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(71) Applicant: TICONA LLC [US/US]; 8040 Dixie Highway, Florence, Kentucky 41042 (US).

(72) Inventor: KIM, Young, Shin; 8040 Dixie Highway, Florence, Kentucky 41042 (US).

(74) Agent: JOHNSTON, Jason, W.; Dority & Manning, P.A., P O Box 1449, Greenville, South Carolina 29602-1449 (US).

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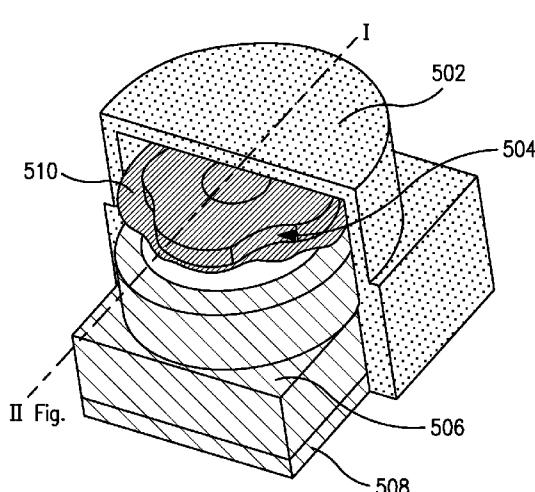


FIG. 6

(57) Abstract: A liquid crystalline polymer composition having a reduced tendency to create a static electric charge during a molding operation is provided. More particularly, the composition contains an ionic liquid that is distributed within a liquid crystalline polymer matrix. In addition to being electrically conductive, the ionic liquid can exist in liquid form during melt processing, which allows it to be more uniformly blended within the liquid crystalline polymer matrix. This improves electrical connectivity and thereby enhances the ability of the composition to rapidly dissipate static electric charges from its surface.

## ANTISTATIC LIQUID CRYSTALLINE POLYMER COMPOSITION

### Related Applications

**[0001]** The present application claims priority to U.S. Provisional Application Serial Nos. 61/714,337 (filed on Oct. 16, 2012) and 61,779,260 (filed on March 13, 2013), which are incorporated herein in its entirety by reference thereto.

### Background of the Invention

**[0002]** Electrical components often contain molded parts that are formed from liquid crystalline polymers due to their ability to form highly ordered structures. For instance, attempts have been made to use liquid crystalline polymers for the molded parts of a compact camera module (“CCM”), such as the lens barrel or the base on which it is mounted. Unfortunately, various problems are often experienced when attempting to form such molded parts from liquid crystalline polymers. When the part is ejected from the mold, for example, a static electric charge may be created that results in the attachment of dust particles to a surface of the part. In certain products, such as compact camera modules, these dust particles are detrimental and can lead to significant product defects. As such, a need exists for a liquid crystalline polymer composition that has a reduced tendency to create a static electric charge during a molding operation.

### Summary of the Invention

**[0003]** In accordance with one embodiment of the present invention, a polymer composition is disclosed that comprises an ionic liquid that is distributed within a liquid crystalline polymer matrix. The ionic liquid has a melting temperature of about 400°C or less and is a salt that contains a cationic species and counterion.

**[0004]** In accordance with another embodiment of the present invention, a molded part is disclosed that comprises a polymer composition. The polymer composition comprises an ionic liquid distributed within a liquid crystalline polymer matrix. The part exhibits a surface resistivity of about  $1 \times 10^{15}$  ohms or less as determined in accordance with IEC 60093.

**[0005]** In accordance with yet another embodiment of the present invention, a compact camera module is disclosed that comprises a generally planar base on

which is mounted a lens barrel. The base, barrel, or both have a thickness of about 500 micrometers or less and are formed from a part that contains a polymer composition comprising a liquid crystalline polymer matrix. The part exhibits a surface resistivity of about  $1 \times 10^{15}$  ohms or less as determined in accordance with IEC 60093.

**[0006]** Other features and aspects of the present invention are set forth in greater detail below.

#### **Brief Description of the Figures**

**[0007]** A full and enabling disclosure of the present invention, including the best mode thereof to one skilled in the art, is set forth more particularly in the remainder of the specification, including reference to the accompanying figures, in which:

**[0008]** Fig. 1 is an exploded perspective view of one embodiment of a fine pitch electrical connector that may be formed according to the present invention;

**[0009]** Fig. 2 is a front view of opposing walls of the fine pitch electrical connector of Fig. 1;

**[0010]** Fig. 3 is a schematic illustration of one embodiment of an extruder screw that may be used to form the polymer composition of the present invention;

**[0011]** Figs. 4-5 are respective front and rear perspective views of an electronic component that can employ an antenna structure formed in accordance with one embodiment of the present invention; and

**[0012]** Figs. 6-7 are perspective and front views of a compact camera module (“CCM”) that may be formed in accordance with one embodiment of the present invention.

#### **Detailed Description**

**[0013]** It is to be understood by one of ordinary skill in the art that the present discussion is a description of exemplary embodiments only, and is not intended as limiting the broader aspects of the present invention.

**[0014]** Generally speaking, the present invention is directed to a liquid crystalline polymer composition having a reduced tendency to create a static electric charge during a molding operation. More particularly, the composition contains an ionic liquid that is distributed within a liquid crystalline polymer matrix. In addition to being electrically conductive, the ionic liquid can exist in

liquid form during melt processing, which allows it to be more uniformly blended within the liquid crystalline polymer matrix. This improves electrical connectivity and thereby enhances the ability of the composition to rapidly dissipate static electric charges from its surface. This antistatic behavior can be characterized by a relatively low surface and/or volume resistivity as determined in accordance with IEC 60093. Namely, a molded part formed from the polymer composition may exhibits a surface resistivity of about  $1 \times 10^{15}$  ohms or less, in some embodiments about  $1 \times 10^{14}$  ohms or less, in some embodiments from about  $1 \times 10^{10}$  ohms to about  $9 \times 10^{13}$  ohms, and in some embodiments, from about  $1 \times 10^{11}$  to about  $1 \times 10^{13}$  ohms. Likewise, the molded part may also exhibit a volume resistivity of about  $1 \times 10^{15}$  ohm-m or less, in some embodiments from about  $1 \times 10^{10}$  ohm-m to about  $9 \times 10^{14}$  ohm-m, and in some embodiments, from about  $1 \times 10^{11}$  to about  $5 \times 10^{14}$  ohm-m.

**[0015]** The present inventor has also discovered that the ability of the ionic liquid to be readily dispersed within the liquid crystalline polymer matrix can allow for the use of relatively low concentrations to achieve the desired antistatic properties. Because it is employed in relatively low concentrations, however, the thermal and mechanical properties of the composition are not adversely impacted. In this regard, ionic liquids typically constitute from about 0.1 wt.% to about 10 wt.%, in some embodiments from about 0.3 wt.% to about 5 wt.%, in some embodiments from about 0.4 wt.% to about 3 wt.%, and in some embodiments, from about 0.5 wt.% to about 1.5 wt.% of the polymer composition. While the concentration of the liquid crystalline polymers may generally vary based on the presence of other optional components, they are typically present in an amount of from about 25 wt.% to about 95 wt.%, in some embodiments from about 30 wt.% to about 80 wt.%, and in some embodiments, from about 40 wt.% to about 70 wt.%.

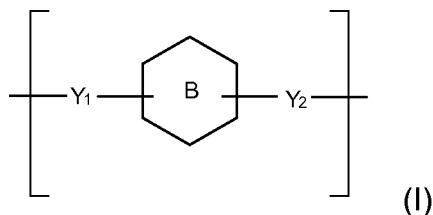
**[0016]** Various embodiments of the present invention will now be described in more detail.

I. Liquid Crystalline Polymer

**[0017]** The thermotropic liquid crystalline polymer generally has a high degree of crystallinity that enables it to effectively fill the small spaces of a mold. Suitable thermotropic liquid crystalline polymers may include aromatic polyesters,

aromatic poly(esteramides), aromatic poly(estercarbonates), aromatic polyamides, etc., and may likewise contain repeating units formed from one or more aromatic hydroxycarboxylic acids, aromatic dicarboxylic acids, aromatic diols, aromatic aminocarboxylic acids, aromatic amines, aromatic diamines, etc., as well as combinations thereof.

**[0018]** Liquid crystalline polymers are generally classified as “thermotropic” to the extent that they can possess a rod-like structure and exhibit a crystalline behavior in its molten state (e.g., thermotropic nematic state). Such polymers may be formed from one or more types of repeating units as is known in the art. The liquid crystalline polymer may, for example, contain one or more aromatic ester repeating units, typically in an amount of from about 60 mol.% to about 99.9 mol.%, in some embodiments from about 70 mol.% to about 99.5 mol.%, and in some embodiments, from about 80 mol.% to about 99 mol.% of the polymer. The aromatic ester repeating units may be generally represented by the following Formula (I):



wherein,

ring B is a substituted or unsubstituted 6-membered aryl group (e.g., 1,4-phenylene or 1,3-phenylene), a substituted or unsubstituted 6-membered aryl group fused to a substituted or unsubstituted 5- or 6-membered aryl group (e.g., 2,6-naphthalene), or a substituted or unsubstituted 6-membered aryl group linked to a substituted or unsubstituted 5- or 6-membered aryl group (e.g., 4,4-biphenylene); and

$Y_1$  and  $Y_2$  are independently O, C(O), NH, C(O)HN, or NHC(O).

**[0019]** Typically, at least one of  $Y_1$  and  $Y_2$  are C(O). Examples of such aromatic ester repeating units may include, for instance, aromatic dicarboxylic repeating units ( $Y_1$  and  $Y_2$  in Formula I are C(O)), aromatic hydroxycarboxylic repeating units ( $Y_1$  is O and  $Y_2$  is C(O) in Formula I), as well as various combinations thereof.

**[0020]** Aromatic dicarboxylic repeating units, for instance, may be employed that are derived from aromatic dicarboxylic acids, such as terephthalic acid, isophthalic acid, 2,6-naphthalenedicarboxylic acid, diphenyl ether-4,4'-dicarboxylic acid, 1,6-naphthalenedicarboxylic acid, 2,7-naphthalenedicarboxylic acid, 4,4'-dicarboxybiphenyl, bis(4-carboxyphenyl)ether, bis(4-carboxyphenyl)butane, bis(4-carboxyphenyl)ethane, bis(3-carboxyphenyl)ether, bis(3-carboxyphenyl)ethane, etc., as well as alkyl, alkoxy, aryl and halogen substituents thereof, and combinations thereof. Particularly suitable aromatic dicarboxylic acids may include, for instance, terephthalic acid ("TA"), isophthalic acid ("IA"), and 2,6-naphthalenedicarboxylic acid ("NDA"). When employed, repeating units derived from aromatic dicarboxylic acids (e.g., IA, TA, and/or NDA) typically constitute from about 5 mol.% to about 60 mol.%, in some embodiments from about 10 mol.% to about 55 mol.%, and in some embodiments, from about 15 mol.% to about 50% of the polymer.

**[0021]** Aromatic hydroxycarboxylic repeating units may also be employed that are derived from aromatic hydroxycarboxylic acids, such as, 4-hydroxybenzoic acid; 4-hydroxy-4'-biphenylcarboxylic acid; 2-hydroxy-6-naphthoic acid; 2-hydroxy-5-naphthoic acid; 3-hydroxy-2-naphthoic acid; 2-hydroxy-3-naphthoic acid; 4'-hydroxyphenyl-4-benzoic acid; 3'-hydroxyphenyl-4-benzoic acid; 4'-hydroxyphenyl-3-benzoic acid, etc., as well as alkyl, alkoxy, aryl and halogen substituents thereof, and combination thereof. Particularly suitable aromatic hydroxycarboxylic acids are 4-hydroxybenzoic acid ("HBA") and 6-hydroxy-2-naphthoic acid ("HNA"). When employed, repeating units derived from hydroxycarboxylic acids (e.g., HBA and/or HNA) typically constitute from about 10 mol.% to about 85 mol.%, in some embodiments from about 20 mol.% to about 80 mol.%, and in some embodiments, from about 25 mol.% to about 75% of the polymer.

