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(54) **ULTRASOUND CATHETER**

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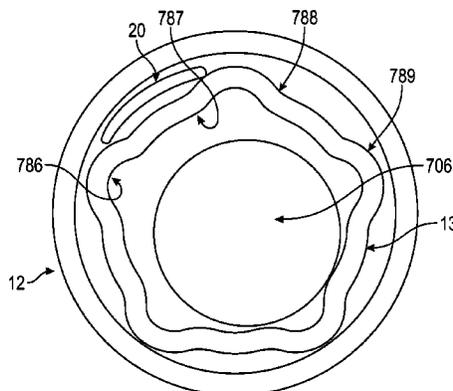
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(57) **ABSTRACT**

A first tubular body having a first longitudinal axis extending centrally through the tubular body includes at least one delivery port extending through a wall of the first tubular body. A second tubular body having a second longitudinal axis extends through the second tubular body, the first and second longitudinal axes being displaced from each other such that an asymmetrical longitudinally extending gap is formed between an outer surface of the second tubular body and an interior surface of the first tubular body. A temperature sensor forming a thermocouple extending longitudinally within the gap between the first tubular body and the

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second tubular body. An inner core is positioned within the second tubular body. The inner core includes least one ultrasound element.

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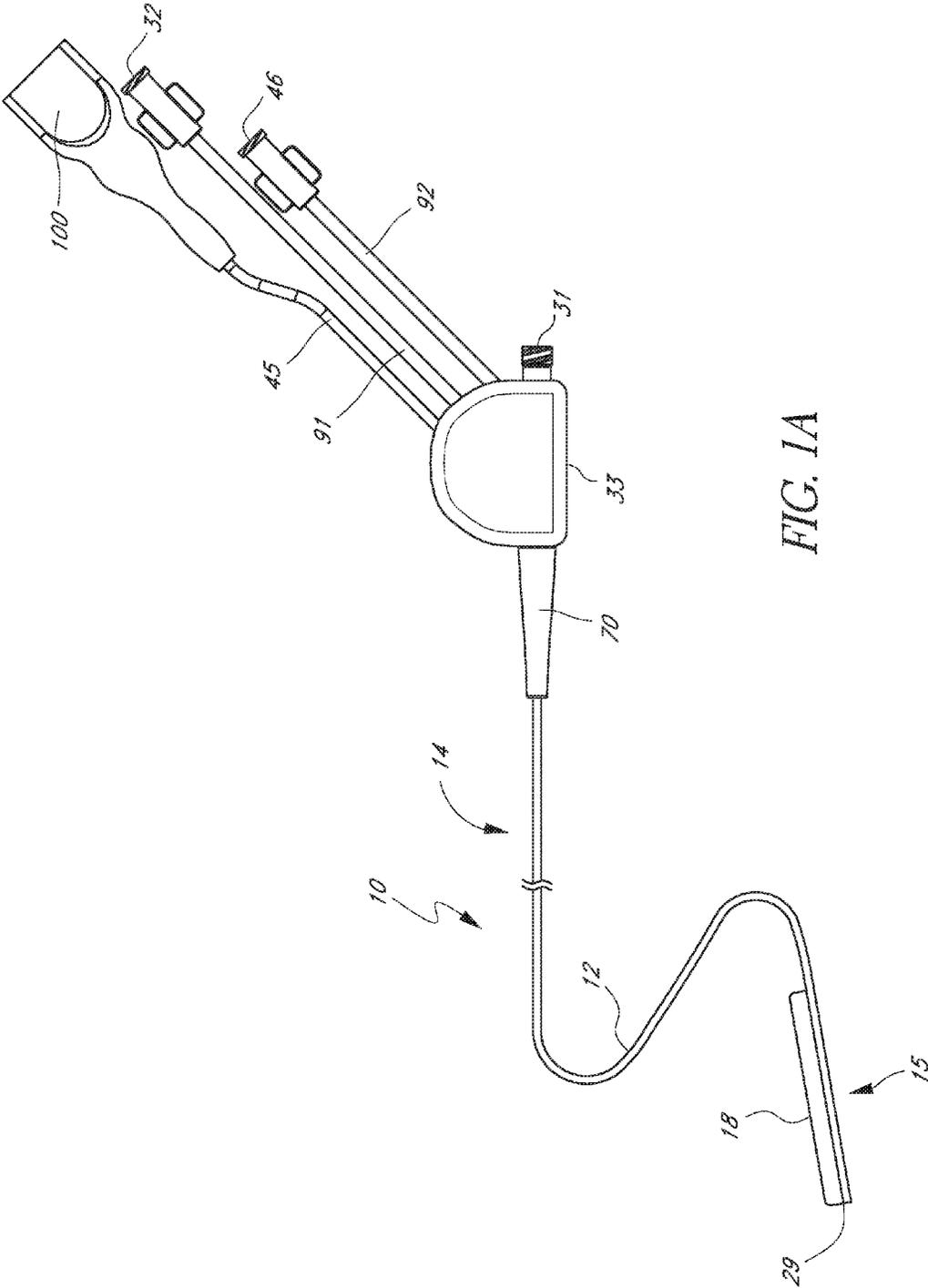
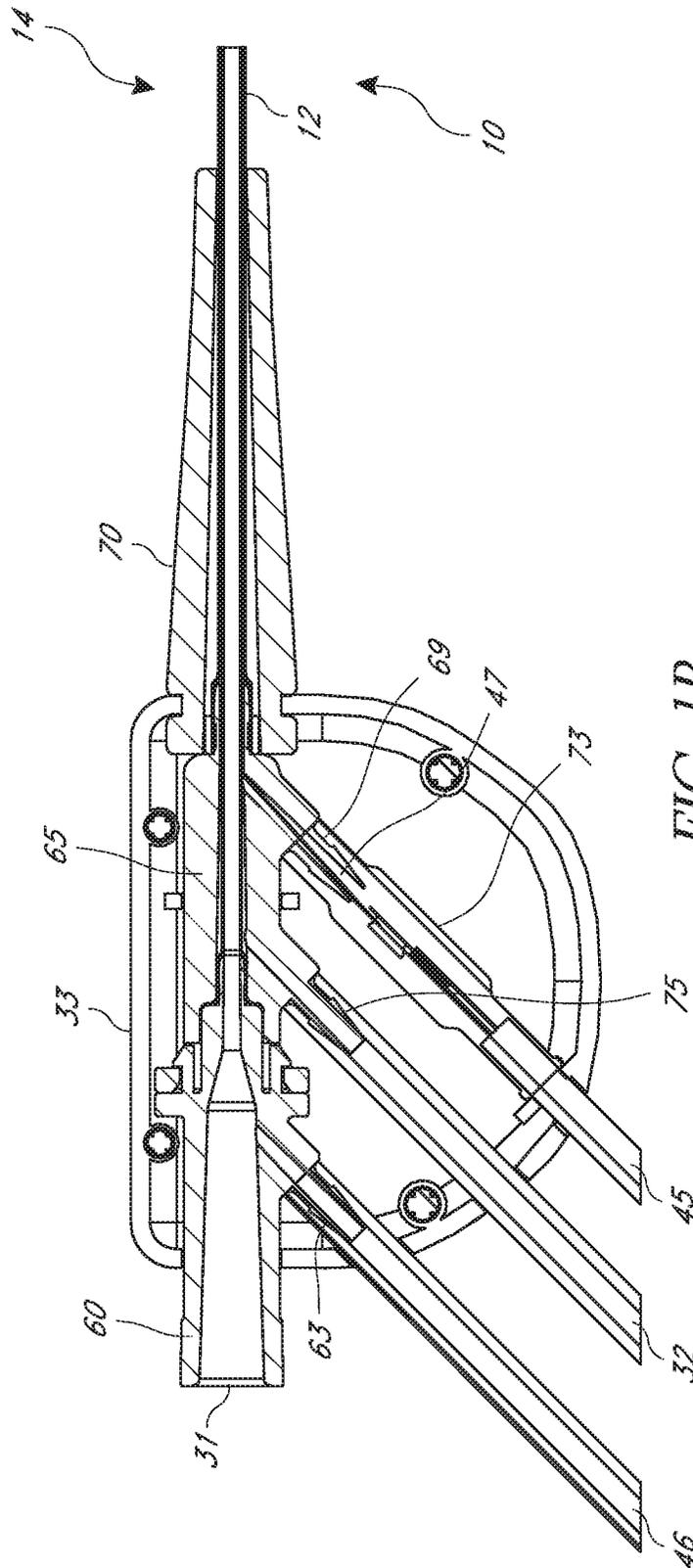
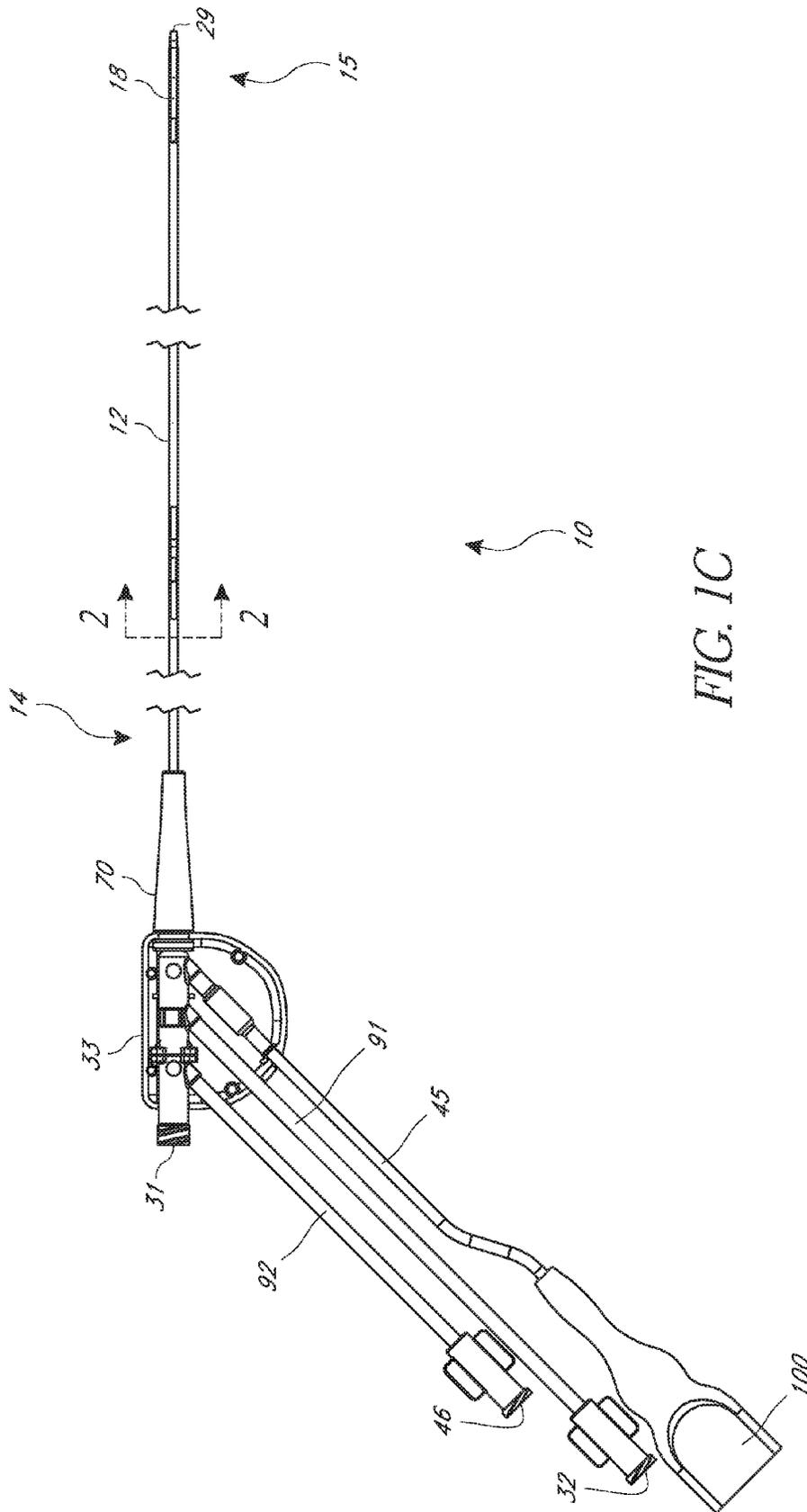


