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(54) Title: METHOD OF MAKING GOLF CLUBS USING METAL POWDER AND A HIGH ENERGY SOURCE
(57) Abstract: A method for making golf club heads includes using direct metal laser sintering (DMLS), selective laser melting (SLM) and other computer controlled high energy sintering or melting techniques to form club heads with customized user parameters. The powdered metals can be selected by type and quantity to achieve a desired density or weight distribution. Club heads made by these techniques are characterized by having customized parameters chosen by the user. By sintering powdered metal to form areas of different porosity, club heads with desired weight distributions can be achieved.

FIG. 1
METHOD OF MAKING GOLF CLUBS

FIELD OF THE INVENTION

The present invention relates to methods of making golf club heads, and more specifically, to a method of making iron type golf club heads using powdered metal rather than conventional metal forgings or castings.

BACKGROUND OF THE INVENTION

Golf clubs are formed through a variety of methods. Commonly, a golf club head is forged or cast and then machined or ground and polished to the requisite dimensions and desired aesthetic quality. These processes have proven to be time consuming and inefficient.

In addition, golf clubs are typically manufactured to fit an average person of average dimensions. Thus, the same club is manufactured regardless of the particular golfer's needs. This standard approach to golf club manufacturing is utilized due to the expensive and time consuming process associated with altering or manufacturing a new mold to incorporate changes in club design. Therefore, in order to save time and money, manufacturers use the same mold that is not readily adjustable with respect to the particular characteristics of the golf club. However, this presents a problem due to the fact that not all golfers are built the same, and not all golfers have identical swings. In addition, due to manufacturing tolerances, many golf clubs that claim to be a particular lie, loft, or face angle may be off by as much as 1°. Due to the variety of golf swings, golfers, and manufacturing flaws and/or tolerances, each individual golfer may benefit from an optimization of lie angle, loft angle, or other club head design parameter.

The lie angle of any golf club is the angle formed between the center of the shaft and the ground line of the club when the club is soled in its proper playing position (address position). Therefore, a taller golfer is likely to benefit from an increase in lie angle, which would allow for the golfer to comfortably address the ball properly. In a similar fashion, a short golfer would probably benefit from a reduction in lie angle.

Loft angle is a measurement, in degrees, of the angle at which the face of the club lies relative to a perfectly vertical face. Using a club with a high loft angle will typically
result in a golf shot with a high initial trajectory. In contrast, utilizing a club with a low loft angle will typically result in a golf shot with a low initial trajectory.

Currently, manufacturers rely on post-manufacturing methods for custom fitting golf clubs, the majority of which involve placing the club in a vice and bending the metal until the desired specifications are met. However, frequent modifications or improper bends may result in fatigue of the metal or weakening of the club head.

Finally, due to manufacturing tolerances, current methods of manufacturing frequently require additional steps to bring the club close to the desired specifications. For example, a club head that is designed to have a loft angle of 9° may be manufactured with a loft angle of 8°. Therefore, the additional step of bending the hosel is necessary to achieve the desired loft angle.

As such, there remains a need in the art for a method of manufacturing golf clubs that allows implementation of design variations while maintaining efficiency and cost effectiveness. In addition, there remains a need for a method of manufacturing golf clubs that allows a designer to create a golf club near specifications thereby reducing the need for finishing or bench work.

**SUMMARY OF THE INVENTION**

The present invention relates to a method of making a golf club head by applying a controlled source of energy to a powdered metal to form a golf club head. The method includes selecting a club design, selecting at least one design parameter, providing a powdered metal, and applying a controlled source of energy to the powdered metal to form a golf club head having a desired design parameter.

The controlled source of energy may include a direct metal laser sintering (DMLS) system, a selective laser melting system, an electron beam melting apparatus, or similar apparatus.

The club design may be selected from a parametric CAD file and then altered according to the designer’s specifications. Alternatively, the club design may be selected from a library of CAD files.

The designer may select from a wide range of parameters to customize a golf club head. For example, the designer may select any of the following parameters: weight,
weight distribution, bounce angle, lie angle, offset, loft angle, shape, hardness, sole camber, sole width, cavity undercut, center of gravity, face height, hosel outer diameter, hosel inner diameter, hosel taper, hosel) depth, toe height, groove width, groove depth, and groove shape.

According to another aspect of the invention, the powdered metal may be used alone or in combination with another powdered metal. Powdered metals suitable for use in the invention include, but are not limited to steel, stainless steel, iron, copper, bronze, aluminum, tungsten, titanium, titanium alloy, chromium-cobalt alloy, and combinations thereof.

