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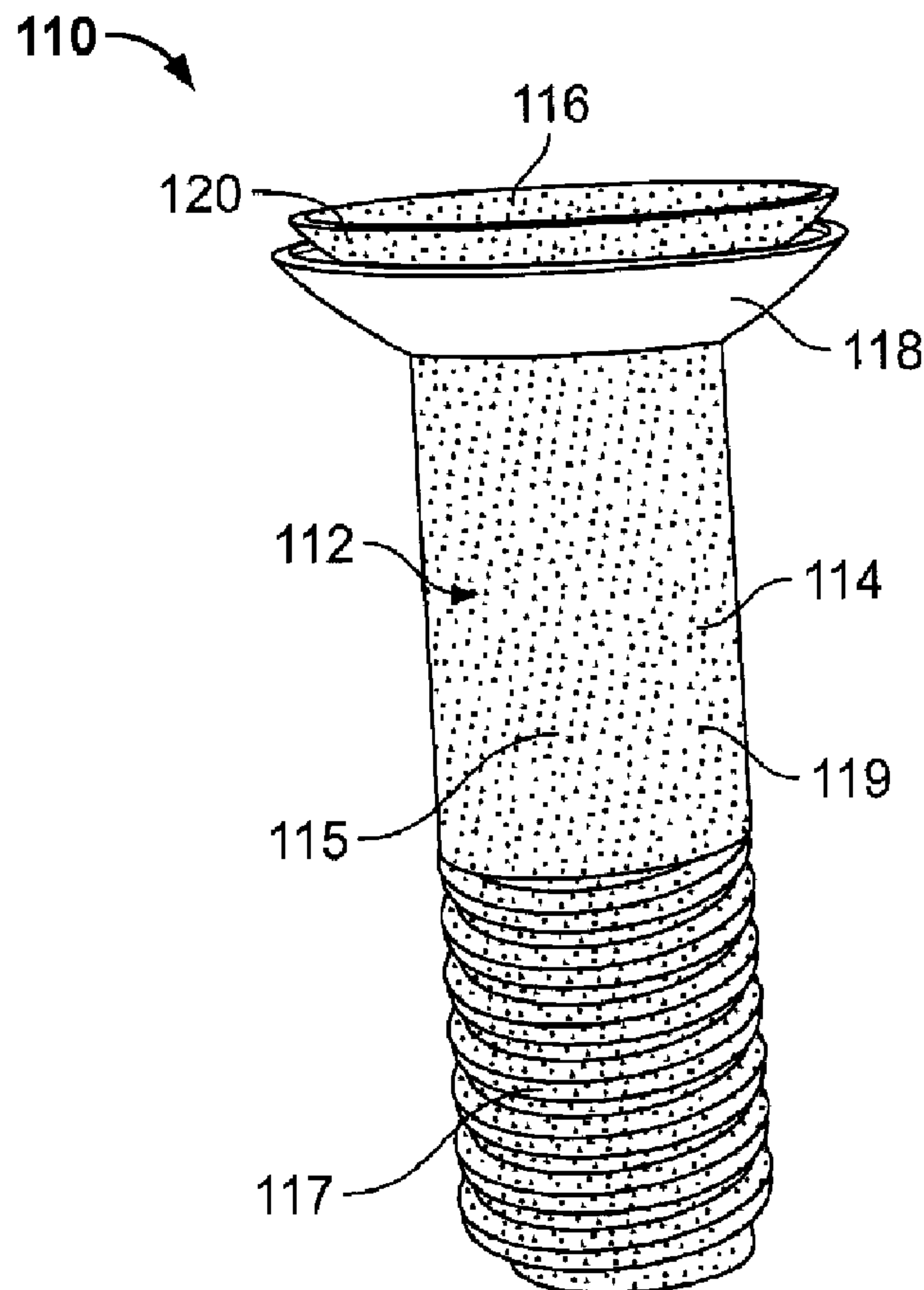
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(54) **Titre : FIXATIONS REVETUES DOTEES DE JOINTS D'ETANCHEITES CONFORMANT**

(54) **Title: COATED FASTENERS WITH CONFORMING SEALS**



(57) **Abrégé/Abstract:**

A pin member for a fastener includes an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface

(57) Abrégé(suite)/Abstract(continued):

located on the bearing surface of the head, and a threaded portion located at the second end of the elongated shank. The pin member can be fully coated with a coating. A conformable seal element is attached to the pin member, which is adapted to fill the microscopic voids between the bearing surface of the head of the pin member and the surrounding structure under the axial load exerted by the fastener during installation. The seal element can be separate and distinct from the pin member. The seal element can be attached to the pin member for the sake of convenience, but the seal element can deform independently of the pin member and the surrounding structure in response to the forces exerted by the fastener.

Abstract

A pin member for a fastener includes an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface located on the bearing surface of the head, and a threaded portion located at the second end of the elongated shank. The pin member can be fully coated with a coating. A conformable seal element is attached to the pin member, which is adapted to fill the microscopic voids between the bearing surface of the head of the pin member and the surrounding structure under the axial load exerted by the fastener during installation. The seal element can be separate and distinct from the pin member. The seal element can be attached to the pin member for the sake of convenience, but the seal element can deform independently of the pin member and the surrounding structure in response to the forces exerted by the fastener.

COATED FASTENERS WITH CONFORMING SEALS

Cross-Reference to Related Applications

This application relates to and claims the benefit of commonly-owned, co-
5 pending U.S. Application Serial No. 15/059,608 entitled "FASTENERS WITH
CONFORMING SEALS," filed March 3, 2016, which claims the benefit of co-pending
U.S. Application Serial No. 14/854,223 entitled "FASTENERS WITH COATED AND
TEXTURED PIN MEMBERS," filed September 15, 2015, which claims the benefit of
commonly-owned, co-pending U.S. Provisional Patent Application Serial No.
10 62/051,602, entitled "FASTENERS WITH COATED AND TEXTURED PIN MEMBERS,"
filed September 17, 2014, the entireties of which are incorporated herein by reference.
The present application also claims the benefit of commonly-owned, co-pending U.S.
Provisional Patent Application Serial No. 62/211,250 entitled "CONFORMING CONICAL
SEAL FOR FASTENERS," filed August 28, 2015, the entirety of which is incorporated
15 herein by reference.

Technical Field of the Invention

The present invention relates to fasteners and, more particularly, to fasteners
having coated pin members and conforming conical seals.

20

Background of the Prior Art

Continuous fiber reinforced composites are extensively used in both primary and
secondary aircraft components for a variety of applications where light weight, higher

strength and corrosion resistance are primary concerns. Composites are typically composed of fine carbon fibers that are oriented at certain directions and surrounded in a supportive polymer matrix. Since the plies of the composite material are arranged at a variety of angles, and depending upon the direction of major loading, the resultant structure is typically a stacked laminated structure, which is highly anisotropic and heterogeneous. A significant portion of the composite structure is fabricated as near net-shape, but is drilled in order to facilitate joining of components using mechanical fasteners. Drilling fastener holes in composite does not compare to the uniformity of aluminum or steel since individual carbon fibers fracture at irregular angles and form microscopic voids between the fastener and the hole. As the cutting tool wears down, there is an increase of surface chipping and an increase in the amount of uncut fibers or resin and delamination. The composite microstructure containing such defects is referred to as “machining–induced micro texture.”

In addition to their machining challenges, composite structures in aircrafts are more susceptible to lightning damage compared to metallic structures. Metallic materials, such as aluminum, are very conductive and are able to dissipate the high currents resulting from a lightning strike. Carbon fibers are 100 times more resistive than aluminum to the flow of current. Similarly epoxy, which is often used as a matrix in conjunction with carbon fibers, is 1 million times more resistive than aluminum. The composite structural sections of an aircraft often behave like anisotropic electrical conductors. Consequently, lightning protection of a composite structure is more complex, due to the intrinsic high resistance of carbon fibers and epoxy, the multi-layer construction, and the anisotropic nature of the structure. Some estimates indicate that,

on average, each commercial aircraft in service is struck by lightning at least once per year. Aircraft flying in and around thunderstorms are often subjected to direct lightning strikes as well as to nearby lightning strikes, which may produce corona and streamer formations on the aircraft. In such cases, the lightning discharge typically originates at
5 the aircraft and extends outward from the aircraft. While the discharge is occurring, the point of attachment moves from the nose of the aircraft and into the various panels that compromise the skin of the aircraft. The discharge usually leaves the aircraft structure through the empennage.

The protection of aircraft fuel systems against fuel vapor ignition due to lightning
10 is even more critical. Since commercial aircraft contain relatively large amounts of fuel and also include very sensitive electronic equipment, they are required to comply with a specific set of requirements related to the lightning strike protection in order to be certified for operation. It is a well-known fact that fasteners are often the primary pathways for the conduction of the lightning currents from skin of the aircraft to
15 supporting structures such as spars or ribs, and poor electrical contact between the fastener body and the parts of the structure can lead to detrimental fastener arcing or sparking.

To avoid the potential for ignition at the fastener/composite structure interface, some aircraft use fasteners which are in intimate contact with the fastener hole.
20 Intimate contact between bare metallic fasteners and the hole in the composite structure has been known to be the best condition for electrical current dissipation. One approach to achieve fastener-to-composite hole intimacy is to use a sleeved fastener. This approach involves first inserting a close fitting sleeve in the hole. An interference-

fit pin is then pulled into the sleeve. This expands the sleeve to bring it in contact with the wall of the hole in the composite structure. Although the sleeve substantially reduces the gap between the fastener and composite structure, it cannot eliminate the small gaps created due to the presence of drilling induced texture across the composite inner-hole surface. This machining induced texture also entraps excess sealant, an insulating material, inhibiting the intimate contact between the sleeve and the hole. This situation becomes even worse as the cutting tool wears, resulting in more and larger machining induced defects.

In order to avoid this condition, the current must dissipate through the carbon fibers exposed along the inner surface of the fastener hole. If the fastener is not in intimate contact with the inside of the hole, the instantaneous joule energy driven by the lightning strike leads to plasma formation within the gap that leads to air/metal vapor ionization which leads to pressure buildup that blows out in the form of a spark or hot particle ejection. The intrinsic high conductivity of metallic fasteners and the large number of fasteners used in aircraft construction combine to create a condition of a high probability of lightning attachment to fasteners.

Disclosure of the Invention

In an embodiment, a fastener comprising a pin member including an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface located on the underside of the head, and a threaded portion located at the second end of the elongated shank; and a seal element attached

to the pin member and juxtaposed with the bearing surface of the head of the pin member. In an embodiment, the seal element is made of copper. In an embodiment, the seal element includes a sealing portion having a first side and a second side opposite the first side, a lip extending from the first side of the sealing portion. In an
5 embodiment, the lip extends angularly from the sealing portion. In an embodiment, the seal element includes a tubular portion extending axially from the side of the sealing portion. In an embodiment, the seal element includes a thickness in a range of about 5 microns to about 100 microns. In an embodiment, the pin member includes a coating. In an embodiment, the coating is a metallic coating. In an embodiment, the metallic
10 coating is selected from the group consisting of gold, silver, and copper. In an embodiment, the coating is made from a material having an electrical conductivity higher than 20% IACS.

In an embodiment, the head of the pin member is coated with the coating. In an embodiment, the outer surface of the cylindrical shank portion of the pin member is
15 coated with the coating. In an embodiment, the head of the pin member and the cylindrical shank portion of the pin member are coated with the coating. In an embodiment, the threaded portion of the pin member and the cylindrical shank portion of the pin member are coated with the coating. In an embodiment, the pin member is fully coated with the coating.

20 In an embodiment, in combination, a structure; and a fastener installed within the structure, the fastener including a pin member having an elongated shank with a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a

bearing surface located on the underside of the head, and a threaded portion located at the second end of the elongated shank, and a seal element attached to the pin member and juxtaposed with the bearing surface of the head of the pin member. In an embodiment, the structure includes a composite material. In an embodiment, the structure is substantially made from the composite material. In an embodiment, the structure is partially made from the composite material. In an embodiment, the structure includes a metallic material. In an embodiment, the metallic material is aluminum. In an embodiment, the structure is made substantially from the metallic material. In an embodiment, the structure is made partially from the metallic material.

In an embodiment, a method of making a fastener, comprising the steps of: providing a pin member including an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface located on the underside of the head, and a threaded portion located at the second end of the elongated shank; and attaching a seal element to the pin member in a position that is juxtaposed with the bearing surface of the head of the pin member. In an embodiment, the method includes the step of coating at least a portion of the pin member with a coating. In an embodiment, the coating is a metallic coating. In an embodiment, the metallic coating is selected from the group consisting of gold, silver, and copper. In an embodiment, the coating is made from a material having an electrical conductivity higher than 20% IACS. In an embodiment, the coating step includes coating the head of the pin member with the coating. In an embodiment, the coating step includes coating the outer surface of the cylindrical shank portion with the coating.

In an embodiment, the coating step includes coating the head of the pin member and the cylindrical shank portion with the coating. In an embodiment, the coating step includes coating the threaded portion and the cylindrical shank portion of the pin member with the coating. In an embodiment, the coating step includes coating the pin member fully with the coating.

In an embodiment, a method of installing a fastener into a structure, comprising the steps of: providing a fastener having a pin member including an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface located on the underside of the head, and a threaded portion located at the second end of the elongated shank and a seal element adapted to be positioned on the pin member such that the seal member is juxtaposed with the bearing surface of the head of the pin member; and installing the fastener into the structure in an installed position. In an embodiment, the method includes the step of coating at least a portion of the pin member with a coating. In an embodiment, the coating is a metallic coating. In an embodiment, the metallic coating is selected from the group consisting of gold, silver, and copper. In an embodiment, the coating is made from a material having an electrical conductivity higher than 20% IACS. In an embodiment, the coating step includes coating the head of the pin member with the coating. In an embodiment, the coating step includes coating the outer surface of the cylindrical shank portion with the coating. In an embodiment, the coating step includes coating the head and the cylindrical shank portion of the pin member with the coating. In an embodiment, the coating step includes coating the cylindrical shank portion and

the threaded portion of the pin member with the coating. In an embodiment, the coating step includes coating the pin member fully with the coating. In an embodiment, the structure includes a composite material. In an embodiment, the structure is substantially made from the composite material. In an embodiment, the structure is partially made from the composite material. In an embodiment, the structure includes a metallic material. In an embodiment, the metallic material is aluminum. In an embodiment, the structure is made substantially from the metallic material. In an embodiment, the structure is made partially from the metallic material. In an embodiment, the method further comprises the step of trimming the seal element flush with the structure. In an embodiment, the trimming step includes sanding the seal element. In an embodiment, the method further comprises the step of providing a metallic mesh on an outer surface of the structure, wherein when the fastener is in its installed position, the sealing element of the fastener is in direct physical and electrical contact with the metallic mesh. In an embodiment, the seal element includes a sealing portion having a first side and a second side opposite the first side, a lip extending from the first side of the sealing portion, the lip being in direct physical and electrical contact with the metallic mesh. In an embodiment, the metallic mesh is made from copper.

Brief Description of the Drawings

FIG. 1 is a side elevational view of an embodiment of a pin member having selected surfaces coated with a material;

FIG. 2 is a bottom perspective view of an embodiment of a seal;

FIG. 3 is a bottom perspective view of the pin member and the seal shown in **FIGS. 1** and **2**, respectively, assembled together;

FIG. 4 is a photograph of an embodiment of an outer surface of the coated pin member shown in **FIG. 1**;

5 **FIG. 5** is a photograph of the topography of an outer surface of an embodiment of the coated pin member shown in **FIG. 1**;

FIGS. 6 and **7** are photographs of an embodiment of a pin member having a textured surface;

10 **FIG. 8** is a side elevational view of an embodiment of a pin member having a conforming seal element;

FIGS. 9A and **9B** are top plan and side views, respectively, of an embodiment of a conforming seal element;

FIG. 10 illustrates a screenshot of a stress distribution analysis of an installed fastener;

15 **FIG. 11** is a micro-photograph of the cross-section of a standard fastener installed in a structure;

FIG. 12A is a micro-photograph that illustrates a standard fastener installed in a structure, while **FIG. 12B** is a micro-photograph that illustrates the pin member and the seal element shown in **FIG 8** installed in a structure;

20 **FIGS. 13A** and **13B** depict photographs showing pre-sanding and post-sanding steps of a structure containing a fastener of **FIG. 8** installed therein;

FIGS. 14A and **14B** are schematic illustrations of the fastener of **FIG. 8** before and after a sanding step, respectively;

FIG. 15A is a micro-photograph of a standard fastener installed in a structure with an associated copper mesh, while **FIG. 15B** is a micro-photograph of a fastener shown in **FIG 8** installed in a structure with an associated copper mesh;

FIG. 15C is graph and associated photographs corresponding to specific data points on the graph showing flushness tolerance between the fastener shown in **FIG. 8** and a standard fastener;

FIGS. 16A and **16B** are micro-photographs of a conventional fastener installed in a structure (40 times and 600 times magnification, respectively), while **FIGS. 16C** and **16D** are micro-photographs of a fastener as shown in **FIG. 8** installed in a structure (25 times and 1000 times magnification, respectively);

FIG. 17A is a photograph showing the effects of lightning damage on a standard fastener installed in a structure, while **FIG 17B** is a photograph showing the effects of lightning damage on a fastener as shown in **FIG. 8** installed in a structure;

FIG. 17C is a micro-photograph showing the effects of lightning damage on a standard fastener installed in a structure, while **FIG 17D** is a micro-photograph showing the effects of lightning damage on a fastener as shown in **FIG. 8** installed in a structure;

FIG. 18A through **18F** illustrate a series of simulation results showing reduction of contact resistance and optimized electrical intimacy of the fastener of **FIG.8**; and

FIG. 19 is a graph showing electric contact resistivity versus preload force between the fastener shown in **FIG. 8**, a fastener with a coated pin member, and an anodized fastener.

Best Mode For Carrying Out The Invention

Referring to **FIG. 1**, in an embodiment, a pin member **12** includes an elongated shank **14** having a cylindrical shank portion **16**, a head **18** at one end of the cylindrical shank portion **16** and a threaded portion **20** at an opposite end of the cylindrical shank portion **16**. In an embodiment, the head **18** is a countersunk head. In an embodiment, the outer surfaces of the head **18**, including an underside surface (e.g., bearing surface) **21** of the head **18**, and the cylindrical shank portion **16** are coated with coating **22**. In an embodiment, the coating **22** is tungsten. In another embodiment, the coating **22** is molybdenum. In another embodiment, the coating **22** is a refractory metal, such as tantalum or niobium. In another embodiment, the coating **22** is a refractory ceramic, such as alumina (Al_2O_3), silica (SiO_2) or other metal oxides. In another embodiment, only the outer surfaces of the head **18** are coated with the coating **22**. In another embodiment, only the outer surface of the cylindrical shank portion **16** is coated with the coating **22**. In an embodiment, the coating **22** lowers electrical contact resistance and reduces probability of arc initiation/damage. In an embodiment, the coating **22** includes a high electrical conductivity (higher than 20% IACS) and be galvanically compatible to a structure (e.g., anodic index less than 1.0V) for corrosion resistance. In an embodiment, the structure includes a composite structure. In another embodiment, the structure includes a metal structure. In another embodiment, the structure includes a fiber metal laminate structure.

In an embodiment, the coating **22** is a thin film coating having a thickness in a range of about one (1) nanometer to about two-hundred (200) microns. In an embodiment, the coating **22** is applied by physical vapor deposition. In another

embodiment, the coating **22** is applied by chemical vapor deposition. In another embodiment, the coating **22** is applied by a selective additive process. In another embodiment, the coating **22** is applied by electroplating. In another embodiment, the coating **22** is applied by a spraying process. In another embodiment, the coating **22** is applied by cold spraying. In another embodiment, the coating **22** is applied by thermal spraying. In another embodiment, the coating **22** is applied by plasma coating. In another embodiment, the coating **22** is applied by a sputter deposition process.

In another embodiment, the outer surfaces of the head **18** and the cylindrical shank portion **16** are textured. In an embodiment, the outer surfaces of the head **18** and the cylindrical shank portion **16** of the pin member **12** are textured to conform to the machine-induced micro texture inherent in fastener holes drilled in composite structures, and to provide mechanical interlocking between the pin member **12** and the composite structure. In an embodiment, the textured pin member **12** excavates excess entrapped sealant during installation of the fastener while bringing the fastener in intimate contact with the structure, and, thus, lowering the electrical contact resistance at the interface. The term "intimate contact" as used herein means that the textured outer surface of the pin member **12** is deformed into all or substantially all of voids between the pin member and the composite structure. In another embodiment, only the outer surfaces of the head **18** are textured. In another embodiment, only the outer surface of the cylindrical shank portion **16** is textured.

In an embodiment, the textured surfaces of the pin member **12** are created by surface reshaping processes, such as media blasting. In an embodiment, the textured surfaces of the pin member **12** are grit blasted. In an embodiment, the grit blasting

utilizes fine grit glass bead media (100-170 mesh). In an embodiment, the grit blasting is performed until there is full coverage of the outer surfaces of the pin member **12** to be textured. In an embodiment, the grit blasting is performed for at least one minute. In another embodiment, the grit blasting is performed for about one minute. In an
5 embodiment, the grit blasting step is performed twice. In another embodiment, the textured surfaces of the pin member **12** are created by removal processes, such as selective electro-etching, laser etching, abrasive blasting, and mechanical polishing. In another embodiment, the textured surfaces of the pin member **12** are created by chemical etching. In an embodiment, the chemical etching utilizes 50/50 hydrochloric
10 acid (HCl). In an embodiment, the chemical etching is performed for about 30 minutes. In an embodiment, the pin member **12** is rinsed with distilled water for about 15-20 seconds, and dried with forced, room-temperature air for approximately 1 to 2 minutes.