**[0022]** Other repeating units may also be employed in the polymer. In certain embodiments, for instance, repeating units may be employed that are derived from aromatic diols, such as hydroquinone, resorcinol, 2,6-dihydroxynaphthalene, 2,7-dihydroxynaphthalene, 1,6-dihydroxynaphthalene, 4,4'-dihydroxybiphenyl (or 4,4'-biphenol), 3,3'-dihydroxybiphenyl, 3,4'-dihydroxybiphenyl, 4,4'-dihydroxybiphenyl ether, bis(4-hydroxyphenyl)ethane, etc., as well as alkyl, alkoxy, aryl and halogen substituents thereof, and combinations

thereof. Particularly suitable aromatic diols may include, for instance, hydroquinone (“HQ”) and 4,4'-biphenol (“BP”). When employed, repeating units derived from aromatic diols (e.g., HQ and/or BP) typically constitute from about 1 mol.% to about 30 mol.%, in some embodiments from about 2 mol.% to about 25 mol.%, and in some embodiments, from about 5 mol.% to about 20% of the polymer. Repeating units may also be employed, such as those derived from aromatic amides (e.g., acetaminophen (“APAP”)) and/or aromatic amines (e.g., 4-aminophenol (“AP”), 3-aminophenol, 1,4-phenylenediamine, 1,3-phenylenediamine, etc.). When employed, repeating units derived from aromatic amides (e.g., APAP) and/or aromatic amines (e.g., AP) typically constitute from about 0.1 mol.% to about 20 mol.%, in some embodiments from about 0.5 mol.% to about 15 mol.%, and in some embodiments, from about 1 mol.% to about 10% of the polymer. It should also be understood that various other monomeric repeating units may be incorporated into the polymer. For instance, in certain embodiments, the polymer may contain one or more repeating units derived from non-aromatic monomers, such as aliphatic or cycloaliphatic hydroxycarboxylic acids, dicarboxylic acids, diols, amides, amines, etc. Of course, in other embodiments, the polymer may be “wholly aromatic” in that it lacks repeating units derived from non-aromatic (e.g., aliphatic or cycloaliphatic) monomers.

**[0023]** Although not necessarily required, the liquid crystalline polymer may be a “low naphthenic” polymer to the extent that it contains a minimal content of repeating units derived from naphthenic hydroxycarboxylic acids and naphthenic dicarboxylic acids, such as naphthalene-2,6-dicarboxylic acid (“NDA”), 6-hydroxy-2-naphthoic acid (“HNA”), or combinations thereof. That is, the total amount of repeating units derived from naphthenic hydroxycarboxylic and/or dicarboxylic acids (e.g., NDA, HNA, or a combination of HNA and NDA) is typically no more than 30 mol.%, in some embodiments no more than about 15 mol.%, in some embodiments no more than about 10 mol.%, in some embodiments no more than about 8 mol.%, and in some embodiments, from 0 mol.% to about 5 mol.% of the polymer (e.g., 0 mol.%). Despite the absence of a high level of conventional naphthenic acids, it is believed that the resulting “low naphthenic” polymers are still capable of exhibiting good thermal and mechanical properties.

**[0024]** In one particular embodiment, the liquid crystalline polymer may be formed from repeating units derived from 4-hydroxybenzoic acid (“HBA”) and terephthalic acid (“TA”) and/or isophthalic acid (“IA”), as well as various other optional constituents. The repeating units derived from 4-hydroxybenzoic acid (“HBA”) may constitute from about 10 mol.% to about 80 mol.%, in some embodiments from about 30 mol.% to about 75 mol.%, and in some embodiments, from about 45 mol.% to about 70% of the polymer. The repeating units derived from terephthalic acid (“TA”) and/or isophthalic acid (“IA”) may likewise constitute from about 5 mol.% to about 40 mol.%, in some embodiments from about 10 mol.% to about 35 mol.%, and in some embodiments, from about 15 mol.% to about 35% of the polymer. Repeating units may also be employed that are derived from 4,4'-biphenol (“BP”) and/or hydroquinone (“HQ”) in an amount from about 1 mol.% to about 30 mol.%, in some embodiments from about 2 mol.% to about 25 mol.%, and in some embodiments, from about 5 mol.% to about 20% of the polymer. Other possible repeating units may include those derived from 6-hydroxy-2-naphthoic acid (“HNA”), 2,6-naphthalenedicarboxylic acid (“NDA”), and/or acetaminophen (“APAP”). In certain embodiments, for example, repeating units derived from HNA, NDA, and/or APAP may each constitute from about 1 mol.% to about 35 mol.%, in some embodiments from about 2 mol.% to about 30 mol.%, and in some embodiments, from about 3 mol.% to about 25 mol.% when employed.

**[0025]** Regardless of the particular constituents and nature of the polymer, the liquid crystalline polymer may be prepared by initially introducing the aromatic monomer(s) used to form ester repeating units (e.g., aromatic hydroxycarboxylic acid, aromatic dicarboxylic acid, etc.) and/or other repeating units (e.g., aromatic diol, aromatic amide, aromatic amine, etc.) into a reactor vessel to initiate a polycondensation reaction. The particular conditions and steps employed in such reactions are well known, and may be described in more detail in U.S. Patent No. 4,161,470 to Calundann; U.S. Patent No. 5,616,680 to Linstid, III, et al.; U.S. Patent No. 6,114,492 to Linstid, III, et al.; U.S. Patent No. 6,514,611 to Shepherd, et al.; and WO 2004/058851 to Waggoner. The vessel employed for the reaction is not especially limited, although it is typically desired to employ one that is commonly used in reactions of high viscosity fluids. Examples of such a reaction

vessel may include a stirring tank-type apparatus that has an agitator with a variably-shaped stirring blade, such as an anchor type, multistage type, spiral-ribbon type, screw shaft type, etc., or a modified shape thereof. Further examples of such a reaction vessel may include a mixing apparatus commonly used in resin kneading, such as a kneader, a roll mill, a Banbury mixer, etc.

**[0026]** If desired, the reaction may proceed through the acetylation of the monomers as known the art. This may be accomplished by adding an acetylating agent (e.g., acetic anhydride) to the monomers. Acetylation is generally initiated at temperatures of about 90°C. During the initial stage of the acetylation, reflux may be employed to maintain vapor phase temperature below the point at which acetic acid byproduct and anhydride begin to distill. Temperatures during acetylation typically range from between 90°C to 150°C, and in some embodiments, from about 110°C to about 150°C. If reflux is used, the vapor phase temperature typically exceeds the boiling point of acetic acid, but remains low enough to retain residual acetic anhydride. For example, acetic anhydride vaporizes at temperatures of about 140°C. Thus, providing the reactor with a vapor phase reflux at a temperature of from about 110°C to about 130°C is particularly desirable. To ensure substantially complete reaction, an excess amount of acetic anhydride may be employed. The amount of excess anhydride will vary depending upon the particular acetylation conditions employed, including the presence or absence of reflux. The use of an excess of from about 1 to about 10 mole percent of acetic anhydride, based on the total moles of reactant hydroxyl groups present is not uncommon.

**[0027]** Acetylation may occur in a separate reactor vessel, or it may occur *in situ* within the polymerization reactor vessel. When separate reactor vessels are employed, one or more of the monomers may be introduced to the acetylation reactor and subsequently transferred to the polymerization reactor. Likewise, one or more of the monomers may also be directly introduced to the reactor vessel without undergoing pre-acetylation.

**[0028]** In addition to the monomers and optional acetylating agents, other components may also be included within the reaction mixture to help facilitate polymerization. For instance, a catalyst may be optionally employed, such as metal salt catalysts (e.g., magnesium acetate, tin(I) acetate, tetrabutyl titanate,

lead acetate, sodium acetate, potassium acetate, etc.) and organic compound catalysts (e.g., N-methylimidazole). Such catalysts are typically used in amounts of from about 50 to about 500 parts per million based on the total weight of the recurring unit precursors. When separate reactors are employed, it is typically desired to apply the catalyst to the acetylation reactor rather than the polymerization reactor, although this is by no means a requirement.

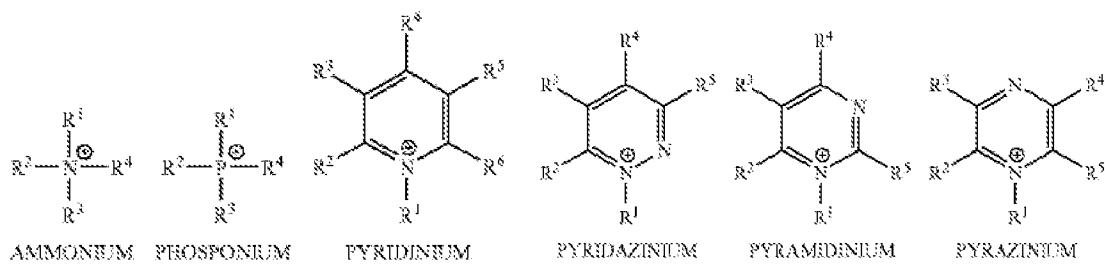
**[0029]** The reaction mixture is generally heated to an elevated temperature within the polymerization reactor vessel to initiate melt polycondensation of the reactants. Polycondensation may occur, for instance, within a temperature range of from about 250°C to about 400°C, in some embodiments from about 280°C to about 395°C, and in some embodiments, from about 300°C to about 380°C. For instance, one suitable technique for forming the liquid crystalline polymer may include charging precursor monomers and acetic anhydride into the reactor, heating the mixture to a temperature of from about 90°C to about 150°C to acetylate a hydroxyl group of the monomers (e.g., forming acetoxy), and then increasing the temperature to from about 250°C to about 400°C to carry out melt polycondensation. As the final polymerization temperatures are approached, volatile byproducts of the reaction (e.g., acetic acid) may also be removed so that the desired molecular weight may be readily achieved. The reaction mixture is generally subjected to agitation during polymerization to ensure good heat and mass transfer, and in turn, good material homogeneity. The rotational velocity of the agitator may vary during the course of the reaction, but typically ranges from about 10 to about 100 revolutions per minute (“rpm”), and in some embodiments, from about 20 to about 80 rpm. To build molecular weight in the melt, the polymerization reaction may also be conducted under vacuum, the application of which facilitates the removal of volatiles formed during the final stages of polycondensation. The vacuum may be created by the application of a suctional pressure, such as within the range of from about 5 to about 30 pounds per square inch (“psi”), and in some embodiments, from about 10 to about 20 psi.

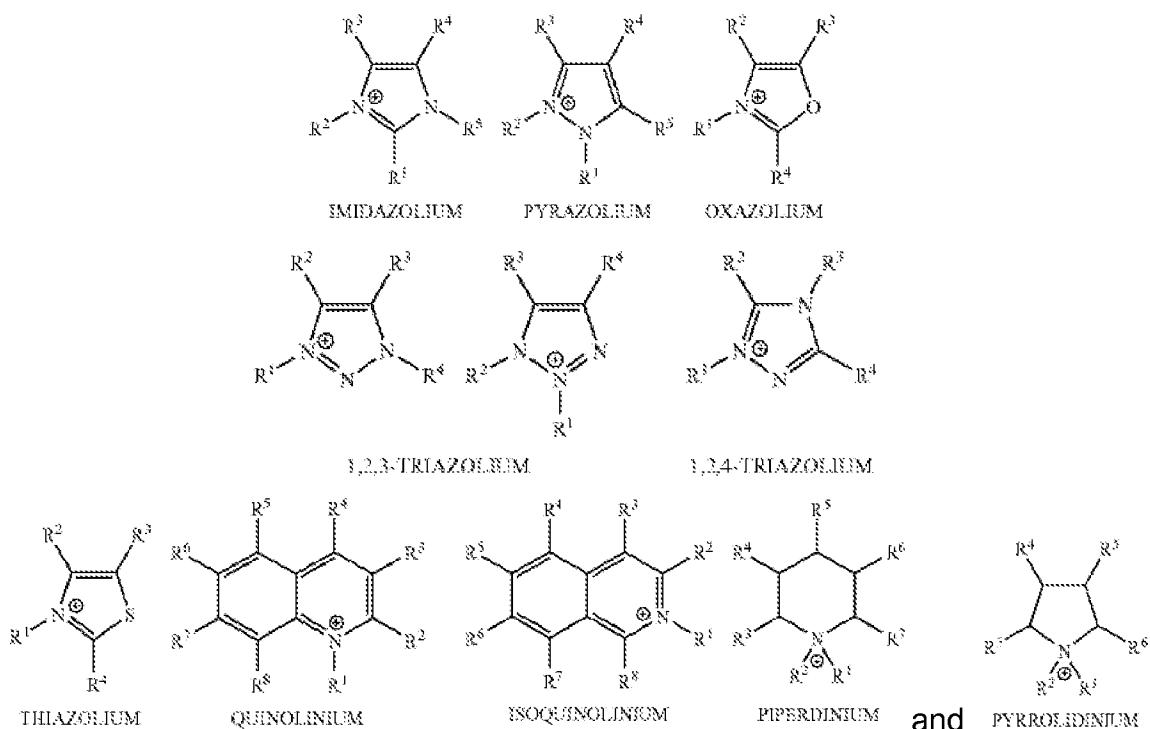
**[0030]** Following melt polymerization, the molten polymer may be discharged from the reactor, typically through an extrusion orifice fitted with a die of desired configuration, cooled, and collected. Commonly, the melt is discharged through a perforated die to form strands that are taken up in a water

bath, pelletized and dried. In some embodiments, the melt polymerized polymer may also be subjected to a subsequent solid-state polymerization method to further increase its molecular weight. Solid-state polymerization may be conducted in the presence of a gas (e.g., air, inert gas, etc.). Suitable inert gases may include, for instance, include nitrogen, helium, argon, neon, krypton, xenon, etc., as well as combinations thereof. The solid-state polymerization reactor vessel can be of virtually any design that will allow the polymer to be maintained at the desired solid-state polymerization temperature for the desired residence time. Examples of such vessels can be those that have a fixed bed, static bed, moving bed, fluidized bed, etc. The temperature at which solid-state polymerization is performed may vary, but is typically within a range of from about 250°C to about 350°C. The polymerization time will of course vary based on the temperature and target molecular weight. In most cases, however, the solid-state polymerization time will be from about 2 to about 12 hours, and in some embodiments, from about 4 to about 10 hours.

