason the reproducibility of the production process are reduced by wall effect is the degree of wall effect and location of the wall effect are unpredictable from column to column.

The columns with large channels in the prior art patents cited above have low surface area and capacity. The low capacities of the columns are detrimental for purification process which requires high sample loadings. In spite of much effort, time and expense in trying to solve the problems of shrinkage, the prior art fails to show a liquid mixture to reduced capacity.

Because of the above phenomena and/or other deficiencies, the columns prepared by the above methods have several disadvantages, such as for example: (1) they provide columns with little more or less resolution than commercially available columns packed with beads; (2) the separations obtained by these methods have little more or no better resolution and speed than the conventional columns packed with either silica beads or polymer beads, particularly with respect to separation of large molecules; (3) the wide pore distribution that results from stacking of the irregular particles with various

shapes and sizes lowers the column efficiency; (4) the non-homogeneity of the size effective openings resulting from the non-homogeneity of the particle sizes and shapes in the above materials contribute heavily to the zone spreading; (5) the large amount of micropores in the above materials also contributes greatly to the zone spreading; and (6) shrinkage of the material used in the columns reduces the efficiency of the columns. These problems limit their use in high resolution chromatography.

U.S. Patent 5,453,185 proposed a method of reducing the shrinkage by reducing the amount of monomers in the polymerization mixture using insoluble polymer to replace part of the monomers. This reduces the shrinkage but is detrimental to the capacity and retention capacity factor of the columns which require high amount of functional monomers. There is nothing mentioned in these patents regarding the detrimental effect of shrinkage on resolution and the resulting irregular voids on the surface of the porous polymer and irregularity of the separation-effective openings inside the polymer, which are detrimental to the column efficiency and the reproducibility of the production process.

Prior art European Patent 1,188,736 describes a method of making porous poly(ethylene glycol methacrylate-co-ethylene glycol dimethacrylate) by *in situ* copolymerization of a monomer, a crosslinking agent, a porogenic solvent and an initiator inside a polytetrafluoroethylene tube sealed at one end and open at the other end. The resulting column was used for gas-liquid chromatography. This prior art approach has the disadvantage of not resulting in materials having the characteristics desirable for the

practical uses at least partly because it uses polymerization in a plastic tube with an open end.

U.S. Patents 2,889,632; 4,923,610 and 4,952,349 disclose a method of making thin macroporous membranes within a sealed device containing two plates and a separator. In this method the desired membrane support was punched out of a thin layer of porous polymer sheet and modified to have desired functional groups. The layers of porous sheets are held in a support device for "membrane separation". These patents extended the method described in European patent 1,188,736 to prepare a porous membrane and improve the technique for practical applications in membrane separation. The resulting material is a macroporous membrane including pores from micropores of size less than 2 nanometers to large pores. The size of the particles of the polymer is less than 0.5 micrometers. The separation mechanism of membrane separation is different from that of conventional liquid chromatography.

This porous material has several disadvantages, such as for example: (1) the thinness of the membrane limits its retention factor; and (2) the pores formed by these particles are small and can not be used at high flow rate with liquid chromatography columns that have much longer bed lengths than the individual membrane thicknesses. The micropores and other trapping pores trap molecules that are to be separated and contribute to zone spreading. The term "trapping pore" in this specification means pores that contribute to zone spreading such as pores ranging in size from slightly larger than the molecule being separated to seven times the diameter of the pore being separated.

U.S. Patents 5,334,310; 5,453,185 and 5,728,457 each disclose a method of making macroporous poly(glycidyl methacrylate-co-ethylene glycol dimethacrylate) polystyrene *in situ* within sealed columns. This method extends the methods described in both the European patent 1,188,736 and U.S. patents 2,889,632; 4,923,610 and 4,952,349 for preparing liquid chromatography columns for the separation of proteins. U.S. patents 5,334,310; 5,453,185 and 5,728,457 profess the intention of improving the column efficiency by removing the interstitial volume of conventional packed columns having beads. The plugs formed according to these patents have a separation-effective opening size distribution that is controlled by the type and amount of porogens, monomers and polymerization temperature. The macroporous polymers consist of interconnected aggregates of particles of various sizes which form large pore channels between the aggregates for the transport of the mobile phase. Among the aggregates or clusters there exist small pores for separations. The small particles are formed from tightly packed extremely small particles ca 100-300 nanometers.

The materials made in accordance with these patents have a disadvantage in that the micropores within or between these particles physically trap the sample molecules and degrade the separation. Although these patents claim that there are no interstitial spaces in the monolithic media as in the packed bed with beads, the large channels between the aggregates and interconnected particles actually cause the same problem as the interstitial spaces between the beads in conventional packed columns with beads. The large channels formed from various sizes of aggregates or clusters are

inhomogeneous and provide random interstitial spaces, even with narrow particle size distribution. Because of the random interstitial spaces the column efficiency is poor.

U.S. patents 5,334,310; 5,453,185 and 5,728,457 disclose the preparation of the separation media inside a column with cross section area from square micrometers to square meters. The processes disclosed in these patents have some disadvantages. Some of the disadvantages were disclosed by the inventors named in those patents in 1997 in *Chemistry of Materials*, 1997, 9, 1898.

One significant disadvantage is that larger diameter (26 mm I.D.) columns prepared from the above patented process have a separation-effective opening size distribution that is too irregular to be effective in chromatography separation. The irregular distribution of the sizes of the separation-effective openings is caused by the detrimental effect of polymerization exotherm, the heat isolating effect of the polymer, the inability of heat transfer, autoaccelerated decomposition of the initiator and concomitant rapid release of nitrogen by using azobisisobutyronitrile as initiator in a mold with 26 mm diameter. It has been found that the temperature increase and differential across the column created by the polymerization exotherm and heat transfer difficulties results in accelerated polymerization in large diameter molds such as for example molds having a diameter of more than 15 mm and in a temperature gradient between the center of the column and the exterior wall of the column which results in inhomogeneous pore structure. It was suggested in this article that the problem might be reduced by slow addition of

polymerization mixture. This helps to solve the problem partly but does not solve the problem completely. There is still a temperature gradient for the larger diameter columns, which result in a lack of homogeneity in the separation-effective opening size distribution.

5 This problem was also verified by theoretical calculations in the publication of *Analytical Chemistry*, 2000, 72, 5693. This author proposes a modular approach by stacking thin cylinders to construct large diameter columns for radial flow chromatography. However, sealing between the discs to form a continuous plug is difficult and time consuming.

10 U.S. patents 5,334,310; 5,453,185 and 5,728,457 disclose the material of weak anion exchange and reversed phase columns. The weak anion exchanger prepared had low resolution, low capacity, low rigidity, slow separation and very poor reproducibility. The reversed phase media has very little capacity, non-ideal resolution, and very poor reproducibility. They can not
15 be used in mobile phase with high water content such as less than 8% acetonitrile in water due to wall channeling effect resulting from shrinkage of the very hydrophobic media in this very polar mobile phase. This media is also compressed during separation and result in excess void volume in the head of the column. The above patents provide little guidance on how to prepare a
20 weak cation exchanger, strong cation exchanger, strong anion exchanger, normal phase media and hydrophobic interaction media. These media based on membrane, beads or gels are known. However, the known preparation is performed off-line and can not be used for *in situ* preparation of monolithic columns. The monolithic membranes prepared according to U.S. patents

2,889,632; 4,923,610 and 4,952,349 have low capacity and resolution.

It is known from Peters et al., "Preparation of Large-Diameter 'Molded' Porous Polymer Monoliths and the Control of Pore Structure Homogeneity", *Chemistry of Materials* v. 9, n7, July 1997 to polymerize the monolithic plug slowly in an effort to avoid temperature gradients. In one embodiment, the temperature is held at a constant low temperature of 55 degrees Centigrade or at 60 degrees Centigrade. In another embodiment, the rate of polymerization is maintained low and exothermal heat reduced by gradually adding monomer and thus limiting the rate of reaction.

These processes have the disadvantage of providing inhomogeneous separation-effective opening size distribution, low stiffness of the polymer plug and separation-effective openings that are impractically large for many liquid chromatography separations. The low temperature results in reduced cross linking and, for some polymers, results in a plug that is not sufficiently stiff.

This publication also describes the process by which the authors obtained information about the internal temperature of the columns during polymerization. That process included the embedding of temperature measuring devices in the column.

SUMMARY OF THE INVENTION

Accordingly, it is an object of the invention to provide a novel separating system having synergistic relationships with a polymer having separation-effective openings.

It is a further object of the invention to provide a novel chromatographic

column.

It is a still further object of the invention to provide a novel apparatus for making a chromatographic column.

5 It is a further object of the invention to provide a novel method for forming chromatographic columns.

It is a still further object of the invention to provide a novel permeable monolithic medium.

It is a still further object of the invention to provide a permeable monolithic column with improved resolution.

10 It is a still further object of the invention to provide a permeable monolithic column with improved capacity.

It is a still further object of the invention to provide a column with improved flow rate.

15 It is a still further object of the invention to provide a column with reduced tendency to swell when used with aqueous solvent.

It is a still further object of the invention to provide a column with improved reproducibility.

20 It is a still further object of the invention to provide a novel technique for the formation of permeable monolithic columns with controlled size of the separation-effective openings selected for the purpose of improving capacity or resolution or flow rate.

It is a still further object of the invention to provide a novel method of preparing large diameter columns for preparative separations.

It is a still further object of the invention to provide a novel large diameter column.

It is a still further object of the invention to provide a method of preparing polymeric materials including permeable polymer support using irradiation methods.

It is a still further object of the invention to provide a novel weak anion exchange column.

It is a still further object of the invention to provide a novel reverse phase column.

It is a still further object of the invention to provide a high performance strong anion exchange column.

It is a still further object of the invention to provide a high performance weak cation exchange column.

It is a still further object of the invention to provide a high performance strong cation exchange column.

It is a still further object of the invention to provide a high performance normal phase column.

It is a still further object of the invention to provide a method of avoiding a reduction in the quality of a separating medium caused by shrinkage during polymerization or swelling of the medium during washing or during separation.

It is a still further object of the invention to provide a chromatographic system in which an array of columns, in which the columns are very close in characteristics, are operated together.

It is a still further object of the invention to provide a novel process for

making monolithic permeable solid support for applications in chromatography including liquid, gas and supercritical fluid chromatography, electrochromatography, catalytic reactor, filtration or others requiring permeable polymer supports or solid permeable polymer holders adjacent or positioned at least partly horizontally from a sample .

It is a further object of the invention to provide a novel high resolution media and novel method of obtaining it.

It is a further object of the invention to provide a novel permeable solid support with homogeneous separation-effective opening size distribution resulting from more homogeneous size and shape of the interconnected aggregated particles.

It is a further object of the invention to provide a novel permeable solid support with less or no micropores.

It is a further object of the invention to provide a novel permeable solid support with no voids on the wall of the polymeric support.

It is a further object of the invention to provide a novel method for improving the capacity of monolithic chromatography media.

It is a still further object of the invention to provide a permeable monolithic column with improved resolution.

It is a still further object of the invention to provide a novel technique for the formation of permeable monolithic columns with controlled size separation-effective openings selected for the purpose of improving capacity or resolution or flow rate.

It is a still further object of the invention to provide a method of preparing

large diameter columns for preparative separations.

It is a still further object of the invention to provide a high performance catalytic reactor.

5 It is a still further object of the invention to provide a high performance solid phase extraction bed.

It is a still further object of the invention to provide a novel permeable monolithic medium with covalently bonded particles having a controlled minute thoroughly convoluted surface configuration but with few or no micropores.

10 It is still a further object of the invention to provide a monolithic chromatographic bed with negligible non-uniformities due to thermal effects during polymerization reaction.

It is a still further object of the invention to provide a novel method for controlling polymerization in a chromatographic column with reliance on conduction of heat into the column.

15 It is still a further object of the invention to control the rate of polymerization, and resulting thermal gradients, by means of controlled radiation impinging on the bed.

20 It is still a further object of the invention to control polymerization with a relatively safe radiation source such as those providing medium energy X-ray (e.g. below 200 keV), UV or visible radiation.

It is a still further object of the invention to provide a permeable, high capacity, column with few or no micropores.

It is a still further object of the invention to provide a method of preparing columns with small diameters from nanometers to millimeters.

It is a still further object of the invention to provide a method of preparing chromatographically uniform columns with medium diameters up to 100 mm and large diameter columns up to 1000 mm or larger.

5 It is a still further object of the invention to provide a method of polymerization in which the effect of temperature gradients on homogeneity of the separation-effective openings in a porous polymer are minimized.

It is a still further object of the invention to provide a method of polymerization in which run-away temperatures of exothermic reactions are avoided.

10 It is a still further object of the invention to provide a method of polymerization in which the highest temperature within the polymer mixture is lower than the self-sustaining run-away temperature but the temperature is at least some of the time within the reaction range of the polymer mixture.

15 It is a still further object of the invention to provide a novel method of using energy conduction to form large monolithic columns.

It is a still further object of the invention to provide a novel method of polymerizing in which the temperature is maintained at a level that avoids significant differences in temperature across the cross-section of a monolithic plug during polymerization but provides sufficient energy from heat to permit
20 adequate cross linking during the later states of polymerization and a high degree of completion of polymerization in a reasonable amount of time without an exothermic runaway temperature being reached.

It is a still further object of the invention to provide a novel method of preparing chromatography columns using step temperature increases and

gradient (continuous, gradual changes rather than abrupt changes) temperature increases to prepare monolithic columns.

It is a still further object of the invention to provide a novel method of controlling the rate of heat generation and dissipation during the polymerization process.

It is a still further object of the invention to provide a method for improving the rigidity of polymers.

In accordance with the above and further objects of the invention, a polymerization mixture is polymerized in place with a porogen or solvent to form a polymer plug that has separation effective openings. In this specification, "separation-effective openings" means pores or channels or other openings that play a role in separation processes such as for example chromatography. The term "pores" generally means openings in the particles that are substantially round and may be through pores passing through particles (through pores) or openings into the particles or in some cases, openings into or through aggregates of particles. By being substantially round in cross-section, it is meant that the pores are not perfect circles and for example may be bounded by sectors of imperfect spheres with the pores being the open spaces between the adjacent spherical surfaces. Some other terms are defined below as they are used in this specification. Separation factors includes those factors that effect retention and capacity or other factors that play a role in separation processes. The term "macroporous" in this specification is given its usual meaning in referring to monolithic materials in separation systems. Its usual meaning refers to pores or other voids between globules of particles, which

pores or other voids have a diameter of over 50 nm regardless of the length of an opening, rather than its literal connotation that would limit the openings to pores with a substantially circular cross section and no cross sectional dimension substantially longer than the other.

5 The term "permeable" in this specification shall be interpreted in the same manner as the term "macroporous" is most commonly used with reference to monolithic materials in the separation arts but is used in preference to the term "macroporous" to distinguish materials having channels and other openings as well as pores from those having only one or the other and to permit
10 the use of adjectives with the word "permeable" to distinguish non-porous permeable materials from those containing pores to avoid confusion with the literal meaning of the term "macroporous". In this specification the term "permeable non-porous" describes media having openings such as channels or the like but not containing pores as defined above. The run-away
15 temperature is the temperature at which the reaction continues without the addition of heat because the heat generated by the reaction maintains the temperature above the reaction temperature independently of the added heat so that the reaction becomes self-sustaining. The words "temperature-time moderated" means monolithic material that has been polymerized at
20 temperatures below the run away temperature but at a temperature high enough for a time long enough to accomplish the polymerization to a high degree of completion with the polymer still having the desired characteristics such as adequate stiffness, appropriate separation-effective opening sizes, homogeneous separation effective-opening size distribution and the like. This

is often related to the rate of polymerization so that temperature-time moderation is accomplished by controlling the rate of polymerization by controlling externally applied heat.

One constraint on the temperature-time moderation polymerization of particular concern is that the time and temperature of polymerization be appropriate to form the desired amount of cross linking for the stiffness or lack of stiffness necessary for the particular application. This constraint is satisfied in the preferred embodiment by balancing a number of polymerization-affecting factors such as the rate energy is introduced into the polymerization mixture, the amount of activated initiator or activator, the amount of monomer available and the temperature needed for adequate cross-linking in view of the type of polymer and monomer and the interference with bonding such as the steric hindrance or blocking by other molecules after substantial polymerization has taken place.

One way of balancing the polymerization-affecting factors is to control the rate at which energy is introduced into the mixture and/or the way energy is introduced into the mixture from an external source such as heat energy from a water bath being introduced by conduction at the surface of the mixture or X-ray energy being introduced into the mixture by radiation. In the preferred embodiment, heat is introduced at the surface of the mixture with a water bath. The exothermic heat is controlled by controlling the rate of reaction, which in turn, is controlled by controlling the temperature of the water bath. The temperature of the water bath in this embodiment controls the rate of exothermic heat emission to a level that, considering the rate of heat dissipation

from the mixture and the heat entering the mixture from the water bath, keeps the temperature below the self-sustaining reaction temperature but high enough to obtain a substantially complete reaction with adequate cross-linking in a reasonable time.

5 In one embodiment, the heat emitted by the reaction is controlled by the temperature of the water bath. It can be controlled by the temperature of the water bath because the exothermic heat emitted by the reaction is generally proportional to the rate of the reaction and increases with an increasing rate. The rate of reaction can be increased by adding heat to the water bath to
10 increase the temperature of the water bath, either gradually (gradient temperature control) or step by step as the polymerization proceeds. For example, in gradient temperature control, the temperature is increased at a rate that keeps the rate of increase of polymerization constant in view of the effects that impede polymerization such as the exhaustion of monomers so that the
15 reaction rate is so low as to preclude run-away polymerization and low enough to avoid thermal gradients that otherwise could cause lack of uniformity in the characteristics of the column. It is still possible with these constraints to control the reaction to provide the desired characteristics, even for very large columns.

20 With this technique, the enthalpy of the mixture, which in the preferred embodiment is determined by the temperature, is increased to a predetermined level that activates an initiator and provides polymerization at a rate that can provide a temperature-time moderated polymer by the planned procedure without reaching the self-sustaining reaction rate. This predetermined level of enthalpy is referred to in this specification as the control-initiation point. After

reaching the control-initiation point, the reaction rate is kept substantially constant up to the level of polymerization at which the temperature may be increased in one or more steps, if desired, to a higher enthalpy until completion of the polymerization, which is commonly 95 percent or higher. The point at which the level of polymerization is sufficient so that the temperature may be increased to a level desired to achieve temperature-time moderation is referred to as the safe-point or safe-points, where there is more than one step increase or a large increase in temperature.

In one embodiment of this invention, shrinkage during polymerization is compensated for and in another embodiment of this invention, swelling after polymerization, which might otherwise later result in shrinkage is avoided. Shrinkage results in enlarged voids on the polymer surface and may result in a lack of homogeneity of pore or other separation-effective opening size distribution inside the polymer. The voids are believed to be created by decreased volume of orderly structured polymer compared to the volume of monomers prior to polymerization when created during polymerization. The voids are mostly located in between the column wall and polymer due to the difference in surface free energy. The voids are probably occupied by the nitrogen gas generated by azobisisobutyronitrile (AIBN), which is a common initiator for the polymerization.

In a first embodiment, the compensation for shrinkage is accomplished by applying sufficient pressure during polymerization to create uniformity in the distribution of separation-effective openings and to avoid wall effect voids. This pressure has been found to also control particle size and the nature and shape

of the openings in the plug to some extent. Maintaining the column at atmospheric pressure during polymerization to accommodate shrinkage does reliably prevent the formation of voids. Generally 250 psi pressure is used for convenience but higher and lower pressures have been used successfully. The voids are removed when the plug stops shrinking when put under amounts of pressure. In a second embodiment, shrinkage that otherwise would occur after polymerization is avoided. For example, some plugs tend to expand when exposed to some liquid mixtures such as organic solvent and then shrink later such as during a separating run in aqueous mobile phase, causing voids. In these embodiments, shrinkage is prevented by holding the column from shrinkage when exposed to the liquid mixtures. The application of pressure is one method of preventing shrinkage during exposure to the aqueous liquid mixtures. Other methods for compensating for shrinking and/or swelling, for reducing shrinking or for avoiding shrinking are also used as described in greater detail below. It is believed that the externally applied pressure overcomes uneven forces internal to the reacting polymerization mixture and between the polymerization mixture and internal wall of the column to maintain homogeneous separation effective factors, separation-effective opening size and distribution and uniform continuous contact of the polymer to the internal wall of the column.

Surprisingly, some types of polymer plugs contain no pores if they are subject to pressure during polymerization to compensate for shrinking or in the case of some reversed phase columns to compensate for shrinkage when exposed to hydrophilic liquid mixtures such as for example in the aqueous

mobile phase Instead, they contain solid particles ca 2 micrometers in diameter, covalently bonded together with relatively large flow channels between them (separation-effective openings). The surprising thing is that, although these particles have no pores, the chromatographic capacity of the plug is high. This is believed to happen because of the unexpected formation of ca 50-200 nm deep and wide grooves or corrugations and other odd surface features. A typical particle resembles a telescopic view of a very small asteroid.

The pressure applied during polymerization is selected in accordance with the desired result and may be, for example, a linearly increasing pressure, a constant pressure or a step pressure gradient. In one embodiment, separation-effective opening size is controlled by selecting the type and proportion of porogen that generates the pores during polymerization and the porogen that must be washed out of the plug after polymerization. This proportion is selected by trial runs to obtain the desired characteristic. The total amount of porogen is also selected.

In another embodiment, intended to prepare plugs of materials that tend to expand when exposed to some liquid mixtures such as organic washing liquid mixtures and then shrink later such as during a separating run in the aqueous mobile phase, creating voids between column wall and polymer support and variations in separation-effective opening size distribution. For example, some reverse phase plugs with separation-effective openings may shrink when polymerized others may not, and after polymerization, some of the plugs that did not shrink during polymerization and some that did may shrink if exposed to water or some other polar liquid mixtures. In embodiments intended to

improve plugs of such materials, the compensation for this shrinkage may be compression with a piston during polymerization and/or compression after polymerization during conditions that would normally cause shrinking equal or more than the shrinkage that could happen during the separation run to force reordering or repositioning or to compensate for the shrinking. In either case where shrinkage is compensated for with pressure or where shrinkage is prevented to avoid causing voids, non-fluidic pressure such as with a piston is preferred rather than pressure with fluid. The word "pressure" in this specification excludes and differentiates from the term "compression" if the word "compression" is used to indicate the application of salt liquid mixtures to gel monoliths to open the pores of such gel monoliths.

Another way of solving this problem is to introduce hydrophilicity to the reversed phase media to result in swelling and prevent the shrinkage of the polymer in highly hydrophilic environment during the separation run. More specifically, a polymerization mixture is applied to a column in the preferred embodiment or to some other suitable mold and polymerization is initiated within the column or mold. The column or mold is sufficiently sealed: (1) to avoid unplanned loss by evaporation if polymerization is in an oven; or (2) to avoid contamination or dilution if polymerization is in a water bath. During polymerization, pressure is applied to the polymerization liquid mixture. Preferably the pressure is maintained at a level above atmospheric pressure to prevent the formation of voids by shrinkage until polymerization has resulted in a solid plug of separating medium or polymerization is completed. The inner surface of the column or mold with which the polymerization liquid mixture is in

contact during polymerization may be non-reactive or may be treated to increase adhesion to the surface of the plug.

The polymerization mixture in some embodiments includes: (1) selected monomers; (2) for some types of columns, an additive; (3) an initiator or catalyst; and (4) a porogen or porogens to form separation-effective openings.

In some embodiments function groups can be added before or after polymerization. The porogen, initiator, functional group to be added, additives, and reaction conditions and the monomer and/or polymer are selected for a specific type of column such as reverse phase, weak cation, strong cation, weak anion, strong anion columns, affinity support, normal phase, solid phase extraction and catalytic bed. The selection of components of the polymerization mixture is made to provide the desired quality of column.

A chromatographic column in accordance with this invention preferably includes a casing having internal walls to receive a permeable monolithic polymeric plug in which the separation-effective openings or surface features are of a controlled size formed in the polymer by a porogen in the polymerization mixture and are controlled in size by pressure during polymerization. This plug serves as a support for a sample in chromatographic columns. The permeable monolithic polymeric plug has smooth walls with no visible discontinuity in the plug wall and substantially no discontinuity or opening within the plug. Discontinuity in this specification means a raised portion or opening or depression or other change from the normal smoothness or pattern sufficient in size to be visible with the unaided eye. In this specification, the term "size-compensated polymers" or "size-compensated polymeric" means

monolithic polymeric permeable material having separation-effective openings in which discontinuities and lack of homogeneity in the separation-effective openings have been prevented by the methods referred to in this specification such as for example applying pressure and/or temperature-time moderation during polymerization or after polymerization during exposure to polar liquid mixtures in the case of some types of columns or by using a column that is prevented from further shrinkage in the presence of an aqueous liquid mixture by the application of pressure in the presence of the aqueous liquid mixture either during washing with an aqueous liquid mixture or during use in a separation operation using an aqueous liquid mixture. One type of discontinuity or lack of homogeneity is wall effects and another type is size difference in the separation-effective openings at different cross sectional locations in the polymeric plug.

One embodiment of column is made using a temperature controlled reaction chamber adapted to contain a polymerization mixture during polymerization and means for applying pressure to said polymerization mixture in said temperature controlled reaction chamber. The polymerization mixture comprises at least a polymer forming material and a porogen. In one embodiment, the pressure is applied by a movable member having a smooth surface in contact with the polymerization mixture under external fluid or mechanical pressure, although pressure can be applied directly to the polymerization mixture with gas such as nitrogen gas or with a liquid under pressure.

An embodiment of reversed phase media has been formed with different

hydrophobicity, and hydrophilicity from the prior art. The reversed phase media include polystyrenes, polymethacrylates and their combinations. These media are prepared by direct polymerization of monomers containing desired functionalities including phenyl, C4, C8, C12, C18 and hydroxyl groups or other combination of hydrophobic and hydrophilic groups to have different selectivity and wettability in the aqueous mobile phase. The polymerization conditions and porogens are investigated and selected to give high resolution separation of large molecules, in particular, the proteins, peptides, oligonucleotides and synthetic homopolymers. In one embodiment a reversed phase media is based on poly(styrene-co-divinylbenzene). In another embodiment of this patent, a reversed phase media is based on poly(stearyl methacrylate-co-divinylbenzene). In another embodiment, a reversed phase media is based on poly(butyl methacrylate-co-ethylene glycol dimethacrylate).

A reverse phase plug with exceptional characteristics is principally formed of copolymers of crosslinkers including divinylbenzene (DVB), and ethylene glycol dimethacrylate and monomers including styrene (ST) or methacrylates (MA) containing different carbon chain length. Generally, the best results are when the crosslinkers are greater than 40 percent by weight. Preferably the ratio of divinylbenzene and styrene is a value of divinylbenzene in a range between 7 to 1 and 9 to 1 and preferably 4 to 1 by weight, but may instead be 64 DVB or 40 percent styrene and 72 percent by weight DVB or 1 g divinylbenzene, 1 g styrene. The column may also be in the range of ratios between 17 to 3 and 19 to 1 and preferably 9 parts divinylbenzene to 1 part styrene. Monomers with hydrophilic functional groups can be added to reduce

shrinkage of the polymeric medium in aqueous mobile phase to prevent the wall effect during separations. The content of DVB in total monomers is preferably from 40% to 100%. In one preferred embodiment, the content of DVB is 80% (which is the highest commercially available) to improve the loading capacity of the column. The plug may also include methacrylates with hydrophobic surface groups or instead of being a vinyl compound including urea formaldehyde or silica.

Ion exchange plugs are formed principally of methacrylate polymers. A weak anion exchange plug is principally formed of polymers of glycidyl methacrylate (GMA) and of ethylene glycol dimethacrylate (EDMA). A strong anion exchanger plug is principally polymers of glycidyl methacrylate, 2-(acryloyloxyethyl) trimethylammonium methyl sulfate (ATMS), ethylene glycol dimethacrylate. The polymerization mixture may also include 1, 4-butanediol, propanol and AIBN. A weak cation exchanger plug is formed principally of glycidyl methacrylate, acrylic acid (AA) and ethylene glycol dimethacrylate. A strong cation exchanger plug is formed principally of glycidyl methacrylate, 2-Acrylamido-2-methyl-1-propanesulfonic acid (AMPS) and ethylene glycol dimethacrylate. In all these ion exchangers, functional groups can be added before or after the plug is formed. The content of EDMA in total monomers is preferably from 40% to 80%.

An increase of the content of crosslinker, such as EDMA, increases the rigidity of the column by reducing the swelling of the media in aqueous phase. Each of the polymerization mixtures is modified under the pressurized polymerization to obtain high flow rate and high resolution at both high and low

flow velocity. The coupling of copolymerization of the monomers containing desired functional groups for interaction and the controlled modification of other functional monomers to contain the desired interactive functional groups increases the capacity of the column while improving the rigidity of the separation media. This controlled modification may also improve the hydrophilicity of the columns in general by covering the potential hydrophobic surface area with hydrophilic functional groups. The modification conditions are chosen to not only provide the higher capacity and higher hydrophilicity of the media but also to prevent the swelling of polymer matrix in aqueous liquid mixture, which happens in other highly hydrophilic polymer matrices including both beads and monolith.

The polymer plugs may be formed in a column of any size or shape including conventional liquid chromatographic columns that may be circular cylinders, or coiled, bent or straight capillary tubes, or microchips or having any dimension or geometry. The sample or mixture to be separated into its components is injected into the column and the liquid phase is moved through the column to separate the sample into its components. The components may be detected and/or collected in a fraction collector and/or inserted into another device such as a gas chromatograph or mass spectrometer. In one embodiment, a plurality of columns is connected in parallel in a chromatographic system that includes a pumping system, solvent system and detecting system. The columns are permeable polymeric columns with high reproducibility so as to enable them to work together for related separations. In one embodiment, chromatographic discs or plugs having diameters much

greater than 25 mm are produced.

In one embodiment, the reaction is controlled by independent means such as for example electromagnetic radiation such as for example UV-vis, X-ray, or gamma ray instead of or in addition to reliance only on time, temperature
5 of a water bath and the reactants in the polymerization mixture. In this embodiment as in embodiments not using independent means heat may also be added to the column by conduction such as conduction of heat to or from a water bath. The heat may be added from a heat source or removed by cooling means in contact with a significantly large portion of coolant of the thermal mass
10 and in the reactor under the control of feedback to maintain the temperature of the reaction mass in the desired temperature range or to vary it during the reaction if desired.

In one version of this embodiment, variable intensity or variable wavelength X-rays may be used to control the polymerization rates of the
15 reactants such that the exotherms are under control. In one variation of this version, X-ray radiation penetrates the column to impart energy throughout the column or at a selected location to increase or decrease polymerization rates. This may be done by irradiating the monomer sufficiently to disassociate its double bonds to make monomers free radicals and thus increase their
20 reactivity. Another way is to use an initiator sensitive to the radiation that is activated by the radiation in the temperature region to be used for the reaction mass. The initiator is chosen to have an activation time and temperature considerably less than that of the monomers alone. Because the initiator forms free radicals only upon radiation of sufficient intensity, the radiation may be

used to control the polymerization reaction independently of the other factors.

The use of photoinitiators to control polymerization can be enhanced by added ingredients such as scintillators and sensitizers. For example, X-rays may activate scintillators within the solvent to emit light in response to the X-rays. Preferably, the scintillation light may be aided by adding fluorescent sensitizers to increase the activity of the photoinitiators in causing polymerization. The scintillators and sensitizers are selected to cause efficient absorbance of energy from the X-rays by the scintillators and radiation of light at an efficient wavelength within the absorbance band of the photoinitiators.

Polymerization using irradiation such as X-ray is used for preparing monolithic materials with cross sections from micrometers to meters. X-rays can penetrate the materials in depth. Both organic and inorganic polymers can be prepared using X-ray or γ -ray. High energy X-ray and γ -ray can travel the materials in high depth. Low energy to medium X-ray penetrates the materials in less depth resulting in a longer polymerization time but is safer to use. In one embodiment, a lower energy X-ray is used to initiate the polymerizations using the combination of X-ray scintillator and photoinitiators. We have discovered that non-thermal (photoinitiation) control of polymerization times from less than 12 hours to more than one week provides satisfactory chromatographic columns. Thermal polymerization of columns usually suffers from runaway exothermic reaction and extreme temperature gradients with columns over 20 mm in diameter. This causes ununiformities which degrade chromatographic properties. The slower, controlled, polymerization rate available with x- or γ -rays, or even UV causes a slower polymerization with tolerable rates of

exotherm while still maintaining reasonable rates of polymerization. Thermal gradients caused by exotherms may be made small enough to not degrade the properties of columns over 1 meter in diameter.

Excessive rates of exotherm and resulting process (polymerization) temperature and temperature gradient may be prevented with choice of a stabilizing additive. This stabilizing additive should have properties such that the reaction can proceed freely up to rate at which the desired polymer is formed, but not at a higher rate producing too high a temperature. For example, with peroxide initiators Disterylhidipropionate (DSTDP) quenches the hydroxyl radical which results from a side reaction, which later would go on to produce the further heat per event compared to the main reaction. Another approach is to use a stabilizer for the main reaction. This stabilizer is selected for limited solubility in the primary solvents or activity at the reaction temperature and more solubility above the reaction temperature. Under analogous conditions, a stabilizer, preferentially soluble in the porogen and having a temperature dependent of solubility or activity, may be used.

It is desirable to scale up the size of the column to have higher volume of media is highly desired in preparative chromatography and catalytic reactors. In one embodiment of the invention, the large diameter column is prepared by two staged polymerization inside the column. First, multiple thin cylindrical columns with the diameter smaller than that of the targeted column are prepared in a mold under pressure or without pressure. The thin columns are placed inside a large column filled with the same polymerization liquid mixture as used in formation of the thin columns. The thickness in one side of the thin

column should not exceed the 8mm which is the known maximum to prevent the formation of temperature gradient due to the difficulty in heat dissipation during exothermic polymerization. The temperature gradient results in vary inhomogeneous separation-effective opening size distribution which is detrimental to chromatography use.

In making size-compensated polymers for use in separation systems, the characteristics for a given type of separation can be tailored with a given polymer to the application by altering the amount of pressure applied during polymerization and/or, in the case of some polymers such as used in forming reverse phase separation media, applying pressure when used or when otherwise brought into contact with a polar solvent such as an aqueous solvent or washing fluid. After the nature of the polymer itself has been selected for a class of applications, columns can be made and tested. Based on the tests, the characteristics can be altered in some columns by applying pressure. It is believed that the application of pressure in some columns increases the uniformity of particle size and either because of the change in particle size or for other reasons, the size distribution and uniformity of separation effective openings throughout the polymer is increased. The increase in homogeneity of the particle size and separation-effective opening sizes improves resolution. An increase in pressure generally improves capacity and resolution and the pressure-time gradient. It is believed that in some columns micropores are greatly reduced or eliminated thus reducing zone spreading by the application of pressure during polymerization and/or during use or washing of the polymer with polar liquid mixtures.

In general, the characteristics of columns of small or large size can be controlled by controlling the enthalpy of the polymerization mixture during polymerization. This is accomplished in the preferred embodiment by the introduction and/or removal of energy. In some embodiments, the enthalpy is controlled by temperature control or by temperature and pressure during polymerization without the need for introducing energy by radiation but, under some circumstances, energy can also be added by radiation. This control can reduce the lack of homogeneousness of the separation-effective openings as well as producing other desirable characteristics. For this purpose the enthalpy is maintained within the range of polymerization but below the run-away enthalpy and at an enthalpy in which excessive exotherms that prevent the material from being time-temperature moderated are not created by the heat of reaction. It is especially economical to do this with a water bath. For some polymerization mixtures, for example, this enthalpy is maintained within this range by the introduction or removal of heat or by the controlled use of radiation such as UV radiation, IR radiation, X-ray radiation, visible light radiation or the like or a combination of heat conducted into the polymerization mixture and radiation. The enthalpy is also increased by the application of pressure. In the case of exothermic reactions, the enthalpy is maintained below the run-away temperature by permitting the heat to escape at a rate commensurate with its generation.

With some polymerization mixtures, the reaction is initiated by increasing the temperature to the desired reaction temperature using only the introduction of heat such as through a heated water bath. The amount of heat transferred

to the polymeric mixture can be controlled by changing the reaction periodically while heat is transferred by altering the temperature of the medium to which the heat is transferred from the polymeric mixture of controlling the rate of generation of heat. In the preferred embodiment, the temperature of the surface in contact with the external surface of the plug is kept low enough to avoid heat being introduced at a rate that results in excessive temperature gradients in the column but high enough for adequate cross linking of the polymer. This is accomplished by increasing the temperature of the outside surface, step wise or gradually, such as for example linearly with a slow rate of increase. The temperature added is controlled between the control-initiation point and the first safe-point to cause the rate of change of the reaction to be low. This keeps the exothermic heat low until the polymerization is far enough along to increase the temperature to complete the polymerization in a reasonable time and produce a temperature-time moderated polymer.