FIG. 1A





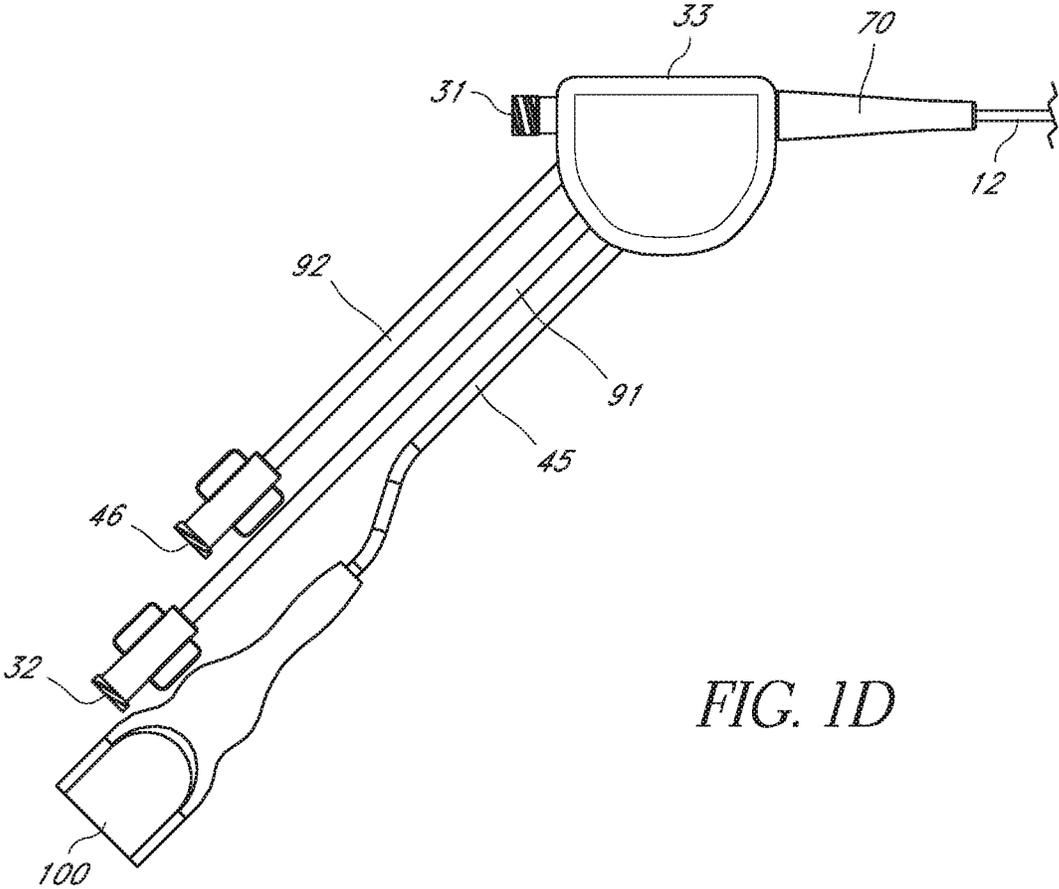


FIG. 1D

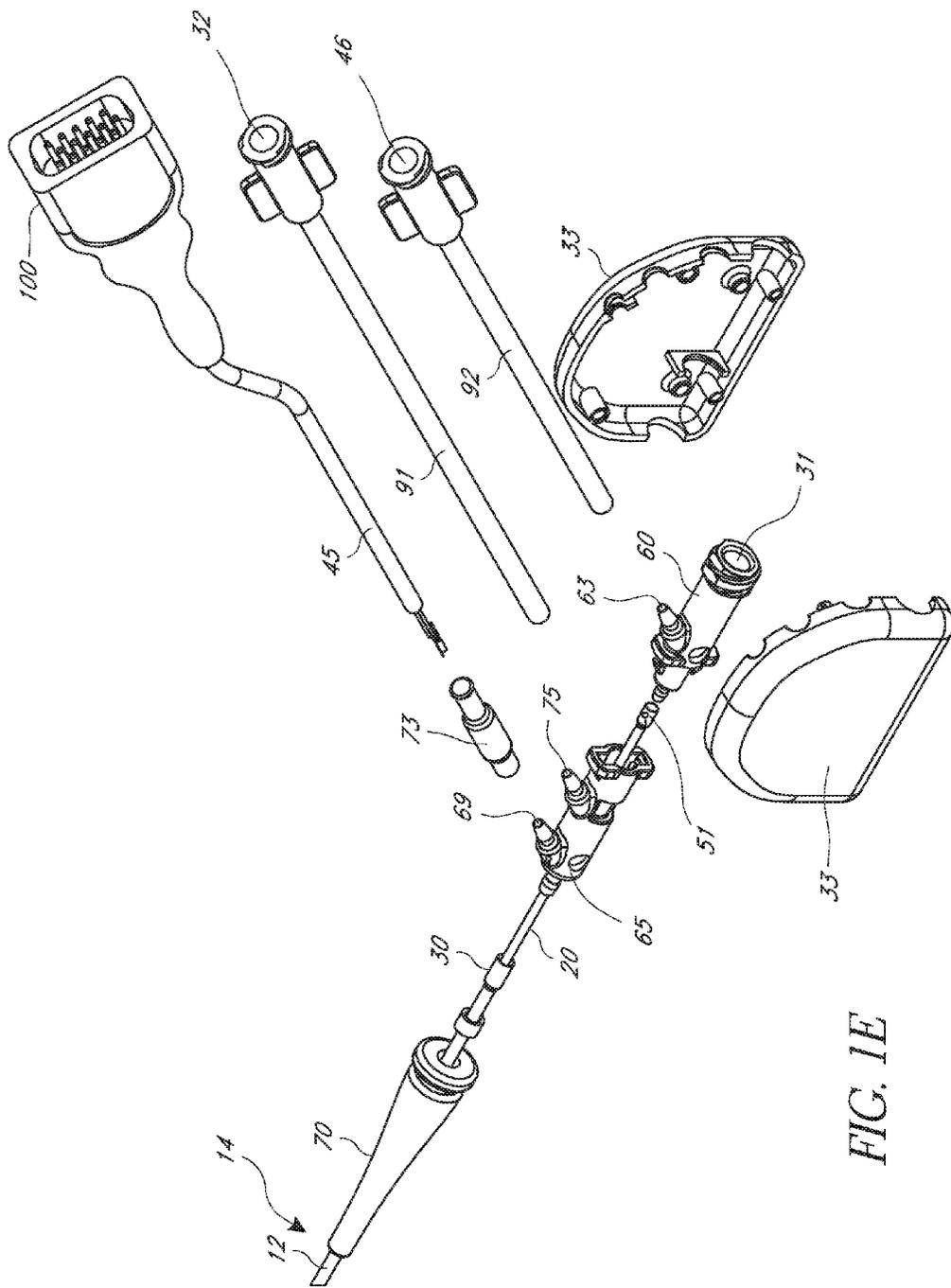


FIG. 1E

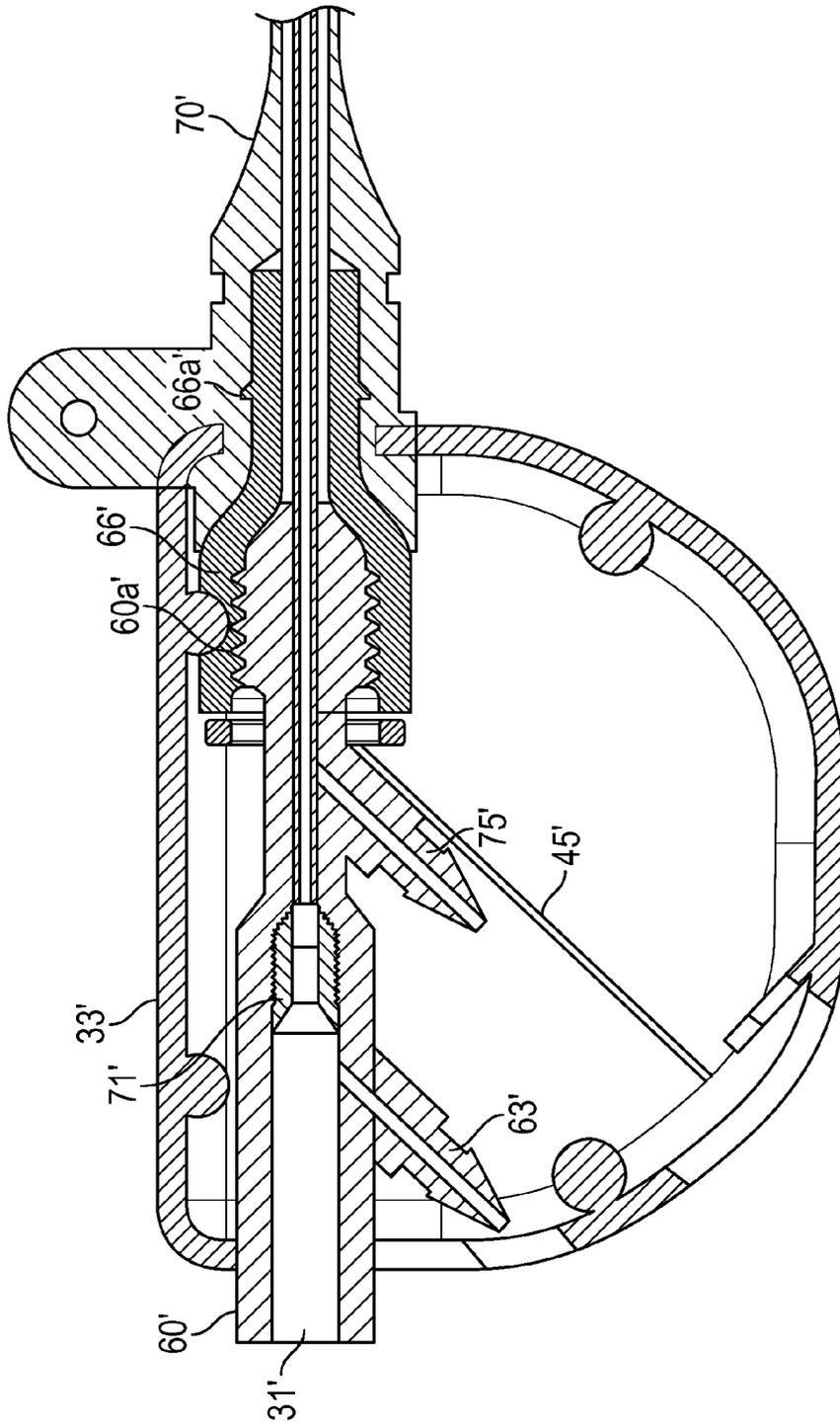


FIG. 1F

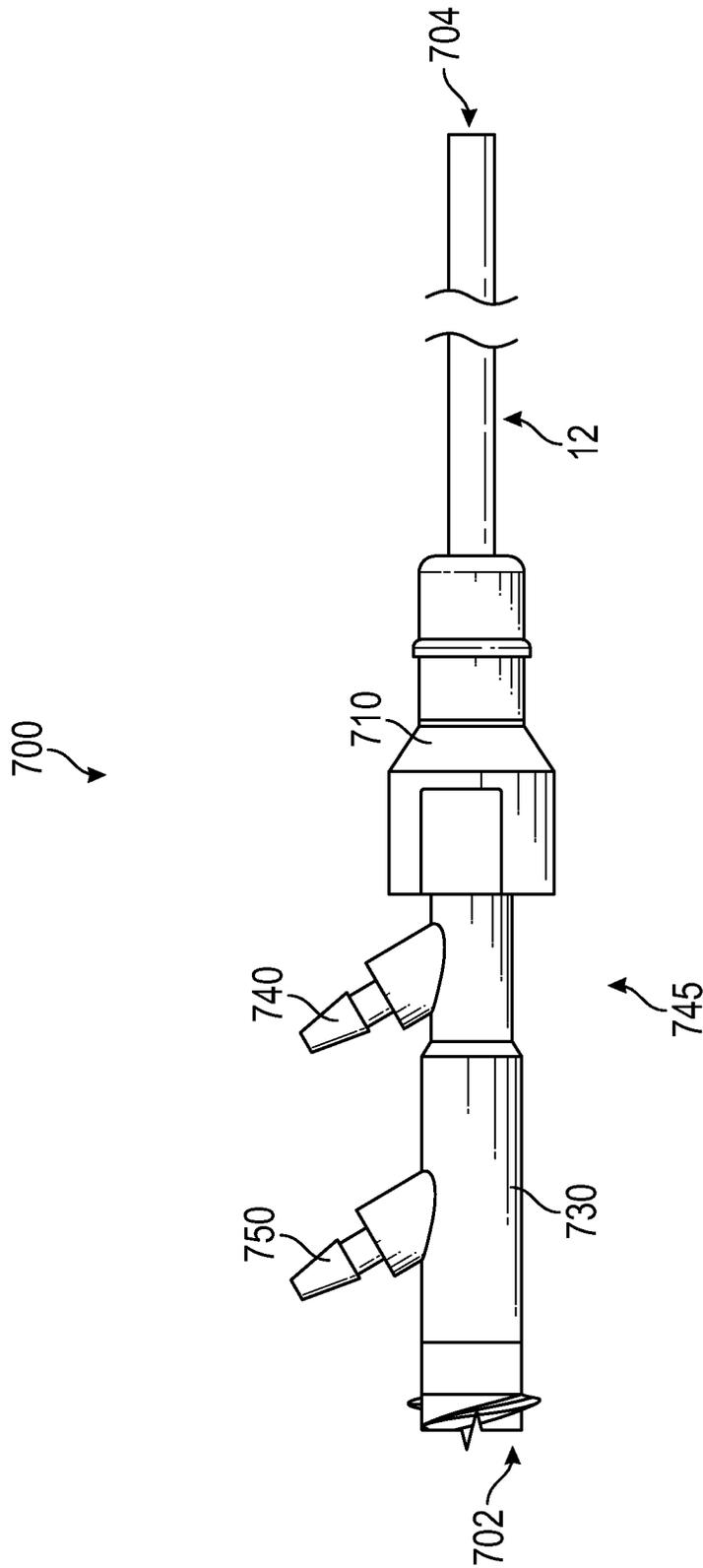


FIG. 1G

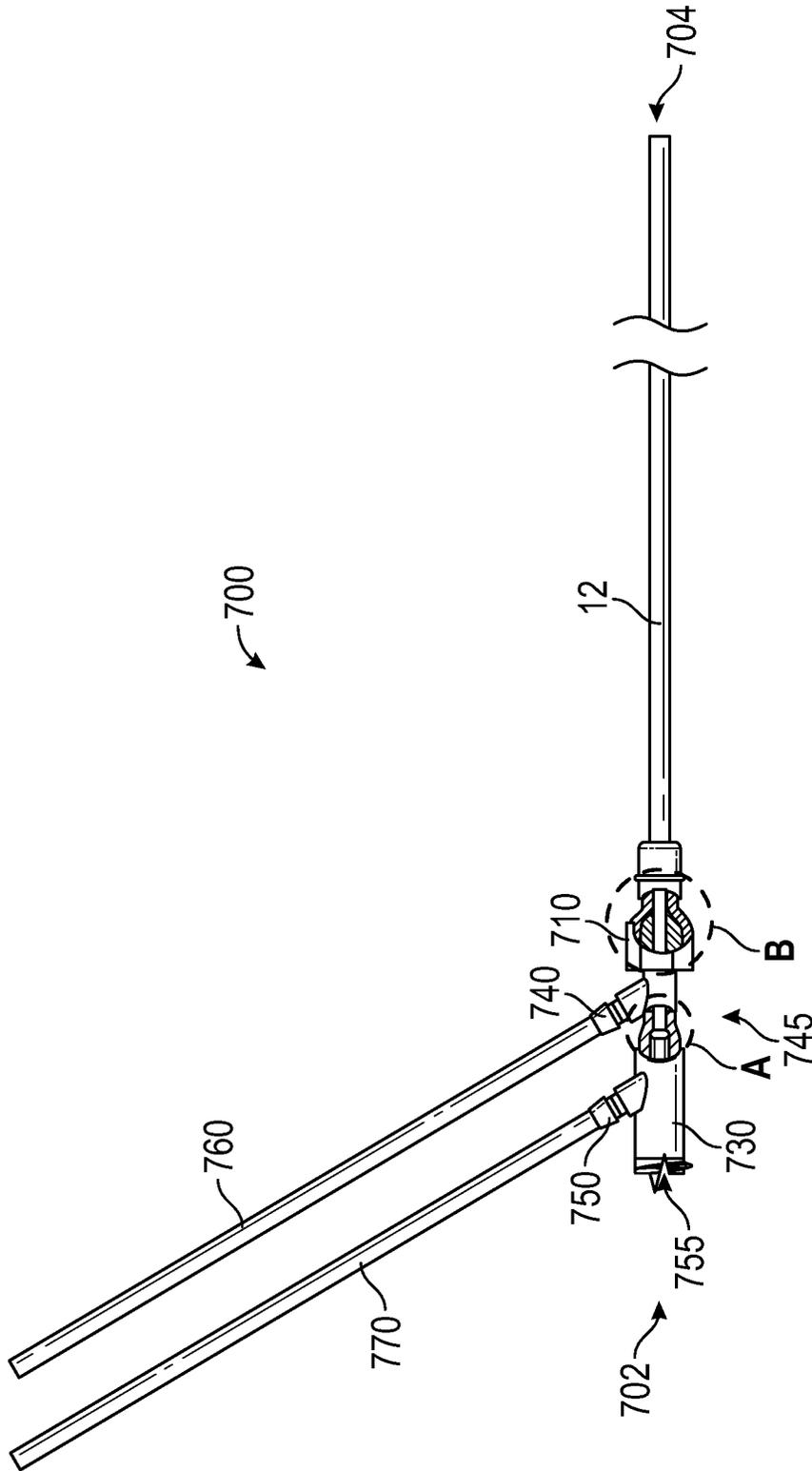
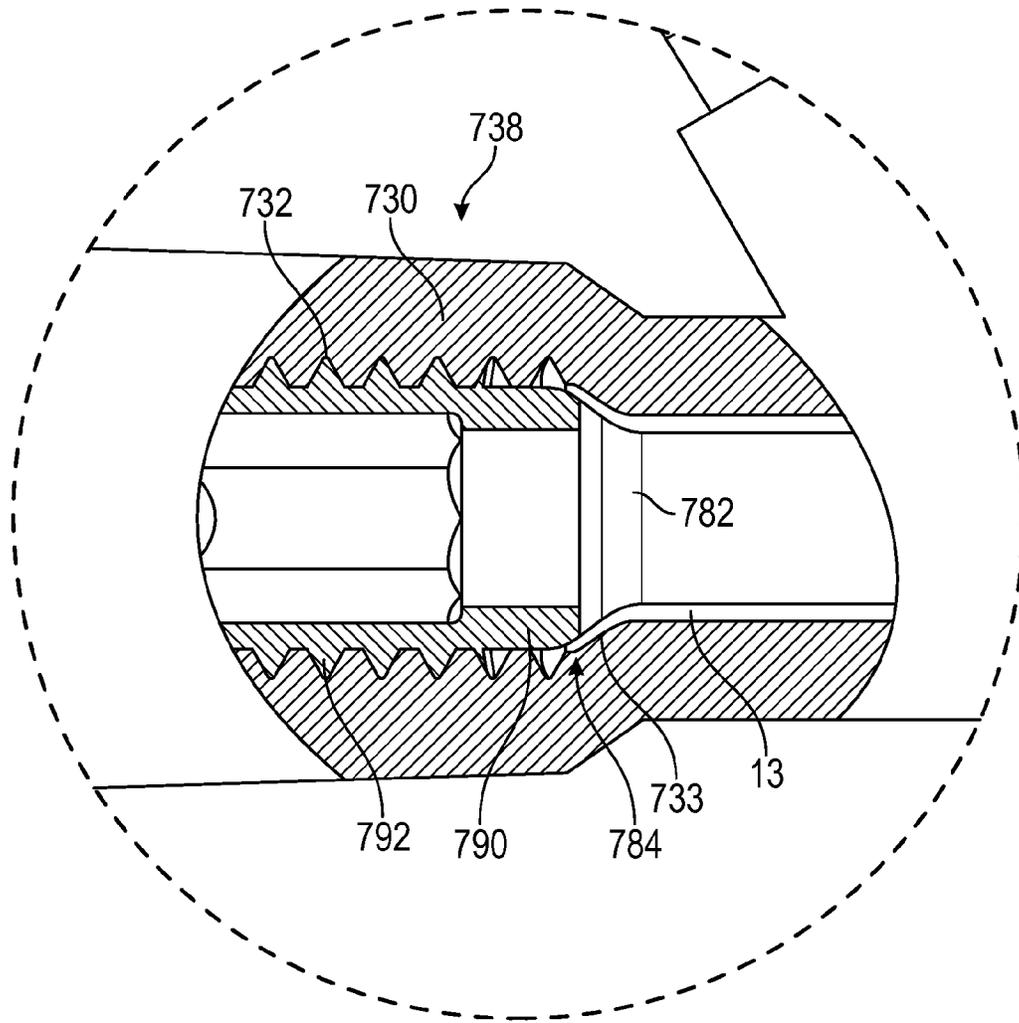
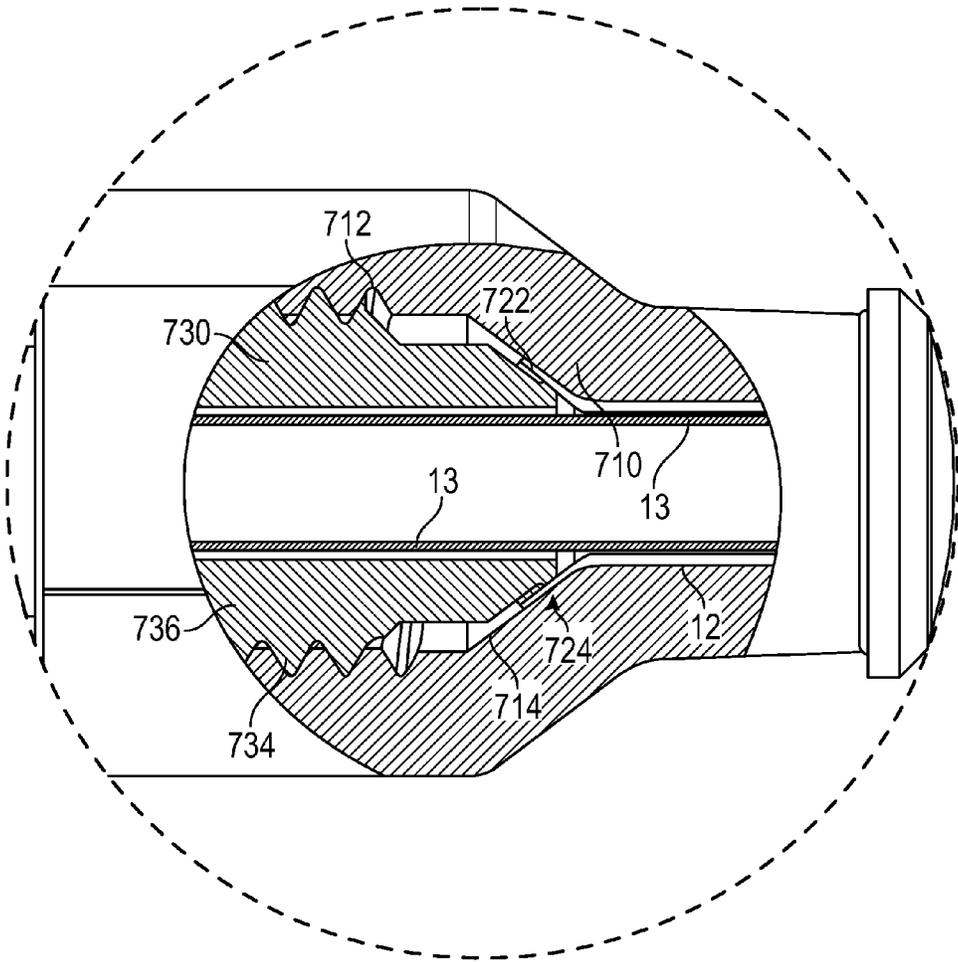


FIG. 1H



A-A

FIG. 11



B-B

FIG. 1J

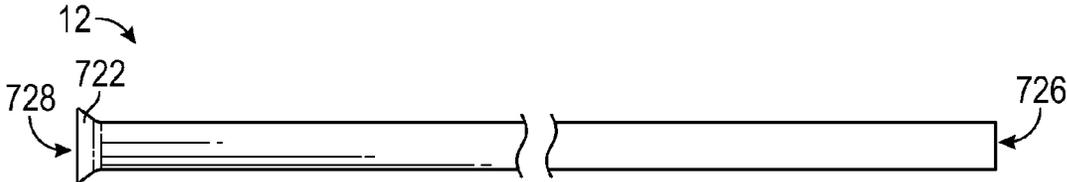


FIG. 1K

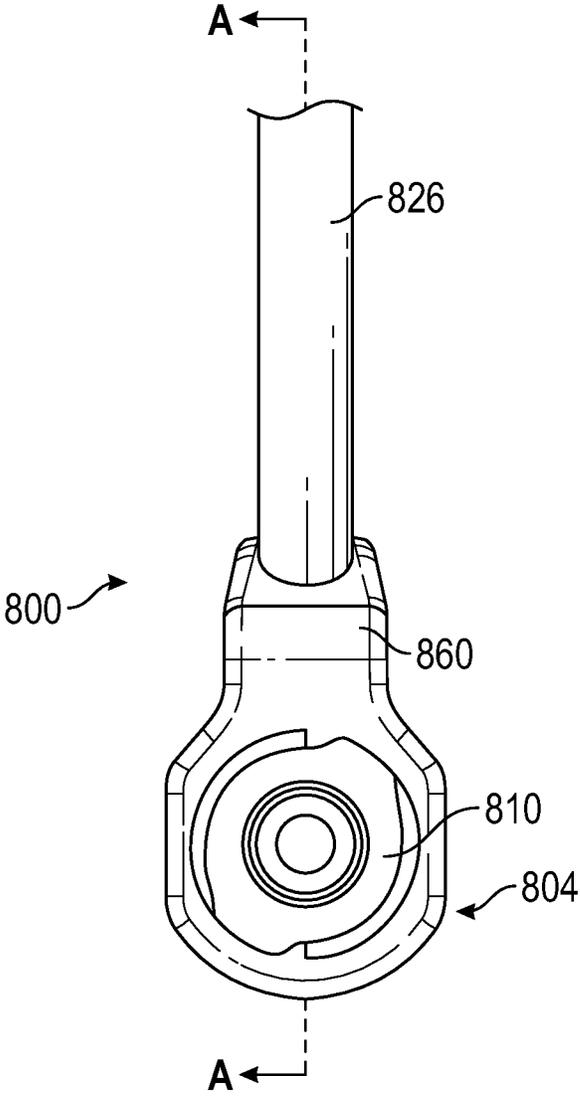


FIG. 1L

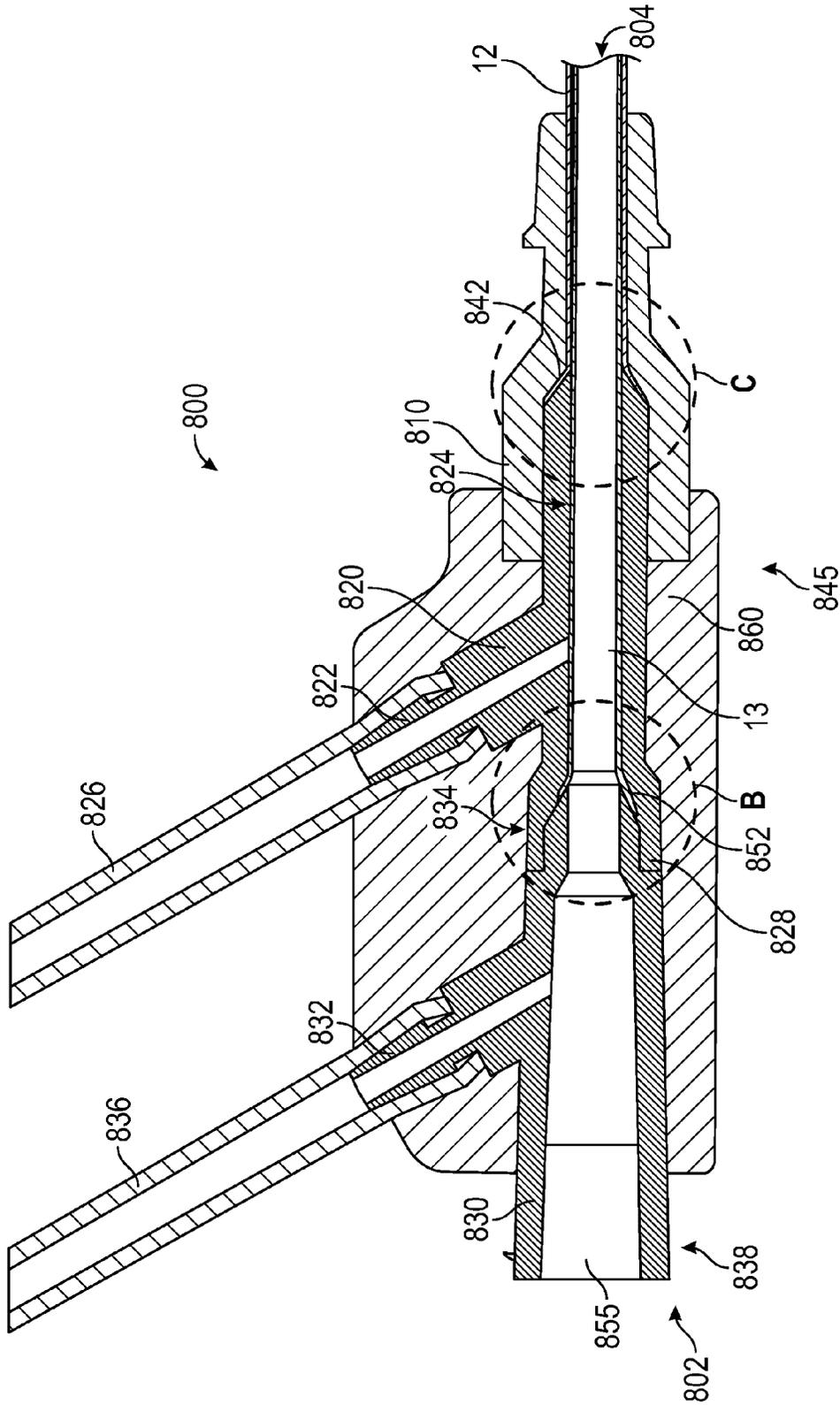
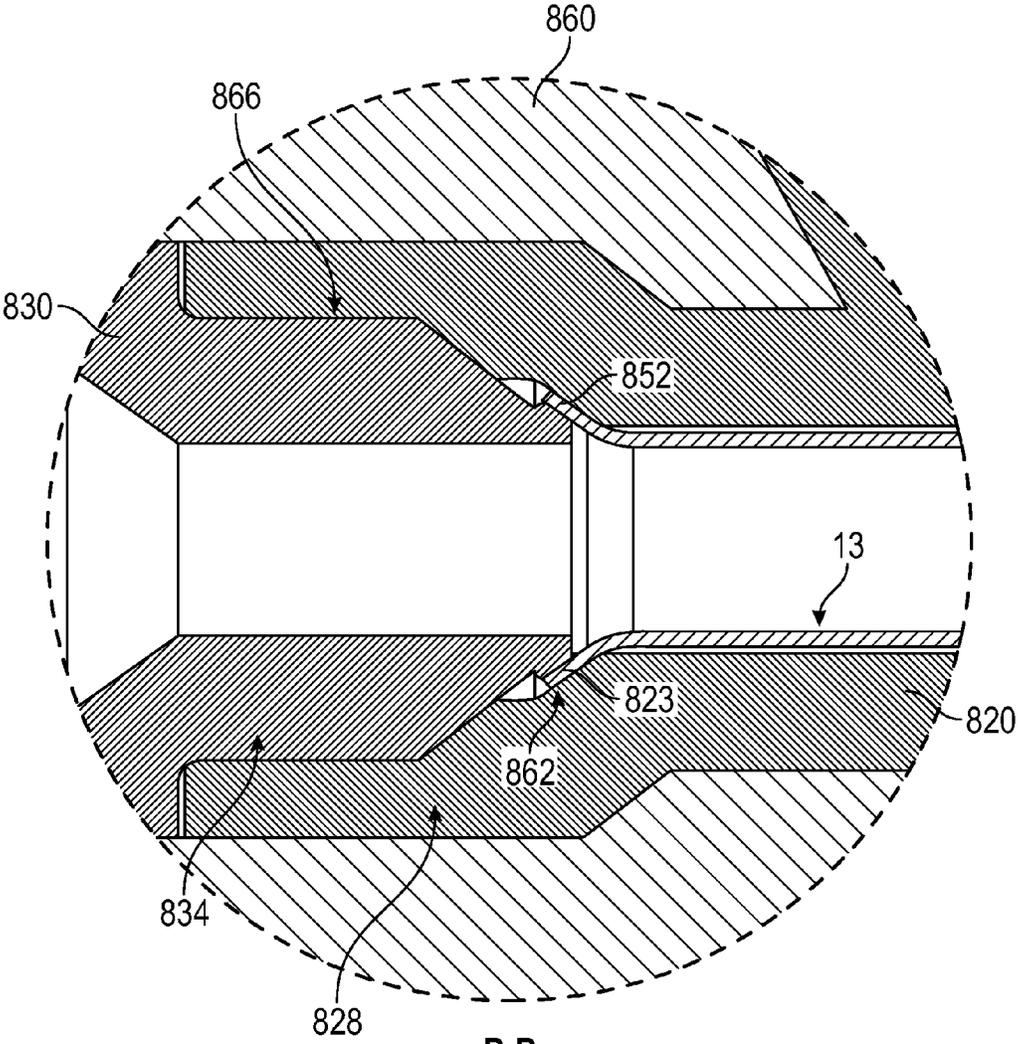
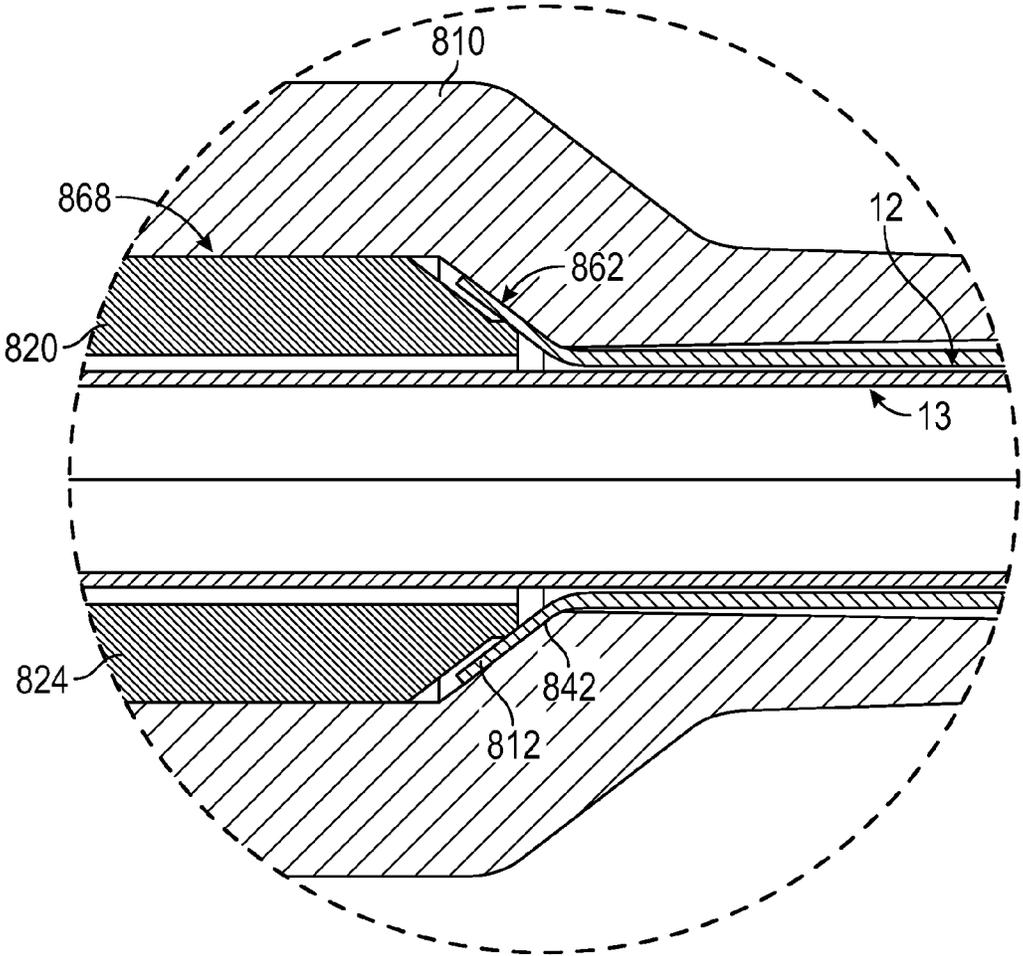