In one embodiment, a first powdered metal may be used for a first portion of the club head, and a second powdered metal may be used for a second portion of the club head. The first powdered metal may have a density that is greater than the density of the second powdered metal. For example, the first density may be greater than the second density by about 5 g/cm³. In addition, the first density may be greater than about 10 g/cm³. Alternatively, the first density may be greater than about 7 g/cm³.

In one embodiment, the density is controlled by controlling the porosity of portions of the club head. For example, a first portion may be made of a sintered metal having a first porosity, and a second portion may be made of a sintered metal having a second porosity. The porosity of the first portion may be greater than the porosity of the second portion, which results in a lower density for the first portion.

The low density first portion may occupy about 1% to about 99% of the entire volume of the club head. Alternatively, at least 95% of the total volume of the golf club head is formed from the low density first portion. The porosity of the low density first portion may be about 99% porosity to about 1% porosity. In another embodiment, the low density first portion has a porosity that is greater than about 90%.

**BRIEF DESCRIPTION OF THE DRAWINGS**

Further features and advantages of the invention can be ascertained from the following detailed description that is provided in connection with the drawings described below:

**FIG. 1** is a front view of an iron type club head of the present invention;
FIG. 2 is a rear view of a cross section of a club head of the present invention;
FIG. 3 is a rear view of a club head of the present invention;
FIG. 4 is a cross sectional view of a club head of the present invention taken
along 1-1 of FIG. 3;
FIG. 5 is a cross sectional view of a club head of the present invention taken
along 1-1 of FIG. 3;

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The present invention is directed to a process for manufacturing golf clubs using
an additive process. For example, powdered metal sintering and metal deposition are
suitable processes for use in the present invention. The process may be used to
manufacture any type of golf club head including, but not limited to: irons, woods,
putters, utility clubs, and wedges.

Powdered metal sintering systems involve a bed of metal powder that is sintered
or melted layer by layer by a laser or electron beam to create metal parts. After the part
has been created, the surrounding powder can be brushed away or shaken out of the part.
In addition, a variety of metal powders can be melted in these systems. There are a
number of commercially available systems suitable for use in the present invention. For
example, the "MCP Realizer", a selective laser melting system, which is the product of
Mining and Chemical Products Limited of Germany, can create parts from any number of
metals including the following powders: zinc, bronze, stainless steel, titanium,
chromium-cobalt, silicon carbide, and aluminum oxide. In addition, various machines
from EOS of Germany are available that rely on direct metal laser sintering (DMLS).

ARCAM of Sweden produces machines that rely on electron beam melting (EBM)
technology.

Direct Metal Laser Sintering (DMLS) has recently emerged outside the golf
industry as a way of manufacturing metal parts. The DMLS process involves using a
laser that fires into a layer of powdered metal guided by a computer program. DMLS is
an "additive" technology that sinters very fine powders layer by layer from the bottom up
until the product is completed. The process begins by the input of 3-D CAD files and, a
control program converts the CAD files into instructions for controlling the layer by layer
formation of the metal parts. The layer by layer formation is accomplished by laser
sintering a 'first layer' of approximately 20 to 40 micron powder onto a steel platform.
The platform then lowers by approximately 20 to 80 microns, a fresh layer of powder is
swept over the previously sintered layer, and the next layer is sintered or added on top of
the previously built one. The additive process is repeated until the desired part is
complete.

Metal deposition systems use a 3D printing process to create metal parts in a
similar manner to how ink is deposited from print heads on an inkjet printer. Multiple
heads can be incorporated into these systems to increase the production speed. Metal
deposition systems are currently available from FCUBIC AB of Sweden and ProMetal,
LLC of Troy, Michigan. This process may be used to create a solid part with uniform or
non-uniform material properties or to add layers of powdered metal to an existing
substrate. For example, a metal deposition device may be employed to coat a portion of a
surface of a golf club head with a material that has a high density in order to alter the
center of gravity or other design specification of the golf club head.

The general procedure that applies to all machines is to design a part in a 3-D
CAD application, convert the CAD file to an STL file, and then transfer the STL file to
the machine for processing. "STL" stands for stereolithography; and is a file format that
is widely used to describe the shape of a three dimensional object. This file format is
supported by many software packages and is widely used for transferring CAD models to
rapid prototyping and direct manufacturing machines.

