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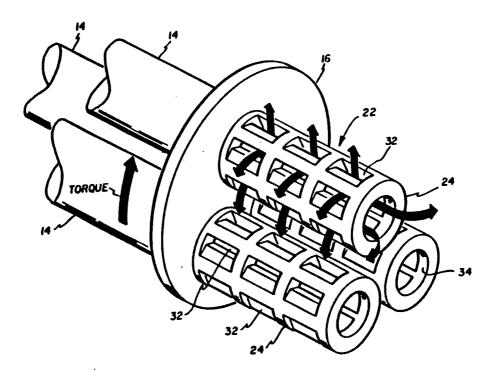
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(54) Title: TORQUE ASSIST DEVICE FOR A MULTI-BARREL WEAPON



#### (57) Abstract

There is provided for a Gatling type gun, a muzzle brake torque assist (22) having a plurality of radial flow turbines (32), each centered on a respective gun barrel (14) of the gun (5), each turbine for providing a respective pure torque centered on the respective barrel (14), and which torques translate into a summation torque centered on the longitudinal axis of the cluster of barrels (14) without generating any lateral loads on the stationary portions of the gun.

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# TORQUE ASSIST DEVICE FOR A MULTI-BARREL WEAPON

#### FIELD OF THE INVENTION

This invention relates to a supplemental gas drive and brake device for a Gatling type gun.

## BACKGROUND OF THE INVENTION

Gatling type guns, having a plurality of gun barrels disposed in an annular row in a rotor for rotation in a housing, are well known, having been first disclosed in U.S. Pat. No. 36,836 issued Nov. 4, 1862 to R. J. Gatling. The early Gatling guns had manual crank drives. C. J. Ebbets in U.S. Pat. No. 550,262 issued Nov. 26, 1895, and W. E. Simpson in U.S. Pat. No. 598,822 issued Feb. 8, 1898, respectively disclose supplemental gas drives wherein gun gas is bled from a port in the side of each barrel to operate a ratchet drive for the rotor. The modern Gatling gun was first disclosed in U. S. Pat. No. 2,849,921 issued Sept. 2, 1958 to H. Otto which had an electric motor drive.

Muzzle brakes for single barrel guns are also well known and are shown, for example, in U.S. Pat. No. 1,994,458 issued Mar. 19, 1935 to G. M. Barnes; U.S. Pat. No. 2,457,802 issued Jan. 4, 1949 to A. Bauer; and U.S. Pat. No. 2,567,826 issued Sept. 11, 1951 to J. E. Prache.

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Muzzle brake torque assist devices for Gatling guns are shown in U.S. Pat. No. 3,703,122 issued Nov. 21, 1972 to D. A. Farrington et al, and U.S. Pat. No. 3,898,910 issued Aug. 12, 1975 to R. T. Groff. These patents respectively disclose a single turbine having a single annular row of curved radial passageways. Since each of the plurality of gun barrels in the rotor respectively provides gas mainly to the adjacent portion or sector of radial passageways; there is a lateral load which must be reacted by the stationary structure at the radius of the turbine outlets to react the force generated at the turbine outlets. The diameter of the single turbine must be larger than the diameter of the annular row of gun barrels, since the outlets of the single turbine are disposed radially outwardly beyond the maximum radius of the row of barrels.

#### SUMMARY OF THE INVENTION

It is an object of this invention to provide for a Gatling gun a muzzle brake torque assist device without a lateral reaction force applied to the gun mount.

It is another object of this invention to provide for a Gatling gun a muzzle brake torque assist device whose diameter is no greater than the maximum diameter of the barrel cluster of the gun.

A feature of this invention is the provision for a

25 Catling gun of a muzzle brake torque assist device having a

plurality of radial flow turbines, each centered on a respective gun barrel, each turbine for providing a respective pure torque centered on the respective barrel, and which torques translate into a summation torque centered on the longitudinal axis of the cluster of barrels without generating any lateral loads on the stationary portions of the gun.

## BRIFF DESCRIPTION OF THE INVENTION

These and other objects, features and advantages of this
invention will be apparent from the following specification
thereof taken in conjunction with the accompanying drawing in
which:

- FIG. 1 is a perspective view of a Gatling type gun embodying this invention;
- FIG. 2 is a detail perspective view of the muzzle brake torque assist device of FIG. 1;
  - FIG. 3 is a detail perspective cutaway view of the device of FIG. 2;
- FIG. 4 is graph showing the power provided by the device of FIG. 2 for a typical Gatling gun installation;
  - FIG. 5 is a side elevation of the device of FIG. 2, and FIG. 6 is a front cross-section taken along the plane VI-VI of FIG. 5.