FIG. 1M



B-B
FIG. 1N



C-C
FIG. 10

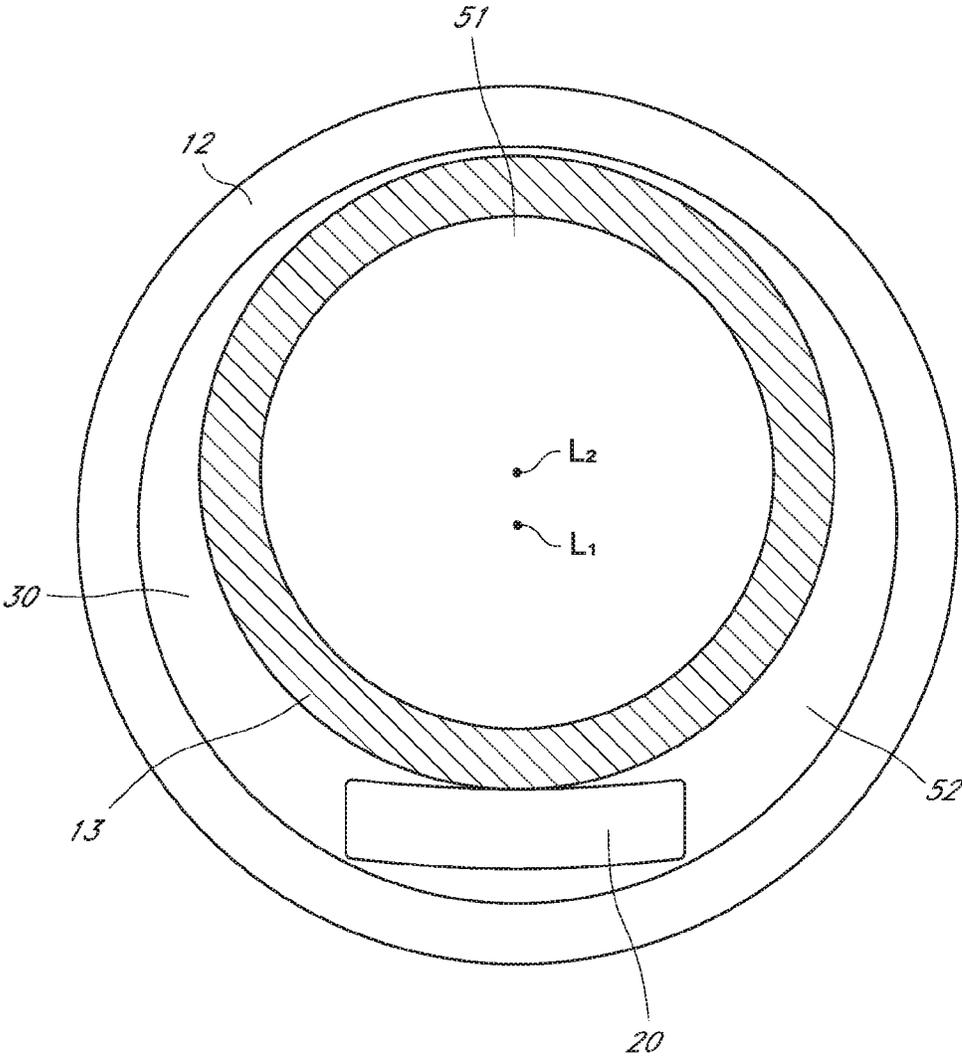


FIG. 2

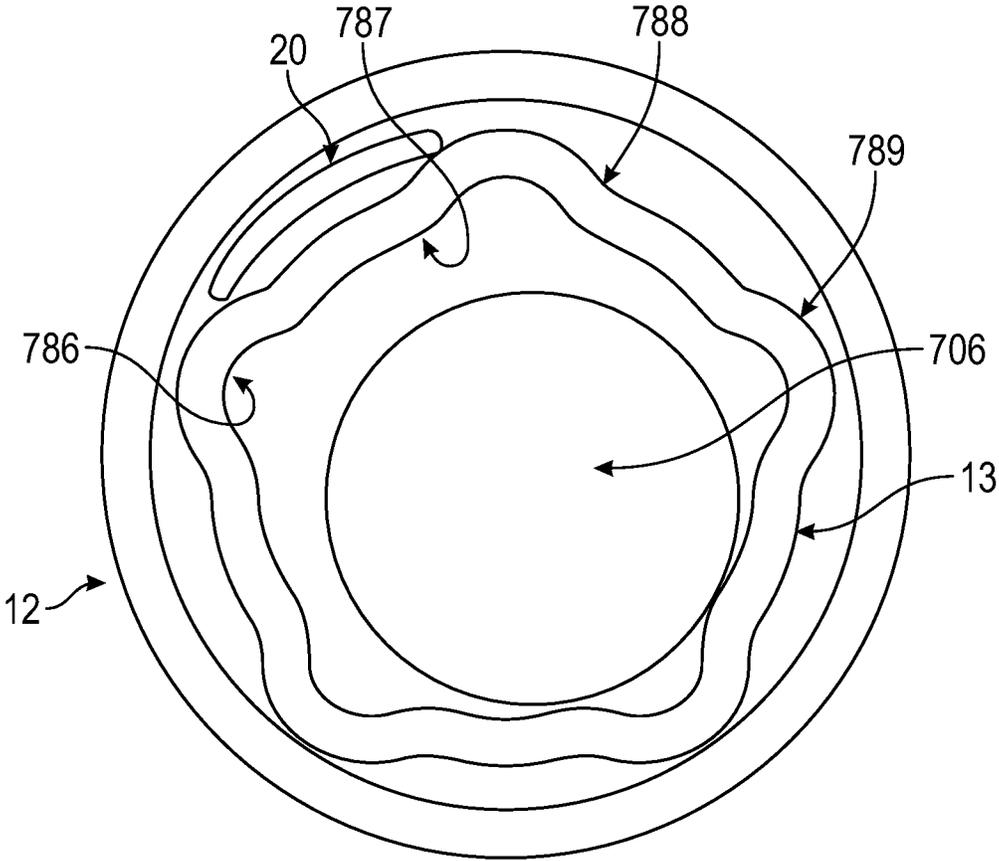


FIG. 2A

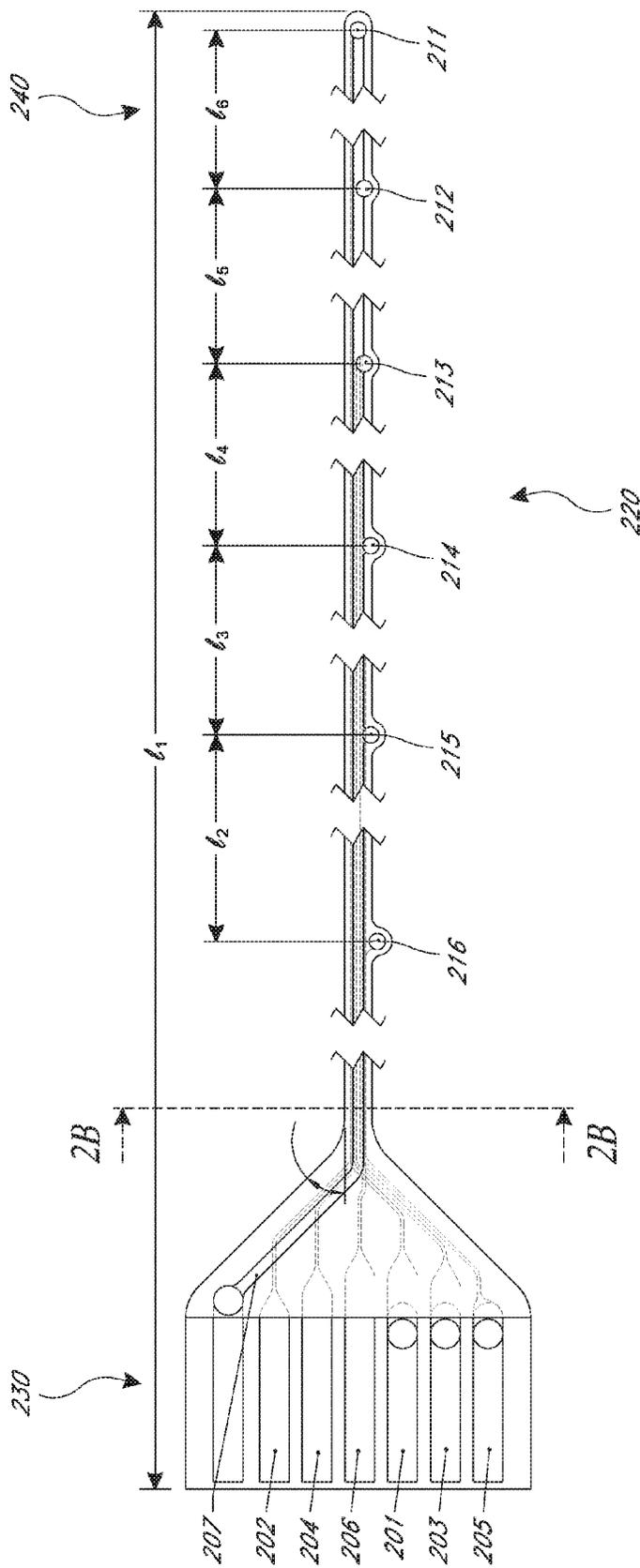


FIG. 2B

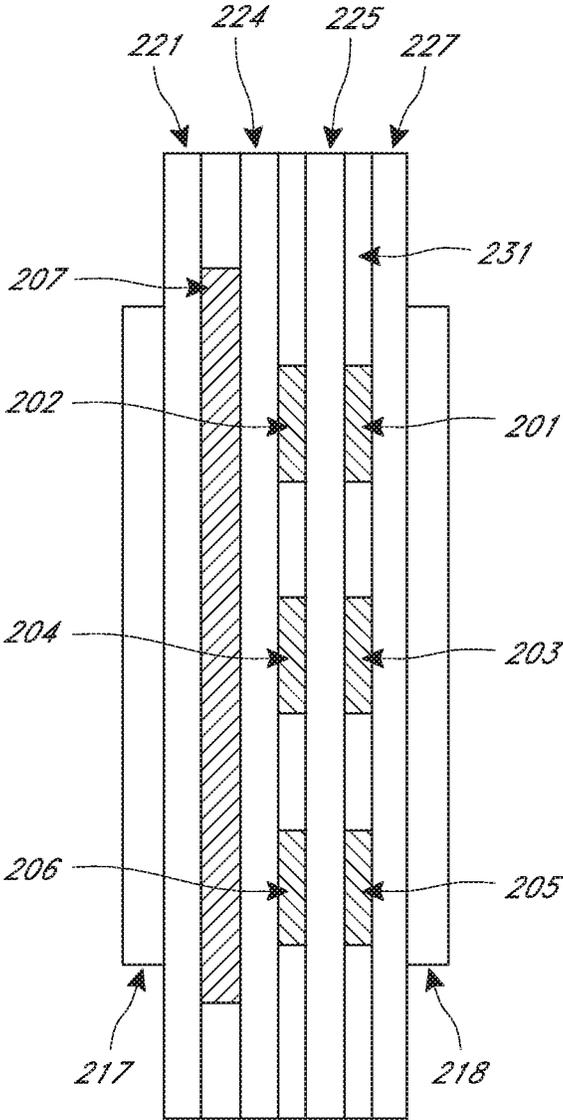


FIG. 2C

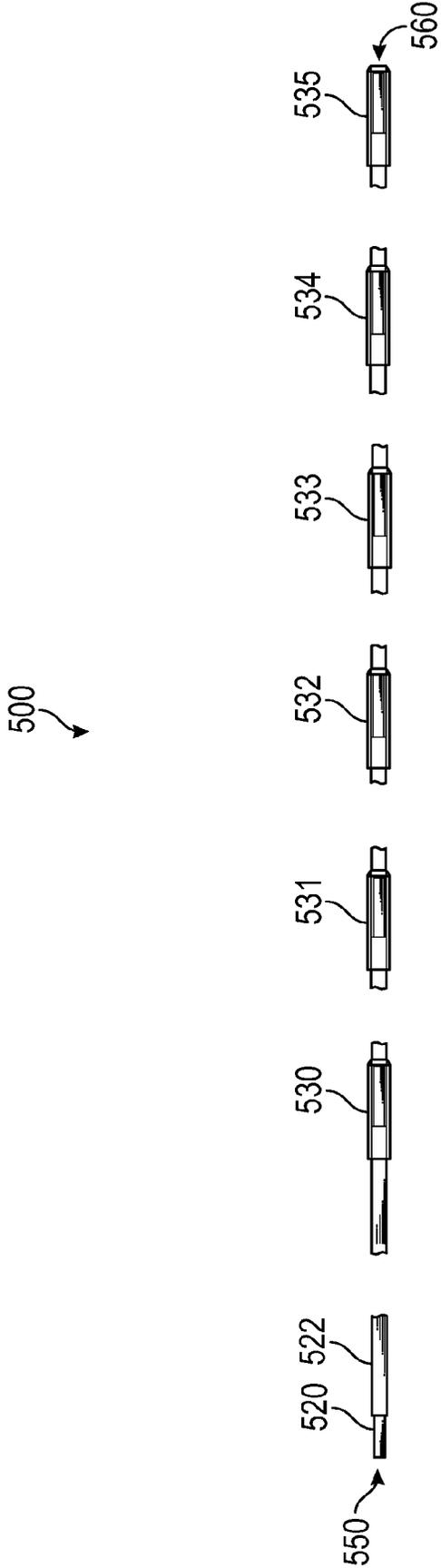


FIG. 2D

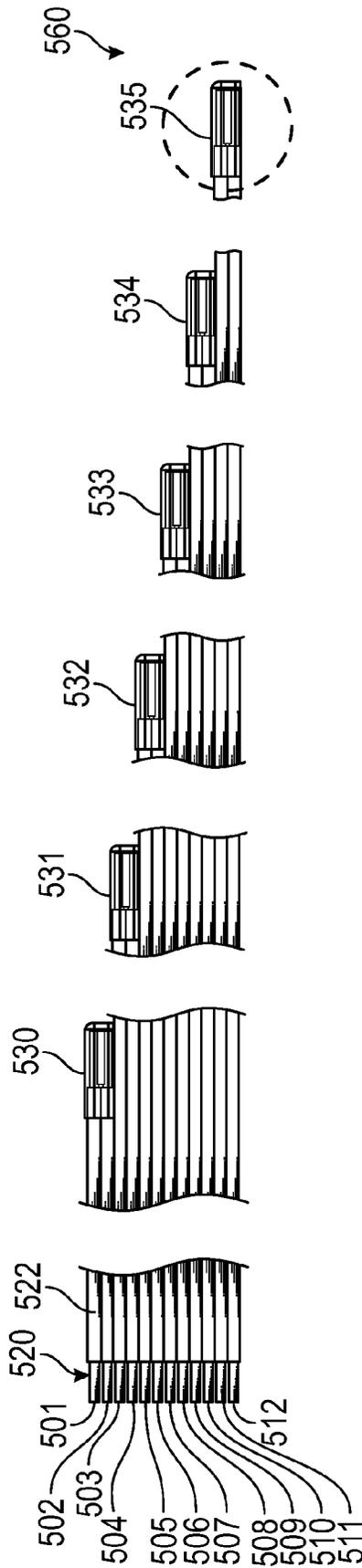


FIG. 2E

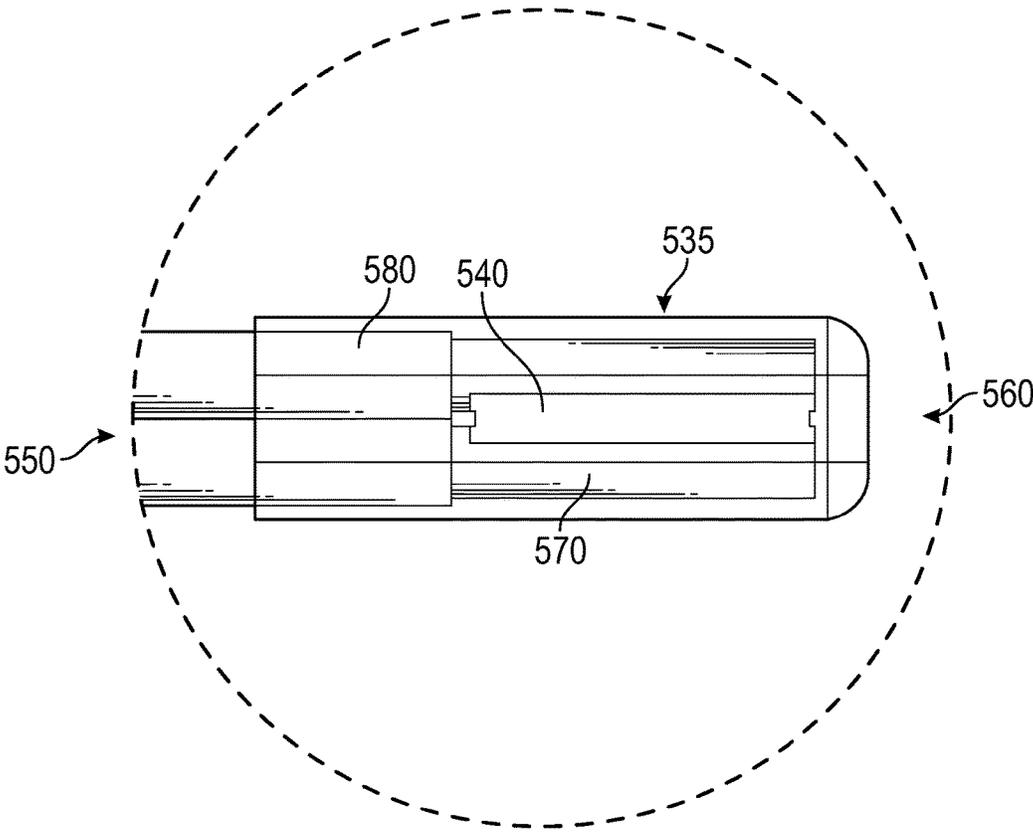


FIG. 2F

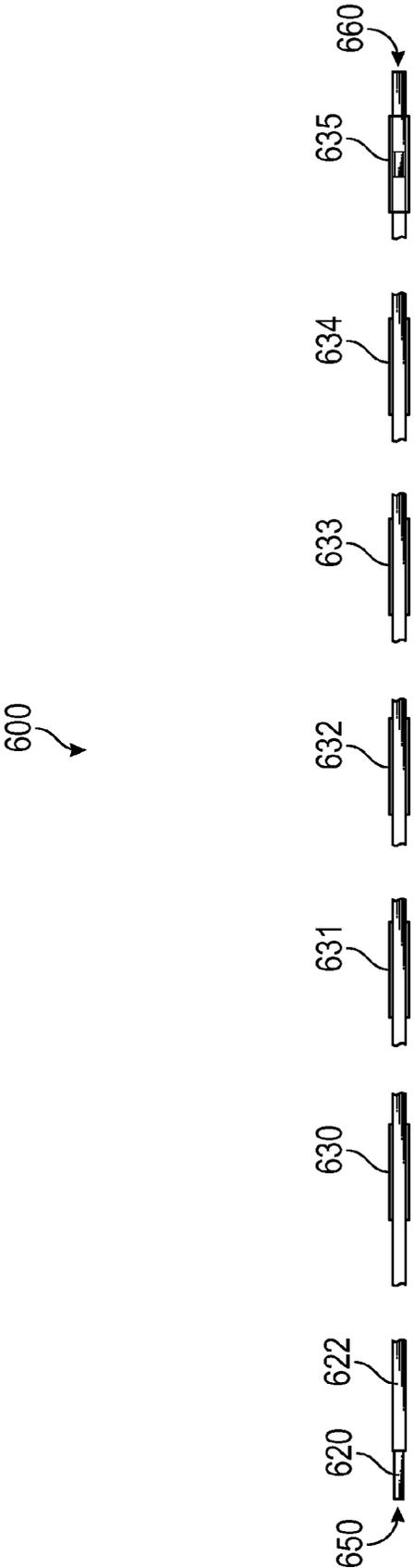
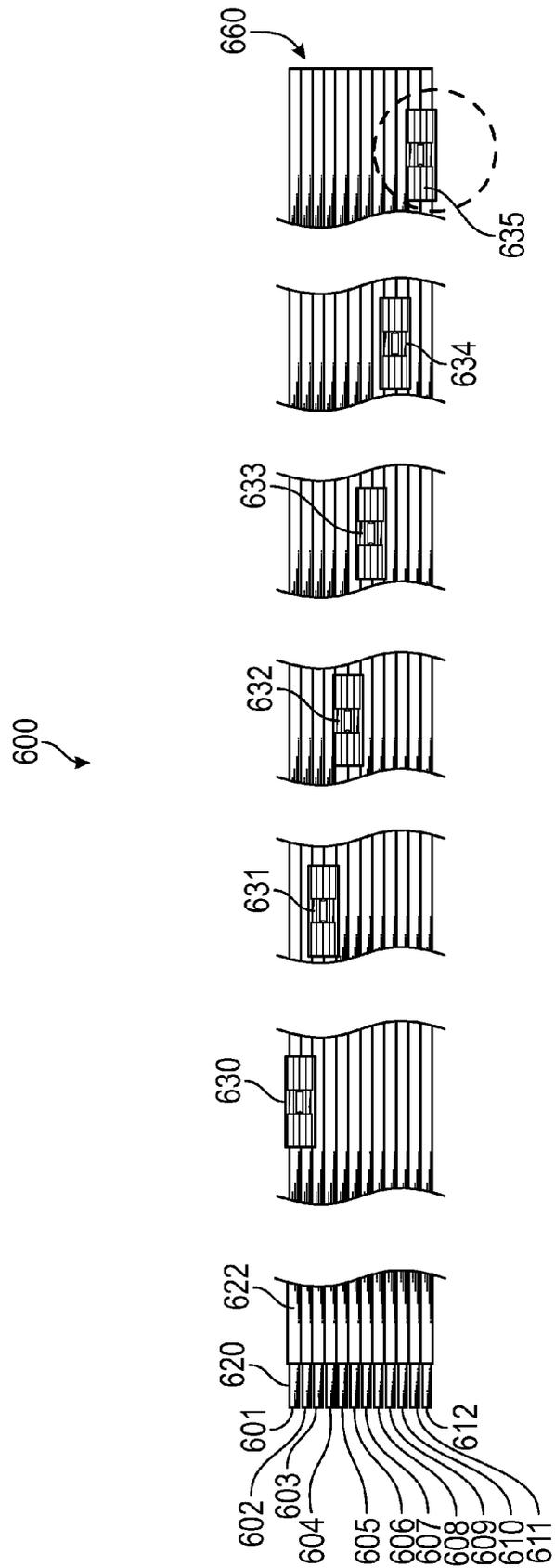