In another embodiment, the surfaces of the head **18** and the cylindrical shank portion **16** of the pin member **12** are coated and textured by a combination of a coating
15 process and a texturing process as described above. In an embodiment, a combination of the coating and texturing processes can be used to develop functional characteristics of the pin member **12**, based on a specific loading pattern thereof. For example, in an embodiment, where the preload is high, the texturing/coating is performed to lower contact resistance. At locations which carry no preload and are not in intimate contact
20 with the composite layer, mitigation of plasma generation and arc formation/damage is desired.

In an embodiment, the pin member **12** is part of a fastener that is adapted to secure a plurality of work pieces of to one another, and is adapted to be installed within

aligned holes in such work pieces. In an embodiment, the work pieces are made of a composite material. In another embodiment, the work pieces are made of metal. In another embodiment, the work pieces are made from a fiber metal laminate. In an embodiment, the fastener includes a locking member (not shown in the Figures). In an embodiment, the locking member is a nut. In another embodiment, the locking member is a collar. In an embodiment, a fastener **10** includes the pin member **12** and a seal **24** installed on the bearing surface **21** of the head **18** of the pin member **12**, as shown in **FIGS. 2** and **3**, and to be discussed in further detail below.

During a lightning strike on an aircraft, the lightning typically attaches to the head **18** of the pin member **12** first. In an embodiment, the coated and/or textured pin member **12** improves contact resistance. In this regard, all solid surfaces are rough on a micro-scale and contact between two engineering bodies occurs at discrete spots produced by the mechanical contact of asperities on the two surfaces. For all solid materials, the true area of contact is a small fraction of the apparent contact area. Electrical current lines get increasingly distorted as the contact spot is approached and flow lines bundle together to pass through “a-spots”. An electrical junction consists of a number of contact “a-spots” through which electrical current passes from one connector component to the other and is often characterized by electrical contact resistance of the interface.

When a fastener is installed in a composite structure using a clearance fit, the primary load bearing surface of the pin member **12** as installed is the bearing surface **21** of the head **18**. This is an electrical contact through which it is desired to pass a high frequency, high voltage current and is a significant first line of defense to the lightning

strike. If the current has a path to flow easily, no arcing and resultant damage would occur. The pin or bolt to composite interface can prove to be an inefficient electrical contact due to dissimilar materials, presence of electrically insulating films like aircraft sealant and/or hard oxide layers on the surface and irregular cut pattern of the composite. To allow current to flow easily through the pin/bolt to composite interface, the interface contact resistance is desired to be low.

Contact resistance is highly dependent on the applied load on both the surfaces that brings them in contact and electrical and mechanical properties of the material surface in contact. A soft material at the interface with high electrical conductivity lowers the contact resistance, as do higher loads. The load in a pin member joint is provided by the preload and is primarily geometry/design dependent. As described above, the material coating **22** or texturing on the bearing surface **21** of the head **18** is used to both provide a low resistivity material at the contact interface and a soft conforming layer for better contact with the structure. Soft materials with high electrical conductivity, such as copper, gold, silver or other metals/materials can be used to lower contact resistance (see, e.g., the copper seal **24** shown in **FIGS. 2** and **3**).

The surfaces of the pin member **12**, as described above, can also be textured to enable better intimacy with the surrounding composite layer. As the textured pin member **12** is installed, the textured pin member deforms into the small voids that are created during drilling of the composite layer. As the textured surfaces deform into the voids, they displace the entrapped sealant during fastener installation. The insertion of the pin member **12** causes the excess sealant to be extruded outside the pin member **12**/composite interface. Thus, the textured pin member **12** excavates excess entrapped

sealant during installation of the fastener while bringing the pin member **12** in intimate contact with the composite structure. The finish texture of the pin member's **12** surfaces is adjusted to provide a surface micro-roughness (Sa) value in order to increase the level of conformity and mechanical interlocking. In an embodiment, the surface roughness (Sa) is greater than 0.5 micron.

As described above, **FIG. 1** shows an embodiment of a tungsten coated pin member **12**. In an embodiment, plasma coating was used to deposit tungsten on the pin member **12** and achieve a surface roughness (Sa) equal or greater than 7 micron.

FIG. 2 shows the seal **24** and **FIG. 3** shows the pin member **12** with the seal **24** installed on it to promote intimacy with the composite layer on the bearing surface **21** of the head **18**. In an embodiment, the seal **24** is frusto-conical in shape, and is sized and shaped to fit on the bearing surface **21** of the head **18**. In another embodiment, this can also be achieved by copper coating the bearing surface **21** of the head **18**. In another embodiment, the seal **24** is a captive washer. In another embodiment, the seal **24** is coated with a coating. In an embodiment, the coating of the seal **24** includes the coating **22**.

FIG. 4 shows a photograph of the texture variation of the coated pin member **12**, while **FIG. 5** shows the surface topography of the coated pin member **12**. In an embodiment, the coated surfaces of the pin member **12** have an average surface roughness (Sa) of 7.5 micron. **FIGS. 6** and **7** are photographs of the textured pin member **12** at 40X and 190X magnification, respectively. As can be seen in **FIGS. 6** and **7**, the textured pin member **12** exhibits a substantially rough finish. In an embodiment, the textured pin member **12** provides improved electrical contact along the

textured surfaces of the pin member **12**, which minimizes the dielectric effect caused by the sealant, promotes easier transfer of electric current, reduces the voltage potential across the pin member **12**/composite interface, and thus enables transfer of electric current without any breakdown effects like arcing.

5 In an embodiment, in a clearance fit hole, there is no preload between the shank **14** of the pin member **12** and the composite layer, and thus electrical contact is relatively poor. Thus, it would be difficult to ensure significant current flow between the pin member **12** and the composite layer. In case sufficient currents are not conducted by the bearing surface **21** of the head **18**, there would be a possibility of arcing at the
10 gap between the shank **14** and the adjacent composite layers. Arc formation under such conditions typically initiates in the metal vapor itself. The presence of a high temperature melting material with high conductivity will ensure that sufficient metal vapor is not present to initiate arcing. Even if arcing is initiated, the volume of plasma will be low. Higher conductivity will also ensure that current is more easily passed
15 between the shank **14** and composite layer if contact is available. As described above, in certain embodiments, materials like tungsten, molybdenum, or refractory metals/ceramics can be used as the coating **22** on the shank **14** of the pin member **12** to ensure reduction in arc damage. Since lightning strikes generate high frequency currents, current would typically flow close to the fastener surface due to "skin effect".
20 The coating on the pin member **12** also helps in this respect that a higher temperature melting point and high conductivity material would carry most of the current lowering the likelihood of fastener melting or plasma generation.

Thus, the coated/textured pin member **12**:

- Improves electrical contact between composite and fastener surface;
- Minimizes fastener arcing during lightning strikes;
- Provides gap filling and mechanical interlocking capabilities;
- Reduces likelihood of plasma formation during arcing around the fastener shank;
- In case arcing occurs in the fastener, reduces the volume of plasma generated to make it easier to be contained.

Coated Fasteners with Conforming Conical Seals

Referring to **FIGS. 8, 9A and 9B**, in an embodiment, a fastener **110** includes a pin member **112** having an elongated shank portion **114** with a smooth cylindrical shank portion **115**, a head **116** at one end of the smooth cylindrical shank portion **115** and a threaded portion **117** at an opposite end of the smooth cylindrical shank portion **115**. In an embodiment, the head **116** is a countersunk head. In an embodiment, a locking member is adapted to be installed to the pin member **112** (not shown in the Figures). In an embodiment, the locking member is a threaded nut that engages the threaded portion **117** of the pin member **112**. In another embodiment, the locking member is a collar adapted to be swaged into the lock grooves of the threaded portion **117** of the pin member **112**.

In an embodiment, the pin member **112** is fully coated with a coating **119**. In an embodiment, the coating **119** is a metallic coating. In an embodiment, the coating **119** is a soft, metallic coating. That is, the coating **119** is applied to the elongated shank portion **114**, including the smooth cylindrical shank portion **115** and the threaded portion **117**, and the head **116**, including an underside (e.g., bearing surface **120**) of the head

116. In an embodiment, the coating **119** is copper. In another embodiment, the coating **119** is silver. In another embodiment, the coating **119** is gold. In other embodiments, the coating **119** is made from a material having a high electrical conductivity, for example, a material having an electrical conductivity higher than 20% IACS.

5 In other embodiments, the coating **119** can consist of any one of the coatings **22** with respect to the embodiment of the pin member **12**, which are described in detail above.

 In another embodiment, the pin member **112** is partially coated with the coating **119**. In an embodiment, the coating **119** is applied to the head **116**, including the
10 underside **120** of the head **116**, of the pin member **116**. In another embodiment, the coating **119** is applied to the head **116** (including the underside **120** of the head **116**) and to the smooth cylindrical shank portion **115** of the pin member **112**. In another embodiment, the coating **119** is applied to the smooth cylindrical shank portion **115** of the pin member **112**. In another embodiment, the coating **119** is applied to the smooth
15 cylindrical shank portion **115** and the threaded portion **117** of the pin member **112**.

 In another embodiment, the pin member **112** does not include the coating **119**.

 Still referring to **FIGS. 8, 9A** and **9B**, in an embodiment, a conforming seal element **118** is attached to the elongated shank portion **114** and juxtaposed with the bearing surface **120** of the head **116** of the pin member **112**. In an embodiment, the
20 seal element **118** is separate and distinct from the pin member **112**. In an embodiment, the seal element **118** can be positioned within a hole of a structure and the pin member **112** can then be inserted into the seal element **118** during installation of the fastener **110**. In an embodiment, the seal element **118** is frusto-conical in shape and includes a

centrally located, circular-shaped aperture **122** that is sized and shaped to fit around the shank portion **114** of the pin member **112** and juxtaposed with the bearing surface **120** of the head **116** of the pin member **112**. In an embodiment, the seal element **118** includes a sealing portion **121**. In another embodiment, a lip **123** extends from one side of the sealing portion **121**. In an embodiment, the lip **123** is angled upwardly from the sealing portion **121**. In another embodiment, a tubular portion **125** extends axially from an opposite side of the sealing portion **121**. In an embodiment, the seal element **118** is made from copper. In an embodiment, the sealing portion **121** of the seal element **118** has a thickness in a range of about 5 microns to about 100 microns.

It is noted that all solid surfaces of the pin member **112** and a structure **150** in which the fastener **110** is adapted to be installed are rough on a microscopic scale. Surface micro-roughness consist of peaks and troughs whose shape, variations in height, average separation and other geometric characteristics depend on the details of the process used to generate the surfaces. Contact between two engineering bodies occurs at discrete microscopic spots that are the result of mechanical contact of asperities on the two surfaces. For all solid materials, the area of true contact is a small fraction of the nominal contact area for a wide range of normal contact loads.

Referring to **FIGS. 10** and **11**, when mechanical load is exerted through this contact area, the mode of deformation of contact asperities is elastic, plastic, or a mixture of plastic and elastic depending on the local mechanical stresses, and on the properties of the material such as the elastic modulus and hardness. In a bulk electrical interface where the mating components are metals, the contacting surfaces often contain an oxide or other electrical insulating layers. Generally the interface becomes

electrically conductive only when electrically insulation films are displaced at the asperities of the contacting surfaces or the potential across the interface exceeds the dielectric strength of the electrically insulation film. For the sake of simplicity in the field of electrical connectors, the discrete spots are often assumed to be circular. This
5 assumption provides an acceptable geometric description of the average contact spots where the roughness topographies of the mating surfaces are isotropic. While this assumption is acceptable for metallic structures, it becomes invalid when the mating surfaces are characterized by directional micro-texture or are clearly anisotropic in nature. The true area of contact between a fastener and the surrounding CFRP
10 structure is a very small percent of the nominal area due to the multi-layered construction and anisotropic nature of CFRP structures, which further complicates quality of the electrical contact between the fastener and surrounding CRFP structure.

FIG. 12A illustrates a standard fastener installed in a structure (e.g., an aluminum panel), which shows microgaps between the head of a pin member and the
15 structure. In an embodiment, with reference to **FIG. 12B**, the conforming seal element **118** is adapted to maximize the true area of contact between the fastener (e.g., the bearing surface **120** of the head **116** of the pin member **112**) and a structure **150** with minimum mechanical load. In an embodiment, the structure **150** includes a composite material. In another embodiment, the structure **150** is substantially made from a
20 composite material. In another embodiment, the structure **150** is partially made from a composite material. In another embodiment, the structure **150** includes a metallic material. In an embodiment, the metallic material is aluminum. In another embodiment,

the structure **150** is made substantially from a metallic material. In another embodiment, the structure **150** is made partially from a metallic material.

In an embodiment, the conforming seal element **118** includes a multi-layer construction with a relatively soft, yet highly electrically conductive base layer, which provides macroscopic conformity, and a softer top layer, which provides microscopic conformity.

In an embodiment, a method by which the fastener **110** with the seal element is installed is described hereinbelow. In an embodiment, with reference to **FIGS. 8, 9A, 9B, 13A, 13B, 14A** and **14B**, the method includes the steps of coating the pin member **112** with the coating **119** (either fully or partially as described above), attaching the seal element **118** to the fastener **110** (e.g., the pin member **112**), and installing the fastener **110** in the structure **150**. In an embodiment, the coating step is not included when the pin member **112** is not coated with the coating **119** as described above. In another embodiment, the seal element **118** can be positioned within a hole of the structure **150** and the pin member **112** can then be inserted into the seal element **118** during installation of the fastener **110**. In an embodiment, with respect to the installation step, a preload to the fastener **110** is provided by the locking member (e.g., nut or collar), and a force is exerted on the structure **150** by the pin member **112** with the seal element **118** positioned between the head **116** of the pin member **112** and the structure **150**. As the seal element **118** conforms to the inherent micro-roughness between the head **116** of the pin member **112** and the structure **150**, a portion of the seal element **118** is extruded upward the edge of the pin member **112** and protrudes above the surface of the structure **150**. With reference to **FIGS. 13A, 14B, 14A** and **14B**, the seal element **118** is

trimmed flush with the surface of the structure **150** by sanding the top of the seal element **118** (e.g., proximate to the lip **123**) and, if necessary, the structure **150**. In an embodiment, the sanding step is simultaneous with the preparation of the surface of the structure **150** for the application of paint **152**.

5 **FIGS. 15A** and **15B** are photographs illustrating the cross-sections of a pin member without the seal element **118** (**FIG. 15A**) and the pin member **112** with the seal element **118** (**FIG. 15B**). As shown, the inclusion of the seal element **118** is provided along with a copper mesh **154** and improves paint adhesion.

Referring to **FIG. 15C**, the fastener **110** improves a range of countersink within
10 the structure **150** over which the connection with the copper mesh **152** is maintained. As seen on the graph shown in **FIG. 20**, the flushness tolerance of the fastener **110**, shown on the left, is wider than a baseline fastener without the seal element, as shown on the right.

FIGS. 16A through **16D** are photographs showing the difference in pin/CFRP
15 interface between a conventional fastener without a seal element (**FIGS. 16A** and **16B**) and a fastener with the seal element **18** (**FIGS. 16C** and **16D**). Micro-level conformance between the seal element **118** and the CFRP structure **50** enhances the current transfer from fastener to the structure **150** and reduce arcing.

FIGS. 17A through **17D** illustrate the differences in the effects of damage in
20 aluminum panels of a fastener without the seal element **118** (**FIGS. 17A** and **17C**) and a fastener with the seal element **118** (**FIGS. 17B** and **17D**). The seal element **118** increases the electrical intimacy between the fastener **110** and the structure in the area

adjacent to the seal element **118**. As will be described in more detail below, this reduces the magnitude of the electric field near the locking member (e.g., nut or collar).

With reference to **FIGS. 18A** through **18F**, which illustrate simulation results, the seal element **118** reduces contact resistance around the head **116** of the pin member **112** and results in optimized electrical intimacy. This nanoscale conformity leads to improved current transfer into the upper panel of the aircraft structure **150**. During a lightning strike, the external discharge, which attaches to the head **116**, will tend to attach to regions having larger electric fields. In the case of the fastener **110** having the seal element **118**, the electric fields are much lower, resulting in so-called equipotential surfaces with a flatter field profile. This field flattening effect minimizes the amount of structural damage caused by large concentrated flows through sharp edges.

An advantage of the seal element **118** is the large reduction of the charge buildup between the fastener **110** and surrounding materials within the fastener assembly. The time dependent electric potential has a lower peak value, which results in a large reduction of the electric field magnitudes around the bearing surface of the nut region. Typically, large fields around the nut region and sharp edges can result in dielectric breakdown and edge glow phenomenon. The large reduction in electric fields is a direct result of the enhanced current transport.

Referring to **FIG. 19**, the fastener **110** includes a reduced contact resistance. Contact resistivity measurements show current transfer improvement with the fastener **110** having the coating **119** and the seal element **118** over baseline pin members without the coating **119** and the seal element **118**.

It should be understood that the embodiments described herein are merely exemplary and that a person skilled in the art may make many variations and modifications without departing from the spirit and scope of the invention. All such variations and modifications are intended to be included within the scope of the claims.

CLAIMS

What is claimed is:

1. A fastener, comprising:

a pin member including an elongated shank having a first end, a second end
5 opposite the first end, a cylindrical shank portion having an outer surface, a head
located at the first end of the elongated shank, the head including a bearing surface
located on the underside of the head, and a threaded portion located at the second end
of the elongated shank; and

a seal element attached to the pin member and juxtaposed with the bearing
10 surface of the head of the pin member.

2. The fastener of Claim 1, wherein the seal element is made of copper.

3. The fastener of Claim 2, wherein the seal element includes a sealing portion
15 having a first side and a second side opposite the first side, a lip extending from the first
side of the sealing portion.

4. The fastener of Claim 3, wherein the lip extends angularly from the sealing
portion.

20 5. The fastener of Claim 4, wherein the seal element includes a tubular portion
extending axially from the side of the sealing portion.

6. The fastener of Claim 5, wherein the seal element includes a thickness in a range of about 5 microns to about 100 microns.

7. The fastener of Claim 1, wherein the pin member includes a coating.

5

8. The fastener of Claim 7, wherein the coating is a metallic coating.

9. The fastener of Claim 8, wherein the metallic coating is selected from the group consisting of gold, silver, and copper.

10

10. The fastener of Claim 7, wherein the coating is made from a material having an electrical conductivity higher than 20% IACS.

11. The fastener of Claim 7, wherein the head of the pin member is coated with the
15 coating.

12. The fastener of Claim 7, wherein the outer surface of the cylindrical shank portion of the pin member is coated with the coating.

20 13. The fastener of Claim 12, wherein the head of the pin member is coated with the coating.

14. The fastener of Claim 12, wherein the threaded portion of the pin member is coated with the coating.

15. The fastener of Claim 7, wherein the pin member is fully coated with the coating.

5

16. In combination, a structure; and a fastener installed within the structure, the fastener including a pin member having an elongated shank with a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface
10 located on the underside of the head, and a threaded portion located at the second end of the elongated shank, and a seal element attached to the pin member and juxtaposed with the bearing surface of the head of the pin member.

17. The combination of Claim 16, wherein the seal element is made of copper.

15

18. The combination of Claim 17, wherein the seal element includes a sealing portion having a first side and a second side opposite the first side, a lip extending from the first side of the sealing portion.

20 19. The combination of Claim 18, wherein the lip extends angularly from the sealing portion.

20. The combination of Claim 19, wherein the seal element includes a tubular portion extending axially from the side of the sealing portion.

21. The combination of Claim 20, wherein the seal element includes a thickness in a
5 range of about 5 microns to about 100 microns.

22. The combination of Claim 16, wherein the pin member includes a coating.

23. The combination of Claim 22, wherein the coating is a metallic coating.

10 24. The combination of Claim 23, wherein the metallic coating is selected from the group consisting of gold, silver, and copper.

25. The fastener of Claim 22, wherein the coating is made from a material having an
15 electrical conductivity higher than 20% IACS.

26. The combination of Claim 22, wherein the head of the pin member is coated with the coating.

20 27. The combination of Claim 22, wherein the outer surface of the cylindrical shank portion of the pin member is coated with the coating.

28. The combination of Claim 27, wherein the head of the pin member is coated with the coating.

29. The combination of Claim 27, wherein the threaded portion of the pin member is
5 coated with the coating.

30. The combination of Claim 22, wherein the pin member is fully coated with the coating.

10 31. The combination of Claim 16, wherein the structure includes a composite material.

32. The combination of Claim 31, wherein the structure is substantially made from the composite material.

15

33. The combination of Claim 31, wherein the structure is partially made from the composite material.

34. The combination of Claim 16, wherein the structure includes a metallic material.

20

35. The combination of Claim 34, wherein the metallic material is aluminum.

36. The combination of Claim 34, wherein the structure is made substantially from the metallic material.

37. The combination of Claim 34, wherein the structure is made partially from the
5 metallic material.

38. A method of making a fastener, comprising the steps of:

providing a pin member including an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a
10 head located at the first end of the elongated shank, the head including a bearing surface located on the underside of the head, and a threaded portion located at the second end of the elongated shank; and

attaching a seal element to the pin member in a position that is juxtaposed with the bearing surface of the head of the pin member.

15 39. The method of Claim 38, further including the step of coating at least a portion of the pin member with a coating.

40. The method of Claim 39, wherein the coating is a metallic coating.

20 41. The fastener of Claim 40, wherein the metallic coating is selected from the group consisting of gold, silver, and copper.

42. The fastener of Claim 39, wherein the coating is made from a material having an electrical conductivity higher than 20% IACS.

43. The fastener of Claim 39, wherein the coating step includes coating the head of the pin member with the coating.

44. The fastener of Claim 39, wherein the coating step includes coating the outer surface of the cylindrical shank portion with the coating.

45. The fastener of Claim 44, wherein the coating step includes coating the head of the pin member with the coating.

46. The fastener of Claim 44, wherein the coating step includes coating the threaded portion of the pin member with the coating.