## II. Ionic Liquid

**[0031]** The ionic liquid of the present invention is generally a salt that has a low enough melting temperature so that it can be in the form of a liquid when melt processed with the liquid crystalline polymer. For example, the melting temperature of the ionic liquid may be about 400°C or less, in some embodiments about 350°C or less, in some embodiments from about 1°C to about 100°C, and in some embodiments, from about 5°C to about 50°C. The salt contains a cationic species and counterion. The cationic species contains a compound having at least one heteroatom (e.g., nitrogen or phosphorous) as a “cationic center.” Examples of such heteroatomic compounds include, for instance, quaternary oniums having the following structures:





**[0032]** wherein,  $R^1$ ,  $R^2$ ,  $R^3$ ,  $R^4$ ,  $R^5$ ,  $R^6$ ,  $R^7$ , and  $R^8$  are independently selected from the group consisting of hydrogen; substituted or unsubstituted  $C_1$ - $C_{10}$  alkyl groups (e.g., methyl, ethyl, n-propyl, isopropyl, n-butyl, isobutyl, sec-butyl, tert-butyl, n-pentyl, etc.); substituted or unsubstituted  $C_3$ - $C_{14}$  cycloalkyl groups (e.g., adamantyl, cyclopropyl, cyclobutyl, cyclopentyl, cyclooctyl, cyclohexenyl, etc.); substituted or unsubstituted  $C_1$ - $C_{10}$  alkenyl groups (e.g., ethylene, propylene, 2-methypropylene, pentylene, etc.); substituted or unsubstituted  $C_2$ - $C_{10}$  alkynyl groups (e.g., ethynyl, propynyl, etc.); substituted or unsubstituted  $C_1$ - $C_{10}$  alkoxy groups (e.g., methoxy, ethoxy, n-propoxy, isopropoxy, n-butoxy, t-butoxy, sec-butoxy, n-pentoxyl, etc.); substituted or unsubstituted acyloxy groups (e.g., methacryloxy, methacryloxyethyl, etc.); substituted or unsubstituted aryl groups (e.g., phenyl); substituted or unsubstituted heteroaryl groups (e.g., pyridyl, furanyl, thienyl, thiazolyl, isothiazolyl, triazolyl, imidazolyl, isoxazolyl, pyrrolyl, pyrazolyl, pyridazinyl, pyrimidinyl, quinolyl, etc.); and so forth. In one particular embodiment, for example, the cationic species may be an ammonium compound having the structure  $N^+R^1R^2R^3R^4$ , wherein  $R^1$ ,  $R^2$ , and/or  $R^3$  are independently a  $C_1$ - $C_6$  alkyl (e.g., methyl, ethyl, butyl, etc.) and  $R^4$  is hydrogen or a  $C_1$ - $C_4$  alkyl group (e.g., methyl or ethyl). For example, the cationic component may be tri-butylmethylammonium, wherein  $R^1$ ,  $R^2$ , and  $R^3$  are butyl and  $R^4$  is methyl.

**[0033]** Suitable counterions for the cationic species may include, for example, halogens (e.g., chloride, bromide, iodide, etc.); sulfates or sulfonates (e.g., methyl sulfate, ethyl sulfate, butyl sulfate, hexyl sulfate, octyl sulfate, hydrogen sulfate, methane sulfonate, dodecylbenzene sulfonate, dodecylsulfate, trifluoromethane sulfonate, heptadecafluorooctanesulfonate, sodium dodecylethoxysulfate, etc.); sulfosuccinates; amides (e.g., dicyanamide); imides (e.g., bis(pentafluoroethyl-sulfonyl)imide, bis(trifluoromethylsulfonyl)imide, bis(trifluoromethyl)imide, etc.); borates (e.g., tetrafluoroborate, tetracyanoborate, bis[oxalato]borate, bis[salicylato]borate, etc.); phosphates or phosphinates (e.g., hexafluorophosphate, diethylphosphate, bis(pentafluoroethyl)phosphinate, tris(pentafluoroethyl)-trifluorophosphate, tris(nonafluorobutyl)trifluorophosphate, etc.); antimonates (e.g., hexafluoroantimonate); aluminates (e.g., tetrachloroaluminate); fatty acid carboxylates (e.g., oleate, isostearate, pentadecafluorooctanoate, etc.); cyanates; acetates; and so forth, as well as combinations of any of the foregoing. To help improve compatibility with the liquid crystalline polymer, it may be desired to select a counterion that is generally hydrophobic in nature, such as imides, fatty acid carboxylates, etc. Particularly suitable hydrophobic counterions may include, for instance, bis(pentafluoroethylsulfonyl)imide, bis(trifluoromethylsulfonyl)imide, and bis(trifluoromethyl)imide.

### III. Optional Components

#### A. Conductive Fillers

**[0034]** In addition to the ionic liquid, other conductive fillers may also be employed in the polymer composition to help improve its antistatic characteristics. Examples of suitable conductive fillers may include, for instance, metal particles (e.g., aluminum flakes), metal fibers, carbon particles (e.g., graphite, expanded graphite, grapheme, carbon black, graphitized carbon black, etc.), carbon nanotubes, carbon fibers, and so forth. Carbon fibers and graphite are particularly suitable. In certain embodiments, a synergistic affect may be achieved by using the ionic liquid and conductive fillers in combination. Without intending to be limited by theory, the present inventor believes that the ionic liquid is able to readily flow during melt processing to help provide a better connection and electrical pathway between certain conductive fillers (e.g., carbon fibers, graphite, etc.) and

the liquid crystalline polymer matrix, thereby further reducing surface resistivity. When employed, the conductive fillers typically constitute from about 0.5 wt.% to about 30 wt.%, in some embodiments from about 1 wt.% to about 25 wt.%, and in some embodiments, from about 2 wt.% to about 20 wt.% of the polymer composition.

B. Fibrous Fillers

**[0035]** Fibrous fillers, which are not generally conductive, may also be employed in the polymer composition to help improve strength. Examples of such fibrous fillers may include those formed from glass, ceramics (e.g., alumina, silica, titanium dioxide, etc.), minerals (e.g., wollastonite, xonotlite, dawsonite, etc.), polymers, such as aramids (e.g., Kevlar® marketed by E.I. DuPont de Nemours, Wilmington, Delaware, polyolefins, polyesters, etc., as well as mixtures thereof.

**[0036]** Particularly suitable glass fibers may include, for instance, E-glass, A-glass, C-glass, D-glass, AR-glass, R-glass, S1-glass, S2-glass, etc., and mixtures thereof. The volume average length of such glass fibers may be relatively small, such as from about 10 to about 500 micrometers, in some embodiments from about 100 to about 400 micrometers, in some embodiments from about 150 to about 350 micrometers, and in some embodiments, from about 200 to about 325 micrometers. The glass fibers may also have a narrow length distribution. That is, at least about 70% by volume of the fibers, in some embodiments at least about 80% by volume of the fibers, and in some embodiments, at least about 90% by volume of the fibers have a length within the ranges noted above. Such a small length and/or narrow distribution can further help achieve a desirable combination of strength, flowability, and surface quality, which enables it to be uniquely suited for molded parts with a small dimensional tolerance. In addition to possessing the length characteristics noted above, the glass fibers may also have a relatively high aspect ratio (average length divided by nominal diameter) to help improve the mechanical properties and surface quality of the resulting polymer composition. For example, the fibers may have an aspect ratio of from about 1 to about 100, in some embodiments from about 10 to about 60, and in some embodiments, from about 30 to about 50 are particularly beneficial. The fibers may, for example, have a nominal diameter of from about 1 to about 35 micrometers, in some embodiments from about 2 to

about 20 micrometers, and in some embodiments, from about 3 to about 10 micrometers.

**[0037]** Mineral fibers (also known as “whiskers”) are also suitable for use in the present invention. Particularly suitable are anhydrous calcium sulfate and wollastonite fibers, such as those available from Nyco Minerals under the trade designation NYGLOS® (e.g., NYGLOS® 4W or NYGLOS® 8). The volume average length of such mineral fibers may be relatively small, such as from about 1 to about 200 micrometers, in some embodiments from about 2 to about 150 micrometers, in some embodiments from about 5 to about 100 micrometers, and in some embodiments, from about 10 to about 50 micrometers. In addition to possessing the length characteristics noted above, the mineral fibers may also have a relatively high aspect ratio (average length divided by nominal diameter) to help further improve the mechanical properties and surface quality of the resulting polymer composition. For example, the mineral fibers may have an aspect ratio of from about 1 to about 50, in some embodiments from about 2 to about 20, and in some embodiments, from about 4 to about 15. The whiskers may, for example, have a nominal diameter of from about 1 to about 35 micrometers, in some embodiments from about 2 to about 20 micrometers, and in some embodiments, from about 3 to about 15 micrometers.

**[0038]** Regardless of the particular type employed, the relative amount of the fibrous filler in the polymer composition may be selectively controlled to help achieve the desired mechanical properties without adversely impacting other properties of the composition, such as its flowability. For example, fibrous fillers (e.g., glass fibers, mineral fibers, etc., as well as combinations thereof) typically constitute from about 2 wt.% to about 40 wt.%, in some embodiments from about 5 wt.% to about 35 wt.%, and in some embodiments, from about 6 wt.% to about 30 wt.% of the polymer composition. Although the fibers may be employed within the ranges noted above, one particularly beneficial aspect of the present invention is that small fiber contents may be employed while still achieving the desired mechanical properties. Without intending to be limited by theory, it is believed that the narrow length distribution of the fibers can help achieve excellent mechanical properties, thus allowing for the use of a smaller amount of fibers.

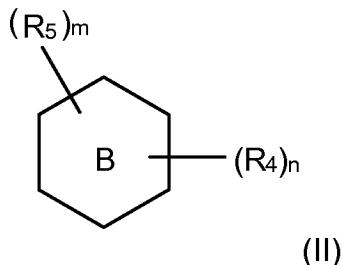
### C. Particulate Fillers

**[0039]** Particulate fillers, which are not generally conductive, may also be employed in the polymer composition to help achieve the desired properties and/or color. When employed, such particulate fillers typically constitute from about 5% by weight to about 40% by weight, in some embodiments from about 10% by weight to about 35% by weight, and in some embodiments, from about 10% by weight to about 30% by weight of the polymer composition. Clay minerals may be particularly suitable for use in the present invention. Examples of such clay minerals include, for instance, talc ( $Mg_3Si_4O_{10}(OH)_2$ ), halloysite ( $Al_2Si_2O_5(OH)_4$ ), kaolinite ( $Al_2Si_2O_5(OH)_4$ ), illite ( $(K,H_3O)(Al,Mg,Fe)_2(Si,Al)_4O_{10}[(OH)_2,(H_2O)]$ ), montmorillonite ( $(Na,Ca)_{0.33}(Al,Mg)_2Si_4O_{10}(OH)_2 \cdot nH_2O$ ), vermiculite ( $(Mg,Fe,Al)_3(Al,Si)_4O_{10}(OH)_2 \cdot 4H_2O$ ), palygorskite ( $(Mg,Al)_2Si_4O_{10}(OH) \cdot 4(H_2O)$ ), pyrophyllite ( $Al_2Si_4O_{10}(OH)_2$ ), etc., as well as combinations thereof. In lieu of, or in addition to, clay minerals, still other particulate fillers may also be employed. For example, other suitable silicate fillers may also be employed, such as calcium silicate, aluminum silicate, mica, diatomaceous earth, wollastonite, and so forth. Mica, for instance, may be a particularly suitable mineral for use in the present invention. There are several chemically distinct mica species with considerable variance in geologic occurrence, but all have essentially the same crystal structure. As used herein, the term "mica" is meant to generically include any of these species, such as muscovite ( $KAl_2(AlSi_3)O_{10}(OH)_2$ ), biotite ( $K(Mg,Fe)_3(AlSi_3)O_{10}(OH)_2$ ), phlogopite ( $KMg_3(AlSi_3)O_{10}(OH)_2$ ), lepidolite ( $K(Li,Al)_{2-3}(AlSi_3)O_{10}(OH)_2$ ), glauconite ( $(K,Na)(Al,Mg,Fe)_2(Si,Al)_4O_{10}(OH)_2$ ), etc., as well as combinations thereof.