## DESCRIPTION OF THE INVENTION

The Gatling gum shown in FIG.1 includes a stationary housing 10 which is mounted, as to a vehicle, by a pair of recoil adapters 12. A plurality of gum harrels 14, hereshown as three, are fixed in an annular row to a rotor (not visible) which is journaled for rotation within the housing. The barrels are held in a cluster by a forward barrel clamp 16, a mid-barrel clamp 18 is journaled for rotation in a slide mount 20. A similar type of gum mount is shown in U.S. Pat. No. 4,345,504 issued to R. G. Kirkpatrick et al on Aug. 24, 1982. The gum may be of any suitable Gatling type, as shown, for example in U.S. Pat. No. 4,314,501 issued to R. G. Kirkpatrick on Feb. 9, 1982, or in U.S. Pat. No. 4,216,698 issued to R. E. Chiabrandy on August 12, 1980, or in U.S. Pat. No. 3,760,683 issued to J. M. Seemann on Sept. 25, 1973.

As shown in FIG. 2, the forward barrel clamp 16 serves as part of the muzzle brake torque assist device 22. The device 22 includes a plurality of barrel extension tubes 24, serving as torque tubes, here shown as three, one for each barrel, that are fixed to the clamp 16. Each extension tube has a plurality of radial slots 32 cut through its tube wall, shown as six in FIG. 3, to provide a like plurality of torque tube vanes 28 each having a face 30. However, as shown in FIG. 2, to provide rigidity to the tube structure, each slot is actually formed as a longitudinally extending set of ports 32, each set here shown as three in number.

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The muzzle device 22 deflects a large percentage of the muzzle gas from axial flow to radial flow by impact with the aft facing surfaces formed by the plurality of slots. This change in direction of the high-velocity muzzle gas provides a forward thrust on the barrel cluster, to which the muzzle device is attached, which partially counteracts the recoil force. It may be noted that when firing a round of ammunition having a large amount of propellant, the contribution of the propellant gas to the total recoil impulse is nearly half the total. Thus, deflecting the gas radially reduces the average recoil force as well as the peak recoil force.

The radially directed flow of muzzle gas through the ports 32 against the faces 30 of the vanes 28 imparts a torque about the longitudinal axis of the respective gun barrel, shown in FIG. 3 as counter clock-wise when viewed from the rear. These torques about the gun barrel axes resolve into a torque about the longitudinal axis of the gun barrel cluster which is the axis of rotation of the rotor, shown in FIG. 2 as counter clock-wise.

As shown in FIG. 5, the face 30 of the vane 28 is a plane which is tangential to the inner bore 34 of the torque tube.

The outlet cross-sectional area of the port 32 is enlarged by removing part of the back wall at 36.

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The outlets of the ports 32 are radially within the radius of the nonrotating slide mount 20, within which the mid-barrel clamp 18 rotates. Since gases flow equally through all slots of the extension tube there is no lateral load which must be reacted by the mount 20 to react the forces generated at the outlets. The radius of the housing 10 is similarly greater than the radius of the outlets.

While the face 30 has been shown as tangential to the inner bore 34, it will be appreciated that the face may be at any angle that will deflect the generally radial flow of gas into a more tangential flow and absorb energy nonsymmetrically from such deflection to generate a torque. As a limiting value, if the port 32 is cut on a true radius to the longitudinal axis of the tube, such energy as will be absorbed, will be absorbed symmetrically, and no torque will be generated. The face 30 may also be formed concave, rather than flat, as shown.

A round of ammunition having a projectile mass of 1600 grains and a propellant mass of 120 grams can generate an impulse per shot of approximately 55 lb.-sec. The muzzle device can reduce this impulse by 30% to 10 lb-sec. per round, and generate 32 H.P. The gun system power requirement (without the muzzle device) as a function of time during system acceleration, is shown in the upper curve of FIG. 4. Note that the required power rises to a peak of 49 H.P. and then declines to 40 H.P. steady state. The gun system power

requirement (with the muzzle device) as a function of time during system acceleration, as shown in lower curve of FIG.

4. Note that the required power rises to a peak of merely 26 H.P. and then declines to 8 H.P. steady state. This reduction of the external power requirement allows a broad spectrum of potential power sources to drive the gun: electric, engine bleed air, self-contained pneumatic and hydraulic.