From the above description it can be understood that the novel monolithic solid support of this invention has several advantages, such as for example: (1) it provides chromatograms in a manner superior to the prior art; (2) it can be made simply and inexpensively; (3) it provides higher flow rates for some separations than the prior art separations, thus reducing the time of some separations; (4) it provides high resolution separations for some separation processes at lower pressures than some prior art processes; (5) it provides high resolution with disposable columns by reducing the cost of the columns; (6) it permits columns of many different shapes to be easily prepared, such as for example annular columns for annular chromatography and prepared in any

dimensions especially small dimensions such as for microchips and capillaries and for mass spectroscopy injectors using monolithic permeable polymeric tips; (7) it separates both small and large molecules rapidly; (8) it can provide a superior separating medium for many processes including among others extraction, chromatography, electrophoresis, supercritical fluid chromatography and solid support for catalysis, TLC and integrated CEC separations or chemical reaction; (9) it can provide better characteristics to certain known permeable monolithic separating media; (10) it provides a novel approach for the preparation of large diameter columns with homogeneous separation-effective opening size distribution; (11) it provides a separation media with no wall effect in highly aqueous mobile phase and with improved column efficiency; (12) it improves separation effective factors; and (13) it reduces the problems of swelling and shrinking in reverse phase columns.

BRIEF DESCRIPTION OF THE DRAWINGS

The above noted and other features of the invention will be better understood from the following detailed description, when considered with reference to the accompanying drawings in which:

FIG. 1 is a schematic diagram of one embodiment of a process for making a chromatographic column in accordance with an embodiment of the invention;

FIG. 2 is an assembly of a fixture for applying pressure to a glass column during polymerization;

FIG. 3 is an assembly of another fixture for applying pressure to a

stainless steel column during polymerization;

FIG. 4 is an assembly of still another fixture for applying pressure to a glass column during polymerization;

FIG. 5 is a Scanning Electron Microscopy (SEM) picture of the strong cation exchanger polymerized inside a cylinder column under 120 psi hydraulic pressure.

FIG. 6 is a chromatogram showing peaks from a protein sample with a column in which distortions have been avoided by pressure during polymerization;

FIG. 7 is a photograph showing three columns with the one on the left made with pressure during polymerization and the two on the right polymerized without pressure;

FIG. 8 is a block diagram of a chromatographic system with an array of columns and having reproducible characteristics which are similar to each other in the array.

FIG. 9 is a chromatogram showing the chromatography separation achieved with medium energy (110 kEV)X-ray irradiated polymerization.

FIG. 10 is a top view of a UV or visible light polymerization apparatus for chromatographic columns;

FIG. 11 is a sectional side elevational view of the apparatus of FIG. 10.

FIG. 12 is a schematic elevational view of an X-ray polymerization apparatus for chromatographic columns;

FIG. 13 is a top view of a portion of the apparatus of FIG. 12;

FIG. 14 is an elevational sectional view of a portion of the apparatus of

FIG. 12 taken through lines 14-14;

FIG. 15 is an elevational sectional view taken through lines 15-15 of FIG. 13;

FIG. 16 is a schematic drawing of apparatus for polymerizing a mixture to form a monolithic column;

FIG. 17 is a broken-away, simplified fragmentary sectional view of a column with temperature measuring devices in it to monitor temperature gradients useful in the embodiment of FIG. 16;

FIG. 18 is a graph comparing low-temperature constant-temperature polymerization with low-temperature variable-temperature polymerization as to the degree of polymerization obtainable in a reasonable amount of time;

FIG. 19 is a graph showing the temperature from the center of a column to the outer surface in a process in which the temperature of the outer surface is kept at the same temperature as the center of the column;

FIG. 20 is a drawing having equation 1, equation 2 and equation 3 illustrating a method and a modification of a method for a copolymerization of AMPS with GMA and EDMA; and

FIG. 21 is a chromatogram of a separation in a temperature-time moderated column.

DETAILED DESCRIPTION

Broadly, a polymerizable mixture is placed in a container with a porogen or solvent and polymerized to form a plug having separation-effective openings for use in a separation system such as for example a chromatographic column.

Advantageously, the polymerization is done in a container in which the plug is to be used such as a chromatographic column or extraction chamber or the like. In one embodiment of the invention, the mixture is polymerized while compensating for the effect of shrinkage during polymerization to form a size compensated polymeric plug. In other embodiments shrinkage is avoided by applying pressure to materials that tend to swell in the presence of water to form another embodiment of size compensated polymeric plug. In still other embodiments separation-effective opening size and distribution is controlled by pressure and/or by selection of the ingredients of the polymerization mixture and/or by processes using external influences such as electromagnetic radiation and/or by temperature-time moderation. Shrinking is compensated for or avoided because it may cause enlarged voids adjacent to the wall of the container and have a deleterious effect on pore or other separation-effective opening size distribution within the column.

In a preferred embodiment, the compensation is accomplished by applying pressure during polymerization to at least maintain the integrity of the material having separation-effective openings as it shrinks during polymerization. Maintaining the column at atmospheric pressure to accommodate shrinkage may not prevent the formation of voids in every case and may provide poor reproducibility. The polymers, monomers, initiators and porogens have been selected to improve the characteristics of the column and may be used with the embodiments of polymerization under pressure during polymerization or with other processes. In another embodiment, pressure is applied to the plug after it has been formed and after or during swelling caused

by other reactions such as washing with an aqueous liquid mixture after polymerization in the case of some reverse phase plugs. The surface of the column or mold with which the polymerization liquid mixture is in contact during polymerization may be non-reactive or may be treated to increase adhesion.

5 In one embodiment, the polymerization mixture includes at least one vinyl compound and a porogen. An initiator is included in the polymerization mixture or an initiation process is applied to a vinyl monomer and a porogen to form a monolithic plug for a chromatographic column or other device using a polymeric plug for separation. Generally the polymerization mixture includes, in
10 addition to the vinyl monomer, a vinyl polymer, or mixture of monomers and polymers, an initiator and a porogen. However, other approaches to polymerization without incorporating an initiator in the polymerization mixture are known in the art and can be used, such as radiation to form polymers. Moreover, some of the aspects of this invention may be applied to monomers
15 and polymers in a polymerization reaction other than vinyl groups such as for example urea formaldehyde or silica to form urea formaldehyde or silica plugs.

A chromatographic column formed by these processes includes a support having internal walls to receive a permeable monolithic polymeric plug having separation-effective openings of a preselected size distribution formed
20 during polymerization and controlled in size partly by pressure during polymerization and partly by selection of the components and proportions of the components of the polymerization mixture. For example, separation-effective opening size is controlled by the amount and type of porogen in the polymerization mixture in proportion to the amount of some of the other

ingredients. The pressures may be selected in a range of slightly above atmospheric pressure to a value within the strength of the walls of the column. The permeable monolithic polymeric plug has smooth walls and substantially no micropores within the plug. The plugs may have surface functional groups. For example, hydrophobic surface groups such as phenolic groups may be added to decrease swelling with aqueous based solvents in reverse phase plugs but capacity may also be decreased in this case. Similarly, hydrophilic surface groups may be added to increase capacity in reverse phase plugs.

One embodiment of permeable, monolithic, polymeric plug that is free of micropores or channeling openings in the wall is formed principally of vinyl polymers although many other polymers may be used in practicing the invention. A weak ion exchange permeable monolithic polymeric plug is principally formed of polymers of methacrylate such as glycidyl methacrylate and ethylene dimethacrylate in the ratios by weight of a value in the range between 2.5 and 3.5 to a value between 1.8 and 2.2 and preferably 3 to 2. A reverse phase permeable monolithic polymeric plug with exceptional characteristics is principally formed of polymers of divinylbenzene and of styrene. Preferably the ratio of divinylbenzene and styrene is approximately in a range of a value between 3.5 and 4.5 to a value between 0.8 and 1.2 and preferably 4 to 1 by weight, but may instead be 64 DVB (divinylbenzene) or 40 percent styrene and 72 percent by weight DVB or in the ratio of divinylbenzene to styrene in the range of a ratio of 2 to 3 and a ratio of 3 to 2 or preferably 1 to 1. The column may also be in the ratio of divinylbenzene to styrene in a range of the ratio of 8 to 1 and 10 to 1 and preferably 9 to 1. One hundred percent

DVB is also preferred.

In FIG. 1 there is shown a block diagram of one embodiment 10 of a method for making chromatographic columns comprising the step 12 of preparing a polymerization mixture, the step 14 of polymerizing the mixture, the step 16 of preparing the column for chromatographic run and the step 18 of performing a chromatographic run. The polymerization mixture used in step 14 of polymerizing a mixture includes a monomer and or polymer capable of polymerization, an initiator or initiation process such as radiation, and a porogen, many of which are known in the art. The step 12 of preparing the chromatographic mixture, the step 14 of polymerizing, the step 16 of preparing for a chromatographic run and the step 18 of performing the chromatographic run all may take different forms. Some of these variations will be described hereinafter.

The step 14 includes the substeps 20 of reacting the polymerization compound while compressing it to reduce voids, the substep 22 of washing the polymer, and in some embodiments, the step 24 of reacting the polymer to add certain functional groups. While a workable column may be obtained without compressing the polymerization mixture while polymerizing, significant improvements have been obtained by applying this compression. These improvements have been significant enough so as to make the difference between a competitive commercial column and one which would not be competitive in some types of columns and for some applications. The voids and inhomogeneous separation-effective openings that are prevented from forming by this compression may result from the inhomogeneous distribution of the

empty space created by shrinkage of the polymer during polymerization in a sealed container. The inhomogeneous distribution of the empty space may be due to the differences in surface tension between the column wall surface, polymer surface, nitrogen and porogens. The compression must be sufficient to take up this shrinkage and thus reduce the total volume of the column during polymerization. This process may also affect the separation-effective opening size in the column and can be used in a step by step process to create variations in separation-effective opening size if desired.

The washing step 22 is a conventional step intended to remove porogens and unreacted monomers or other ingredients that may be used for a specific column but are not intended to remain in the column. This step may be followed by reacting in a manner to add functional groups such as the groups described above that are important if the column is intended to separate proteins. In some embodiments, the washing step causes swelling of the plug followed by later shrinkage. Because the shrinkage may cause channeling voids, pressure is applied to the swollen plug in one embodiment to prevent the formation of voids during shrinking.

In FIG. 2, there is shown a block diagram of a polymerizing apparatus 28 having a pressure source 23, a pressure transfer mechanism 25 for applying pressure to a polymerization mixture 32 compression piston 27 and a confinement vessel 21. In the preferred embodiment, the source of pressure 23 is a regulated source of constant hydraulic pressure but other sources such as a spring or source of air or an inert gas may be used. Similarly, in the preferred embodiment, the mechanism 25 is a piston with a smooth surface to

provide a smooth surface to the polymerized plug that the piston surface has pressed against during polymerization but other sources such as a gas applied directly to the permeable monolithic polymeric plug may be used. In the preferred embodiment, the compression piston 27 moves inwardly into the column department 21 to exert pressure on the polymerization mixture within the compartment 32 during the polymerization reaction. When the polymerization reaction is complete, the porogen can be removed by a solvent pumped through the column. The polymerization occurs in a temperature controlled environment 29, which in the preferred embodiment is a water bath but can be any such temperature control mechanism such as a heated chamber. The materials for this device can be any conventional materials known in the art.

In FIG. 3 there is shown a sectional view of one embodiment of the polymerizing apparatus 28 having a metal column casing 1022, a confinement vessel 88, a transfer mechanism 25, a compression piston 112 and a pressure cap 80. The metal column 1022 is tightly held against the confinement vessel 88 with a seal 1021 between them. Compression of the seal 1021 is provided by a shoulder 1052 in the barrel 122 and wrench flats 1023A and B of the apparatus, which is attached to the column 1022 with threads 1053, thus providing a leak free connection between the column 1022 and the confinement vessel 88. The transfer mechanism 25 consists of a compression piston 112, an o-ring 110, a rod 106, a retaining collar 104, another o-ring 100, and a hydraulic piston head 602, all of which are arranged and fitted into the barrel 122 such that the compression piston 112 and o-ring 110 form a tight seal

inside the confinement vessel 88. The pressure cap 80 contains a fluid inlet port 33 fitted to the barrel 122, with a gasket 94 between them.

The pressure cap 80 and the barrel 122 are tightly connected, preventing the leakage of pressurized fluid applied through the fluid inlet 33. The transfer mechanism 25 is then positioned as shown, creating a volume in the confinement vessel 88. The square of the ratios of the inside diameter of the barrel 122 at o-ring 100 to the inside diameter of confinement vessel 88 provides a pressure multiplication factor. The opposite end of the column 1022 is filled with the polymerization reactants in the column compartment 32, and a containment plug 1024 is fitted in the opening. A containment cap 604 is threaded onto the column 1022, forcing the containment plug 1024 to seal the opening. Although the preferred embodiment here shows a tight fitting plug 1024 to provide the sealing, an alternate sealing arrangement, such as an o-ring, could as easily be used to provide either a face seal or a radial seal. The fluid inlet 33 is connected to a controlled pressure source, such as a controllable fluid pump or regulated bottle of compressed gas.

This description of the preferred embodiment employs a fluid source; either compressed gas or compressed liquid applied through the fluid inlet 33, however the compressive force could as easily be supplied by alternate means; such as, but not limited to a spring pressing on the transfer mechanism 25, weights stacked on the transfer mechanism 25 utilizing gravity to provide the compression, or centripetal force arranged to cause the transfer mechanism 25 to compress the monolithic polymeric column material inside the column compartment 32.

Once assembled, the apparatus 28 is placed in a temperature-controlled environment 29, which is a thermally controlled water bath in the preferred embodiment. Fluid pressure is then applied through the fluid inlet port 33, which is contained by the pressure cap 80, the gasket 94 the hydraulic piston head 602 and the o-ring 100. This applied force causes the hydraulic piston head 602 to move away from the pressure cap 80, and exerts force on the end of the rod 106. This rod 106 communicates the force to the compression piston 112, applying compressive pressure to the monolithic polymeric column material, preferably at the smooth surface 1101. This smooth surface causes a continuous, uniform surface to be created on the monolithic polymeric material exposed to the analytical fluids in the ultimate application and reduces the adhesion of the monolithic polymeric column material to the compression piston 112.

The containment plug 1024, column 1022, seal 1021 confinement vessel 88, and the compression piston 112 confine the monolithic polymeric material. As the chemical reaction proceeds, the volume of the monolithic polymeric material decreases, and the transfer mechanism 25 moves further into the confinement vessel 88. Air trapped between the o-ring 100 and the o-ring 110 is allowed to escape through an air escape opening 603 in the barrel 122. The compression of the reactant materials in this manner prevents the formation of undesirable voids in the monolithic polymeric material and eliminates wall effects between the monolithic polymeric material and the column 1022, which would reduce the performance of the column in use.

As the reaction proceeds and the monolithic polymeric material volume

reduces, the compression piston 112 moves closer to the column 1022. Near the end of the polymerization, the retaining collar 104 contacts the shoulder 1052 in the barrel 122, halting the forward motion of the transfer mechanism 25. Crushing of the newly formed monolithic polymeric material is prevented by this action. At this position, the smooth surface 1101 of the compression piston 112 is approximately even with the end of the column, and the monolithic polymeric material fills the column 1022 without undesired voids in the material or wall effects between the material and the column 1022. Using the wrench flats 1023A and 1023B, the polymer apparatus 28 is separated from the column 1022 as an assembly. Chromatographic fittings are then installed on both ends.

In FIG. 4 there is shown a sectional view of another embodiment of polymerizing apparatus 28A similar to the embodiment of polymerizing apparatus 28 having a glass column casing 922, a piston head assembly 401, a displacement piston 40 and a containment plug 923. In some analytical chemistry applications, the wetted surfaces must not contain metal components. Although the present discussion of this preferred embodiment refers to a glass column 922 and plastic pieces, any non-metallic material; such as, but not limited to glass, ceramic, or plastic which provides acceptable mechanical properties can be used. Further, the discussion here refers to the pressure applied being provided by a suitable fluid pressure source, alternative means of providing compression; including, but not limited to springs, weights, or mechanical means could as easily be used.

The piston head assembly 401 comprises a piston 76, an o-ring 38 and an intermediate portion 50, assembled and fitted into the column 922. A plunger

assembly 20 consisting of the displacement piston 40 and an o-ring 64 are assembled and fitted into the hydraulic cylinder portion 21 such that the recess 92 is away from the fluid inlet port 33 in the hydraulic cylinder portion 21. This plunger assembly 20 is pushed fully into the displacement chamber 60.

5 The hydraulic cylinder portion 21 and plunger assembly 30 are then threaded onto the column 922. Using a suitable tool, the piston assembly 401 is pushed into the hydraulic cylinder portion 21 until the annular shoulder 42 contacts the displacement piston 40, with the reduced diameter neck 48 fitting into the recess 92. The column 922 is filled with the reactant, and the
10 containment plug 923 is inserted into the open end of the column 922. A containment cap 924 is then threaded onto the end of the column 922, tightly holding the containment plug 923 to the column 922. Although this embodiment utilizes a tight fit between the containment plug 923 and the column 922, alternate methods; including, but not limited to an o-ring creating a face or radial
15 seal can as easily be used.

 A fluid pressure source is then applied through the fluid inlet port 33. The fluid is contained within the displacement chamber 60 by the hydraulic cylinder portion 21, the displacement piston 40 and the o-ring 64. The assembled components are then placed in a temperature-controlled environment 29. For
20 this embodiment, a thermally controlled water bath was used, but any suitable method of controlling the reaction temperature can be employed.

 The application of such fluid pressure causes the displacement piston 40 to move away from the fluid inlet port 33. This movement of the displacement piston 40 applies force to the annular shoulder 42 of the

intermediate portion 50, which then applies pressure to the monolithic polymeric material in the column 922 through the piston 76.

As the reactant chemicals polymerize, the volume decreases. The controlled application of pressure to the monolithic polymeric material prevents the formation of undesirable voids within the monolithic polymeric material and the formation of wall effects between the monolithic polymeric material and the wall of the column 922 as the volume decreases. As the reaction progresses, the piston 76 moves further into the column 922 to displace this reduction in volume. A smooth surface 74 on the piston creates a uniform surface of the monolithic polymeric material to provide a consistent interface to the analytic fluids in its final use, and to prevent the monolithic polymeric material from adhering to the surface of the piston 76.

Near the end of the reaction, the annular shoulder 42 comes in contact with the end of the column 922, preventing any further movement of the intermediate portion 50 into the column 922. This prevents the crushing of the monolithic polymeric material after the voids and wall effects have been eliminated. This annular shoulder 42 also limits the distance that the piston can travel, allowing control of the porosity and size of the resultant monolithic polymeric material in the column 922.

After the polymerization is completed, the hydraulic cylinder portion 21 is removed from the column 922, together with the displacement piston 40 and its o-ring 64. The confinement cap 924 and confinement plug 923 are then removed, and finally the piston head assembly 401 is removed. Chromatographic fittings are then installed on both ends.

It is also possible to provide compression on the reactant chemicals by the direct application of compressed gas directly to the reactant chemical's surface. Such a method is considered inferior to the above techniques because the surface of the resultant monolithic polymeric material will not be smooth or even, and may be more porous than the body of the monolithic polymeric material, when particular column formats are chosen. In other column formats the direct application of gas may be more applicable. It may be necessary to cut off the end of the polymer rod to achieve high resolution separation. In FIG. 5 there is shown a Scanning Electron Microscopy (SEM) picture of a strong cation exchanger polymerized inside a column casing under 120 psi hydraulic pressure magnified 9,000 times to show globules of particles with no pores but with channels between them having high surface area because of the irregular surface area and to a lesser extent the more stacked-plate like configurations of the globules of particles. The rough surface area of the particles with projections covering their surface area shows signs that may indicate growth by accretion.

In FIG. 6, there is shown a chromatogram having peaks from a protein sample separated in a column in which the problems of swelling and shrinking avoided by the application of pressure. The peaks are distinctive and relatively high with good resolution. This particular chromatogram is for gradient elution at a flow rate of 3 ml/min on a protein sample of conalbumin, ovalbumin and trypsin inhibitor using a 0.01 MTris buffer of pH 7.6 as one solvent and a 1M sodium chloride as the other solvent with a gradient of 0 to 50 percent the second solvent in 5 minutes time. The back pressure is 250 pounds per square

inch in this column whereas a column without such compensation would be expected to have a higher back pressure for the same gradient.

In FIG. 7, there is shown three plugs with the one on the left made with pressure during polymerization and the two on the right polymerized without pressure. FIG. 7 illustrates the discontinuities formed on the surface of columns caused by shrinkage during formation of the column. There are similar discontinuities inside the column in the form of relatively large openings unpredictably spaced. These figures also illustrate that the discontinuities can be removed, resulting in better reproducibility between columns of the same composition and the same size and improved resolution during chromatographic runs.

In FIG. 8, there is shown a block diagram of a preparatory liquid chromatographic system 101 having a pumping system 121, a column and detector array 141, a collector system 117, a controller 119, and a purge system 123. The column and detector array 141 includes a plurality of columns with permeable plugs in them. Preferably the plugs are size-compensated polymeric plugs. The pumping system 121 supplies solvent to the column and detector array 141 under the control of the controller 119. The purge system 123 communicates with a pump array 135 to purge the pumps and the lines between the pumps and the columns between chromatographic runs. The pump array 135 supplies solvent to the column and detector array 141 from which effluent flows into the collector system 117 under the control of the controller 119. The controller 119 receives signals from detectors in the column and detector array 141 indicating bands of solute and activates the fraction

collector system 117 accordingly in a manner known in the art. One suitable fraction collector system is the FOXY7 200 fraction collector available from Isco, Inc., 4700 Superior Street, Lincoln, NE 68504.

To supply solvent to the pump array 135, the pumping system 121
5 includes a plurality of solvent reservoirs and manifolds, a first and second of which are indicated at 131 and 133 respectively, a pump array 135 and a motor 137 which is driven under the control of the controller 119 to operate the array of pumps 135. The controller 119 also controls the valves in the pump array 135 to control the flow of solvent and the formation of gradients as the motor
10 actuates the pistons of the reciprocating pumps in the pump array 135 simultaneously to pump solvent from a plurality of pumps in the array and to draw solvent from the solvent reservoirs and manifolds such as 131 and 133.

While in the preferred embodiment, an array of reciprocating piston pumps are used, any type of pump is suitable whether reciprocating or not and
15 whether piston type or not. A large number of different pumps and pumping principles are known in the art and to persons of ordinary skill in the art and any such known pump or pumping principle may be adaptable to the invention disclosed herein with routine engineering in most cases. While two solvents are disclosed in the embodiment of FIG. 1, only one solvent or two or more than two
20 solvents may be used .

To process the effluent, the collector system 117 includes a fraction collector 141 to collect solute, a manifold 143 and a waste depository 145 to handle waste from the manifold 143. One or more fraction collectors communicate with a column and detector array 143 to receive the solute from

the columns, either with a manifold or not. A manifold may be used to combine solute from more than one column and deposit them together in a single receptacle or each column may deposit solute in its own receptacle or some of the columns each may deposit solute in its own corresponding receptacle and others may combine solute in the same receptacles. The manifold 143 communicates with the column and detector array 141 to channel effluent from each column and deposit it in the waste depository 145.

Because the system of FIG. 8 includes an array of columns each involved in a similar task, reproducibility of the column is particularly important since it is desirable for each column performing a single task to have characteristics as similar to all of the other columns performing that task as possible. Consequently, there is a substantial advantage in any group of columns that are intended to cooperate in the performing of a separation of samples closely related to each other, the permeable polymeric columns of this invention have particular application.

To make a column or other device having a polymeric plug as a separating medium without openings in the side walls or large openings in the body of the plug, one embodiment of polymerization equipment includes a temperature controlled reaction chamber adapted to contain a polymerization mixture during polymerization and means for applying pressure to said polymerization mixture in said temperature controlled reaction chamber. The polymerization mixture comprises a monomer, polymer and a porogen. In a preferred embodiment the means for applying pressure is a means for applying pressure with a movable member. The polymerization mixture comprises a

cross-linking reagent and a cross-linking monomer. The rigidity, capacity and separation-effective opening distribution are controlled by the amount of cross-linking reagent, monomer, polymerization temperature and pressure.

5 The polymerization takes place in a closed container to avoid loss of solvent in the case of an oven or to avoid dilution or contamination of the mixture with water in the case of a water bath reaction chamber. Pressure is applied during polymerization of some mixtures such as mixtures for ion exchange columns to balance vacuum formed by shrinkage. The polymer plug is washed after polymerization to remove the porogen. In the case of some
10 polymer, the plug may have a tendency to swell during washing or during a chromatographic run if aqueous liquid mixtures are applied such as if the plug is a reverse phase plug.

To separate a mixture into its components, a permeable polymeric plug is formed as described above. It may be formed in a column of any size or
15 shape including conventional liquid chromatographic columns that are right regular tubular cylinders, or capillary tubes, or microchips or having any dimension or geometry. A sample is located in juxtaposition with the plug and the components of the sample are separated one from the other as they are moved through the plug.

20 For example, to separate proteins from a mixture of proteins in a sample by liquid chromatography, a column is formed as a plug and polymerized in place with a porogen. Shrinkage is compensated for before use. The sample is injected into the column and a solvent caused to flow through the column, whereby the sample is separated into its components as it is carried through the

plug. In one embodiment, a plurality of samples are separated simultaneously in separate columns with high reproducibility.

One embodiment of chromatographic columns used in separation processes have a chromatographic casing with internal casing walls and have a permeable monolithic polymeric plug in the casing walls. The plug is a polymer having separation-effective openings which may be of a controlled size formed in the polymer by a porogen in the polymerization mixture before polymerization and controlled in size at least partly by pressure during polymerization. The permeable monolithic polymeric plug has smooth walls and substantially no pores within the permeable monolithic polymeric plug. In the preferred embodiment, the plug is formed of vinyl polymers but may be formed of others such as urea formaldehyde or silica. These may include surface groups such as hydrophobic groups to reduce swelling with aqueous solvents or hydrophilic groups to increase capacity.

Some examples of the proportions of the ingredients in polymerization mixtures and the ingredients in different plugs are illustrative. For example, a weak ion exchanger permeable monolithic polymeric plug that is free of channeling openings is formed principally of methacrylate polymer. Advantageously, the permeable monolithic polymeric plug is principally formed of polymers of glycidyl methacrylate and of ethylene dimethacrylate in the ratio by weight in a range of ratios between 1 to 1 and 7 to 3 and preferably 3 to 2.

A strong anion exchanger includes as its principal ingredients glycidyl methacrylate (GMA) and ethylene divinylmethacrylate (EDMA) in the ratio of a value in the range of .8 to 1.2 to a value in the range of 2.8 to 3.2 and preferably

a ratio of 1 to 3. The polymerization liquid mixture in the preferred embodiment includes 0.4 grams GMA, 0.5 grams of 2-(acryloyloxyethyl) trimethylammonium methyl sulfate, 1.2 grams EDMA, 1.5 grams of 1, 4-butanediol, 1.35 grams propanol, 0.15 grams water and 0.02 grams AIBN.

5 A weak cation exchanger included a polymerization liquid mixture of methyl methacrylate (MMA), GMA and EDMA in the ratio of a value of MMA in the range of 4.5 to 5.5 to a value of GMA in the range of .8 to 1.2 to a value of EDMA in a range of 11 to 13, and preferably a ratio of 5 to 1 to 12. The polymerization liquid mixture includes 0.2 grams AA, 0.5 grams methyl
10 methacrylate (MMA), 0.1 grams GMA, 1.2 grams EDMA, 2.55 grams dodecanol, 0.45 grams cyclohexanol and 0.02 grams AIBN. After polymerization, this column is hydrolyzed in a 0.25 M sodium chloroacetate in 5 M (molar) sodium hydroxide NaOH at 60°C for six hours.

Other examples are: (1) glycidyl methacrylate and of ethylene
15 dimethacrylate in a ratio by weight in the range of from 1 to 1 and 2 to 1; or (2) divinylbenzene and styrene in a ratio in the range of 3 to 1 and 9 to 1; or (3) divinylbenzene and styrene in a ratio in the range of 4 to 1 or with the amount divinylbenzene being in the range of 35 percent and 80 percent by weight divinylbenzene and preferably 64 percent by weight divinylbenzene; or (4)
20 divinylbenzene, styrene and porogen are in the ratio of 8 to 2 to 15 respectively; or (5) divinylbenzene, styrene and dodecanol in a proportion within the range of 7 to 9 units of divinylbenzene to 1.5 to 2.5 units of styrene to 13-17 units of dodecanol combined with an initiator; or (6) divinylbenzene, styrene and dodecanol in the range of 8 to 2 to 15 respectively combined with an initiator;

or (7) divinylbenzene, styrene dodecanol and toluene in the proportions of 7-9 to 1.5-2.5 to 9-13 to 2.5-3.5 respectively, combined with an initiator; or (8) divinylbenzene, styrene dodecanol and toluene combined in the proportions of 8 to 2 to 11 to 3 respectively, combined with an initiator; or (9) glycidyl methacrylate, ethylene dimethacrylate, cyclohexanol and dodecanol in the proportions of 0.5-0.7 to 0.3-0.5 to 1-2 to 0.1-2.5, combined with an initiator; or (10) glycidyl methacrylate, ethylene dimethacrylate, cyclohexanol and dodecanol in the proportions of 0.6 to 0.4 to 1.325 to 0.175 respectively.

In general, a process of preparing a monolithic polymer support having separation-effective openings for a targeted application may include the following steps: (1) preparing a polymerization mixture with a selected formula; (2) placing the mixture in a container, sometimes referred to as a column in some of the embodiments of this invention, with desired shape and size; (3) sealing the column with pressurizing fittings or non-pressure sealing; (4) polymerizing the polymerization mixture in a heating bath or oven with controlled temperature under selected pressure or without pressure; (5) taking the columns from the heating bath or oven and applying selected or specially designed fittings for the desired function; (6) washing the porogens and soluble materials out of the columns with selected solvent preferably by programmed flow; (7) in some embodiments, pumping a formulated modification liquid mixtures to obtain the desired functionality for interaction; (8) performing special modification in a heating bath or oven under controlled conditions; (9) washing the modification liquid mixtures out of the columns preferably with a programmed flow; (10) stabilizing, assembling and conditioning the column for

its use at desired conditions with high resolution; (11) characterizing the columns with sample separation in the target application; and (12) replacing the liquid in the column with selected storage liquid mixture. Steps 7 to 9 are optional or repetitive depending on the functionality of the media to be used. Steps 1 to 5 are modified and repeated in the two or multiple staged polymerization process.

In some of the embodiments of this invention, a polymerization mixture includes a single or a plurality of: (1) monomers; (2) porogens; (3) initiators or catalysts; and/or (4) additives or fillers (optional). The polymerization mixture may be degassed with helium for more than 15 minutes, or by vacuum, or by combination of both prior to be filled or injected to the column. The goal of this degassing is to get rid of the oxygen inside the mixture. The oxygen can act as an inhibitor or initiator at different situations resulting in some unpredictable behavior of the polymerization, which is detrimental to the resolution and reproducibility of the columns.

The suitable monomers for the above process comprise mono, di and multiple functional monomers known in the art, preferably monomers containing the vinyl or hydroxyl silica functional groups, which might be generated *in situ* as an intermediate. The typical monovinyl monomers include styrene and its derivatives containing hydroxyl, halogen, amino, sulfonic acid, carboxylic acid, nitro groups and different alkyl chains such as c4, c8, c12 and c18, or their protected format which could be used to generate those functionalities before or after polymerization; and include acrylates, methacrylates, acrylamides, methacrylamides, vinylpyrrolidones, vinylacetates, acrylic acids, methacrylic

acids, vinyl sulfonic acids, and the derivatives or these groups which could be used to generate these compounds *in situ*. The mixture of these monomers can be used. Siloxanes with hydroxyl group, vinyl groups, alkyl groups or their derivative and mixture thereof are preferred. The amount of the monofunctional monomers are varied from 2% to 60% of the total monomers in the
5 embodiments of this invention. They vary dramatically depending on the type of media.

The typical di or multifunctional monomers are preferably the di or multiple vinyl- containing monomers with a bridging moiety such as benzene,
10 naphthalene, pyridine, alkyl ethylene glycol or its oligoes. Examples of these polyvinyl compounds are divinylbenzene, divinyl naphthalene, alkylene diacrylates, dimethacrylates, diacrylamides and dimethacrylamide, divinylpyridine, ethylene glycol dimethacrylates and diacrylates, polyethylene glycol dimethacrylates and acrylates, pentaerythritol di-, tri-, or
15 tetramethacrylate and acrylate, trimethylopropane trimethacrylate and acrylate, and the mixture of these compounds. Siloxanes with di, tri and tetrahydroxyl groups, which are often generated *in situ* are also preferred in this invention. The typical amount of the multifunctional monomers are from 40% to 80% in the embodiments of this invention.

20 The initiators comprise all the initiators known in the art such as azo compounds and peroxides. Example of the typical initiators are azobisisobutyronitrile, benzoyl peroxide, 2,2'-azobis(isobutyramide)dehydrate, 2,2'-azobis(2-amidinopropane)dihydrochloride. The typical amount of the initiator is from 0.5% to 2% of the total monomers in the embodiments of this

invention. When siloxane is used, a catalyst such as an acid is used instead of an initiator. The amount of catalyst is from milimoles to moles per liter of polymerization mixture. Other approaches to polymerization without incorporating an initiator in the polymerization mixture are known in the art and can be used, such as radiation to form polymers.

The porogen is any material or compound that can be removed after polymerization to generate separation-effective opening structures. The typical porogens that may be used are organic solvents, water, oligomers, polymers, decomposable or soluble polymers. Some example of the organic solvents are alcohols, esters, ethers, aliphatic and aromatic hydrocarbons, ketones, di, tri, tetraethylene glycols, butane diols, glycerols or the combination of these solvents. The choice of porogens depends on the separation-effective opening size and separation-effective opening distribution needed.

In some embodiments, a single or a combination of porogenic solvents is chosen. The single or a combination of porogenic solvents is mixable with the monomers and initiators to form a homogeneous fluid mixture but the single or a combination of porogenic solvents have poor solvating power with the polymers formed. The polymerization usually starts from the initiator. The formation of oligomers is followed by crosslinking forming crosslinked polymer or nuclei, and the continuous growth of the polymer or nuclei. These polymer chains and nuclei precipitate out of the liquid mixture at the size allowed by the solvating power of the porogenic solvents. These polymer chains and nuclei are suspended in the liquid mixture first and form small particles through collision and crosslinking. The small particles are swelled by the porogens and

monomers, and continue to grow by both polymerization and aggregation with other nucleis or particles. The larger particles aggregate together by collision and are held in place by crosslinking. The time and speed of the precipitation of the polymer and nuclei dramatically affect the size of particles, aggregates or clusters and the separation-effective opening size formed among these particles and aggregates as well as the separation-effective opening size distribution.

It has been discovered that the combination of a very poor solvent and a fairly good solvent is usually better to tune the solubility or swellability of the polymer in the liquid mixture, which result in the desired porosity and separation-effective opening size distribution. The choice of poor solvent is more important since generation of the large separation-effective opening is the most important. After the generation of large separation-effective opening, it is always easier to find a good or fairly good solvent to tune the separation-effective opening size down. It has been discovered that the alcohols or the neutral compounds containing a hydroxyl group or multiple hydroxyl groups are the better choice of the poor solvents for the media made of polystyrenes, polymethacrylates, polyacrylates, polyacrylamides and polymethacrylamides. The solubility or solvation power can be easily tuned to using alcohols of different chain lengths and number of hydroxyl groups. A good solvent for the polymers can be chosen from many conventional good solvents such as toluene, tetrahydrofuran, acetonitrile, formamide, acetamide, DMSO. The typical amount of the porogens vary from 20% to 80%, more preferably 40% to 60% in the embodiments of this invention.

The additives or fillers used in this invention are those materials which can add a specifically desired feature to the media. One important characteristic of polymers having separation-effective openings is the rigidity of the polymer. Insoluble rigid polymer particles, silica particles, or other inorganic particles can be added into the polymerization mixture to strengthen the polymer having separation-effective openings after the polymerization. Polymers with a very large number or amount of separation-effective openings usually do not have good strength or toughness. They are fragile most of the time. The rigid particles can act as framework for the polymers. In another embodiment, the problem of heat transfer during the preparation of large diameter columns is reduced by adding very mono-dispersed nonporous particles to the polymerization mixture. Quite often, a large diameter column is required for high flow preparative chromatography or catalytic bed to allow high flow rate with only low back pressure.