FIG. 2G



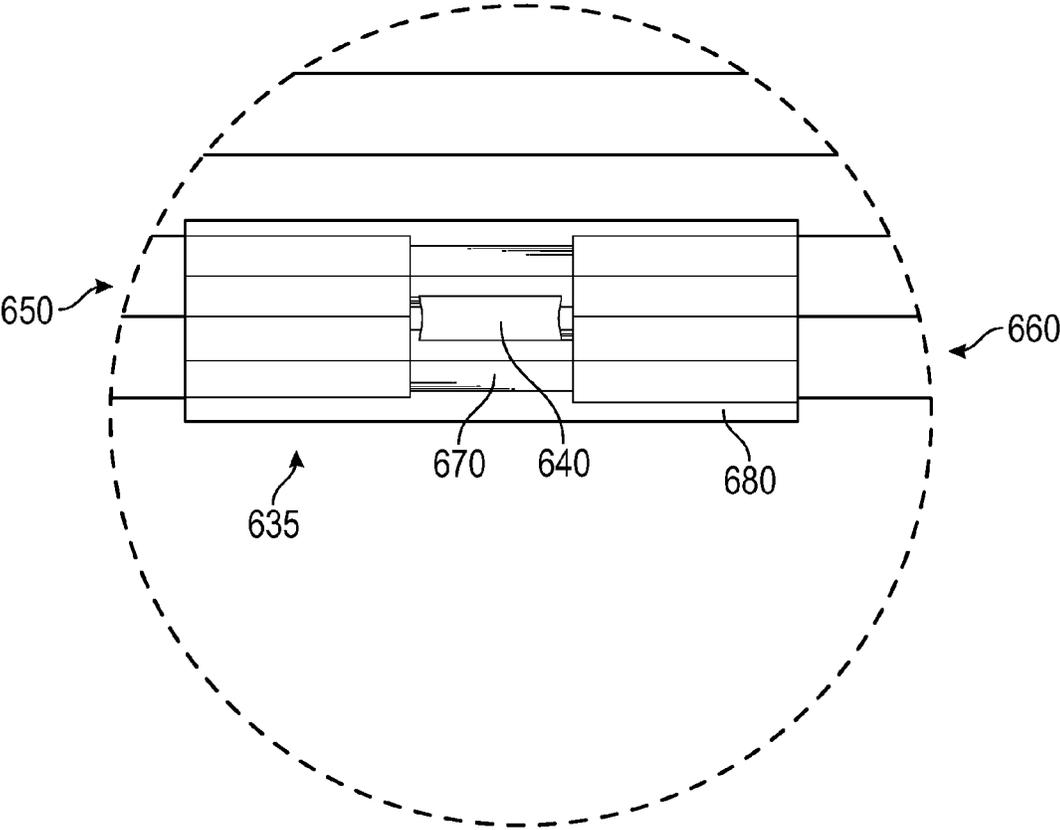


FIG. 21

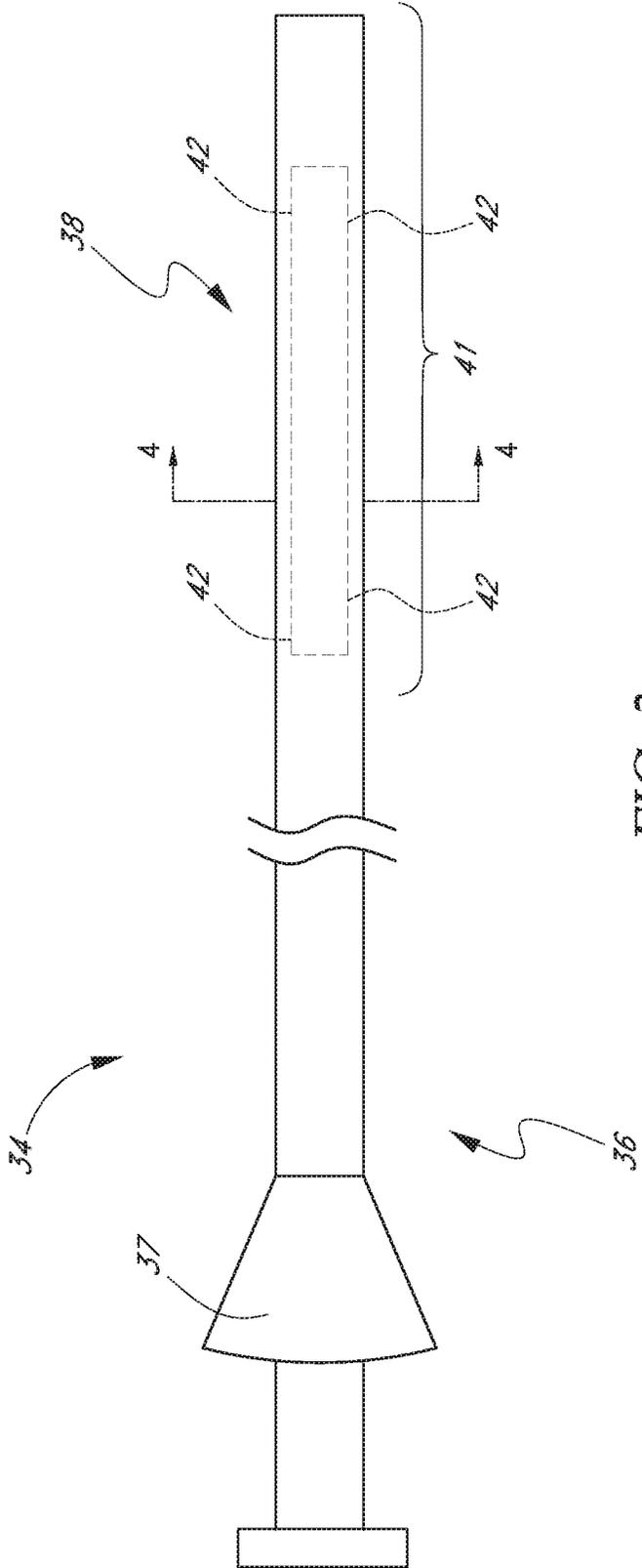


FIG. 3

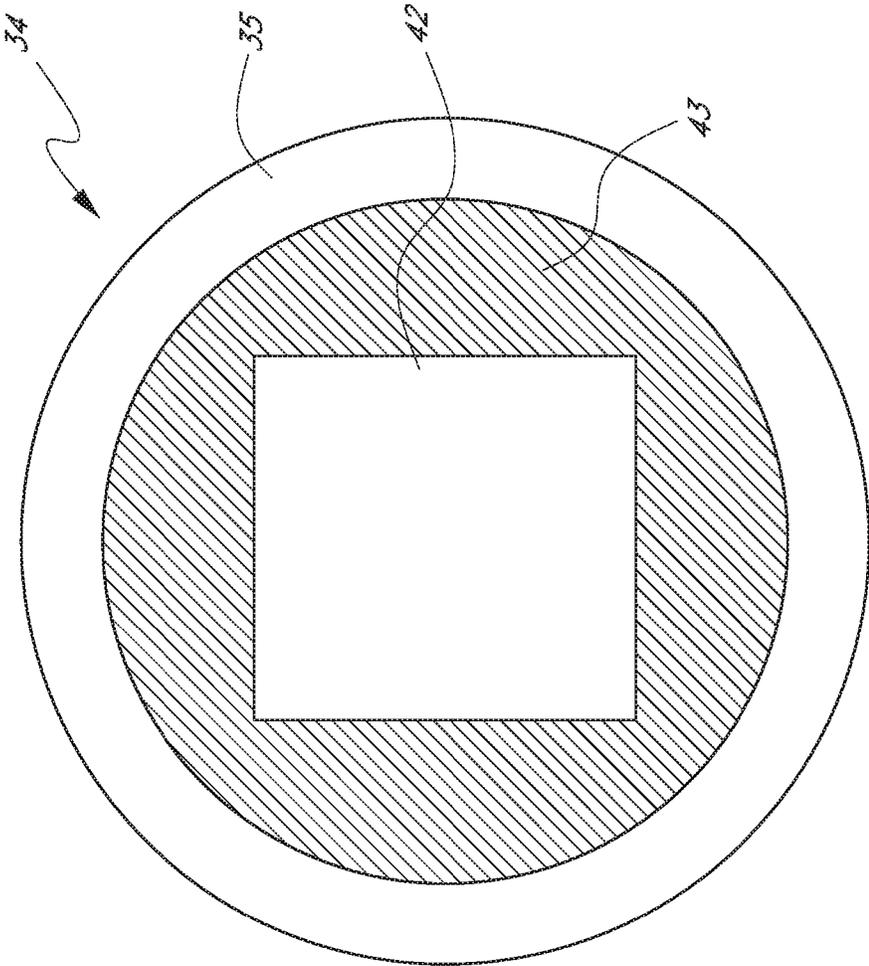
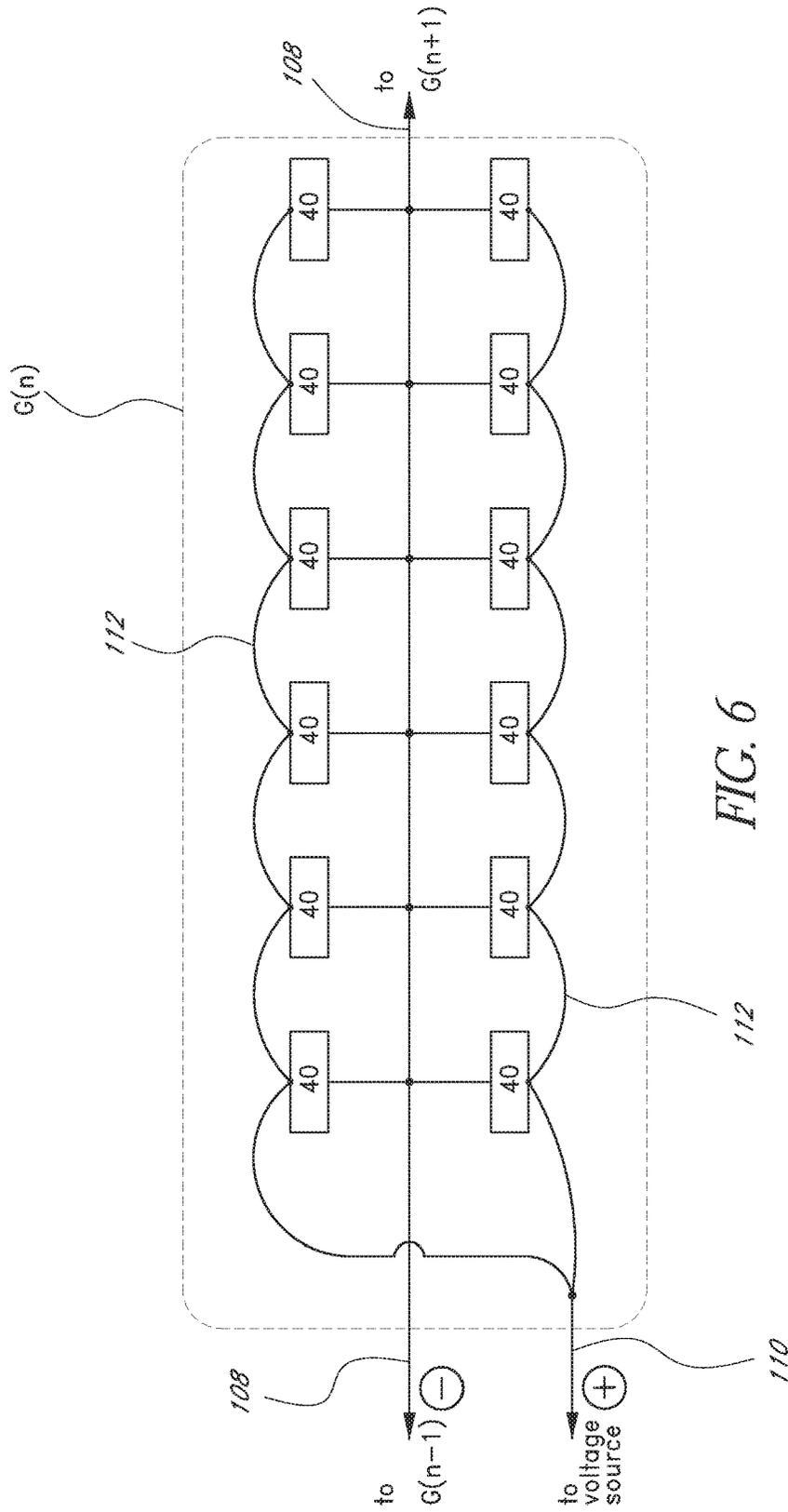


FIG. 4



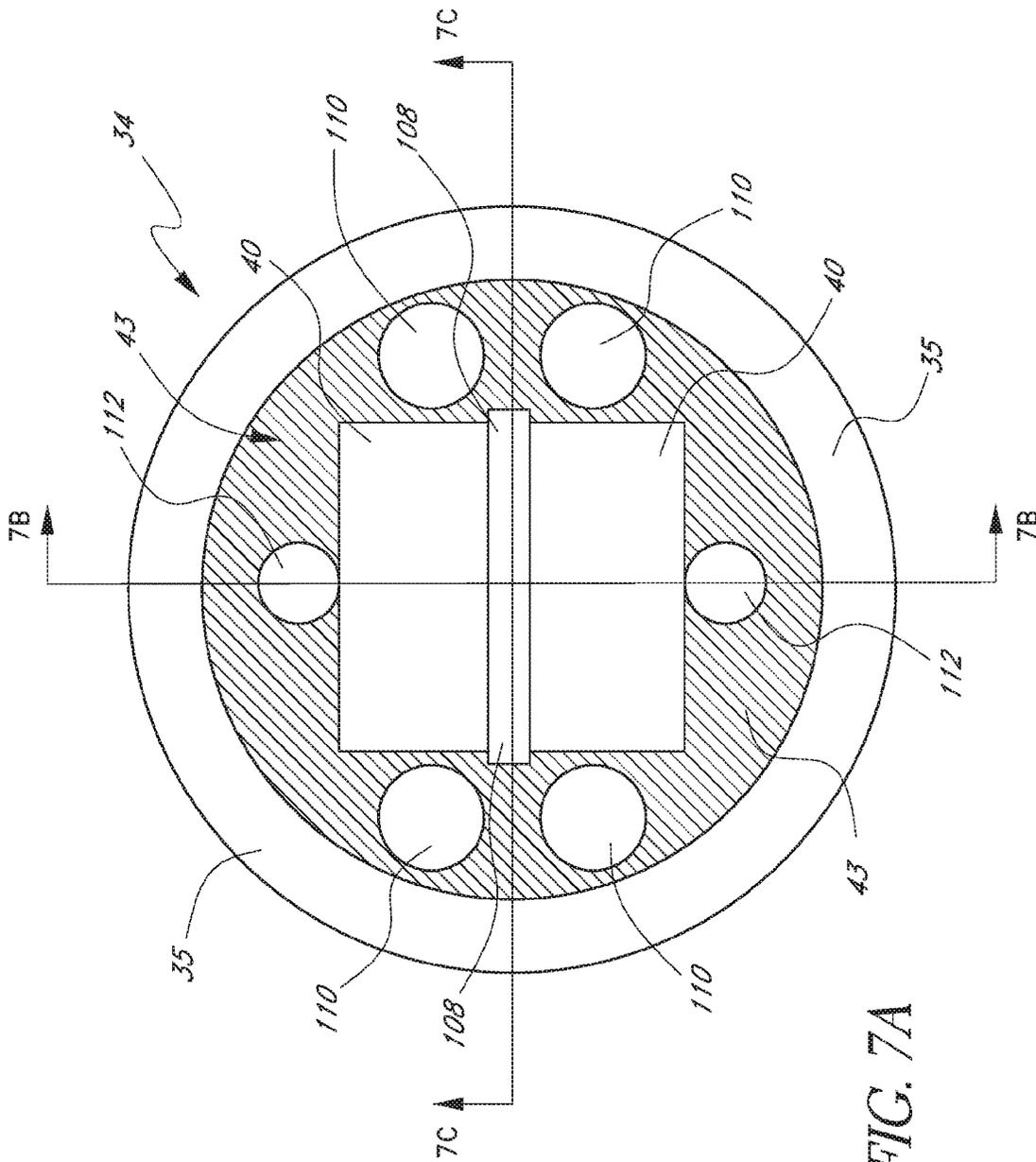


FIG. 7A

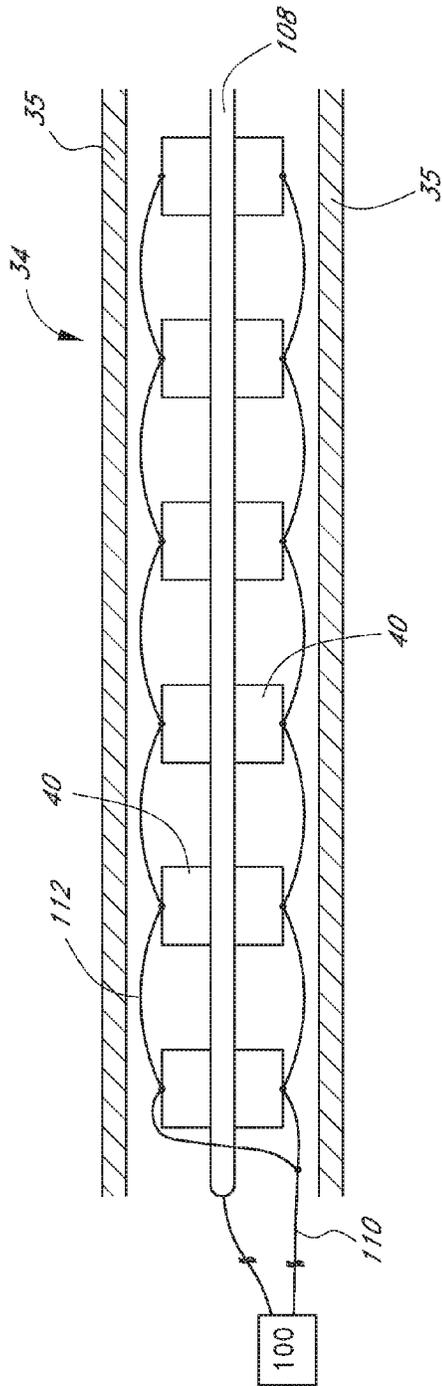


FIG. 7B

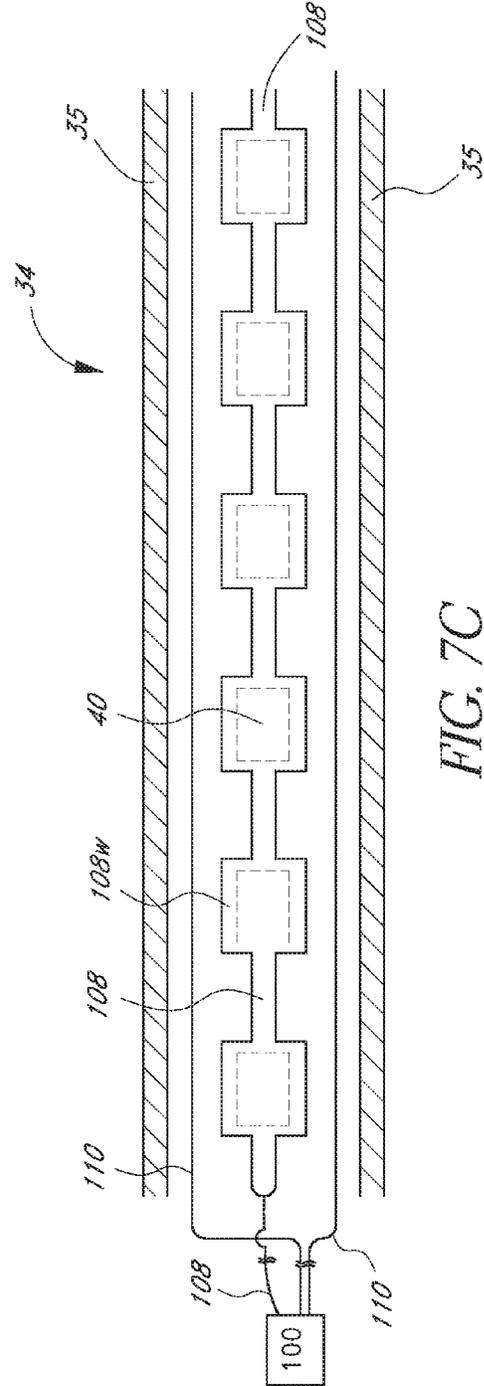


FIG. 7C

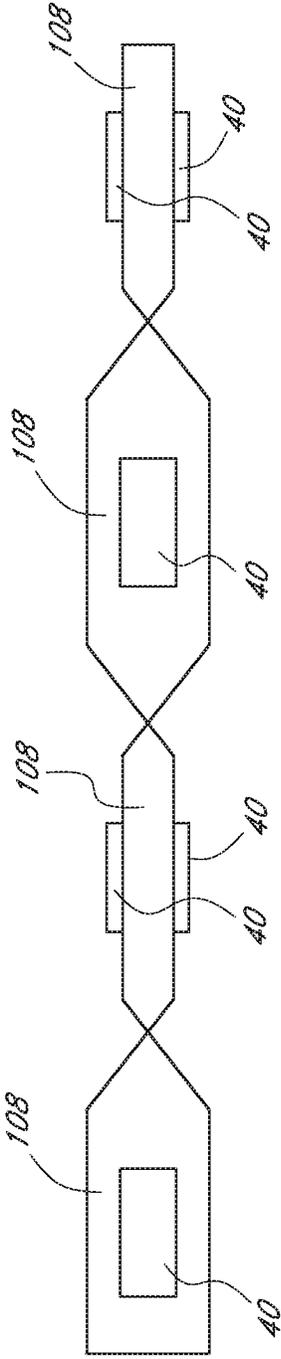


FIG. 7D

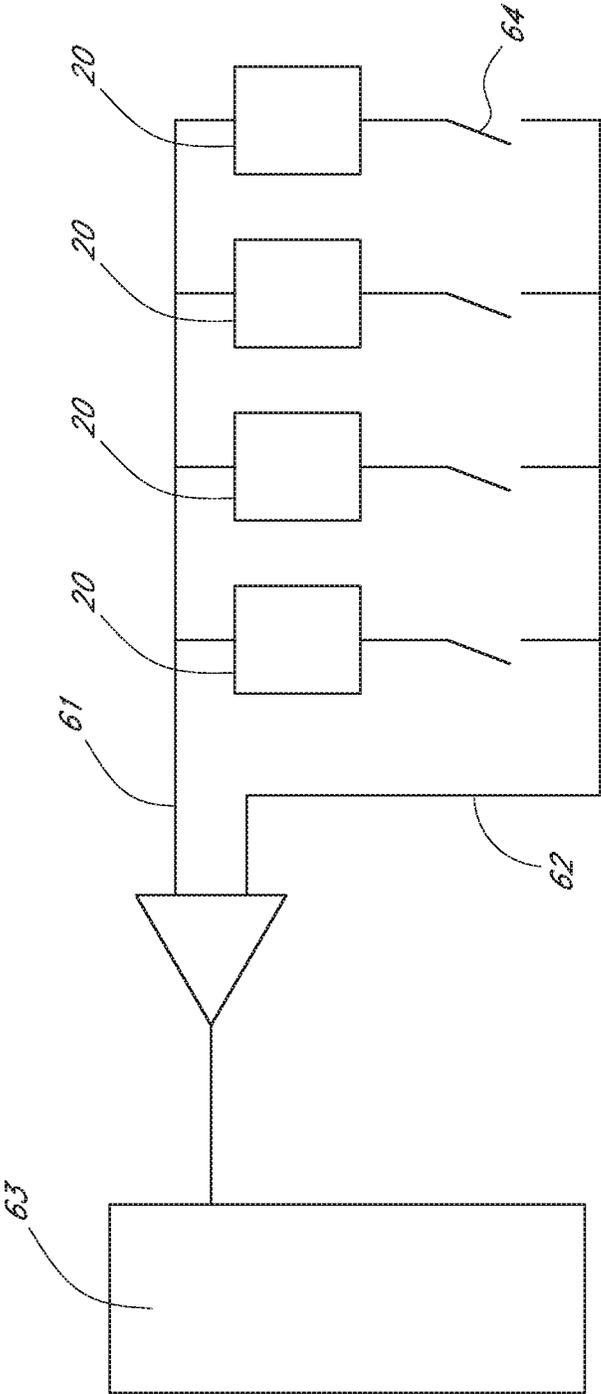


FIG. 9

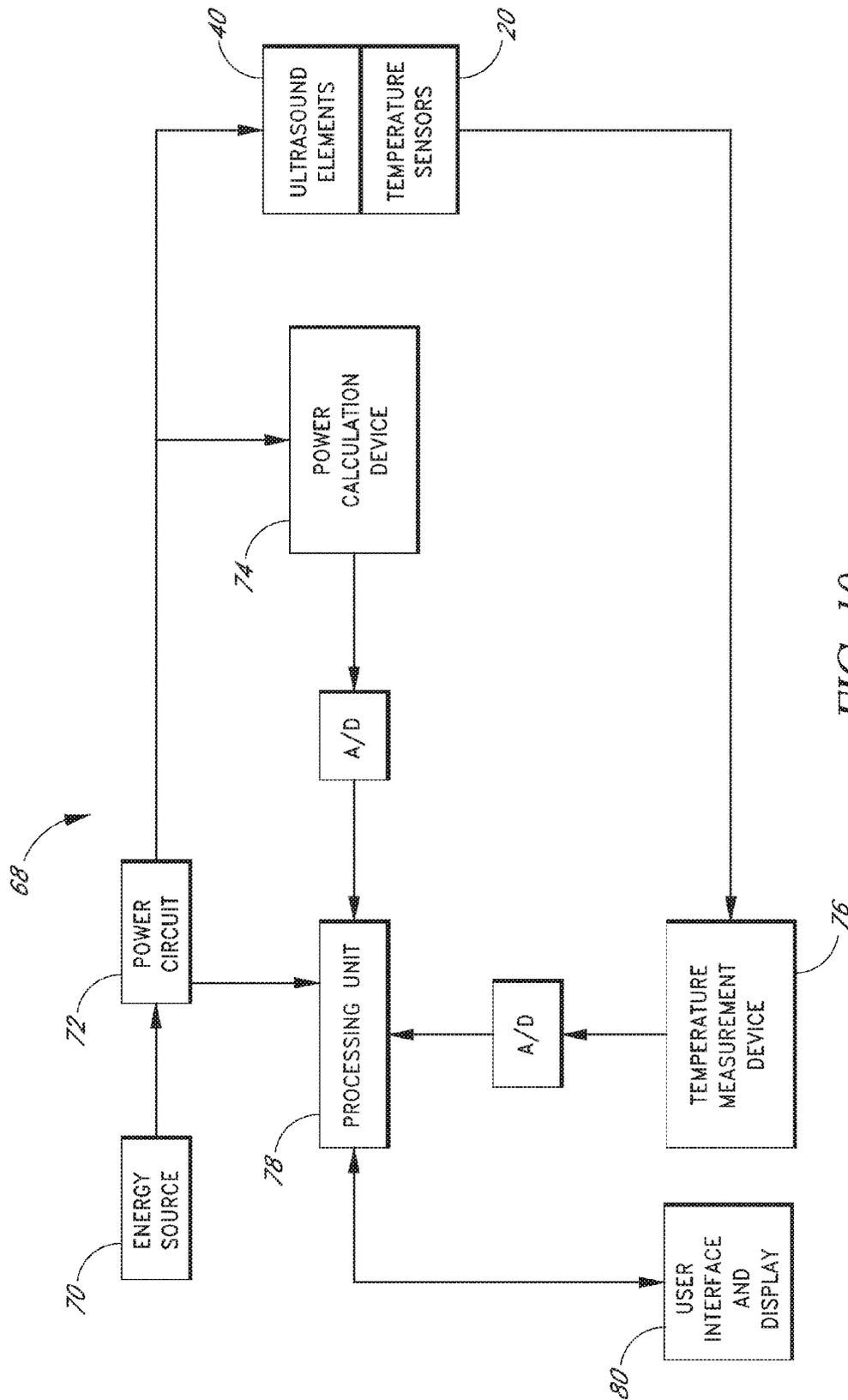


FIG. 10

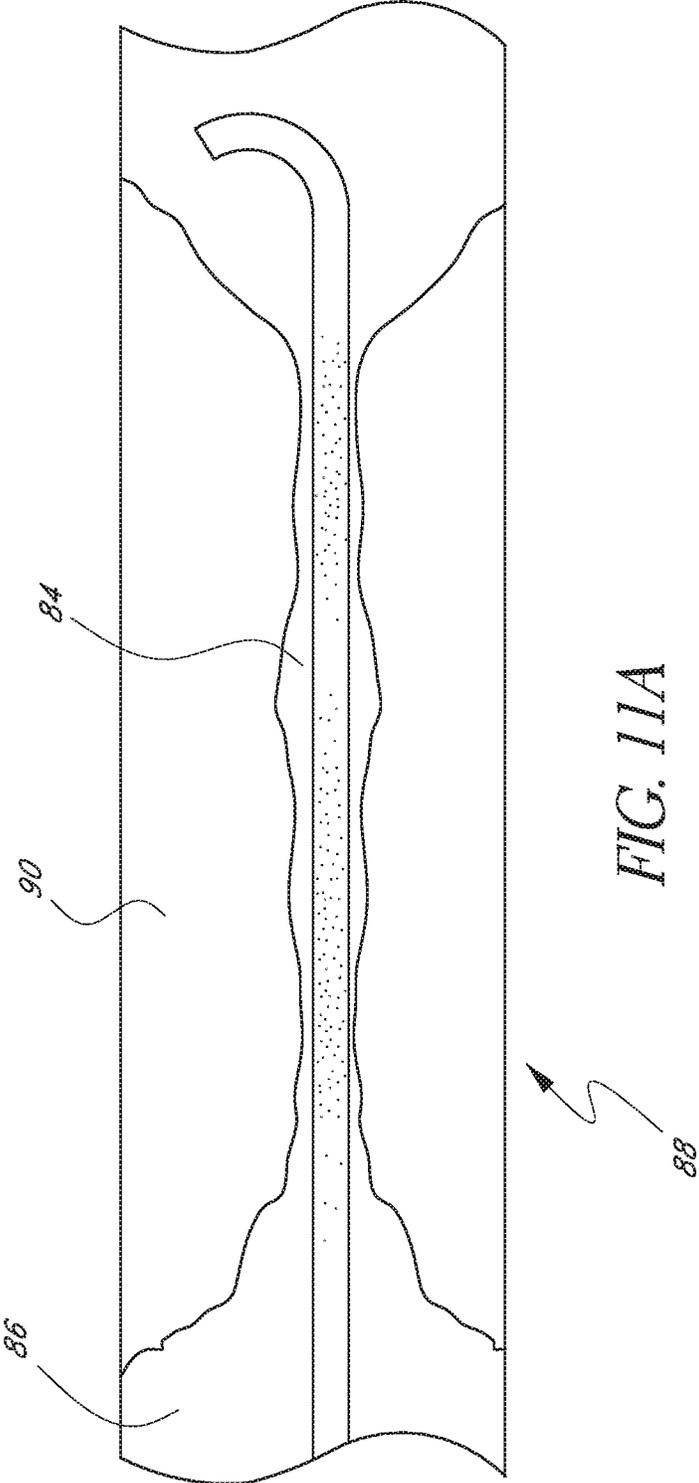
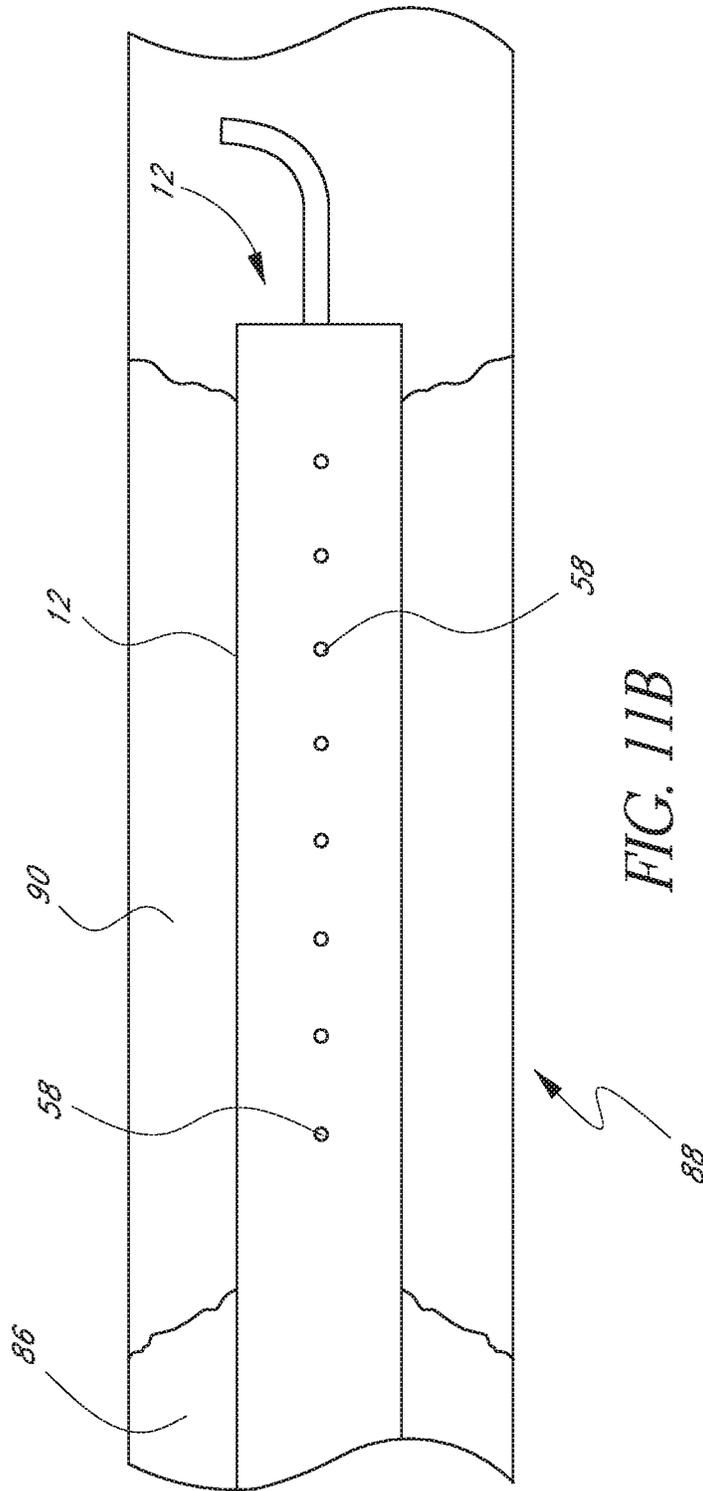