47. The fastener of Claim 39, wherein the coating step includes coating the pin member fully with the coating.

48. A method of installing a fastener into a structure, comprising the steps of:

providing a fastener having a pin member including an elongated shank having a first end, a second end opposite the first end, a cylindrical shank portion having an outer surface, a head located at the first end of the elongated shank, the head including a bearing surface located on the underside of the head, and a threaded portion located at

the second end of the elongated shank and a seal element adapted to be positioned on the pin member such that the seal member is juxtaposed with the bearing surface of the head of the pin member; and

installing the fastener into the structure in an installed position.

5

49. The method of Claim 48, further including the step of coating at least a portion of the pin member with a coating.

50. The method of Claim 49, wherein the coating is a metallic coating.

10

51. The method of Claim 50, wherein the metallic coating is selected from the group consisting of gold, silver, and copper.

52. The fastener of Claim 49, wherein the coating is made from a material having an electrical conductivity higher than 20% IACS.

15

53. The method of Claim 49, wherein the coating step includes coating the head of the pin member with the coating.

54. The method of Claim 49, wherein the coating step includes coating the outer surface of the cylindrical shank portion with the coating.

20

55. The method of Claim 54, wherein the coating step includes coating the head of the pin member with the coating.

56. The method of Claim 54, wherein the coating step includes coating the threaded
5 portion of the pin member with the coating.

57. The method of Claim 50, wherein the coating step includes coating the pin member fully with the coating.

10 58. The method of Claim 48, wherein the structure includes a composite material.

59. The method of Claim 58, wherein the structure is substantially made from the composite material.

15 60. The method of Claim 58, wherein the structure is partially made from the composite material.

61. The method of Claim 48, wherein the structure includes a metallic material.

20 62. The method of Claim 61, wherein the metallic material is aluminum.

63. The method of Claim 61, wherein the structure is made substantially from the metallic material.

64. The method of Claim 61, wherein the structure is made partially from the metallic material.

65. The method of Claim 48, further comprising the step of trimming the seal element
5 flush with the structure.

66. The method of Claim 65, wherein the trimming step includes sanding the seal element.

10 67. The method of Claim 65, further comprising the step of providing a metallic mesh on an outer surface of the structure, wherein when the fastener is in its installed position, the sealing element of the fastener is in direct physical and electrical contact with the metallic mesh.

15 68. The method of Claim 67, wherein the seal element includes a sealing portion having a first side and a second side opposite the first side, a lip extending from the first side of the sealing portion, the lip being in direct physical and electrical contact with the metallic mesh.

20 69. The method of Claim 68, wherein the metallic mesh is made from copper.

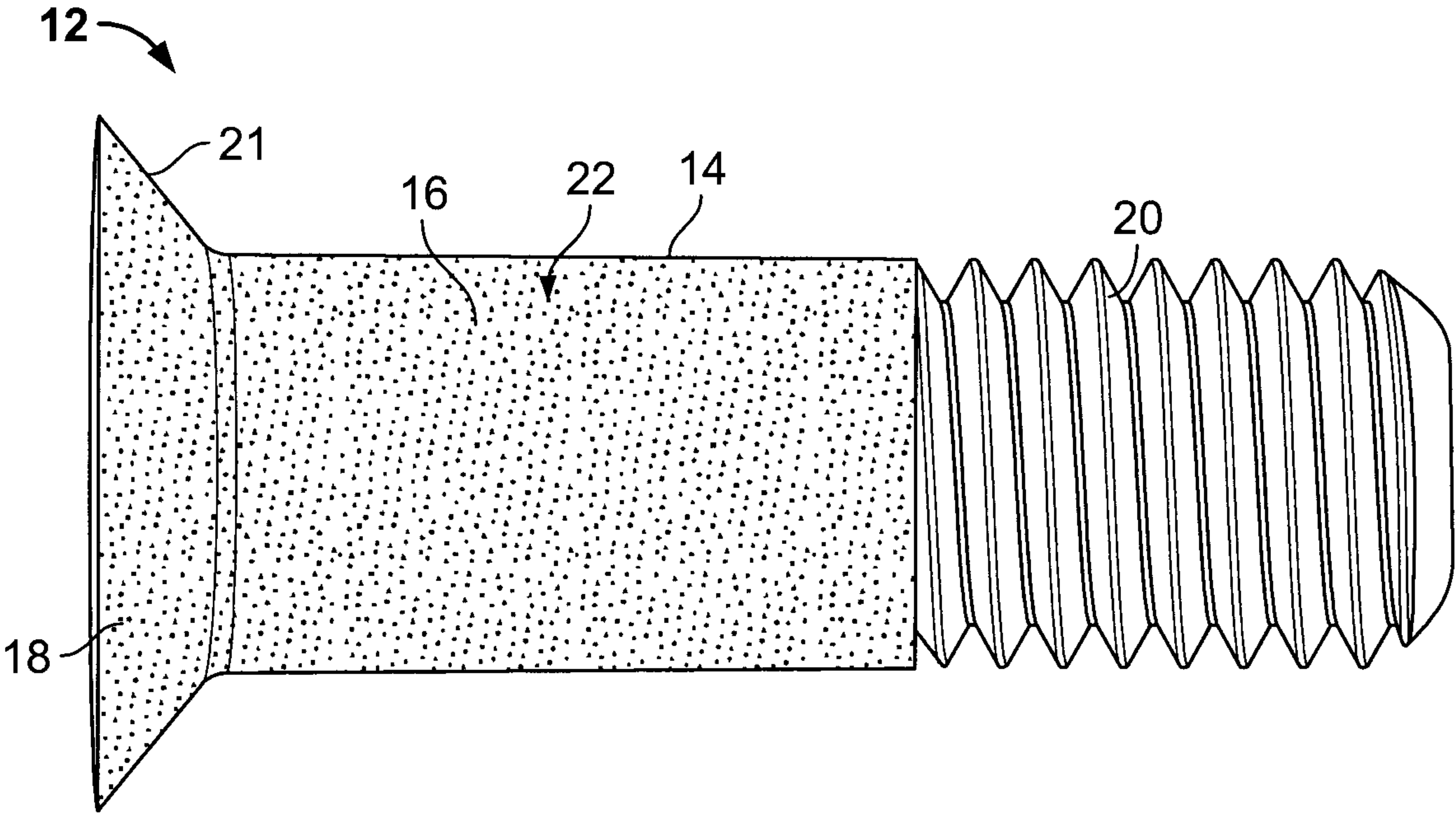


FIG. 1

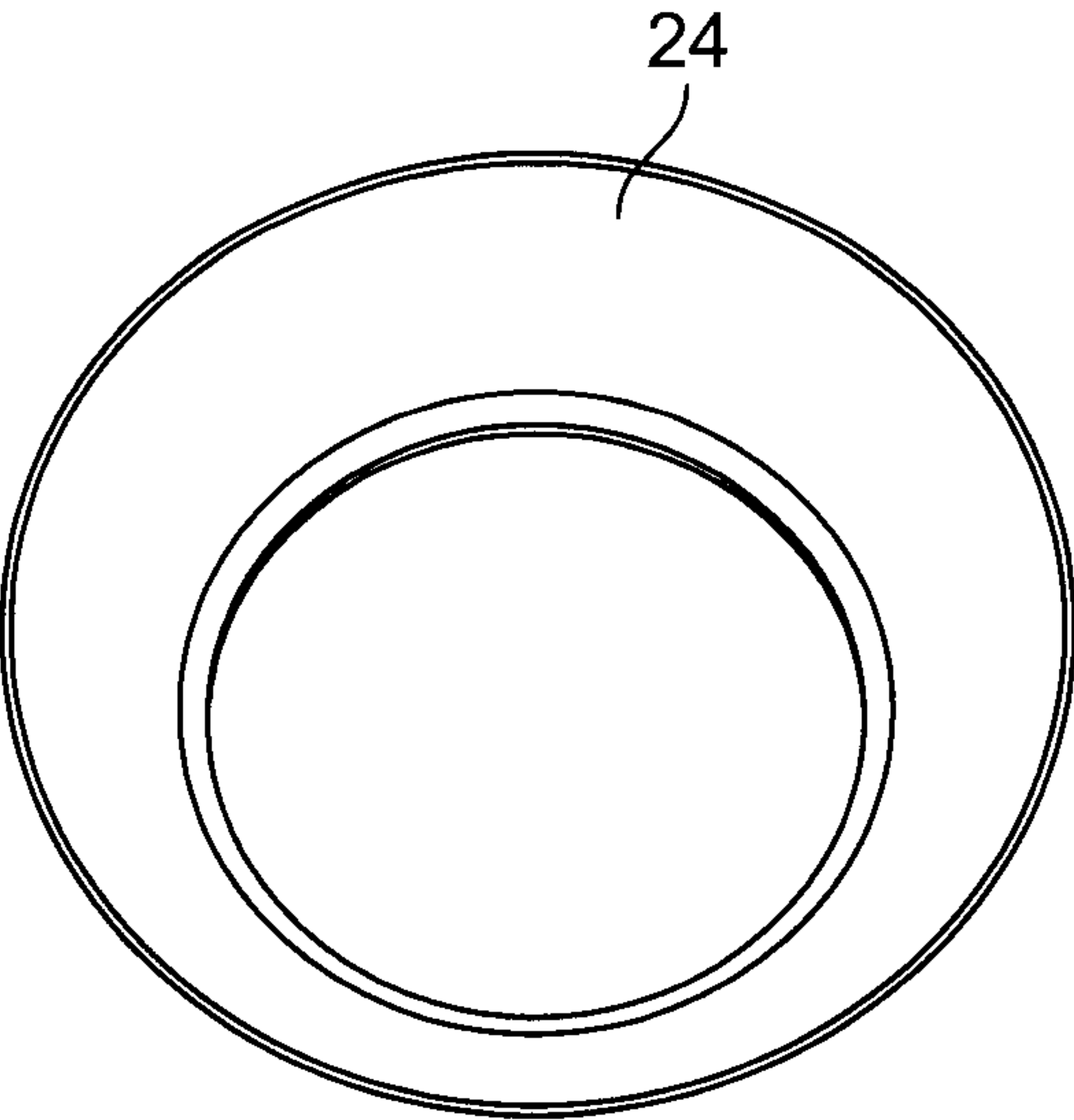


FIG. 2

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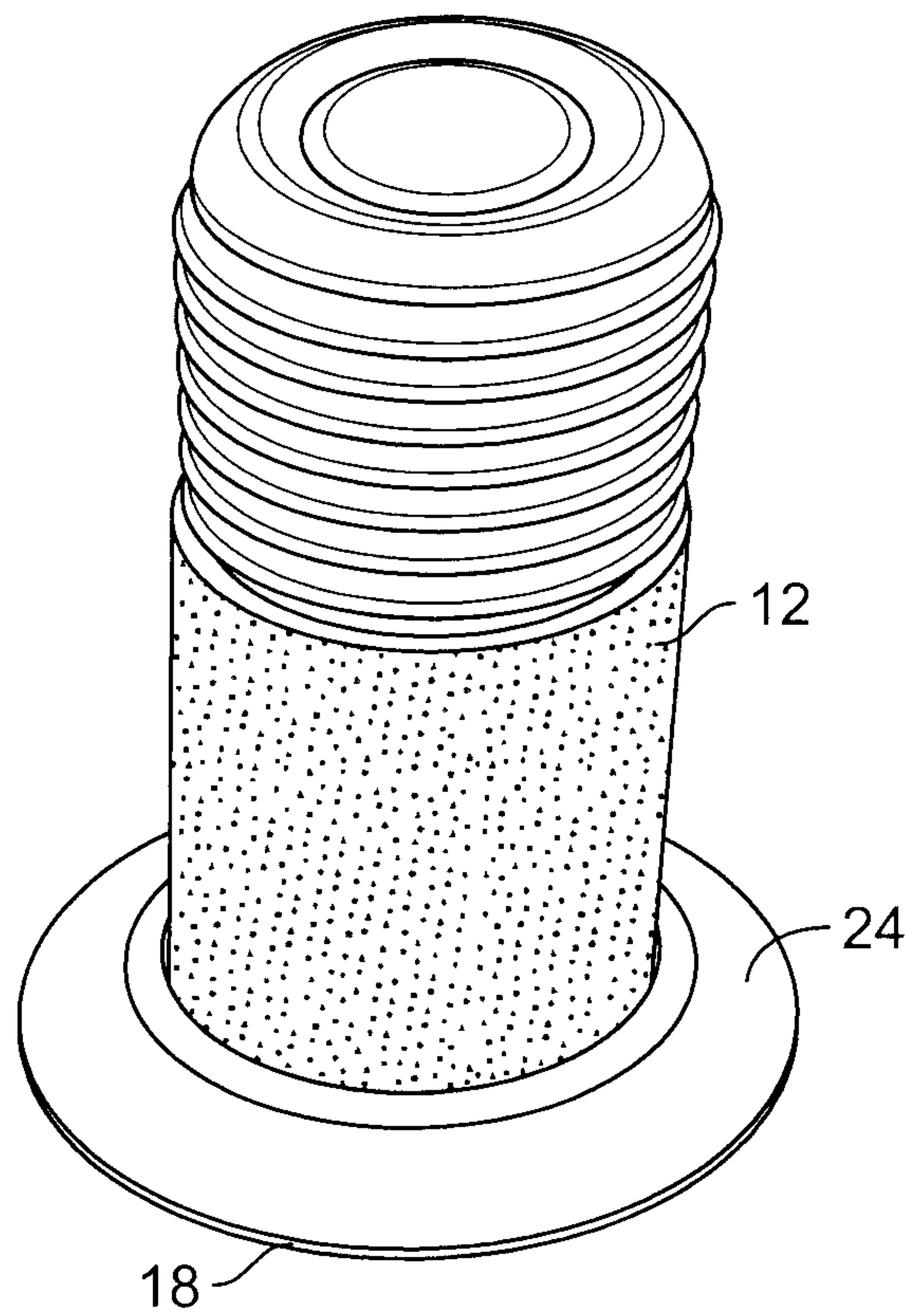