#### CLAIMS:

- 1. A muzzle brake torque assist device for a Gatling type gun having a cluster of a plurality of gun barrels disposed in an annular row and journaled for rotation within a nonrotating structure about a longitudinal axis disposed through the center of said row, comprising:
- a like plurality of extension tubes, each fixed at the muzzle end of, and having a longitudinal bore in longitudinal alignment with, a respective gun barrel;
- disposed in a uniformly spaced apart annular row, each port passing from said bore through the wall of said tube and having a respective vane surface adapted to be impacted by the flow of gun gas from the respective gun barrel flowing into the tube and out through said port, whereby said vane surface absorbs energy from the flow of gun gas through said port to generate a torque in the respective tube about the longitudinal axis of said respective tube.
  - 2. A device according to claim 1 wherein:

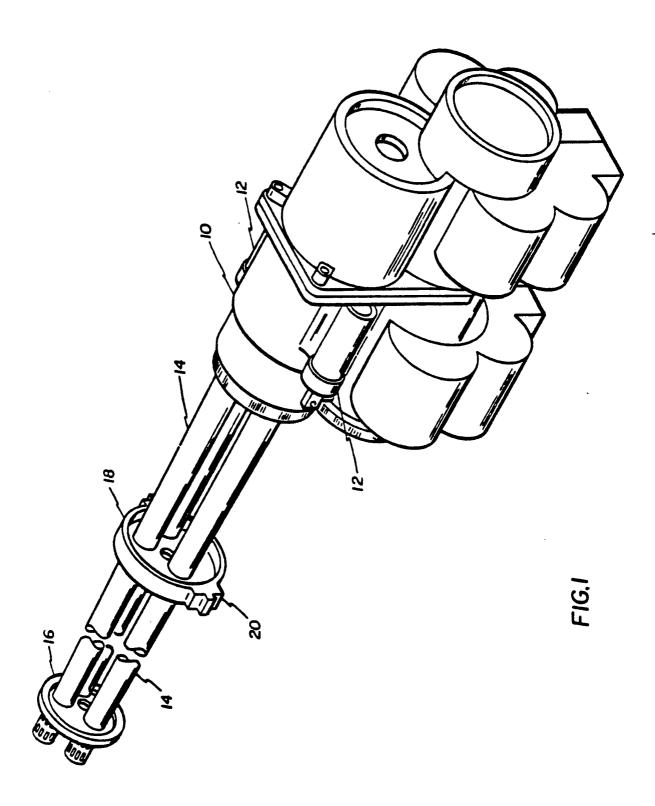
said torques generated in each tube resolve into a torque about said longitudinal axis of said cluster of gun barrels.

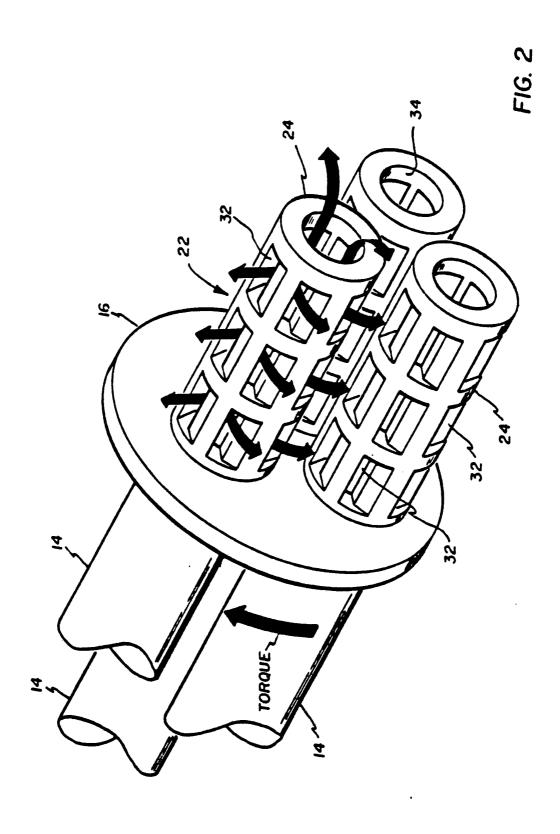
3. A device according to claim 2 wherein:

each of said vane surfaces is formed along a plane which is substantially tangential to the inner wall of said bore of said tube.

- 4. A device according to claim 3 wherein:

  said port has an inlet having a first crosssectional area opening onto said bore of said tube and an
  outlet, having a second cross-section area, opening onto the
  exterior of said tube, said second area being greater than
  said first area.
  - 5. A device according to claim 1 wherein:
    said nonrotating structure has a minimum inner
    radius which is greater than the maximum radius of said gas
    ports.