FIG. 11A



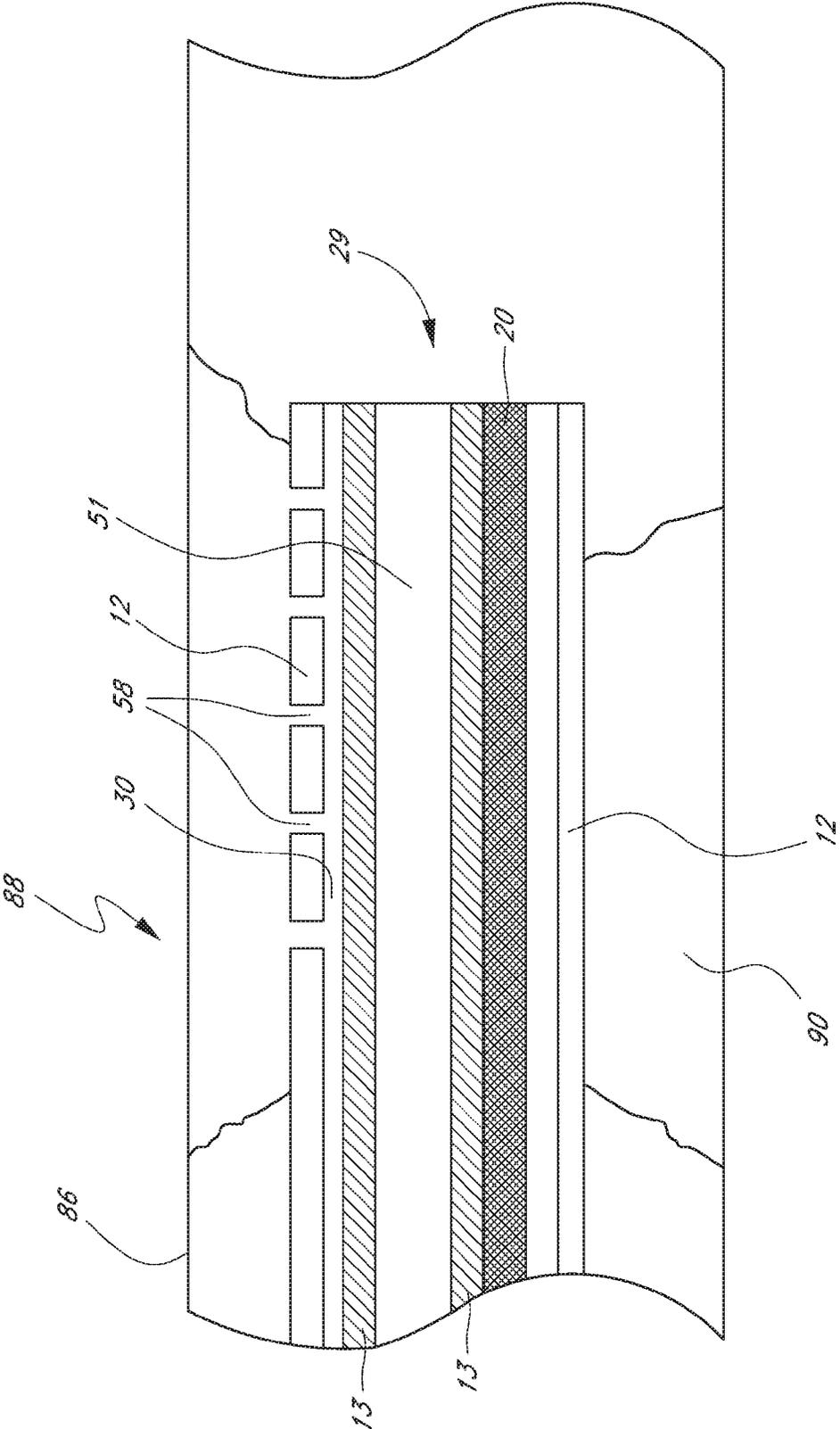


FIG. 11C

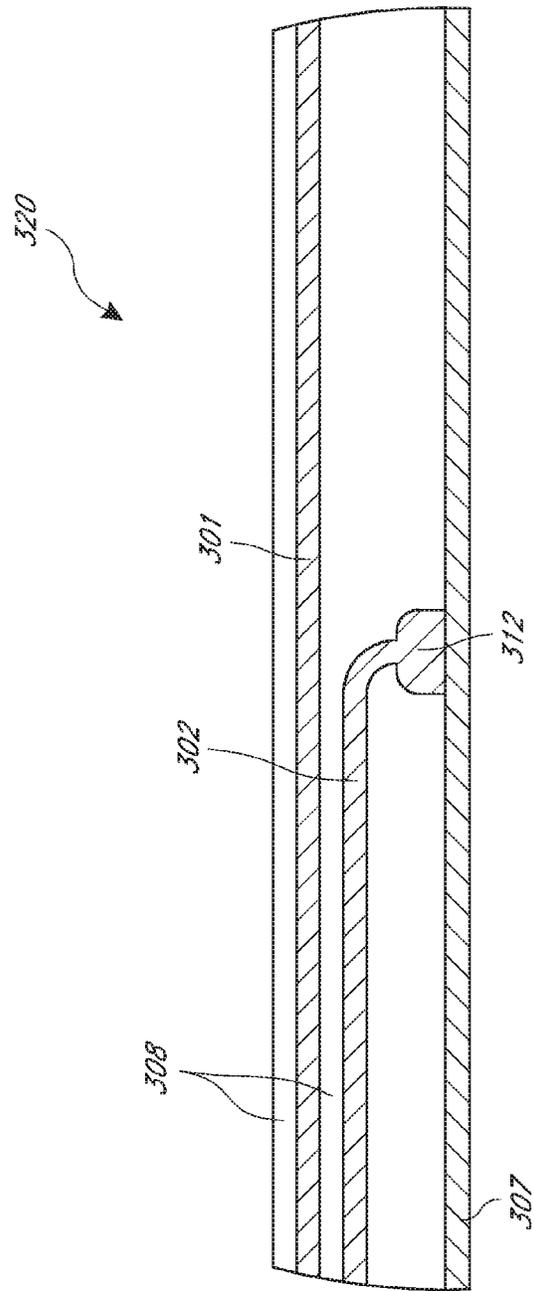


FIG. 12A

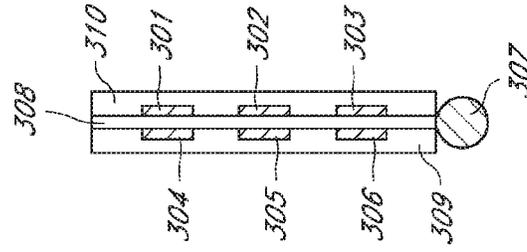


FIG. 12B

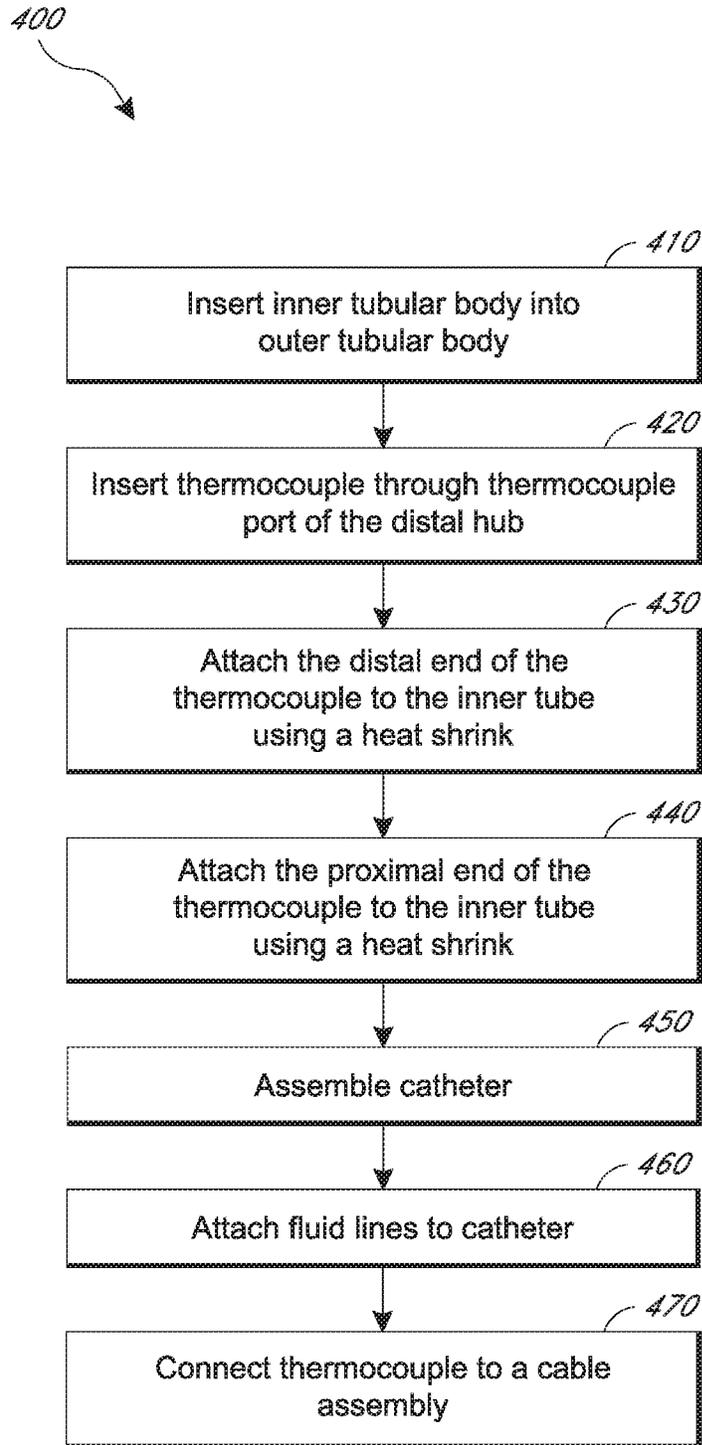


FIG. 13

ULTRASOUND CATHETER

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims priority to U.S. Provisional Application No. 62/173,863, filed Jun. 10, 2015, the entirety of which is hereby incorporated by reference herein.

FIELD

The present disclosure relates generally to an ultrasonic catheter and more specifically to an ultrasonic catheter configured to deliver ultrasonic energy and a therapeutic compound to a treatment site.

BACKGROUND

Several medical applications use ultrasonic energy. For example, U.S. Pat. Nos. 4,821,740, 4,953,565 and 5,007,438 disclose the use of ultrasonic energy to enhance the effect of various therapeutic compounds. An ultrasonic catheter can be used to deliver ultrasonic energy and a therapeutic compound to a treatment site within a patient's body. Such an ultrasonic catheter typically includes an ultrasound assembly configured to generate ultrasonic energy and a fluid delivery lumen for delivering the therapeutic compound to the treatment site.

As taught in U.S. Pat. No. 6,001,069, ultrasonic catheters can be used to treat human blood vessels that have become partially or completely occluded by plaque, thrombi, emboli or other substances that reduce the blood carrying capacity of the vessel. To remove or reduce the occlusion, the ultrasonic catheter is used to deliver solutions containing therapeutic compounds directly to the occlusion site. Ultrasonic energy generated by the ultrasound assembly enhances the effect of the therapeutic compounds. Such a device can be used in the treatment of diseases such as peripheral arterial occlusion, deep vein thrombosis or acute ischemic stroke. In such applications, the ultrasonic energy enhances treatment of the occlusion with therapeutic compounds such as urokinase, tissue plasminogen activator ("tPA"), recombinant tissue plasminogen activator ("rtPA") and the like. Further information on enhancing the effect of a therapeutic compound using ultrasonic energy is provided in U.S. Pat. Nos. 5,318,014, 5,362,309, 5,474,531, 5,628,728, 6,001,069, 6,210,356 and 7,341,569.

Another use for ultrasonic catheters is in the treatment of pulmonary embolisms. Pulmonary embolisms ("PE") are caused when a large blood clot obstructs the major blood vessels leading from the heart to the lungs. The victim's heart can be suddenly overwhelmed, with the task of pushing blood past this obstruction. About 5% of PEs are classified as massive and can result in rapid heart failure, shock and death without immediate therapy. Such massive PEs have traditionally been treated by a large dose of clot-dissolving drug (i.e., a thrombolytic). However, such treatment can result in unintended bleeding and even fatalities. Up to 40% of PEs are less critical obstructions, often called sub-massive PE. Current treatment protocols include treatment with anti-coagulant medication. Such treatments do not remove the clot but simply prevent the clot from growing larger. Recent studies suggest that failure to remove these sub-massive clots may have long-term adverse consequences including recurrent PE, chronic pulmonary hypertension and death.

SUMMARY

In some embodiments, disclosed is an ultrasound catheter that includes a first tubular body having a first longitudinal axis extending centrally through the tubular body, the first tubular body including at least one delivery port extending through a wall of the first tubular body. In some embodiments, the ultrasound catheter includes a second tubular body having a second longitudinal axis extending centrally through the second tubular body, the first and second longitudinal axes being displaced from each other such that an asymmetrical longitudinally extending gap is formed between an outer surface of the second tubular body and an interior surface of the first tubular body. In some embodiments, the ultrasound catheter includes a temperature sensor forming a thermocouple extending longitudinally within the gap between the first tubular body and the second tubular body. In some embodiments, the disclosure includes an inner core positioned within the second tubular body, the inner core comprising at least one ultrasound element. In certain embodiments, the temperature sensor comprises a flexible circuit. In certain embodiments, the temperature sensor comprises a plurality of filament pairs wherein each of the filaments is insulated; and a plurality of thermocouples wherein each of the plurality of thermocouples are formed between each of the plurality of filament pairs.

In some embodiments, disclosed is a method of manufacturing a catheter. In some embodiments, the method includes inserting an inner tubular body into an outer tubular body. In some embodiments, the method includes placing a temperature sensor between the outer and inner tubular body, wherein the temperature sensor is adjacent to an outer surface of the inner tubular body such that the inner tubular body does not extend along the same longitudinal axis as the outer tubular body. In certain embodiments, the temperature sensor comprises a flexible circuit. In certain embodiments, the temperature sensor comprises a plurality of filament pairs wherein each of the filaments is insulated; and a plurality of thermocouples wherein each of the plurality of thermocouples are formed between each of the plurality of filament pairs.

In some embodiments, disclosed is an ultrasound catheter including an elongate inner tubular body. In some embodiments, the ultrasound catheter includes an elongate outer tubular wherein the elongate inner tubular body is positioned within the elongate outer tubular body to form an asymmetrical gap between an outer surface of the inner tubular body and an interior surface of the elongate outer tubular body to form a fluid delivery lumen. In some embodiments, the ultrasound catheter includes a temperature sensor extending along the outer surface of the inner tubular body within the gap. In some embodiments, the ultrasound catheter includes an inner core positioned within the inner tubular body and comprising at least one ultrasound element. In certain embodiments, the temperature sensor comprises a flexible circuit. In certain embodiments, the temperature sensor comprises a plurality of filament pairs wherein each of the filaments is insulated; and a plurality of thermocouples wherein each of the plurality of thermocouples are formed between each of the plurality of filament pairs.

In some embodiments, disclosed is a method of manufacturing a catheter including inserting an inner tubular body into an outer tubular body. In some embodiments, the method of manufacturing includes placing a temperature sensor between the outer and inner tubular body, wherein the temperature sensor is adjacent to an outer surface of the

inner tubular body such that the inner tubular body does not extend along the same longitudinal axis as the outer tubular body. In certain embodiments, the temperature sensor comprises a flexible circuit. In certain embodiments, the temperature sensor comprises a plurality of filament pairs wherein each of the filaments is insulated; and a plurality of thermocouples wherein each of the plurality of thermocouples are formed between each of the plurality of filament pairs

In some embodiments, disclosed is an ultrasound catheter including an elongate inner tubular body. In some embodiments, the ultrasound catheter includes an elongate outer tubular wherein the elongate inner tubular body is positioned within the elongate outer tubular body to form an asymmetrical gap between an outer surface of the inner tubular body and an interior surface of the elongate outer tubular body to form a fluid delivery lumen. In some embodiments, the ultrasound catheter includes a temperature sensor extending along the outer surface of the inner tubular body within the gap. In some embodiments, the ultrasound catheter includes an inner core positioned within the inner tubular body and comprising at least one ultrasound element.

In some embodiments, disclosed is a flexible circuit for a catheter. In some embodiments, the flexible circuit includes a plurality of traces formed on the flexible circuit separated by insulating material. In some embodiments, the plurality of traces includes at least two traces of a first material connected to a single trace of second dissimilar material at different points along a length of the flexible circuit. In some embodiments, a temperature sensor for a catheter comprises a plurality of filament pairs wherein each of the filaments is insulated; and a plurality of thermocouples wherein each of the plurality of thermocouples are formed between each of the plurality of filament pairs.

For purposes of summarizing the invention and the advantages achieved over the prior art, certain objects and advantages of the invention have been described in this application. It is to be understood that not necessarily all such objects or advantages may be achieved in accordance with any particular embodiment of the invention. Thus, for example, those skilled in the art will recognize that the invention may be embodied or carried out in a manner that achieves or optimizes one advantage or group of advantages as taught herein without necessarily achieving other objects or advantages as may be taught or suggested herein.

All of these embodiments are intended to be within the scope of the invention herein disclosed. These and other embodiments of the present invention will become readily apparent to those skilled in the art from the following detailed description of the embodiments having reference to the attached figures, the invention not being limited to any particular embodiment(s) disclosed.

BRIEF DESCRIPTION OF THE DRAWINGS

Exemplary embodiments of the vascular occlusion treatment system are illustrated in the accompanying drawings, which are for illustrative purposes only. The drawings comprise the following figures, in, which like numerals indicate like parts.

FIG. 1A is a schematic illustration of an ultrasonic catheter configured for insertion into large vessels of the human body.

FIG. 1B is a cross-sectional view of the ultrasonic catheter of FIG. 1A.

FIG. 1C is an enlarged cross-sectional view of a hub portion of the ultrasonic catheter of FIG. 1A.

FIG. 1D is a side view of the hub portion ultrasonic catheter of FIG. 1A.

FIG. 1E is an exploded illustration the hub portion of the ultrasonic catheter of FIG. 1A.

FIG. 1F is an enlarged cross-sectional side view of a modified hub portion of the ultrasonic catheter of FIG. 1A.

FIG. 1G is a side view of an embodiment of the hub portion of the ultrasonic catheter configured for insertion into the human body.

FIG. 1H is a side view of the embodiment of the hub portion of the ultrasonic catheter of FIG. 1G with attached fluid tubes configured for insertion into the human body.

FIG. 1I is an enlarged cross-sectional view of the hub portion of the ultrasonic catheter of FIG. 1H along section A-A.

FIG. 1J is an enlarged cross-sectional view of the hub portion of FIG. 1H along section B-B.

FIG. 1K is a side view of the exterior tubular body of the hub portion of FIG. 1G.

FIG. 1L is a front view of another embodiment of the hub portion of the ultrasonic catheter configured for insertion into the human body.

FIG. 1M is a cross-sectional view of the hub portion of the ultrasonic catheter of FIG. 1L.

FIG. 1N is an enlarged cross-sectional view of the hub portion of the ultrasonic catheter of FIG. 1L along section B-B.

FIG. 1O is an enlarged cross-sectional view of the hub portion of the ultrasonic catheter of FIG. 1L along section C-C.

FIG. 2 is a cross-sectional view of the ultrasonic catheter taken along line 2-2 of FIG. 1C or anywhere along the length of the exterior tubular body of FIG. 1K.

FIG. 2A is a cross-sectional, view of another embodiment of the ultrasonic catheter taken along line 2-2 of FIG. 1C or anywhere along the length of the exterior tubular body of FIG. 1K.

FIG. 2B is a top cross-sectional view of an embodiment of a flexible circuit ("flexcircuit") that can be configured to form a thermocouple to serve as a temperature sensor in the ultrasonic catheter illustrated in FIGS. 1A-1O and FIGS. 2-2A.

FIG. 2C is a side cross-sectional view of the embodiment of the flexcircuit illustrated in FIG. 2B.

FIG. 2D is a side view of an embodiment of a temperature sensor composed of a plurality of insulated wires configured to form a plurality of thermocouples.

FIG. 2E is a top view of an embodiment of the temperature sensor of FIG. 2D.

FIG. 2F is an enlarged top view of a thermocouple junction of the temperature sensor of FIG. 2D.

FIG. 2G is a side view of another embodiment of a temperature sensor composed of a plurality of insulated wires configured to form a plurality of thermocouples.

FIG. 2H is a top view of another embodiment of a temperature sensor of FIG. 2G.

FIG. 2I is an enlarged top view of a thermocouple junction of the temperature sensor of FIG. 2G.

FIG. 3 is a schematic illustration of an elongate inner core configured to be positioned within the central lumen of the catheter illustrated in FIG. 2.

FIG. 4 is a cross-sectional view of the elongate inner core of FIG. 3 taken along line 4-4.

FIG. 5 is a schematic wiring diagram illustrating an exemplary technique for electrically connecting five groups of ultrasound radiating members to form an ultrasound assembly.

FIG. 6 is a schematic wiring diagram illustrating an exemplary technique for electrically connecting one of the groups of FIG. 5.

FIG. 7A is a schematic illustration of the ultrasound assembly of FIG. 5 housed within the inner core of FIG. 4.

FIG. 7B is a cross-sectional view of the ultrasound assembly of FIG. 7A taken along line 7B-7B.

FIG. 7C is a cross-sectional view of the ultrasound assembly of FIG. 7A taken along line 7C-7C.

FIG. 7D is a side view of an ultrasound assembly center wire twisted into a helical configuration.

FIG. 8 illustrates the energy delivery section of the inner core of FIG. 4 positioned within the energy delivery section of the tubular body of FIG. 2.

FIG. 9 illustrates a wiring diagram for connecting a plurality of temperature sensors with a common wire.

FIG. 10 is a block diagram of a feedback control system for use with an ultrasonic catheter.

FIG. 11A is a side view of a treatment site.

FIG. 11B is a side view of the distal end of an ultrasonic catheter positioned at the treatment site of FIG. 11A.

FIG. 11C is a cross-sectional schematic view of the distal end of the ultrasonic catheter of FIG. 11B positioned at the treatment site before a treatment.