In an embodiment of polymer having separation-effective openings, mono-dispersed large non-porous particles or beads are packed tightly with the pattern of close to dense packing. The polymerization mixture is filled into the interstitial space of the large beads and polymerized in these spaces. The flow pattern and column efficiency are improved by the densely packed monodispersed beads. Materials with a very large number of or amount of separation-effective openings can be prepared in this large diameter columns without fear of collapse of the media with low rigidity since the large monodispersed beads are the supporting materials for the large columns. High flow rate can be achieved owing to the large number or amount of separation-

effective openings but robust structure of the polymer.

In another embodiment, the heat dissipation problem is avoided in preparation of the large columns with two or multiple staged polymerization incorporating polymers having separation-effective openings as fillers. In one embodiment of the invention, multiple thin columns having separation-effective openings prepared from the same polymerization mixture are used as a filler to reduce the heat dissipation problem during *in situ* preparation of the large columns. In another embodiment of the invention, a polymer rod is used as the filler for the same purpose. In one embodiment of this invention, the filler material is large non-porous silica beads.

The polymers, monomers, initiators, porogens, additives and polymerization temperature are selected to improve the characteristics of the column and may be used with an embodiment of polymerization using pressure during polymerization or with other processes. Some of the aspects of this process may be applied to monomers and polymers formed in a polymerization reaction other than free radical reactions such as the polycondensation reactions and sol gel process which form silica monolith.

The column hardware in one embodiment of the invention includes rigid tubes to be used as chromatographic columns, with various shapes including cylindrical, conical, rectangular, and polygonal or an assembly of these tubes. The tube may be made from any conventional materials known in the art including metal, glass, silica, plastic or other polymers, more preferably stainless steel or glass. The inner dimension of this tube can be from micrometers to meters in diameter, thickness, width, or depth. The permeable

solid material may span the entire cross-section area of the tube where the separation of the samples take place by passing through the tube axially or radially (Lee, W-C, et al, "Radial Flow Affinity Chromatography for Trypsin Purification", Protein Purification (book), ACS Symposium Series 427, Chapter 8, American Chemical Society, Washington, D.C., 1990.) depending on the mode of separation, more specifically the axial or direct flow chromatography or the radial flow chromatography. The inner surface of the column or mold with which the polymerization liquid mixture is in contact during polymerization may be non-reactive or may be treated to increase adhesion to the surface of the plug. The tube can incorporate any usable fittings known in the art to connect it with other instruments, more specifically chromatography instruments.

In an embodiment of this invention, the monolithic permeable solid polymer is formed in a capillary tube, which can be for example a capillary tube with an internal diameter of 150 microns. In another, very significant, embodiment, the monolithic permeable rigid material is formed and sealed, often under pressure, in a removable 80.mm i.d. Teflon® sealing ring. This ring and column may be sold as a low-cost, reliable, high capacity, high resolution, very fast, easily replaceable, replacement chromatographic column. In another embodiment, the diameter of the tube is 10 mm. In another embodiment, the tube diameter is 4.6 mm and the material is stainless steel. In another embodiment of this invention, a plastic syringe barrel is used as a column. In another embodiment, the monolithic matrix is formed in a mold containing a metal container, a sealing plate and an insert with multiple cylindrical holes. The thickness of the insert varies from 1 to 10 mm. A mold can be a micro device

with plurality of channels or grooves on a plate made of silica or rigid polymers. The monolithic materials can be formed in any sizes and shape make it suitable for a specially designed micro-sized device, for example micro-titer plates with multiple wells containing the subject media and optionally having a small elution port in the bottom. There is no limit for the designed shape and size or the applications with these devices.

The polymerization mixture is filled or injected into a column with desired shape and size depending on the final use of the product to be polymerized to form a plug having separation-effective opening for use as a solid support. Advantageously, the polymerization is done in a column in which the plug is to be used such as a chromatographic column, catalytic bed, extraction chamber or the like. In one embodiment of the invention, the positive pressure is exerted to the polymerization mixture during polymerization to control the particle size of the aggregates and to compensate for volume shrinkage during polymerization. The particle size of the aggregate has been found to be more homogeneous and larger than that from non-pressurized polymerization. The volume shrinkage during polymerization is compensated by a positive air pressure or a moving piston with positive pressure.

More specifically, a polymerization mixture is applied to a column in the preferred embodiment or to some other suitable mold. Polymerization is initiated within the column or mold. The column or mold is sufficiently sealed to avoid unplanned loss by evaporation of porogens or monomers if the polymerization is in an oven, or to avoid contamination or dilution if polymerization is in a water bath. During polymerization, pressure is applied to

the polymerization liquid mixture. Preferably the pressure is maintained at a level above atmospheric pressure to control the size of the aggregates and its distribution in the polymer, and to prevent the formation of voids on the polymer wall surface and inside the media by shrinkage, and to prevent the media from separating from the wall of the column which forms an alternative fluid path through the gap or wall channels, until polymerization has been completed. Maintaining the column at atmospheric pressure to accommodate shrinkage did not prevent the formation of voids in every case and provided poor reproducibility. The pressure source can be a gas pressure, a pressure from non-compatible liquid, a piston driven by air pressure, spring force or hydraulic pressure.

In one embodiment of the invention, any number of pressurized molds (tubes) can be kept at a constant or controlled temperature in a single water bath, and identically pressurized from a single (e.g. nitrogen, water, etc.) manifold. This increases both uniformity and speed of production.

In another embodiment of the invention, a selected pressure is exerted on the polymerization mixture by high pressure nitrogen. In still another embodiment of the invention, a selected pressure is exerted on the polymerization mixture during polymerization by a pressurization device shown in FIGS. 2, 3 or 4. The column is sealed in one end and the polymerization mixture is filled into this column. The other end is sealed by the device shown in FIGS. 2, 3 or 4. The whole assembly of the polymerization fixture including the column is shown in FIGS. 2, 3 or 4. The pressure is applied to the polymerization by a piston with a smooth Teflon plug driven by a hydraulic

pressure from a syringe pump. The polymerization mixture was sealed in the column by the Teflon plug and an o-ring. When a constant positive pressure is applied to the polymerization mixture, the actual pressure is the difference between the hydraulic pressure and the friction. During the polymerization, the piston moves into the column upon the conversion of the monomers to polymers to compensate the voids generated due to the shrinkage of the polymers. This prevents any negative pressure and void space generated inside the sealed column due to this shrinkage, thus improving the column efficiency.

It is believed that the shrinkage is in every direction. The resulting voids are probably occupied by the nitrogen gas generated by AIBN or by solvent vapor with negative pressure inside the column. The voids can be large irregular dents on the polymer wall or small irregular dents spreading the entire polymer surface. The voids can also be distributed inside the polymer resulting in inhomogeneity of the separation-effective opening size distribution. These irregular voids and gaps result in the wall effect or zone spreading of the column. They are detrimental to the column efficiency and lower the resolution of the column. These voids and gaps also result in low reproducibility of the column performance from one to the other in the same batch of production or from batch to batch of the productions.

In one embodiment of the invention, a selected pressure is exerted to the polymerization mixture to control the size of the aggregates and the separation-effective opening size distribution. The particle size changes with the change of the pressure on the polymerization mixture during polymerization. The particle size is larger at higher pressure. Under the positive pressure, the

shrinkage of the polymer during polymerization happens only at the direction of the pressure force. This prevents the formation of voids inside the polymer and the voids/gaps on the wall surface adjacent to the column wall.

During the polymerization process, the monomer concentration continues to decrease with the increasing conversion of the monomers to polymers. The crosslinked polymers continue to precipitate out of the liquid mixture and aggregate with each other to form larger particles or clusters. These particles precipitate and link to each other by crosslinking agents such as an active polymer chain with a vinyl group. These interconnected particles sediment to the bottom of the column, which result in the lower monomer concentration at the top part of the column.

The separation-effective opening size is highly affected by the total monomer concentration and their ratios. An in-homogeneous separation-effective opening size gradient is formed along the direction of gravity, which results in zone spreading. Since the particle size is partly controlled by the pressure of polymerization, the gradient of separation-effective opening size can be corrected by adjusting the pressure during the polymerization. In one embodiment, the linearly increased pressure is exerted to the polymerization mixture during polymerization. In another preferred embodiment, the step pressure gradient is exerted to the polymerization mixture during polymerization. The speed and pattern of increasing/decreasing the pressure is chosen to control the particle size of the aggregates and its distribution during the entire polymerization process. When a linear gradient of separation-effective opening size distribution is desired, it can also be achieved by

changing the pressure during the polymerization with different speed and different maximum pressure.

The polymerization temperature depends on the choice of initiator. When AIBN and Benzoyl Peroxide are used, the typical temperature range is from 50 to 90 degrees Centigrade. The heating source can be any known in the art. The preferred ways are temperature controlled heating bath or oven. The reaction time can be from 0.5 to 48 hours depending on the choice of initiator and reaction temperature. In one embodiment of this invention, the polymerization is carried out in a temperature controlled water bath at 60 degrees Centigrade for 20 hours.

Irradiation, such as IR, UV-vis or X-ray, is used as the source for polymerization when a light sensitive initiator is used. In one embodiment the reaction starts by thermal activation of the initiator. In another it starts by the application of energetic radiation such as X-rays, either with or without a chemical initiator. If X-rays are used, the initiator should be selected to thermally activate at temperatures well above the polymerization temperature. On the other hand, the initiator activates when under X-ray irradiation at temperatures in the given region desirable for the reaction mass to receive activation. The initiator is also selected so that activation time and temperature for dissociation is considerably less than for the monomers alone. The production of active initiator (free radical) is controlled only by the X-ray's intensity. Since the X-ray intensity is controllable, the reaction rate is controllable and won't "run away" or overheat. Moreover, the initiator may be chosen to activate when under X-ray irradiation at temperatures in the given

region desirable for the reaction mass to receive activation.

In one embodiment, X-rays supply all or part of the energy for polymerization. The energy of the X-ray photons is varied in accordance with the preparation of the polymers and with the difference in thickness or cross-sections. Lower energy X-rays are used for preparation of smaller diameter polymer rods and higher energy X-rays or exposure to lower energy X-ray for a longer period of time may be used for preparation of large diameter polymer rods. In the preferred embodiment, the polymerization temperature is controlled by switching the X-ray on/off. When X-ray is switched off, the polymerization is quickly shut off within several seconds since the lifetime of the free radical is typically around one second.

In one embodiment, a photoinitiator is used to initiate the polymerization using X-ray as the energy source. The photoinitiators are the typical photoinitiators used in photo polymerizations in the polymer field including γ -ray, X-ray, UV, Visible and IR sensitive photoinitiators. The photoinitiators include azo compounds such as azobisisobutyronitrile, peroxides such as Diphenyl (2,4,6, - Trimethyl Benzoyl) Phosphine Oxide, ketones such as phenanthrenequinone, 2-chlorothioxanthen-9-one, 4,4'-bis(dimethylamino)benzophenone, 4,4'-bis(diethylamino)benzophenone, 4,4'-bis(dimethylamino)bezebophenone, 2-chlorothioxanthen-9-one, Benzil Dimethyl ketal, Organic metallic complexes. These photoinitiators include the ones used in both cationic and free radical polymerizations. In one embodiment, AIBN is used as the photo initiator. In another embodiment, phenanthrenequinone is used as the photo initiator.

In one embodiment, scintillators and sensitizers are used to enhance the activity of photoinitiators. For example, X-rays may cause scintillation by energizing the solvent so that it transfers energy to known scintillators that have been added or by directly causing scintillation of a solvent having scintillation properties. Preferably, the scintillation light is aided by adding fluorescent sensitizers to increase the activity of the photoinitiators in causing polymerization. The scintillators and sensitizers are selected to cause efficient absorbance of energy from the X-rays by the scintillators and radiation of light in an efficient wavelength within the absorbance band of the photoinitiators.

The scintillators which can be used include any of the luminescence materials in the prior art. Generally, the scintillators include the compound containing benzene rings such as terphenyls, quaternary phenyls, naphthalenes, anthracenes, compounds containing heterocycles, compounds with a carbonyl group, compounds with two or more fluorophores and organometallic compounds, and inorganic compounds such as ZnTe, ZnSe, ZnS, CsI, Gd_2O_2S and $CaWO_4$. In some embodiments, 2,5-diphenyloxazole (PPO), 2-phenyl-5-(4-biphenyl) 1,3,4-oxadiazole (PBD), 2-(1-Naphthyl)-5-phenyloxazole (α -NPO) are used as scintillators. In one embodiment, terphenyl is used as the scintillator. In another embodiment, ZnSe is used as the scintillator.

Preferably, a multiple step initiation process is used for the x-ray aided polymerization using photoinitiators. The mechanism of the initiation using the combination of scintillators and photoinitiators is believed to be a multiple step initiation process. First, the X-rays activate the solvent molecules to form

electronically excited solvent molecules. The excited solvent molecules rapidly transfer their excitation energy to the scintillator forming electronically excited scintillation. Then, the excited state of the scintillator relaxes to ground state by emission of photons. The emitted photons are absorbed by the photoinitiators and form active free radicals. The free initiator free radicals contact the vinyl function groups of the monomers and start the polymerization process. The process can be depicted as followings: X-ray $h\nu$ -- excited solvent molecule^{*} -- excited scintillator molecules^{*} -- UV or Visible $h\nu'$ -- excited initiator molecules^{*} -- initiator free radicals -- polymer radicals

X-ray irradiated polymerization can be used for preparing homopolymers such as polystyrene, polytetrahydrofuran, resins such epoxy or other crosslinked materials, and porous polymer support such as separation media in the shape of columns, membranes, or materials in any other housings. The method can be used for preparation of molded parts in any shape. In one embodiment, polystyrene is prepared by using X-ray irradiation as an energy source. Polystyrene is prepared in a mold of a glass vial with a narrow opening and in a shape of a cylinder. Both liquid mixture polymerization and bulk polymerization are used to prepare homoporous styrene (homopolystyrene) materials. In another embodiment, polyglycidylmethacrylate resin is prepared by using the same method. In another embodiment, porous poly(styrene-co-divinylbenzene) is prepared. In another embodiment, porous poly(glycidyl methacrylate-co-ethylene glycol dimethacrylate) polymer support is prepared.

X-rays can be used for preparing porous monolithic polymer supports with cross sections from micrometers to meters. X-ray irradiated

polymerizations are used to prepare monolithic liquid chromatography columns including capillary and microbore analytical columns, conventional analytical columns, and preparative and process columns. In one embodiment, porous monolithic support in a glass column with an inner diameter of 1 cm is prepared.

5 The column is characterized by SEM, porosimetry and chromatography.

The poly(styrene-co-divinylbenzene) monolithic column in this glass housing shows excellent separation of peptides. X-rays can penetrate the materials in depth. Both organic and inorganic polymers can be prepared using X-ray or γ -ray. High energy X-ray and γ -ray can travel the materials in high
10 depth. If a greater such depth is required, the unpolymerized mixture can be placed in the X-ray beam, and rotated and translated in a way chosen that the overall, time-averaged irradiation is sufficiently uniform throughout the body being polymerized. Note that radiation aligned in the intended direction of chromatographic flow does not cause significant chromatographic nonuniformity
15 in the bed because of absorbance of the radiation beam. Axial nonuniformities do not necessarily degrade performance as radial nonuniformities do.

Low energy X-ray penetrates the materials in less depth but is safer to use. In one embodiment, low energy X-ray was used to prepare a porous monolithic support in a glass column with the diameter of 3.5 cm. In another
20 embodiment, a monolithic support in a polymeric column housing with 88 mm diameter is prepared. The temperature of polymerization is controlled by controlling the intensities and energies of the X-ray photons and by a water jacket so at least one side of the reaction mixture is controlled. Preferably such water cooling cools the column in its axial direction but not the radial direction

to avoid thermal gradient and resulting inhomogeneity. All flow paths experience the same inhomogeneity in the direction of chromatographic flow, and thus have no effect upon the separation. The polymerization temperature in the center of this large diameter column is about the same as the polymerization temperature on the edge of the column during the whole polymerization process. The conversions of the monomers are completed after four days of polymerization.

X-ray irradiated polymerization can be combined with thermal polymerization. Polymerization rate and porosities can be controlled by the rate of polymerization, which can be controlled by the energies and intensities of X-ray, and the temperature of polymerization. In consideration of the economy and safety of irradiated polymerization process, lower energy and intensity X-ray is preferably used in preparation of large diameter monolithic polymer support. The conversion of monomers is more than 70% complete after 48 hours of polymerization in the 3.5 cm diameter column. In order to speed up the polymerization rate and finish the conversion in a short time, thermal polymerization at the desired temperature corresponding to the initiators is used. In one embodiment, porous poly(styrene-co-divinylbenzene) is prepared by using X-ray irradiation followed by thermal polymerization at 70°C after the X-ray irradiated polymerization. The porosity of the polymer can be controlled by monomer compositions, X-ray intensity and energy, choice of initiator and scintillator combination, and the polymerization temperature in both X-ray irradiated polymerization and thermal polymerization. The porogenic solvents used in this polymerization process is the same as those used in pure thermal polymerization described earlier. Excellent polymer support is obtained for liquid

chromatography use.

Ultraviolet and visible light radiation has been used in the past for preparing polymers including homopolymers, slab-shaped polymer resins and porous polymer surface coatings but not the polymer materials in this invention.

5 Both UV and visible light can penetrate thin, solid, clear materials. Ultraviolet and visible lights have been used to prepare thin, clear materials such as membranes. The homogeneity of a porous polymer becomes more of a problem when the thickness of materials increases. This is due to the scattering and attenuation of lights through the porous solid materials. The
10 depth that the light can travel through the solid materials decreases quickly depending on the functional groups and the refractive indexes of the materials. Consider an acrylic, dry porous column, made of two phases: acrylic resin refractive index about 1.5 and air with refractive index of 1.00. This scatters light so completely that this material looks like chalk, white and opaque.
15 Heretofore then these apparent differences have prevented the use of UV or visible light for polymerization.

Ultraviolet and visible lights can be used to prepare polymer materials including materials listed above with high homogeneity and to prepare polymer materials that are many inches thick. In one embodiment of column and
20 method of making a column using ultraviolet and visible light, a solvent of very similar or the same refractive index to the targeted polymer resins at the selected wavelength of light is chosen for the polymerizations. The light at the selected wavelength can travel through the polymers during the polymerization due to the little used Christiansen Effect, wherein the targeted porous resin

becomes quite translucent or transparent. Light in a particular wavelength range show transparency because the pores are full of solvent. Preferably, monochromatic light, of which the indices of the refraction in both the polymer solid and solvents are very close, is chosen for the polymerization. An initiator
5 activated by light rather than heat is used with a photoinitiator. If white light is used, the transmitted light corresponds to the particular wavelength at which the refractive indexes of the light in both polymer solid and the solvent or solvent combinations are very close. A photo initiator is chosen to absorb and be activated by light in the near transparent polymer and solvent wavelength range.
10 The initiator absorbs this wavelength range.

Preferably, when a photoinitiator is activated it breaks up onto fragments lacking in the original chromophores. Such fragments have no absorption in the range of selected wavelength of the light. When a light ray is absorbed by the chromophore in a photo initiating molecule the result is local polymerization at
15 the surface. If the chromophores survive this reaction they will be there to block the next ray of light from activating the next photo initiator molecule, hence limiting polymerization to the original surface. Therefore, the light can travel through the polymer mixture in more depth and the transmission of the light increases. This effect is known as Bleaching Effect. It has been found that a
20 good photo initiator in this respect is 2,4,6-trimethylbenzoyldiphenylphosphine oxide. The bleaching effect and the Christiansen effect are synergistic in the production of very thick layer, or deep, porous polymers by photoinitiation or e-ray initiation. In the latter case, X-rays excite the solvent which then transmits secondary energy to a so-called "sensitizer" which then fluoresces to activate

the initiator. If the solvent when excited by X-ray also in itself fluoresces, an additional degree of synergy exists. Often p-terphenyl is used as a sensitizer for X-ray polymerizations. Fluorescing solvents that are used include many aryl compounds such as toluene, o-, m-, or p-xylene, or the 1,2,3 (or other isomers of) mestylene. In one embodiment, homo-poly(glycidyl methacrylate) is prepared by ordinary liquid mixture polymerization using o-xylene as the porogenic solvent. The refractive indexes of o-xylene, the monomer and especially the polymer are close. The resulted polymer in liquid mixture is close to transparent but a little translucent due to minor scattering of the white light.

The refractive indexes of target polymers are measured. Both the good and poor solvents are selected to have the refractive indexes close to the refractive indexes of the target polymers. By tuning the ratio of the solvents, the refractive indexes of the solvent mixture will be almost the same as the polymer. Therefore, the transmission of the light through the polymer swelled by the solvents can reach the maximum. In one embodiment, porous polymethacrylate based monolith is prepared by using the combination of solvents.

In preparing temperature-time moderated polymer plugs having a large diameter, it is necessary to avoid non-homogeneous polymeric monoliths caused by non-homogeneous polymerization temperatures during polymerization. A homogeneous polymer should have less than a 25 percent variation in the mode of pore size distribution of the separation-effective openings in a given cross-section and preferably less than a 2 percent variation for most separations to be performed. In this specification, the mode is the peak of the distribution curve. The distribution curve is the percentage of the

pore volume per unit weight of the porous materials at different diameters of the pore size (openings). The non-homogeneous polymerization temperatures are created if there is a faster rate of heat generation than heat dissipation. The tendency to have non-homogeneous polymerization temperatures is increased by self-acceleration of polymerization which results in increases in heat in a manner difficult to control and at times in a geometrically non-homogeneous manner. The tendency for self-acceleration of polymerization is increased by the combination of the gel effect and increases in the polymerization temperature.

To have homogeneous polymerization temperatures, the rate of heat generation needs to be the same as the rate of heat dissipation. The desired polymerization temperature is determined by the equilibration rates of heat generation and dissipation during polymerization. The heat dissipation rate can be controlled to equal the heat generation rate by optimizing the polymerization temperature.

The self acceleration of polymerization does not happen when the polymerization temperature is low enough. At low polymerization temperatures, the rates of free radical generation from initiators and polymerization are slow. Although the polymer radicals are less prone to be terminated by collision of the polymer radicals or initiator radicals due to the high viscosity of the gel, the low polymerization rate and free radical generation rate increase the chance of termination of polymerization due to hydrogen transfer or polymer chain rearrangement. The overall polymerization rate is not increased due to the opposite effects on terminations of the active polymer radicals.

Self-acceleration of polymerization occurs when the polymerization temperature is higher than a threshold temperature. This threshold temperature varies with the polymerization or copolymerization rate of the monomers and depends on the environment of the polymerization mixture such as the porogens and monomers. Different porogens can have different termination effects on polymer and initiator radicals. Different monomers have different polymerization rates and rates of termination. Therefore, a low temperature can be chosen to balance the heat generation and dissipation while avoiding the self-acceleration of the polymerization due to the gel effect. In an embodiment of this invention, low temperature is used for polymerization to avoid the self-acceleration of the polymerization and to control the heat generation and dissipation rate in different diameter of columns including large diameter columns during a portion of the polymerization process and the gel effect permits higher temperatures later in another portion of the polymerization process. For example, in one polymerization using this method, ambient polymerization temperature was used to prepare porous separation media in a column with a diameter of 50 mm and length of 25 cm.

However, a disadvantage under some circumstances with polymerizing at low temperatures is the lack of rigidity. This is probably because that the degree of cross-linking of polymer matrix is not high enough so that the porous polymer swells in the solvent. It is also because the conversion of the monomers at low temperature is not high enough which result in enormous sizes of the separation-effective openings in the matrix. The extra-large pores decrease the strength of the polymer matrix dramatically so that the porous

polymer is not useful for chromatography separation under medium or high pressure, or at medium or high flow rate. However, increasing the polymerization temperature after the initial polymerization at low temperature can improve the degree of cross-linking and the conversion of the monomers.

5 In this invention, polymerization temperature is increased after the initial polymerization to improve the degree of cross-linking and conversion of the monomer in order to improve the rigidity of porous polymer matrix. High temperature curing process is used to improve the rigidity of the porous polymer. In one embodiment of this invention, 70°C is used to cure the porous
10 polymer after low temperature polymerization at ambient polymerization temperature. In another embodiment of this invention, 60°C is used to cure the polymer after low temperature polymerization at 40°C.

A critically important property of the porous polymer matrix for chromatography separation is the homogeneity of the distribution of the
15 separation-effective openings sizes. The combination of the low temperature and high temperature polymerization often results in a non-homogeneous distribution of the sizes of the separation-effective openings in the matrix due to the difference of the sizes of the separation-effective openings generated by different polymerization temperatures at different locations. The sizes of the
20 separation-effective openings of the porous polymer matrix were not changed by higher temperatures enough to affect the chromatographic property of the porous polymer after a certain degree of the conversion of the monomers and a certain degree of cross-linking. Further increases of the polymerization temperature after this point has been reached do not change the distribution

of the sizes of the separation-effective openings enough to affect the chromatographic properties of the porous polymer but instead improve the rigidity of the polymer matrix by increasing the degree of conversion of the monomers and the degree of cross-linking.

5 In this invention, temperature and time of polymerization was optimized to achieve a high degree of conversion of monomers and cross-linking, and to equilibrate the heat generation and dissipation rate of polymerization to achieve homogeneous size distribution of the separation-effective openings that is good enough for chromatography separations. Polymerization temperature was
10 further increased to improve the conversion of monomers and the degree of cross-linking. The program of steps of polymerization temperature and time of polymerization was used to prepare porous separation media for chromatographic use and other uses that require homogeneous separation-effective opening size distribution. For example, in one embodiment of this
15 invention, an optimized programmed step increase of the polymerization temperatures from ambient temperature to 70°C at desired length of polymerization was used to prepare porous polymer matrix with good chromatographic properties.

For some polymerizations, a programmed step increase in
20 polymerization temperature and time at the safe-point provided a good separation media but for other polymerizations this may not be good enough. An alternate procedure is available to improve the plug in such cases. Also the alternate procedure can decrease the polymerization time to achieve the desired degree of conversion and cross-linking. This alternate procedure is

available for those situations in which, the desired cross-linking degree and conversion might not be achievable due to too low polymerization temperature which is required to equilibrate the heat generation and dissipation rate and/or avoid the self-acceleration of the polymerization in the first procedure.

5 The alternate procedure uses a slow linear increase of the polymerization temperature after a certain amount of conversion of the monomers at low temperature polymerization. This alternate procedure increases the polymerization rate, shortens the polymerization time, increases the degree of conversion of the monomers to polymer while maintaining the
10 equilibration of heat generation and dissipation during the polymerization. The heat generation at increased temperature in this situation was not faster due to the decrease of the concentration of monomers during polymerization after a certain amount conversion of the monomers. The self-acceleration of the polymerization also does not happen due to the decreased concentration of
15 monomers. In this invention, the linear gradient of polymerization temperature was optimized to couple with low temperature polymerization and high temperature curing process to achieve optimal distribution of the sizes of the separation-effective openings of the porous polymer for chromatographic separations.

20 In one embodiment of this invention, a linear gradient of polymerization temperature from ambient temperature to 70°C was used for preparation of the porous polymer with good chromatographic properties. In another embodiment of this invention, a linear gradient of polymerization temperature from 40°C to 60°C in combination of initial polymerization at 40°C and curing at 60°C was

used to prepare a separation media with good chromatographic properties.

The programmed step, multi-step or linear increase of polymerization temperature is not only applicable to large diameter columns but also very useful for preparation of small diameter columns to improve the chromatographic properties of the media. It was found that this method could be used for scaling up preparation of the chromatographic columns from small to large diameter columns. In one embodiment of this invention, the exact same program of temperature was used to prepare the columns with diameters of 4.6 mm and 34 mm to achieve the same chromatographic properties of the separation media. In another embodiment of this invention, the programmed temperature is modified to prepare the columns with 34 mm diameter.

In FIG. 18, there is shown a graph 352 having abscissae of time, a left axis ordinates of temperature and a right axis of ordinates of the percentage of completion of polymerization with two solid curves 354 and 356 and two dashed line curves 364 and 366. The curve 354 is a curve showing temperature and the curve 364 is a curve showing the percentage of completion for different amounts of lapsed time for polymerization at a low constant temperature on the surface of the column that maintains the temperature in the polymerization mixture below the self sustaining temperature. The polymerization rises rapidly and then levels off at a value of polymerization that is too low. The low temperature results in a lack of stiffness and inhomogeneous polymer. The lack of stiffness is the result of the low temperature that reduces cross-linking to a low value as soon as the gel effect becomes significant and increases the size of the separation-effective openings to an undesirable size. Generally

there will be an increase in temperature between the center of the column and the surface of several degrees Centigrade resulting in a non-homogeneous polymer. The curve 366 illustrates the percentage completion for different amounts of lapsed time between the control-initiation point 358 and the safe-point 360 and from the safe-point 360 to a substantially complete point 362 for a temperature gradient process of polymerization and the curve 356 shows the change in temperature at the surface of the column between the same points.

The temperature at the surface of the column increases more slowly and the rate of polymerization between the control-initiation point 358 and the safe-point 360 increases slowly and does not result in a significant increase in the temperature of the polymerization mixture up to the safe-point 360. The temperature prior to the control-initiation point 358 increases faster to a point where the polymerization is initiated and then very slowly since there is little steric hindrance and there is ample monomer to react. At the safe-point 360 the steric hindrance has increased and the amount of monomer decreased and the temperature can be increased to cause more cross-linking and to drive the polymerization reaction to completion. The rate of increase at the surface of the column varies with the composition of the polymerization mixture and desired characteristics of the monolith but between the control initiation point and the safe point is generally lower than 5 degrees Centigrade per hour and after the safe-point is reached is generally more than 15 degrees Centigrade per hour.

In FIG. 19, there is shown a fragmentary longitudinal sectional view of a column 372 having a central longitudinal axis 374 with a thermistor 380 positioned close enough to measure its temperature and an imaginary

concentric column 376 midway between the outer surface 378 and the central longitudinal axis with a thermistor 382 positioned close enough to measure its temperature at this quarter point in the column. The temperature of the external surface is controlled by any heating or cooling means but in the preferred
5 embodiment is a water bath, the temperature of which may be measured by any means such as the thermistor 384.

A temperature profile 370 across column 372 is shown as it may appear during one mode of temperature gradient polymerization. In this mode of temperature gradient polymerization, the outside temperature of the column is
10 maintained at the same temperature as the temperature at the center of the column and both temperatures are caused to increase gradually by controlling the temperature at the outside surface of the column. As illustrated by the temperature profile 370, the temperature at which the outside temperature is increased at a slow rate so as to control the rate of reaction to a level that
15 maintains the rate of generation of exothermic heat substantially the same as the heat dissipation and the external temperature is slowly increased with the rate of increase at the outside surface equal to the rate of increase at the center, there is a low point at the concentric cylinder. This low point should be maintained within two and one half degrees of the outer temperature and
20 preferably within one degree for homogeneity. The gradual increase in temperature is intended to compensate in part for the gel effect and maintain a good rate of polymerization with a homogeneous polymer in view of exothermic generation of heat in the column between the control initiation point and the safe point to decrease the time needed for polymerization.

FIG. 21 is a chromatogram of a separation in a temperature-time moderated column having the following chromatographic conditions: (a) sample: (1) ribonuclease A, (2) cytochrome C and (3) lysozyme; (b) column: WCX (250 by 35mm I.D.) prepared by polymerization at a gradient temperature of 40-60 degrees C in 24 hours and then further curing at 60 degrees C for 12 hours; (c) mobile phase: buffer A: 10 mM phosphate buffer, pH=7.6, buffer B: 1M NaCl in buffer A, pH=7.6, gradient: 20-50 percent B in 4 CV, then 50 to 100 percent B in 0.8 CV; flow rate: 50 ml/min..

The permeable polymers described in this specification may have more than one suitable configuration. One configuration has a desirable separation-effective opening size distribution for some target applications. In general, it includes small separation-effective openings less than 300 nm in at least one direction that provide high surface area for separation, and large irregular openings that provide little or no separation such as larger than 500 nm for the majority mobile phase to go through. Preferably the sizes of the separation-effective openings are between 50 and 200 nanometers and the larger irregular openings are between 2-5 microns for medium and low pressure separations and 0.6 to 2 microns for high pressure separations. The separation-effective opening size distribution and the irregular feature size distribution can be controlled by the types and amount of porogens, monomers, initiators and polymerization temperature, time and pressure. In one embodiment, the monomers are selected not only to have desired functionality, but also to help improve the column efficiency by changing the kinetics of polymerization and polymer structure, which leads to more ideal separation-effective opening size

distribution. The ratio of monomers is selected for the same purpose. The type and amount of porogens are selected after careful investigation for the generation of the desired separation-effective opening size distribution. The use and selection of pressure during polymerization is particularly important for the generation of the desired separation-effective opening size distribution and the homogeneity of the separation-effective opening size distribution throughout the whole column. It also prevents the formation of irregular voids and wall channels which happened in conventional sealed or open polymerization.

It has been found that the formation of micropores can be drastically reduced or prevented by using pressure during polymerization and the careful tuning of the other polymerization conditions and reagents. From Scanning Electron Microscopy (SEM) studies of this polymer having separation-effective openings, it is found that the polymer particle morphology is similar to some form of coral. The coral-like polymer is formed of interconnected corrugated particles which apparently have grown by accretion. The interior of these particles are non-porous. The surface is highly corrugated and contains huge number of small open shallow grooves with various sizes of openings. In SEM study of one of the polymers, the particles are core-shell structured with short depth of the openings. These unusual corrugated polymer structures and core-shell particle structures without through pores in the individual particles greatly improve the capacity of the monolith compared to regular non-porous separation media while avoiding the mass transfer problem in conventional macroporous media containing a large number of micropores and mesopores inside the particles or beads. These structures are also dramatically different

from the so called "Perfusion Beads" or monoliths with though pores disclosed in the literatures. Conditioning the aggregates of particles in some columns by the application of pressure or by holding the volume against expansion when internal forces tend to swell or expand the polymer results in stacked generally flat or nested configuration rather than the aggregated substantially round aggregates of particles.

The monolith in this invention combines the advantages of high resolution in non-porous particle packing and the high capacity of macroporous packing while avoiding their problems. These corrugated particles may grow by accretion from polymer nucleus which are swelled and surrounded by monomers and active oligomers, and merging with other polymer nucleus. These particles aggregate with each other and are reinforced by crosslinking. This structure improves the column efficiency greatly by prevention of the trapping of sample molecules in the micropores, and in the pores inside the particles, which are one of the major reasons for zone spreading according to the theoretical model. The size of the particles, aggregates or clusters can be finely tuned to be more homogeneous, and the separation-effective opening size distribution can be improved to give high resolution separation by careful control of pressure in combining with the selections of other factors discussed earlier.

Satisfactory separation of more hydrophilic compounds in liquid chromatography often requires the starting mobile phase to be 100% water with no organic solvent. This type of separation can not be achieved to a satisfactory extent with reversed phase media based on pure styrene/divinylbenzene,

polymethacrylates and their derivatives containing C4, C8, C12 and C18, which are very hydrophobic. The polymers shrink in aqueous mobile phase with low organic solvent contents. The shrinkage results in void space between the column wall and the polymer media, which leads to so called "wall channeling" in chromatography. As the consequence, the sample and mobile phase bypass the media and go through wall channels instead of the media. The sample is not retained or partly retained which results in multiple peaks for each pure sample.

In one embodiment, wall effect is avoided by first shrinking the media down to the maximum extent by passing pure water or salt liquid mixture through the media, and then followed by compression of the media with piston fittings until the void space between the wall and the polymer media is sealed. The piston is held in place by a nut fitting. The fittings are shown in FIGS. 3 and 4. The shrinkage and sealing of the wall void can be monitored by first decreasing then increasing the back pressure of the column. This process prevents the formation of the "wall channeling" during the separation process. In one embodiment, the polymer is shrunk in pure water and compressed with PEEK piston fittings. In another embodiment of this invention, the polymer is shrunk in 1 mol/l NaCl liquid mixture and compressed with PEEK piston fittings.

In highly polar environments, the linear polymer chain, and the chains of C4, C8, C12, C18 on the polymer surface collapse to the surface resulting in poor interaction between the sample molecules and the surface of the media. Also, the bed is very poorly wetted by the mobile phase due to the extreme difference in polarity of the media and mobile phase. The mass transport and

interactions between the sample and stationary phase is very poor, which result in low column efficiency and resolution. These problems and the problem of "wall channelling" are reduced by increasing the hydrophilicity of the polymer matrix while maintaining the desired hydrophobicity for sample retention and separation.

The polymer matrix contains hydrophilic functional groups such as hydroxyl, amide, carbamide or hydrophilic moieties in the polymer repeating units. The polymer can be wetted and swelled by water due to the hydrophilicity of the polymer matrix. The surface of the polymer media still contains highly hydrophobic polystyrene chain, or C4, C8, C12 and C18 chains for the hydrophobic interaction in reversed phase chromatography. The shrinkage of the polymer in water is reduced or completely prevented, which also solve the problem of wall channeling. The hydrophilicity can be improved by direct copolymerization of monomers containing hydrophilicity moieties, or by modification of polymers to incorporate the hydrophilic moieties.