### D. Functional Compounds

**[0040]** If desired, functional compounds may also be employed in the present invention to, among other things, help reduce the melt viscosity of the polymer composition. In one embodiment, for example, the polymer composition of the present invention may contain a functional aromatic compound. Such compounds typically contain one or more carboxyl and/or hydroxyl functional groups that can react with the polymer chain to shorten its length, thus reducing the melt viscosity. In certain cases, the compound may also be able to combine smaller chains of the polymer together after they have been cut to help maintain

the mechanical properties of the composition even after its melt viscosity has been reduced. The functional aromatic compound may have the general structure provided below in Formula (II):



or a metal salt thereof, wherein,

ring B is a 6-membered aromatic ring wherein 1 to 3 ring carbon atoms are optionally replaced by nitrogen or oxygen, wherein each nitrogen is optionally oxidized, and wherein ring B may be optionally fused or linked to a 5- or 6-membered aryl, heteroaryl, cycloalkyl, or heterocyclyl;

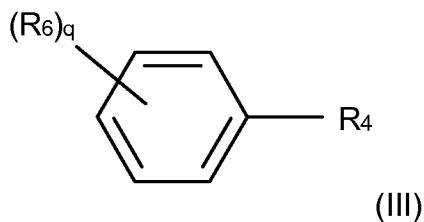
R<sub>4</sub> is OH or COOH;

R<sub>5</sub> is acyl, acyloxy (e.g., acetyloxy), acylamino (e.g., acetylamino), alkoxy, alkenyl, alkyl, amino, aryl, aryloxy, carboxyl, carboxyl ester, cycloalkyl, cycloalkyloxy, hydroxyl, halo, haloalkyl, heteroaryl, heteroaryloxy, heterocyclyl, or heterocycloxy;

m is from 0 to 4, in some embodiments from 0 to 2, and in some embodiments, from 0 to 1; and

n is from 1 to 3, and in some embodiments, from 1 to 2. When the compound is in the form of a metal salt, suitable metal counterions may include transition metal counterions (e.g., copper, iron, etc.), alkali metal counterions (e.g., potassium, sodium, etc.), alkaline earth metal counterions (e.g., calcium, magnesium, etc.), and/or main group metal counterions (e.g., aluminum).

**[0041]** In one embodiment, for example, B is phenyl in Formula (II) such that the resulting phenolic compounds have the following general formula (III):



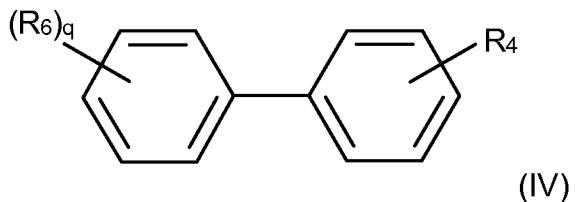
or a metal salt thereof, wherein,

R<sub>4</sub> is OH or COOH;

R<sub>6</sub> is acyl, acyloxy, acylamino, alkoxy, alkenyl, alkyl, amino, carboxyl, carboxyl ester, hydroxyl, halo, or haloalkyl; and

q is from 0 to 4, in some embodiments from 0 to 2, and in some embodiments, from 0 to 1. Particular examples of such phenolic compounds include, for instance, benzoic acid (q is 0); 4-hydroxybenzoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); phthalic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); isophthalic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); terephthalic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); 2-methylterephthalic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and CH<sub>3</sub> and q is 2); phenol (R<sub>4</sub> is OH and q is 0); sodium phenoxide (R<sub>4</sub> is OH and q is 0); hydroquinone (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); resorcinol (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); 4-hydroxybenzoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is C(O)OH, and q is 1), etc., as well as combinations thereof.

**[0042]** In another embodiment, B is phenyl and R<sub>5</sub> is phenyl in Formula (II) above such that the diphenolic compounds have the following general formula (IV):



or a metal salt thereof, wherein,

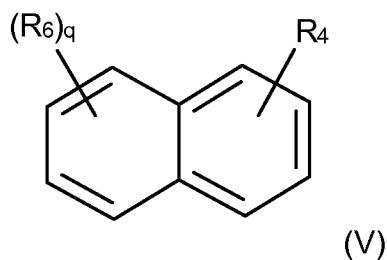
R<sub>4</sub> is COOH or OH;

R<sub>6</sub> is acyl, acyloxy, acylamino, alkoxy, alkenyl, alkyl, amino, aryl, aryloxy, carboxyl, carboxyl ester, cycloalkyl, cycloalkyloxy, hydroxyl, halo, haloalkyl, heteroaryl, heteroaryloxy, heterocyclyl, or heterocycloxy; and

q is from 0 to 4, in some embodiments from 0 to 2, and in some embodiments, from 0 to 1. Particular examples of such diphenolic compounds include, for instance, 4-hydroxy-4'-biphenylcarboxylic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 4'-hydroxyphenyl-4-benzoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 3'-hydroxyphenyl-4-benzoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 4'-hydroxyphenyl-3-benzoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 4,4'-bibenzoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); 3,3'-biphenol (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); 3,4'-biphenol (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q

is 1); 4-phenylphenol (R<sub>4</sub> is OH and q is 0); bis(4-hydroxyphenyl)ethane (R<sub>4</sub> is OH, R<sub>6</sub> is C<sub>2</sub>(OH)<sub>2</sub>phenol, and q is 1); tris(4-hydroxyphenyl)ethane (R<sub>4</sub> is OH, R<sub>6</sub> is C(CH<sub>3</sub>)biphenol, and q is 1); 4-hydroxy-4'-biphenylcarboxylic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 4'-hydroxyphenyl-4-benzoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 3'-hydroxyphenyl-4-benzoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 4'-hydroxyphenyl-3-benzoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); etc., as well as combinations thereof.

**[0043]** In yet another embodiment, B is naphthyl in Formula (II) above such that the resulting naphthenic compounds have the following general formula (V):



or a metal salt thereof, wherein,

R<sub>4</sub> is OH or COOH;

R<sub>6</sub> is acyl, acyloxy, acylamino, alkoxy, alkenyl, alkyl, amino, aryl, aryloxy, carboxyl, carboxyl ester, cycloalkyl, cycloalkyloxy, hydroxyl, halo, haloalkyl, heteroaryl, heteroaryloxy, heterocyclyl, or heterocycloxy; and

q is from 0 to 4, in some embodiments from 0 to 2, and in some embodiments, from 0 to 1. Particular examples of such naphthenic compounds include, for instance, 1-naphthoic acid (R<sub>4</sub> is COOH and q is 0); 2-naphthoic acid (R<sub>4</sub> is COOH and q is 0); 2-hydroxy-6-naphthoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 2-hydroxy-5-naphthoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 3-hydroxy-2-naphthoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 2-hydroxy-3-naphthoic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is OH, and q is 1); 2,6-naphthalenedicarboxylic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); 2,3-naphthalenedicarboxylic acid (R<sub>4</sub> is COOH, R<sub>6</sub> is COOH, and q is 1); 2-hydroxy-naphthelene (R<sub>4</sub> is OH and q is 0); 2-hydroxy-6-naphthoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 2-hydroxy-5-naphthoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 3-hydroxy-2-naphthoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 2-hydroxy-3-naphthoic acid (R<sub>4</sub> is OH, R<sub>6</sub> is COOH, and q is 1); 2,6-dihydroxynaphthalene (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); 2,7-

dihydroxynaphthalene (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1); 1,6-dihydroxynaphthalene (R<sub>4</sub> is OH, R<sub>6</sub> is OH, and q is 1), etc., as well as combinations thereof.

**[0044]** In certain embodiments of the present invention, for example, the polymer composition may contain an aromatic diol, such as hydroquinone, resorcinol, 4,4'-biphenol, etc., as well as combinations thereof. When employed, such aromatic diols may constitute from about 0.01 wt.% to about 1 wt.%, and in some embodiments, from about 0.05 wt.% to about 0.4 wt.% of the polymer composition. An aromatic carboxylic acid may also be employed in certain embodiments, either alone or in conjunction with the aromatic diol. Aromatic carboxylic acids may constitute from about 0.001 wt.% to about 0.5 wt.%, and in some embodiments, from about 0.005 wt.% to about 0.1 wt.% of the polymer composition. In particular embodiments, a combination of an aromatic diol (R<sub>4</sub> and R<sub>6</sub> are OH in the formulae above) (e.g., 4,4'-biphenol) and an aromatic dicarboxylic acid (R<sub>4</sub> and R<sub>6</sub> are COOH in the formulae above) (e.g., 2,6-naphthelene dicarboxylic acid) is employed in the present invention to help achieve the desired viscosity reduction.

**[0045]** In addition to those noted above, non-aromatic functional compounds may also be employed in the present invention. Such compounds may serve a variety of purposes, such as reducing melt viscosity. One such non-aromatic functional compound is water. If desired, water can be added in a form that under process conditions generates water. For example, the water can be added as a hydrate that under the process conditions (e.g., high temperature) effectively "loses" water. Such hydrates include alumina trihydrate, copper sulfate pentahydrate, barium chloride dihydrate, calcium sulfate dehydrate, etc., as well as combinations thereof. When employed, the hydrates may constitute from about 0.02 wt.% to about 2 wt.%, and in some embodiments, from about 0.05 wt.% to about 1 wt.% of the polymer composition. In one particular embodiment, a mixture of an aromatic diol, hydrate, and aromatic dicarboxylic acid are employed in the composition. In such embodiments, the weight ratio of hydrates to aromatic diols is typically from about 0.5 to about 8, in some embodiments from about 0.8 to about 5, and in some embodiments, from about 1 to about 5.

#### E. Other Additives

**[0046]** Still other additives that can be included in the composition may include, for instance, antimicrobials, pigments, antioxidants, stabilizers, surfactants, waxes, solid solvents, flame retardants, anti-drip additives, and other materials added to enhance properties and processability. Lubricants may also be employed in the polymer composition that are capable of withstanding the processing conditions of the liquid crystalline polymer without substantial decomposition. Examples of such lubricants include fatty acids esters, the salts thereof, esters, fatty acid amides, organic phosphate esters, and hydrocarbon waxes of the type commonly used as lubricants in the processing of engineering plastic materials, including mixtures thereof. Suitable fatty acids typically have a backbone carbon chain of from about 12 to about 60 carbon atoms, such as myristic acid, palmitic acid, stearic acid, arachic acid, montanic acid, octadecinic acid, parinric acid, and so forth. Suitable esters include fatty acid esters, fatty alcohol esters, wax esters, glycerol esters, glycol esters and complex esters. Fatty acid amides include fatty primary amides, fatty secondary amides, methylene and ethylene bisamides and alkanolamides such as, for example, palmitic acid amide, stearic acid amide, oleic acid amide, N,N'-ethylenebisstearamide and so forth. Also suitable are the metal salts of fatty acids such as calcium stearate, zinc stearate, magnesium stearate, and so forth; hydrocarbon waxes, including paraffin waxes, polyolefin and oxidized polyolefin waxes, and microcrystalline waxes. Particularly suitable lubricants are acids, salts, or amides of stearic acid, such as pentaerythritol tetrastearate, calcium stearate, or N,N'-ethylenebisstearamide. When employed, the lubricant(s) typically constitute from about 0.05 wt.% to about 1.5 wt.%, and in some embodiments, from about 0.1 wt.% to about 0.5 wt.% (by weight) of the polymer composition.

#### IV. Formation

**[0047]** The liquid crystalline polymer, ionic liquid, and other optional additives may be melt processed or blended together within a temperature range of from about 250°C to about 450°C, in some embodiments, from about 280°C to about 400°C, and in some embodiments, from about 300°C to about 380°C to

form the polymer composition. Any of a variety of melt processing techniques may generally be employed in the present invention. For example, the components (e.g., liquid crystalline polymer, ionic liquid, etc.) may be supplied separately or in combination to an extruder that includes at least one screw rotatably mounted and received within a barrel (e.g., cylindrical barrel) and may define a feed section and a melting section located downstream from the feed section along the length of the screw.