FIG. 11D is a cross-sectional schematic view of the distal end of the ultrasonic catheter of FIG. 11C, wherein an inner core has been inserted into the tubular body to perform a treatment.

FIG. 12A is a horizontal cross-section showing a top view of another embodiment of a flexcircuit, with protective second coverlay 310 removed, that can be configured to form a thermocouple to serve as a temperature sensor in the ultrasonic catheter illustrated in FIGS. 1A-E.

FIG. 12B is a vertical cross-sectional view of the embodiment of the flexcircuit illustrated in FIG. 12A at a more proximal point.

FIG. 13 illustrates a schematic of a method of manufacturing a catheter comprising a flexcircuit.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

As described above, it is desired to provide an ultrasonic catheter also referred to herein as “ultrasound catheter(s)” having various features and advantages. Examples of such features and advantages include the ability to apply ultrasonic energy to a treatment site. In other embodiments, the catheter has the ability to deliver a therapeutic compound to the treatment site. Embodiments of an ultrasonic catheter having certain of these features and advantages are described herein. Methods of using such an ultrasonic catheter are also described herein.

The ultrasonic catheters also referred to herein as “ultrasound catheter(s)” described herein can be used to enhance the therapeutic effects of therapeutic compounds at a treatment site within a patient’s body. As used herein, the term “therapeutic compound” refers broadly, without limitation, to a drug, medicament, dissolution compound, genetic material, anti-cancer drug, or any other substance capable of effecting physiological functions. Additionally, any mixture comprising any such substances is encompassed within this definition of “therapeutic compound”, as well as any substance falling within the ordinary meaning of these terms.

The enhancement of the effects of therapeutic compounds using ultrasonic energy is described in U.S. Pat. Nos. 5,318,014, 5,362,309, 5,474,531, 5,628,728, 6,001,069 and 6,210,356, the entire disclosures of which are hereby incorporated by herein by reference. Specifically, for applications that treat human blood vessels that have become partially or completely occluded by plaque, thrombi, emboli or other substances that reduce the blood carrying capacity of a vessel, suitable therapeutic compounds include, but are not limited to, an aqueous solution containing Heparin, Urokinase, Streptokinase, TPA and BB-10153 (manufactured by British Biotech, Oxford, UK).

Certain features and aspects of the ultrasonic catheters disclosed herein may also find utility in applications where the ultrasonic energy itself provides a therapeutic effect. Examples of such therapeutic effects include preventing or reducing stenosis and/or restenosis; tissue ablation, abrasion or disruption; promoting temporary or permanent physiological changes in intracellular or intercellular structures; and rupturing micro-balloons or micro-bubbles for therapeutic compound delivery. Further information about such methods can be found in U.S. Pat. Nos. 5,261,291 and 5,431,663, the entire disclosures of which are hereby incorporated by herein by reference.

The ultrasonic catheters described herein can, be configured for applying ultrasonic energy over a substantial length of a body lumen, such as, for example, the larger vessels located in the leg. In other embodiments, the catheter can be configured for treatment of pulmonary embolisms, (“PE”), which can be caused when a large blood clot obstructs the major blood vessels leading from the heart to the lungs. However, it should be appreciated that certain features and aspects of the present disclosure may be applied to catheters configured to be inserted into other vessels or cavities such as the small cerebral vessels, in solid tissues, in duct systems and in body cavities. Additional embodiments that may be combined with certain features and aspects of the embodiments described herein are described in U.S. Patent Publication US2004/0019318, entitled “Ultrasonic Assembly For Use With A Catheter” and filed Nov. 7, 2002, the entire disclosure of which is hereby incorporated herein by reference.

FIG. 1A schematically illustrates an ultrasonic catheter 10 configured for use in the large vessels of a patient’s anatomy. For example, the ultrasonic catheter 10 illustrated in FIG. 1A can be used to treat long segment peripheral arterial occlusions, such as those in the vascular system of the leg. In other examples, the ultrasonic catheter 10 illustrated in FIG. 1A can be used for treatment of a pulmonary embolism as described, for example, in U.S. Patent Publication US2012/0289889 (filed May 10, 2012), which is hereby incorporated by reference herein in its entirety. As will be explained in detail below, in some embodiments, the catheter is configured to be introduced into the patient’s major blood vessels leading from the heart to the lungs (e.g., the pulmonary artery). In one embodiment of use, femoral venous access may be used to place the catheter 10 into such vessels. In such embodiments, the catheter 10 can be advanced through femoral access site, through the heart and into the pulmonary artery. The dimensions of the catheter 10 are adjusted based on the particular application for which the catheter 10 is to be used.

As illustrated in FIG. 1A, the ultrasonic catheter 10 can include a multi-component, elongate flexible exterior tubular body 12 having a proximal region 14 and a distal region 15. The exterior tubular body 12 can include a flexible energy delivery section 18 located in the distal region 15 of

the catheter 10. The exterior tubular body 12 and other components of the catheter 10 can be manufactured in accordance with any of a variety of techniques well known in the catheter manufacturing field. Suitable materials and dimensions can be readily selected based on the natural and anatomical dimensions of the treatment site and on the desired percutaneous access site.

For example, in some embodiments, the proximal region 14 of the exterior tubular body 12 can comprise a material that has sufficient flexibility, kink resistance, rigidity and structural support to push the energy delivery section 18 through the patient's vasculature to a treatment site. Examples of such materials include, but are not limited to, extruded polytetrafluoroethylene ("PTFE"), polyethylenes ("PE"), polyamides and other similar materials. In certain embodiments, the proximal region 14 of the exterior tubular body 12 is reinforced by braiding, mesh or other constructions to provide increased kink resistance and pushability. For example, nickel titanium or stainless steel wires can be placed along or incorporated into the exterior tubular body 12 to reduce kinking.

In some embodiments configured for treating thrombus in the arteries of the leg, the exterior tubular body 12 has an outside diameter between about 0.060 inches and about 0.075 inches (between about 0.15 cm and about 0.19 cm). In another embodiment, the exterior tubular body 12 has an outside diameter of about 0.071 inches (about 0.18 cm). In certain embodiments, the exterior tubular body 12 has an axial length of approximately 106 to 135 centimeters, although other lengths may be appropriate for other applications.

The energy delivery section 18 of the exterior tubular body 12 can include a material that is thinner than the material comprising the proximal region 14 of the exterior tubular body 12 or a material that has a greater acoustic transparency. Thinner materials generally have greater acoustic transparency than thicker materials. Suitable materials for the energy delivery section 18 can include, but are not limited to, high or low density polyethylenes, urethanes, nylons, and the like. In certain modified embodiments, the energy delivery section 18 may be formed from the same material or a material of the same thickness as the proximal region 14.

In certain embodiments, the exterior tubular body 12 can be divided into three sections of varying stiffness. In some embodiments, the first section, can include the proximal region 14, which can have a relatively higher stiffness. The second section, which can be located in an intermediate region between the proximal region 14 and the distal region 15 of the exterior tubular body 12, can have a relatively lower stiffness. This configuration further facilitates movement and placement of the catheter 10. The third section, which can include the energy delivery section 18, can, be generally lower in stiffness than the second section in spite of the presence of the ultrasound radiating members 40.

To provide access to the interior of the exterior tubular body 12, a plurality of inlets can be fluidly connected to the proximal region 14 of catheter 10. In some examples, the proximal region 14 of the catheter 10 can include a cooling inlet port 46, a drug inlet port 32, and/or a proximal access port 31. In some embodiments, to provide an electrical connection to the energy delivery section 18, the catheter 10 can further include a cable 45 that can include a connector 101 to the control system 100 (shown in FIG. 10). In some variants, the cable 45 can be connected to the catheter 10 at the proximal region 14 through the proximal access port 31. In some examples, the catheter 10 can further include a

backend hub 33 that helps to secure the various inlet ports at the proximal region 14 of the catheter 10.

FIGS. 1B-E illustrate various views of the ultrasound catheter of FIG. 1A. FIGS. 1B-1C illustrate cross-sectional views of the hub 33 and FIG. 1D-D illustrates a side view of the hub 33. FIG. 1E illustrates an exploded view of the hub 33.

FIG. 2 illustrates a cross section of the exterior tubular body 12 taken along line 2-2 in FIG. 1B. As shown in FIG. 2, in the illustrated embodiment the catheter 10 may be formed of two lumens—fluid delivery lumen 30 and central lumen 51, which can be formed from an interior wall of an exterior tubular body 12 and an interior wall of an interior tubular body 13, respectively. In some examples, the interior tubular body 13 can be located within the exterior tubular body 12 such that a gap 52 is formed between an interior wall of the exterior tubular body 12 and an exterior wall of the interior tubular body 13 such that the fluid delivery lumen 30 extends coaxially about the interior tubular body. In the embodiment shown in FIG. 2, the exterior tubular body 12 has a first longitudinal axis L1 extending centrally through the exterior tubular body 12, and the interior tubular body 13 has a second longitudinal axis L2 extending centrally through the interior tubular body 13. The first and second longitudinal axes L1, L2 are displaced from each other such that an asymmetrical gap 52 is formed between an outer surface of the interior tubular body 13 and an interior surface of the exterior tubular body 12. In other embodiments, more or fewer fluid delivery lumens can be formed by a plurality of tubular bodies located within the exterior tubular body 12 and/or by the addition of dividers and/or channels.

With continued reference to FIG. 2, in some examples, the exterior tubular body 12 can further include a temperature sensor 20 that can be positioned within the fluid delivery lumen 30 between the outside surface of the of the interior tubular body 13 and the interior surface of the exterior tubular body 12. As will be described in more detail below, the temperature sensor 20 shown in FIGS. 2 and 8 can be a flexible circuit or "flexcircuit" 220 as shown in FIGS. 2A and 2B or flexcircuit 320 as shown in FIGS. 12A and 12B. In some embodiments the flexible circuit is configured to form a thermocouple. In certain embodiments, the temperature sensor 20 shown in FIGS. 2 and 8 can be a ribbon thermocouple 500 as shown in FIGS. 2D-2F or a ribbon thermocouple 600 as shown in FIGS. 2G-2I. As described below, there are potential advantages to embodiments that utilize a flexible circuit 220, 320 and/or thermocouple ribbon 500, 600 as described herein. However, in certain embodiments of the ultrasonic catheter 10, the temperature sensor 20 can take other configurations or forms. In some embodiments, the temperature sensor 20 is positioned on a side of the interior tubular body 13 such that the interior tubular body 13 is positioned asymmetrically within the exterior tubular body 12. In such an arrangement, an asymmetrical longitudinally extending gap 52 is formed between an outer surface of the interior tubular body (corresponding to the second tubular body) and an interior surface of the exterior tubular body (corresponding to the first tubular body); thus in the illustrated arrangement the gap 52 between the outer surface of the interior tubular body and the interior surface of the exterior tubular body can be an asymmetrical gap 52 (a crescent shape), which can have certain advantages as described below. It is therefore preferred that the flexible circuit or ribbon thermocouple is positioned in the widest portion of the asymmetrical gap 52, and optionally, adjacent the exterior surface of the interior

tubular body. In an embodiment, the flexible circuit or ribbon thermocouple can be coupled to the outside surface of the interior tubular body 13 at one or more locations. In an embodiment, the flexible circuit or ribbon thermocouple can be coupled to the outside surface of the interior tubular body 13 at a distal end of the catheter 10. While not illustrated in FIGS. 2 and 8, in some embodiments, the flexible circuit or ribbon thermocouple can contact an interior surface of the exterior tubular body 12 (corresponding to the first tubular body) in addition to or, as an alternative, in some embodiments, to contacting the outer surface of the interior tubular body 13 (corresponding to the second tubular body). In certain embodiments, the flexible circuit 220 as shown in FIGS. 2A and 2B or flexcircuit 320 as shown in FIGS. 12A and 12B or be ribbon thermocouple 500 as shown in FIGS. 2D-2F or a ribbon thermocouple 600 as shown in FIGS. 2G-2I when positioned as shown in FIGS. 2 and 8, can bend and be curved as shown in FIGS. 2 and 8 to form a crescent shape corresponding to the outer surface of the interior tubular body 13 (corresponding to the second tubular body) and/or the interior surface of the exterior tubular body 12 (corresponding to the first tubular body).

FIG. 2A illustrates another embodiment of the cross section of an exterior tubular body 12. As shown in FIG. 2A, the exterior tubular body 12 can be disposed about the interior tubular body 13. An inner core 706 can be inserted within the interior tubular body 13 and positioned at a treatment site. As noted with regard to FIG. 2, the exterior tubular body 12 can also include a temperature sensor 20 which can be arranged in accordance with any of the embodiments described herein.

In some embodiments, the interior tubular body 13 can include an uneven exterior and/or interior surface that can, as will be discussed in more detail, additional cooling within the device. In some embodiments, the interior tubular body 13 can have a non-circular cross-section. In some embodiments, the interior tubular body 13 can include a plurality of indentations 786 and/or protrusions 787 such that the interior tubular body 13 does not have a circular interior surface and/or exterior surface. Because the diameter of the inner core 706 is less than the diameter of the interior tubular body, in an interior tubular body with a circular interior surface, the inner core 706 could be placed against the interior tubular body 13 such that there could be a relatively large portion with no or minimal gap between the exterior surface of the inner core 706 and the interior surface of the interior tubular body 13 and/or a relatively large portion with no or minimal gap between the exterior of the interior tubular body 13 and the interior of the exterior tubular body 12. This can potentially cause uneven over-heating of the inner core 706. The indentations 786 can therefore ensure that cooling fluid will have room to flow past the inner core 706 and contact more external surfaces of the inner core 706. In a similar manner, drug flowing between the interior tubular body 13 and the exterior tubular body 12 can be more uniformly distributed between the two tubular components as a result of an uneven surface about the exterior of the interior tubular body 13. In some embodiments, the exterior of the interior tubular body 13 can include indentations 788 and/or protrusions 789. In some embodiments, the plurality of indentations 788 and/or protrusions 789 can ensure that the inner core 706 does not cause overheating within the exterior tubular body 12. In some examples, as the indentations 786, 788 and/or protrusions 787, 789 can be of any shape or size, this can reduce manufacturing costs as any imperfection on the inner and/or outer surface of the tubular body 13 would provide additional cooling benefits to the

inserted inner core 706. The indentations 786, 788 and/or protrusions 787, 789 can extend longitudinally along the length of the interior tubular body 13. In certain embodiments, the indentations 786, 788 and/or protrusions 787, 789 can extend longitudinally along at least 50% of the length of the interior tubular body 13 and along at least 75% of the length of the interior tubular body 13 and in certain embodiments along at least 90% of the length of the interior tubular body 13. The embodiment of the interior tubular body 13 with indentations 786, 788 and/or protrusions 787, 789 can be used in combination with the temperature sensors described herein and/or used independently to promote uniform cooling. In some embodiments, the inner core includes a third longitudinal axis that is configured to extend centrally through the inner core. In some examples, the inner core is displaced from a first longitudinal axis that is configured to extend centrally through the exterior tubular body. In some embodiments, the inner core is displaced from a second longitudinal axis that is configured to extend centrally through the interior tubular body.

Temperature Sensor

Turning first to the flexcircuits illustrated in FIGS. 2B-C and 12A-12B, as described above, the temperature sensor 20 can comprise a flexible circuit ("flexcircuit") that is configured to form one or more thermocouples. The flexcircuit can be used to measure the temperature at different points along the length of the catheter 10, and so it is preferred that the flexible circuit extends along the length of the central first tubular body.

FIG. 2B illustrates a top view of one embodiment of the flexcircuit 220 and FIG. 2C is a cross-sectional view of the flexcircuit 220. FIGS. 12A-12B illustrate two views of another embodiment of a flexcircuit 320. With reference to FIGS. 2B and 2C, on one embodiment, the flexcircuit 220 is composed of a plurality of traces. In one embodiment, the flexcircuit 220 includes a first trace 207 that runs the entire length of the flexcircuit 220. The first trace is preferably constantan. Constantan is a copper-nickel alloy that has a constant resistivity over a wide range of temperatures. The first trace 207 can therefore provide good temperature sensitivity along its length. While a constantan trace is preferred, modified embodiments can include a trace of a different material.

To form the thermocouple, the flexcircuit 220 includes a plurality of second traces formed of a material different than the first trace 207. Each individual trace of this plurality of second traces extends from the proximal end 230 to a different point along the length of the flexcircuit 220. In some examples, the individual traces of this plurality of second traces are made of copper overlaid on the flexcircuit 220. In the illustrated embodiment, the first trace is Constantan and the plurality of second traces are formed from copper. In other embodiments, the first and second materials can be a different combination of materials. For example, the first material can be Alumel (consisting of approximately 95% nickel, 2% manganese, 2% aluminium and 1% silicon) and the second material can be Chromel (90% nickel and 10% chromium) as can be found in a Type K thermocouple or other combinations of dissimilar materials. In one example, the flexcircuit 220 can include a trace 201 that extends from the proximal end 230 of the flexcircuit 220 to a joint 211 at the distal end 240 of the flexcircuit 220. Similarly, the flexcircuit 220 can include one or more of any of the following traces: trace 201 that extends from the proximal end 230 to a joint 211 close to a distal end of the flexcircuit 220, trace 202 that extends from the proximal end 230 to a joint 212, trace 203 that extends from the proximal

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end **230** to a joint **213**, trace **204** that extends from the proximal end **230** to a joint **214**, trace **205** that extends from the proximal end **230** to a joint **215**, and trace **206** that extends from the proximal end **230** to a joint **216** closer to a proximal end of the flexcircuit **220**. In some examples, the plurality of joints (e.g. joint **211**, joint **212**, joint **213**, joint **214**, joint **215**, and joint **216**) allows the temperature to be taken along several points along the length of the flexcircuit **220**. In some variants, this can help to measure the temperature of the ultrasonic catheter along the entire length of the device or a portion of the device (e.g., a portion of the device that includes the ultrasound elements described below). In modified embodiments, the traces **201-206** and joints **211-216** can be arranged in different orders or configurations.

When temperature differential is experienced by the different conductors (e.g., between one of the traces **201-206** and the first trace **207**), it produces a voltage when the temperature of one of the spots differs from the reference temperature at other parts of the circuit. In this manner, temperatures along the flexcircuit **220** can be measured by measuring the voltages between one of the traces **201-206** and the first trace **207**. The illustrated preferred embodiment of FIG. 2B includes a single first trace of Constantan and six (6) traces of copper, although in other embodiments other dissimilar material combinations such as Alumel and Chromel may be used together, respectively. In modified embodiments more or fewer traces and/or traces formed of different materials each dissimilar from the first trace may be used. An advantage of the illustrated embodiment is that a single first trace can be used to measure the temperature at multiple locations along the length of the flexcircuit **220**, which can reduce the overall size of the flexcircuit as compared to a circuit with multiple first traces; in the preferred embodiment, a single Constantan trace is used as the first trace, which can reduce the overall size of the flexcircuit as compared to a circuit with multiple Constantan first traces. In modified embodiments, the flexcircuit can include multiple first traces that are each individually associated with the individual traces of the plurality of second traces of dissimilar materials.

In some embodiments, the flexcircuit **220** can be of variable length and can be configured to run the entire length or a portion of the catheter **10**. Similarly, to measure temperature along the length of the flexcircuit **220**, the distance between the joints **211-216** can be varied for the catheter **10**. In the one embodiment, the flexcircuit **220** can have a length l_1 from proximal end **230** to distal end **240** of about 115 cm. In some embodiments, the distance between each of the joints **211-216** (e.g. length l_2 , length l_3 , length l_4 , length l_5 , length l_6) can be approximately 10 cm. In additional embodiments, the distance between each of the joints **211-216** can be between 1.0 cm and 50.0 cm depending upon the number of joints and the desired overall length of the flexcircuit **220**. The distance between the joints **211-216** need not be uniform in certain embodiments. As mentioned above, in one arrangement, the joints are positioned generally along the length of the catheter in which the ultrasound elements are positioned such that the temperature of the catheter around the ultrasound elements can be monitored. Accordingly, in the illustrated embodiment the joints **211**, **212**, **213**, **214**, **215**, **216** are positioned in the energy delivery section **18** of the exterior tubular body **12**.

FIG. 2C illustrates a side cross-sectional view of the flexcircuit **220**. As described previously, the flexcircuit **220** can be formed by a plurality of layered traces. In one example, the flexcircuit **220** includes the first trace **207**

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formed on a bottom middle layer **224**. In some variants, the first trace **207** can be 0.001 inch (0.003 cm) thick. The flexcircuit **220** can include three traces **202**, **204**, **206** and **201**, **203**, **205** formed on a top middle layer **225**, respectively, that can be formed from a different material than the first trace **207** and arranged as described above. Each of the second or copper traces can be separated from each other by adhesive **231** which can fill in the gaps between layers of the flexcircuit and traces. In the illustrated embodiments the flexcircuit **220** can include a plurality of insulating layers between each of the layers containing the traces. As discussed above, aside from where a joint between two of the conductive layers are formed (e.g. joint **211**, joint **212**, joint **213**, joint **214**, joint **215**, and joint **216**), the plurality of insulating layers covers the length of the trace to insulate each of the traces from each other. The flexible circuit therefore comprises a plurality of joints **211**, **212**, **213**, **214**, **215** and **216** between the dissimilar materials of the first trace **207** and each of the plurality of second traces **201**, **202**, **203**, **204**, **205** and **206**. As illustrated in FIG. 12B, the flexcircuit **220** can include a bottom coverlay **221**, the bottom middle layer **224**, top middle layer **225**, and a top coverlay **227** that forms an insulating layer between each of the trace layers. The flexcircuit **220** of the illustrated embodiment also includes additional top insulating layer **218** and bottom insulating layer **217** which can cover electrically conducting vias which form the joints **211-216** that connect corresponding traces. In the preferred embodiment, each of these insulating layers can be formed of polyimide. In an embodiment, the top insulating layer **218** and bottom insulating layer **217** can extend along the entire length of the flexcircuit **220**. In another embodiment, the top insulating layer **218** and bottom insulating layer **217** can cover portions of the flexcircuit **220** around the joints **211-216**. In one embodiment, the joints **211-216** are formed by forming an electrically conducting via through the flexcircuit **220** to electrically connect the respective first trace **207** and second traces **201-206**. The via can then be covered with the top insulating layer **218** and bottom insulating layer **217**. As shown in FIG. 2C, gaps between the respective layers and traces can be filled in with an adhesive **231**.

FIGS. 12A-12B illustrate another embodiment of a flexcircuit **320**. FIG. 12A shows a vertical cross-sectional view of the flexcircuit **320** at a proximal point. As shown, the flexcircuit **320** can include a plurality of traces that are located on each of the top and bottom surfaces of the flexcircuit **320**. As an example illustrated in FIG. 12B, the top surface can include a plurality of second traces **301**, **302**, and **303** whereas the bottom surface can include a plurality of second traces **304**, **305**, and **306**, with a first trace **307** running laterally on a side, in this case the right side. The traces on the top and bottom surface of the flexcircuit **320** are separated by an insulator **308**. In some examples, the bottom surface of the flexcircuit **320** can include a protective first coverlay **309** whereas the top surface of the flexcircuit **320** can include a protective second coverlay **310**. The thickness of the flexcircuit **320** can be approximately 0.004 cm and the width of the flexcircuit **320** can be approximately 0.021 cm. In some embodiments, each of the traces of the flexcircuit **320** can be separated by a space of 0.003 cm.

The flexcircuit **320** can include a first material trace **307** that runs parallel to the length of the flexcircuit **320**. In order to measure temperature at a specific point along the flexcircuit **320**, each of the traces (e.g. trace **301**, trace **302**, trace **303**, trace **304**, trace **305**, and trace **306**) runs a varied distance along the flexcircuit **320**. Traces (e.g. trace **301**, trace **302**, trace **303**, trace **304**, trace **305**, and trace **306**) can

be made of a second material different from the first material. As with the embodiment of FIGS. 2A-2B, in one embodiment, the first material is Constantan and the second material is copper. In other embodiments, other dissimilar material combinations such as Alumel and Chromel can be used together. In some examples, where a temperature measurement is desired, one of the traces can make a right angle and form a node to contact the constantan trace 307.

FIG. 12A is a horizontal cross section illustrating a top view of a section of the flexcircuit 320 with protective second coverlay 310 removed. As illustrated, a temperature measurement can be obtained at node 312—a point along the flexcircuit 320. Each of the traces (e.g. trace 301, trace 302, trace 303, trace 304, trace 305, and trace 306) can run parallel along the length of the flexcircuit 320. At varying points, a node is formed where the trace turns to contact the first material trace 307. FIG. 12A shows a view taken at a more distal point than that shown in FIG. 12B, as at the segment of the flexcircuit 320 shown in FIG. 12A, the trace 303 has already formed a node to determine the temperature at a point further ahead proximally and therefore does not appear in this view. As well, trace 301 continues to run distally across the length of the segment shown in FIG. 12A and can therefore determine the temperature of the flexcircuit 320 distally further down along the length of the flexcircuit 320. The node 312 (and any of nodes 311, 313, 314, 315 and 316 (not shown)) can have a width of 0.011 cm and a height of 0.006 cm. Nodes 311, 312, 313, 314, 315 and 316 therefore constitute a plurality of joints between the dissimilar materials of the first material trace 307 and each of the plurality of second traces 301, 302, 303, 304, 305 and 306.

In certain embodiments, the temperature sensor 20 can be a ribbon thermocouple composed of a plurality of wires or that are coupled together. For example, FIGS. 2D-2F illustrate an embodiment of ribbon thermocouple 500. In some embodiments, the ribbon thermocouple 500 can be composed of a plurality of filaments and a plurality of thermocouple junctions. The plurality of filaments can be adhered together along the entire length of the ribbon thermocouple 500, from the proximal end 550 to the distal end 560. As will be discussed in more detail below, each of the plurality of filaments are adhered together except within 0.50 inches of the formed thermocouple junction.