In one embodiment of this invention, hydrophilic hydroxylethyl methacrylate is copolymerized with styrene and divinylbenzene for the prevention of "wall channeling" and collapse of the hydrophobic interaction chains in water. In one embodiment of this invention, stearyl acrylamide is copolymerized with stearyl methacrylate and ethylene glycol dimethacrylate. The addition of hydrophilic monomers also may decrease protein denaturation in reversed phase columns. In one preferred embodiment, acrylonitrile is copolymerized with styrene and divinylbenzene. The polymers swell more and more with the increase of the hydrophilicity of the hydrophilic monomers. The

reverse phase separation media constructed with the polymer containing hydrophilic moieties will swell in both aqueous and non-aqueous liquid mixtures. This enlarges the applicability of reversed phase separation media in aqueous mobile phase.

5 *In situ* polymerization can be used to prepare the columns with any sizes and shapes. In one embodiment, a capillary column with cylindrical shape of inner diameter of 75 micrometers was prepared. In another embodiment, a column with 4.6 mm ID was prepared. In another embodiment, a column with 88 mm ID was prepared. In another embodiment, a square capillary column
10 with cross-section of 100 micrometers and on up to 700 micrometers was prepared. In another embodiment, a polymer disk with 3 mm thickness and 1 cm inner diameter was prepared. In another embodiment, a donut shape monolith with 1 cm outer diameter and 4.6 mm inner diameter was prepared. In another embodiment, a microchip column with 100 micrometers inner
15 diameter grooves was prepared.

Hydrophobic interaction chromatography requires very hydrophilic separation media with mild hydrophobicity. Upon further increase of the hydrophilicity of the matrix with less hydrophobic carbon chain or polymer chain, the reversed phase media can be turned into hydrophobic interaction media.

20 Normal phase chromatography requires hydrophilic media, whose surface is fully covered by hydrophilic functional groups. Hydrolysis of the epoxy group in poly(glycidyl methacrylate-co-ethylene glycol dimethacrylate) was used in prior art to obtain normal phase separation media. The Normal Phase separation media is prepared by *in situ* direct polymerization of

hydrophilic monomers containing hydrophilic functional groups such as hydroxyl and amide. In one embodiment hydroxylethyl methacrylate is copolymerized with a crosslinker, such as EDMA, to obtain normal phase media. In one embodiment of this invention, the column hardware is a polypropylene barrel reinforced with glass fibers.

The reversed phase monolithic media prepared according to prior art has extremely low capacity and is compressed during separation. The loading capacity of the liquid chromatography media and the rigidity of the media is increased by increasing the crosslinking density of the media. The crosslinking density is increased by using higher amounts of crosslinker, such as divinylbenzene, in poly(styrene-co-divinylbenzene) monolith. In one embodiment of this invention, 100% of the crosslinker is divinylbenzene (80% purity which is the highest purity grade available commercially.). The capacity is six times higher than the monolith prepared in the prior art. The high capacity monolith prepared under pressurized polymerization has high resolution as well as high capacity. In one embodiment of this invention, 90% of the divinylbenzene (80% purity) in total monomer is used. In another embodiment, 80% of the divinylbenzene (80% purity) in total monomer is used.

Another method of improving the rigidity and resolution of the media is by increasing the total polymer density in the column. The total polymer content is increased by increasing the total monomer content in the mixture. By increasing the total monomer content in the polymerization mixture, the resolution of column is improved as well. The separation-effective opening size and its distribution are highly affected by the total monomer concentration in the

polymerization mixture. In one embodiment of this invention, 46% weight percent of total monomers is used to improve the rigidity and resolution of the media.

The monolithic media prepared in the prior art has poor resolution, low speed of separation, low rigidity and extremely low capacity. The prior-art monolithic polymethacrylate based weak anion exchanger was prepared by modification of poly(glycidyl methacrylate-co-ethylene glycol dimethacrylate) with neat diethylamine. It swells extensively in water and can not be used at high flow velocity. This medium has very low rigidity and is not stable at flow velocities more than 6 cm/min. The back pressure of the column keeps increasing during the runs. Two methods of improving the rigidity of the hydrophilic medium are provided.

First, the rigidity of the medium can be improved by increasing the crosslinking density of the polymer matrix. At low crosslinking density, there are a lot of non-cross linked linear polymer chains which are solvated by water and extend out to the solvents. The polymer matrix expands due to this extensive solvation. The expansion of polymer matrix in a polymer narrows the size of the separation-effective openings and interstitial spaces between the interconnected particles. The porosity is also decreased. These result in high back pressure. The highly solvated porous polymer has characteristics of soft gel. Under a pressure, the soft polymer can be compressed easily and leads to higher pressure. The increase of pressure will further compress the medium and lead to even higher pressure. The cycle of pressure increases and compressions makes the prior art monolith not useful for the application in high

speed separation.

Upon the increase of crosslinking density, the swellable linear polymer chains are shortened and the swelling is reduced. The polymer with separation-effective openings becomes more rigid. The structure with separation effective openings is maintained in aqueous solvents. High porosity and larger separation-effective opening size can be obtained with highly crosslinked polymer matrix, which allows higher flow rate to be used without the detrimental cycles of the compression and pressure increase. High speed separation can be achieved by using high flow rate.

In one embodiment of this invention, the cross linking density of the ion exchanger is greatly improved by using 70% crosslinker, ethylene glycol dimethacrylate (EDMA). In a preferred embodiment, the amount of EDMA is 50%. In another preferred embodiment, the amount of EDMA is 60%. EDMA is more hydrophobic than its copolymers containing ion exchange groups. By increasing the amount of EDMA, the hydrophilicity of the polymer matrix is reduced. This results in a decrease of swelling and improves the rigidity. This is the additional advantage from using more hydrophobic cross linker instead of hydrophilic crosslinker when high rigidity of the polymer in aqueous phase is highly desired.

Second, the rigidity and column efficiency of the polymer separation media are both improved by controlled modification in this invention. The glycidyl methacrylate (GMA) is hydrophobic before it is modified to contain ion exchange functional groups. The GMA in prior art monolithic weak anion exchanger (WAX) is modified by reaction with neat diethylamine at 60°C for 3

hours. Neat diethylamine can swell the polymer and diffuse into the polymer particles to access the GMA epoxide groups. This modification reaction modifies not only the GMA moieties on the separation-effective opening surface of the polymer but also those inside the polymer matrix. The hydrophilic moieties containing the ion exchange functional groups intermingle with hydrophobic backbone both inside and outside the separation-effective openings after modification. This non-selective modification makes the whole polymer matrix swell extensively in water while some hydrophobic backbones are exposed on the surface of the separation effective openings. The hydrophobic patches on the surface of the separation openings can result in secondary hydrophobic interaction during ion exchange chromatography separations, which leads to zone-broadening.

A controlled modification of the GMA on the surface of the polymer particles can keep the internal part of the particle more hydrophobic and less swellable in water. After modification of the surface GMA, the surfaces of the particles become much more hydrophilic and attract the water molecules. Those more hydrophobic backbones retreat to an inner part of the polymer particles to stay with more hydrophobic cores of the particles, and get away from the very polar buffer environment during chromatography separation. This increases the coverage of surface with hydrophilic ion exchange groups and prevents the zone-broadening from secondary hydrophobic interaction. The controlled surface modification is accomplished by catalyzed modification reaction in aqueous liquid mixture at lower temperature. The catalyst is preferably an acid or reagent which can generate protons *in situ*.

In the preferred embodiments of this invention, a dialkyl amine hydrogen chloride salt is used as a catalyst. The salt liquid mixture is very polar and has less tendency to swell the hydrophobic polymer. The ionic catalyst tends to stay in liquid mixture instead of diffusing into the very hydrophobic internal matrix.

5 The lower reaction temperature reduces the swellability of the polymer. Diethyl amine might diffuse into the polymer matrix but the reaction of diethyl amine with GMA at low temperature is very slow and insignificant. In one embodiment of this invention, the dialkyl amine hydrogen chloride catalyst is diethyl amine hydrogen chloride. In another embodiment of this invention, the catalyst is
10 trimethyl amine hydrogen chloride. In one embodiment of this invention, the reaction temperature is 25°C. In another embodiment of the invention, the modification temperature is 30°C.

The prior art processes for the synthesis of monolithic weak cation exchangers are based on membrane, beads and gels and none of them can be
15 used directly in the *in situ preparation* process of monolithic columns. Seven methods for preparing a weak cation exchanger are described below. All the modification reactions in these methods are carried out by pumping the modification liquid mixture through the column continuously at a selected temperature, or the reagents are sealed inside the column and heated in a
20 heating bath or oven after the reagents are pumped into the column.

The first method is the two-step modification of poly(glycidyl methacrylate-co-ethylene glycol dimethacrylate) (PGMAEDMA) with chloroacetate salt. Sodium chloroacetate has been used to modify hydroxylethyl methacrylate based material to obtain carboxylic acid groups in the literature.

In order to take advantage of the above reaction for the modification of monolith, the epoxide ring in GMA is first opened to obtain hydroxyl group by hydrolysis using 1 M H_2SO_4 aqueous liquid mixture. In the second step, chloroacetate couples with the hydroxyl group in the polymer to attach the carboxylic group to the polymer. This reaction is catalyzed by strong base such as sodium hydroxide. The reaction temperature is from 40 to 80°C, preferably from 50 to 70°C. The reaction time is varied from 1 to 24 hours, preferably less than six hours. In one embodiment of this invention, the modification reaction takes place by pumping 5 M sodium hydroxide aqueous liquid mixture through the monolithic column at 60°C for 2 hours. The capacity of this media is not ideal although the column efficiency is good. The capacity can be increased by longer reaction and higher reaction temperature. However, the separation medium becomes soft due to the side hydrolysis reaction of the esters in the polymer. The crosslinking density is lowered since the crosslinker EDMA is hydrolyzed as well.

The second method is a one-step modification of the GMA in the polymer to obtain the carboxylic functional groups using glycolic acid as reagent. Glycolic acid is reacted with PGMEDMA at a temperature between 40 to 90°C for 1 to 24 hours. This reaction is a self catalyzed reaction since glycolic acid is a catalyst itself. The reaction can be catalyzed by other stronger acid such as trifluoroacetic acid (TFA). The reaction is simple but the capacity of the weak cation exchanger is low due to a parallel side reaction. The epoxide ring can be opened by hydrolysis reactions as the side reaction. In order to prevent this reaction, the non aqueous solvent is used. Preferably, solvent containing

protons is used. In one embodiment of this invention, glycolic acid liquid mixture in formic acid containing TFA catalyst is pumped through the column for 3 hours at 80°C.

The third method is a double modification of the PGMEDMA with both glycolic acid and chloroacetate. There are several advantages of the double modification reactions. First, they can all be performed in aqueous liquid mixture. Second, both reaction steps lead to desired product. Third, the side reaction of the first step leads to the desired functional group for the second step modification. Fourth, the conditions of double modification reaction can be milder than the single reaction to obtain the same or higher capacity while avoiding the hydrolysis of the backbone which maintains the rigidity of the matrix. In one embodiment of this invention, the first reaction is performed in glycolic acid aqueous liquid mixture containing TFA as catalyst and the second reaction is the substitution reaction of chloroacetate by NaOH aqueous liquid mixture.

The fourth method is a one-pot reaction of glycolic acid and chloroacetate. Instead of the double sequential reactions, both reagents are put into the liquid mixture together during reaction. The reaction with glycolic acid is base-catalyzed instead of acid-catalyzed. This method has the advantage of the third method but with lower capacity due to less reactivity of the base-catalyzed ring-opening reactions by glycolic acid in water.

The fifth method is a hydrolysis reaction of acrylates or methacrylates. The hydrolysis of the ester groups leads to the carboxylic functional groups. The

direct hydrolysis of PGMEDMA membrane or beads is known in the prior art. However, the resulting media did not have either good capacity or separation. It is discovered in our work that both the resolution and capacity can be dramatically improved by hybridizing the hydrophilic and hydrophobic acrylates or methacrylates. The hydrolysis reaction is much more efficient since the water molecule can diffuse into the surface of the particles and wet the surface much better due to the hydrophilic moieties of the acrylates. The reaction can be catalyzed by both acid and base, such as TFA or NaOH aqueous liquid mixture. In one embodiment of this invention, poly(methyl methacrylate-co-hydroxyethyl methacrylate-co-ethylene glycol diemthacrylate) is prepared and hydrolyzed to obtain a weak cation exchanger. In another embodiment of this invention, poly(hydroxyethyl methacrylate-co-ethylene glycol dimethacrylate) is hydrolyzed. In another embodiment of this invention, PGMEDMA is hydrolyzed by acid first and base in the second step. The weak cation exchanger obtained in this method is softer due to the hydrolysis of the backbone crosslinker.

The sixth method is a direct copolymerization of acrylic or methacrylic acid. The direct copolymerization of the acid leads to the weak cation exchanger in one step. This method greatly simplifies the preparation method. The capacity of the weak cation exchanger is relatively higher than the modification method but still not ideal. The ratio of the acidic monomer to crosslinking monomer is between 2% to 30%, preferably 5% to 15%. With the higher content of the acid monomer, the capacity is higher but the media is softer. The direct polymerization method is applicable to the preparation of monolithic membranes, columns, chips, tubes or any format known in the art.

The seventh method is the combination of direct copolymerization and the controlled modification. It was discovered in this invention that this combination leads to high capacity while maintaining the rigidity of the media. The resulting media can be used for high-throughput separation using high flow velocity. The improved capacity by direct polymerization of acrylic or methacrylic acid reaches a limit due to the softness of the media containing a high amount of the acid. The acidic monomers are randomly polymerized and dispersed throughout these matrixes. These acids are converted to salts in buffer and resulted in extensive swelling of the media in aqueous mobile phase. Also, the hydrophobic backbone consists of carbon chains and esters are exposed on the surface resulting in secondary hydrophobic interaction during ion exchange chromatography separations. This leads to zone-broadening and tailing. The hydrophobic surface can be further modified to become hydrophilic while improving the capacity. The controlled modification improves the capacity and hydrophilicity of the media while preventing the softness of the media. Over-modified media leads to the modification inside the particles besides the modification on the surface. As discussed in the preparation of weak anion exchanger, the modification inside the particle results in extensive swelling which blocks the separation-effective opening or changing of the morphology which leads to detrimental cycle of pressure increase and compression. In one embodiment of this invention, weak cation exchanger is prepared by copolymerization of acrylic acid, methyl methacrylate (MMA) and EDMA in the first step, and hydrolysis of the methyl methacrylate in the second step. The hydrolysis of MMA is base-catalyzed and accelerated by the presence of very

hydrophilic acrylate salt, which is the conversion product of the acrylic acid after reaction with NaOH.

This methodology of combining direct polymerization and modification is applicable to the preparation of all hydrophilic polymer supports which require a high number of functional groups and rigidity of the matrix at the same time. It is applicable in preparation of monolithic tubes or columns, monolithic membranes, monolithic capillary and chips or any other monolith in different format, as well as polymeric particles, gels, membranes or any other type of polymeric separation media. In particular, the resolution and capacity of a monolithic membrane can be improved with this method. The improvement can be achieved by *in situ* process or by off-line process. The monoliths or beads obtained by direct polymerization can be modified by pumping the reaction liquid mixture through the packed columns or membranes, or immersing them into the modification liquid mixture. The beads can be suspended in the modification liquid mixture. By using this methodology, a high capacity strong anion exchanger (SAX) and a strong cation exchanger (SCX) were developed.

The prior art processes for making monolithic strong anion exchangers are based on membranes, beads and gels and are not applicable to the manufacture of monolithic strong anion exchange columns. Three methods of preparing monolithic strong anion exchange columns *in situ* are provided below.

Method one is the combination of highly rigid polymer and controlled modification of the surface. Modification of PGMEDMA with trimethylamine hydrogen chloride has been used to obtain membrane and bead based strong anion exchanger. When the reaction is used for preparation of monolithic strong

anion exchangers, the resulting media is soft and can not be used for high speed separation. The rigidity is improved in two ways as in the preparation of monolithic weak anion exchanger in this invention: High crosslinking density and Controlled Modification reaction.

5 The basic polymer for SAX is formulated to contain high crosslinking density by using higher ratio of crosslinking monomer to functional monomer. The amount of crosslinker is increased to more than 50% of the total monomers in the polymer. In one embodiment of this invention, 60% EDMA in total monomers is used. The porogens and their ratios are selected to offer optimal
10 resolution at relatively low pressure.

 The controlled modification is accomplished by catalyzed amination of the PGMEDMA. The catalyst can be any base known in the art. In one embodiment of this invention, trimethyl amine is used as catalyst. The amount of the catalyst is from 1% to 50% volume of the liquid mixture, preferably
15 between 10% and 30%. The reaction temperature is between 10 to 60°C, preferably between 20 to 50°C. The reaction time is between 10 minutes to 24 hours, preferably between 1 to 4 hours. The selected catalytic reaction modifies the surface of the particles more than the internal part of the particles, which results in the media to be used at high flow rate. In one embodiment of this
20 invention, the reaction is carried out at 40°C for 3 hours.

 Method two is the direct copolymerization of monomers containing the quarternary amine, or their intermediate which can generate the quaternary amine *in situ*. In one embodiment of this invention, the functional monomer containing quaternary amine is 2-(acryloyloxyethyl] trimethylammonium methyl

sulfate (ATMS). The polymer has high crosslinking density. The ratio of the crosslinking monomer in the total monomers is between 50% to 70%. In one embodiment of this invention, 60% EDMA is used. The amount of ATMS is between 2% to 20%, preferably between 5% to 15%. The third monomer which makes up the rest of monomer is preferred to be hydrophilic monomers such as HEMA although hydrophobic monomer can be used as well.

Method three is the combination of direct polymerization and controlled surface modification shown in method two and one. The strong anion exchanger obtained by method one is rigid and have high resolution. However, it suffers from non-ideal capacity. Method two improves the capacity but not sufficient and suffers from lower resolution. The combination of direct polymerization and controlled surface modification doubles the capacity and improves the resolution and recovery. The recovery of proteins is improved since the surface is fully covered by hydrophilic protein benign groups. Secondary hydrophobic interaction, which is the main reason for lower protein recovery, is minimized. The porogens are researched and selected to offer the desired flow rate. In one preferred embodiment of this invention, the combination of butanediol, propanol and water is used as porogens. The polymerization mixture and conditions are formulated to offer the optimal resolution at the desired flow rate.

Prior art processes for preparing monolithic strong cation exchangers are based on membrane, beads and gels and are not transferable to the *in situ* preparation of monolithic strong cation exchange columns. Three methods for preparing monolithic strong cation exchange columns *in situ* are provided

below.

Method one is the modification of PGMEDMA with butane sultone or propane sultone catalyzed by strong base soluble in organic solvent. Modification of PGMEDMA with propane sultone using NaOH liquid mixture as the catalyst has been used to prepared membrane or bead-based strong cation exchanger. The reaction was a two-phase reaction since propane sultone is not soluble in NaOH aqueous liquid mixture. The two-phase reaction mixture can not be pumped through the column to carry out the modification. Several approaches have been taken to carry out the modification reaction.

Approach one is a two-step modification reaction consisting of activation of the media with strong base such as potassium t-butoxide in the first step followed by nucleophilic ring-opening reaction with butane sultone. Butane sultone is preferred since it is a liquid and propane sultone is a solid at room temperature. Potassium t-butoxide is preferred since it has higher solubility than its sodium counterpart. The solvent is a good solvent of a reagent such as dimethylsulfone (DMSO). The modification liquid mixture has to be homogeneous in order to be pumped through the column for *in situ* modification. Approach two is a one-pot reaction consisting of both activation and modification steps. Both strong base and butane sultone are dissolved in a strong solvent. The liquid mixture is pumped through the column continuously or sealed at a selected temperature for several hours. The reaction temperature is preferably between 80 and 120°C. In one embodiment of this invention, 90°C is used. In another embodiment of this invention, 120°C is used.

Method two is a direct polymerization of monomers containing a strong

cation exchange group. In the preferred embodiment of this invention, 2-Acrylamido-2-methyl-1-propanesulfonic acid (AMPS) is used as the functional monomer containing sulfonic group. The amount of AMPS is between 2% to 20%, preferably 5% to 15%. The capacity of this polymer is greatly improved compared to the first method. The polymerization mixture is formulated to offer the optimal resolution at the desired flow rate.

Method three is the combination of direct polymerization and controlled modification. In one embodiment of this invention, AMPS is copolymerized with GMA and EDMA. The polymer is further modified by controlled modification as described in method 1. Both the capacity and resolution is greatly improved compared to methods 1 and 2. The amount of EDMA is preferably between 50% to 70%. The amount of AMPS is preferably between 2% to 15%. The rest of the monomer is GMA. In another embodiment of this invention, the AMPS is copolymerized with HEMA and EDMA. The porogens are researched and selected to offer the desired flow rate. The polymerization mixture and conditions are improved to offer high resolution and high speed chromatography.

The controlled modification of hydroxyl containing polymer matrix to contain the sulfonic group for SCX was found to be very effective by using the following process. In one embodiment of this process, the glycidyl methacrylate in the copolymer matrix was hydrolyzed to contain two hydroxyl groups. These hydroxyl groups were further modified with chlorosulfonic acid. In another version of this process, the modification was performed with a pyridine salt liquid mixture of chlorosulfonic acid. The first process is shown in equations 1

and 2 of FIG. 20 and the second version of this process is shown in equation 3 of FIG. 20.

Preparation of large diameter monolithic columns for effective chromatography separation by *in situ* polymerization method has been a very difficult task due to the heat isolating effect of polymer formed by exothermic polymerization. It was found that the heat transfer is fast enough to prevent the inhomogeneity of the polymerization temperature as long as the shortest distance (defined as radius in this writing) between the center of the monolith to the surface of the monolith is less than 8 mm depending on the materials of the column hardware.

One technique for preparing large diameter monolithic columns, with reduced heat of polymerization problems, is to use multiple staged polymerizations. In this technique, the resulting polymer monoliths in each stage of polymerization have radius up to 8 mm if the mold for polymerization is made of good heat transferring material. This is accomplished by first preparing columns with a radius of less than 8 mm and using them as fillers for the second stage polymerization, in which the radius of the polymerization liquid mixtures between the fillers and the column wall is also less than 8mm, and the distance between the fillers is less than 2 mm. It is found in this work that the thickness of the polymerization liquid mixture between the fillers less than 2 mm has insignificant effect on the variations of the polymerization temperature. Multiple thin polymer columns are filled into a large diameter column and filled with the second stage polymerization mixture. The column is sealed with regular fittings or fittings to allow pressurization during polymerization. The large

diameter column is then placed into a temperature controlled heating bath or oven to carry out the second stage polymerization. The thin columns are prepared by the process disclosed above with pressurized or non-pressurized polymerization. The thin monolithic columns prepared in the first stage polymerization are preferably preserved without washing and further modification. A polymerization mixture for the second stage polymerization is the same or different from the polymerization mixture of the first stage polymerization depending on the types of media.

In this process, the thin columns with a radius of less than 8 mm can be solid rods, discs, hollow tubes with thickness of the cylinder wall less than 8 mm, or a membrane. The shapes of the above thin columns can be any shape known in the art, such as round, rectangular, triangle, etc. It is perceivable that the fillers can be other particles described in the section of filler materials in this specification.

In one embodiment of this invention, multiple thin columns with radius of 5 mm are used. In one preferred embodiment of this invention, monolithic polymer rods with a size of 50 mm x 10 mm I.D. are used as fillers. In another preferred embodiment of this invention, monolithic polymer rods with a size of 10 mm x 34 mm I.D. are used as fillers. In another preferred embodiment of this invention, the monolithic polymer cylinder with various inner and outer diameters are used as fillers.

Another technique for preparing large diameter columns is to use temperature-time moderation as described earlier. In using this technique, weak cation columns and strong anion columns have been prepared and it is

understood from these results that the other types of columns can be prepared with temperature-time moderation as well. One method of making a weak cation column, comprises the steps of applying a polymerization mixture comprising 1 part of GMA to between 4 and 6 parts of MMA and 10 and 14 parts of EDMA and an initiator into a container and shaking the mixture gently until the mixture becomes a homogeneous liquid mixture. Then a porogen is added into the homogeneous liquid mixture and it is shaken until the new mixture is homogeneous to form a polymerization liquid mixture. The polymerization liquid mixture is usually degassed at this point and a column is filled with the polymerization liquid mixture. Of course the liquid mixture could be initially prepared using the column as a container or part of the container for mixing the polymeric mixture. The polymerization liquid mixture is polymerized in the column under temperature-time moderation conditions to form a plug and the plug is washed to remove the porogen.

For some types of columns, the column preferably includes means further applying pressure to the polymerization liquid mixture. In these embodiments, after the column is sealed and polymerization initiated, pressure may be applied to the polymerization mixture as described earlier. In one embodiment, the polymerizing mixture is polymerized at a gradient temperature starting at the control initiation point at a value between 35 and 45°C and gradually increased to a safe point in 12 hours and cured at a temperature of between 55 and 65°C for 24 hours. In another embodiment, the polymerizing mixture is polymerized at a temperature of between 35 and 45°C for 72 hours and then cured at a temperature of between 55 and 65°C for 24

hours.

Similarly, a strong anion column has been prepared by applying a polymerization mixture comprising between 2 and 4 parts of GMA to between 2 and 4 parts of ATMS to between 7 and 11 parts of EDMA and an initiator into a container, shaking the mixture gently until the mixture becomes a homogeneous liquid mixture, weighing a porogen into the homogeneous liquid mixture and shaking it until the new mixture is homogeneous to form a polymerization liquid mixture, degassing the liquid mixture, filling a column with the polymerization liquid mixture and polymerizing the polymerization liquid mixture in the column under temperature-time moderation conditions to form a plug. The plug then may be washed to remove the porogen.

As in the making of a weak cation exchanger, the column may include means for applying pressure to the polymerization liquid mixture further comprising the steps of sealing the column and applying pressure to the polymerization mixture. In one embodiment the polymerizing mixture is polymerized at a gradient temperature starting at the control initiation point at a value between 35 and 45°C and increasing gradually to a safe-point at between 55 and 65°C in 12 hours and cured at a temperature of between 55 and 65°C for 24 hours. In another embodiment, the polymerizing mixture is polymerized at a temperature of between 35 and 45°C for 72 hours and then cured at a temperature of between 55 and 65°C for 24 hours.

The performance of capillary columns also can be improved by the procedures described earlier. One method is to choose the right combination of porogenic solvents to generate separation media with and without pressure.

The choice of solvents with the right polarity and solvating power of the polymers can result in porous polymer support with no micropores or small pores which can affect separation efficiency of the column. Exertion of pressure during polymerization will further improve the uniformity of the media and avoid the formation of micropores. In one embodiment, the capillary columns of internal diameter 320 micrometers is prepared with the combination of solvents including chlorocyclohexane and 1-decanol to generate the monolithic porous polymer support containing no micropores or small pores which result in poor mass transfer of the sample molecules with and without the pressure of 120 psi. In another embodiment, the combination of solvents including 1-ethylhexanoic acid and mineral oil has been used to prepare monolithic porous materials containing no micropores with and without pressure.

The employment of X-ray, UV-vis can improve the performance of capillary greatly. X-rays can penetrate materials with low energy and with low intensity loss. X-ray can penetrate a capillary with almost no intensity loss. Sensitizers or scintillators can absorb X-ray energy transferred by the solvents effectively and emit fluorescence or phosphorescence light homogeneously in the liquid mixtures. The homogeneous fluorescence and phosphorescence light can be absorbed by initiators which initiate the polymerization homogeneously in the polymerization liquid mixtures. This leads to homogeneity of the porous structure of the porous polymer support including monolithic separation media and particles. This improves the column efficiency of the monolithic capillary greatly. The low temperature polymerization using X-ray as the energy source results in a slow polymerization rate due to the lower polymerization

temperature. Fine tuning the intensity and energy of X-ray results in the desired polymerization rate which can lead to the formation of homogeneous separation media. The employment of X-ray, scintillators/sensitizers, solvents with right solvating powers and the pressure during polymerization can leads to the formation of separation media with no micropores or small pores with similar size to the sample molecules which leads to greatly improved performance. In one embodiment, capillary columns have been prepared using X-ray as energy source. In another embodiment, microchip columns have been prepared with X-ray as energy source.

The right choice of solvents with a reflective index very close to the polymers allows the light to travel through the capillary with little loss of intensity of the light, which is known as Christiansen Effect and described earlier. The use of initiators having Bleaching Effect allows the UV-vis light to travel through the capillary columns with negligible loss of intensity. The lights are homogeneous in the polymerization liquid mixtures. The absorptions of the homogeneous light result in homogeneous initiations of the polymerization which is unlike the initiation promoted by thermal heating or the UV-vis initiated polymerization without the consideration of the Christiansen effect and bleaching effect. This leads to the formation of homogeneous polymerization in the liquid mixture. As the result, more homogeneous porous structure can be formed. This leads to the much improved performance of the capillary columns. The combination of the above method with solvents of good solvating power, pressurized polymerization can lead to formation of the homogeneous media containing no micropores or small pores having no impact on column

performance. In one embodiment, capillary columns have been prepared using UV-visible light. In another embodiment, microchip columns have been prepared using UV-vis light.

EXAMPLES

5 While many other values of the variables in the following examples can be selected from this description with predictable results, the following non-limiting examples illustrate the inventions:

GENERAL

10 In general, the preparation of each type of media in the following examples include three major steps, which are: (1) preparation of polymer matrix; (2) modification of the polymer matrix to contain desired functional groups; and (3) characterization of the media.

15 Firstly, the preparation major step includes several substeps, which are: (1a) formulation of the polymerization mixture by varying the types and amount of monomers, porogens and initiators; (1b) degassing the polymerization mixture by vacuum and helium purge. (1c) assembly of the empty column with a different diameter and material of tubing as a mold, frequently with one end of the column sealed with a cap or stopper; (1d) filling the column with the polymerization mixture; (1e) sealing the other end of the mold with a cap or a
20 specially designed fitting to add pressure during the polymerization; (1f) preheating the liquid mixture in the mold with one open end if a glass column is used and applying a selected pressure using various pressure sources

including hydraulic pressure, air pressure or mechanic pressure; (1g) placing the mold in a temperature-controlled heating bath or oven at a selected temperature; (1h) polymerizing for various amount of time; (1i) taking the column out of the heating bath after polymerization and replacing the sealing cap or pressurization device with column fittings for pumping the washing liquid through; and (1j) washing the column with organic solvents and/or water.

Secondly, the modification process includes: (2a) formulating the modification reaction mixture with various types and amounts of reactants and catalysts; (2b) pumping more than 5 bed volume modification liquid mixture through the column and sealing it, or pumping more liquid mixture continuously; (2c) carrying out the modification reaction at various temperatures and times in a temperature-controlled heating bath; and (2d) washing the column with organic solvents and water.

The columns are characterized using varieties of methods including liquid chromatography separation, porosimetry, BET surface area measurement, Scanning Electron Microscopy, UV spectroscopy and visual observation. Liquid chromatography characterization includes various modes of separation at different speeds. The commonly used devices, processes and methods are described in the following preceding the specific examples.

DEGASSING OF THE POLYMERIZATION LIQUID MIXTURE

The polymerization mixture is degassed by vacuum generated by water aspirator for 5 minutes using an ultrasonic degasser. It is followed by purging the liquid mixture for a minimum of 20 minutes.

STABILIZING AND CONDITIONING METHODS

The ion exchange columns were subject to a stabilizing and conditioning procedure following the washing step after modification reaction. The stabilizing and conditioning procedure for a glass column (100 x 10 mm I.D.) of strong anion exchanger was as follows: the flow rate of 0.01 mol/l Tris.HCl buffer at pH 7.6 was increased linearly from 0 ml/min to 20 ml/min in 1 minute, and kept for 0.5 minutes. The compression liquid was changed to 1 mol/l NaCl in the same buffer by gradient in 2 minutes, kept for 0.5 minutes. The stabilizing and conditioning procedure for a PEEK-lined stainless steel column is the same as above except the maximum flow rate was 5 ml/min instead of 20 ml/min. The procedures for other ion exchange columns depend on the maximum flow rate allowed.

CHARACTERIZATION PROCEDURES

1. Characterizations with liquid chromatography (LC) separations

1a. LC Characterization Method 1: Liquid chromatography separation of proteins and peptides

Mobile phases:

Mobile phase A (or Buffer A):

Anion Exchange Chromatography: 0.01 M Tris.HCl (pH 7.6)

Cation Exchange Chromatography: 0.01 M sodium phosphate (pH 7.0)

Reversed Phase Chromatography: 0.15% Trifluoroacetic acid (TFA) in water

Mobile phase B (or Buffer B):

Ion Exchange Chromatography: 1 M NaCl in Buffer A

Reversed Phase Chromatography: 0.15% TFA in acetonitrile
(ACN) chromatography

5 Samples:

Anion Exchange Chromatography:

0.6 mg/ml myoglobin, 1 mg/ml conalbumin, 1 mg/ml ovalbumin and
1 mg/ml trypsin inhibitor.

Cation Exchange Chromatography:

10 1 mg/ml conalbumin, 1 mg/ml ovalbumin and 1 mg/ml trypsin
inhibitor.

Reversed Phase Chromatography for proteins:

1.5 mg/ml Ribonuclease A, 0.5 mg/ml Cytochrome C, 1.5 mg/ml
BSA, 0.9 mg/ml Carbonic Anhydrase, 1.5 mg/ml Ovalbumin.

15 Reversed phase chromatography for peptides:

33 g/ml Met-Enkephalin, Let-Enkephalin, Angiotensin II,
Physalaemin, Substance P

Sample preparation:

20 Filled 8 ml of buffer A in a 15 ml graduated plastic sample tube;
Weighed appropriate amount of protein samples and placed them into
this sample tube; Sealed the tube with cap and tumbled the tube gently
until all the proteins dissolved; Added in more buffer liquid mixture until
the 10 ml mark on the sample tube was reached.

A column was characterized by protein separation according to the following

procedure: The column was attached to an Isco 2350 Two Pump System. Pump A contained 0.01 mol/l Tris.HCl buffer (Buffer A) and Pump B contained 1 mol/l NaCl in Buffer A (Buffer B). The mobile phases were degassed with helium purging for more than 20 minutes before use. The UV detector was set at 0.05 sensitivity and 280 nm wavelength for protein separation (214 nm for peptide separation). The volume of the sample injection was 20 micro liters. The column was first cleaned by 20 bed volume of Buffer B and conditioned by 15 bed volume of Buffer A at the 3 ml/min for 4.6 mm I.D. column (10 ml/min for 10 mm I.D. column). The separation was achieved by a gradient from 0 to 50% Buffer B for 20 bed volume at the flow rate of 3 ml/min for 4.6 mm I.D. column and 10 ml/min for 10 mm I.D. column.

1b. LC Characterization Method 2: Binding Capacity Measurement of Ion Exchangers

The binding capacity of an ion exchange column was measured by frontal analysis. The column was cleaned with 20 bed volume of Buffer B and conditioned with 15 bed volume of Buffer A. The columns were saturated with the sample protein by pumping 5 mg/ml BSA or lysozyme liquid mixture (BSA for anion exchanger and reversed phase, and lysozyme for cation exchanger) in Buffer A through the column until there was no further increase of the absorbance of the eluent, followed by

cleaning the non-adsorbed proteins with 100% Buffer A. The protein bound to the columns was eluted by a gradient from 0 to 50% Buffer B for 20 bed volume. The eluted protein was collected in a sample vial and the protein concentration was determined by UV spectrometer at 280 nm. The total binding capacity of the column was calculated by multiplying the concentration of collected protein with the volume of collection.

1c. LC Characterization Method 3: Hydrophobic Interaction Chromatography

This column was characterized for hydrophobic interaction chromatography of proteins. A mixture of proteins containing Ribonuclease, Cytochrome C, Lysozyme, Bovine Serum Albumin and Carbonic Anhydrase (1, 0.3, 0.2, 1 and 0.5 mg/ml in 0.01 M Tris.HCl buffer liquid mixture at pH 7.0.) was separated by a 15 minute gradient of 0.5 mol/l NaCl in 0.01 mol/l Tris.HCl buffer (pH 7.6) to the same buffer at the flow rate of 1 ml/min.

1d. LC Characterization Method 4: Polymer molecular weight determination by precipitation-redissolution chromatography

Characterization method 6 was used for polymer molecular weight determination using Precipitation/Redissolution Chromatography. Seven polymer standards (Mp: 12,900, 20,650, 34,500, 50,400, 96,000, 214,500, 982,000) were separated by a 6 minute gradient from 15% to

80% THF in methanol at the flow rate of 2.6 ml/min. The polymer standards were dissolved in 50% THF in methanol with the total concentration of 56 mg/ml. The injection volume was 20 μ l.