**[0048]** The extruder may be a single screw or twin screw extruder. Referring to Fig. 3, for example, one embodiment of a single screw extruder 80 is shown that contains a housing or barrel 114 and a screw 120 rotatably driven on one end by a suitable drive 124 (typically including a motor and gearbox). If desired, a twin-screw extruder may be employed that contains two separate screws. The configuration of the screw is not particularly critical to the present invention and it may contain any number and/or orientation of threads and channels as is known in the art. As shown in Fig. 3, for example, the screw 120 contains a thread that forms a generally helical channel radially extending around a core of the screw 120. A hopper 40 is located adjacent to the drive 124 for supplying the liquid crystalline polymer and/or other materials (e.g., inorganic particles and/or functional compound) through an opening in the barrel 114 to the feed section 132. Opposite the drive 124 is the output end 144 of the extruder 80, where extruded plastic is output for further processing.

**[0049]** A feed section 132 and melt section 134 are defined along the length of the screw 120. The feed section 132 is the input portion of the barrel 114 where the liquid crystalline polymer and/or the ionic liquid are added. The melt section 134 is the phase change section in which the liquid crystalline polymer is changed from a solid to a liquid. While there is no precisely defined delineation of these sections when the extruder is manufactured, it is well within the ordinary skill of those in this art to reliably identify the feed section 132 and the melt section 134 in which phase change from solid to liquid is occurring. Although not necessarily required, the extruder 80 may also have a mixing section 136 that is located adjacent to the output end of the barrel 114 and downstream from the melting section 134. If desired, one or more distributive and/or dispersive mixing elements may be employed within the mixing and/or

melting sections of the extruder. Suitable distributive mixers for single screw extruders may include, for instance, Saxon, Dulmage, Cavity Transfer mixers, etc. Likewise, suitable dispersive mixers may include Blister ring, Leroy/Maddock, CRD mixers, etc. As is well known in the art, the mixing may be further improved by using pins in the barrel that create a folding and reorientation of the polymer melt, such as those used in Buss Kneader extruders, Cavity Transfer mixers, and Vortex Intermeshing Pin mixers.

**[0050]** When employed, fibers (e.g., conductive fillers, such as carbon fibers, and/or fibrous fillers, such as glass fibers) can also be added to the hopper 40 or at a location downstream therefrom. In one particular embodiment, fibers may be added a location downstream from the point at which the liquid crystalline polymer is supplied, but yet prior to the melting section. In Fig. 3, for instance, a hopper 42 is shown that is located within a zone of the feed section 132 of the extruder 80. The fibers supplied to the hopper 42 may be initially relatively long, such as having a volume average length of from about 1,000 to about 5,000 micrometers, in some embodiments from about 2,000 to about 4,500 micrometers, and in some embodiments, from about 3,000 to about 4,000 micrometers. Nevertheless, by supplying these long fibers at a location where the liquid crystalline polymer is still in a solid state, the polymer can act as an abrasive agent for reducing the size of the fibers to a volume average length and length distribution as indicated above. It should be understood, however, any optional fibers may simply be supplied to the extruder at the desired length. In such embodiments, the fibers may, for example, be supplied at the mixing and/or melting sections of the extruder, or even at the feed section in conjunction with the liquid crystalline polymer. In yet other embodiments, fibers may not be employed at all.

**[0051]** Regardless of the particular manner in which it is formed, the present inventor has discovered that the resulting polymer composition can possess excellent thermal properties. For example, the melt viscosity of the polymer composition may be low enough so that it can readily flow into the cavity of a mold having small dimensions. In one particular embodiment, the polymer composition may have a melt viscosity of from about 0.1 to about 80 Pa-s, in some embodiments from about 0.5 to about 50 Pa-s, and in some embodiments,

from about 1 to about 30 Pa-s, determined at a shear rate of 1000 seconds<sup>-1</sup>. Melt viscosity may be determined in accordance with ISO Test No. 11443 at a temperature that is 15°C higher than the melting temperature of the composition (e.g., 350°C). The composition may also have a relatively high melting temperature. For example, the melting temperature of the polymer may be from about 250°C to about 400°C, in some embodiments from about 280°C to about 395°C, and in some embodiments, from about 300°C to about 380°C.

#### V. Molded Parts

**[0052]** Once formed, the polymer composition may be molded into any of a variety of different shaped parts using techniques as is known in the art. For example, the shaped parts may be molded using a one-component injection molding process in which dried and preheated plastic granules are injected into the mold. Regardless of the molding technique employed, it has been discovered that the polymer composition of the present invention, which possesses the unique combination of good antistatic properties, high flowability and good mechanical properties, is particularly well suited for electronic parts having a small dimensional tolerance. Such parts, for example, generally contain at least one micro-sized dimension (e.g., thickness, width, height, etc.), such as from about 500 micrometers or less, in some embodiments from about 50 to about 450 micrometers, and in some embodiments, from about 100 to about 400 micrometers.

**[0053]** One such part is a fine pitch electrical connector. More particularly, such electrical connectors are often employed to detachably mount a central processing unit (“CPU”) to a printed circuit board. The connector may contain insertion passageways that are configured to receive contact pins. These passageways are defined by opposing walls, which may be formed from a thermoplastic resin. To help accomplish the desired electrical performance, the pitch of these pins is generally small to accommodate a large number of contact pins required within a given space. This, in turn, requires that the pitch of the pin insertion passageways and the width of opposing walls that partition those passageways are also small. For example, the walls may have a width of from about 500 micrometers or less, in some embodiments from about 50 to about 450 micrometers, and in some embodiments, from about 100 to about 400

micrometers. In the past, it has often been difficult to adequately fill a mold of such a thin width with a thermoplastic resin. Due to its unique properties, however, the polymer composition of the present invention is particularly well suited to form the walls of a fine pitch connector.

**[0054]** One particularly suitable fine pitch electrical connector is shown in Fig. 1. An electrical connector 200 is shown that a board-side portion C2 that can be mounted onto the surface of a circuit board P. The connector 200 may also include a wiring material-side portion C1 structured to connect discrete wires 3 to the circuit board P by being coupled to the board-side connector C2. The board-side portion C2 may include a first housing 10 that has a fitting recess 10a into which the wiring material-side connector C1 is fitted and a configuration that is slim and long in the widthwise direction of the housing 10. The wiring material-side portion C1 may likewise include a second housing 20 that is slim and long in the widthwise direction of the housing 20. In the second housing 20, a plurality of terminal-receiving cavities 22 may be provided in parallel in the widthwise direction so as to create a two-tier array including upper and lower terminal-receiving cavities 22. A terminal 5, which is mounted to the distal end of a discrete wire 3, may be received within each of the terminal-receiving cavities 22. If desired, locking portions 28 (engaging portions) may also be provided on the housing 20 that correspond to a connection member (not shown) on the board-side connector C2.

**[0055]** As discussed above, the interior walls of the first housing 10 and/or second housing 20 may have a relatively small width dimension, and can be formed from the polymer composition of the present invention. The walls are, for example, shown in more detail in Fig. 2. As illustrated, insertion passageways or spaces 225 are defined between opposing walls 224 that can accommodate contact pins. The walls 224 have a width "w" that is within the ranges noted above. When the walls 224 are formed from a polymer composition containing fibers (e.g., element 400), such fibers may have a volume average length and narrow length distribution within a certain range to best match the width of the walls. For example, the ratio of the width of at least one of the walls to the volume average length of the fibers is from about 0.8 to about 3.2, in some

embodiments from about 1.0 to about 3.0, and in some embodiments, from about 1.2 to about 2.9.

**[0056]** In addition to or in lieu of the walls, it should also be understood that any other portion of the housing may also be formed from the polymer composition of the present invention. For example, the connector may also include a shield that encloses the housing. Some or all of the shield may be formed from the polymer composition of the present invention. For example, the housing and the shield can each be a one-piece structure unitarily molded from the polymer composition. Likewise, the shield can be a two-piece structure that includes a first shell and a second shell, each of which may be formed from the polymer composition of the present invention.

**[0057]** Of course, the polymer composition may also be used in a wide variety of other components. For example, the polymer composition may be molded into a planar substrate for use in an electronic component. The substrate may be thin, such as having a thickness of about 500 micrometers or less, in some embodiments from about 50 to about 450 micrometers, and in some embodiments, from about 100 to about 400 micrometers. In one embodiment, for example, the planar substrate may be applied with one or more conductive elements using a variety of known techniques (e.g., laser direct structuring, electroplating, etc.). The conductive elements may serve a variety of different purposes. In one embodiment, for example, the conductive elements form an integrated circuit, such as those used in SIM cards. In another embodiment, the conductive elements form antennas of a variety of different types, such as antennae with resonating elements that are formed from patch antenna structures, inverted-F antenna structures, closed and open slot antenna structures, loop antenna structures, monopoles, dipoles, planar inverted-F antenna structures, hybrids of these designs, etc. The resulting antenna structures may be incorporated into the housing of a relatively compact portable electronic component, such as described above, in which the available interior space is relatively small.

**[0058]** One particularly suitable electronic component that includes an antenna structure is shown in Figs. 4-5 is a handheld device 410 with cellular telephone capabilities. As shown in Fig. 4, the device 410 may have a housing

412 formed from plastic, metal, other suitable dielectric materials, other suitable conductive materials, or combinations of such materials. A display 414 may be provided on a front surface of the device 410, such as a touch screen display. The device 410 may also have a speaker port 440 and other input-output ports. One or more buttons 438 and other user input devices may be used to gather user input. As shown in Fig. 5, an antenna structure 426 is also provided on a rear surface 442 of device 410, although it should be understood that the antenna structure can generally be positioned at any desired location of the device. As indicated above, the antenna structure 426 may contain a planar substrate that is formed from the polymer composition of the present invention. The antenna structure may be electrically connected to other components within the electronic device using any of a variety of known techniques. For example, the housing 412 or a part of housing 412 may serve as a conductive ground plane for the antenna structure 426.

**[0059]** A planar substrate that is formed from the polymer composition of the present invention may also be employed in other applications. For example, in one embodiment, the planar substrate may be used to form a base of a compact camera module (“CCM”), which is commonly employed in wireless communication devices (e.g., cellular phone). Referring to Figs. 6-7, for example, one particular embodiment of a compact camera module 500 is shown in more detail. As shown, the compact camera module 500 contains a lens assembly 504 that overlies a base 506. The base 506, in turn, overlies an optional main board 508. Due to their relatively thin nature, the base 506 and/or main board 508 are particularly suited to be formed from the polymer composition of the present invention as described above. The lens assembly 504 may have any of a variety of configurations as is known in the art, and may include fixed focus-type lenses and/or auto focus-type lenses. In one embodiment, for example, the lens assembly 504 is in the form of a hollow barrel that houses lenses 604, which are in communication with an image sensor 602 positioned on the main board 508 and controlled by a circuit 601. The barrel may have any of a variety of shapes, such as rectangular, cylindrical, etc. In certain embodiments, the barrel may also be formed from the polymer composition of the present invention and have a wall thickness within the ranges noted above. It should be

understood that other parts of the camera module may also be formed from the polymer composition of the present invention. For example, as shown, a polymer film 510 (e.g., polyester film) and/or thermal insulating cap 502 may cover the lens assembly 504. In some embodiments, the film 510 and/or cap 502 may also be formed from the polymer composition of the present invention.

**[0060]** Yet other possible electronic components that may employ the polymer composition include, for instance, cellular telephones, laptop computers, small portable computers (e.g., ultraportable computers, netbook computers, and tablet computers), wrist-watch devices, pendant devices, headphone and earpiece devices, media players with wireless communications capabilities, handheld computers (also sometimes called personal digital assistants), remote controllers, global positioning system (GPS) devices, handheld gaming devices, battery covers, speakers, camera modules, integrated circuits (e.g., SIM cards), housings for electronic devices, electrical controls, circuit breakers, switches, power electronics, printer parts, etc.