As shown in FIG. 2E, in some embodiments, the ribbon thermocouple 500 can include filament 501, filament 502, filament 503, filament 504, filament 505, filament 506, filament 507, filament 508, filament 509, filament 510, filament 511, and filament 512. In some examples, each of the filaments is composed of a conductor 520 and an insulator 522. In some embodiments, the conductor 520 of each of the filaments is composed of a material such as copper or constantan. In some embodiments, the material of the conductor 520 of each of the filaments alternates. For example, filament 501, filament 503, filament 505, filament 507, filament 509, and filament 511 is composed of copper and filament 502, filament 504, filament 506, filament 508, filament 510, and filament 512 is composed of constantan. In some embodiments, the insulator 522 of each of the filaments is composed of polyesterimide.

In some examples, the ribbon thermocouple 500 can be configured to form a plurality of thermocouples along the length of the ribbon thermocouple 500 from the proximal end 550 to the distal end 560. In some embodiments, each of the thermocouples can be formed by stripping adjacent filaments of insulation and soldering the exposed conductor 520 together to form a thermocouple joint. As illustrated in

FIGS. 2D-2E, thermocouple junction 530 can be formed by stripping filament 501 and filament 502 and soldering them together, thermocouple junction 531 can be formed by stripping filament 503 and filament 504 and soldering them together, thermocouple junction 532 can be formed by stripping filament 505 and filament 506 and soldering them together, thermocouple junction 533 can be formed by filament 507 and filament 508 and soldering them together, thermocouple junction 534 can be formed by filament 509 and filament 510 and soldering them together, and thermocouple junction 535 can be formed by filament 511 and filament 512 and soldering them together.

In some examples, the two filaments of the thermocouple junction are formed of different materials. In some embodiments, one of the two filaments of the thermocouple junction is formed of copper and one of the two filaments of the thermocouple junction is formed of constantan.

As shown in FIG. 2E, in some embodiments, the filaments are terminated at the formed thermocouple junction. FIG. 2F illustrates an enlarged view of the thermocouple junction 535 along section A-A of FIG. 2E. As discussed above, the distal end 560 of the pair of filaments has a stripped portion 570. In some embodiments, the stripped portion 570 of the pair of filaments is attached together with a solder 540. In some examples, the attachment of the two filaments is done by laser welding. In some examples, the insulation of the pair of filaments is laser stripped. In, some embodiments, the solder is composed of about 95% to about 99% tin. In some examples, the thermocouple junction 535 includes a joint insulation 580. In some embodiments, the joint insulation 580 is composed of a polymer.

FIGS. 2G-2I illustrate another embodiment of a ribbon thermocouple 600 composed of a plurality of filaments and a plurality of thermocouple junctions. The plurality of filaments can be adhered together along the entire length of the ribbon thermocouple 600, from the proximal end 650 to the distal end 660. As will be discussed in more detail below, each, of the plurality of filaments can be adhered together along the entire length of the ribbon thermocouple 600.

As shown in FIG. 2H, in some embodiments, the ribbon thermocouple 600 can include filament 601, filament 602, filament 603, filament 604, filament 605, filament 606, filament 607, filament 608, filament 609, filament 610, filament 611, and filament 612. In some examples, each of the filaments is composed of a conductor 620 and an insulator 622. In some embodiments, the conductor 620 of each of the filaments is composed of a material such, as copper or constantan. In some embodiments, the conductor 620 of each of the filaments alternates. For example, filament 601, filament 603, filament 605, filament 607, filament 609, and filament 611 is composed of copper and filament 602, filament 604, filament 606, filament 608, filament 610, and filament 612 is composed of constantan.

In some examples, the ribbon thermocouple 600 can be configured to form a plurality of thermocouples along the length of the temperature sensor 600 from the proximal end 650 to the distal end 660. In some embodiments, each of the thermocouples can be formed by stripping adjacent filaments of insulation and soldering the exposed conductor 520 together to form a thermocouple joint. As illustrated in FIGS. 2G-2I, thermocouple junction 630 can be formed by stripping filament 601 and filament 602 and soldering them together, thermocouple junction 631 can be formed by stripping filament 603 and filament 604 and soldering them together, thermocouple junction 632 can be formed by stripping filament 605 and filament 606 and soldering them together, thermocouple junction 633 can be formed by

filament 607 and filament 608 and soldering them together, thermocouple junction 634 can be formed by filament 609 and filament 610 and soldering them together, and thermocouple junction 635 can be formed by filament 611 and filament 612 and soldering them together.

In some examples, the two filaments of the thermocouple junction are formed of different materials. In some embodiments, one of the two filaments of the thermocouple junction is formed of copper and one of the two filaments of the thermocouple junction is formed of constantan.

As shown in FIG. 2H, each of the filaments extends from the proximal end 650 to the distal end 660, with the thermocouple junctions formed on a portion of the filaments. FIG. 2I illustrates an enlarged view of the thermocouple junction 635 along section A-A of FIG. 2H. As discussed above, a portion of the pair of filaments has a stripped portion 670 to form a window in the insulator 622 along the pair of filaments. In some examples, the insulation of the pair of filaments is laser stripped. In some embodiments, the stripped portion 670 of the pair of filaments is attached together with a solder 640. In some examples, the attachment of the two filaments is done by laser welding. In some embodiments, the solder is composed of about 95% to about 99% tin. In some embodiments, the thermocouple junction 635 includes a joint insulation 680. In some examples, the joint insulation 680 is composed of a polymer.

The illustrated embodiments of FIGS. 2-2I and 12A-12B have several advantages. For example, prior art ultrasound catheters have included a plurality of separate thermocouple wires extending along the length of the catheter in order to measure the temperature of the catheter at several locations along the energy delivery section of the catheter. By replacing the plurality of wires with a single flexible circuit or ribbon thermocouple with a plurality of nodes along the length of the flexcircuit or ribbon thermocouple, the complexity and costs associated with assembling the catheter can be reduced as only a single element (flex circuit or ribbon thermocouple) needs to be inserted between the catheter elements. In addition, as shown in FIGS. 2-2A, exterior tubular body 12 and the interior tubular body 13 can be configured into an asymmetrical arrangement so as to accommodate the flexcircuit or ribbon thermocouple. This asymmetrical arrangement can provide additional room for the flexcircuit or ribbon thermocouple and its plurality of traces or wires. However, surprisingly the asymmetrical shape of the asymmetrical gap 52 between the exterior tubular body 12 and the interior tubular body 13 does not adversely affect the delivery of drug through the catheter and to the treatment zone.

In some embodiments, the ribbon thermocouple design of FIGS. 2D-2I can include a gap between each of the pair of wires that are configured to form a thermocouple. In some examples, the distance between the conductors of each of the wires is closer together than the distance between each of the pair of wires that are configured to form a thermocouple. In some embodiments, this can help with the forming of the thermocouples. The distance between each of the pair of wires can aid in the removal of insulation material and the subsequent electrical connection of the exposed, conductors. As discussed, above, in some embodiments, the formation of an electrical connection of the exposed conductors can be through welding, soldering, or other electrical coupling method.

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Turning back to FIG. 1E, to provide access to the interior of the catheter 10, the proximal region 14 can include a distal hub 65 that can provide access to the asymmetrical gap 52

and a proximal hub 60 that can be configured to provide access to the central lumen 51. With reference to FIGS. 1B and 1E, a proximal end of the exterior tubular body 12 can extend through a nose cone 70 and can be coupled to the distal hub 65 through by a barbed fitting on the distal hub 65. In this manner, the distal hub 65 can provide access to asymmetrical gap 52 between the tubular body 12 and the internal tubular body 13 as shown in FIG. 2. Fluid lumen 30 includes a gap 52 between the exterior tubular body 12 and the interior tubular body 13. With reference to FIGS. 1B and 2, the fluid lumen inlet port 32 and the cable port 47 are in communication with this asymmetrical gap 52. That is to say, the fluid lumen inlet port 32 is a first fluid injection port in fluid communication with the gap 52. A cable 45 can extend through the cable port 47 and can be coupled the temperature sensor 20. The interior tubular body 13 can extend through the distal hub 65 and can be coupled to the proximal hub 60 such that the interior of the proximal hub 60 is in communication with the central lumen 51. As shown in FIG. 1B, the interior fluid port 46 is in communication with the interior of the proximal hub 60 such that fluid injected through the fluid port 46 will enter the central lumen 51. Thus, interior fluid port 46 is a fluid injection port in fluid communication with the interior of the interior tubular body 13. As illustrated, the proximal hub 60 can, in turn, be connected to a proximal end of the internal tubular body 13 by a barbed fitting on the proximal hub. While in the illustrated embodiment, barb fittings are used to connect the exterior tubular body 12 and the internal tubular body 13 to the distal hub 65 and proximal hub 60 respectively, in modified embodiments, other connection configurations can be such as such as flanged and threaded flared connections.

For example, FIG. 1F illustrates a cross-sectional view of another embodiment of the backend hub 33'. As discussed with regard to the backend hub 33 in FIGS. 1B & 1E, the backend hub 33' can include a plurality of components that can provide access to the interior of the exterior tubular body 12. In some embodiments, the backend hub 33' can be configured to retain a proximal hub 60'.

Unlike the hub described in FIGS. 1B & 1E which is composed of a distal hub 65 and a proximal hub 60, the proximal hub 60' spans the entire length of the backend hub 33' and provides a fluid connection to the interior of the catheter 10. The proximal end of the interior tubular body 13 is secured to the inside surface of the backend hub 33' through a threaded flared fitting 71'.

The proximal hub 60' also includes a plurality of inlets to provide fluid communication with the interior of the catheter 10. The proximal hub 60' can have a proximal access port 31'. In some examples, the proximal hub 60' can include a second barb inlet 75' which can provide fluid communication to the gap 52 and a third barb inlet 63' that can provide access to the central lumen 51. In the embodiment illustrated in FIG. 1F, the cable 45' can be provided through, an opening in, the proximal hub 60'. As discussed above, the cable 45' can provide an electrical connection for the temperature sensor 20.

The proximal hub 60' can be secured to the nosecone 70' through a plurality of components. As illustrated in FIG. 1F, the distal end of the proximal hub 60' includes a plurality of threads 66a' that is secured to the inside surface of a flared fitting 66'. The flared fitting 66' can further include a plurality of barbed connectors that protrude from the surface of the nose cone 70 to secure the proximal hub 60' and flanged fitting 66' to the inside of the nosecone 70'.

With continued reference to FIGS. 1B and 1E, the distal hub 65 can include a first barb inlet 69 can be coupled to a

connector 73 through which a cable 45 can extend. The temperature sensor 20 can be connected to the cable with one or both components extending partially through the first barb inlet 69 and connector 73. The distal hub 65 can also include a second barb inlet 75 which can be connected to the inlet port 32 to provide fluid communication to the gap 52. The proximal hub 60 can include a third barb inlet 63 and a proximal access port 31 that provides access to the central lumen 51. The third barb inlet 63 can be connected to the interior fluid port 46. In a modified embodiment, one or more of the first, second and third barb inlets 69, 75 and/or 63 can be replaced with flanged and/or flared fittings.

As discussed above, a plurality of components may be attached to the inlets of the distal hub 65 and proximal hub 60 to be in fluid communication with the interior of the exterior tubular body 12. As illustrated in FIGS. 1B-1E, a cable 45 can be attached to or extend through the first barb inlet 69 to form an electrical connection with the temperature sensor 20. In some embodiments the cable 45 is secured to the first barb inlet 69 through the use of connector 73 which can include an adhesive lining. In some embodiments, the cable 45 can include a connector 101 to the control system 100. Similarly, the fluid line 91 with fluid inlet port 32 can be attached to the second barb inlet 75 to provide fluid access to the asymmetrical gap 52. As well, in some embodiments, the cooling fluid line 92 with cooling fluid inlet port 46 can be attached to the barb inlet 63 to provide fluid access to the cooling fluid inlet port 46. The fluid inlet port 32 and cooling fluid inlet port 46 can be provided with luer fittings to facilitate connections to other components.

In order to secure the aforementioned components in the proximal region 14 of the catheter 10, the catheter 10 can include a housing structure to secure the fluid line 91 and cooling fluid line 92 to the inlets of the distal hub 65 and proximal hub 60. In some examples, as illustrated in FIG. 1E, the catheter 10 can include a backend hub 33 that has a first and second portion. The two parts of the backend hub 33 can be disposed about the proximal hub 60 and distal hub 65 so as to secure the distal hub 65 and proximal hub 60 in place. In some examples, the 65 and proximal hub 60 is further secured by the nosecone 70. In some embodiments, the nosecone 70 can be further retained by the backend hub 33 which secures the nosecone 70 at the distal end of the distal hub 65.

As noted above, in some embodiments, the arrangement of the exterior tubular body 12 and the interior tubular body 13 can be configured into an asymmetrical arrangement so as to accommodate the temperature sensor 20. As illustrated in FIG. 2, the central lumen 51 and temperature sensor 20 are located within the fluid delivery lumen 30. The cross-section of the exterior tubular body 12, as illustrated in FIG. 2, can be substantially constant along the length of the catheter 10. Thus, in such embodiments, substantially the same cross-section is present in both the proximal region 14 and the distal region 15 of the catheter 10, including the energy delivery section 18. In certain embodiments, the same or asymmetrically shaped cross-section is present along at least 50% of the length of the catheter, in other embodiments, at least 75% of the length of the catheter and in other embodiments at least 90% of the length of the catheter.

In some embodiments, the central lumen 51 has a minimum diameter greater than about 0.030 inches (greater than about 0.076 cm). In other embodiments, the central lumen 51 has a minimum diameter greater than about 0.037 inches (greater than about 0.094 cm), although other dimensions may be used in other applications. As described above, the

central lumen 51 can extend through the length of the exterior tubular body 12. As illustrated in FIG. 1C, the central lumen 51 can have a distal exit port 29 and a proximal access port 31. As noted above, in some embodiments, the proximal access port 31 forms part of the backend hub 33, which is attached to the proximal region 14 of the catheter 10. In some examples, the backend hub 33 can further include cooling fluid inlet port 46 which is hydraulically connected to the central lumen 51. In some embodiments, the backend hub 33 can also include a fluid inlet port 32, which is in hydraulic connection with the asymmetrical gap 52 in the fluid delivery lumen 30, and which can be hydraulically coupled to a source of drug or therapeutic compound via a hub such as a Luer fitting. This embodiment of the disclosure therefore comprises a first fluid injection port (fluid inlet port 32) in fluid communication with the gap 52.

The central lumen 51 can be configured to receive an inner core 34 comprising a plurality of ultrasound radiating members extending along a length of the ultrasound catheter, FIG. 3 illustrates an embodiment of elongate inner core 34, which can be inserted into the central lumen 51. In some embodiments, the elongate inner core 34 can include a proximal region 36 and a distal region 38. A proximal hub 37 can be fitted on the inner core 34 at one end of the proximal region 36. As will, be described below, in, an arrangement, one or more ultrasound radiating members can be positioned within an inner core 34 located within the distal region 38. The ultrasound radiating members 40 can form an ultrasound assembly 42, which will be described in detail below. In one embodiment, when the inner core 34 can be positioned within the central lumen such that the ultrasound assembly 42 is positioned generally within the energy delivery section 18 of the catheter 10. As noted above, in one embodiment, the joints 212, 213, 214, 215, 216 of the flex circuit can be positioned adjacent the ultrasound, assembly 42 and/or within the energy delivery section 18 of the catheter 10 and/or the thermocouple junctions of a the ribbon thermocouple can be positioned adjacent the ultrasound assembly 42 and/or within the energy delivery section 18 of the catheter.

FIGS. 1G-1J illustrate another embodiment of a back end hub 745, which can be used in the embodiments describe herein. As with the other embodiments, the hub 745 can be coupled to the, the exterior tubular body 12, the interior tubular body 13, and a plurality of inlets. In some examples, the ultrasonic catheter 700 can include a plurality of inlets. For example, the ultrasonic catheter 700 can include a first barb inlet 740, a second barb inlet 750, and a proximal access port 755.

In some embodiments, the hub 745 of the ultrasonic catheter 700 can be composed of a plurality of nested components that are sealed together. As illustrated in FIGS. 1G-1H, in some examples, the hub 745 can be composed of a cap 710 and a manifold body 730. A cross-section of each of the portions of the hub 745 is illustrated in greater detail in FIGS. 1I-1J. In some examples, the components of the hub 745 can be composed of a high density poly ethylene ("HDEV"). In some embodiments, the components of the hub 745 can be composed of a polycarbonate.

Turning first to FIG. 1J, illustrated is a cross-section along circle B-B of the cap 710 in FIG. 1H. In some embodiments, the cap 710 is disposed about a distal end of the distal end 736 of the manifold body 730. As shown, in some examples, the cap 710 has internal threads 312 that are disposed about the internal surface of the cap 710. The cap internal threads 712 are configured to engage with the external threads 734

disposed about the external surface of the distal end **736**. As will be discussed in more detail below, in some embodiments, the manifold body **730** and the cap **710** have an interior lumen that secures the exterior tubular body **12** and interior tubular body **13**.

In some embodiments, the cap **710** can include an internal taper **714** that reduces in diameter. As shown in FIG. 1J, the internal taper **714** can accommodate a flared end **722** of the exterior tubular body **12**. FIG. 1K illustrates a side view of an embodiment of the exterior tubular body **12**. As illustrated, the exterior tubular body **12** can include a distal end **726** and a proximal end **728**. In some embodiments, the flared end **722** of the exterior tubular body **12** can be located at the proximal end **728**. In some examples, the distal end **736** of the manifold body **730** can, when secured within the cap **710**, be configured to engage with and secure the flared end **722** of the exterior tubular body **12**. As the distal end **736** of the manifold body **730** is rotated within the cap **710**, the distal end **736** of the manifold body **730** can apply pressure to the flared end **722** to form a seal **724**. As will be discussed in more detail below, the seal **724** can allow fluid to be pumped into the exterior tubular body **12** and prevent fluid, from leaking out of the exterior tubular body **12**.

In some examples, as shown in FIG. 1J, the exterior tubular body **12** can be disposed about the interior tubular body **13**. As discussed above, the interior tubular body **13** can be configured to accommodate the inner core **706**. In some embodiments, as will be discussed in more detail below, the interior tubular body **13** can provide for a coolant to flow through the interior tubular body **13** to maintain the temperature of the inner core **706**. In some embodiments, as will be discussed in more detail below, the exterior surface of the interior tubular body **13** and the interior surface of the exterior tubular body **12** can provide for a drug or therapeutic compound to flow through.

Turning next to FIG. 1I, illustrated is a cross-section along circle A-A of the manifold body **730** of the hub **745**. In some embodiments, the proximal end **738** of the manifold body **730** can be configured to engage with and secure the interior tubular body **13**. In some examples, the proximal end **738** of the manifold body **730** can include internal threads **732** that are disposed along the inner surface of the manifold body **730**. In some embodiments, the proximal end of the interior tubular body **13** can be engaged with a threaded insert **790**. The external threads **792** of the threaded insert **790** can be rotated to engage with the internal threads **732** of the manifold body **730**.

In some embodiments, the manifold body **730** can include an internal taper **733** that reduces in diameter. As shown in FIG. 1I, the internal taper **733** can accommodate a flared end **782** of the interior tubular body **13**. In some examples, the distal end of the threaded insert **790** can, when secured within the manifold body **730**, be configured to engage with and secure the flared end **782** of the interior tubular body **13**. As the threaded insert **790** is secured within the proximal end **738** of the manifold body **730**, the distal end of the threaded insert **790** can apply pressure to the flared end **782** to form a seal **784**. As will be discussed in more detail below, the seal **784** can prevent fluid from leaking out of the interior tubular body **13**.

As noted above, the hub **745** can include a number of openings to allow access to the interior of the exterior tubular body **12** and the interior tubular body **13** as shown in FIGS. 2 and 2A. In some embodiments, the hub **745** can include the first barb inlet **740**. The first barb inlet **740** can be located near the distal end **736** of the manifold body **730**. In some embodiments, the first barb inlet **740** can be fluidly

connected to the opening between the interior surface of the exterior tubular body **12** and the exterior surface of the interior tubular body **13**. This can be, for example, the asymmetric gap **52** of FIG. 2. The first barb inlet **740** can be fluidly connected to a drug inlet tube **760** and allow a drug or a therapeutic compound to flow from the drug inlet tube **760** and into the exterior tubular body **12** such that the drug or therapeutic compound flows between the interior surface of the exterior tubular body **12** and the exterior surface of the interior tubular body **13**.

In some examples, as illustrated in FIGS. 1G-1H, the hub **745** can include the second barb inlet **750**. The second barb inlet **750** can be located near the proximal end **738** of the manifold body **730**. In some embodiments, the second barb inlet **750** can be fluidly connected to the interior of the interior tubular body **13**. This can be, for example, through the central lumen as illustrated in FIG. 2. The second barb inlet **750** can be fluidly connected to a coolant inlet tube **770** and allow a cooling fluid to flow through the interior tubular body **13**. As noted above, in some examples, the cooling fluid can help to maintain the temperature of the inserted inner core.

In some embodiments, as illustrated in FIGS. 1G-1H, the hub **745** can include a proximal access port **755** that can provide access to the interior of the interior tubular body **13**. In some embodiments, the proximal access port **755** can be configured to allow an inner core (for example the inner core **34** of FIG. 2 or the inner core **706** of FIG. 2A) to be inserted into the ultrasonic catheter **700**.

FIGS. 1L-1O illustrate another embodiment of hub **845** which can be used with any of the embodiments described herein. In some embodiments, the ultrasonic catheter **800** can include a hub **845**, an exterior tubular body **12**, an interior tubular body **13**, and, a plurality of inlets. For example, the ultrasonic catheter **800** can include a first barb inlet **822**, a second barb inlet **832**, and a proximal access port **855**.

In some embodiments, the hub **845** of the ultrasonic catheter **800** can be composed of a plurality of nested components that are secured together. In some examples, the various components of the hub **845** can be composed of a polycarbonate. As will be discussed in more detail below, the hub **845** can include an external overmold that provides an easy and secure way of attaching the various components of the hub **845**. As illustrated in FIG. 1L-1M, in some examples, the hub **845** can be composed of a manifold cap **810**, a distal manifold **820**, a proximal manifold **830**, and an overmold **860**. A cross-section of each of the junctions between each of the components of the hub **845** is illustrated in greater detail in FIGS. 1N-1O.

Turning first to FIG. 1O, illustrated is a cross-section along circle C-C of the manifold cap **810** in FIG. 1M. In some embodiments, the manifold cap **810** is disposed about a distal end **824** of the distal manifold **820**. As illustrated, in some examples, the manifold cap **810** is press fit **868** about the distal end **824** of the distal end **824**.

In some embodiments, the manifold cap **810** can include an internal taper **812** that reduces in diameter. As shown in FIGS. 1M and 1O, the internal taper **812** can accommodate a flared end **842** of the exterior tubular body **12**. In some examples, when the distal end **824** of the distal manifold **820** is secured within the manifold cap **810**, the distal manifold **820** can be configured to engage with and secure the flared end **842** of the exterior tubular body **12**. In some embodiments, as the distal, end **824** of the distal manifold **820** is inserted within the manifold cap **810**, the distal end **824** of the distal manifold **820** can apply pressure to the flared end

842 to form a seal **862**. As will be discussed in more detail below, the seal **862** can allow fluid to be pumped into the exterior tubular body **12** and prevent fluid from leaking out of the exterior tubular body **12**.

In some examples, as shown in FIGS. **1M** and **1O**, the exterior tubular body **12** can be disposed about the interior tubular body **13**. As discussed above, the interior tubular body **13** can be configured to accommodate an inner core. In some embodiments, as will be discussed in more detail below, the interior tubular body **13** can provide for a coolant to flow through the interior tubular body **13** to maintain the temperature of the inserted inner core. In some embodiments, as will be discussed in more detail below, the exterior surface of the interior tubular body **13** and the interior surface of the exterior tubular body **12** can provide for a drug or therapeutic compound to flow through.

Turning next to FIGS. **1M-1N**, illustrated is a cross-section along circle B-B of the connection between the proximal manifold **830** and the distal manifold **820** of the hub **845**. In some embodiments, the proximal end **828** of the distal manifold **820** can, be disposed about the distal end **834** of the proximal manifold **830**. In some examples, the distal manifold **820** is press fit **866** about the proximal manifold **830**.

In some embodiments, the proximal end **828** of the distal manifold **820** can be configured to engage with and secure the interior tubular body **13**. In some embodiments, the distal manifold **820** can include an internal taper **823** that reduces in diameter. As shown in FIG. **1N**, the internal taper **823** can accommodate a flared end **852** of the interior tubular body **13**. In some examples, the distal end **834** of the proximal manifold **830** can, when secured within the proximal end **828** of the distal manifold **820**, be configured to engage with and secure the flared end **852** of the interior tubular body **13**. In some embodiments, the distal end **834** of the proximal manifold **830** can apply pressure to the flared end **852** to form a seal **862**. As will be discussed in more detail below, the seal **862** can prevent fluid from leaking out of the interior tubular body **13**.

As noted above, the hub **845** can include a number of openings to allow access to the interior of the exterior tubular body **12** and the interior tubular body **13** as shown in FIGS. **2** and **2A**. In some embodiments, the hub **845** can include the first barb inlet **822**. The first barb inlet **822** can be located on the distal manifold **820**. In some embodiments, the first barb inlet **822** can be fluidly connected to the opening between the interior surface of the exterior tubular body **12** and the exterior surface of the interior tubular body **13**. This can be, for example, the asymmetric gap **52** of FIG. **2**. In some embodiments, the drug inlet tube **826** can be disposed about the first barb inlet **822**. The first barb inlet **822** can be fluidly connected to the drug inlet tube **826** and allow a drug or a therapeutic compound to flow from the drug inlet tube **826** and into the exterior tubular body **12** such that the drug or therapeutic compound flows between the interior surface of the exterior tubular body **12** and the exterior surface of the interior tubular body **13**.