1e. LC separation of nucleotides

5 A sample of Pd(A)₁₂₋₁₈ (2.4 mg/ml in water) was separated by a gradient from 30% to 60% Buffer B in Buffer A (A=20% acetonitrile and 80% 20 mmol/l sodium phosphate; B=1 mol/l NaCl in A) at the flow rate of 1 ml/min.

1f. LC separation of nucleotides with anion exchanger

10 A sample of AMP, ADP and ATP (0.4, 0.8, 0.8 mg/ml in water respectively) was separated in a gradient of 0 to 50% Buffer B in Buffer A as specified in LC Characterization Method 1.

NUMBERED EXAMPLES

Example 1

15 A polymerization liquid mixture was prepared as follows: Weighed 1.2 g of glycidyl methacrylate (GMA), 0.80 g of ethylene dimethacrylate (EDMA) (polymerization mixture 1) and 0.02 g of 2,2'-azobisisobutyronitrile (AIBN) into a 20 ml sample vial and shook the mixture gently until it became a homogeneous liquid mixture; Weighed 2.55 g of cyclohexanol (CHOH) and 0.45
20 g of dodecanol (DODOH) into this liquid mixture and shook it until it is homogeneous. The polymerization mixture was degassed as in the degassing

procedure.

An empty stainless steel column (4.6 mm inner i.d. and 50 mm length), one end of which was sealed by a pressuring device shown in FIG. 4, was filled with this liquid mixture until the column is full. A PEEK-plug contained in the stainless steel screw cap, which was the original cap for the column shown in the same figure, was used to seal the other end of the column. The device of FIG. 3 was connected to a syringe pump. Water was used as the medium to generate the pressure of 120 psi. No air was inside the column. This column was placed into a water bath upright at 60°C and kept for 20 hours. After polymerization, the column was taken out of the water bath and cooled to room temperature.

The device of FIG. 3 was detached from the syringe pump after the pressure was released. The device of FIG. 3 was opened and carefully removed from the column. White polymer extended outside the column. The length of the polymer was found to be about 2mm shorter than the height of the polymerization liquid mixture inside the column and the device of FIG. 3. This extended part of polymer was removed by razor blade. The column was then fitted with the original HPLC column fittings. The column was connected to a HPLC pump and washed with acetonitrile at 0.5 ml/min for 20 minutes at 45°C.

The fittings from one end of the column were detached and the media was pressed out of the column by pumping 10 ml/min acetonitrile into the column through the other end. The wall surface of the polymer media was found to be smooth. The top of the polymer was flat.

Comparative Versions of Example 1

A polymerization liquid mixture was prepared as follows: (1) Weighed 1.2 g of glycidyl methacrylate (GMA), 0.80 g of ethylene dimethacrylate (EDMA) (polymerization mixture 1) and 0.02 g of 2,2'-azobisisobutyronitrile (AIBN) into
5 a 20 ml sample vial and shook the mixture gently until it became a homogeneous liquid mixture; and (2) Weighed 2.55 g of cyclohexanol (CHOH) and 0.45 g of dodecanol (DODOH) into this liquid mixture and shook it until it is homogeneous. The polymerization liquid mixture was degassed with the above Degassing Procedure.

10 An empty stainless steel column (4.6 mm inner i.d. and 50 mm length), one end of which was sealed by a PEEK-plug contained in the stainless steel screw cap which was the original cap for the column. This column was filled with the above liquid mixture until it was full. A PEEK-plug was carefully placed on the top of the column and sealed with another screw cap. No air should be kept
15 inside the column. This column was placed into a water bath upright at 60°C and kept for 20 hours. After polymerization, the column was taken out of the water bath and cooled to room temperature.

The PEEK-plugs were detached and white polymer was observed in the column. The column was then fitted with the original HPLC column fittings. The
20 column was connected to a HPLC pump and washed with tetrahydrofuran (THF) at 0.5 ml/min for 20 minutes.

The fitting from one end of the column was detached and the media was pressed out of the column by pumping 10 ml/min acetonitrile (ACN) into the column through the other end. The wall surface of the media was found to

contain many small irregular dents.

Other columns were prepared using different monomers. Irregular voids were found on the wall surface of the polymer rods. Pictures of two of these rods and one rod made under pressure were taken and shown in the FIG. 7.

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Alternative Versions of Example 1

The procedure of Example 1 was followed except that different polymerization mixtures were used having different proportions and combinations of the functional monomers and crosslinkers. The functional monomers used include glycidyl methacrylate (GMA), 2-hydroethyl methacrylate (HEMA), methyl methacrylate (MMA), 2-(acryloyloxyethyl)trimethylammonium methyl sulfate (ATMS), acrylic acid (AA), 2-Acrylamido-2-methyl-1-propanesulfonic acid (AMPS), stearyl methacrylate (SMA), lauryl methacrylate (LMA), butyl methacrylate (BMA), styrene (ST) and 4-ethylstyrene (EST). The crosslinking monomers (crosslinkers) used include ethyleneglycol dimethacrylate (EDMA), divinyl benzene (DVB). Different proportions of functional monomers, crosslinking monomers and porogens were used. The porogens includes different alcohols such as cyclohexanol, dodecanol, decanol, 1-hexadecanol, butanol, propanol, iso-propanol, ethanol, methanol, 1, 4-butanediol and others such as toluene, N,N-Dimethyl acetamide, acetonitrile, 1,2-dimethoxyethane, 1,2-dichloroethane, dimethyl phthalate, 2,2,4-trimethylpentane, 1,4-dioxane, 2-methoxyethanol, 1,4-butanediol, m-xylene, diisobutyl phthalate, tetra(ethylene glycol) dimethyl ether, tetra(ethylene glycol), poly(propylene glycol) (F.W. 1000), poly(propylene glycol) monobutyl ether

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(F.W. 340, 1000, 2500). The initiators used included 2, 2-prime-azobisobutyronitrile (AIBN) and benzoyl peroxide.

For each of the combinations of monomers and porogens, columns were prepared, examined and characterized.

5 Several columns were made with each polymerization mixture under several pressure conditions. The pressure conditions include: (1) the column opened to the atmosphere during polymerization; (2) the column sealed during polymerization; (3) pressure being applied to the column with gas applied directly to the polymerization mixture using nitrogen as the gas; and (4) each of
10 rubber, plastic and metal pistons being in contact with the polymerization mixture and applying pressure from either a spring, hydraulic pressure, gas pressure or by threading the piston downwardly using the device described above or the modified device when the mechanical force such as a spring was used.

15 The results were: (1) for cases when atmospheric pressure was present there were discontinuities on the surface of a high percentage of columns. Column efficiencies and resolutions were not reproducible; (2) for pressure conditions in which the column was sealed, a higher percentage of columns had discontinuities on the surface, column efficiencies and resolutions were not
20 reproducible; (3) for columns in which gas pressure was applied, the top end surfaces of the columns were soft and irregular, and the wall surfaces were smooth. The separation chromatograms had better reproducibility. The elution peaks are sharper than when pressure was not applied; and (4) reproducibility was very high when pistons were used and the resolution was better than all the

above methods used.

Example 2

A polymerization liquid mixture was prepared as Example 1 with the following polymerization liquid mixture: 2.0g GMA, 2.5g 2-(acryloyloxyethyl)trimethylammonium methyl sulfate (ATMS, 80%), 6.0g EDMA, 7.5g 1,4-butanediol, 6.75g propanol, 0.75g water and 0.1g AIBN.

An empty glass column (10 mm inner i.d. and 100 mm length), one end of which was sealed by a pressuring device shown in FIG. 4, was filled with this liquid mixture until the column is full. A TEFLON-plug contained in the PEEK screw cap shown in the same figure was used to seal the other end of the column. The device of FIG. 4 was connected to a syringe pump. No air was inside the column. This column was placed into a water bath upright at 60°C and kept for 15 minutes. Then the column was pressurized to 120 psi by a syringe pump using water as the medium, and kept for 20 hours. After polymerization, the column was taken out of the water bath and cooled to room temperature.

The device of FIG. 4 was detached from the syringe pump after the pressure was released. The device of FIG. 4 was opened and carefully removed from the column. It was found that the height of the polymer rod was 4mm shorter than the height of the polymerization liquid mixture inside the column. The column was then fitted with the original HPLC column fittings. The column was connected to a HPLC pump and washed with acetonitrile at 2 ml/min for 20 minutes at 45°C.

The fittings from one end of the column were detached and the media was pressed out of the column by pumping 10 ml/min acetonitrile into the column through the other end. The wall surface of the polymer media was found to be smooth. The top of the polymer was flat.

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Alternative Versions of Example 2

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The method of Example 2 was followed with the change of pressures and methods of applying the pressures. Different constant pressures were used during polymerization. The pressures used include 80 psi, 150 psi, 180 psi, 200 psi, 240 psi and 300 psi. The back pressures of these columns are different. The Scanning Electron Microscopy examination of the polymer structure revealed that the particle sizes of these polymers are also different.

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A step gradient of pressure was applied to the polymerization mixture during polymerization. The gradient is as follows: 4 psi/min increase from 10 psi for 5 min, 2 psi/min increase for 10 min, 1 psi/min increase for 20 min, 0.8 psi/min increase for 30 min and then increase the pressure to 180 psi within an hour. The final pressure of 180 psi was kept for 20 hours during polymerization.

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A linear gradient from 15 psi to 180 psi for 2 hours was used to pressurize the reaction at the early stage of polymerization. 180 psi was kept for another 18 hours during the rest of polymerization.

All these columns were modified by pumping in 5 ml liquid mixture of 0.45g/ml trimethylamine hydrochloride in trimethylamine aqueous liquid mixture (50% volume). The columns were sealed and heated in a water bath at 40°C for 3 hours. They were washed with 20 bed volume of water right after

modification. These columns were subjected to Bed Stabilization and Conditioning as described above. They were characterized as above LC Characterization Method for ion exchangers. The backpressures, particle sizes and separation resolutions of these columns all varied with the pressurization methods.

Different polymerization time was also used. A column was prepared as in example 2 except that the polymerization time was 44 hours instead of 20 hours.

Ten columns were prepared in parallel using a ten channel manifold with only one pressure source. The columns prepared have better reproducibility than the individual preparation process.

The polymer morphologies and the internal structures of the particles were examined with Scanning Electron Microscopy (SEM). It was found that the internal structures of these particles are non-porous instead of porous in the other monolithic media known in the art.

Example 3

Two columns were prepared as in Examples 1 and 2 with the following liquid mixture: 17.5g DVB, 19.8g tetra(ethylene glycol), 10.2g tetra(ethylene glycol) dimethyl ether, and 0.18g AIBN. After washing with acetonitrile, the column was further washed with 20 bed volume of water at the flow rate of 16 ml/min. The manually positioned pistons in both ends were compressed into the column. The column was then washed with acetonitrile containing 0.15% trifluoroacetic acid and characterized by LC characterization method 1a and 1b.

The resolutions of these columns for both protein and peptide separation were improved greatly over the columns made in the Comparative Examples. The capacities were more than 5 times higher. The back pressures of these columns were low. High resolutions were achieved with the mobile phase gradient starting from 100% water containing 0.15% TFA. No wall effect was found in these columns. The proteins and peptides pre-eluted out of the column in the columns from the Comparative Examples due to the wall effect in aqueous phase.

Comparative Versions of Example

A polymerization liquid mixture was prepared as Comparative Example of Example 1 with the following reagents: 3ml styrene, 2 ml divinylbenzene, 7.5 ml dodecanol and 0.5 g AIBN. The column was characterized with reversed-phase protein and peptide separation described as LC Characterization 1a and 1b.

Alternative Versions of Example 3

Example 3 was followed with different combinations of porogens, different monomers containing different carbon chain lengths, different amount of total monomer contents, different initiators and different shrinkage solvents.

The porogens used includes: alcohols containing C1 to C12, N,N-Dimethyl acetamide, acetonitrile, 1,2-dimethoxyethane, 1,2-dichloroethane, dimethyl phthalate, 2,2,4-trimethylpentane, 1,4-dioxane, 2-methoxyethanol, 1,4-butanediol, toluene, m-xylene, diisobutyl phthalate, tetra(ethylene glycol)

dimethyl ether, tetra(ethylene glycol), poly(propylene glycol) (F.W. 1000), poly(propylene glycol) monobutyl ether (F.W. 340, 1000, 2500). The combination of some of these solvents led to high resolution columns as well. The alcohols and their combinations can provide large channels for mobile
5 phase to flow through with low back pressure while providing high resolutions. The resolution can be finely tuned with other good solvents as well.

The monomers used include butyl methacrylate and stearyl methacrylate with the above combination of porogens. One column was prepared with the following polymerization liquid mixture: 7g SMA, 10.5g DVB, 19.5g ethanol,
10 13.0g butanol and 0.18g AIBN. Another column was prepared with the following polymerization liquid mixture: 7g lauryl methacrylate (LMA), 1g HEMA, 12g EDMA, 30g dodecanol and 0.2g AIBN. Another column was prepared with the following polymerization liquid mixture: 7g butyl methacrylate (BMA), 1g HEMA, 12g EDMA, 3g water, 16.5g propanol, 10.5g 1,4-butanediol and 0.2g AIBN. The
15 combinations of these monomers containing different carbon chain lengths provide different hydrophobicity and interaction, which offer high resolution and recovery toward samples with different hydrophobicity and characteristics. For example, the butyl methacrylate based media was used for more hydrophobic protein separation and the stearyl methacrylate based media can be used for
20 more hydrophilic protein, peptide or oligonucleotide separations.

Different ratios of monomer to crosslinker were also used to tune the selectivity and resolution. One column was prepared with the following polymerization liquid mixture: 1.05g SMA, 0.7g DVB, 3.25g ethanol and 0.018g AIBN.

A different initiator was also used. A column was prepared using the following polymerization liquid mixture: 10 ml divinylbenzene (80% purity), 30 ml dodecanol, 10 ml styrene and 0.20 g benzoyl peroxide.

A different polymerization time was also used. A column was prepared as in example 3 except that the polymerization time was 44 hours instead of 20 hours.

Different polar solvents were used to shrink the polymer before compression. A column was prepared as Example 3 and washed with 20 bed volume of 1M NaCl after water wash. Manually positioned pistons were compressed into the column after the salt wash. The column showed no wall effect when 0.1 M NaH_2PO_4 (pH 4.0) was used as the starting mobile phase.

These experiments were repeated with different washing liquid mixtures and different catalysts with and without pressure in the presence of an aqueous liquid mixture after the plug was polymerized as well as with different pressures. In each case, when no pressure was applied, there were discontinuities in the outer wall, and upon characterization, there was a lack of repeatability and the peaks of the chromatograms were less pronounced when no pressure was applied after swelling by washing with an aqueous liquid mixture.

Tests have been run at a plurality of pressures both low pressures and high pressures including 60 psi (pounds per square inch) and 120 psi and 600 psi with good results. It is believed that the amount of pressure needed will vary with the diameter of the column and the particular polymerization mixture but satisfactory results can be obtained at a very low pressure in all cases. The upper limit on pressure is the strength of the column walls and fittings.

The amount of pressure also affects the size of separation-effective openings so that the pressure should be selected together with desired separation-effective opening sizes, distribution of the separation-effective sizes and reproducibility of the column.

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Example 4

A column was prepared as Example 2 with the following liquid mixture: 9 g of glycidyl methacrylate, 9 g of ethylene dimethacrylate, 0.18 g, 21.6 g of cyclohexanol and 6.3 g of dodecanol. The length of the polymer was found to be about 7 mm shorter than the height of the polymerization liquid mixture inside the column. The column was then fitted with the original column fittings. The column was connected to a HPLC pump and washed with acetonitrile at 4 ml/min for 20 minutes at 45°C. The column was further modified as follows:

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A liquid mixture containing 570 mg trimethylamine hydrochloride, 24 ml diethylamine and 6 ml water was pumped into these columns at the flow rate of 2 ml/min for 18 minutes. These columns were then placed in a water bath at 30°C for 3 hours. Each column was washed with 100 ml water. The columns were further washed with 0.01 mol/l Tris.HCl buffer at pH 7.6 at 4 ml/min for 30 minutes. The column was stabilized and conditioned by stabilizing and conditioning methods. The pistons from original column fittings were compressed in completely after the wash. The column back pressures were about 360 psi at 10 ml/min in this buffer. The column was characterized as the LC Characterization Method described above.

Example 5

A polymerization liquid mixture was prepared by mixing 1 g styrene, 1 g divinylbenzene (DVB) (80% divinyl benzene and 20% ethylstyrene (EST)), 3 g dodecanol and 0.02 g AIBN.

5 This liquid mixture was degassed by N₂ purging for 20 minutes and filled into a stainless steel column (50 x 4.6 mm i.d.), one end of which was sealed with a PEEK plug inside the screw cap from the column fittings. The other end of the column was sealed with another PEEK plug. It was polymerized at 70 degrees C in a water bath for 24 hours. This column was fitted with the original
10 column fittings and washed with THF at the flow rate of 1ml/min for 10 minutes before it was used for separation of proteins. The back pressure of this column was about 230 psi at the flow rate of 10 ml/min. The compression of the polymer at 10 ml/min of acetonitrile was about 2.9 mm. This column was used for reversed phase protein and peptide separation as LC Characterization
15 Method 1a and 1b.

Alternative Versions of Example 5

Another column was prepared as in example 5 but with higher total monomer contents. The polymerization liquid mixture contained 1.2 g styrene, 1.2 g divinylbenzene, and 2.6 g dodecanol and 0.024g AIBN. The back
20 pressure of the column was 220 psi at 10 ml/min acetonitrile and the compression of the polymer was only 0.9 mm. The higher total monomer content makes the column less compressible.

Columns of different diameters including 22mm, 15mm, 10mm, 8mm,

2.1mm, 1mm, 542 micrometers, and 320 micrometers were prepared as in Example 4. Shorter columns with the size of 10 mm x 2.1 mm i.d. were also prepared. These columns were characterized with reversed phase protein separation by the LC Characterization Method but at the same flow velocity corresponding to the diameters of the columns. The *in situ* polymerization method is applicable in columns with different diameters. It is especially useful for smaller diameter columns or microfluid channels since there is no other packing step involved.

Example 6

Another column was prepared according to Example 5.

This column was fitted with the original column fittings containing a piston and washed with acetonitrile at the flow rate of 1ml/min for 10 minutes. The column was further washed with water for 10 minutes. The pistons in both ends were compressed into the column. This column was characterized by the LC Characterization Method. The compression of the polymer in water by the piston and held by this piston after compression avoid the wall effect resulted from the shrinkage of polymer in water.

Alternative Versions of Example 6

Another column was prepared as Example 5 with the following liquid mixture: 1.8 g divinylbenzene, 0.2 g of styrene, 2.3375 g dodecanol, 0.6625 g toluene, 0.02 g of AIBN and 3.0 g of dodecanol. All the reagents were degassed by vacuum using an aspirator for five minutes, followed by purging

with Helium for 20 minutes, before weighing. The polymerization liquid mixture was filled into a stainless steel column (50 x 4.6 mm i.d.), one end of which was sealed by a PEEK-plug contained in the screw cap. The other end of the column was sealed with another PEEK plug. It was polymerized at 66°C in a water bath for 24 hours. This column was fitted with the original column fittings containing a piston and washed with acetonitrile at the flow rate of 1ml/min for 10 minutes. The column was further washed with water for 10 minutes. The pistons in both ends were compressed into the column. This column was characterized by the LC Characterization Method. The higher content of crosslinker improved the capacity. This version of a column has more than 3 times higher capacity than some other columns prepared in accordance with Example 6.

Another column was prepared with the following polymerization liquid mixture: 10 ml divinylbenzene (80% purity), 10 ml styrene and 0.20 g benzoyl peroxide.

This polymerization liquid mixture was purged by N₂ for 20 minutes. It was filled into a stainless steel column (50 x 4.6 mm i.d.), one end of which was sealed by a PEEK-plug contained in the screw cap. The other end of the column was sealed with another PEEK plug. It was polymerized at 70°C in a water bath for 24 hours. This column was fitted with the original column fittings and washed with tetrahydrofuran at the flow rate of 1ml/min for 10 minutes. It was characterized by reversed phase protein and peptide separation as described in the LC Characterization Method. Different initiators such as benzoyl is also effective in making the monolithic media.

A stainless column of smaller size (50 x 2.1 mm i.d.) and a PEEK column (50 x 4.6 mm i.d.) were prepared and characterized as above example.

Example 7

A column was prepared as in Example 6 with the following liquid mixture:
5 divinybenzene, 0.2 g of hydroxylethylmethacrylate and 0.02 g of AIBN. It was
polymerized at 70°C in a water bath for 24 hours. This column was fitted with
the original column fittings containing pistons. It was washed with acetonitrile
at the flow rate of 1ml/min for 10 minutes, and further washed with water and
0.5 mol/l NaCl in 0.01 mol/l Tris.HCl buffer (pH 7.6). This column was
10 characterized by reversed-phase protein separation as in the LC
Characterization Method.

Alternative Versions of Example 7

A column was prepared and characterized according to the above
procedure except the weight of hydroxylethylmethacrylate and divinybenzene
15 were changed to 0.4 g and 1.6 g.

Another column was prepared and characterized according to the above
procedure except the weight of hydroxylethylmethacrylate and divinybenzene
were changed to 1 g and 1 g.

Another column was prepared as in Example 7 with the following
20 polymerization liquid mixture: -1.8 g divinybenzene, 0.16 g styrene, 0.04 g of
hydroxylethylmethacrylate, and 0.02 g of AIBN.

This column was fitted with the original column fittings containing pistons

after polymerization. It was washed with acetonitrile at the flow rate of 1ml/min for 10 minutes, and further washed with water and 0.5 mol/l NaCl in 0.01 mol/l Tris.HCl buffer (pH 7.6). This column was compressed with pistons and characterized by reversed phase separations of proteins and peptides as in the LC Characterization Method.

Example 8

An empty syringe barrel (70 x 12 mm i.d. Redisep barrel for Combiflash chromatography from Isco, Inc., 4700 Superior Street, Lincoln, NE 68504) was sealed at one end and filled with the following polymerization liquid mixture: 1.6 g hydroxylethyl methacrylate, 6.4 g divinylbenzene, 89 mg AIBN, 12 g dodecanol after degassing with N₂ for 20 minutes. The tip of the barrel was sealed with a blocked needle. This barrel was heated in a water bath at 70°C for 24 hours. It was connected to a HPLC pump and washed with THF at the flow rate of 1 ml/min for 30 minutes. It was then used for both normal phase and reversed phase separation of phenolic compounds.

Example 9

A polymerization liquid mixture was prepared as follows: (1) Weighed 1 g of hydroxylethyl methacrylate, 1 g of ethylene dimethacrylate and 0.02 g of AIBN into a 20 ml sample vial and shook the mixture gently until it became a homogeneous liquid mixture; and (2) Weighed 1 g of cyclohexanol and 2 g of dodecanol into this liquid mixture and shook it until it is homogeneous. All the reagents were degassed by vacuum using aspirator for five minutes, followed

by purging with Helium for 20 minutes, before weighing.

An empty stainless steel column (4.6 mm inner i.d. and 50 mm length), one end of which was sealed by a device of FIG. 4 was filled with this liquid mixture until the column was full. A PEEK-plug contained in the stainless steel screw cap, which was the original cap for the column, was used to seal the other end of the column. The device of FIG. 4 was connected to a syringe pump. Water was used as the medium to generate the pressure of 120 psi. No air should be kept inside the column. This column was placed into a water bath upright at 60°C and kept for 20 hours. After polymerization, the column was taken out of the water bath and cooled to room temperature. The column was connected to a HPLC pump and washed with dry THF (dried by molecular sieve) at 0.5 ml/min for 20 minutes. The column was used for Normal Phase separation of drugs.

Alternative Versions of Example 9

A column was prepared as in Example 9 with the following polymerization liquid mixture: 0.5 g GMA, 0.5g HEMA, 1g EDMA, 1.8g cyclohexanol, 1.2g dodecanol, 0.02 g AIBN.

The columns were washed with water after THF wash at the flow rate of 0.5 ml/min for 20 minutes. 10 ml of 1.0 mol/l sulfuric acid in water was pumped through the columns. The columns were sealed with column plugs and placed into a water bath at 80°C for 3 hours. They were washed with 20 ml water after the modification reaction and further washed with dry THF before characterization with Normal Phase separation.

Another column was prepared with the following polymerization liquid mixture: 1 g glycidyl methacrylate, 1 g ethylene dimethacrylate, 2.4 g cyclohexanol, 0.6 g dodecanol, 0.02 g AIBN.

The columns were washed with water after THF wash at the flow rate of 0.5 ml/min for 20 minutes. 10 ml of 1.0 mol/l sulfuric acid in water was pumped through the columns. The columns were sealed with column plugs and placed into a water bath at 80°C for 3 hours. They were washed with 20 ml water after the modification reaction and further washed with dry THF before characterization with Normal Phase separation.

Example 10

A stainless steel column (50 x 4.6 mm i.d.) was prepared as in Example 3 with the following polymerization liquid mixture contained 0.7g lauryl methacrylate (LMA), 0.1g HEMA, 1.2g EDMA, 3g dodecanol and 0.02g AIBN.

Alternative Versions of Example 10

A column was prepared with the following polymerization liquid mixture containing 0.8g lauryl methacrylate (LMA), 1.2g EDMA, 3g dodecanol and 0.02g AIBN. Another column was prepared with the following polymerization liquid mixture containing 0.175g stearyl methacrylate (SMA), 1.575g DVB (80% pure), 3.25g 1-hexadecanol and 0.018 mg AIBN to form a mixture with a ratio SMA/DVB=10/90. Another column was prepared with the following polymerization liquid mixture containing 0.7g SMA, 1.05g DVB, 3.25g octanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Another column was prepared with the following polymerization liquid mixture containing 1.05g SMA, 0.7g DVB, 3.25g ethanol and 0.018g AIBN to provide a ratio of 60/40 SMA/DVB.

Another column was prepared with the following polymerization liquid mixture containing 0.7 SMA, 1.05g DVB, 1.95g ethanol, 1.30g butanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Other columns were prepared as above using tetradecanol, decanol, octanol, hexanol, butanol, propanol, ethanol and methanol and their combinations as porogenic solvents.

Another column was prepared as above with the following polymerization liquid mixture: 0.7 SMA, 1.05g DVB, 2.925g ethanol, 0.33g methanol, 0.33g isopropanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Another column was prepared as above with the following polymerization liquid mixture: 0.7 SMA, 1.05g DVB, 2.6g ethanol, 0.33g methanol, 0.33g propanol, 0.33g butanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Another column was prepared as above with the following polymerization liquid mixture: 0.7 SMA, 1.05g DVB, 2.762g ethanol, 0.33g methanol, 0.33g propanol, 0.33g butanol, 0.33g hexanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Another column was prepared as above with the following polymerization liquid mixture: 0.7 SMA, 1.05g DVB, 2.435g ethanol, 0.33g methanol, 0.33g propanol, 0.33g butanol, 0.33g hexanol, 0.33g octanol and 0.018g AIBN to provide a ratio of 40/60 SMA/DVB.

Another column was prepared as above with the following polymerization

liquid mixture:-1.05g DVB, 3.08g ethanol, 0.016g ethyl ester and 0.018g AIBN. This column was used for peptide separation as in Example 10, to provide a ratio of 40/60 SMA/DVB.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 3.25g dodecanol and 0.018g AIBN. This column was used for peptide separation as in the first version of Example 10. A series of columns with alcohols containing C1 to C12 were prepared as above and characterized with peptide separation.

A series of columns were prepared as above using the following porogens instead of dodecanol: iso-propanol, N,N-Dimethyl acetamide, acetonitrile, 1,2-dimethoxyethane, 1,2-dichloroethane, dimethyl phthalate, 2,2,4-trimethylpentane, 1,4-dioxane, 2-methoxyethanol, 1,4-butanediol, toluene, m-xylene, diisobutyl phthalate, tetra(ethylene glycol) dimethyl ether, tetra(ethylene glycol), poly(propylene glycol) (F.W. 1000), poly(propylene glycol) monobutyl ether (F.W. 340, 1000, 2500).

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 2.925g isopropanol, 0.325g 1,4-butanediol and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 2.275g isopropanol, 0.975g 2-methoxyethanol and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 2.60g isopropanol, 0.65 dimethyl phthalate and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 2.7g tetraethylene glycol, 0.3g diethylene glycol and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 2.7g tetra(ethylene glycol), 0.3g glycerol and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 1.98g tetra(ethylene glycol), 1.02g tetra(ethylene glycol) dimethyl ether, and 0.018g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1.75g DVB, 1.98g tetra(ethylene glycol), 1.02g tetra(ethylene glycol) dimethyl ether, and 0.018g AIBN.

Example 11

A column (50 x 4.6 mm i.d. stainless steel, which is 50 mm length and 4.6 mm inner i.d.) was prepared as Example 1 with the following polymerization liquid mixture containing 1g methyl methacrylate (MMA), 1g EDMA, 1.8g cyclohexanol, 1.2g dodecanol and 0.02g AIBN-It was connected to a HPLC pump and washed with THF and water at 0.5 ml/min for 20 minutes in sequence.

This column was subjected to a hydrolysis reaction as follows: (1) 2 ml 6 mol/l NaOH was pumped through the column at the flow rate of 0.5 ml/min; and (2) the column was sealed by two column plugs and placed in a water bath at 80°C for 1 hour. It was washed with 20 ml water at the flow rate of 0.5 ml/min

and characterized with protein separation and binding capacity measurement described in the LC Characterization Method.

Alternative Versions of Example 11

5 A column was prepared as Example 11 with the following polymerization liquid mixture: 0.1g acrylic acid (AA), 0.9g methyl methacrylate (MMA), 1g EDMA, 3g dodecanol and 0.02g AIBN. The capacity of the column was measured before and after hydrolysis. The capacity before hydrolysis was about 10 mg lysozyme per ml column volume. It was about 30 mg after
10 hydrolysis.

Another column was prepared as Example 11 with the following polymerization liquid mixture: 0.2g AA, 0.8g MMA, 1g EDMA, 3g dodecanol and 0.02g AIBN. The capacity of the column was measured as in characterization method 11. The capacity before hydrolysis was about 27 mg lysozyme per ml
15 column volume. It was about 50 mg after hydrolysis.

Another column was prepared as Example 11 with the following polymerization liquid mixture: 0.3g AA, 0.7g MMA, 1g EDMA, 3g dodecanol and 0.02g AIBN. The capacity of the column was measured before and after hydrolysis. The capacity before hydrolysis was about 43 mg lysozyme per ml
20 column volume. The capacity was more than 60 mg after hydrolysis.

Another column was prepared as above with the following polymerization liquid mixture: 0.4g AA, 0.6g MMA, 1g EDMA, 3g dodecanol and 0.02g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 0.1g AA, 0.9g tert-butyl acrylate, 1g EDMA, 3g dodecanol and

0.02g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 0.3g AA, 0.3g MMA, 1.4g EDMA, 3g dodecanol and 0.02g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 0.2g AA, 0.7g MMA, 0.1g HEMA, 1g EDMA, 2.85g dodecanol, 0.15g cyclohexanol and 0.02g AIBN. Another column was prepared as above with the following polymerization liquid mixture: 0.4g AA, 1.6g DVB, 3gdodecanol and 0.02g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 1g GMA, 1g EDMA, 2.4g cyclohexanol, 0.6g dodecanol, 0.02g AIBN. This column was subjected to an acid-catalyzed ring opening reaction as in the Alternative versions of Example 9 before base-catalyzed hydrolysis reaction as in Example 11.

Another column was prepared as above with the following polymerization liquid mixture: 0.5 g GMA, 0.5g HEMA, 1g EDMA, 1.8g cyclohexanol, 1.2g dodecanol, 0.02 g AIBN.

Another column was prepared as above with the following polymerization liquid mixture: 0.2g AA, 0.6g MMA, 0.2g GMA, 1g EDMA, 3g dodecanol and 0.02g AIBN. This column was subjected to an acid-catalyzed ring opening reaction before base-catalyzed hydrolysis reaction as above. It was further hydrolyzed with the following liquid mixture: 0.25M Sodium chloroacetate in 5M NaOH at 60°C for 6 hours.

Another column was prepared as above with the following polymerization liquid mixture: 0.2g AA, 0.5g MMA, 0.1g GMA, 1.2g EDMA, 2.55g dodecanol,

0.45g cyclohexanol and 0.02g AIBN. It was hydrolyzed by 0.25M Sodium chloroacetate in 5M NaOH at 60°C for 6 hours.

All these columns were subjected to the Bed Stabilization and Compression Method and characterized with protein separation and binding capacity measurement as in the LC Characterization Method described above.

Example 12

A column (PEEK-lined stainless steel, 50 x 4.6 mm ID) was prepared as Example 1 with the following polymerization liquid mixture: 3 g GMA, 3 g EDMA, 6.9 g cyclohexanol, 2.1 g dodecanol and 0.06 g AIBN.

This column was first modified with a ring-opening reaction under an acidic condition. Five bed volume of the liquid mixture of 0.5 M sulfuric acid in water was pumped through the columns. The column was sealed and heated in a water bath at 50°C for 4 hours. It was washed with 20 bed volume of water after modification.

This column was further modified with an etherification reaction. A five bed volume of a liquid mixture containing 20 g sodium chloroacetate, 20 g NaOH and 64 ml water was pumped through the column. The column was sealed with column plugs and heated in a water bath at 60°C for 2.5 hours. It was washed with water, stabilized and conditioned as in the Stabilization and Conditioning Methods. This column was characterized as in the LC Characterization Method.

Alternative Versions of Example 12

The Example 12 was followed with different modification methods.

A column prepared as in Example 12 was modified by a ring-opening reaction with the following liquid mixture: 6 mol/l glycolic acid and 0.5 M TFI in water for 3 hours.

Another column was modified with the above ring-opening reaction and hydrolysis reaction in 5 M NaOH liquid mixture at 60°C for 2.5 hours.

Another column was first modified by a ring-opening reaction with the following liquid mixture containing 40 g glycolic acid, 60 ml 0.5 M trifluoroacetic acid (TFA) for 2 hours. It was further modified with a liquid mixture containing 20g ClCH₂COONa and 60 ml 5M NaOH for 3 hours.

Example 13

Thirty columns were prepared as Example 2 with the following liquid mixture: 12g AA, 30g MMA, 6g GMA, 72g EDMA, 27g cyclohexanol, 153g dodecanol and 1.2g AIBN. These columns were prepared by parallel synthesis at the same time using three manifolds connected to one syringe pump to obtain 120 psi pressure during polymerization. After polymerization, polymers were pushed out of the columns by a syringe piston (about 9 mm i.d.) for the following uses.

One polymer rod from above was trimmed to be smaller with the diameter about 8mm. It was cut to 1cm thick discs. These discs were used as fillers for a second stage polymerization to prepare another column. 1.8 ml liquid mixture was filled into a glass column (100 x 10 mm i.d.), one end of

which was sealed by the pressurization device shown in FIG. 3. Six polymer discs were filled into the column one by one. All these discs should be covered by the liquid mixture. A Teflon stopper was used to seal the other end of the column. This pressurization device was connected to a syringe pump which was used to add 120 psi pressure to the polymerization liquid mixture at a constant pressure mode. The column was heated in a water bath at 60°C for 20 hours. After polymerization, the column was taken out of the water bath. The pressurization device was detached from the syringe pump after the pressure was released. The pressurization device was opened and slowly removed from the column while the column was still warm. This column was washed with 20 bed volume of acetonitrile and water at the flow rate of 1 ml/min in sequence. It was stabilized and conditioned as in the Stabilization and Conditioning Method. This column was modified with 0.25 mol/l Sodium chloroacetate in 5M NaOH at 60°C for 6 hours. It was characterized as in the LC Characterization method.

Alternative Examples of Example 13

Another column (100 mm x 35 mm ID, glass) was prepared with the two stage polymerization method with the polymer rods as the fillers. This column was sealed with a TEFLON plug in one end. The other end of the column was connected to N₂ tank. The polymerization was under 120 psi for 20 hours at 60°C.

Example 14

Eight short polymer rods (10 mm x 34 mm ID) were prepared with the following liquid mixture: 8 g acrylic acid, 20 g methyl methacrylate, 4 g glycidyl methacrylate, 48 g ethylene glycol dimethacrylate, 102 g dodecanol, 18 g cyclohexanol and 0.8 g AIBN. The polymer rods were prepared under 120 psi N_2 pressure. The rods were used as fillers for the preparation of a large diameter long column using the two stage polymerization method as in Example 12. A glass column (100 mm x 35 mm ID) was filled with the short columns and the same polymerization as above. One end of the column was sealed with a TEFLON plug and the other end was connected with a N_2 tank. The polymerization was carried out under 120 psi pressure at 60°C for 20 hours. The column was washed with 20 bed volume acetonitrile and water. It was subjected to hydrolysis reaction as follows: 0.25M Sodium chloroacetate in 5M NaOH at 60°C for 6 hours. The column was characterized as the LC Characterization Method described above.