There are several advantages to powdered metal sintering production. For
every example, batch size and batch configuration, or mixing different quantities of each part
depending on the demand for each part, is easily adjustable without significantly
affecting part cost. This is a direct result of the ability of the process to rapidly
implement production of a new part by merely altering a CAD file or selecting a new
CAD file. This is in contrast to parts created from tools for which it is necessary to
accurately forecast the quantities of each part so that the appropriate number of tools will
be made.
In addition, design time can be reduced by creating functional prototypes directly from the CAD model. Eliminating the need for prototype tooling can reduce the time before prototype designs can be tested for performance, durability and appearance. The development and production time can be shortened for a design by eliminating or reducing the need for other manufacturing processes. For example, DMLS is more efficient than the casting process, because DMLS eliminates the time for creating tools, wax preparation, creating ceramic shells, pouring metal into shells, breaking shells, cutting parts off of casting trees, and grinding off parting lines and weld beads. Further, the process is capable of implementing changes in design without the need to alter or manufacture a new tool or mold. For example, a change in the design of a club head manufactured by a casting process requires the precise modification of the mold or the production of an entirely new mold. This is a time consuming and expensive process. By contrast, the powdered metal sintering process merely requires the changes to be made to a CAD file, and the process will manufacture the club head based on the CAD file.

Therefore, changes can be easily implemented by the designer without the need for a halt in production or the construction of new tools or molds.

DMLS and similar machines have further advantages over casting and forging in that DMLS can produce more consistent parts. Current manufacturing methods such as casting result in variation in part weight and size due to manufacturing tolerances and changes in environmental conditions, such as heat and humidity. Due to these inconsistencies, parts are intentionally created with extra size and weight so that they can be ground down to the proper specifications. Parts created on a DMLS machine can be created with more consistent size and weight. Since there is less hand finishing required, parts can be created closer to the net finish size, and fewer adjustments need to be made to account for the manufacturing processes. Part size can be adjusted to match the design model by properly calibrating the DMLS machine. In addition, since powdered metal sintering is an additive process, there is a significant reduction in waste resulting from material that must be cut away after molding or forging.

It is also possible to use the DMLS process to create tooling for conventional processes such as casting, forging, stamping, and injection molding. This tooling can be
created directly from the CAD data and does not require programming that is needed for machined tools.

In addition, an additive process such as DMLS can create undercuts or internal channels in tools which would be impossible or difficult to do with a CMC machine.

Undercuts and other features may require the use of a support structure, which may be made using an additive process or other known methods. Upon formation of the undercut, the support is removed by a known method. For example, the support may be formed from a polymer material and subsequently heated to remove.

10 **Materials**

Suitable materials for use in the process are powdered metals composed of particles with an average diameter of less than about 40 microns. Preferably the average diameter is less than about 25 microns. Alternatively, the average diameter may be less than about 35 microns. The average diameter may be between about 30 and about 40 microns. The powdered metal can be any powdered metal available on the market capable of being sintered and includes, but is not limited to, 303 stainless steel, 304 stainless steel, 431 stainless steel, 432 stainless steel, iron, copper, bronze, aluminum, tungsten, chromium-cobalt alloy, titanium and titanium alloys, or similar materials and combinations thereof. The materials may also be combined with another material in order to vary the composition of portions of the club head to achieve a desired characteristic for a particular portion. For example, 303 stainless steel may be used for the body portions of the club head including the top line, heel, toe, and sole portions of the club and a titanium alloy may be used to produce the face portion of the club head.

25 **Powdered Metal Sintering**

The process includes selecting a set of design parameters to match specifications of a specific golfer, providing a powdered metal, and applying energy to the powdered metal to form the club head. In one embodiment a powdered metal sintering process, such as DMLS, is used to form a club head. Initially, the designer inputs a design from a CAD file. However, the system may include a library of existing CAD files or a parametric CAD file that can be modified by inputting a set of new design parameters. The
parametric CAD files include a basic shape of the club head, and the designer selects from a list of parameters to customize the club accordingly. The parameters may include, but are not limited to: density, weight distribution, bounce angle, lie angle, offset, loft angle, hardness, sole camber, sole width, cavity undercut, center of gravity, face height, hosel outer diameter, hosel inner diameter/taper, hosel depth, toe height, groove width, groove depth, and groove shape, or combinations thereof.