FIG. 3

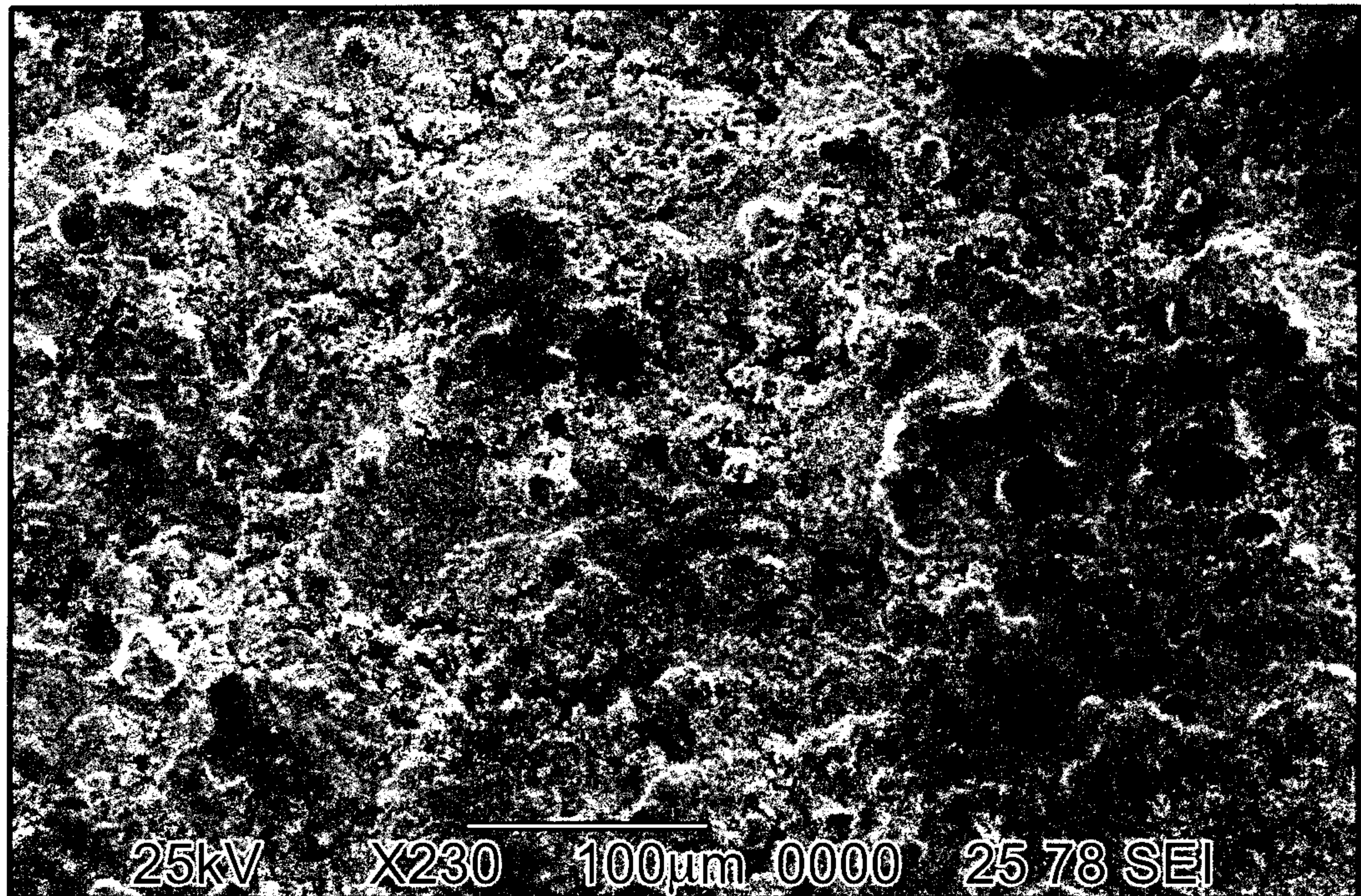


FIG. 4

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Sa: 7.4999 μm
Mag: 6.7500

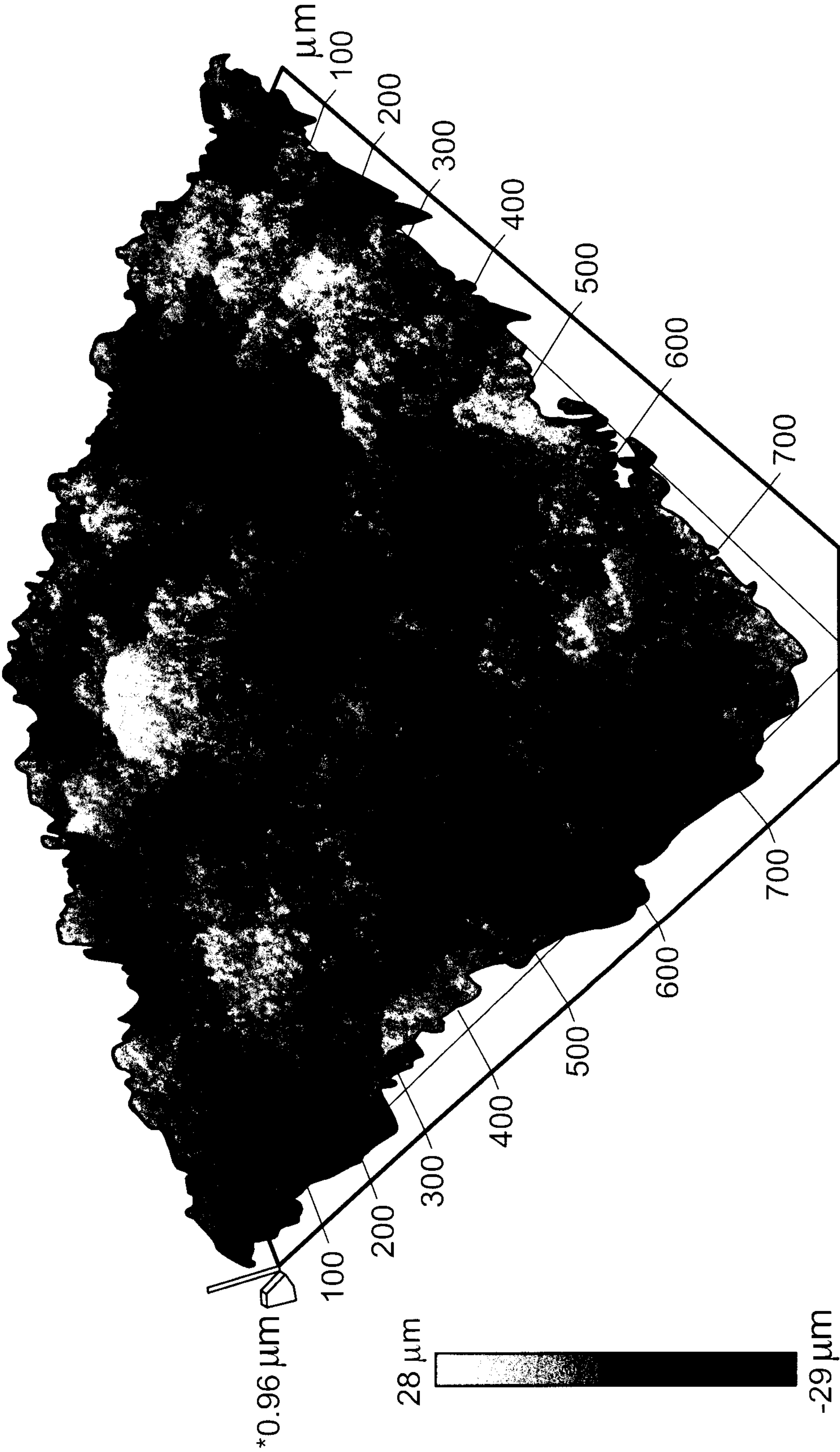


FIG. 5

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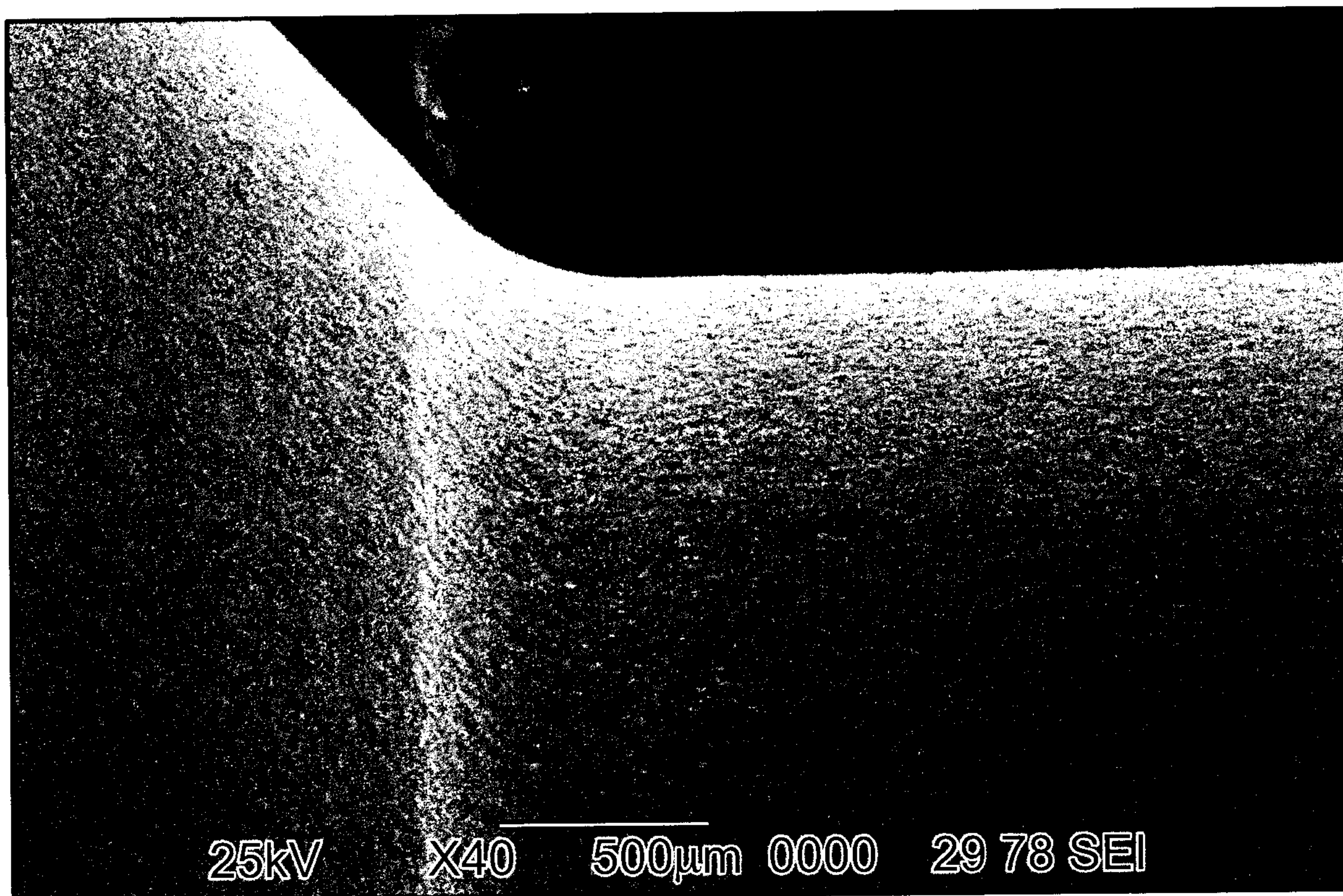


FIG. 6

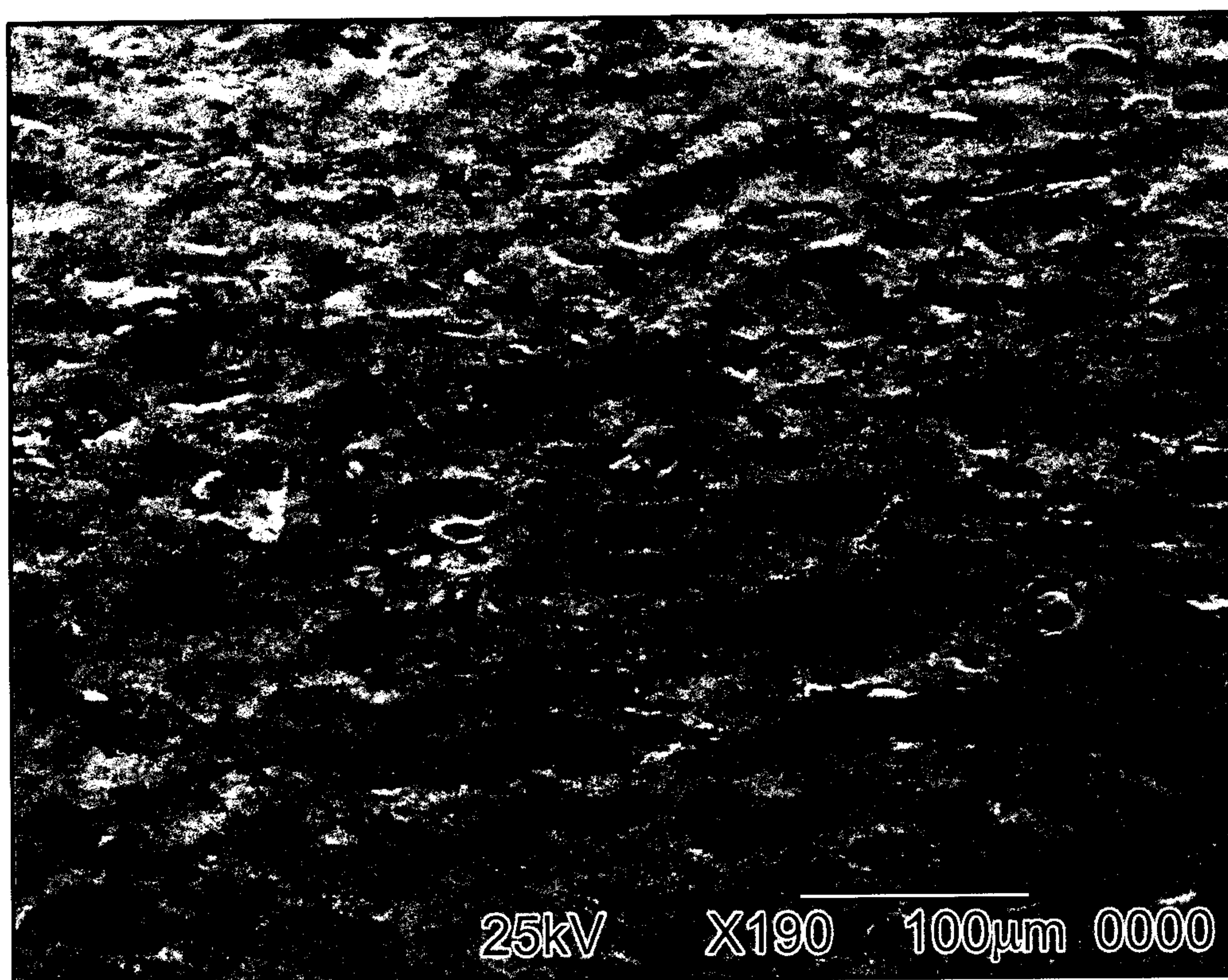


FIG. 7

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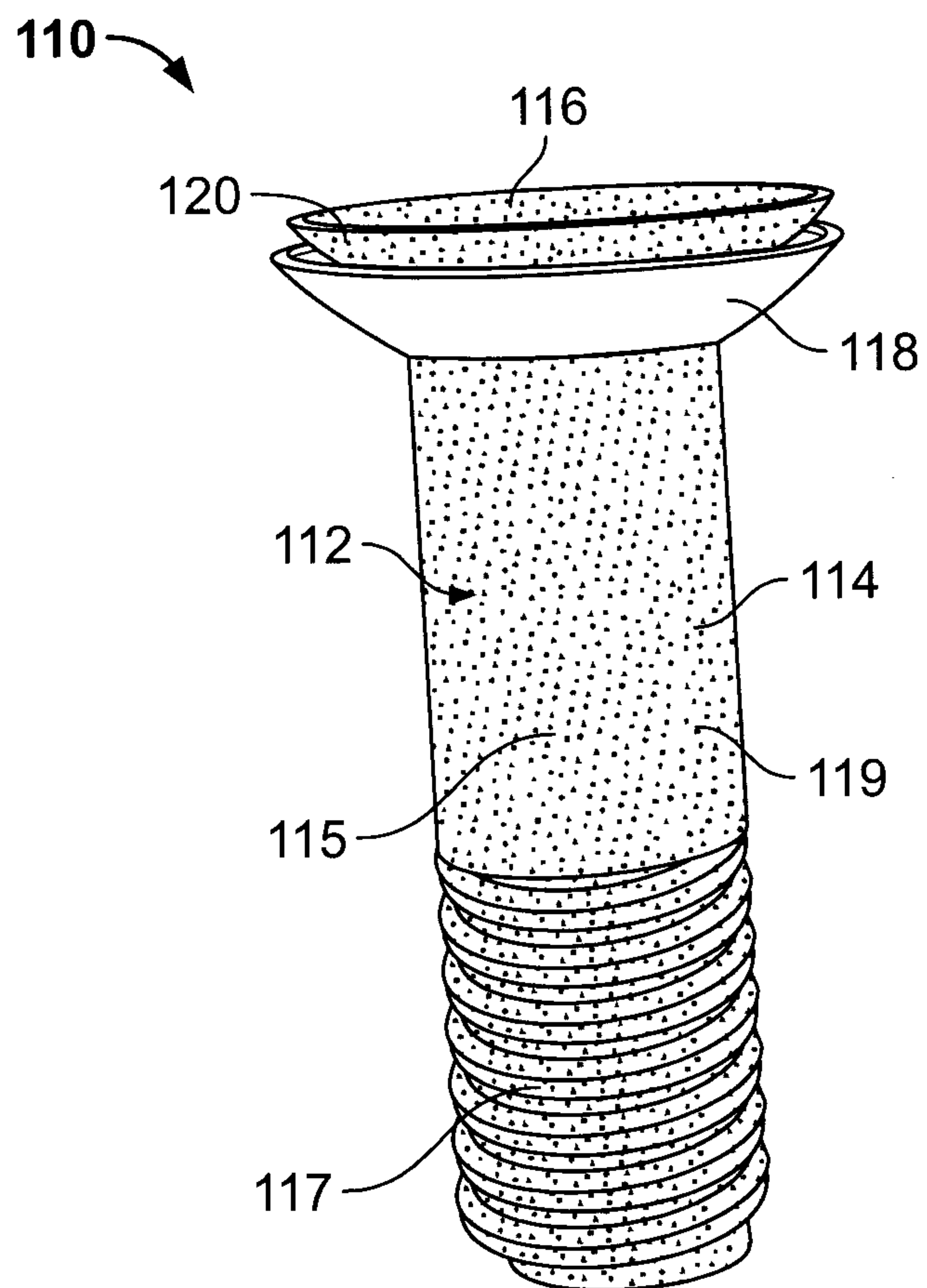