Example 15

A column (PEEK-lined stainless steel, 50 mm x 4.6 mm ID) was prepared as in Example 1 with the following liquid mixture: 4 g GMA, 4 g EDMA, 2.8 g dodecanol, 9.2 g cyclohexanol and 0.08 g AIBN.

This column was first hydrolyzed by 1 M H_2SO_4 liquid mixture at 40°C for 3 hours. After hydrolysis, it was activated by pumping a 5 bed volume of 5% sodium t-butoxide liquid mixture in DMSO through the column and heated in a

water bath at 90°C for 1 hour. Then it was modified with the liquid mixture containing 20% of the activation liquid mixture and 80% of butane sultone at 80°C for 20 hours.

Alternative Versions of Example 15

5 A column was prepared as in Example 15 except that propane sultone was used instead of butane sultone.

Another column was prepared as in Example 15 except the modification and activation temperature was 120°C instead of 90°C in an oil bath.

10 Another column was prepared as in Example 15 with the following liquid mixture: 4 g HEMA, 4 g EDMA, 9.4 g dodecanol, 2.6 cyclohexanol and 0.08 g AIBN. It was modified as in Example 15.

Another column was prepared as in Example 1 with the following liquid mixture: 0.55 g GMA, 1.2 g EDMA, 0.25 g 2-Acrylamido-2-methyl-1-propanesulfonic acid (AMPS), 0.48 g NaOH, 0.5 g water, 1.86 g propanol, 0.64
15 g butanediol and 0.02 g AIBN.

Another column was prepared by direct copolymerization of AMPS as above but was further modified with the modification method described in Example 15.

20 All these columns were characterized with the strong cation exchange protein separation and binding capacity measurement described in the LC Characterization Method.

Example 16

A column was prepared as Example 1 with the following polymerization liquid mixture: 45 ml tetramethoxysilane, 100 ml of 0.01 mol/l aqueous acetic acid, 9g urea and 11.5g poly(ethylene oxide) (MW 10000). This liquid mixture
5 was prepared by stirring this mixture in an ice bath for 30 minutes. The polymerization was carried out in the column under 600 psi pressure and at 40°C for 24 hours. The column was then washed with 20 ml water at the flow rate of 0.5 ml/min and pumped in 5 ml of 0.01 mol/l aqueous ammonium hydroxide liquid mixture. The column was sealed and kept at 120°C for 3 hours
10 followed by ethanol wash.

Example 17

The inhibitors such as methyl ether hydroquinone or tert-butylcatecol were removed from monomers by distillation or normal phase chromatography before uses.

15 A polymerization liquid mixture was prepared as Example 1, but with the following polymerization liquid mixture: 240 mg p-terphenyl, 800 mg AIBN, 16 g styrene and 16 g divinylbenzene (80%), 26.4 g mineral oil, and 21.6 g 2-ethylhexanoic acid.

20 An empty glass column (10 mm inner i.d. and 100 mm length), one end of which was sealed by a pressuring device shown in FIG. 4, was filled with this liquid mixture until the column was full. A TEFLON-plug contained in the PEEK screw cap shown in the same figure, was used to seal the other end of the column. The polymerization was allowed to expose to X-ray with a dosage of

600 R/hour for 72 hours at an X-ray tube voltage-of 111 kVp. The obtained column was further heated to 70°C for 2 hours. Then the column was washed with hexane followed by hexane/acetone (50/50), acetone, acetonitrile, respectively with a 20 bed volume of each solvent.

5 The device of FIG. 4 was detached from the syringe pump after the pressure was released. The device of FIG. 4 was opened and carefully removed from the column. It was found that the height of the polymer rod was 4mm shorter than the height of the polymerization liquid mixture inside the column. The column was then fitted with the original HPLC column fittings. The
10 column was connected to a HPLC pump and washed with acetonitrile at 2 ml/min for 20 minutes at 45°C.

The prepared column was further washed with a 20 bed volume of water and compressed with the piston to get rid of the void volume. The column was then characterized using the LC characterization method described in 1a. The
15 chromatogram is shown in FIG. 9.

Alternative Versions of Example 17

Another column was prepared as in example 17 in a glass column (35mm i.d. x 100 mm length) with the following mixture: 30 g styrene, 30 g divinylbenzene, 38.05 g mineral oil and 22.18 g 2-ethylhexanoic acid, 0.518 g
20 p-terphenyl and 1.31 g AIBN. The columns were washed with a 20 bed volume of acetonitrile and water respectively. It is characterized with the LC characterization method 1a. The separation is shown in FIG. 9.

Another column was prepared as in example 17. The fittings from one

end of the column were detached and the media was pressed out of the column by pumping 10 ml/min acetonitrile into the column through the other end. The separation media was submitted for porosimetry studies using SEM and mercury porosimeter after drying in a vacuum at 50°C for 24 hours.

5 Another column was prepared as in example 17 using a larger diameter glass column (35mm i.d. x 100 mm length). The column was sealed with two TEFLON-plugs contained in the TEFLON screw caps instead of the device in FIG. 4. The polymer was pushed out of the column and dried as in the above example. The polymer was submitted for SEM and porosimetry studies.

10 Another column was prepared as in the above example using a large diameter column (35mm x 100 mm) but using the following polymerization liquid mixture: 240 mg p-terphenyl, 800 mg AIBN, 3.2139 g styrene, 28.8088 g divinylbenzene (80% pure), 37.4060 g 1-dodecanol, 13.25 g toluene.

15 Another column was prepared as in the above example using a large diameter column (35mm x 100 mm) but using the following polymerization liquid mixture: 240 mg p-terphenyl and 800 mg AIBN was dissolved in the monomer mixture of 32.0034 g divinylbenzene (80%). Into the monomer mixture, 31.6926 g tetraethylene glycol, 16.3224 g tetraethylene glycol dimethyl ester was added.

20 Another column was prepared as in the above example within a polymeric housing described in FIGS. 12-15. The polymerization liquid mixture contains 73.2 g divinylbenzene, 73.4 g styrene, 85.2 g mineral oil, 60.8 g 2-ethylhexanoic acid, 0.882 g p-terphenyl and 2.94 g AIBN. The temperature of polymerization in the center of the column was about the same as the one on the edge of the column. The conversions of monomers were almost complete

after 4 days of 110 kV X-ray irradiated polymerization. Complete reaction is attained thermally as the further exotherm has no significant bad effect.

Many other columns using different scintillators, photoinitiators, monomers and porogenic solvents have been prepared. The porogenic solvents used include other alkane such as octane, alcohols such as methanol, propanol and cyclohexanol, ethers such as tetrahydrofuran, dioxane, oligomers such tetraethylene glycol, tetraethylene glycol dimethyl ether. Photoinitiators used include 2-chlorothioxanthen-9-one, 4,4'-bis(dimethylamino)benzophenone, 4,4'-bis(diethylamino)benzophenone, phenanthrenequinone, diphenyl(2,4,6-trimethylbenzoyl)phosphine oxide and azo bisisobutyronitrile (AIBN). The scintillators used include 2,5-diphenyloxazole (PPO), 2-phenyl-5-(4-biphenyl) 1,3,4-oxadiazole (PBD), 2-(1-Naphthyl)-5-phenyloxazole (á-NPO) besides p-terphenyl and ZnSe. The monomers used include acrylonitrile, butyl methacrylate besides glycidyl methacrylate, ethylene glycol dimethacrylate, styrene, divinylbenzene, ethyl styrene.

In FIG. 9, there is shown a chromatogram of a separation in two different diameter columns of the mixture of: (1) Met-Enkephalin; (2) Leu-Enkephalin; (3) Angiotensin; (4) Phyusalaemin; and (5) Substances P on Poly (DVB-co-St) monolithic columns prepared by X-ray irradiation initiated polymerization in a column with a diameter of 10 mm and 35 mm and a length of 65 mm; Mobile phase: (A) water with 0.15% (v/v) TFA ; Gradient: 10-40% B in A in 7 bed volume at a flow rate of 5 ml/min I.D. column and 50 ml/min for 35 I.D. column: Detection: UV at 214 nm.

In FIG. 10, there is shown a top view of an ultraviolet or visible light

polymerization apparatus 150 having a stationary top surface 152, a rotating top surface 156, a support member 157 connected to the stationary support surface 152 and pinned to the rotating surface 156 to permit rotation thereof and four fluorescent lamp holders 154A-154D. Visible or ultraviolet fluorescent lamps are inserted in these holders.

In FIG. 11, there is shown a schematic representation of a side sectional view of the polymerization apparatus 150 showing the driven member 156 rotated reciprocally by a motor 159 to rotate the polymerization apparatus 162. Two of the four lamps 166D and 166B are shown mounted to the lamp holders 154D and 154B and corresponding holders at the bottom end of the elongated lamps 166D and 166B. A piston 164 is used to pressurize the polymerization mixture at 162 during polymerization. A fan 158 aids in cooling the polymerization apparatus and reflective coatings on the cover, the sides and the lamps reflect light back into the light conducting walls of the container 162. With this arrangement, the lamps 166A-166D (166B & 166D being shown in FIG. 11) cause light to impinge on the polymerization mixture to initiate and control the polymerization reaction. The polymerization of relatively large diameter columns may be performed while maintaining radial uniformity in the final plug at all locations along the column in the direction of flow of the solvent and analyte. The light may be turned on and off as desired to control the temperature gradients so that the polymerization may take place under a combination of light and temperature in a controlled manner for uniformity.

In FIG. 12, there is shown a simplified elevational view of an apparatus 170 for polymerization using principally X-ray radiation having a radiation proof

cabinet 172, with a door 174, an upper window 176, a holder 178 and a container 180 to contain a reaction mixture at 182. A piston 184 may be utilized in some embodiments to pressurize the reaction mixture 182. In the apparatus 170, X-rays or other suitable radiation such as gamma rays may be used to control the reaction in the polymerization container in a safe convenient manner.

In some embodiments, pressure may be applied through the piston 184 by applying air through a conduit 186 to move the piston 184 inwardly against the reaction mixture 182 in a manner described above in connection with other embodiments. In the preferred embodiment, the apparatus 170 is a small user friendly cabinet X-ray system resembling a microwave in that it has a door and controls mounted on the cabinet. It uses low voltage levels and can be operated by personnel safely from next to the cabinet because it has low penetration which is sufficient however for large columns. It is suitable for the polymerization of this invention because processes described hereinabove use added substances to aid in polymerization such as photoinitiators, fluorescing solvents, or porogens, X-ray sensitizers and/or scintillators. This unit permits X-ray control of the polymerization and other units such as those of FIGS. 10 and 11 permit other radiation control of polymerization, thus permitting for example control of polymerization with the aid of radiation up to a point and finishing the polymerization using heat to decrease the time and yet avoid destructive head build-up.

In FIG. 13, there is shown a top view of the reaction vessel 180 having a reactant entry opening 200, a coolant fluid inlet 203, a coolant outlet 205, a

casing 204 and an overflow outlet 202. The coolant is preferably water. An opening 206 for air to move the plug 182 (FIG. 14) against the polymerization mixture at 212 (FIG. 14) for pressure thereon is provided. A thermocouple can be provided through the opening 200 after the reactant mixture is placed by turning over the vessel 180 and a plug can be inserted there as well. With this arrangement, the reaction mixture may be irradiated under pressure if desired and subjected to X-rays axially for initiation and control of the polymerization. Water flows through it as a coolant so that the combination of radiation and pressure can control thermal gradients and promote uniformity in the final chromatography plug or support.

In FIG. 14, there is shown a sectional view taken through section lines 14-14 of FIG. 13 showing the transparent X-ray radiation window 192, the port 202 for the coolant water, the opening 200 for reactant, a thermocouple 215 and its conductor 218 and a pin in that sequence, the air pressure opening 206 to move the plug 182 to pressurize the reaction mixture in 212, the reactant housing at 212 for receiving reactant mixture, a first distribution plate at 213 to distribute the solvent and analyte during chromatography when the vessel 180 is used as a column and the second distributor plate 215 to receive the solvent and analyte after separation in the column at 212 after polymerization. With this arrangement, radiation passes through the window 192 to control the polymerization of the reactant. This may be done under pressure applied by the plug 182.

In FIG. 15, there is shown a sectional view of the polymerization vessel 180 taken through lines 15-15 of FIG. 13 showing a piston 182, an air space

210 applying pressure to the piston 182 to pressurize the reactant at 212 while it is being irradiated by X-rays and cooled by flowing water in reservoir 190.

As can be understood from the above description, a polymerization mixture which may include a porogen or solvent is polymerized into a porous plug under the control of radiation. For this purpose, there is at least one substance that is caused by the radiation to effect polymerization. Some of the substances may emit radiation that effect other substances which in turn initiate or promote polymerization. For this purpose, the radiation mixture should include at least one monomer, at least a porogen or a solvent and a substance that effects polymerization. X-rays may be used with only a monomer to prepare a support. If a porogen or solvent is included, the support may be porous. The X-rays are a particularly safe type of radiation and may have wide application in forming polymeric supports. The radiation may cause polymerization or irradiate a substance such as a solvent that emits further energy that causes initiation or promotion of polymerization.

Example 18

Homopolymers, polymer resins and porous polymer support have been prepared using 110 kV X-ray irradiation. The polymers were prepared in the glass vials and columns. A polymerization mixture containing 1% AIBN and 0.1% p-terphenyl in styrene was degassed as described in the degassing method and filled into a 1 ml glass vial. The vial was sealed with a screw cap. The vial was exposed in 600 R/hour X-ray using 111 kVp power for two days. A rigid bulk polystyrene polymer was obtained in the shape of the vial after

breaking the glass of the vial.

Alternative Versions of Example 18

A homopolyglycidyl methacrylate was prepared according to the above method.

5 A homopolystyrene was prepared using liquid mixture polymerization according to the above method. 50% of styrene in toluene containing 1% of AIBN and 0.1% of p-terphenyl was polymerized under 600 R/h X-ray for two days. Polystyrene was obtained after polymerization under the same conditions as above as to radiation.

10 A poly(styrene-co-divinylbenzene) resin was prepared according to the above method using the following 1:1 ratio of styrene and divinyl benzene. The polymerization mixture contains 0.9 g styrene, 0.9g divinylbenze, 17 mg AIBN, 5.7mg p-terphenyl. The polymer resin was obtained after polymerization. Gelation happened after 5 hours of polymerization under the same conditions as above as to radiation..

15 A poly(glycidyl-co-ethylene glycol dimethacrylate) resin was prepared according to the above method using the following 1:1 ratio of glycidyl methacrylate (GMA) and ethylene glycol dimethacrylate (EDMA). The polymerization mixture contains 0.9 g GMA, 0.9g EDMA, 17 mg AIBN, 5.7mg p-terphenyl. The polymer resin was obtained after polymerization. Gelation happened after 5 hours of polymerization under the same conditions as above as to radiation..

20 A poly(glycidyl-co-ethylene glycol dimethacrylate) porous support was

prepared according to the above method using the following 1:1 ratio of glycidyl methacrylate (GMA) and ethylene glycol dimethacrylate (EDMA). The polymerization mixture contains 0.45 g GMA, 0.46g EDMA, 0.91 g cyclohexanol, 20 mg AIBN, 1.5 mg p-terphenyl. A porous polymer was obtained after polymerization. Gelation happened after 6 hours of polymerization under the same conditions as above as to radiation..

A poly(styrene-co-divinylbenzene) porous support was prepared according to the above method using the following polymerization mixture containing 0.45 g styrene, 0.45g divinylbenzene (80% pure), 0.91 g cyclohexanol, 20 mg AIBN, 6.5mg p-terphenyl. A porous polymer was obtained after polymerization. Gelation happened after 4.5 hour of polymerization under the same conditions as above as to radiation..

Example 19

Silica capillary with different inner diameters including 75 micrometers, 100 micrometers, 200 micrometers, 250 micrometers, 320 micrometers, 530 micrometers and 700 micrometers were modified with 1 M sodium hydroxide liquid mixture at 90°C for 2 hours in an oven. The capillary was then washed with 60 column volumes of deionized water and acetone. It was dried by nitrogen purging through the column for 20 minutes. The capillary tubing was filled with a silanizing liquid mixture containing 50% (v/v) 3-(trimethoxysilyl)propyl methacrylate and 0.02% (w/v) hydroquinone in N,N-dimethylformamide (DMF). After both ends of the capillary were sealed, it was heated in an oven at 100 °C for about 10 h, and then washed with DMF and

acetone. The capillary was dried with a nitrogen purging after the wash.

Polymerization liquid mixtures were prepared as described in Example 1 with the composition of components listed in Table 1.

Each modified capillary (usually 15~20cm) was filled with the above
5 polymerization liquid mixture. Two ends of the capillary were sealed in two 1.8mL glass vials, respectively, which were also filled with polymerization liquid mixture. Teflon and parafilm were used to double seal the cap of the vial. About 500 microliters empty space was left in each vial and the ends of the capillary located at the half height of the vial. Two to four columns can be prepared by
10 using the same sealing vials. The capillaries were hung vertically in the water bath at certain temperatures listed in Table 1 for 20 hours by clamping the top vial on a stand. After polymerization, the monolithic capillary columns were washed with about 20 column volume organic solvent, usually acetonitrile, sometimes hexane when mineral oil was used as porogen.

15 The columns were characterized with the LC characterization method 1a at the flow rate of 3, 5 and 10 microliters/min. Great resolutions have been achieved.

Table 1. Polymerization liquid mixture composition and polymerization conditions.

	Reactants	I		II		III		IV		V	
		vol%	g	vol%	g	wt%	g	vol%	g	wt%	g
5	Styrene	20	2.1	16	1.6	20	2.0	20	2.1	8	0.8
	Divinylbenzene	20	2.1	24	2.5	20	2.0	20	2.1	32	3.2
	Tetrahydrofuran	7.5	0.8								
	chlorocyclohexane			9.5	1.1						
10	THP							7.0	0.7		
	1-decanol	52.5	5.0	50.5	4.8			53	5.1		
	Toluene									8	0.8
	1-dodecanol									52	5.2
	1-ethylhexanoic acid					27	2.7				
15	Mineral oil					33	3.3				
	AIBN	0.04 g									
	Polymerization	70		70		70		70		80	
	Temp, °C										

Alternative Versions of Example 19

A monolithic capillary column was prepared as in the above example with the following polymerization liquid mixture: .40g BMA, 2.6g EDMA, 3.8g 1-propanol, 1.6g 1, 4-butanediol, 0.6g water and 0.04g AIBN. The polymerization was carried out at 60°C. This column was characterized with the LC characterization method 1a with a microanalytical liquid chromatography system. The flow rate was 5 microliters/min. Excellent separations of proteins were achieved.

Many other poly(acrylate) based capillary monoliths were synthesized with the variation of BMA /EDMA ratios (1/3 to 3/2) and different porogen concentrations (1-propanol with 34 to 39 wt% of the total reaction mixture while 1, 4-butanediol with 20 to 15 wt%).

Another column was prepared as in Example 19 with the following polymerization mixture: 2.2g DVB, 1.3g styrene, 0.9g acrylonitrile, 4.7g mineral

oil, 0.8g toluene and 0.044g AIBN. The polymerization temperature is 75°C. Many other columns of this type were prepared with the variation of acrylonitrile content in the polymer matrix from 0 to 50%. The polymers showed increasing hydrophilicity but different retentativities of proteins. Another column was prepared as in Example 19 with the following polymerization mixture: 0.8 g GMA, 2.4g EDMA, 0.8g ATMS, 3.1g 1-propanol, 2.6g 1, 4-butanediol, 0.3g water and 0.04g AIBN. The polymerization reaction was carried out at 60°C for 20 hours. After polymerization, the porogenic solvents in columns were washed away with acetonitrile. Then they were filled with modification liquid mixture, which is a mixture of TMA and water with volume ratio of 1 to 2 and with 0.45g/mL TMA HCl. The modification was carried out at 40°C for 4 hours.

Example 20

The polymerization liquid mixture is prepared as in Example 1 but with the following mixture: 3.2154g acrylic acid, 8.0026 g methyl methacrylate, 1.6064 g glycidyl methacrylate, 19.2055 g ethylene glycol dimethacrylate, 43.8952 g 1-dodecanol, 9.0017 g cyclohexanol, 320 mg diphenyl (2,4,6 trimethyl(benzole) phosphine oxide. The polymerization mixture was sonicated for 5 minutes and poured into the column, one end of which was sealed by a TEFLON cap, then the column was sealed with another TEFLON cap. The polymerization was exposed to ordinary ceiling light for 7 days. The column was washed with 20 bed volume of acetonitrile followed by a 20 bed volume of water. The column was characterized with chromatography.

Alternative Versions of Example 20

A glass column of size 10 cm x 1 cm ID was prepared as the above example with the following mixture: 2.5074 g glycidyl methacrylate, 2.5003 g ethylene glycol dimethacrylate, 7.5003 g p-xylene, and 58.2 mg diphenyl (2,4,6 trimethyl(benzole) phosphine oxide. The polymerization mixture was exposed to ordinary ceiling light for 24 hours. The same polymerization was carried out in another 2 ml vial for 24 hours. The conversion of monomers was 92%.

A homopolyglycidyl methacrylate was prepared in a vial with the following polymerization mixture: 10 g GMA and 0.1 g diphenyl (2,4,6 trimethyl(benzole) phosphine oxide. The liquid mixture was exposed to ordinary ceiling light for 24 hours. The polymer gelled up after 3 hours. A very clear polymer was obtained.

A homopoly(glycidyl methacrylate) was prepared in a vial with the following polymerization mixture: 10 g GMA, 10 g xylene and 0.1 g diphenyl (2,4,6 trimethyl(benzole) phosphine oxide. The liquid mixture was exposed to ordinary ceiling light for 24 hours. The polymer gelled up after 3 hours. A clear polymer was obtained.

In FIG. 16, there is shown an apparatus 220 for polymerizing chromatographic columns having a temperature readout apparatus 222, a means 224 for controlling heat transfer with the columns and a heat control means 226. The heat transfer apparatus 224 in the preferred embodiment is a water bath in which the columns are immersed but can be any other convenient means for introducing heat into the column such as an oven or radiant heater or electric heater or the like. It is equipped with temperature measuring devices such as thermocouples which are inserted into the

polymerization mixture to continually monitor the temperature cross-section of the columns so as to detect, by a comparison between the readings of the temperature measuring devices within a single column, any temperature gradients or discontinuities in the temperature at different locations in the column. All of the columns may be so monitored for precision but when the polymerization mixtures are the same and the sizes of the columns are the same under some circumstances fewer columns may be monitored, or in the case of very predictable polymerizations, none of the columns may be monitored but past history of the polymerization mixture temperature characteristics may be utilized instead.

In FIG. 16, six columns 228A-228F are shown for illustration purposes only since any convenient number may be utilized. Column 228D is shown as having three conductors 230A-230C extending from it. One end of the conductors is connected to the temperature measuring device and the other end to the temperature readout apparatus 222 to provide a profile of the temperature changes and detect any differences between them. Similarly the other columns have conductors schematically extending from them and intended to represent any number of conductors from any number of thermocouples able to monitor the temperature cross-section. Commonly, two conductors are sufficient with one being in the center of the column and another near the wall of the column.

The heat control device 226 in the preferred embodiment is a heater 232 which may be an electric heater immersed in the water bath although other types of heaters controlled by their corresponding devices can be used. A

heater control 234 which in the preferred embodiment is a source of electric power for controlling the heater and a temperature measuring device 336 which in the preferred embodiment is a thermostatic device immersed in the water bath. A temperature readout and control 240 which may be connected to the heater control 234 in the manner of a thermostat but at least will readout the temperature in the environment of the columns such as the water bath. A water circulation system may also be included with the capability of changing water to cool the water bath in a controlled manner if desired. The temperature readout device 222 includes three readout devices which may be in the form of a strip chart recorder or digital recorder of any kind that will record the temperature at three points. A comparator detector may be included to determine if any of the three points deviates from any other point by a predetermined amount indicating the existence of an exotherm. One such device is shown at 242 and the other is indicated generally at 244. The temperatures from each measuring device may on the other hand be read individually by an operator and any temperature adjustments required made at that time.

In FIG. 17, there is shown a fragmentary, schematic view of a portion of the column 228D having a column wall 346 filled with a polymerization mixture 348 and inserted into it three temperature measuring devices, a wall measuring device 350A, a measuring device in the center of the column 350B, and a measuring device intermediate the center and the wall 350C. The devices may be placed at any suitable location to provide a profile that will detect temperature gradients in radial directions from the column. The thermocouples

are connected to their corresponding conductors 230A, 230B and 230C to indicate the temperature to the temperature measuring device 242.

With this arrangement, the columns in the water bath are raised to a temperature that will provide polymerization with adequate cross-linking but are maintained below a self-sustaining temperature at which the heat given off by polymerization is sufficient to continue the polymerization in a runaway manner generating more and more heat to speed up the reaction and generate still more heat. The heat is introduced at a pace which maintains a constant temperature cross-section to avoid polymerization at different rates in the cross-section of the column.

The polymerization may take place at one temperature as determined either by the past history of that type of column or from the temperature readings in the temperature measuring devices within the column. On the other hand, as the polymerization progresses, different amounts of temperature can be tolerated without moving into the temperature runaway zone and a higher temperature may be safely utilized so as to provide the desirable characteristics for the column. In this mode, the temperature of the water bath may be maintained at one temperature for a period of time and then increased to another temperature. A series of such steps may be utilized.

Example 21

In a 75 mm long x 35 mm ID column, a weak cation exchange column for protein separation was prepared having the following mixture: 36.01 g EDMA, 3.01 g GMA, 15.01 g MMA, 6.09 g acrylic acid, 0.94 g AIBN, 85.67 g 1-

dodecanol and 10.57 g cyclohexanol. The polymerization took place in a water bath at 40°C for 72 hours followed by polymerization at 60°C for 24 hours. The column was washed with a 10 bed volume of acetonitrile at 45° C and at a constant pressure of 300 psi. The column was characterized by liquid chromatography and provided good protein separation.

Example 22

A weak cation exchange column with a 75 mm length x 35 mm inner diameter was prepared with the following mixture: 36.02 g EDMA, 3.03 g GMA, 15.03 g MMA, 6.08 g acrylic acid, 0.93 g AIBN, 85.64 g 1-dodecanol and 10.53 g cyclohexanol.

The column was polymerized at 40°C for 72 hours followed by 60°C for 24 hours. A porogen wash of a 10 bed volume of acetonitrile at 45°C at a constant pressure of 300 psi was used. Good protein separation was obtained.

Example 23

A 35 mm ID, 100 mm long weak cation column was prepared with the following mixture: 12.81 g acrylic acid, 32.01 g MMA, 6.40 g GMA, 76.83 g EDMA, 176.04 g 1-dodecanol, 16.00 g cyclohexanol and 1.96 g AIBN.

Polymerization was performed in a water bath at temperatures of between 40° to 60°C for 12 hours and then at 60°C for 24 hours. The temperature was linearly increased from 40° to 60°C during the first 12 hours. The column was washed with a 10 bed volume of acetonitrile at 45°C at a constant pressure of 300 psi.

Example 24

A weak cationic exchange column was prepared with a 35 mm inner diameter and a 300 mm long column housing having the following mixture: 12.81 g acrylic acid, 32.01 g MMA, 6.40 g GMA, 76.83 g EDMA, 176.04 g 1-dodecanol, 16.00 g cyclohexanol and 1.96 g AIBN.

The polymerization took place with a linear increase in temperature from 40° to 60°C for 12 hours and then at 60°C for 24 hours. The column was washed as in the above example. Good protein separation was provided.

Example 25

A weak cation exchange column was prepared in a 35 mm ID, 300 mm long column housing with the following mixture: 18.05 g acrylic acid, 45.06 g MMA, 9.21 g GMA, 108.13 g EDMA, 238.52 g 1-dodecanol, 31.56 g cyclohexanol and 3.1 g AIBN.

The mixture was polymerized at 40°C for 72 hours and then at 60°C for 24 hours. The column was washed as indicated above and provided a good protein separation.

Example 26

A strong anion exchange column with dimensions of 75 mm long x 35 mm ID was prepared with the following mixture: 8.11 g GMA, 24.09 g EDMA, 8.07 g ATMS, 28.06 g 1-propanol, 29.14 g 1,4-butanediol, 3.05 g water and 0.48 g AIBN.

The mixture was polymerized at 40°C for 72 hours followed by

polymerization at 60°C for 24 hours. The column was characterized by liquid chromatography and provided good protein separation.

Example 27

A strong anion exchange column with dimensions of 35 mm ID and 75 mm long was prepared with the following mixture: 8.0317 g GMA, 24.0089 g EDMA, 8.0295 g ATMS, 27.0134 g 1-propanol, 30.0176 g 1,4-butanediol, 3.0344 g water and 0.6177 g AIBN. It was polymerized at 40°C for 72 hours followed by 60°C for 12 hours. The column was characterized by liquid chromatography and provided good protein separation.

Example 28

A strong anion exchange column with dimensions of 35 mm ID and 300 mm long was polymerized to provide a strong anion exchange column using the following mixture: 25.66 g GMA, 76.81 g EDMA, 25.64 g ATMS, 96.04 g 1-propanol, 86.49 g 1,4-butanediol, 9.62 g water and 1.99 g AIBN.

The mixture was polymerized with a linear progression of between 40°C to 60°C for 24 hours and then it was kept at 60°C for 12 hours. It was subjected to compression from between 10 to 150 psi gradually increasing for 12 hours. The column was characterized by liquid chromatography and provided good protein separation.

Example 29

A column was prepared for separation of peptides having dimensions

of 35 mm ID and 100 mm long with the following mixture: 100.06 g DVB, 108.77 g TEG, 41.26 g TEG-DME and 1.27 g AIBN.

The mixture was polymerized at between 40° to 60°C for 12 hours and then 60°C for 24 hours with compression between 10 and 150 psi increasing linearly for 4 hours. The column was characterized by liquid chromatography and provided good peptide separation.

Example 30

A porous monolithic polymer was prepared in a column with 34 mm ID and 25 cm length was prepared as in Example 2 with the following polymerization mixture: 12.81 g AA, 32.01 g MMA, 6.40 g GMA, 76.83 g EDMA, 176.04 g 1-dodecanol, 16.00 g cyclohexanol, 1.96 g AIBN. The columns was polymerized under 150 psi pressure at 25°C for 48 hours, then at 60°C for 24 hours.

It was connected to a HPLC pump and washed with a 20 bed volume of THF and waters respectively.

This column was subjected to a hydrolysis reaction with 6 mol/l NaOH at 80°C for 1 hour. It was washed with a 20 bed volume of water and characterized with protein separation and binding capacity measurement described in the LC Characterization Method.

Alternative Versions of Example 30a

A column was prepared as in Example 30 except with programmed linear gradient of polymerization temperature of 40°C to 60°C in 24 hours. It was then

cured at 60°C for another 12 hours.

A column with a diameter of 4.6 mm and 5 cm length was prepared as in the above example with the same temperature gradient.

A column with a diameter of 10 mm and 10 cm length was prepared as
5 in the above example with the same temperature gradient.

Example 31

A column with a 34 mm diameter and a 25 cm length was prepared as in Example 21 with the following polymerization liquid mixture: 78.80 g EDMA, 38.46 g GMA, 11.91 g AMPS, 11.72 g 4.9 M NaOH aqueous liquid mixture,
10 12.44 g water, 162.23 g 1-propanol, 38.79 g 1,4-butanediol and 1.97 g AIBN. The column was washed with a 20 bed volume of acetonitrile and water. This polymer was further hydrolyzed in 0.5 M H₂SO₄ at 60°C for 3 hours, and then washed with a 10 bed volume of deionized water. This hydrolyzed polymer was further modified with the following procedure: The column was pre-washed with
15 a 5 bed volume of dried acetonitrile to remove the water in the column. A 5 bed volume of the modification agent was pumped through the column at a constant pressure of 250 psi. The modification reaction was carried out at 60°C for 3 hours. After reaction, the modification agent was washed off from the column with a 5 bed volume of 0.5 M H₂SO₄ followed by another 10 bed volume of
20 nanopure water. The modification agent was prepared as the following procedure: The acetonitrile containing 10% pyridine was cooled down to lower than 10°C in ice batch, then equivalent chlorosulfonic acid was added gradually into the cooled liquid mixture. The temperature of the liquid mixture was

controlled to be lower than room temperature during the whole process of preparation.

Alternative Versions of Example 31a

A column was prepared as in Example 31 except with a programmed
5 linear gradient of polymerization temperature of 40°C to 60°C in 24 hours. It was then cured at 60°C for another 12 hours.

A column with a diameter of 4.6 mm and 5 cm length was prepared as in the above example with the same temperature gradient.

A column with a diameter of 10 mm and 10 cm length was prepared as
10 in the above example with the same temperature gradient.

A column was prepared as in Example 31 except using the following polymerization mixture: 78.80 g. EDMA, 38.46 g GMA , 11.91 g. AMPS, 13.89 g. 4.9 M NaOH aqueous liquid mixture, 6.22 g. water, 140.85 g. 1-propanol, 32.02 g. 1,4-butanediol and 1.97 g AIBN.

15 From the above description it can be understood that the novel monolithic solid support of this invention has several advantages, such as for example: (1) it provides chromatograms in a manner superior to the prior art; (2) it can be made simply and inexpensively; (3) it provides higher flow rates for some separations than the prior art separations, thus reducing the time of some
20 separations; (4) it provides high resolution separations for some separation processes at lower pressures than some prior art processes; (5) it provides high resolution with disposable columns by reducing the cost of the columns; (6) it permits columns of many different shapes to be easily prepared, such as for

example annular columns for annular chromatography and prepared in any dimensions especially small dimensions such as for microchips and capillaries and for mass spectroscopy injectors using monolithic permeable polymeric tips; (7) it separates both small and large molecules rapidly; (8) it can provide a superior separating medium for many processes including among others extraction, chromatography, electrophoresis, supercritical fluid chromatography and solid support for catalysis, TLC and integrated CEC separations or chemical reaction; (9) it can provide better characteristics to certain known permeable monolithic separating media; (10) it provides a novel approach for the preparation of large diameter columns with homogeneous separation-effective opening size distribution; (11) it provides a separation media with no wall effect in a highly aqueous mobile phase and with improved column efficiency; (12) it improves separation effective factors; and (13) it reduces the problems of swelling and shrinking in reverse phase columns.

Although preferred embodiments of the inventions have been described with some particularity, many variations in the invention are possible within the light of the above teachings. Therefore, it is to be understood that, within the scope of the appended claims, the invention may be practiced other than as specifically described.

CLAIMS

1. A chromatographic system comprising: a sample injector; at least one chromatographic column having a column casing and at least one permeable monolithic polymeric plug inside the column casing positioned to receive a sample from the sample injector; a solvent system in communication with the chromatographic column for supplying a solvent to the at least one chromatographic column, whereby the sample is separated into its components within the at least one chromatographic column; said at least one column casing including a column casing wall with an internal column wall surface; and a utility device for receiving fluid from said chromatographic column characterized by at least one permeable monolithic polymeric, temperature-time moderated plug with smooth walls without discontinuities in contact with an internal surface of the column wall.

2. A chromatographic system according to claim 1 characterized in that the at least one chromatographic column includes a corresponding temperature measuring device within a corresponding one of the at least one permeable monolithic polymeric, temperature-time moderated plug.

3. A chromatographic system in accordance with either claim 1 or claim 2 characterized in that the at least one permeable monolithic polymeric temperature-time moderated plug includes divinylbenzene.

4. A chromatographic system in accordance with either claim 1 or claim 2 characterized in that the at least one permeable monolithic polymeric, temperature-time moderated plug includes glycidyl methacrylate with hydrophobic surface groups.

5. A chromatographic system in accordance with either claim 1 or claim 2 characterized in that the at least one permeable monolithic polymeric, temperature-time moderated plug includes urea formaldehyde.

6. A chromatographic system in accordance with either claim 1 or claim 2 in which the at least one permeable monolithic polymeric, temperature-time moderated plug includes silica.

7. A chromatographic system in accordance with any of claims 1-6 characterized in that the column casing is glass.

8. A chromatographic system according to any of claims 1-7 characterized in that the at least one permeable monolithic polymeric, temperature-time moderated plug is size compensated.

9. A method of performing chromatography comprising the steps of: applying a sample to a chromatographic column having a column casing and a polymeric monolithic packing without substantially inhomogeneous pore sizes caused by exotherms; and supplying a solvent to the chromatographic column,

whereby the sample is separated into its components within the chromatographic column characterized in that the polymeric monolithic packing is temperature-time moderated.