Referring to Fig 1, a club head 10 of the present invention has a typical iron type club head shape that includes hosel 12, sole 15, heel 14, and toe 16. A ball striking face 18 has a plurality of parallel, horizontally disposed grooves formed in the surface of the face 18. A lie angle 20 is defined by the center line (CL) of hosel 12 and the horizontal plane (GP) on which the club rests when addressing the ball. The lie angle, in conventional club manufacturing processes, is set when the clubs are forged or cast, and in general, the factory set lie angle is suitable for some golfers, but not all. In forged and cast clubs, the hosel must be bent relative to the remainder of the club head to change the lie angle to suit a particular golfer. In the present invention, the lie angle is one of the parameters that can be customized for each club head of each set to suit the specifications of an individual golfer. Similarly, the bounce angle is defined by the horizontal plane and the line of the sole of the club head next to the club face. This angle can also be adjusted by custom fitting steps, in the prior art, after forging or casting. In the present invention, the bounce angle is another parameter that can be customized for an individual golfer without subsequent processing steps, such as bending, grinding or otherwise working the metal which comprises the club head.

A particularly useful aspect of the powdered metal sintering process is the ability to control the density of various portions of the club head. Varying the density of certain portions of the club head allows the designer to distribute mass throughout the club head in order to control characteristics of the club head such as the center of gravity and moment of inertia. Density control may be accomplished in a variety of ways.

In one embodiment, the process uses at least two different powdered metals or alloys to form the club head. Regions of higher and lower density material, or regions of different materials, can be used to change the center of gravity of the club head, or otherwise redistribute weight in a manner intended to improve payability of the clubs.
Referring to Fig. 2, a region of low density material 26 is formed in the topline, heel, and upper toe portions of the club head, and a region of high density material 28 is formed in the lower portion of the club head, thereby achieving a lower center of gravity.

Although, Fig. 2 only shows one orientation of density distribution, the high and low density portions may be distributed in a variety of ways to achieve a desired specification. For example, a material with a high density may be used in one or more "heavy" portions, and a material with a low density may be used in one or more "light" portions. The heavy portions may be formed from a material with a density greater than about 1 g/cm³. According to one aspect of the invention, the heavy portions may be formed from a material with a density greater than about 3 g/cm³. In one embodiment, the heavy portions may be formed from a material with a density greater than about 7 g/cm³. In one embodiment, the heavy portions are formed from a material with a density greater than about 10 g/cm³. In another embodiment, the heavy portion is composed of a material with a density that is greater than about 15 g/cm³. In addition, the heavy portion may have a density that is greater than the light portion(s) by at least about 1 g/cm³. In another embodiment, the heavy portion has a density that is greater than the light portion by about 3 g/cm³. The heavy portion has a density that is greater than the light portion by about 5 g/cm³. Alternatively, the material of the heavy portion may have a density that is greater than the material of the light portion by about 10 g/cm³.

In another embodiment, the density of various portions of the club head is controlled by varying the porosity of the sintered metal. Porosity is a measure of the void spaces in a material, and is measured as a fraction, between 0-1, or as a percentage between 0% – 100%. For example, by controlling the amount of powder, it is possible to control the density, in terms of porosity, of the particular powdered metal used in the process. Typically, when a metal part is manufactured, it is expected that the finished product has approximately 0% porosity, with limited inclusions.

By using the formation methods of the present invention, it is possible to change the porosity of the material, layer by layer, area by area, to achieve a desired density. This is accomplished by varying the amount of powdered metal used for certain areas of the club head. A reduction in the amount of powder used for a particular layer results in a layer with a greater porosity and a lower density.
Referring to Fig. 3, a club head 10 has a hosel 12, a heel 14 and toe 16. A sole 15 extends between the heel 14 and toe 16. The rear surface 48 is shaped to have a centrally located low density portion 46 surrounded by a higher density portion 48. In effect, club head 10 behaves similar to a cavity-back type club because the orientation of low density portion 46 allows for mass to be freed up and distributed towards the perimeter of the club head. This orientation leads to an increase in the moment of inertia (MOI) of the club head. Inertia is a property of matter by which a body remains at rest or in uniform motion unless acted upon by some external force. MOI is a measure of the resistance of a body to angular acceleration about a given axis, and is equal to the sum of the products of each element of mass in the body and the square of the element’s distance from the axis.

Thus, as the distance from the axis increases, the MOI increases, making the club more forgiving for off-center hits. In addition, moving or rearranging mass to the club head perimeter enlarges the sweet spot and produces a more forgiving club.