FIG. 8

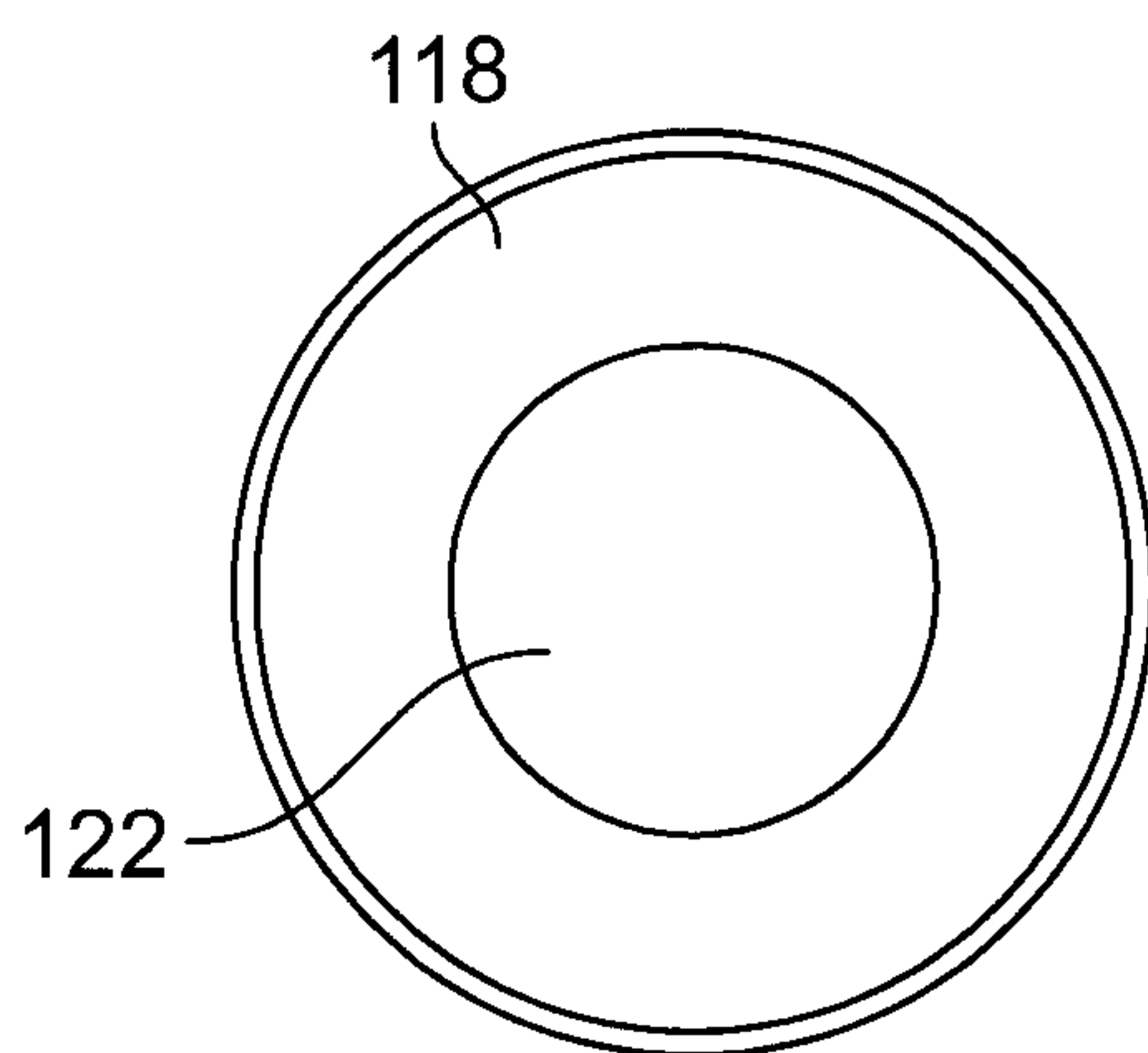


FIG. 9A

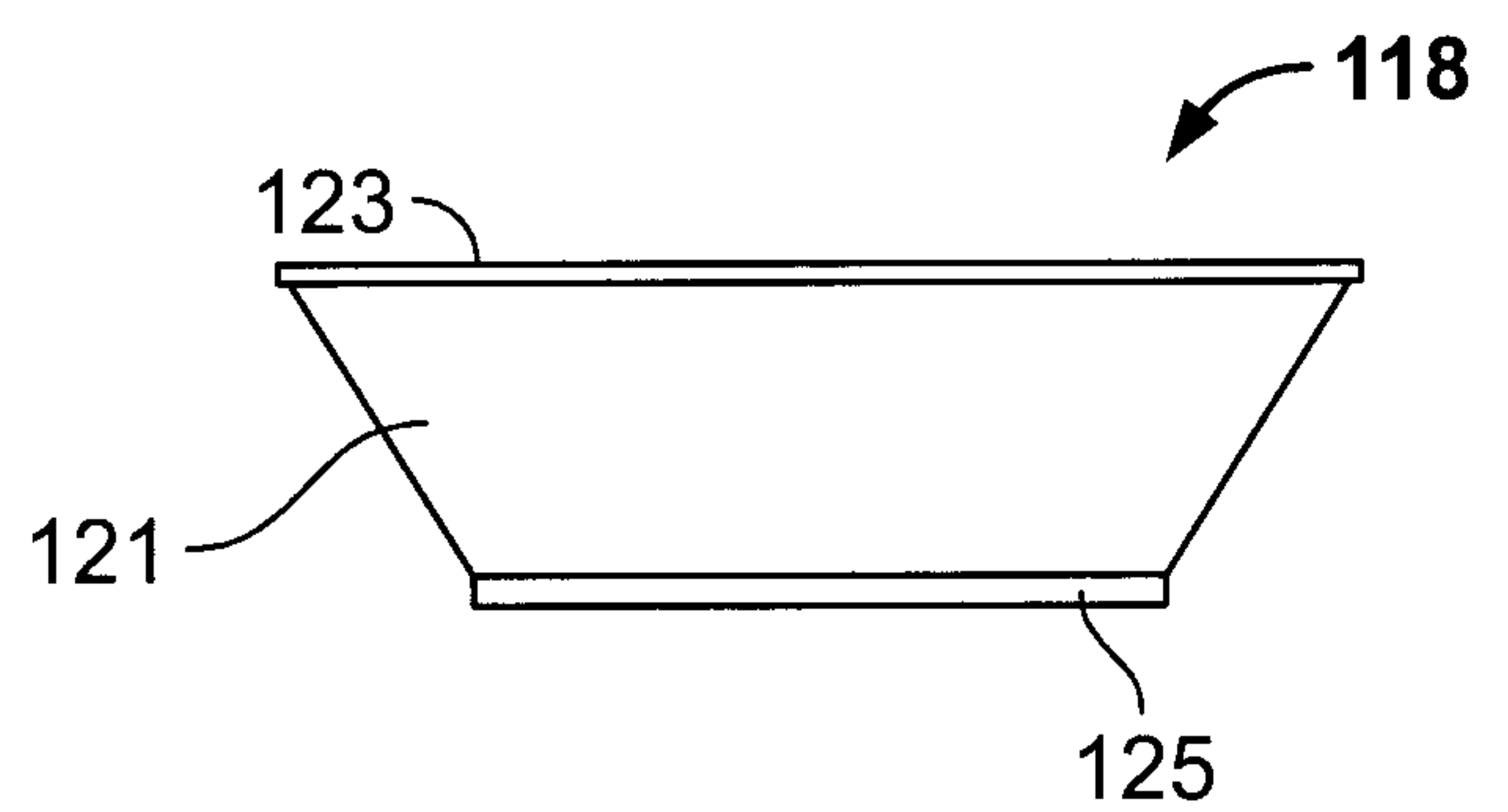


FIG. 9B

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FIG. 10

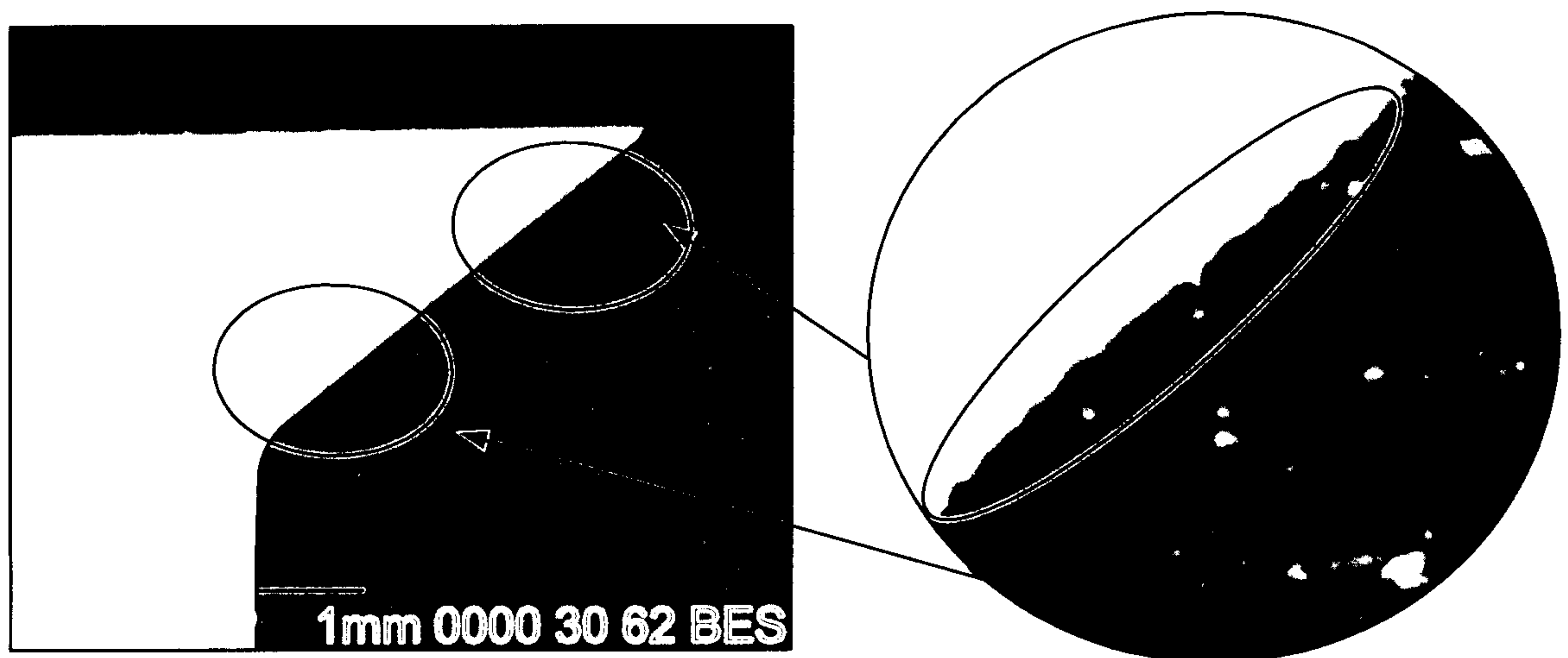


FIG. 11

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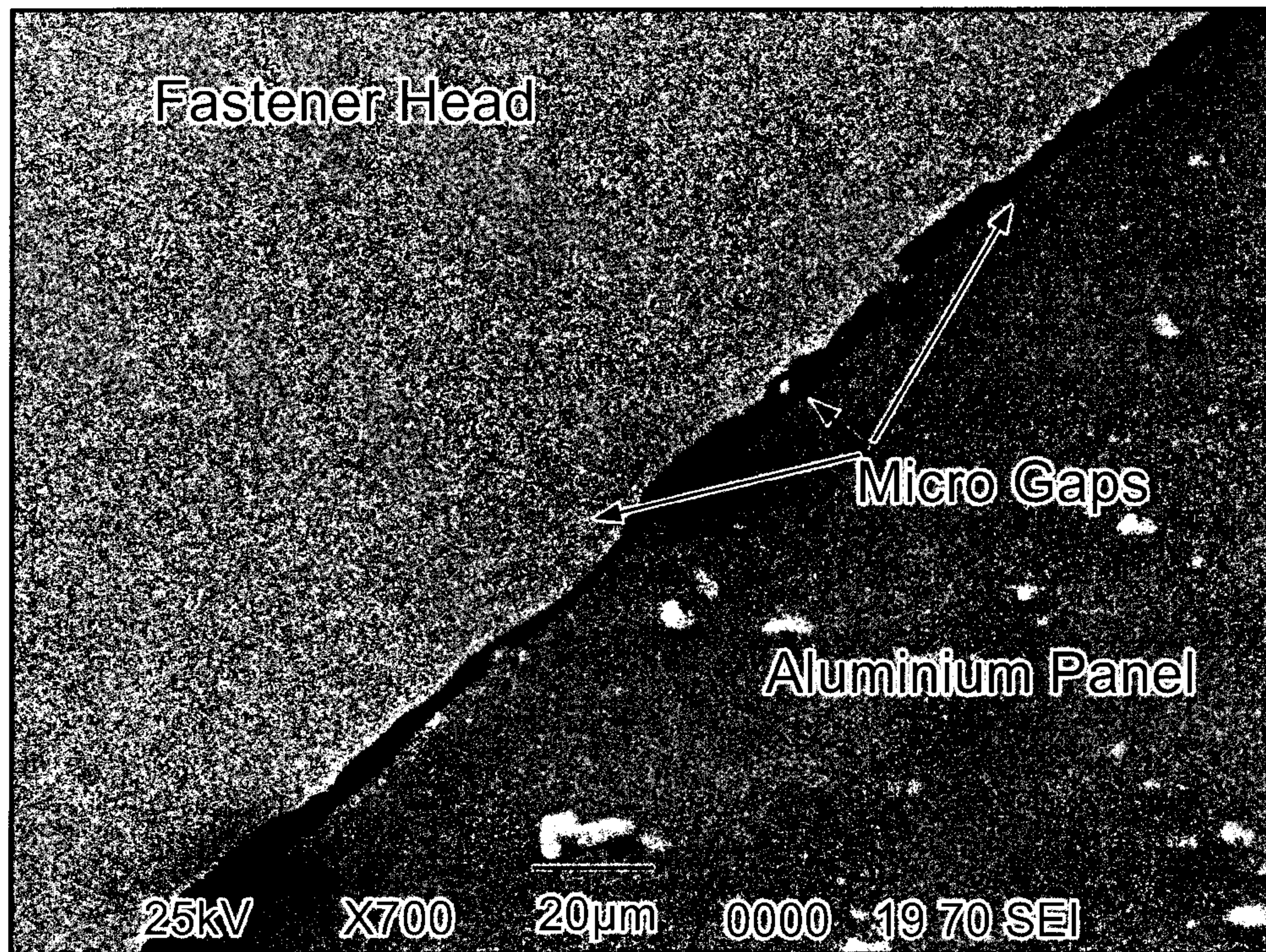


FIG. 12A

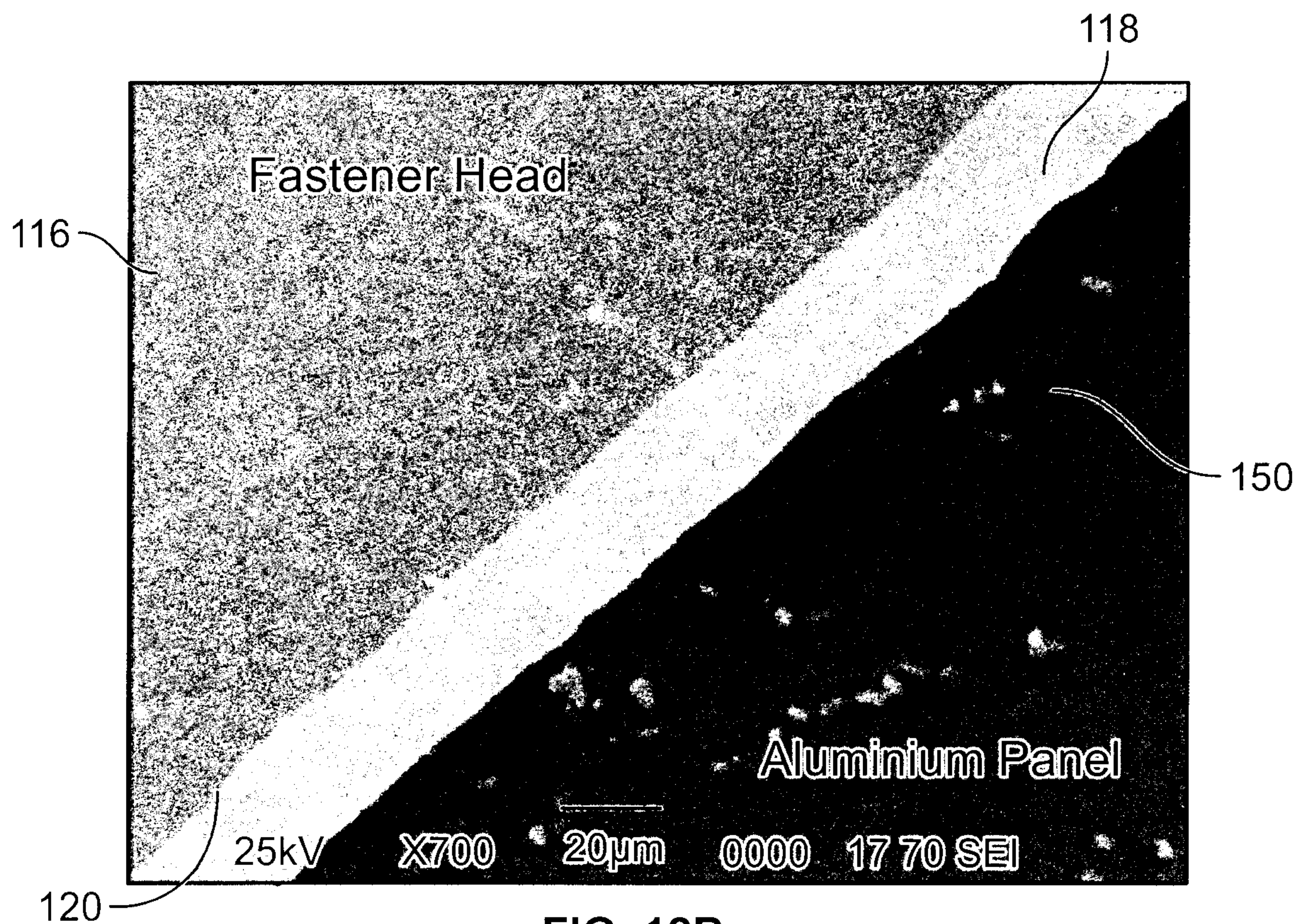


FIG. 12B

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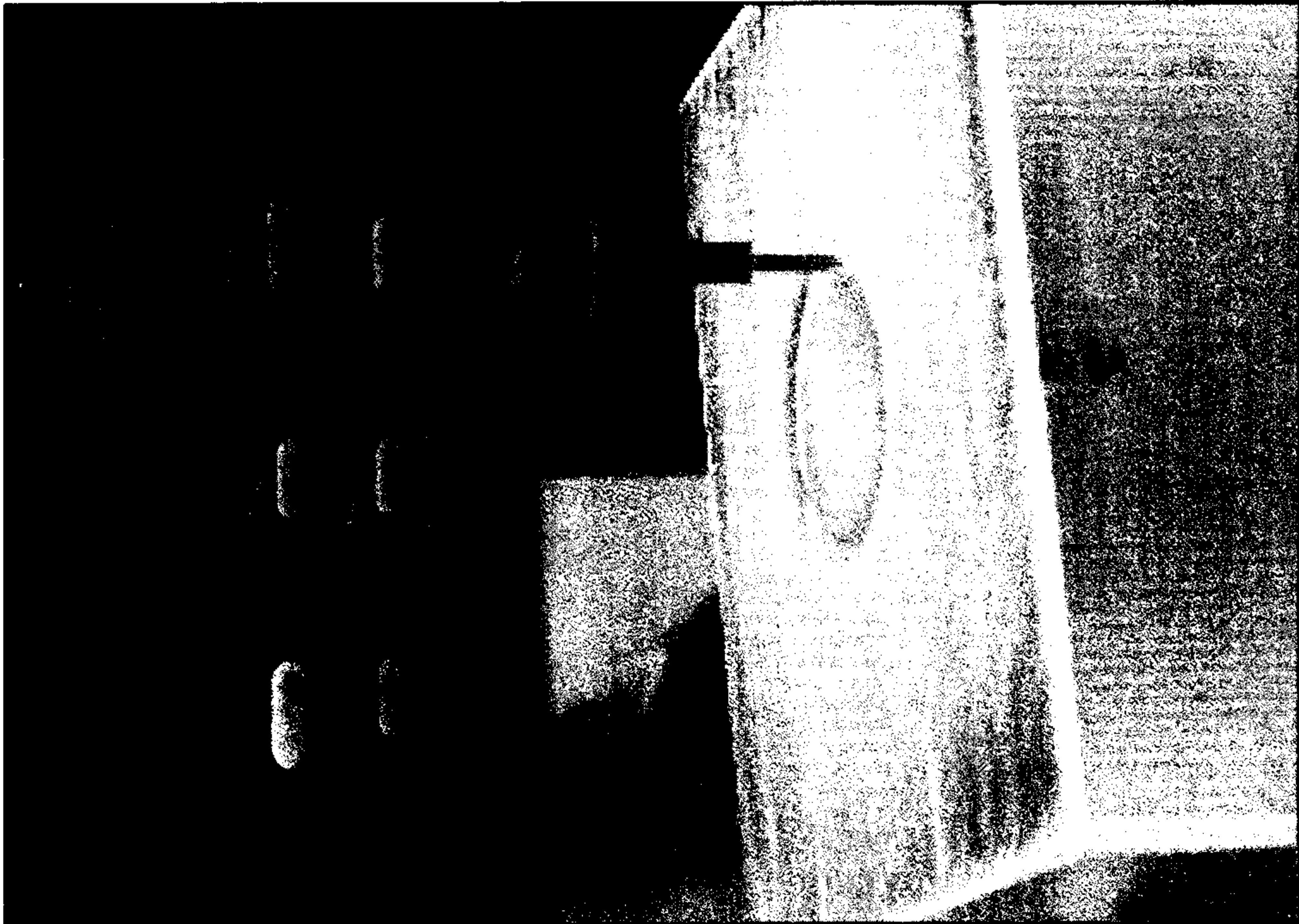


FIG. 13B

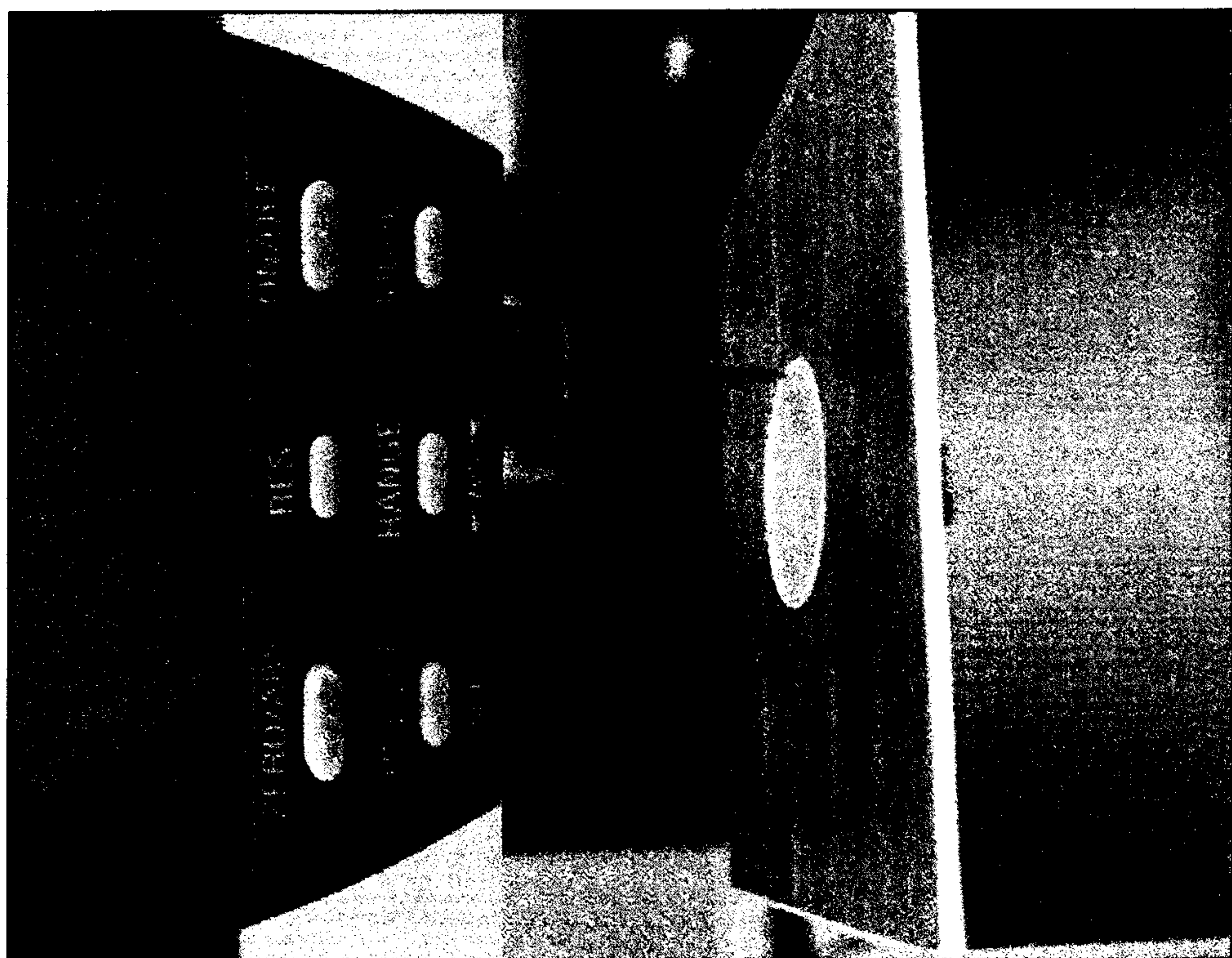


FIG. 13A

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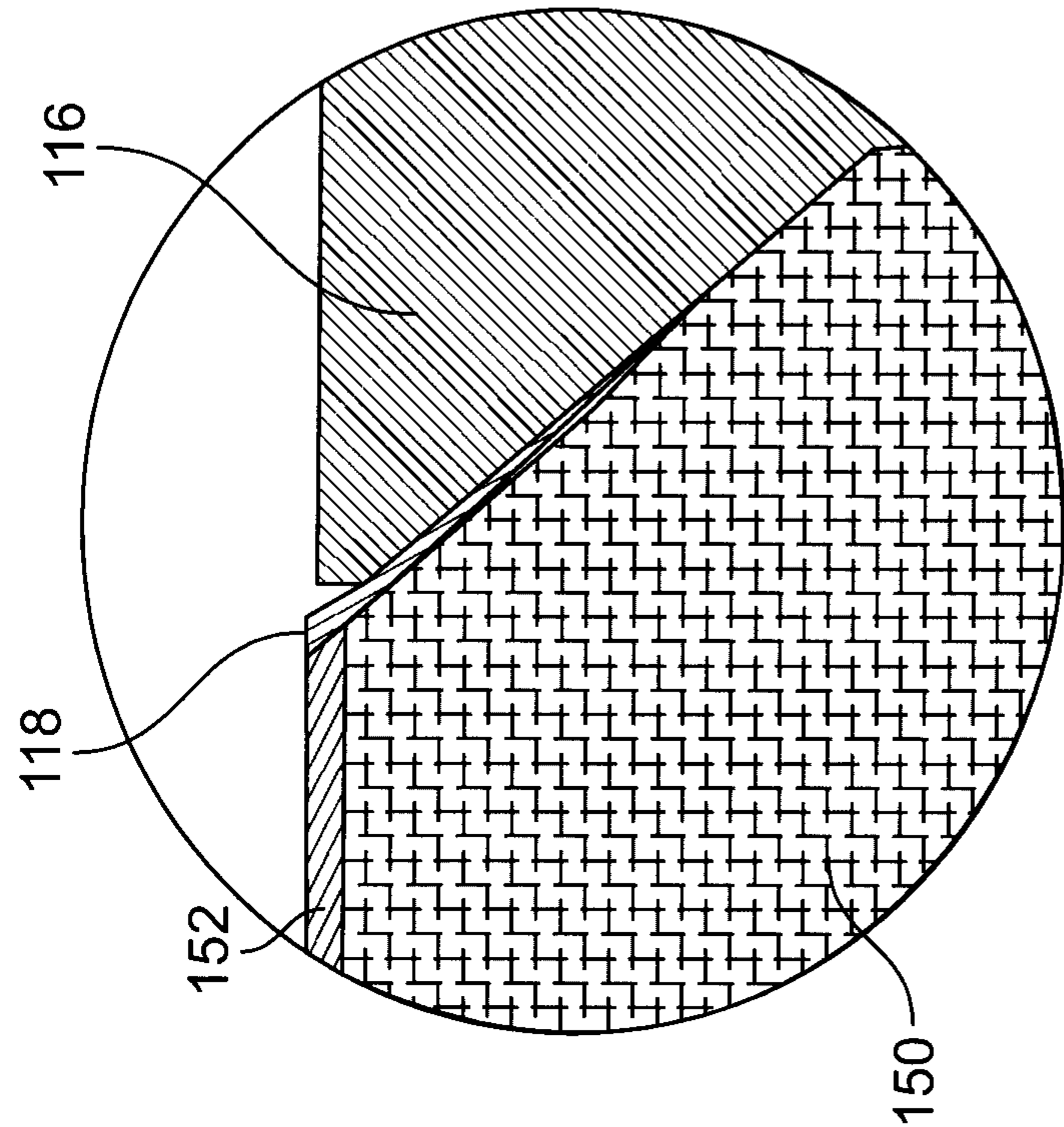