**[0061]** Regardless of the particular manner in which it is employed, the present inventor has discovered that a molded part formed from the polymer composition of the present invention can have excellent mechanical and thermal properties. As indicated above, this is due in part to the unique ability of the ionic liquid to be uniformly blended and dispersed within the liquid crystalline polymer matrix. The molded part may, for instance, possess a relatively high impact strength (Charpy notched impact strength), such as about 4 kJ/m<sup>2</sup> or more, in some embodiments from about 2 to about 60 kJ/m<sup>2</sup>, in some embodiments, from about 2 to about 40 kJ/m<sup>2</sup>, and in some embodiments, from about 3 to about 30 kJ/m<sup>2</sup>, measured at 23°C according to ISO Test No. 179-1 (technically equivalent to ASTM D256, Method B). The tensile and flexural mechanical properties of the part may also be good. For example, the part may exhibit a tensile strength of from about 20 to about 500 MPa, in some embodiments from about 50 to about 400 MPa, and in some embodiments, from about 80 to about 350 MPa; a tensile break strain of about 0.5% or more, in some embodiments from about 0.6% to about 20%, and in some embodiments, from about 0.8% to about 3.5%; and/or a tensile modulus of from about 5,000 MPa to about 30,000 MPa, in some embodiments from about 8,000 MPa to about 20,000 MPa, and in some

embodiments, from about 10,000 MPa to about 15,000 MPa. The tensile properties may be determined in accordance with ISO Test No. 527 (technically equivalent to ASTM D638) at 23°C. The molded part may also exhibit a flexural strength of from about 20 to about 500 MPa, in some embodiments from about 50 to about 400 MPa, and in some embodiments, from about 100 to about 350 MPa; a flexural break strain of about 0.5% or more, in some embodiments from about 0.6% to about 20%, and in some embodiments, from about 0.8% to about 3.5%; and/or a flexural modulus of from about 5,000 MPa to about 30,000 MPa, in some embodiments from about 8,000 MPa to about 20,000 MPa, and in some embodiments, from about 10,000 MPa to about 15,000 MPa. The flexural properties may be determined in accordance with ISO Test No. 178 (technically equivalent to ASTM D790) at 23°C. The molded part may also exhibit a deflection temperature under load (DTUL) of about 200°C or more, and in some embodiments, from about 200°C to about 280°C, as measured according to ASTM D648-07 (technically equivalent to ISO Test No. 75-2) at a specified load of 1.8 MPa.

**[0062]** The molded part may also possess improved flame resistance performance, even in the absence of conventional flame retardants. The flame resistance of the composition may, for instance, be determined in accordance the procedure of Underwriter's Laboratory Bulletin 94 entitled "Tests for Flammability of Plastic Materials, UL94." Several ratings can be applied based on the time to extinguish (total flame time) and ability to resist dripping as described in more detail below. According to this procedure, for example, a molded part formed from the composition of the present invention may achieve a V0 rating, which means that the part has a total flame time of 50 seconds or less and a total number of drips of burning particles that ignite cotton of 0, determined at a given part thickness (e.g., 0.25 or 0.8 mm). For example, when exposed to an open flame, a molded part formed from the composition of the present invention may exhibit a total flame time of about 50 seconds or less, in some embodiments about 45 seconds or less, and in some embodiments, from about 1 to about 40 seconds. Furthermore, the total number of drips of burning particles produced during the UL94 test may be 3 or less, in some embodiments 2 or less, and in

some embodiments, 1 or less (e.g., 0). Such testing may be performed after conditioning for 48 hours at 23°C and 50% relative humidity.

**[0063]** The present invention may be better understood with reference to the following examples.

#### Test Methods

**[0064]** *Antistatic Test:* To test for antistatic behavior, molded disks/plaques are gently rubbed against paper to create an electrostatic charge on the molded part surface. The parts are then brought near the small pieces of papers. If an electrostatic charge is created on the part surface, an attractive force between the part and the paper is created. Likewise, if there is no electrostatic charge created, no movement for the paper occurs as the part is moved closer to the paper. If there is movement in the paper, it is recorded as “no” and if there is no movement in the paper, then it is recorded as “yes.”

**[0065]** *Surface/Volume Resistivity.* The surface and volume resistivity values are generally determined in accordance with IEC 60093 (similar to ASTM D257-07). According to this procedure, a standard specimen (e.g., 1 meter cube) is placed between two electrodes. A voltage is applied for sixty (60) seconds and the resistance is measured. The surface resistivity is the quotient of the potential gradient (in V/m) and the current per unit of electrode length (in A/m), and generally represents the resistance to leakage current along the surface of an insulating material. Because the four (4) ends of the electrodes define a square, the lengths in the quotient cancel and surface resistivities are reported in ohms, although it is also common to see the more descriptive unit of ohms per square. Volume resistivity is also determined as the ratio of the potential gradient parallel to the current in a material to the current density. In SI units, volume resistivity is numerically equal to the direct-current resistance between opposite faces of a one-meter cube of the material (ohm-m).

**[0066]** *Melt Viscosity:* The melt viscosity (Pa-s) may be determined in accordance with ISO Test No. 11443 at a shear rate of 1000 s<sup>-1</sup> and temperature 15°C above the melting temperature (e.g., 350°C) using a Dynisco LCR7001 capillary rheometer. The rheometer orifice (die) had a diameter of 1 mm, length of 20 mm, L/D ratio of 20.1, and an entrance angle of 180°. The diameter of the barrel was 9.55 mm + 0.005 mm and the length of the rod was 233.4 mm.

**[0067]** *Melting Temperature:* The melting temperature (“Tm”) was determined by differential scanning calorimetry (“DSC”) as is known in the art. The melting temperature is the differential scanning calorimetry (DSC) peak melt temperature as determined by ISO Test No. 11357. Under the DSC procedure, samples were heated and cooled at 20°C per minute as stated in ISO Standard 10350 using DSC measurements conducted on a TA Q2000 Instrument.

**[0068]** *Deflection Temperature Under Load (“DTUL”):* The deflection under load temperature was determined in accordance with ISO Test No. 75-2 (technically equivalent to ASTM D648-07). More particularly, a test strip sample having a length of 80 mm, thickness of 10 mm, and width of 4 mm was subjected to an edgewise three-point bending test in which the specified load (maximum outer fibers stress) was 1.8 Megapascals. The specimen was lowered into a silicone oil bath where the temperature is raised at 2°C per minute until it deflects 0.25 mm (0.32 mm for ISO Test No. 75-2).

**[0069]** *Tensile Modulus, Tensile Stress, and Tensile Elongation:* Tensile properties are tested according to ISO Test No. 527 (technically equivalent to ASTM D638). Modulus and strength measurements are made on the same test strip sample having a length of 80 mm, thickness of 10 mm, and width of 4 mm. The testing temperature is 23°C, and the testing speeds are 1 or 5 mm/min.

**[0070]** *Flexural Modulus, Flexural Stress, and Flexural Strain:* Flexural properties are tested according to ISO Test No. 178 (technically equivalent to ASTM D790). This test is performed on a 64 mm support span. Tests are run on the center portions of uncut ISO 3167 multi-purpose bars. The testing temperature is 23°C and the testing speed is 2 mm/min.

**[0071]** *Notched Charpy Impact Strength:* Notched Charpy properties are tested according to ISO Test No. ISO 179-1 (technically equivalent to ASTM D256, Method B). This test is run using a Type A notch (0.25 mm base radius) and Type 1 specimen size (length of 80 mm, width of 10 mm, and thickness of 4 mm). Specimens are cut from the center of a multi-purpose bar using a single tooth milling machine. The testing temperature is 23°C.

**[0072]** *UL94:* A specimen is supported in a vertical position and a flame is applied to the bottom of the specimen. The flame is applied for ten (10) seconds and then removed until flaming stops, at which time the flame is reapplied for

another ten (10) seconds and then removed. Two (2) sets of five (5) specimens are tested. The sample size is a length of 125 mm, width of 13 mm, and thickness of 0.8 mm. The two sets are conditioned before and after aging. For unaged testing, each thickness is tested after conditioning for 48 hours at 23°C and 50% relative humidity. For aged testing, five (5) samples of each thickness are tested after conditioning for 7 days at 70°C.

Vertical Ratings	Requirements
V-0	Specimens must not burn with flaming combustion for more than 10 seconds after either test flame application.
	Total flaming combustion time must not exceed 50 seconds for each set of 5 specimens.
	Specimens must not burn with flaming or glowing combustion up to the specimen holding clamp.
	Specimens must not drip flaming particles that ignite the cotton.
	No specimen can have glowing combustion remain for longer than 30 seconds after removal of the test flame.
V-1	Specimens must not burn with flaming combustion for more than 30 seconds after either test flame application.
	Total flaming combustion time must not exceed 250 seconds for each set of 5 specimens.
	Specimens must not burn with flaming or glowing combustion up to the specimen holding clamp.
	Specimens must not drip flaming particles that ignite the cotton.
	No specimen can have glowing combustion remain for longer than 60 seconds after removal of the test flame.
V-2	Specimens must not burn with flaming combustion for more than 30 seconds after either test flame application.
	Total flaming combustion time must not exceed 250 seconds for each set of 5 specimens.
	Specimens must not burn with flaming or glowing combustion up to the specimen holding clamp.
	Specimens can drip flaming particles that ignite the cotton.
	No specimen can have glowing combustion remain for longer than 60 seconds after removal of the test flame.

### EXAMPLE 1

**[0073]** Samples 1-6 are formed from various percentages of a liquid crystalline polymer, lubricant (Glycolube™ P), and ionic liquid as indicated in Table 1 below. Compounding is performed using an 18-mm single screw extruder. A comparative sample (Comp. Sample 1) is also formed from the liquid crystalline polymer and the lubricant. The liquid crystalline polymer in each of the samples is formed from HBA, HNA, TA, BP, and APAP, such as described in U.S. Patent No. 5,508,374 to Lee, et al. The ionic liquid is tri-n-butylmethylammonium bis-(trifluoromethanesulfonyl)imide (FC-4400 from 3M).

Parts are injection molded from Sample 1 and Control Sample 1 into plaques (60 mm x 60 mm) and tested for resistivity (surface and volume), antistatic behavior, and thermal properties. The results are set forth below in Table 1.

**Table 1**

	Comp. Sample 1	Sample 1	Sample 2	Sample 3	Sample 4	Sample 5	Sample 6
LCP (wt.%)	99.7	96.7	94.7	99.2	98.7	99.4	99.6
Lubricant (wt.%)	0.3	0.3	0.3	0.3	0.3	0.3	0.3
Ionic Liquid (wt.%)	-	3.0	5.0	0.5	1.0	0.3	0.1
Melt Viscosity at 1000 s <sup>-1</sup> and 350°C (Pa-s)	27.2	35.9	27.3	24.2	23.5	22.9	22.7
Melt Viscosity at 400 s <sup>-1</sup> and 350°C (Pa-s)	35.5	34.4	35.9	32.4	32.4	31.2	32.1
T <sub>m</sub> (°C)	336.8	332.2	331.7	330.8	331.4	333.2	335.5
Surface Resistivity (ohm-m)	4.9 x 10 <sup>16</sup>	1.5 x 10 <sup>12</sup>	1.1 x 10 <sup>12</sup>	1.6 x 10 <sup>13</sup>	1.1 x 10 <sup>12</sup>	1.6 x 10 <sup>15</sup>	1.9 x 10 <sup>16</sup>
Volume Resistivity (ohm-m)	1.1 x 10 <sup>13</sup>	5.1 x 10 <sup>12</sup>	4.5 x 10 <sup>12</sup>	2.9 x 10 <sup>14</sup>	4.90 x 10 <sup>13</sup>	1.6 x 10 <sup>14</sup>	2.3 x 10 <sup>14</sup>
Antistatic Testing	No	Yes	Yes	Yes	Yes	No	No

**[0074]** As indicated, an increased amount of the ionic liquid generally resulted in a decrease in surface resistivity, but without a substantial impact on the physical properties of the composition.

**EXAMPLE 2**

**[0075]** A sample (Sample 7) is formed from a liquid crystalline polymer (as described above), glass fibers, talc, lubricant (Glycolube™ P), ionic liquid, black color masterbatch, aluminum trihydrate (“ATH”), 4,4'-biphenol (“BP”), and 2,6-naphthelene dicarboxylic acid (“NDA”). The black color masterbatch contains 80 wt.% liquid crystalline polymer and 20 wt.% carbon black. The liquid crystalline polymer and ionic liquid are the same as described in Example 1, and the fibers are obtained from Owens Corning and have an initial length of 4 millimeters. Compounding is performed using a 25-mm twin screw extruder. A comparative sample is also formed without any antistatic additive (Comp. Sample 2) and with a carbon fiber masterbatch as an antistatic additive (Comp. Samples 3-6). The carbon fiber masterbatch contains 30 wt.% carbon fibers and 70 wt.% liquid crystalline polymer. Parts are injection molded from Sample 7 and Comparative Samples 2-6 into plaques (60 mm x 60 mm) and tested for resistivity (surface and

volume), antistatic behavior, thermal properties, mechanical properties, and flammability. The results are set forth below in Table 2.