For example, the porosity and the density may be altered using a DMLS process. The process may be programmed to space lines of material placed on a substrate to form a layer. The program may allow for a wide space between the lines, which results in a layer formed from less powder. This process forms a layer with a high percentage of porosity and low density. By contrast, a layer may be formed wherein the DMLS process is programmed to place little or no space between the lines. The lack of space between the lines results in a layer that is formed with a low porosity and a high density. Fig. 5 shows an example of the interior of a club head where spaces (66) and lines of material (68) form the interior of a club head.

Another method of increasing porosity is to program the process to leave pockets or voids where no material is placed on the substrate. Fig. 4 shows the interior of a club head where voids 56 contain no material.

In one embodiment, voids or spaces are formed by programming a process as outlined above. The voids may be interconnected throughout the club head. Next, one or more of the voids or spaces are filled with a light weight polymer or other low density material. Alternatively, the interior of the club head may comprise a skeleton or frame made with a high porosity. A low density material may then be injected to fill the areas in
and around the frame. The low density material may have a density that is less than about 1.3 g/cm³.

In one embodiment, a first amount of material may be used for the formation of layers for a first portion of the golf club head, and a second amount of material may be used for the formation of layers for a second portion of the golf club head. The first amount of material is less than the second amount of material, which results in a club head with a first portion that is more porous than the second portion. Therefore, the density of the first portion is less than the density of the second portion. This allows for a lighter overall structure, freeing up weight to optimize play characteristics of the golf club.

In one embodiment, the first portion may comprise about 1% to about 99% of the entire volume of the club head. The first portion may comprise about 5% to about 95% of the entire volume of the club head. In another embodiment the first portion may comprise at least about 95% of the total club head volume. In another embodiment, the first portion of the club head may comprise greater than about 85% of the total volume of the club head.

For example, the first portion may comprise the interior of the club head and the second portion may comprise only the surface of a portion of the club head. In one embodiment the surface of the club head is less than about 0.050 in. thick. Alternatively, the surface of the club head is less than 0.040 in. thick. In another embodiment, the surface is about 0.030 in. thick.

In addition, the porosity of the first portion may range from about 99% porosity to about 1% porosity. In one embodiment, the porosity of the first portion ranges from about 95% to about 5%. Alternatively, the porosity of the first portion may be greater than 90%. The porosity of the first portion may range from about 20% to about 80%. In another embodiment, a third portion may be formed that has a porosity that is greater than the first porosity, which results in a greater density for the first portion in comparison to the third portion.

In another embodiment, a hollow club head may be created using the powdered metal sintering process in combination with a conventional method. Portions of the club head may be made according to the process described above, and subsequently the
portions are joined by a welding process. For example, a front portion may include the
face and the sole, and a back portion may be welded to the front portion in a manner that
creates a hollow area between the front and back portion.

5 Metal Deposition

Another aspect of the present invention is to utilize a metal deposition process to
coat a substrate with powdered metal. For example, an existing part or club head may be
inserted into the metal deposition apparatus, to apply a coating material to be part of the
club head. This process may be used to apply a protective layer over parts of the club
that come into contact with objects. For example, the sole of the club may be coated with
a material that is harder than other parts of the club in order to prevent damage from
repeated impacts with the ground.

In one embodiment, the designer uses the metal deposition process to coat
selected portions to achieve a desired club attribute such as center of gravity, moment of
inertia, hardness, or other club characteristic. For example, a high-density material may
be deposited onto the heel portion of the club in order to move the center of gravity
toward the heel of the club.

By contrast, a low density substrate may be coated with a powdered metal. The
substrate may be a polymer or non-metallic in nature. For example, a low density
polymer can be coated with a powdered metal to form a club head. As a result, the club
head is made lighter and mass can be added to desired locations to achieve various
specifications such as moment of inertia, center of gravity, hardness, or other
characteristic.

In one embodiment, a portion of a substrate may be coated with a metallic coating
by utilizing a vapor deposition or chemical deposition process in combination with a
metal deposition process.

In addition, the modification techniques described for the powdered metal
sintering process are also applicable in the metal deposition process. Specifically, the
density, hardness, and weight distribution can be modified by utilizing powdered metals
of different densities and/or varying the porosity of the sintered metal.
Notwithstanding that the numerical ranges and parameters setting forth the broad scope of the invention are approximations, the numerical values set forth in the specific examples are reported as precisely as possible. Any numerical value, however, inherently contain certain errors necessarily resulting from the standard deviation found in their respective testing measurements. Furthermore, when numerical ranges of varying scope are set forth herein, it is contemplated that any combination of these values inclusive of the recited values may be used.