FIG. 14B

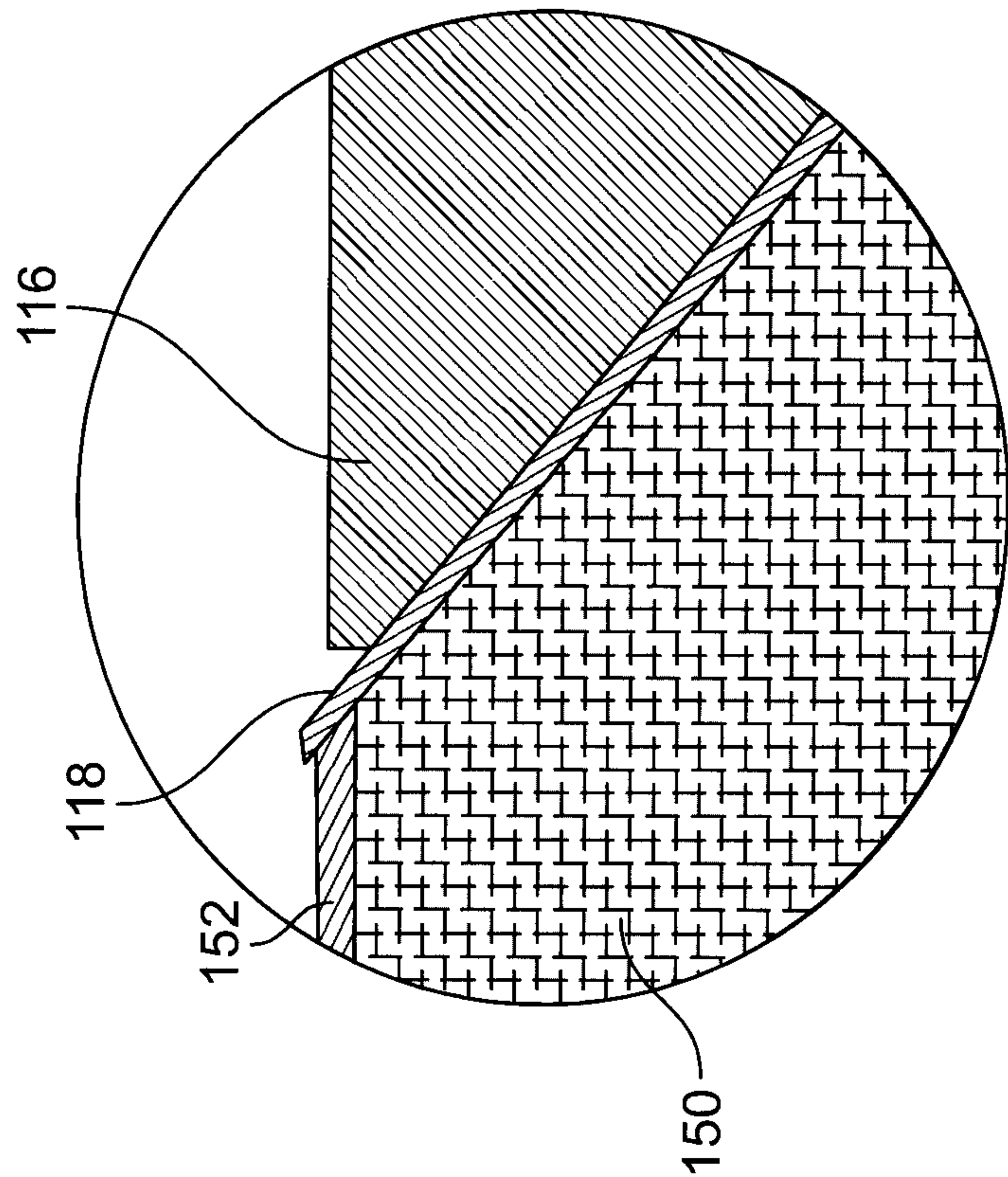


FIG. 14A

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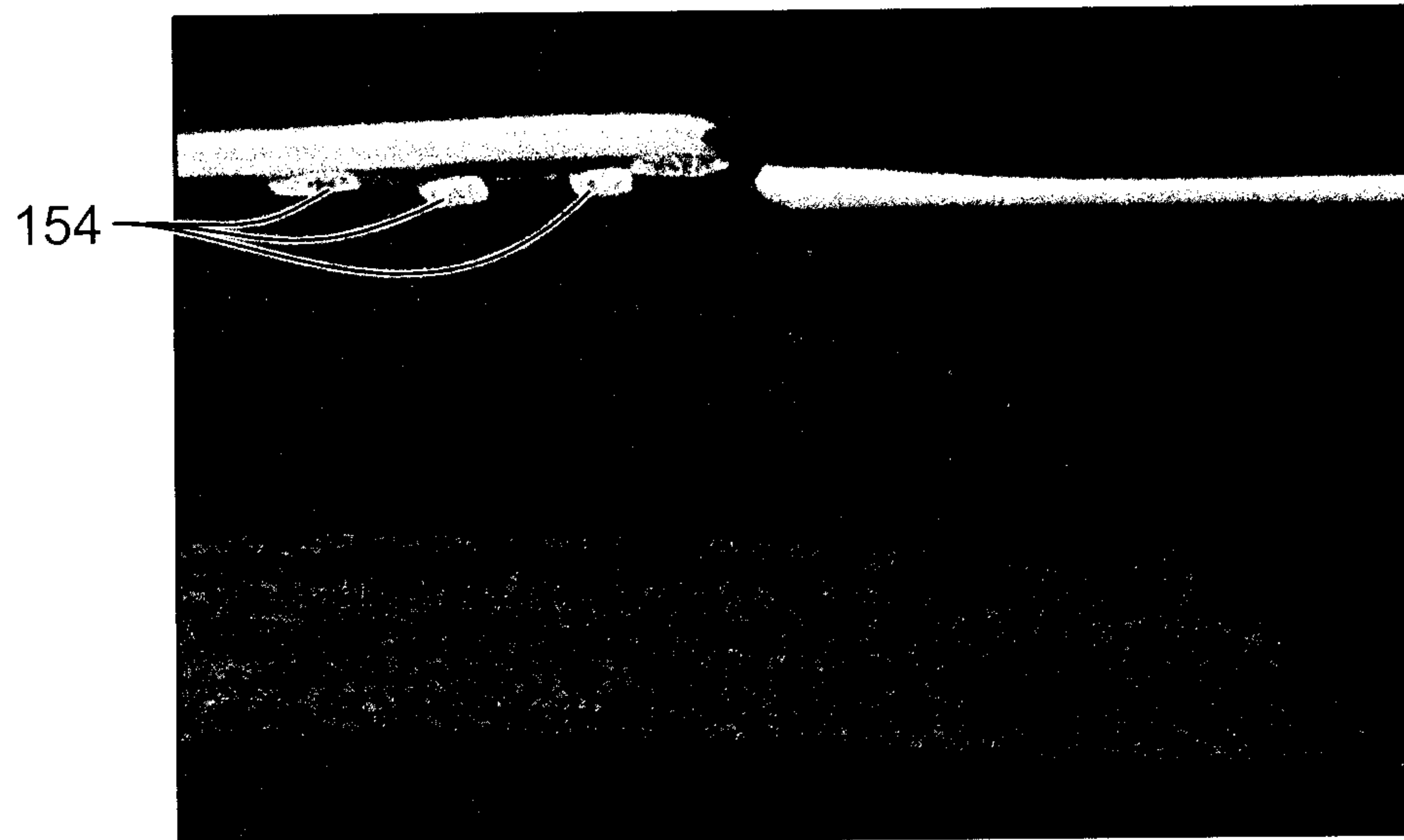


FIG. 15A

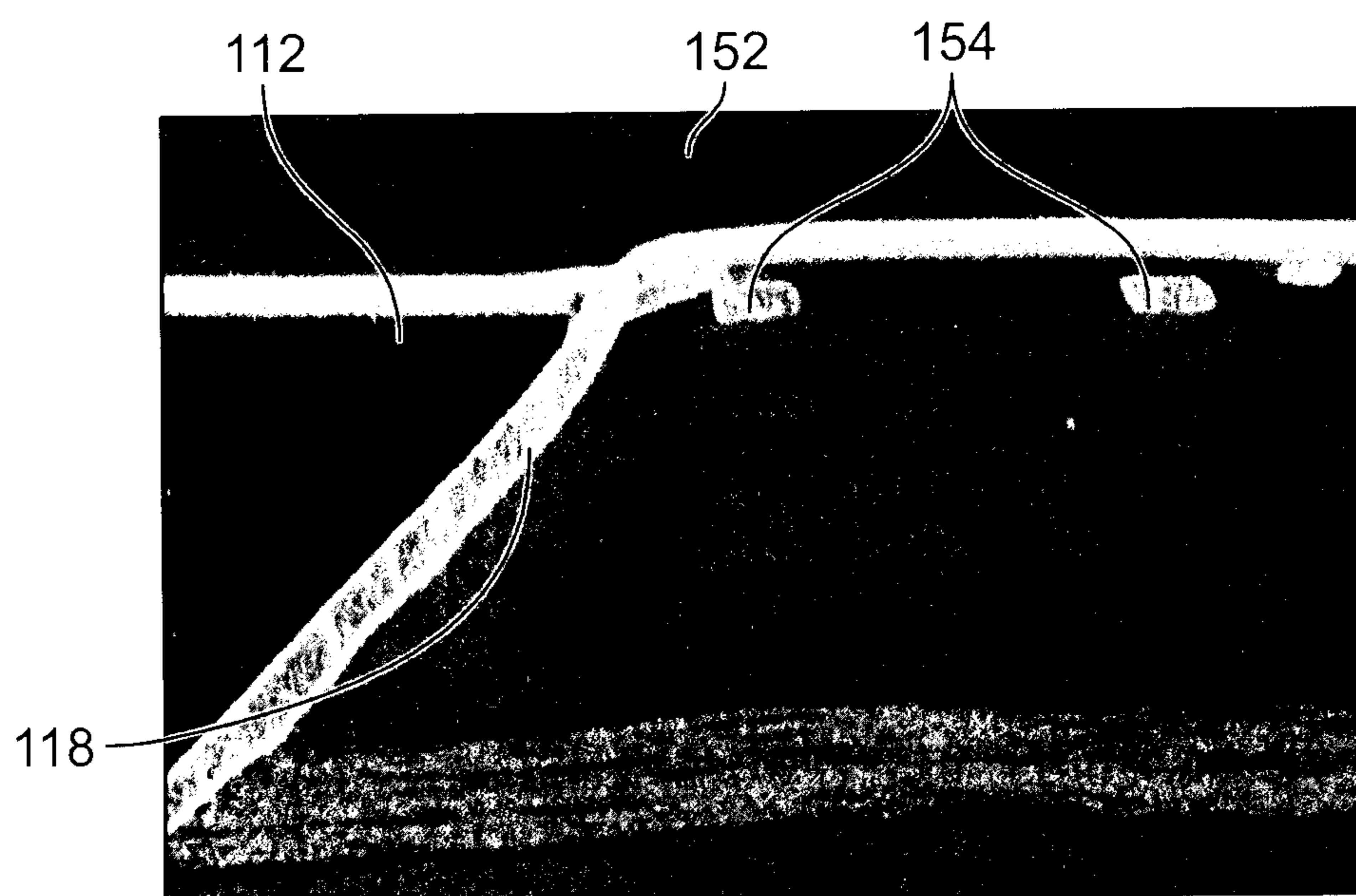


FIG. 15B

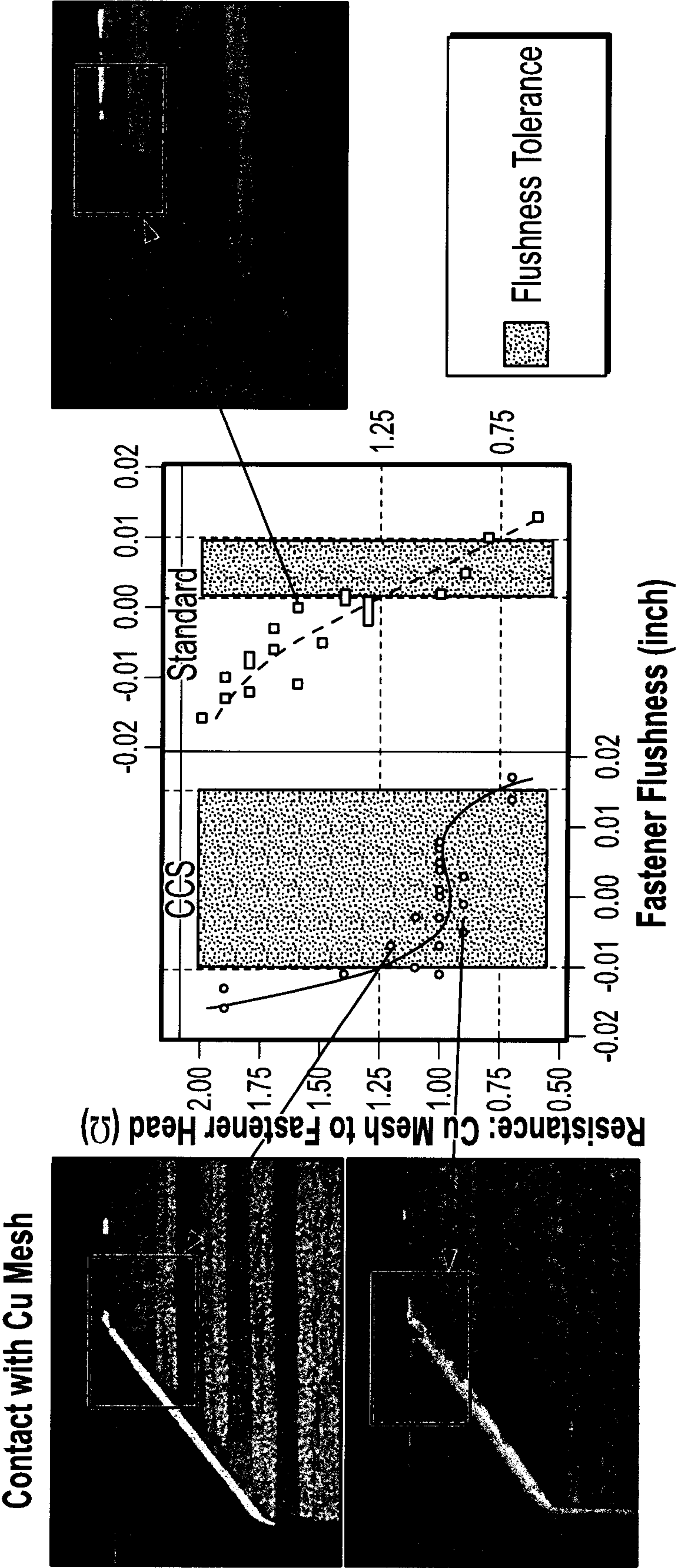
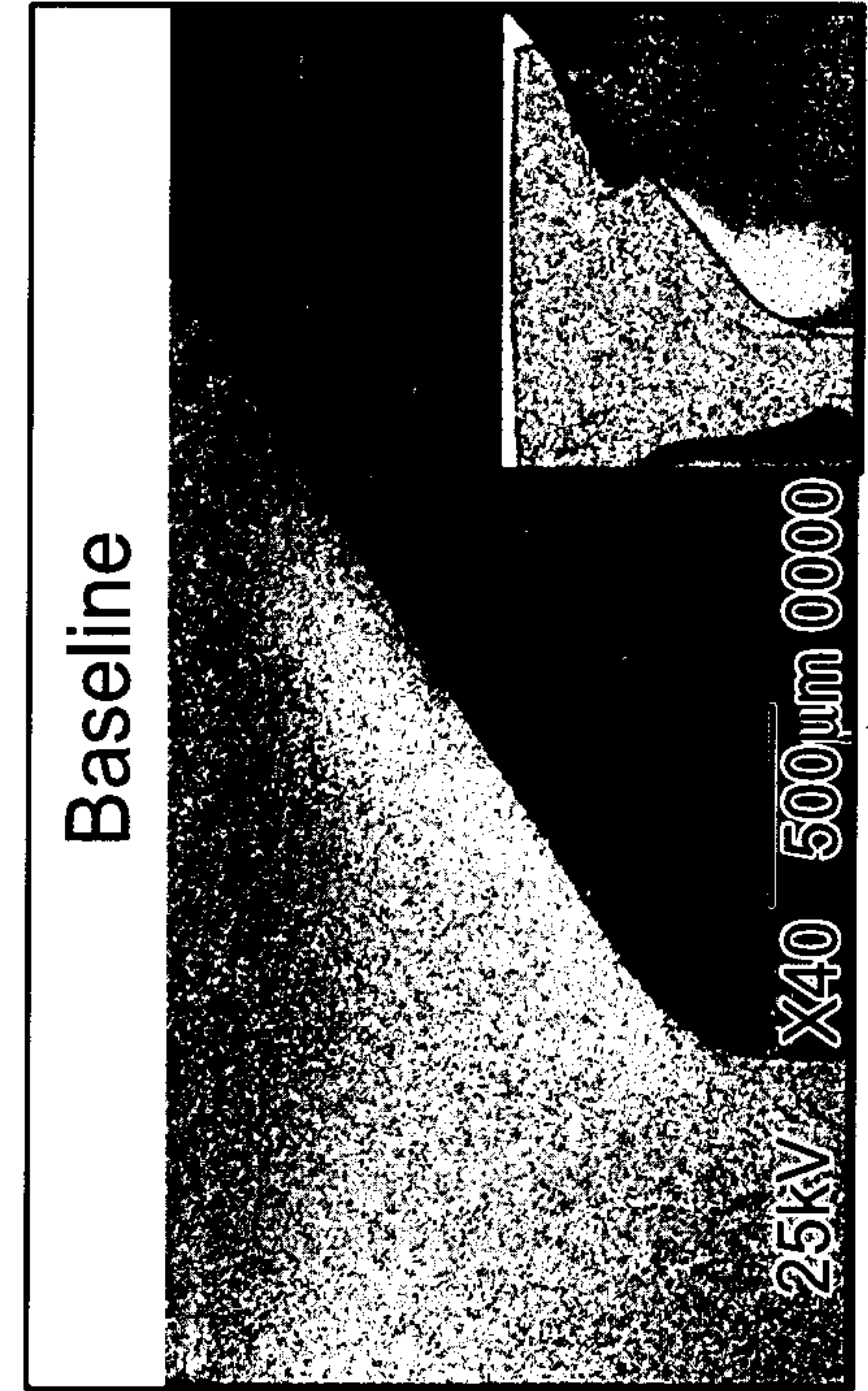
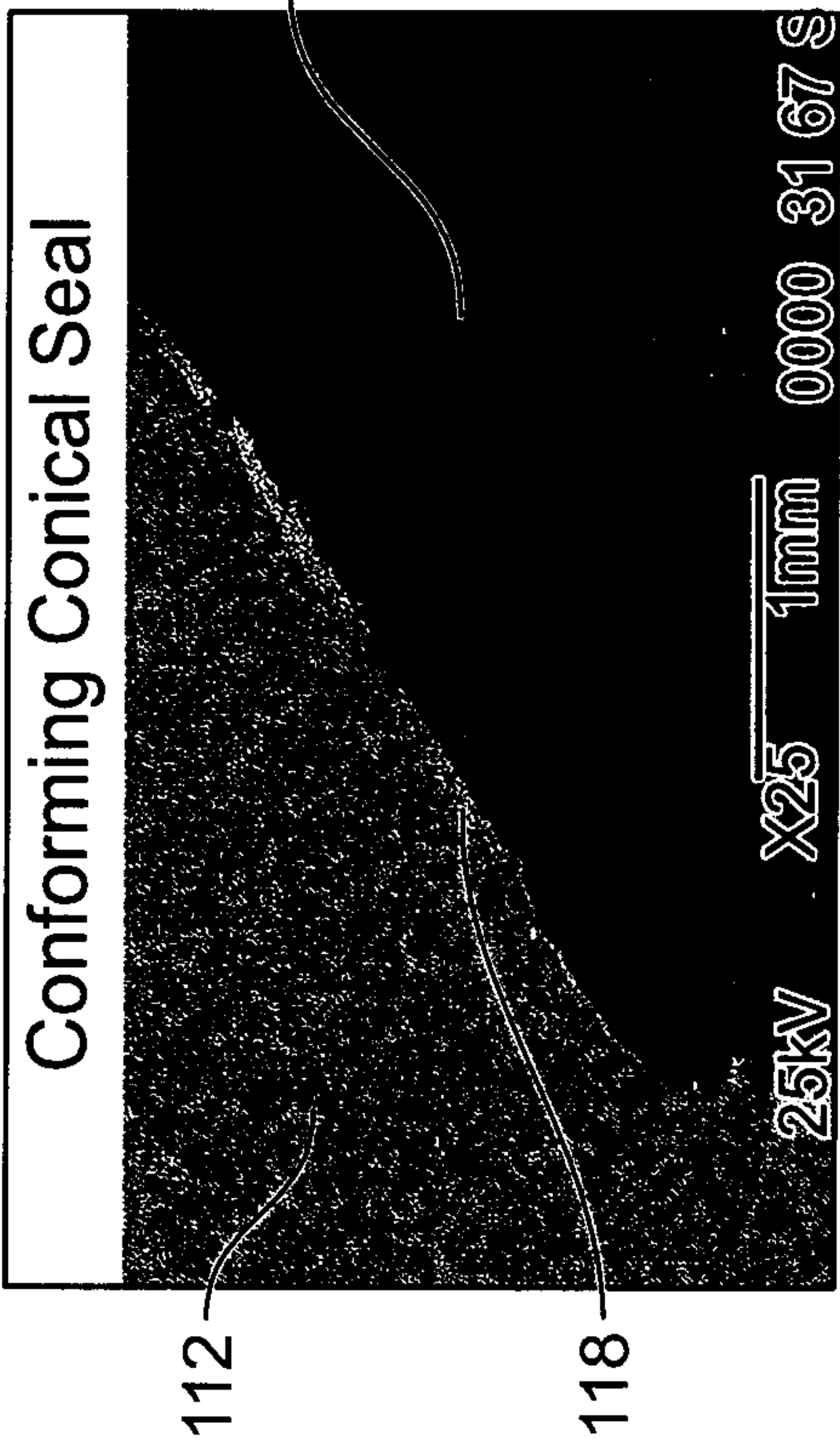