10. A method of performing chromatography in accordance with claim 9 characterized in that the step of applying a sample to a chromatographic column having a column casing and a polymeric monolithic packing comprises the step of applying the sample to a chromatographic column that is size compensated.

11. A method in accordance with either claim 9 or 10 characterized in that the step of applying a sample to a chromatographic column having a column casing and a polymer monolithic packing includes the step of applying the sample to a permeable monolithic polymeric plug that includes a vinyl group.

12. A method in accordance with either claim 9 or 10 characterized in that the step of applying a sample to a chromatographic column having a column casing and a polymeric monolithic packing includes the step of applying the sample to a permeable monolithic polymeric plug that includes urea formaldehyde.

13. A method in accordance with any of claims 9-12 in which the step of applying a sample to a chromatographic column having a column casing and

a polymeric monolithic packing includes the step of applying the sample to a permeable monolithic polymeric plug that includes a silica polymer.

14. A chromatographic column comprising: a chromatographic column support having internal column walls and a permeable monolithic polymeric plug with separation-effective openings within said column walls characterized in that the permeable monolithic polymeric plug is a polymer with cross sectional uniformity formed by polymerization with temperature-time moderation.

15. A chromatographic column according to claim 14 characterized in that sizes of the separation-effective openings are controlled at least partly by pressure during polymerizations.

16. A chromatographic column in accordance with either claim 14 or 15 characterized in that the permeable monolithic polymeric plug has smooth walls and is size compensated by pressure.

17. A chromatographic column in accordance with any of claims 14-16 characterized in that there are substantially no pores within the permeable monolithic polymeric plug and the permeable monolithic polymeric plug has smooth walls.

18. A chromatographic column in accordance with any of claims 14-

17characterized in that the permeable monolithic polymeric plug is free of channeling openings in the walls of the plug.

19. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is formed principally of methacrylate.

20. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is formed principally of methacrylate with hydrophobic surface groups.

21. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is formed principally of urea formaldehyde.

22. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is formed principally of silica.

23. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is principally formed of polymers of glycidyl methacrylate and of ethylene dimethacrylate in a ratio by weight in the range of from 1 to 1 and 2 to 1.

24. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug is principally formed of polymers of glycidyl methacrylate and of ethylene dimethacrylate in a ratio by weight of 3 to 2.

25. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug includes as its principal component a mixture of divinylbenzene and styrene in a ratio in the range of 3 to 1 and 9 to 1.

26. A chromatographic column in accordance with any of claims 14-18 characterized in that the permeable monolithic polymeric plug includes as its principal component a mixture of divinylbenzene and styrene in a ratio in the range of 4 to 1.

27. A chromatographic column in accordance with any of claims 14-18 characterized in that the column is in the range of 35 percent and 80 percent by weight divinylbenzene.

28. A chromatographic column in accordance with claim any of claims 14-18 characterized in that the column is 64 percent by weight divinylbenzene.

29. A chromatographic column in accordance with any of claims 14-18 characterized in that the column includes a polymeric plug with a temperature

measuring device within it.

30. A chromatographic column in accordance with any of claims 14-29 characterized by having a diameter of over 10 mm.

31. A chromatographic column in accordance with any of claims 14-30 characterized in that the volume of pores per square millimeter and mean size of pore openings in the direction of a longitudinal axis of the column per square millimeter does not vary from location to location and does not vary by more than 5 percent.

32. Apparatus for making a chromatographic column comprising a temperature controlled reaction chamber adapted to contain a polymerization mixture during polymerization characterized by means for varying the temperature during polymerization, whereby the polymerization mixture is temperature-time moderated.

33. Apparatus for making a chromatographic column in accordance with claim 32 characterized by means for applying pressure to said polymerization mixture in said temperature controlled reaction chamber.

34. Apparatus according to claim 33 characterized in that the means for applying pressure is a means for applying pressure with a movable member.

35. Apparatus according to claim 34 characterized in that the movable member has a smooth surface positioned to contact said polymerization mixture as pressure is applied during polymerization.

36. Apparatus for making a chromatographic column comprising: a temperature controlled reaction chamber adapted to contain a polymerization mixture during polymerization to form a plug; aqueous processing means for applying an aqueous solution to the plug; and means for applying pressure to said plug to reduce voids in the plug characterized in that the temperature controlled reaction chamber includes means for temperature-time moderation.

37. An apparatus in accordance with claim 36 characterized by radiation means for applying radiation to the plug; and control means for controlling the radiation.

38. A method comprising the steps of: putting a polymerization mixture in a column casing characterized by the step of polymerizing the polymerization mixture in the column casing using a combination of low and high temperature polymerization.

39. A method in accordance with claim 38 in which the step of putting a polymerization mixture in a column casing comprises the step of putting a polymerization mixture in a column casing having a diameter of at least 10 mm.

40. A method comprising the steps of: putting a polymerization mixture in a column casing characterized in that the polymerization mixture comprises a functional monomer containing a sulfonic group; and directly polymerizing the mixture to provide a strong cation exchanger.

41. A method in accordance with claim 40 characterized in that the step of putting a polymerization mixture in a column casing comprises the steps of hydrolyzing a polymer in the polymerization mixture and modifying a hydroxyl formed in the step of hydrolyzing the polymer with chlorosulfonic acid.

42. A method in accordance with either claim 40 or 41 characterized in that the step of putting a polymerization mixture in the column casing comprises the steps of hydrolyzing a polymer in the polymerization mixture and modifying the hydroxyl formed in the step of hydrolyzing the polymer with a pyridine salt solution of chlorosulfonic acid.

43. A method of making a monolithic chromatographic column comprising the step of preparing a polymerization mixture characterized by performing polymerization under temperature-time moderating conditions, whereby temperature gradients are controlled to prevent spacial cross sectional variations in the monolithic chromatographic column.

44. A method in accordance with claim 43 characterized in that the polymerization is performed under pressure, whereby sufficient pressure is

applied to prevent voids from being formed caused by vacuum due to shrinkage during polymerization.

45. A method of making a monolithic chromatographic column comprising the steps of: preparing a polymerization mixture including a porogen characterized by performing polymerization with temperature-time moderation to form a polymer plug; washing the polymer plug to remove the porogen, wherein the plug tends to swell; and applying pressure to prevent swelling of the polymer plug and eliminate voids.

46. A method of making a strong anion column, comprising steps of: mixing GMA, ATMS, EDMA, an initiator and a porogen to form a polymerization mixture; and polymerizing the mixture in the column characterized in that the mixture is polymerized under temperature-time moderation conditions to form a plug.

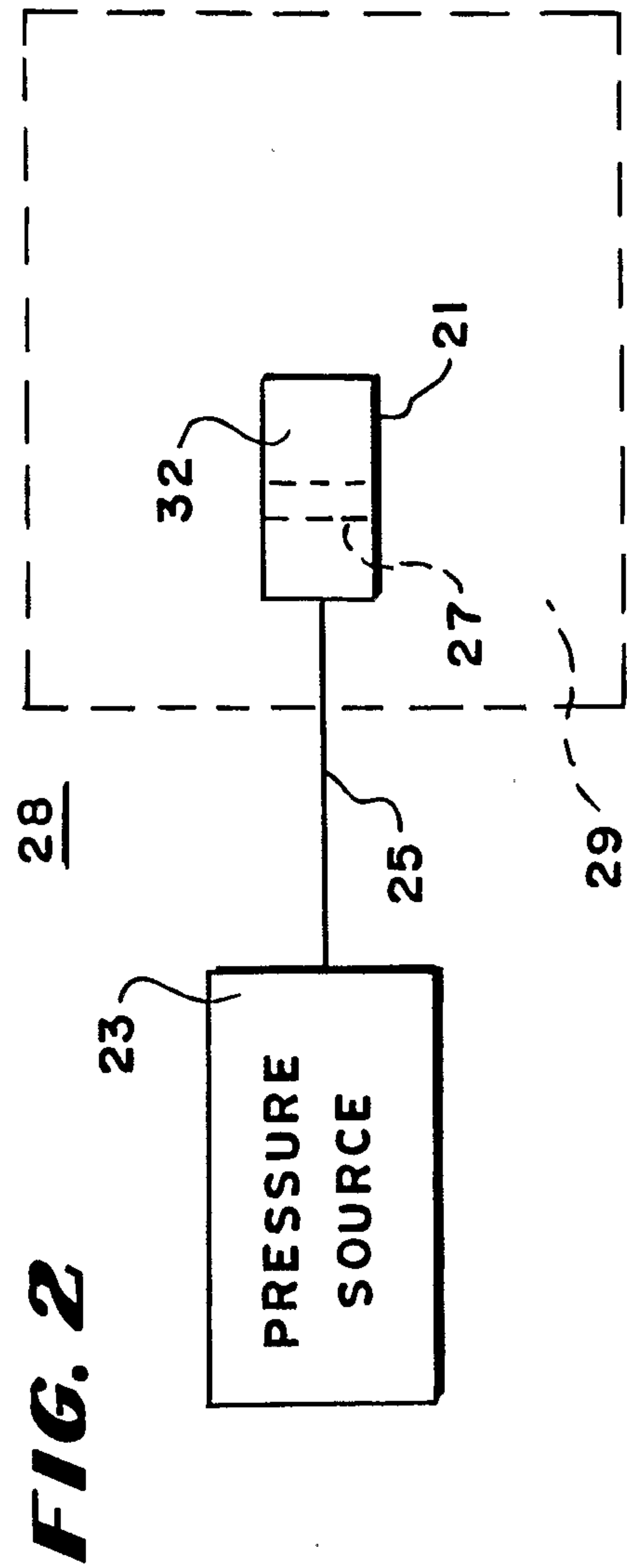
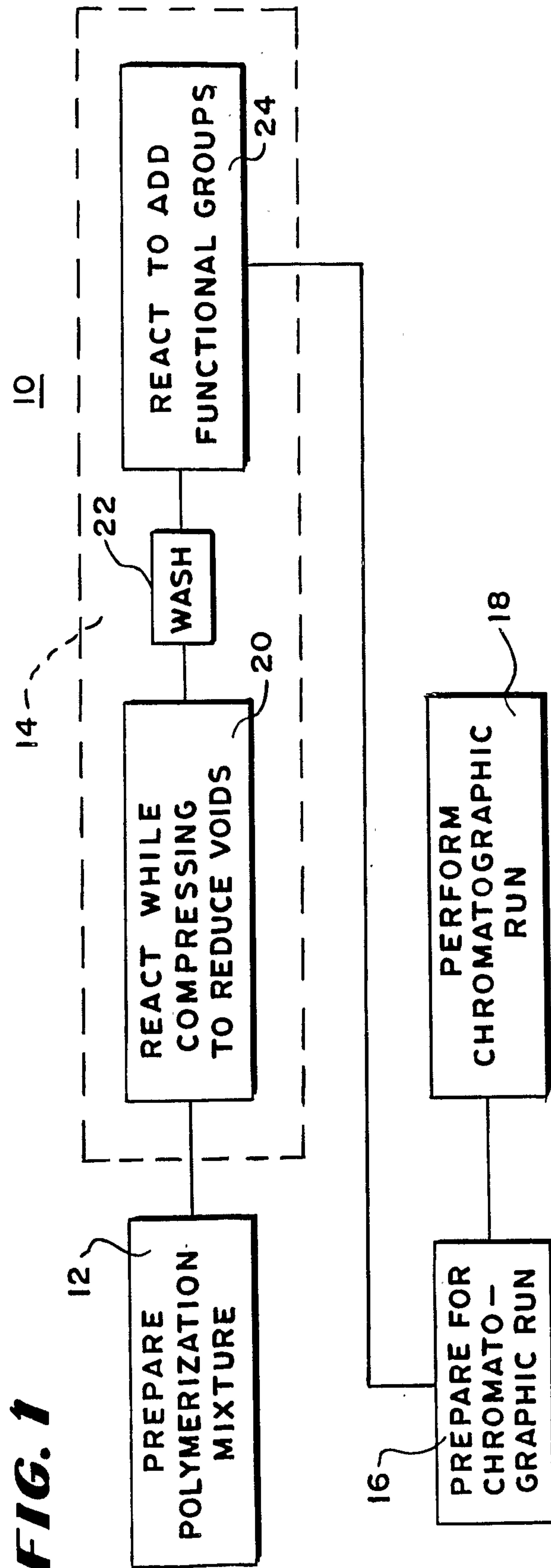
47. A method in accordance with claim 46 characterized in that the step of polymerizing the mixture includes the step of polymerizing at a gradient temperature starting at a control initiation point at a low temperature and gradually increasing the temperature to a safe point and curing at a higher temperature wherein temperature run-away is avoided and adequate polymerization and cross linking is obtained.

48. A method in accordance with claim either claim 46 or claim 47

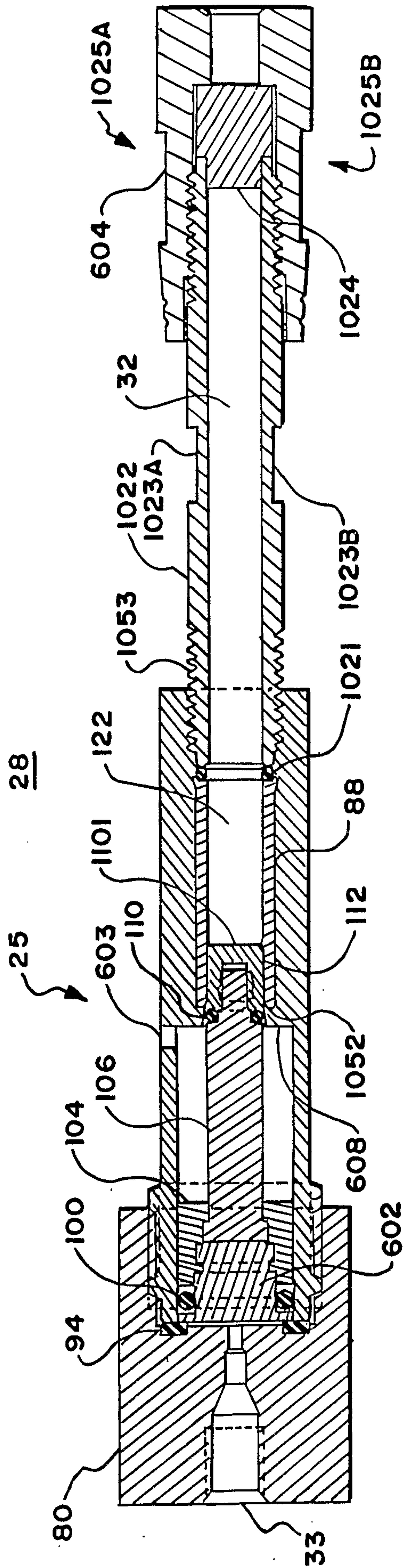
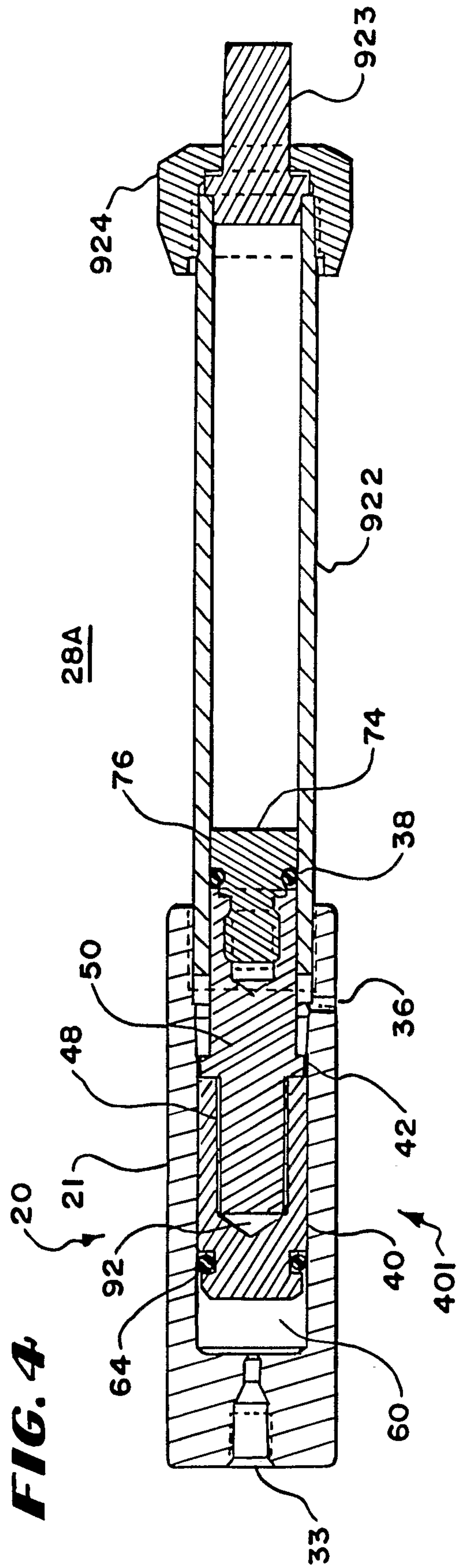
characterized in that the step of polymerizing the mixture includes the step of polymerizing at a gradient temperature starting at the control initiation point at a value between 35 and 45°C and gradually increasing the temperature to a safe point and curing at a higher temperature.

49. A method in accordance with any of claims 46-48 characterized in that the step of polymerizing the mixture includes the step of polymerizing at a gradient temperature starting at the control initiation point and gradually increased to a safe point and curing at a higher temperature.

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FIG. 3**FIG. 4**

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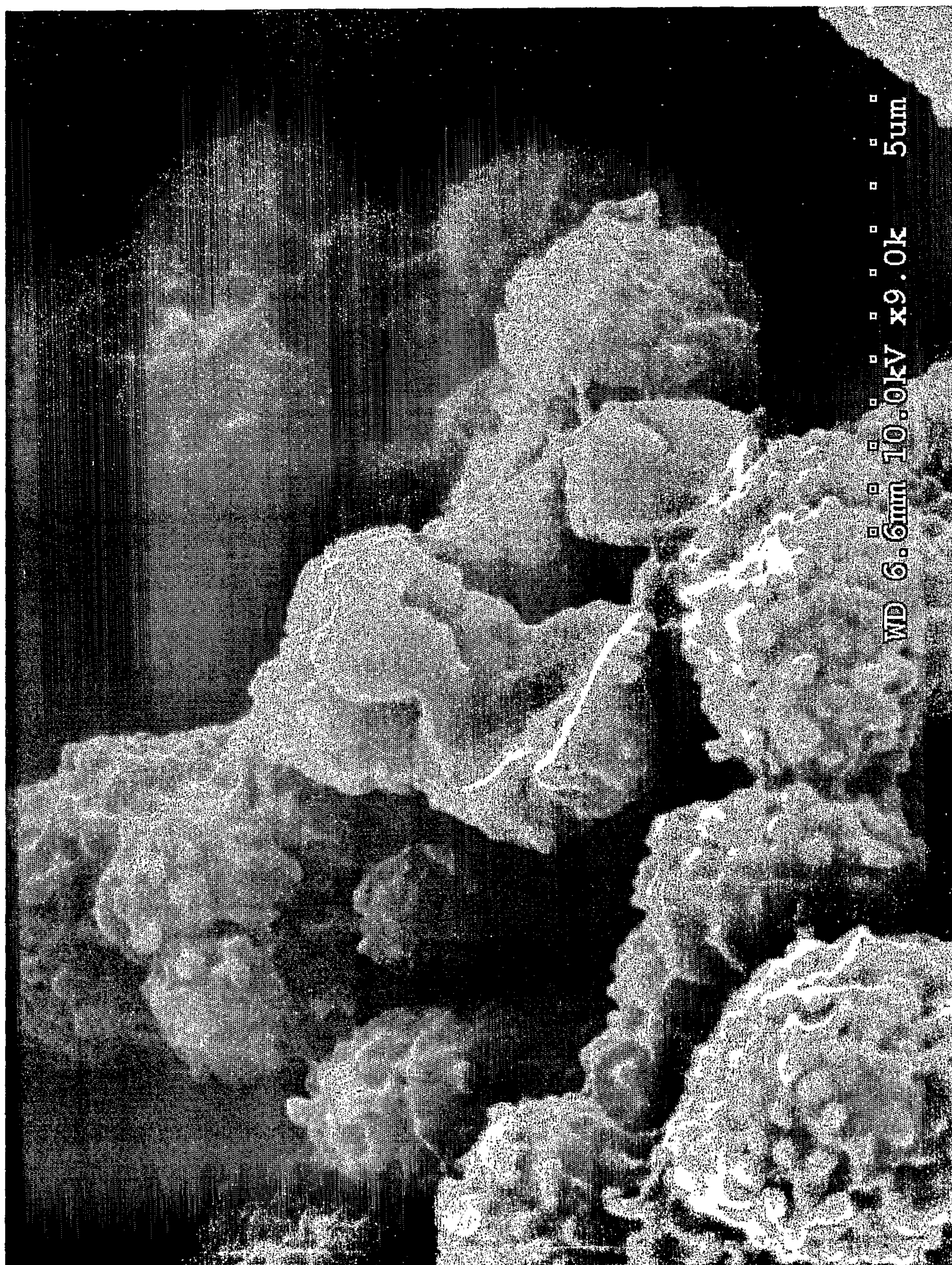
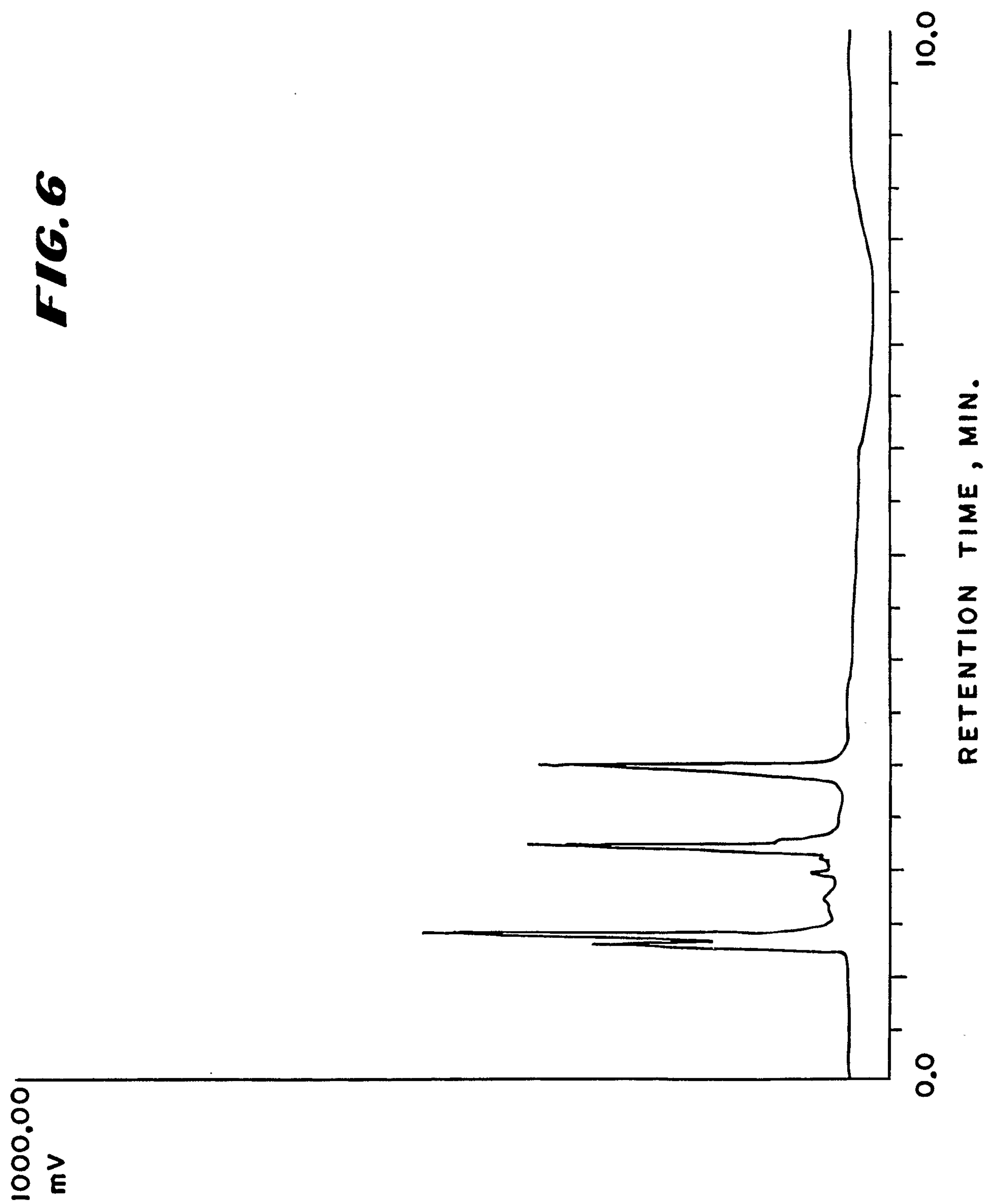


FIG. 5

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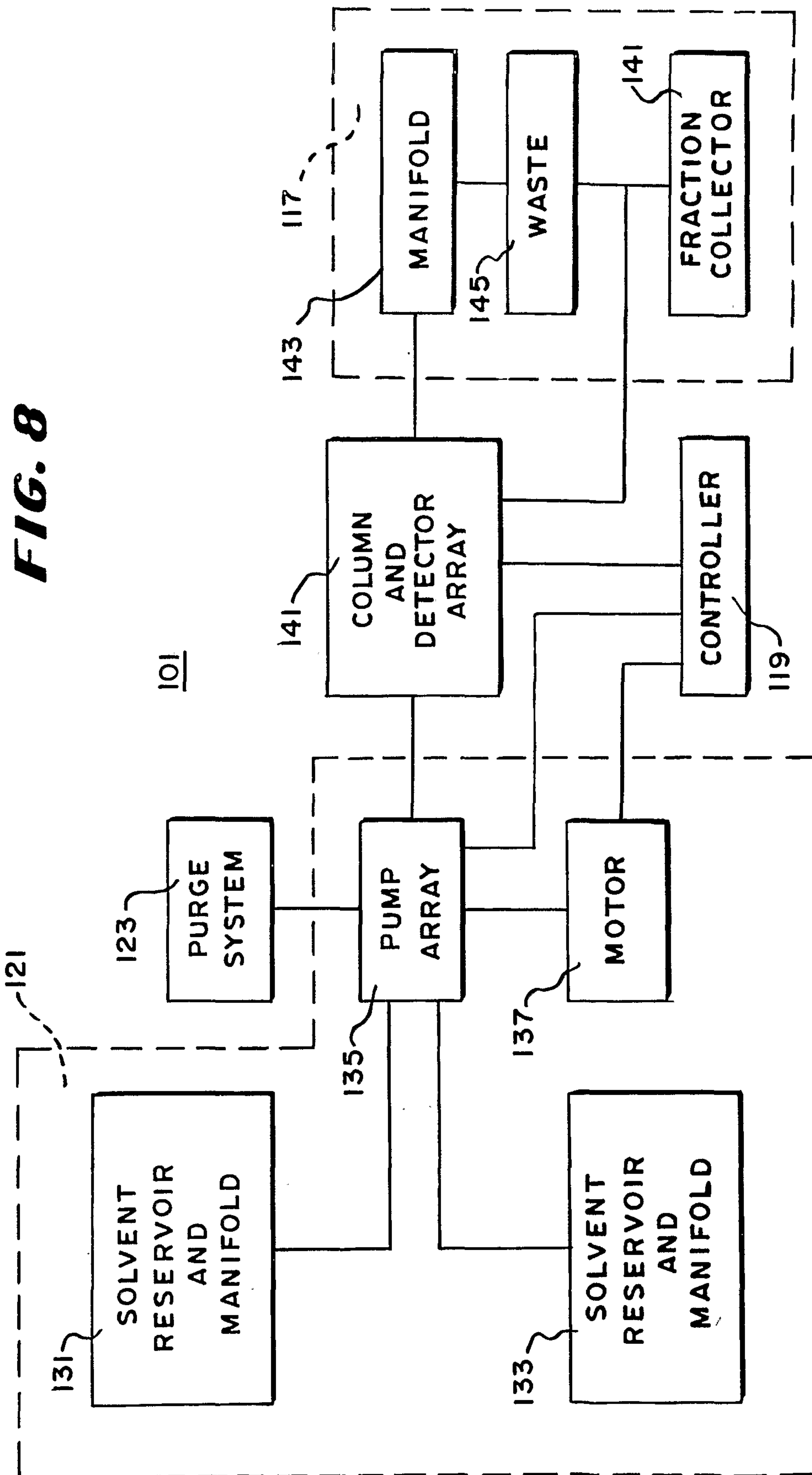


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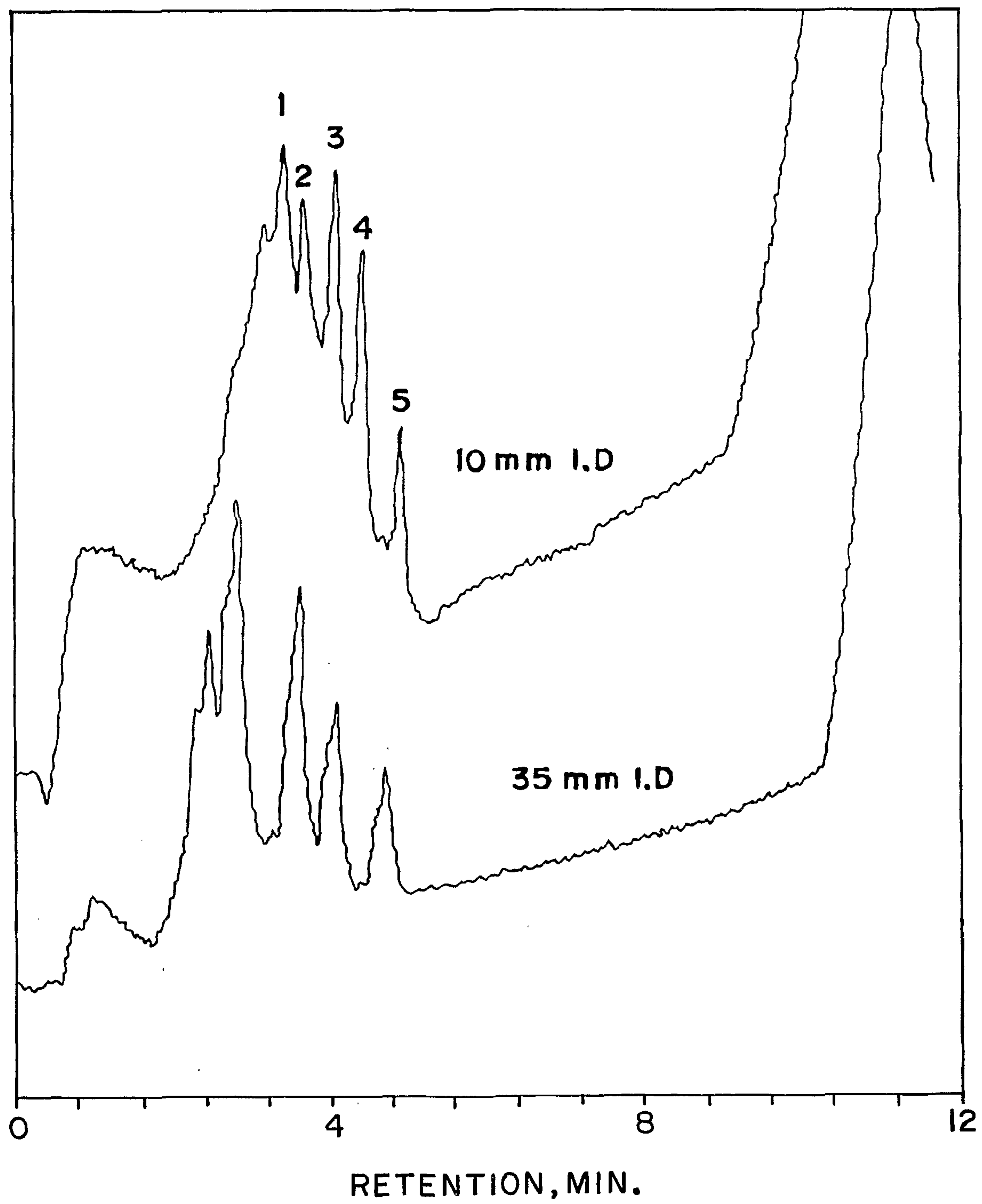