**Table 2**

	Comp. Sample 2	Comp. Sample 3	Comp. Sample 4	Comp. Sample 5	Comp. Sample 6	Sample 7
LCP (wt.%)	50.88	48.89	40.88	35.88	30.88	50.13
Color Masterbatch (wt.%)	12.5	12.5	12.5	12.5	12.5	12.5
Lubricant (wt.%)	0.3	0.3	0.3	0.3	0.3	0.3
Ionic Liquid (wt.%)	-	-	-	-	-	0.75
Carbon Fiber Masterbatch (wt.%)	-	2.0	10.0	15.0	20.0	-
Glass Fibers (wt.%)	18.0	18.0	18.0	18.0	18.0	18.0
Talc (wt.%)	18.0	18.0	18.0	18.0	18.0	18.0
ATH (wt.%)	0.2	0.2	0.2	0.2	0.2	0.2
BP (wt.%)	0.1	0.1	0.1	0.1	0.1	0.1
NDA (wt.%)	0.025	0.025	0.025	0.025	0.025	0.025
Melt Viscosity at 1000 s <sup>-1</sup> and 350°C (Pa-s)	12.4	13.0	15.0	11.0	12.0	10.0
Melt Viscosity at 400 s <sup>-1</sup> and 350°C (Pa-s)	18.6	17.5	21.8	18.0	19.4	15.1
T <sub>m</sub> (°C)	333.7	333.0	332.0	338.6	329.5	330.5
Surface Resistivity (ohm-m)	7.7 x 10 <sup>16</sup>	1.4 x 10 <sup>16</sup>	1.3 x 10 <sup>16</sup>	-	-	3.4 x 10 <sup>13</sup>
Volume Resistivity (ohm-m)	1.1 x 10 <sup>14</sup>	3.2 x 10 <sup>14</sup>	1.7 x 10 <sup>14</sup>	-	-	2.5 x 10 <sup>14</sup>
Antistatic Testing	Yes	No	No	No	No	Yes
DTUL @ 1.8 Mpa (°C)	240.2	241.0	241.0	225.0	220.0	236.8
Ten. Brk stress (MPa)	105.9	102.0	114.0	95.0	76.0	91.1
Ten. Modulus (MPa)	12,053	12,745	14,561	13,956	14,457	11,425
Ten. Brk strain (%)	1.76	1.44	1.54	1.17	0.69	1.34
Flex Brk stress (MPa)	140.8	148.0	155.0	134.0	129.0	123.9
Flex modulus (MPa)	12,353	12,768	14,277	14,272	15,230	11,787
Flex Brk strain (%)	1.93	1.92	1.76	1.39	1.12	1.62
Charpy Notched (KJ/m <sup>2</sup> )	5.5	4.3	4.3	2.9	2.3	3.7
UL94 Rating (before aging)	V-0	V-0	V-0	V-0	V-0	V-0
UL94 Rating (after aging)	V-0	V-0	V-0	V-0	V-0	V-0

**[0076]** As indicated, no antistatic effect was observed for the Comparative Samples containing only carbon fiber as an antistatic additive.

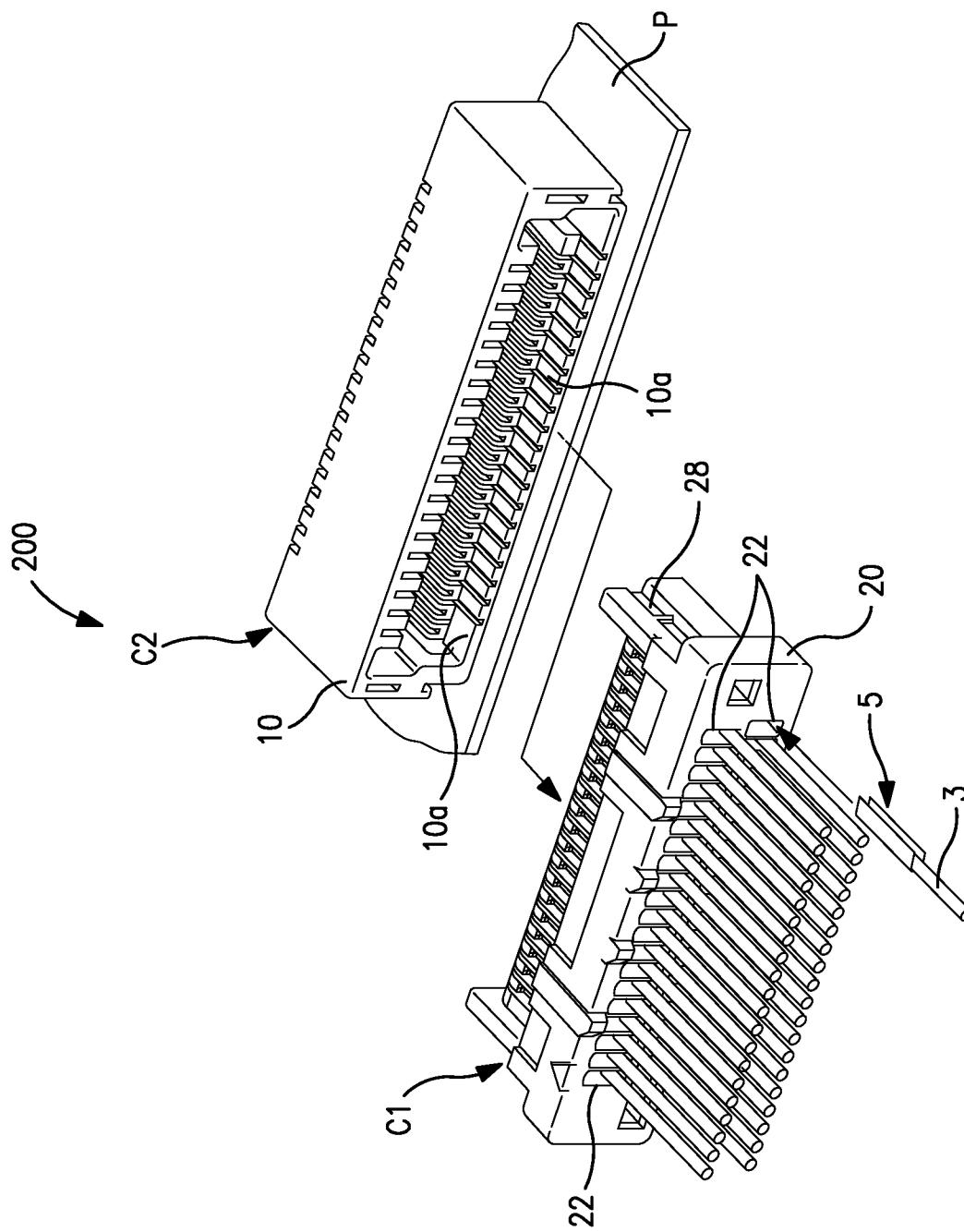
**[0077]** These and other modifications and variations of the present invention may be practiced by those of ordinary skill in the art, without departing from the spirit and scope of the present invention. In addition, it should be understood that aspects of the various embodiments may be interchanged both in whole or in part.

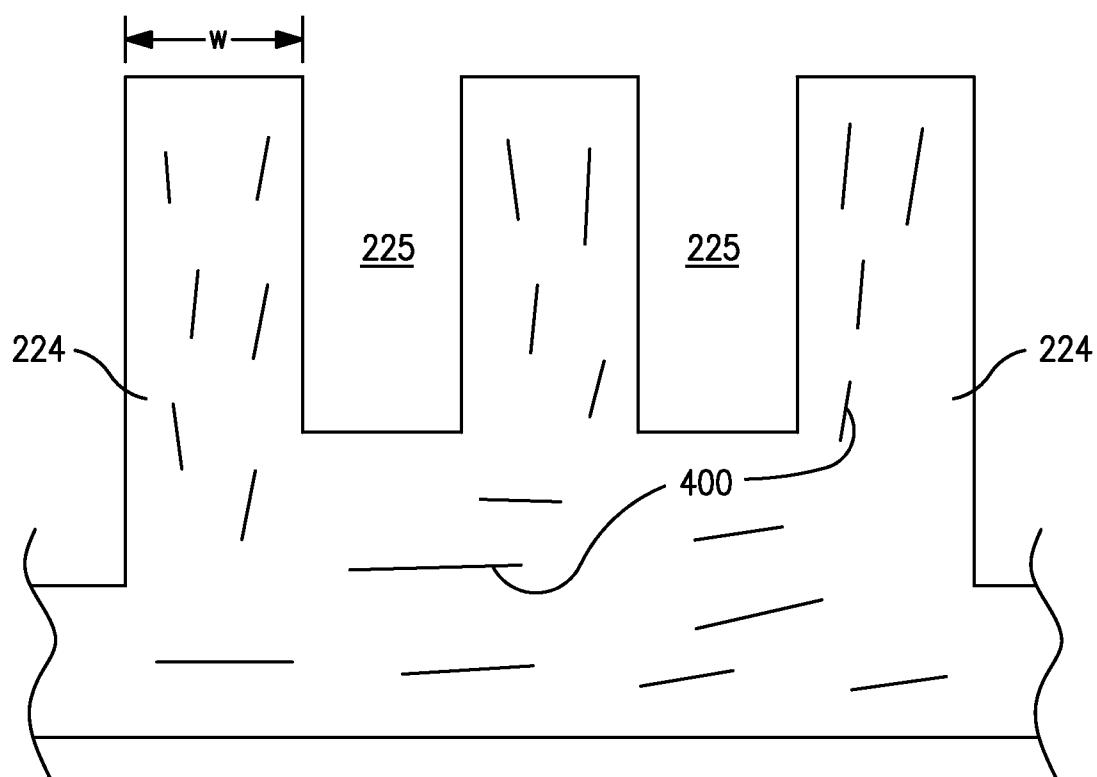
Furthermore, those of ordinary skill in the art will appreciate that the foregoing description is by way of example only, and is not intended to limit the invention so further described in such appended claims.