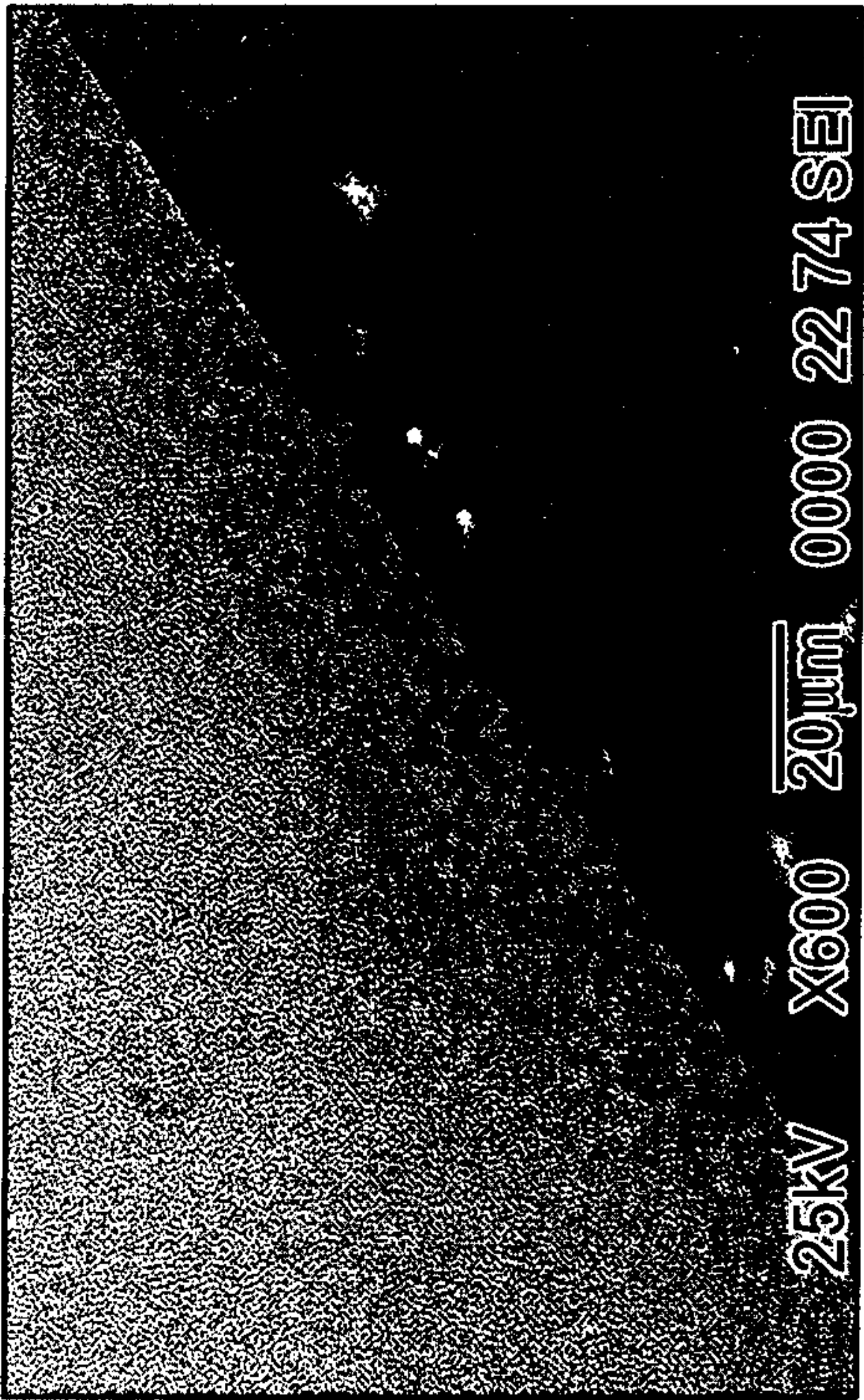
FIG. 15C



Conventional Pin Member at 40X
FIG. 16A



Pin Member with Seal Element at 25X
FIG. 16C



Conventional Pin Member at 600X
FIG. 16B



Pin Member with Seal Element at 1000X
FIG. 16D

Fastener with Seal Element

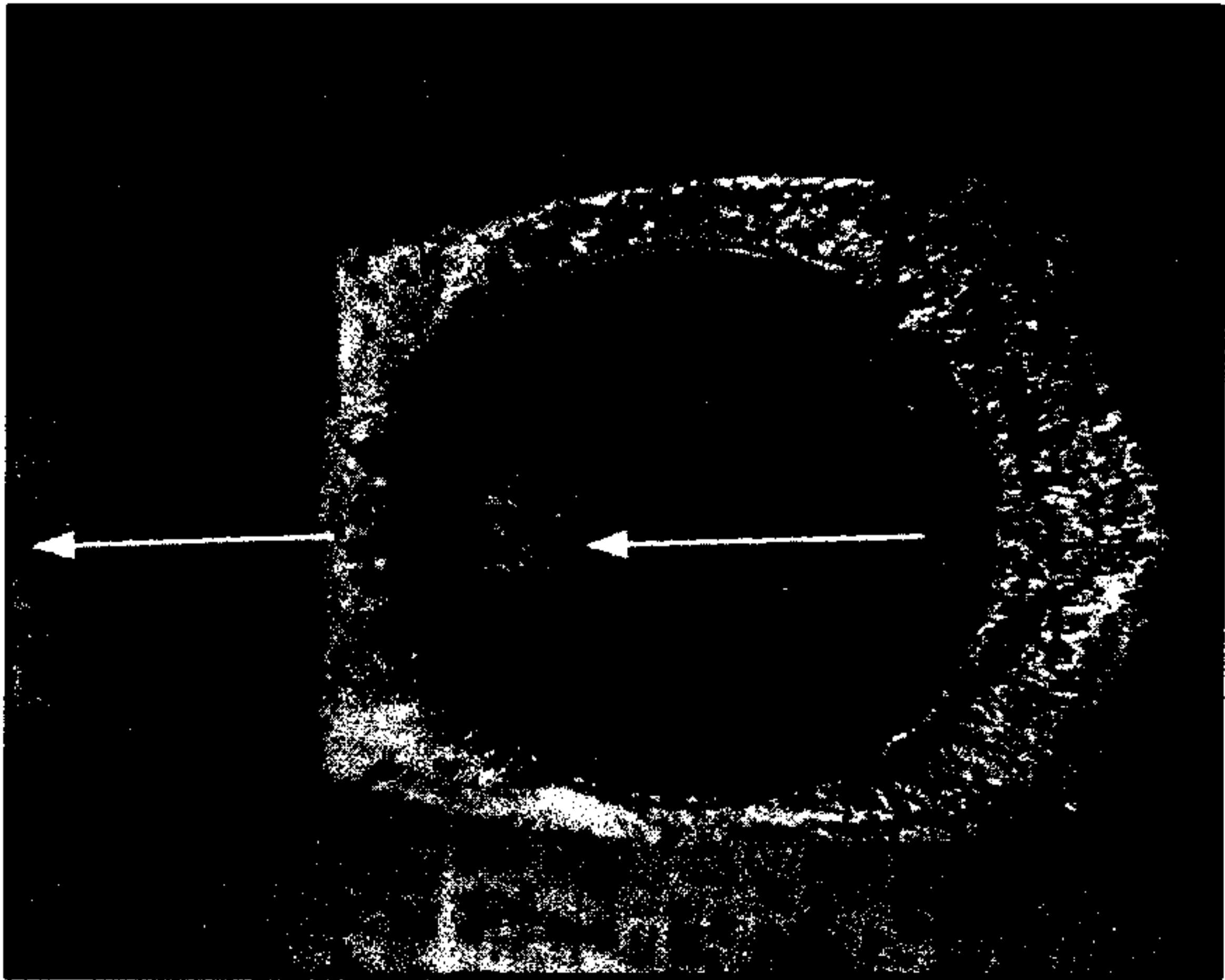


FIG. 17B

Standard Fastener

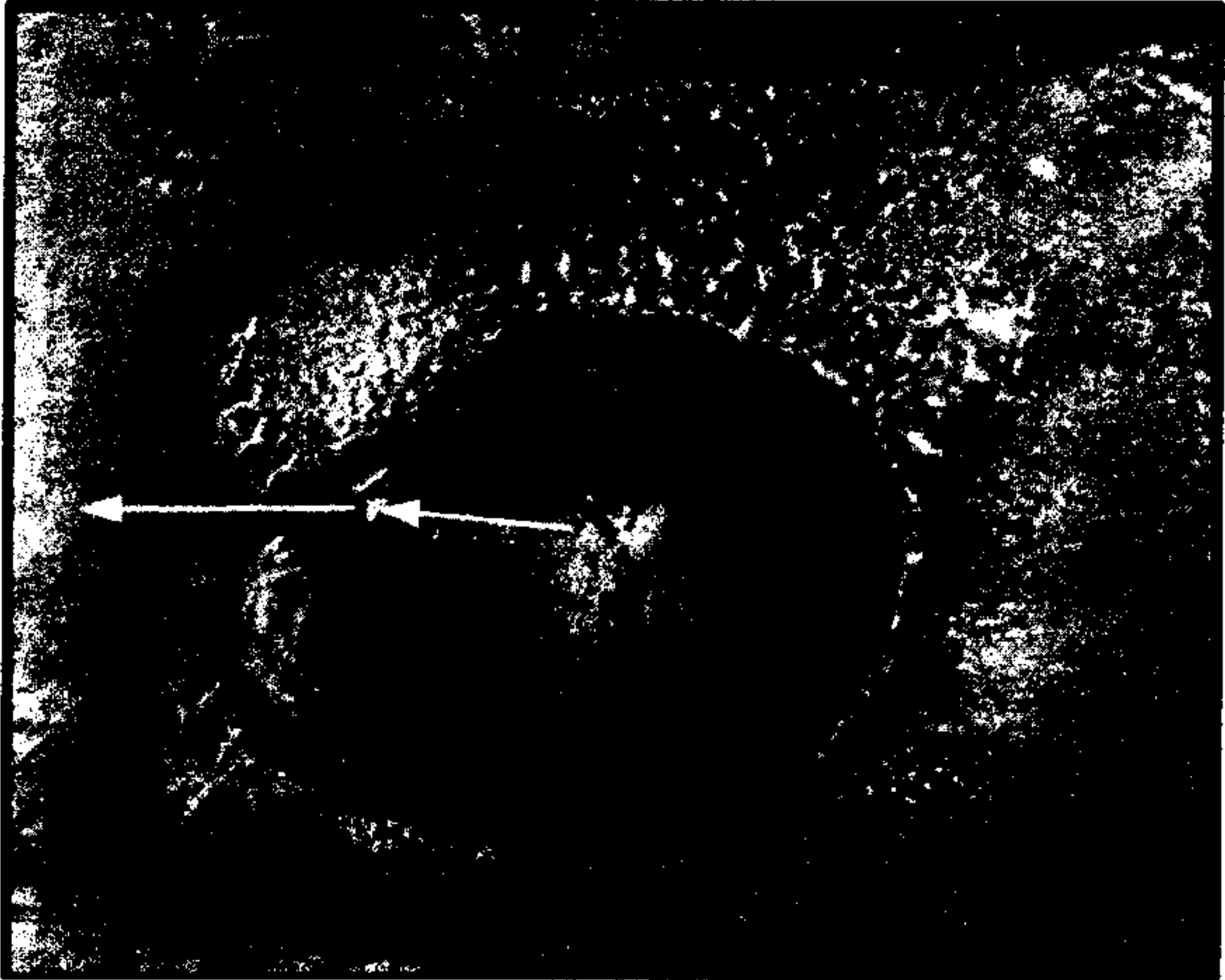
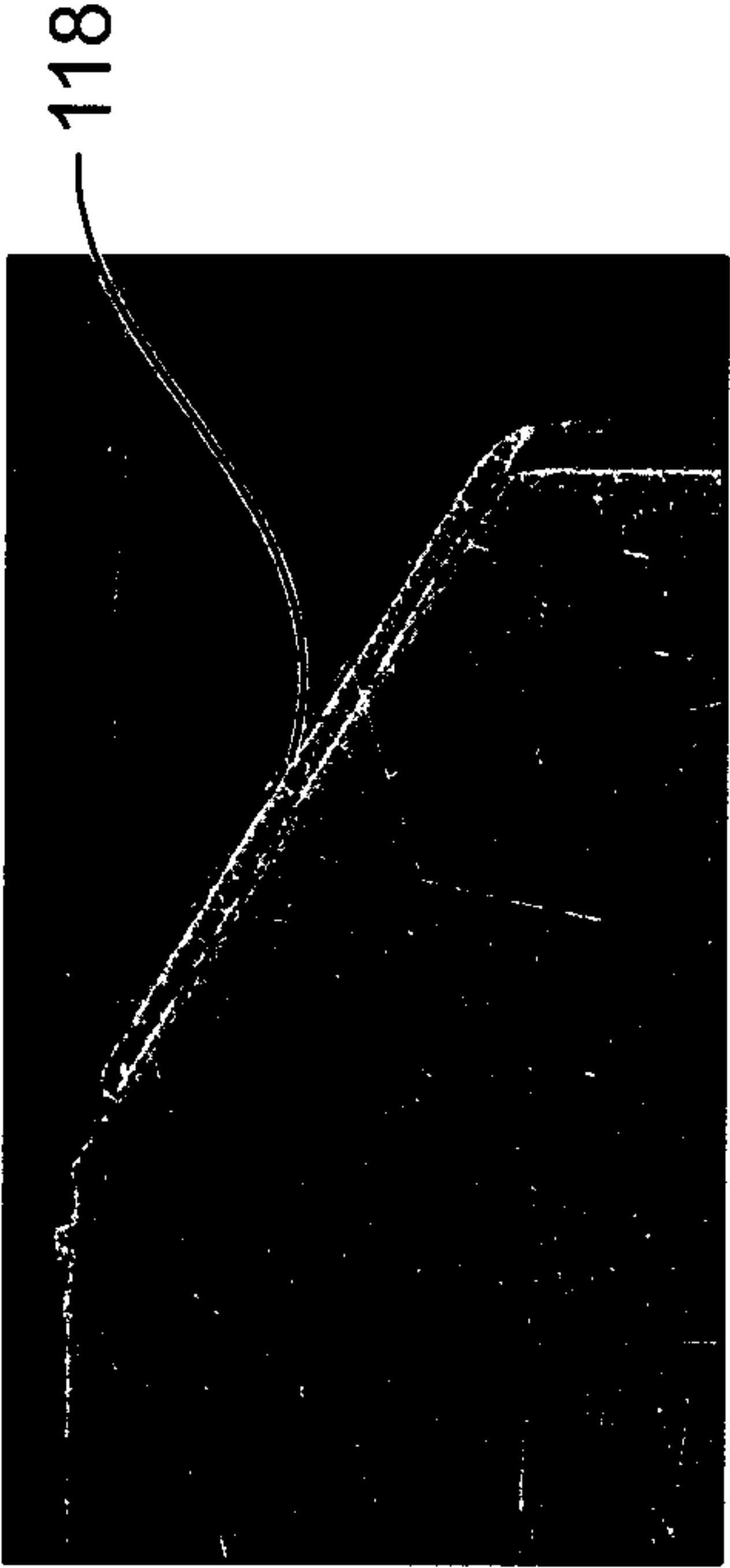
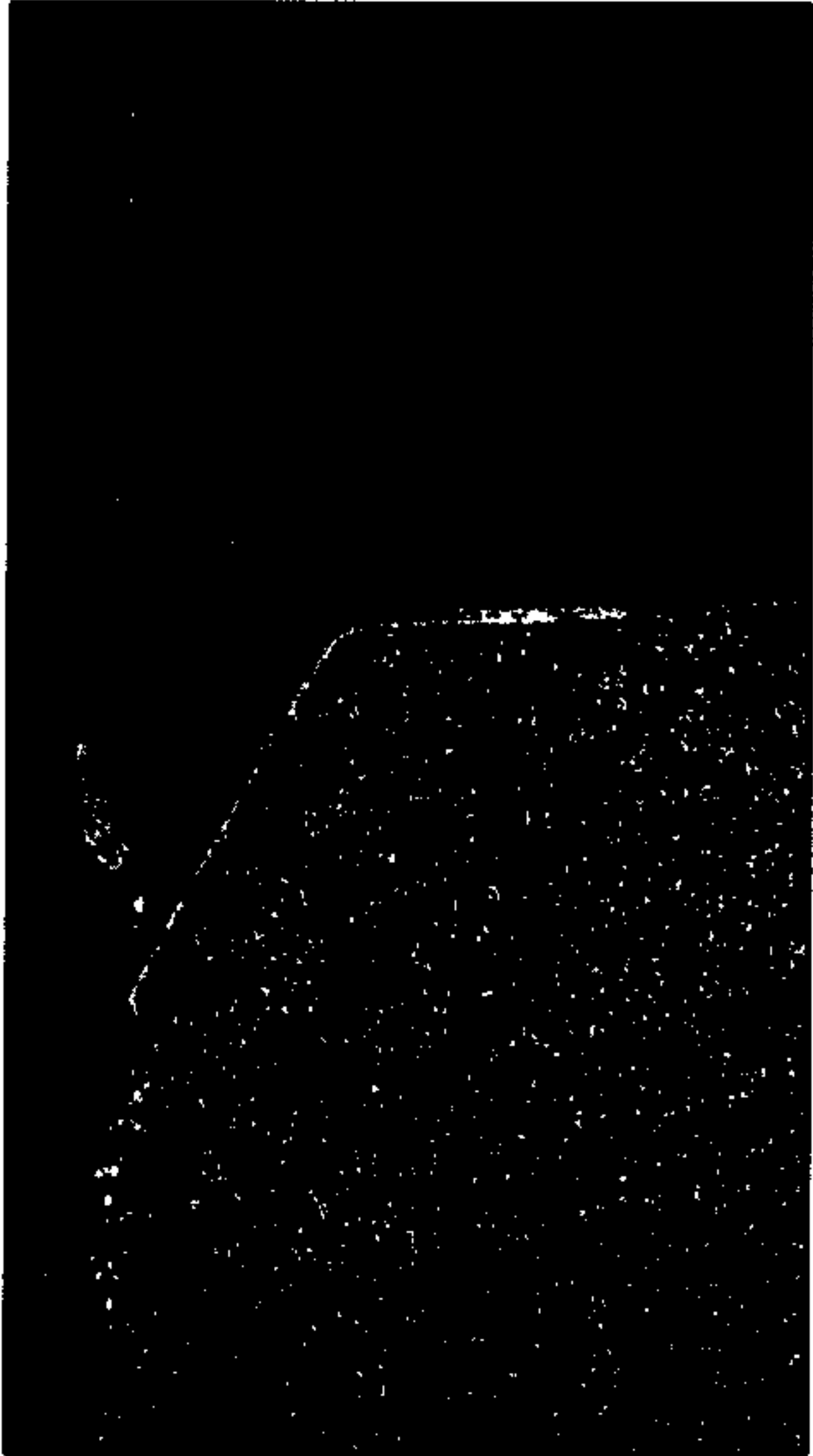


FIG. 17A



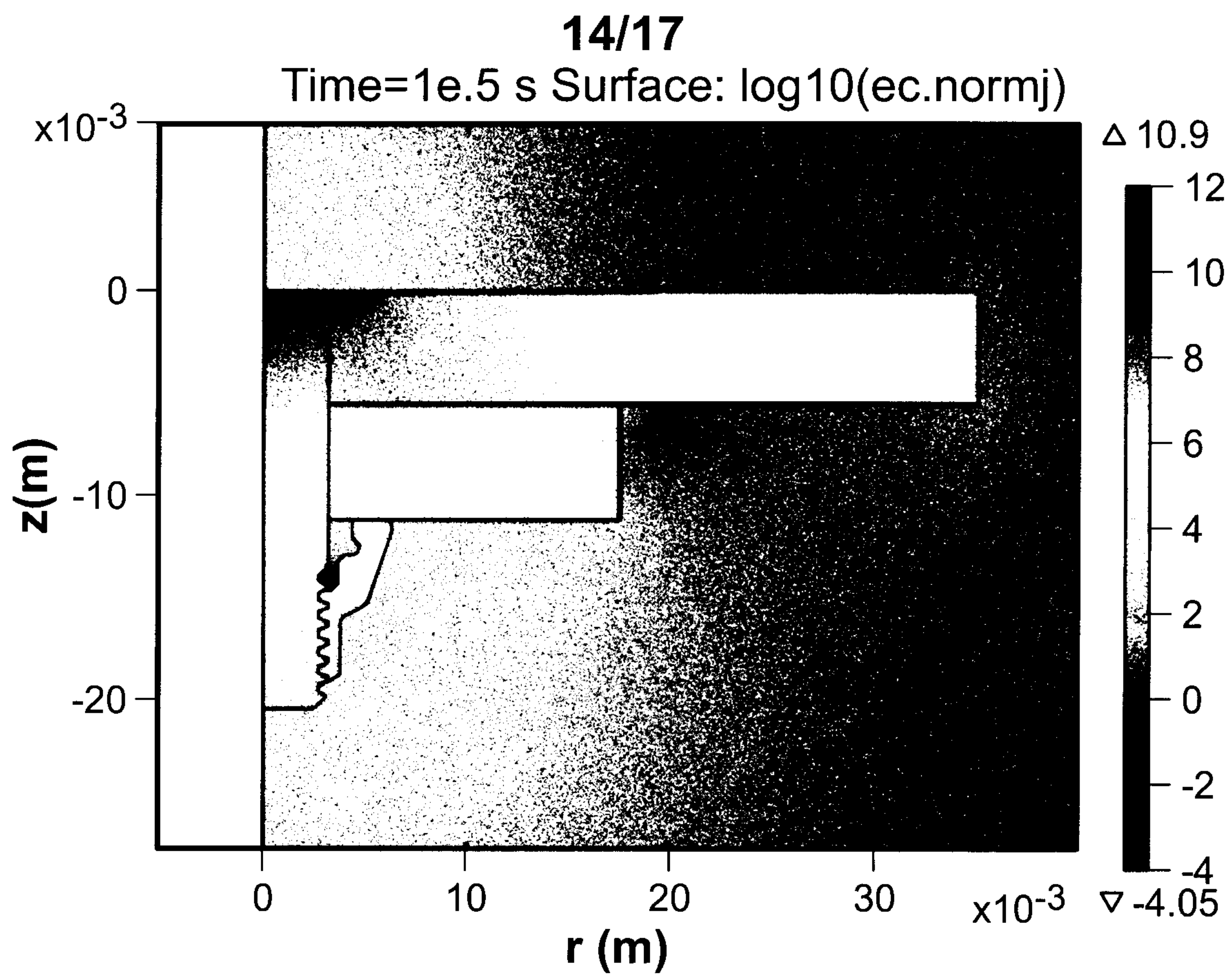
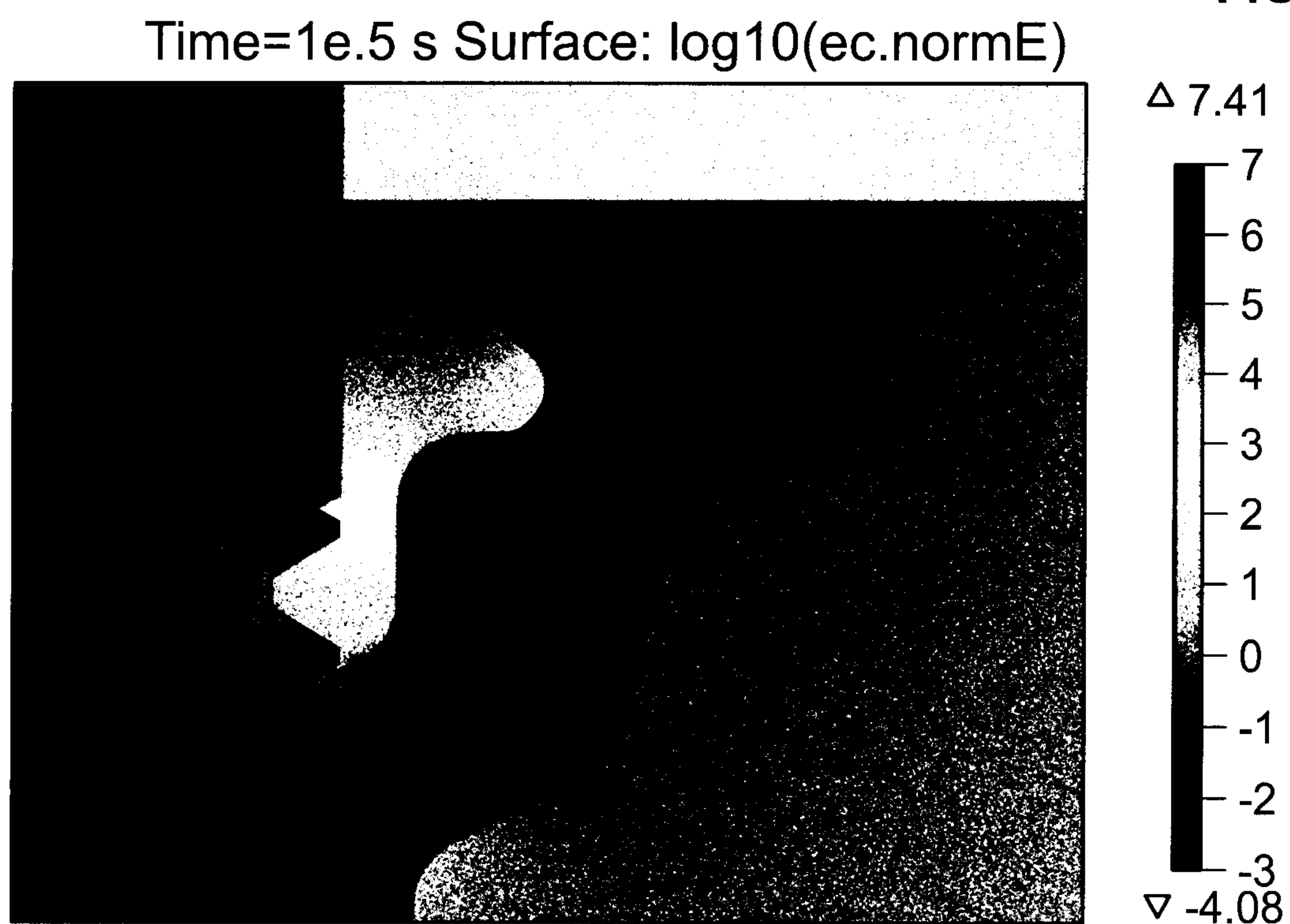
With Seal Element