FIG. 7

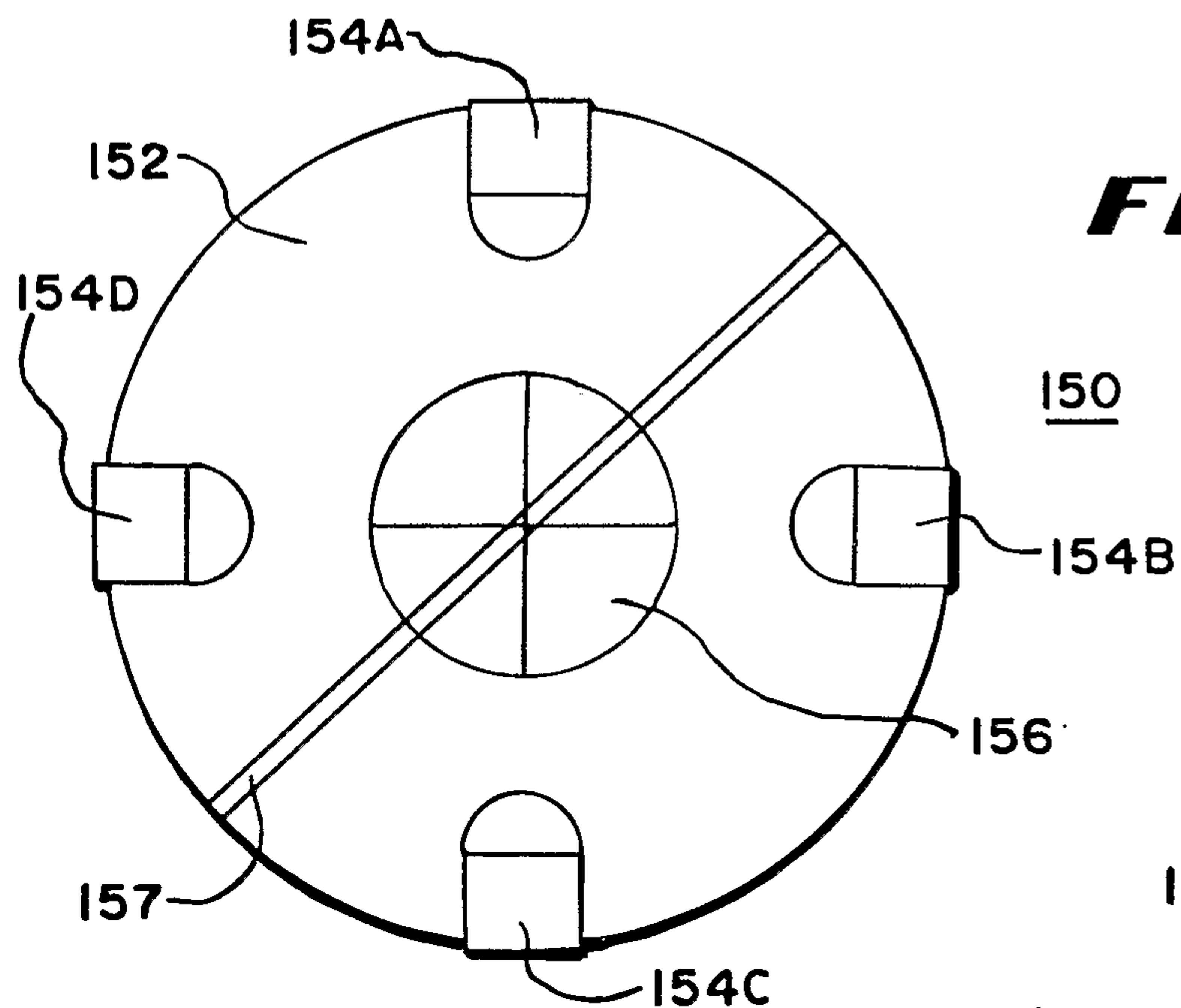
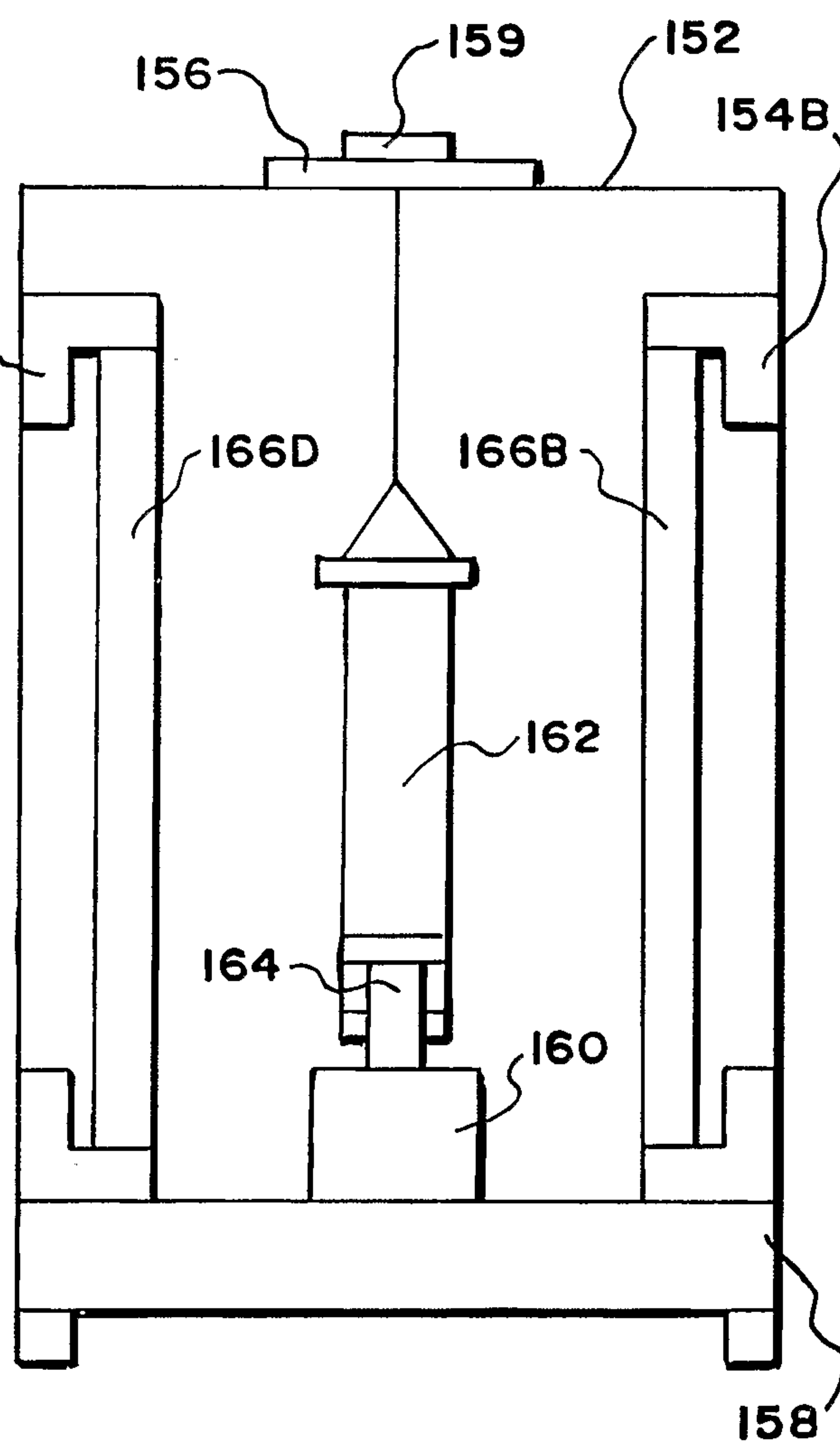
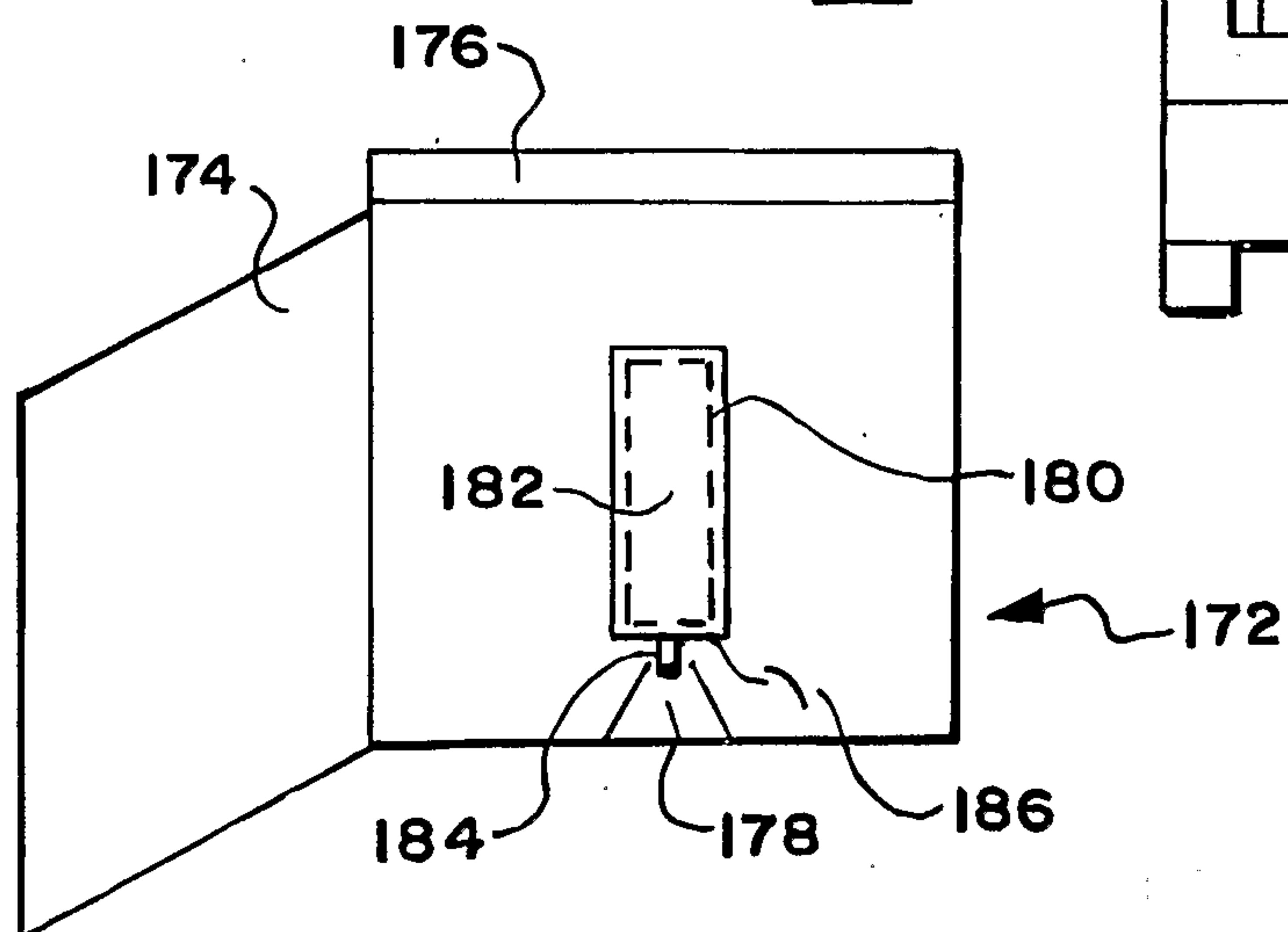
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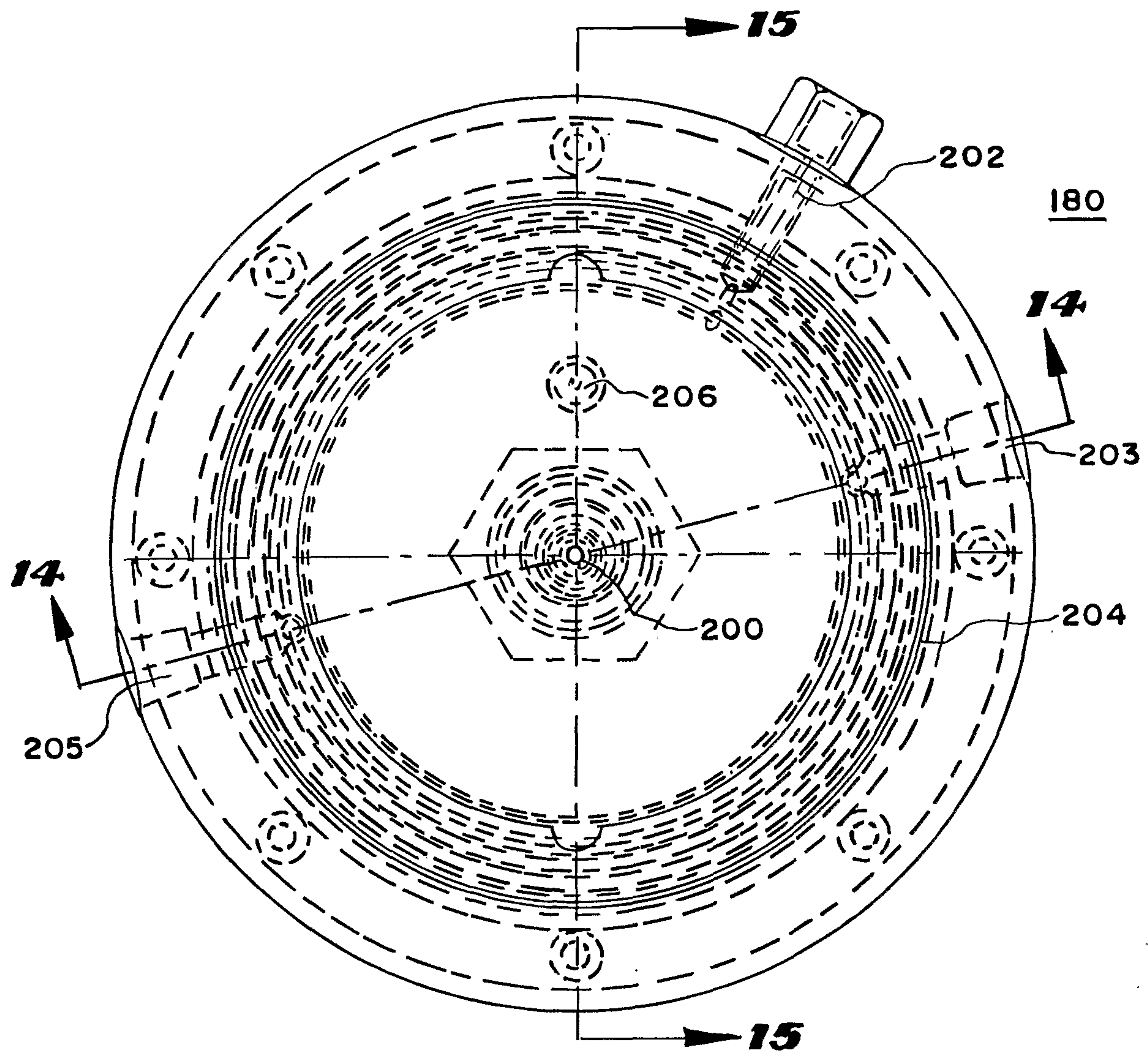
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FIG. 9

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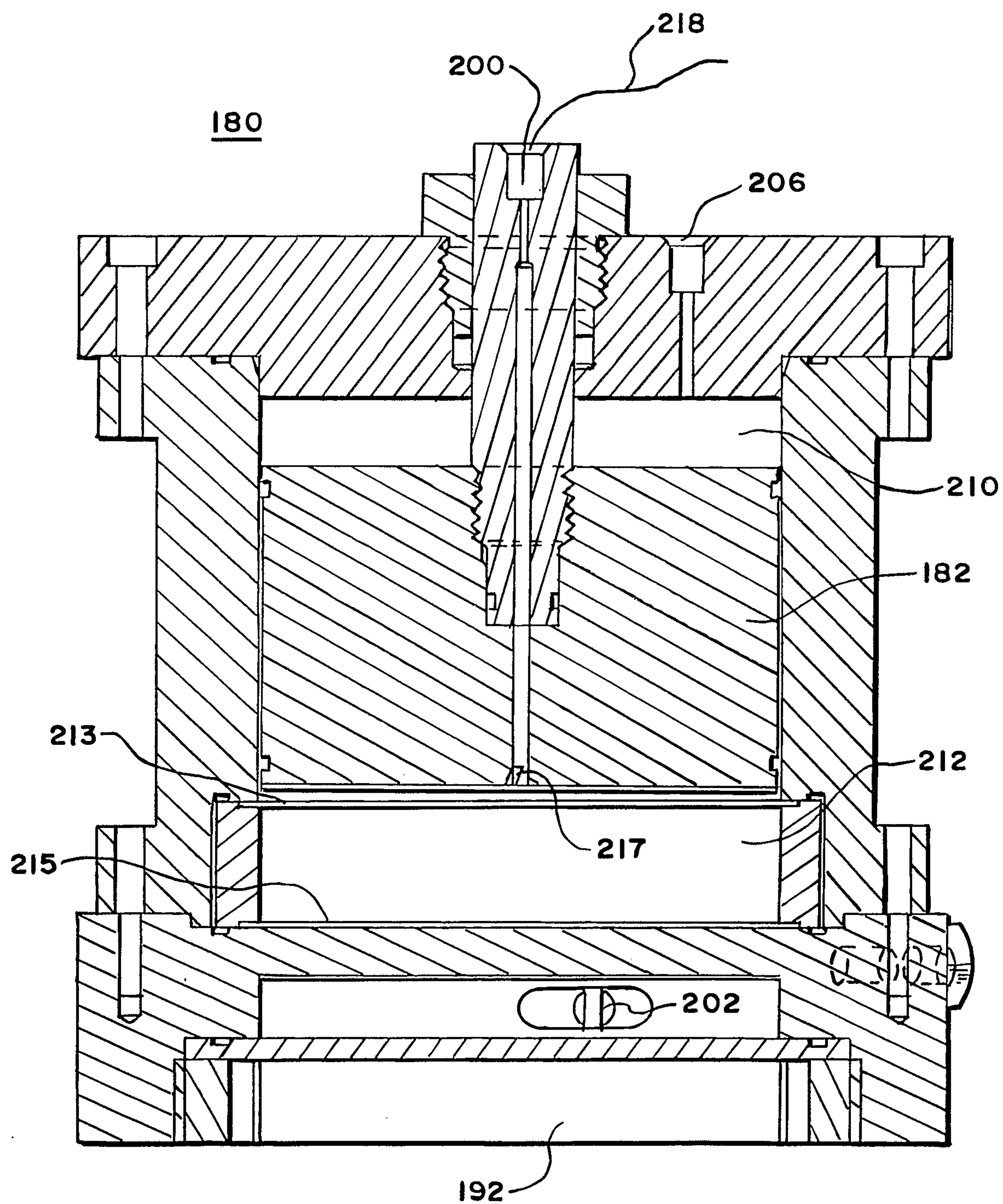
**FIG. 10****FIG. 11**150**FIG. 12**170

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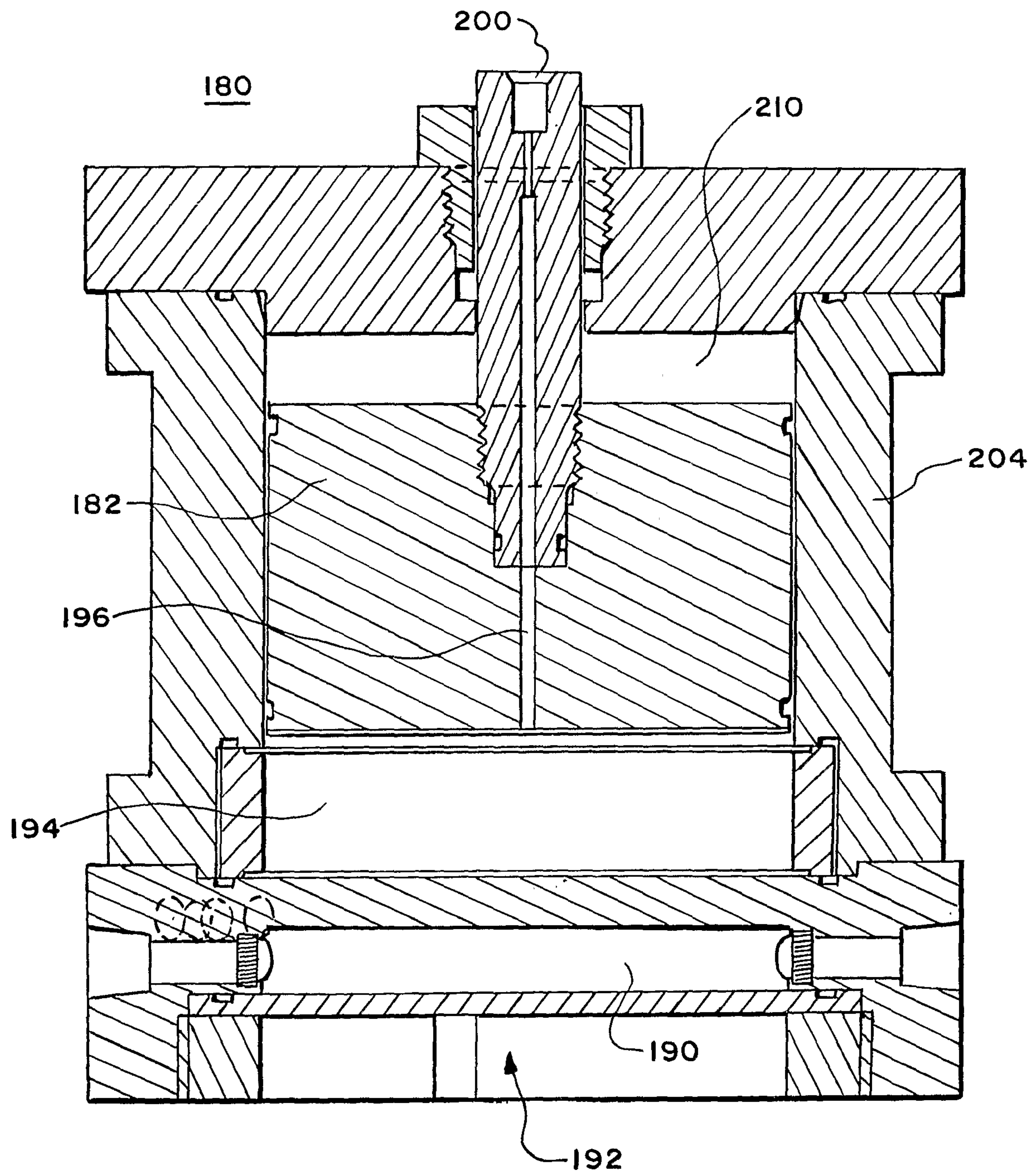
FIG. 13

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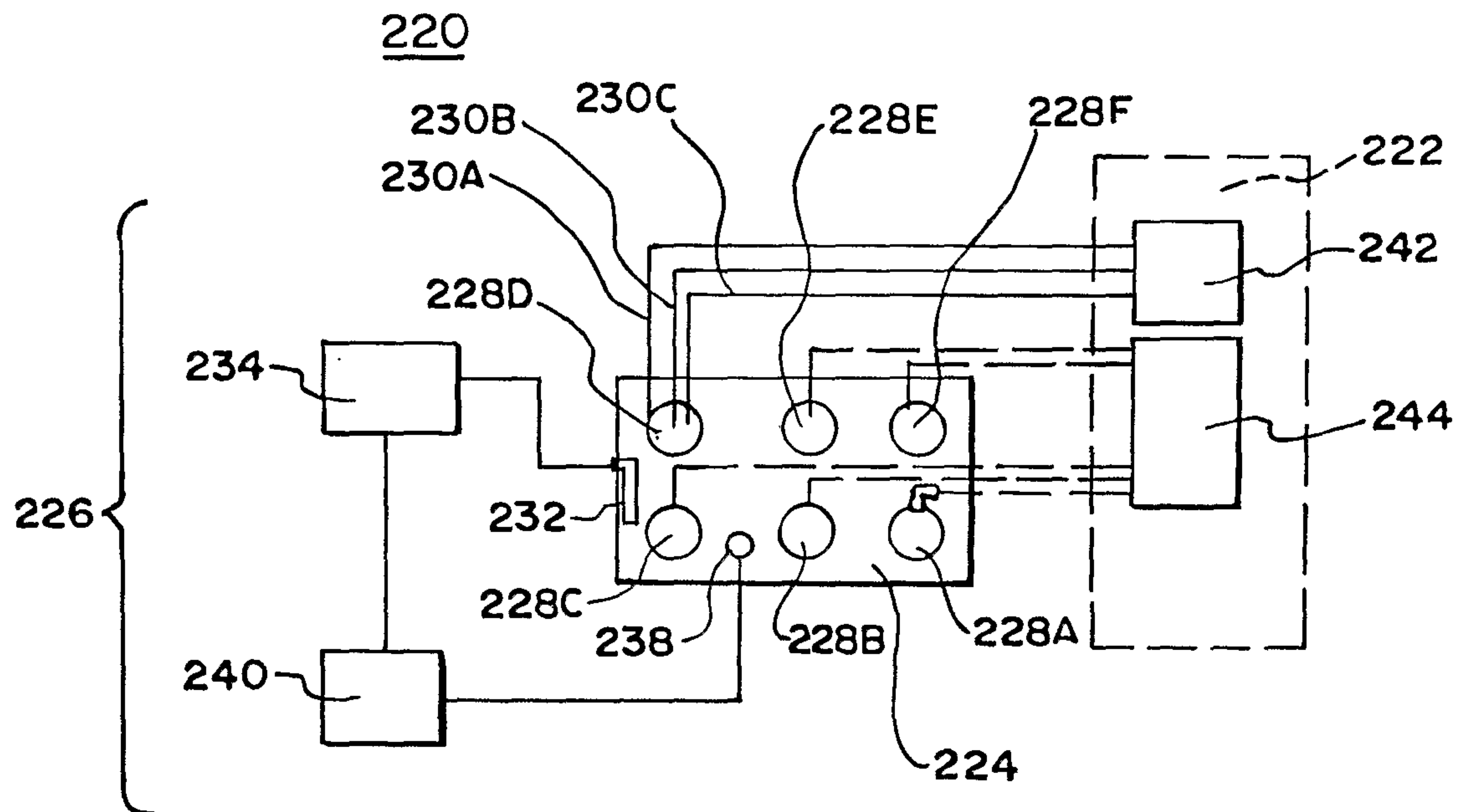
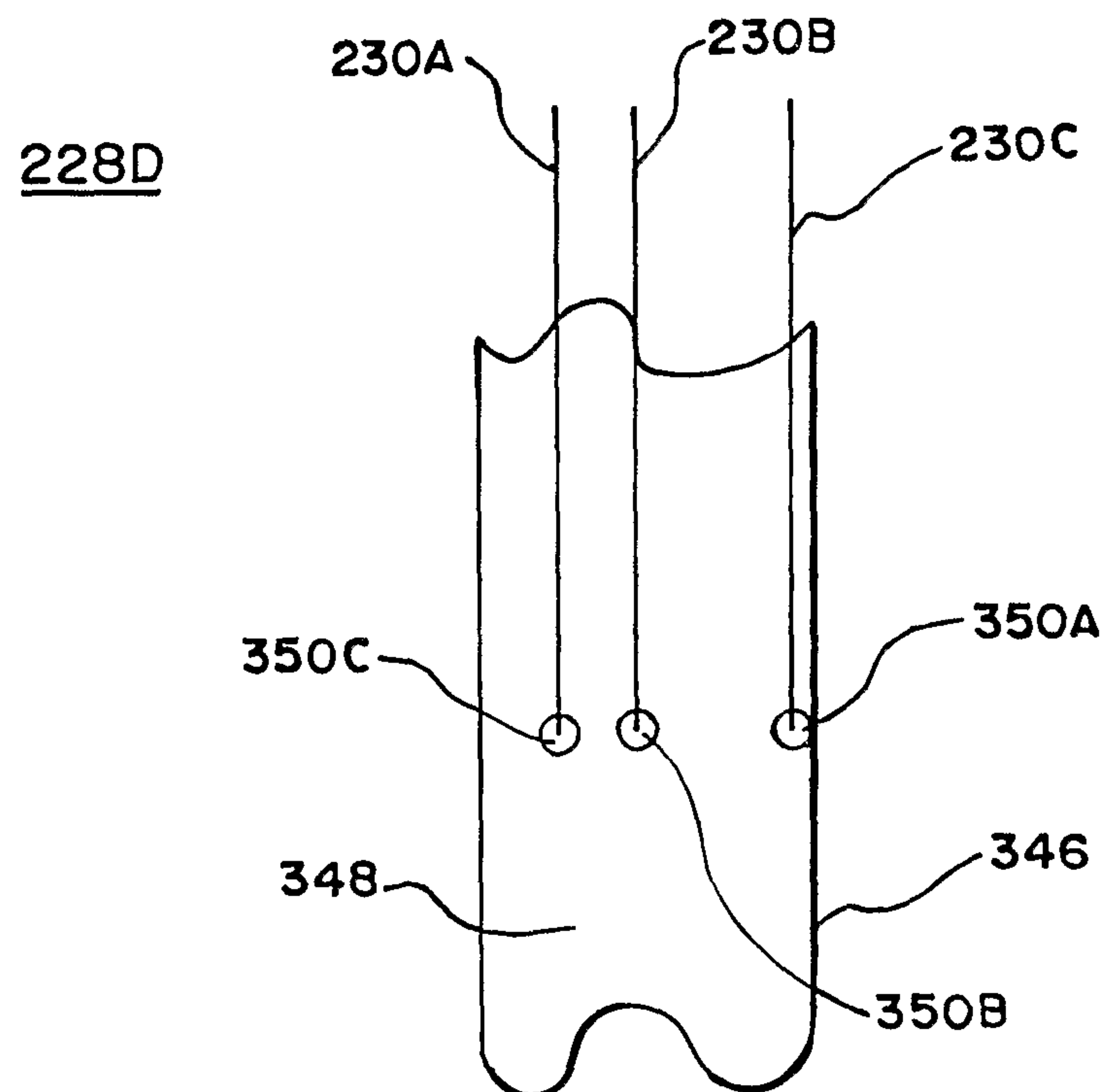
FIG. 14



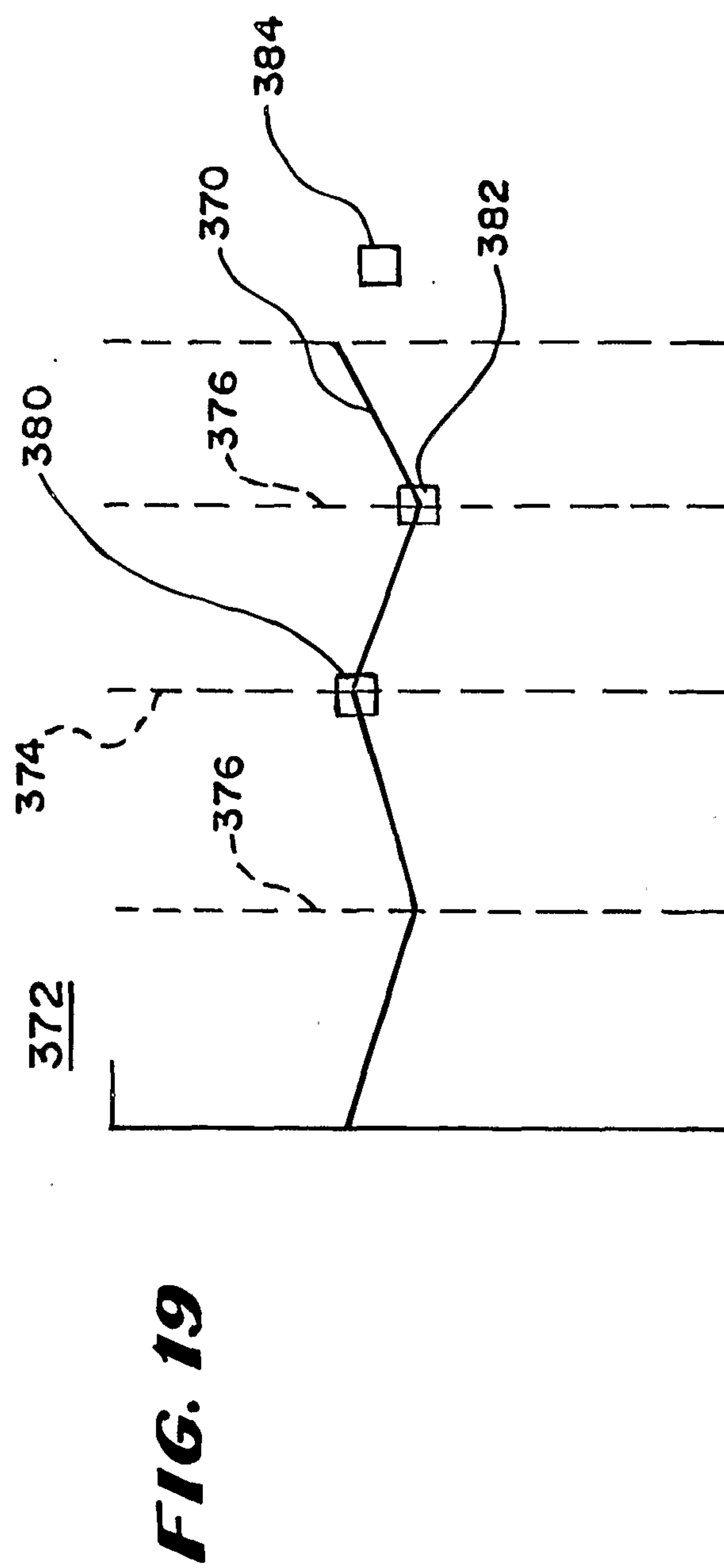
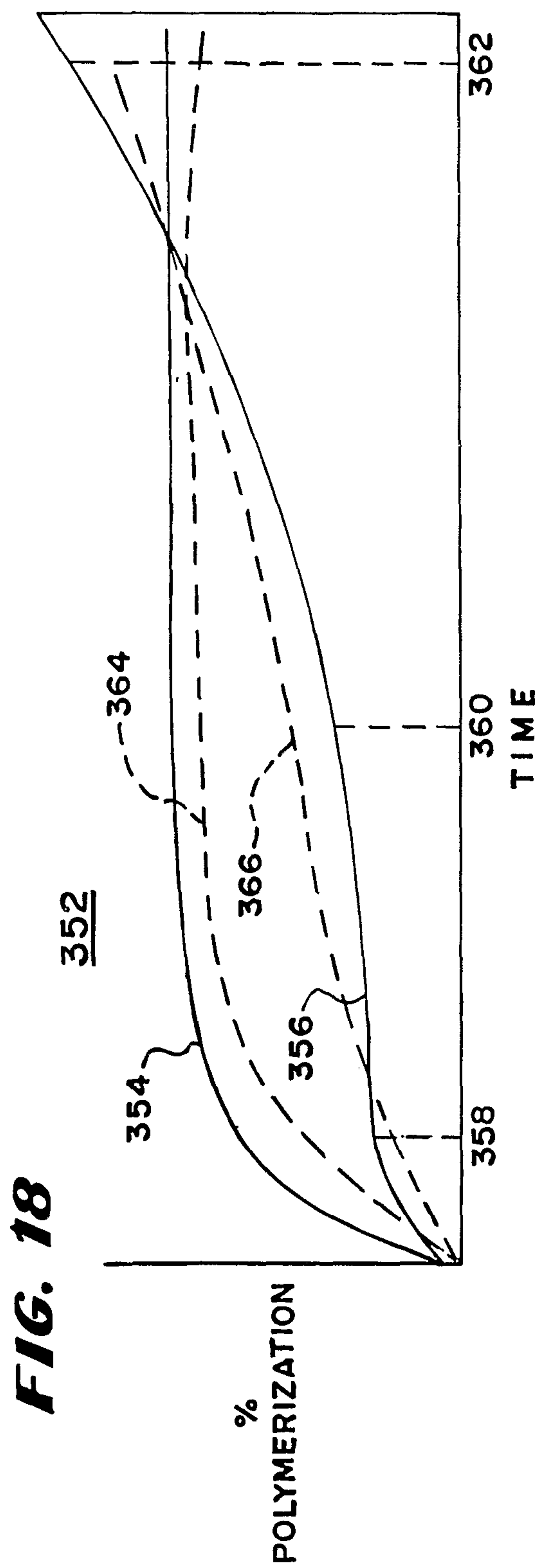
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FIG. 15

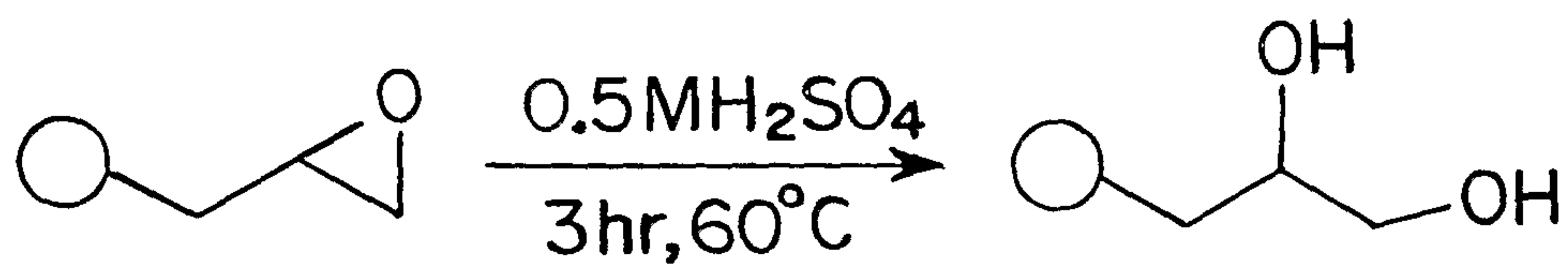
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FIG. 16**FIG 17**

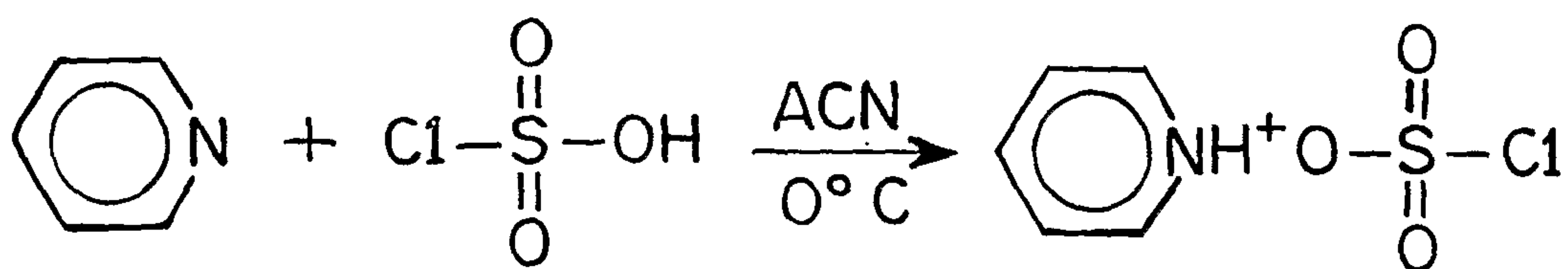
13 / 14



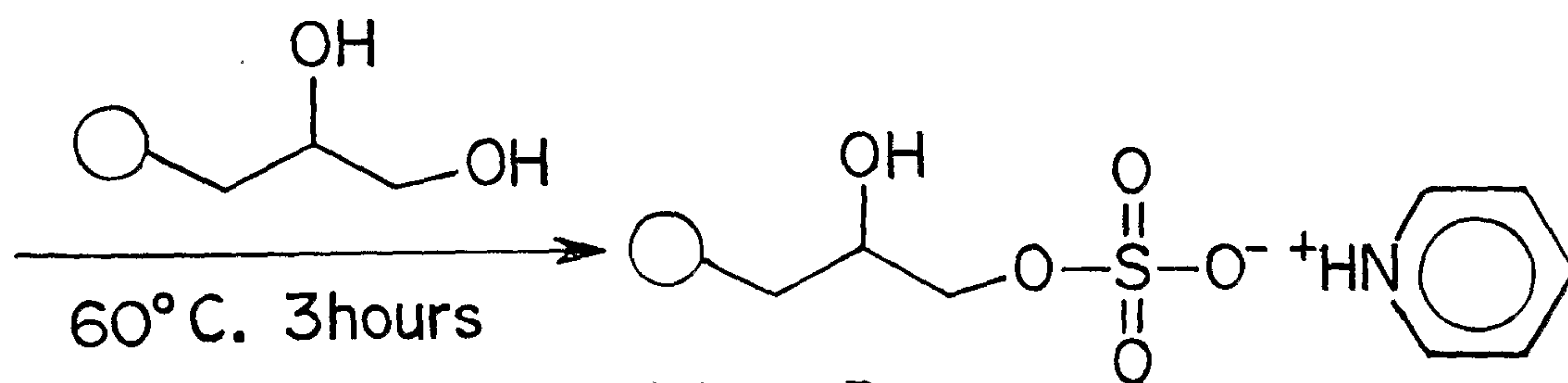
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FIG. 20

EQUATION 1



EQUATION 2



EQUATION 3

FIG. 21