The invention described and claimed herein is not to be limited in scope by the specific embodiments herein disclosed, since these embodiments are intended as illustrations of several aspects of the invention. Any equivalent embodiments are intended to be within the scope of this invention. Indeed, various modifications of the invention in addition to those shown and described herein will become apparent to those skilled in the art from the foregoing description. Such modifications are also intended to fall within the scope of the appended claims. All patents and patent applications cited in the foregoing text are expressly incorporated herein by reference in their entirety.
CLAIMS

We claim:

1. A method of making a golf club head comprising the steps of:
   selecting a club design;
   selecting at least one design parameter;
   providing a powdered metal; and
   applying a controlled source of energy to the powdered metal to form a golf club head having the at least one design parameter.

2. The method according to claim 1, wherein the at least one design parameter is selected from the group consisting of weight, weight distribution, bounce angle, lie angle, offset, loft angle, shape, hardness, sole camber, sole width, cavity undercut, center of gravity, face height, hosel outer diameter, hosel inner diameter, hosel taper, hosel depth, toe height, groove width, groove depth, and groove shape.

3. The method according to claim 1, wherein the step of applying a controlled source of energy comprises sintering powdered metal with an energy source selected from the group consisting of a laser or an electron beam.

4. The method according to claim 1, wherein the powdered metal is selected from the group consisting of steel, stainless steel, iron, copper, bronze, aluminum, tungsten, titanium, titanium alloy, chromium-cobalt alloy, and combinations thereof.

5. The method of claim 1, wherein the step of selecting a club design further comprises:
   modifying a parametric CAD file by selecting a set of parameters to alter.

6. The method of claim 1, wherein the step of selecting a club design further comprises selecting a club design from a library of club designs.
7. The method according to claim 1, wherein the step of providing a powdered metal further comprises:
   providing a first powdered metal with a first density; and
   providing a second powdered metal with a second density.

8. The method according to claim 7, wherein the first density is greater than about 1 g/cm$^3$.

9. The method according to claim 7, wherein the first density is greater than about 3 g/cm$^3$.

10. The method according to claim 7, wherein the first density is greater than the second density by about 1 g/cm$^3$.

11. The method according to claim 7, wherein the first density is greater than the second density by about 3 g/cm$^3$.

12. A golf club head made by the method of claim 1 comprising:
   a first portion made of a sintered metal having a first porosity;
   a second portion made of a sintered metal having a second porosity;
   wherein the first portion comprises about 1% to about 99% of the entire volume of the club head.

13. The golf club head of claim 12, wherein the sintered metal is selected from the group consisting of steel, stainless steel, iron, copper, bronze, aluminum, tungsten, titanium, titanium alloy, chromium-cobalt alloy, and combinations thereof.

14. The golf club head of claim 12, wherein the first portion comprises at least 95% of the total volume of the golf club head.
15. The golf club head of claim 12, wherein the first portion has a porosity of about 99% porosity to about 1% porosity.

16. The golf club head of claim 12, wherein the first portion has a porosity that is greater than about 90%.

17. The method according to claim 1, wherein the powdered metal sintering apparatus is selected from the group consisting of a direct metal laser sintering (DMLS) system, a selective laser melting system, and an electron beam melting apparatus.
INTERNATIONAL SEARCH REPORT

PCT/US2010/035286

A. CLASSIFICATION OF SUBJECT MATTER
INV. A63B53/04 B29C67/00

ADD ...

According to International Patent Classification (IPC) or to both national classification and IPC.

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
A63B B29C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched.

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
<thead>
<tr>
<th>Category</th>
<th>Citation of document with indication where appropriate, of the relevant passages</th>
<th>Relevant to claim No</th>
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<tr>
<td>Y</td>
<td>paragraph [0018]</td>
<td>7-16</td>
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<td>paragraph [0095] - paragraph [0098]</td>
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<td>WO 2009/036240 A1 (NIKE INC [US]; NIKE INTERNATIONAL LTD [US]; DEAN ANTHONY CARL [US])</td>
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Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents

A: document defining the general state of the art which is not considered to be of particular relevance
E: earlier document but published on or after the international filing date
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Date of the actual completion of the international search: 29 July 2010

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Name and mailing address of the ISA/Authorized officer

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Lundblad, Hampus
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