FIG. 17D



Without Seal Element

FIG. 17C

**FIG. 18A****FIG. 18B**

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Time=1e.5 s Surface: log10(ec.normE)

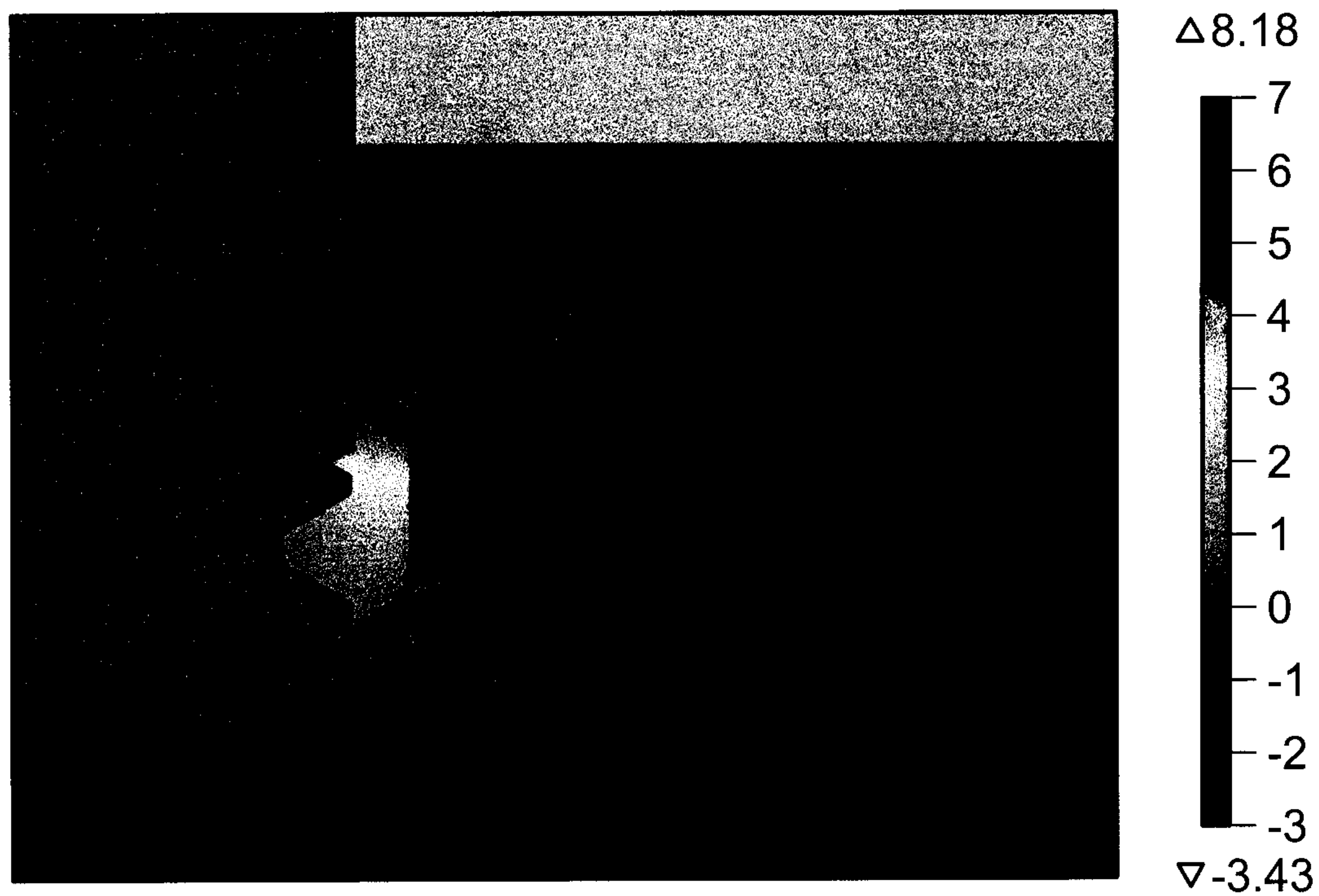


FIG. 18C

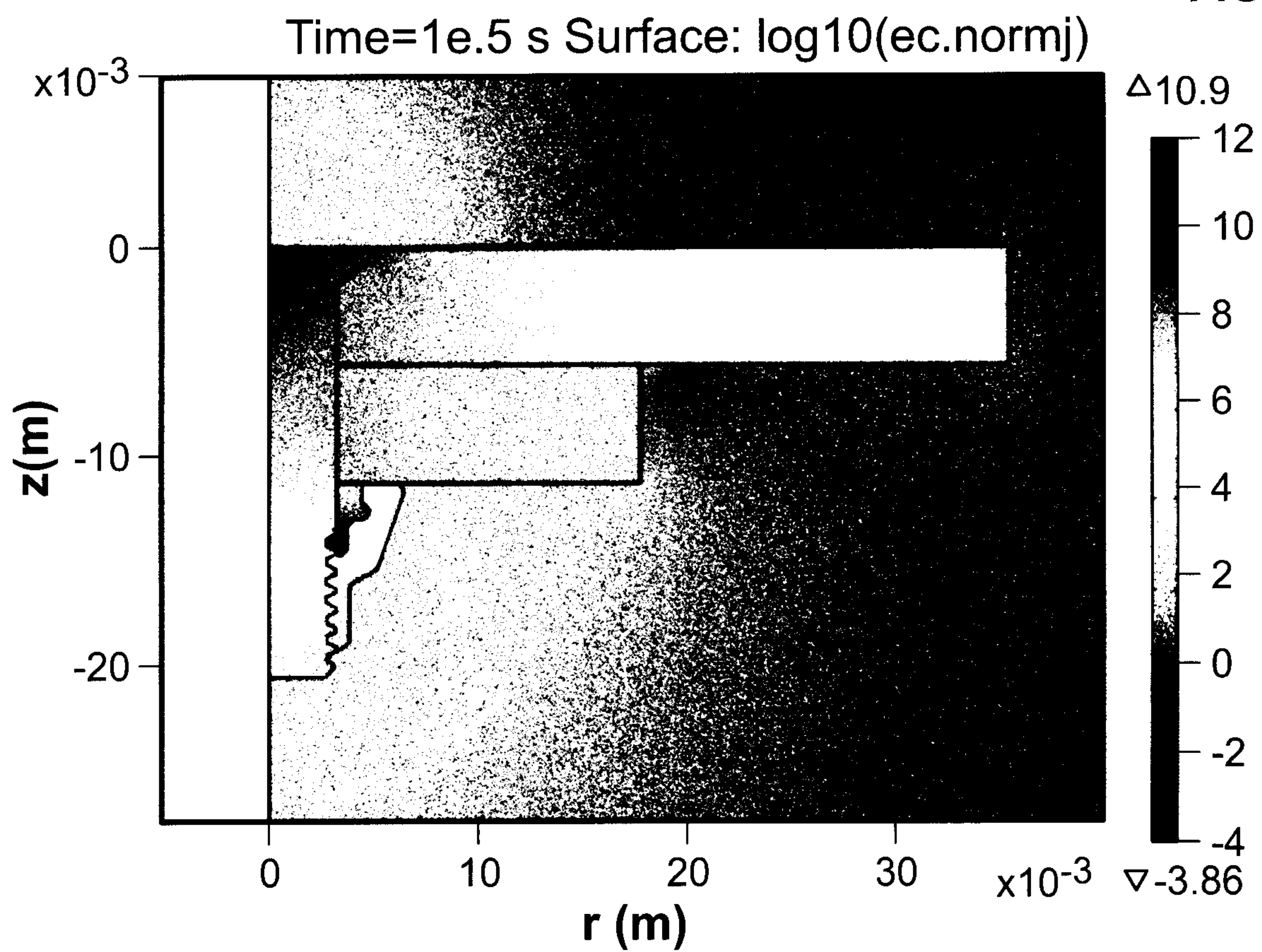


FIG. 18D

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Time=1e.5 s Surface: log10(ec.normE)

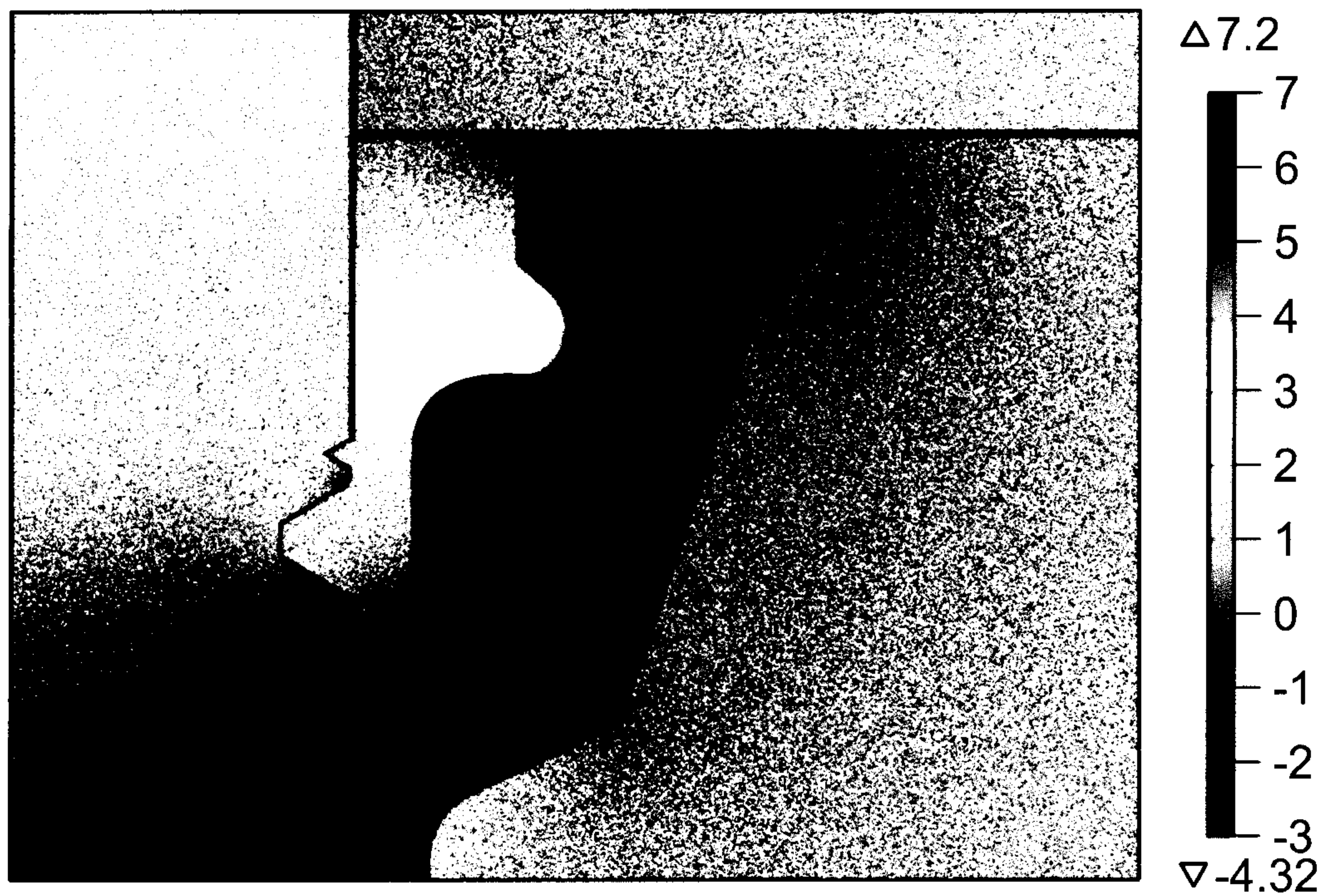


FIG. 18E

Time=1e.5 s Surface: log10(ec.normE)

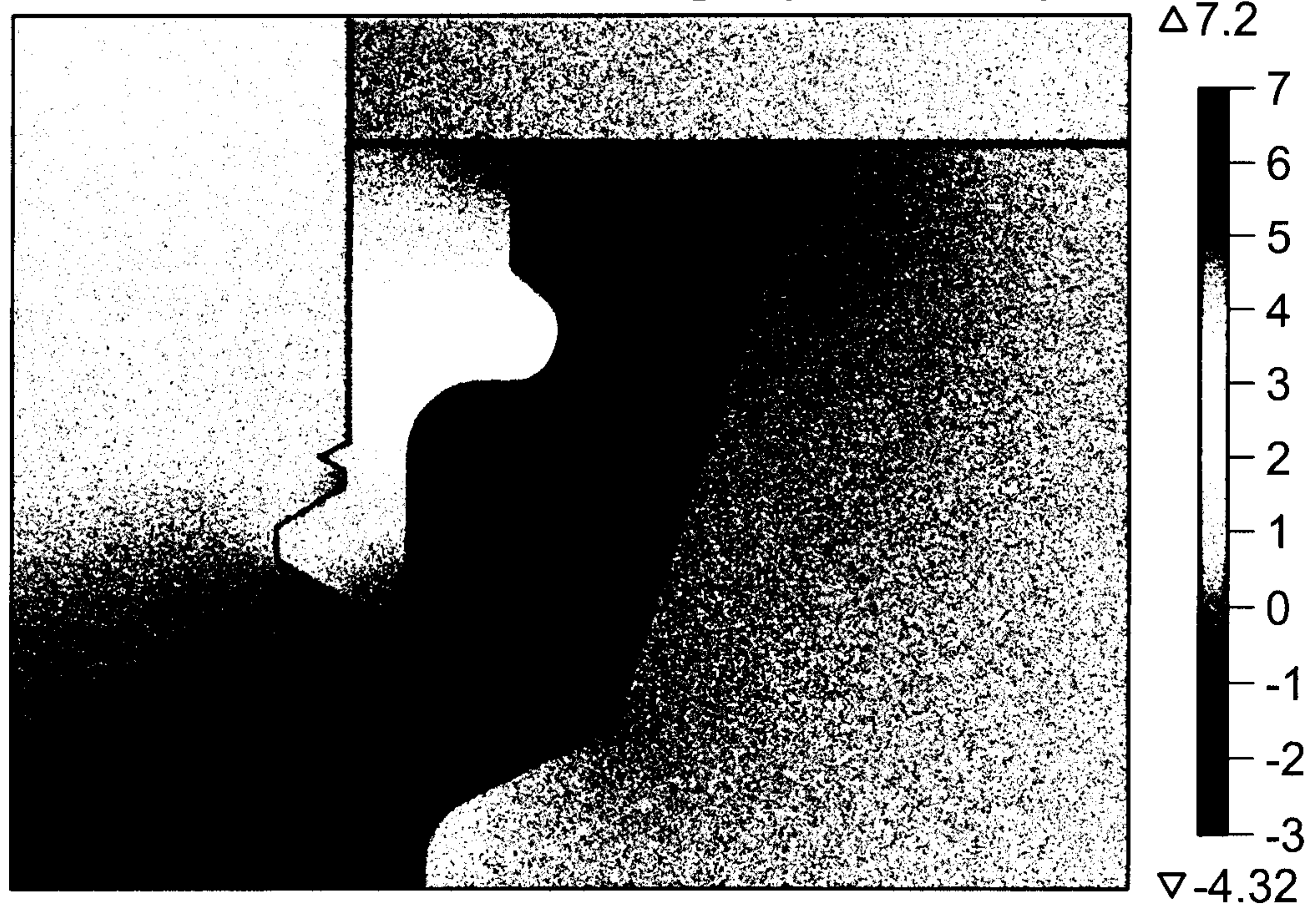


FIG. 18F

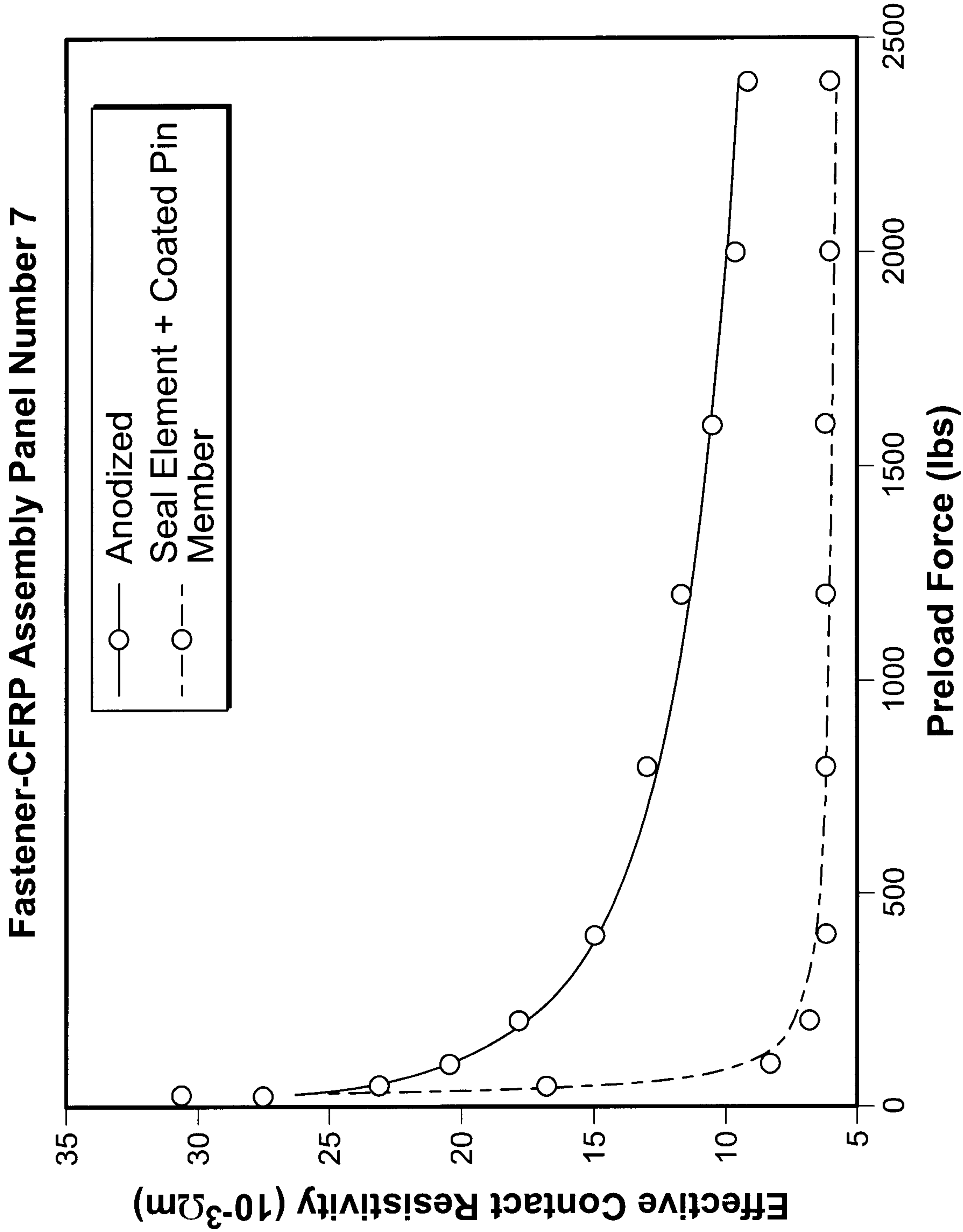


FIG. 19

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