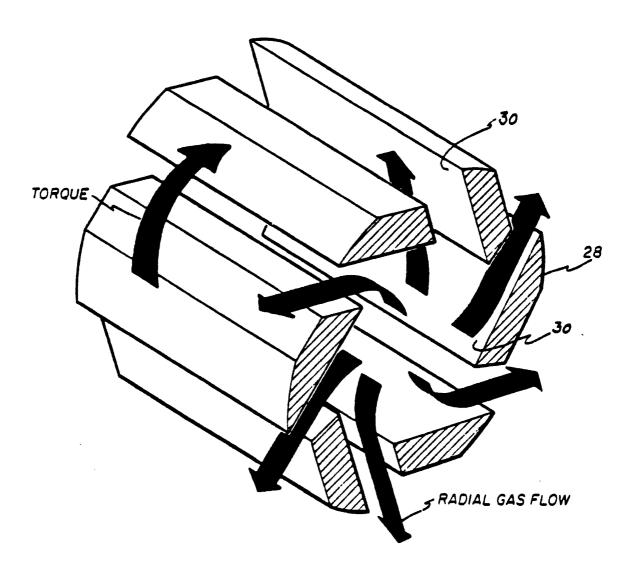
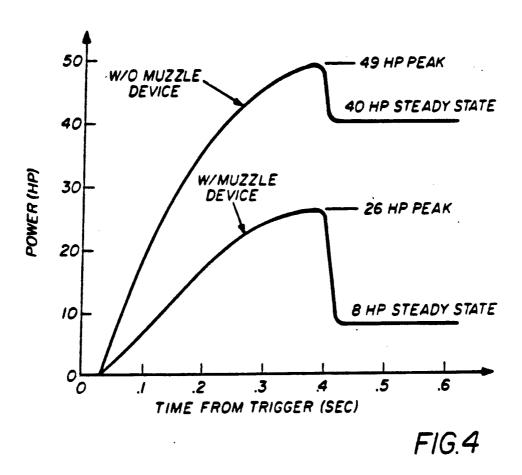
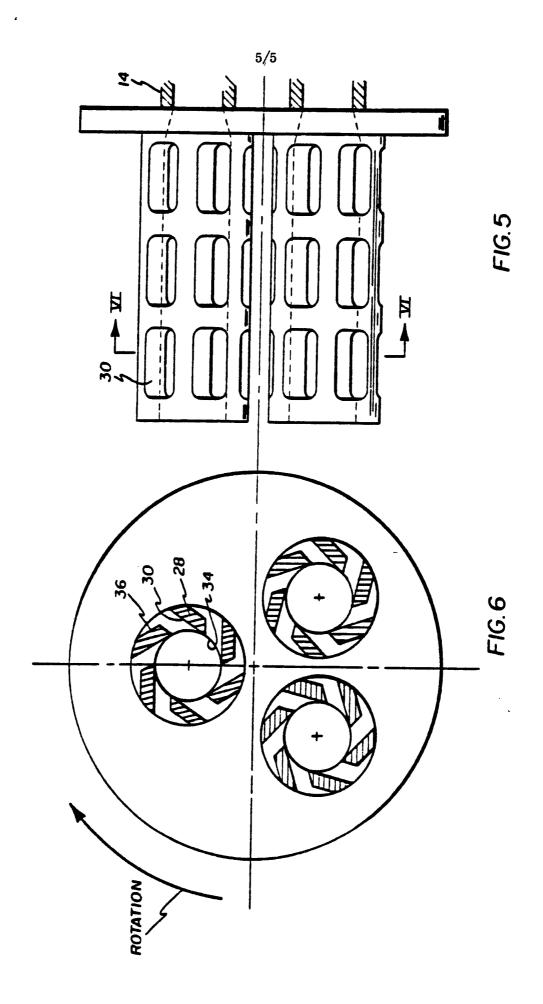


FIG. 3





## INTERNATIONAL SEARCH REPORT

International Application No PCT/US85/00903

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) <sup>3</sup>							
		onal Patent Classification (IPC) or to both Na	tional Classification and IPC				
Int. C	L. 4 F4	1F 17/12; F41D 7/04					
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II. FIELD	SEARCH		entation Searched 4				
Minimum Documentation Searched 4  Classification System   Classification Symbols							
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III. pócu		ONSIDERED TO BE RELEVANT 14					
Category *	Citati	on of Document, 18 with Indication, where ap	propriate, of the relevant passages 17	Relevant to Claim No. 18			
A	US, A	, 3,703,122 (Farrington	et al) 21 November 1972	1-5			
A	US, A	, 3,898,910 (Groff) 12 A	3,898,910 (Groff) 12 August 1975				
A	US, A	, 4,121,496 (Clayson) 24	4,121,496 (Clayson) 24 October 1978				
A	US, A	, 4,398,445 (Ulrich) 16	1-5				
"A" doc con "E" earl	ument defin sidered to b ier documer	of cited documents: 15 ing the general state of the art which is not e of particular relevance it but published on or after the international	"T" later document published after to or priority date and not in conficited to understand the principle invention "X" document of particular relevant to considered poyal or	or theory underlying the			
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