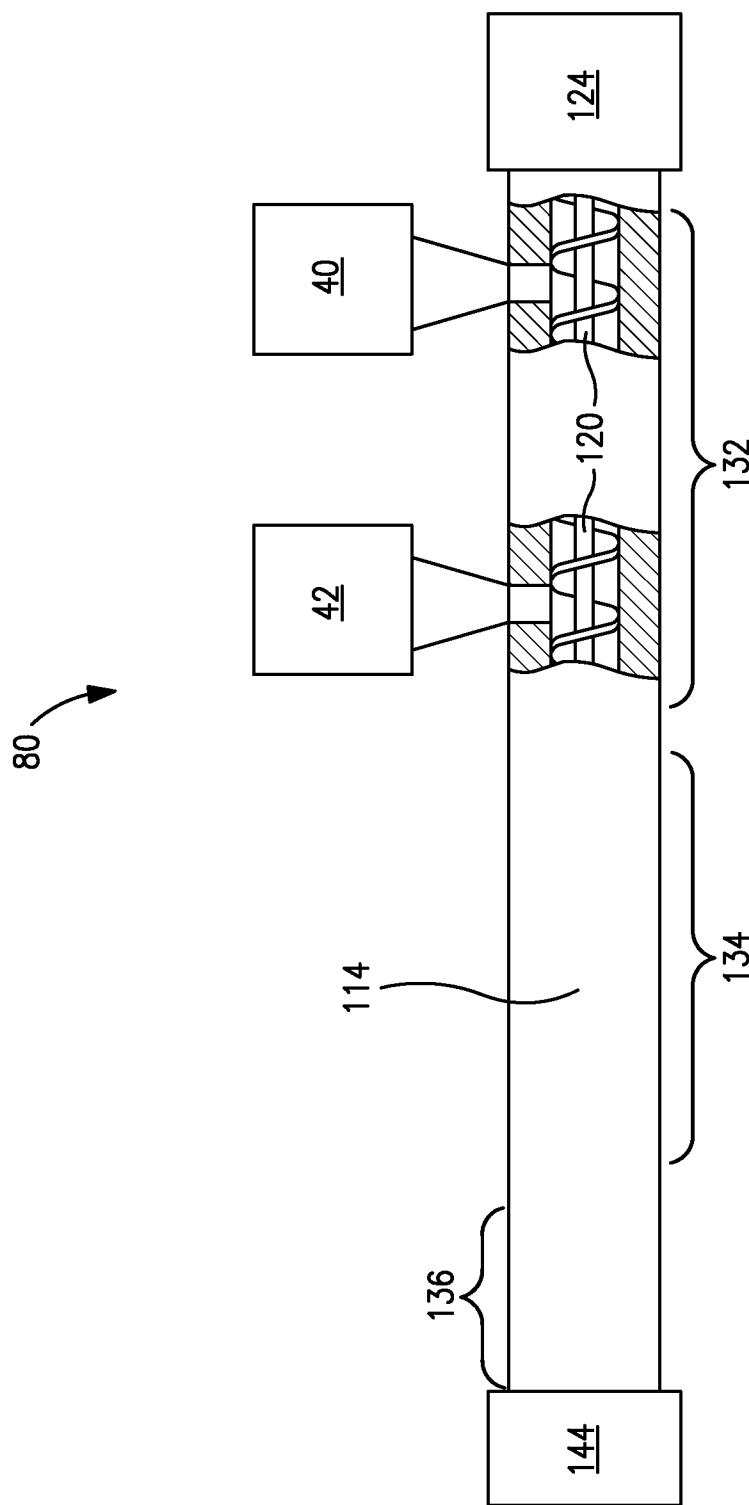
**WHAT IS CLAIMED IS:**

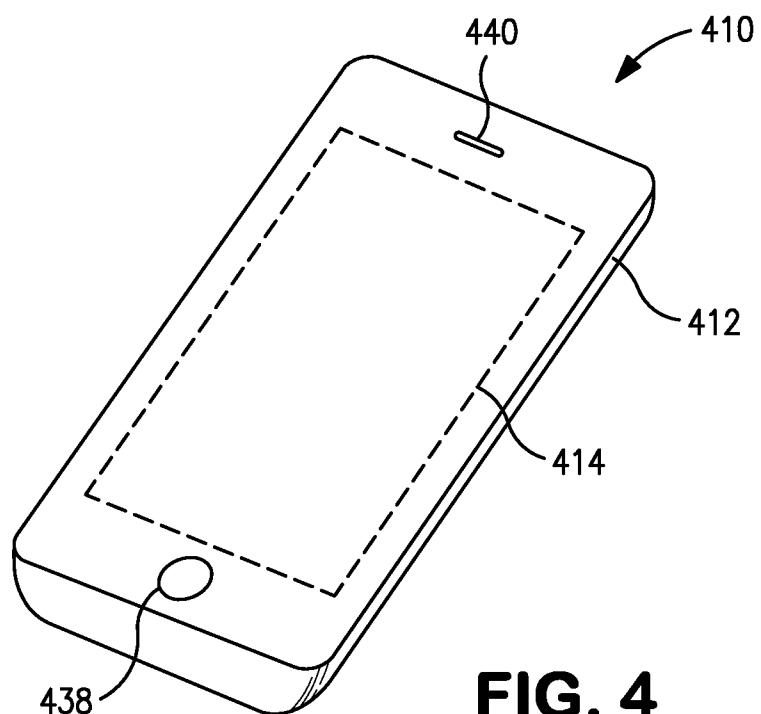
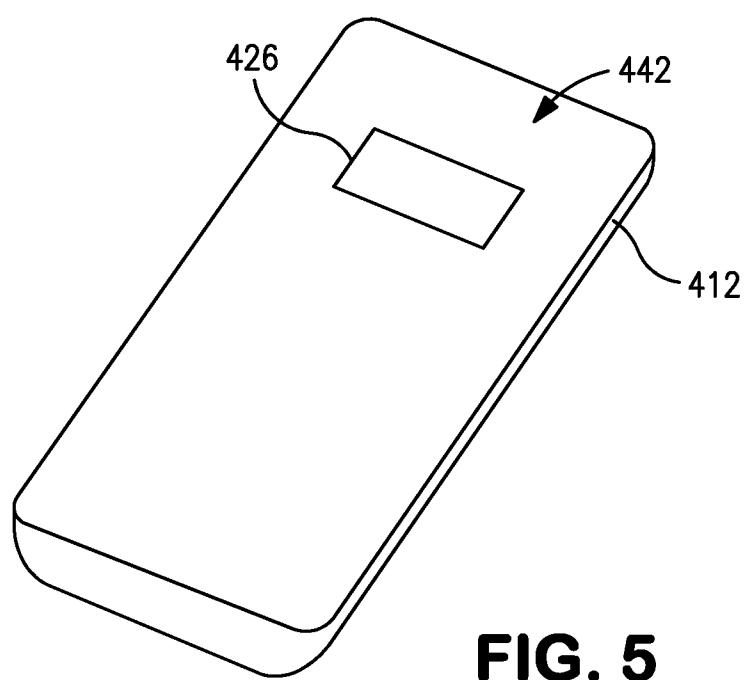
1. A polymer composition that comprises an ionic liquid that is distributed within a liquid crystalline polymer matrix, wherein the ionic liquid has a melting temperature of about 400°C or less and is a salt that contains a cationic species and counterion.
2. The polymer composition of claim 1, wherein ionic liquids constitute from about 0.1 wt.% to about 10 wt.% of the composition.
3. The polymer composition of claim 1 or 2, wherein liquid crystalline polymers constitute from about 25 wt.% to about 95 wt.% of the composition.
4. The polymer composition of any of the foregoing claims, wherein the liquid crystalline polymer matrix is formed from a polymer that contains aromatic dicarboxylic acid repeating units, aromatic hydroxycarboxylic acid repeating units, aromatic diol repeating units, or a combination thereof.
5. The polymer composition of any of the foregoing claims, wherein the cationic species is a quaternary onium.
6. The polymer composition of claim 5, wherein the quaternary onium is an ammonium compound having the structure  $N^+R^1R^2R^3R^4$ , wherein  $R^1$ ,  $R^2$ , and/or  $R^3$  are independently a C<sub>1</sub>-C<sub>6</sub> alkyl and  $R^4$  is hydrogen or a C<sub>1</sub>-C<sub>4</sub> alkyl group.
7. The polymer composition of claim 6, wherein the ammonium compound is tri-butylmethylammonium.
8. The polymer composition of any of the foregoing claims, wherein the counterion is a halogen, sulfate, sulfonate, sulfosuccinate, amide, imide, borate, phosphate, phosphinate, antimonate, aluminate, fatty acid carboxylate, cyanate, acetate, or a combination thereof.
9. The polymer composition of claim 8, wherein the imide is bis(pentafluoroethylsulfonyl)imide, bis(trifluoromethylsulfonyl)imide, or bis(trifluoromethyl)imide.
10. The polymer composition of any of the foregoing claims, further comprising carbon fibers, graphite, carbon black, or a combination thereof.
11. The polymer composition of any of the foregoing claims, further comprising mineral fibers.
12. The polymer composition of claim 11, wherein the mineral fibers include wollastonite fibers.

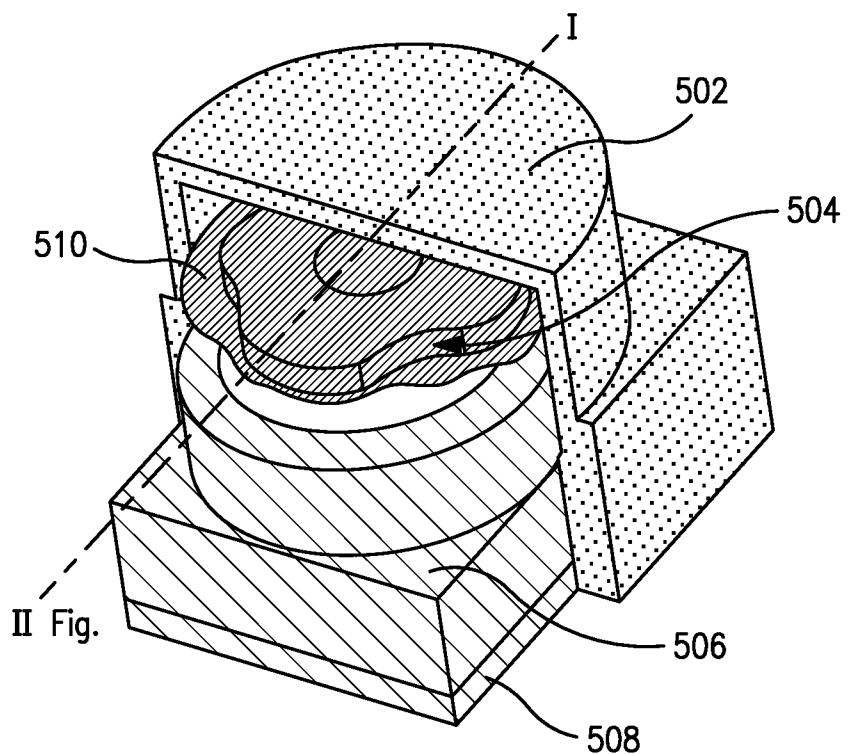
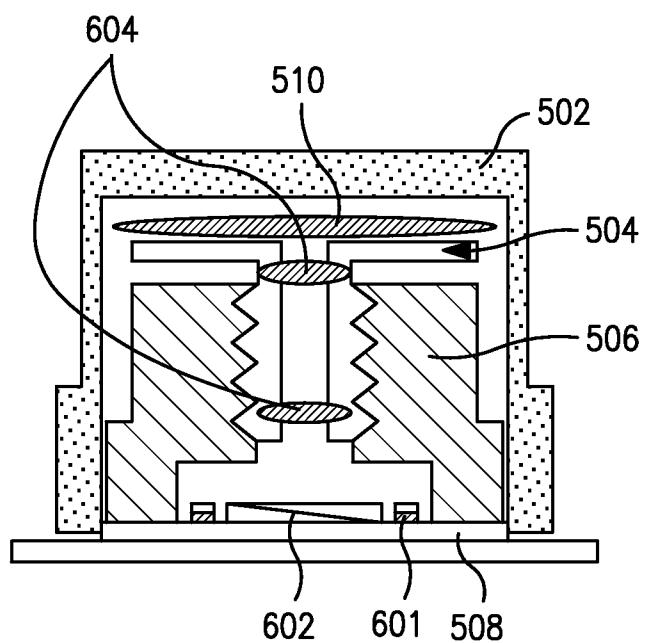
13. The polymer composition of claim 11 or 12, wherein the mineral fibers have a volume average length of from about 1 to about 200 micrometers and a nominal diameter of from about 1 to about 35 micrometers.
14. The polymer composition of any of the foregoing claims, further comprising a functional aromatic compound.
15. The polymer composition of any of the foregoing claims, further comprising a non-aromatic functional compound that includes a hydrate.
16. The polymer composition of any of the foregoing claims, wherein the composition has a melt viscosity of from about 0.1 to about 80 Pa-s, as determined in accordance with ISO Test No. 11443 at a shear rate of 1000  $\text{seconds}^{-1}$  and temperature that is 15°C above the melting temperature of the composition.
17. A molded part that comprises a polymer composition, wherein the polymer composition comprises an ionic liquid distributed within a liquid crystalline polymer matrix, and wherein the part exhibits a surface resistivity of about  $1 \times 10^{15}$  ohms or less as determined in accordance with IEC 60093.
18. The molded part of claim 17, wherein the part exhibits a surface resistivity of from  $1 \times 10^{11}$  to about  $1 \times 10^{13}$  ohms and/or a volume resistivity of about  $1 \times 10^{15}$  ohm-m or less as determined in accordance with IEC 60093.
19. A compact camera module that comprises a generally planar base on which is mounted a lens barrel, wherein the base, barrel, or both have a thickness of about 500 micrometers or less and are formed from a part that contains a polymer composition comprising a liquid crystalline polymer matrix, wherein the part exhibits a surface resistivity of about  $1 \times 10^{15}$  ohms or less as determined in accordance with IEC 60093.
20. The compact camera module of claim 19, wherein an ionic liquid is distributed within the liquid crystalline polymer matrix.



**FIG. 2**

**FIG. 3**

**FIG. 4****FIG. 5**

**FIG. 6****FIG. 7**

# INTERNATIONAL SEARCH REPORT

International application No  
PCT/US2013/064760

A. CLASSIFICATION OF SUBJECT MATTER			
INV.	C09K19/38	C09K19/54	C09K19/58
ADD.	C08J5/10	C08G63/00	C08K5/00

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
C09K C08J C08G C08K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 2006/126861 A1 (BUSAN NAT UNIVERSITY INDUSTRY [KR]; JIN SUNG HO [KR]; LEE JIN KOOK [KR] 30 November 2006 (2006-11-30) paragraph [0001]; examples 4-7 -----	1-16
A	US 2012/235089 A1 (NAKAYAMA TOSHIRO [JP] ET AL) 20 September 2012 (2012-09-20) claims; paragraph [0001] -----	1-20
A	US 2007/219301 A1 (YAMAUCHI HIROYASU [JP] ET AL) 20 September 2007 (2007-09-20) examples; claims; paragraph [0055] -----	1-20
A	US 2008/029735 A1 (GIN DOUGLAS L [US] ET AL) 7 February 2008 (2008-02-07) examples; claims ----- -/-	1-20

Further documents are listed in the continuation of Box C.

See patent family annex.

### \* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier application or patent but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
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Date of the actual completion of the international search	Date of mailing of the international search report
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Name and mailing address of the ISA/  
European Patent Office, P.B. 5818 Patentlaan 2  
NL - 2280 HV Rijswijk  
Tel. (+31-70) 340-2040,  
Fax: (+31-70) 340-3016

Authorized officer

Schoenhentz, Jérôme

## INTERNATIONAL SEARCH REPORT

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