In some examples, as illustrated in FIG. **1M**, the hub **845** can include the second barb inlet **832**. The second barb inlet **832** can be located on the proximal manifold **830**. In some embodiments, the proximal manifold **830** can be fluidly connected to the interior of the interior tubular body **13**. This can be, for example, through the central lumen as illustrated in FIG. **2**. In some embodiments, the coolant inlet tube **836** can be disposed about the second barb inlet **832**. The second barb inlet **832** can be fluidly connected to the coolant inlet tube **836** and allow a cooling fluid to flow through the

interior tubular body **13**. As noted above, in some examples, the cooling fluid can help to maintain the temperature of the inserted inner core.

In some embodiments, as illustrated in FIG. **1M**, the hub **845** can include a proximal access port **855** that can provide access to the interior tubular body **13**. In some examples, the proximal access port **855** can be configured to allow an inner core (for example the inner core **34** of FIG. **2** or the inner core **706** of FIG. **2A**) to be inserted into the ultrasonic catheter **800**.

As discussed above, in some embodiments, the hub **845** can include an overmold **860**. In some examples, the overmold **860** can be composed of a co-polyester. In some embodiments, the overmold **860** can be composed of a polyamide. The overmold **860** can be configured to seal and secure the various components of the hub **845**.

Details and various embodiments of the inner core **34** and its operation of can be found in several patents and patent applications filed by EKOS Corporation of Bothell Wash. including U.S. Pat. No. 7,220,239 and U.S. Patent Publication No. 2008/0171965, which are hereby incorporated by reference in their entirety.

As shown in the cross-section illustrated in FIG. **4**, which is taken along lines **4-4** in FIG. **3**, the inner core **34** can have a cylindrical shape, with an outer diameter that permits the inner core **34** to be inserted into the central lumen **51** of the interior tubular body **13** via the proximal access port **31**. Suitable outer diameters of the inner core **34** include, but are not limited to, about 0.010 inches to about 0.100 inches (about 0.025 cm to about 0.254 cm). In other embodiments, the outer diameter of the inner core **34** can be between about 0.020 inches and about 0.080 inches (about 0.051 cm to about 0.20 cm). In other embodiments, the inner core **34** can have an outer diameter of about 0.035 inches (about 0.089 cm).

Still referring to FIG. **4**, the inner core **34** can include a cylindrical outer body **35** that houses the ultrasound assembly **42**. The ultrasound assembly **42** can include wiring and ultrasound radiating members, described in greater detail in FIGS. **5** through **7D**, such that the ultrasound assembly **42** is capable of radiating ultrasonic energy from the energy delivery section **41** of the inner core **34**. The ultrasound assembly **42** can be electrically connected to the backend hub **33**, where the inner core **34** can be connected to a control system **100** via cable and through a connector (not shown). In one arrangement, an electrically insulating potting material **43** fills the inner core **34**, surrounding the ultrasound assembly **42**, thus preventing or limiting movement of the ultrasound assembly **42** with respect to the outer body **35**. In one embodiment, the thickness of the outer body **35** is between about 0.0002 inches and about 0.010 inches (between about 0.0005 cm and about 0.025 cm). In another embodiment, the thickness of the outer body **35** is between about 0.0002 inches and about 0.005 inches (between about 0.0005 cm and about 0.01 cm). In yet another embodiment, the thickness of the outer body **35** is about 0.0005 inches (about 0.001 cm).

In some embodiments, the ultrasound assembly **42** comprises a plurality of ultrasound radiating members **40** that are divided into one or more groups. For example, FIGS. **5** and **6** are schematic wiring diagrams illustrating one technique for connecting five groups of ultrasound radiating members **40** to form the ultrasound assembly **42**. As illustrated in FIG. **5**, the ultrasound assembly **42** can include five groups G1, G2, G3, G4, and G5 of ultrasound radiating members **40** that can be electrically connected to each other. The five groups are also electrically connected to the control system **100**. In

some embodiments, two, three, or four groups of ultrasound radiating member **40** may be electrically connected to each other and the control system **100**.

In some embodiments, the ultrasound assembly **42** comprises five or less (i.e., one, two, three, four, or five) ultrasound radiating members **40**. The ultrasound radiating members **40** may be divided into one or more groups as described above. The reduced or limited number of ultrasound, radiating members **40** can allow the ultrasound assembly **42** to be driven at a higher power.

As used herein, the terms “ultrasonic energy”, “ultrasound” and “ultrasonic” are broad terms, having their ordinary meanings, and further refer to, without limitation, mechanical energy transferred through longitudinal pressure or compression waves. Ultrasonic energy can be emitted as continuous or pulsed waves, depending on the requirements of a particular application. Additionally, ultrasonic energy can be emitted in waveforms having various shapes, such as sinusoidal waves, triangle waves, square waves, or other wave forms. Ultrasonic energy includes sound waves. In certain embodiments, the ultrasonic energy has a frequency between about 20 kHz and about 20 MHz. For example, in one embodiment, the waves have a frequency between about 500 kHz and about 20 MHz. In another embodiment, the waves have a frequency between about 1 MHz and about 3 MHz. In yet another embodiment, the waves have a frequency of about 2 MHz. The average acoustic power is between about 0.01 watts and 300 watts. In one embodiment, the average acoustic power is about 16 watts.

As used herein, the term “ultrasound radiating member” refers to any apparatus capable of producing ultrasonic energy. For example, in one embodiment, an ultrasound radiating member comprises an ultrasonic transducer, which converts electrical energy into ultrasonic energy. A suitable example of an ultrasonic transducer for generating ultrasonic energy from electrical energy includes, but is not limited to, piezoelectric ceramic oscillators. Piezoelectric ceramics typically comprise a crystalline material, such as quartz, that changes shape when an electrical current is applied to the material. This change in shape, made oscillatory by an oscillating driving signal, creates ultrasonic sound waves. In other embodiments, ultrasonic energy can be generated by an ultrasonic transducer that is remote from the ultrasound radiating member, and the ultrasonic energy can be transmitted, via, for example, vibration through a wire that is coupled to the ultrasound radiating member.

Still referring to FIG. **5**, the control circuitry **100** can include, among other things, a voltage source **102**. The voltage source **102** can comprise a positive terminal **104** and a negative terminal **106**. The negative terminal **106** is connected to common wire **108**, which connects the five groups G1-G5 of ultrasound radiating members **40** in series. The positive terminal **104** can be connected to a plurality of lead wires **110**, which each connect to one of the five groups G1-G5 of ultrasound radiating members **40**. Thus, under this configuration, each of the five groups G1-G5, one of which is illustrated in FIG. **6**, can be connected to the positive terminal **104** via one of the lead wires **110**, and to the negative terminal **106** via the common wire **108**. The control circuitry can be configured as part of the control system **100** and can include circuits, control routines, controllers etc. configured to vary one or more power parameters used to drive ultrasound radiating members **40**.

Referring now to FIG. **6**, in one embodiment, each group G1-G5 can comprise a plurality of ultrasound radiating members **40**. Each of the ultrasound radiating members **40** can be electrically connected to the common wire **108** and

to the lead wire **110** via one of two positive contact wires **112**. Thus, when wired as illustrated, a constant voltage difference will be applied to each ultrasound radiating member **40** in the group. Although the group illustrated in FIG. **6** comprises twelve ultrasound radiating members **40**, one of ordinary skill in the art will recognize that more or fewer ultrasound radiating members **40** can be included in the group. Likewise, more or fewer than five groups can be included within the ultrasound assembly **42** illustrated in FIG. **5**.

FIG. **7A** illustrates one technique for arranging the components of the ultrasound assembly **42** (as schematically illustrated in FIG. **5**) into the inner core **34** (as schematically illustrated in FIG. **4**). FIG. **7A** illustrates a cross-sectional view of the ultrasound assembly **42** taken within group G1 in FIG. **5**, as indicated by the presence of four lead wires **110**. For example, if a cross-sectional view of the ultrasound assembly **42** was taken within group G4 in FIG. **5**, only one lead wire **110** would be present (that is, the one lead wire connecting group G5).

Referring still to FIG. **7A**, the common wire **108** can include an elongate, flat piece of electrically conductive material in electrical contact with a pair of ultrasound radiating members **40**. Each of the ultrasound radiating members **40** can also be in electrical contact with a positive contact wire **312**. Because the common wire **108** is connected to the negative terminal **106**, and the positive contact wire **312** is connected to the positive terminal **104**, a voltage difference can be created across each ultrasound radiating member **40**. In some embodiments, the lead wires **110** can be separated from the other components of the ultrasound assembly **42**, thus preventing interference with the operation of the ultrasound radiating members **40** as described above. For example, in some embodiments, the inner core **34** is filled with an insulating potting material **43**, thus deterring unwanted electrical contact between the various components of the ultrasound assembly **42**.

FIGS. **7B** and **7C** illustrate cross-sectional views of the inner core **34** of FIG. **7A** taken along lines 7B-7B and 7C-7C, respectively. As illustrated in FIG. **7B**, the ultrasound radiating members **40** are mounted in pairs along the common wire **108**. The ultrasound radiating members **40** are connected by positive contact wires **112**, such that substantially the same voltage is applied to each ultrasound radiating member **40**. As illustrated in FIG. **7C**, the common wire **108** can include wide regions **108W** upon which the ultrasound radiating members **40** can be mounted, thus reducing the likelihood that the paired ultrasound radiating members **40** will short together. In certain embodiments, outside the wide regions **108W**, the common wire **108** may have a more conventional, rounded wire shape.

In a modified embodiment, such as illustrated in FIG. **7D**, the common wire **108** can be twisted to form a helical shape before being fixed within the inner core **34**. In such embodiments, the ultrasound radiating members **40** are oriented in a plurality of radial directions, thus enhancing the radial uniformity of the resulting ultrasonic energy field.

One of ordinary skill in the art will recognize that the wiring arrangement described above can be modified to allow each group G1, G2, G3, G4, G5 to be independently powered. Specifically, by providing a separate power source within the control system **100** for each group, each group can be individually turned on or off, or can be driven with an, individualized power. This provides the advantage of allowing the delivery of ultrasonic energy to be “turned off”

in regions of the treatment site where treatment is complete, thus preventing deleterious or unnecessary ultrasonic energy to be applied to the patient.

The embodiments described above, and illustrated in FIGS. 5 through 7, illustrate a plurality of ultrasound radiating members grouped spatially. That is, in such embodiments, all of the ultrasound radiating members within a certain group are positioned adjacent to each other, such that when a single group is activated, ultrasonic energy is delivered at a specific length of the ultrasound assembly. However, in modified embodiments, the ultrasound radiating members of a certain group may be spaced apart from each other, such that the ultrasound radiating members within a certain group are not positioned adjacent to each other. In such embodiments, when a single group is activated, ultrasonic energy can be delivered from a larger, spaced apart portion of the energy delivery section. Such modified embodiments may be advantageous in applications wherein it is desired to deliver a less focused, more diffuse ultrasonic energy field to the treatment site.

In some embodiments, the ultrasound radiating members 40 comprise rectangular lead zirconate titanate ("PZT") ultrasound transducers. In some embodiments, the ultrasound transducer may have dimensions of about 0.017 inches by about 0.010 inches by about 0.080 inches (about 0.043 cm by about 0.025 cm by about 0.20 cm). In other embodiments, other configuration may be used. For example, disc-shaped ultrasound radiating members 40 can be used in other embodiments. In an embodiment, the common wire 108 comprises copper, and is about 0.005 inches (about 0.01 cm) thick, although other electrically conductive materials and other dimensions can be used in other embodiments. Lead wires 110 can comprise 36 gauge electrical conductors, while positive contact wires 112 can be 42 gauge electrical conductors. However, one of ordinary skill in the art will recognize that other wire gauges can be used in other embodiments.

As described above, suitable frequencies for the ultrasound radiating member 40 include, but are not limited to, from about 20 kHz to about 20 MHz. In one embodiment, the frequency is between about 500 kHz and 20 MHz, and in another embodiment 1 MHz and 3 MHz. In yet another embodiment, the ultrasound radiating members 40 are operated with, a frequency of about 2 MHz.

FIG. 8 illustrates the inner core 34 positioned within the exterior tubular body 12 along a cross-sectional line similar to 2-2 in FIG. 1C. Details of the ultrasound assembly 42, provided in FIG. 7A, are omitted for clarity. As described above, the inner core 34 can be slid within the central lumen 51 of the interior tubular body 13, thereby allowing the inner core 34 to be positioned within the energy delivery section 18. For example, in an embodiment, the materials comprising the inner core energy delivery section 41, the tubular body energy delivery section 18, and the potting material 43 all comprise materials having similar acoustic impedance, thereby minimizing ultrasonic energy losses across material interfaces.

FIG. 8 further illustrates placement of fluid delivery ports 58 within the tubular body energy delivery section 18. As illustrated, holes or slits can be formed from the fluid delivery lumen 30 through the exterior tubular body 12, thereby permitting fluid flow from the asymmetrical gap 52 to the treatment site. Thus, a source of therapeutic compound coupled to the inlet port 32 can provide a hydraulic pressure which drives the therapeutic compound through the asymmetric gap 52 in the fluid delivery lumen 30 and out the fluid

delivery ports 58. Thus, inlet port 32 is a first fluid injection port in, fluid communication with the asymmetric gap 52.

In some embodiments, as illustrated in FIG. 8, the fluid delivery lumen 30 is not evenly spaced around the circumference of the exterior tubular body 12. As discussed, in some embodiments, the exterior tubular body 12 further accommodates the temperature sensor 20. As noted above, the temperature sensor can be a flexicircuit such as the flexicircuit 220 described above with respect to FIGS. 2A and 2B or flexicircuit 320 described with respect to FIGS. 12A and 12B. In some embodiments, the temperature sensor 20 can contact the interior tubular body 13 to bias the interior tubular body 13 against the interior surface of the exterior tubular body 12 and/or to one side of the fluid delivery lumen 30.

In some examples, the configuration of the interior tubular body 13 and temperature sensor 20 can provide a manufacturing benefit as it allows for the construction of the catheter 10 by simply inserting the interior tubular body 13 and temperature sensor 20 into the exterior tubular body 12. This can allow the gap 52 to form between the exterior surface of the interior tubular body 13 and the interior surface of the exterior tubular body 12. In some embodiments, the size, location, and geometry of the fluid delivery ports 58 can be selected to provide uniform fluid flow from the fluid delivery ports 58 to the treatment site. For example, in one embodiment, the fluid delivery ports 58 closer to the proximal region of the energy delivery section 18 have smaller diameters than fluid delivery ports 58 closer to the distal region of the energy delivery section 18, thereby allowing uniform delivery of fluid across the entire energy delivery section 18. The configuration of the interior tubular body 13 can also provide better kink resistance and can potentially reduce the ultrasound attenuation. In some embodiments where the fluid delivery ports 58 have similar sizes along the length of the exterior tubular body 12, the fluid delivery ports 58 have a diameter between about 0.0005 inches to about 0.0050 inches (between about 0.001 cm to about 0.013 cm). In another embodiment in which the size of the fluid delivery ports 58 changes along the length of the exterior tubular body 12, the fluid delivery ports 58 have a diameter between about 0.001 inches to about 0.005 inches (between about 0.002 to about 0.01 cm) in the proximal region of the energy delivery section 18, and between about 0.0020 inches to about 0.005 inches (between about 0.005 cm to 0.01 about cm) in the distal region of the energy delivery section 18. The increase in size between, fluid delivery ports 58 depends on the material composition of the exterior tubular body 12, and on the gap 52. In some embodiments, the fluid delivery ports 58 can be created in the exterior tubular body 12 by punching, drilling, burning, or ablating (e.g. with a laser), or by any other suitable methods. The drug or therapeutic compound flowing along the length of the exterior tubular body 12 can be increased by increasing the density of the number of fluid delivery ports 58 toward the distal region 15 of the exterior tubular body 12.

It should be appreciated that it may be desirable to provide non-uniform fluid flow from the fluid delivery ports 58 to the treatment site. In such embodiment, the size, location and geometry of the fluid delivery ports 58 can be selected to provide such non-uniform fluid flow.

Referring still to FIG. 8, placement of the inner core 34 within the exterior tubular body 12 further defines cooling fluid lumen 44. The cooling fluid lumen 44 can be formed between outer surface 39 of the inner core 34 and the inner surface of the interior tubular body 13. In some embodiments, a cooling fluid can be introduced through the proxi-

mal access port **31** such that the cooling fluid flow is produced through cooling fluid lumen **44** and out the distal exit port **29** (see FIG. 1C). Thus, in some embodiments, the proximal access port **31** is a fluid injection port in fluid communication with an interior of the interior tubular body **13**. In the illustrated arrangement, a cooling fluid can be introduced through the port **46** such that the cooling fluid flow is produced through cooling fluid lumen **44** and out the distal exit port **29**. The cooling fluid lumen **44** can be evenly spaced around the inner core **34** so as to provide uniform cooling fluid flow over the inner core **34**. Such a configuration can be desirable to remove unwanted thermal energy at the treatment site. As will be explained below, the flow rate of the cooling fluid and the power to the ultrasound assembly **42** can be adjusted to maintain the temperature of the inner core **34** in the energy delivery section **41** within a desired range.

In some embodiments, the inner core **34** can be rotated or moved within the interior tubular body **13**. Specifically, movement of the inner core **34** can be accomplished by maneuvering the proximal hub **37** while holding the backend hub **33** stationary. The inner core outer body **35** is at least partially constructed from a material that provides enough structural support to permit movement of the inner core **34** within the interior tubular body **13** without kinking of the interior tubular body **13** without kinking of the interior tubular body **13**. Additionally, the inner core outer body **35** can include a material having the ability to transmit torque. Suitable materials for the outer body **35** can include, but are not limited to, polyimides, polyesters, polyurethanes, thermoplastic elastomers and braided polyimides.

In one embodiment, the fluid delivery lumen **30** and the cooling fluid lumen **44** are open at the distal end of the exterior tubular body **12**, thereby allowing the drug or therapeutic compound and the cooling fluid to pass into the patients' vasculature at the distal exit port. Or, if desired, the fluid delivery lumen **30** can be selectively occluded at the distal end of the exterior tubular body **12**, thereby providing additional hydraulic pressure to drive the therapeutic compound out of the fluid delivery ports **58**. In either configuration, the inner core **34** can be prevented from passing through the distal exit port by providing the inner core **34** with a length that is less than the length of the tubular body. In other embodiments, a protrusion is formed on the internal side of the tubular body in the distal region **15**, thereby preventing the inner core **34** from passing through the distal exit port.

In still other embodiments, the catheter **10** further includes an occlusion device (not shown) positioned at the distal exit port **29**. The occlusion device can have a reduced inner diameter that can accommodate a guidewire, but that is less than the inner diameter of the central lumen **51**. Thus the inner core **34** is prevented from extending through the occlusion device and out the distal exit port **29**. For example, suitable inner diameters for the occlusion device include, but are not limited to, about 0.005 inches to about 0.050 inches (about 0.01 cm to about 0.13 cm). In other embodiments, the occlusion device has a closed end, thus preventing cooling fluid, from leaving the catheter **10**, and instead recirculating to the proximal region **14** of the exterior tubular body **12**. These and other cooling fluid flow configurations permit the power provided to the ultrasound assembly **42** to be increased in proportion to the cooling fluid flow rate. Additionally, certain cooling fluid flow configurations can reduce exposure of the patient's body to cooling fluids.

In certain embodiments, as illustrated in FIG. 8, the exterior tubular body **12** can include a temperature sensor **20**, which can be located adjacent the interior tubular body

13. In such embodiments, the proximal region **14** of the exterior tubular body **12** includes a temperature sensor lead which can be incorporated into cable **45** (illustrated in FIG. 1B). As discussed above, in some embodiments the temperature sensor **20** can have a minimal profile such that it can be placed within the exterior tubular body **12** adjacent the interior tubular body **13**. In some embodiments, to have a minimal profile, the temperature sensor **20** can be made of a flexible circuit as described above. For example, the temperature sensor **20** can be the flexcircuit **220** of FIGS. 2A and 2B or the flexcircuit **320** of FIGS. 12A and 12B. In other embodiments, temperature sensor **20** can include, but is not limited to, temperature sensing diodes, thermistors, thermocouples, resistance temperature detectors ("RTDs") and fiber optic temperature sensors which use thermalchromic liquid crystals. In some embodiments, suitable temperature sensor **20** geometries can include a strip that lies along the length of the exterior tubular body **12**. In other embodiments, suitable temperature sensor **20** geometries can include, but are not limited to, a point, a patch or a stripe. In some embodiments, to provide for easy of assembly, the temperature sensor(s) **20** can be positioned within the exterior tubular body **12** (as illustrated), and/or within one or more of the cooling fluid lumen **44**.

FIG. 9 illustrates one embodiment for electrically connecting a plurality of temperature sensor **20**. In such embodiments, each temperature sensor **20** is coupled to a common wire **61** (e.g., a Constantan trace) and is associated with an individual return wire **62**. Accordingly, n+1 wires can be used to independently sense the temperature at n distinct temperature sensor **20**. The temperature at a particular temperature sensor **20** can be determined by closing a switch **64** to complete a circuit between that thermocouple's individual return wire **62** and the common wire **61**. In embodiments wherein the temperature sensor **20** comprise thermocouples, the temperature can be calculated from the voltage in the circuit using, for example, a sensing circuit **63**, which can be located within the external control circuitry **100**.

In other embodiments, each temperature sensor **20** is independently wired. In such embodiments, 2n wires run through the exterior tubular body **12** to independently sense the temperature at n independent temperature sensor **20**.

FIG. 10 illustrates one embodiment of a feedback control system **68** that can be used with the catheter **10**. The feedback control system **68** can be integrated into a control system that is connected to the inner core **34** via cable and/or the temperature sensor **20** via connector **100** (as illustrated in FIG. 1B). The feedback control system **68** allows the temperature at each temperature sensor **20** to be monitored and allows the output power of the energy source to be adjusted accordingly. A physician can, if desired, override the closed or open loop system.

The feedback control system **68** can include an energy source **70**, power circuits **72** and a power calculation device **74** that is coupled to the ultrasound radiating members **40**. A temperature measurement device **76** can be coupled to the temperature sensor **20** in the exterior tubular body **12**. A processing unit **78** can be coupled to the power calculation device **74**, the power circuits **72** and a user interface and display **80**.

In operation, the temperature at each temperature sensor **20** can be determined by the temperature measurement device **76**. The processing unit **78** receives each determined temperature from the temperature measurement device **76**. The determined temperature can then be displayed to the user at the user interface and display **80**.

The processing unit 78 comprises logic for generating a temperature control signal. The temperature control signal can be proportional to the difference between the measured temperature and a desired temperature. The desired temperature can be determined by the user (at set at the user interface and display 80) or can be preset within the processing unit 78.

The temperature control signal can be received by the power circuits 72. In some embodiments, the power circuits 72 can be configured to adjust the power level, voltage, phase and/or current of the electrical energy supplied to the ultrasound radiating members 40 from the energy source 70. For example, when the temperature control signal is above a particular level, the power supplied to a particular group of ultrasound radiating members 40 can be reduced in response to that temperature control signal. Similarly, when the temperature control signal is below a particular level, the power supplied to a particular group of ultrasound radiating members 40 can be increased in response to that temperature control signal. After each power adjustment, the processing unit 78 can be configured to monitor the temperature sensor 20 and produces another temperature control signal which is received by the power circuits 72.

The processing unit 78 can further include safety control logic. The safety control logic detects when the temperature at a temperature sensor 20 has exceeded a safety threshold. The processing unit 78 can then provide a temperature control signal which causes the power circuits 72 to stop the delivery of energy from the energy source 70 to that particular group of ultrasound radiating members 40.

Because, in certain embodiments, the ultrasound radiating members 40 are mobile relative to the temperature sensor 20, it can be unclear which group of ultrasound radiating members 40 should have a power, voltage, phase and/or current level adjustment. Consequently, each group of ultrasound radiating member 40 can be identically adjusted in certain embodiments. In a modified embodiment, the power, voltage, phase, and/or current supplied to each group of ultrasound radiating members 40 is adjusted in response to the temperature sensor 20 which indicates the highest temperature. Making voltage, phase and/or current adjustments in response to the temperature sensed by the temperature sensor 20 indicating the highest temperature can reduce overheating of the treatment site.

The processing unit 78 can also receive a power signal from a power calculation device 74. The power signal can be used to determine the power being received by each group of ultrasound radiating members 40. The determined power can then be displayed to the user on the user interface and display 80.

As described above, the feedback control system 68 can be configured to maintain tissue adjacent to the energy delivery section 18 below a desired temperature. For example, it can, be generally desirable to prevent tissue at a treatment site from increasing more than 6° C. As described above, the ultrasound radiating members 40 can be electrically connected such that each group of ultrasound radiating members 40 generates an independent output. In certain embodiments, the output from the power circuit maintains a selected energy for each group of ultrasound radiating members 40 for a selected length of time.

The processing unit 78 can comprise a digital or analog controller, such as a computer with, software. When the processing unit 78 is a computer it can include a central processing unit ("CPU") coupled through a system bus. As is well known in the art, the user interface and display 80 can comprise a mouse, a keyboard, a disk drive, a display

monitor, a nonvolatile memory system, or any another. In some embodiments, the bus can be coupled to a program memory and a data memory.

In lieu of the series of power adjustments described above, a profile of the power to be delivered to each group of ultrasound radiating members 40 can be incorporated into the processing unit 78, such that a preset amount of ultrasonic energy to be delivered is pre-profiled. In such embodiments, the power delivered to each, group of ultrasound radiating members 40 can then be adjusted according to the preset profiles.

The ultrasound radiating members can be operated in a pulsed mode. For example, in one embodiment, the time average electrical power supplied to the ultrasound radiating members can be between about 0.1 watts and 2 watts and can be between about 0.5 watts and 1.5 watts. In other embodiments, the time average electrical power supplied to the ultrasound radiating members is between, about 0.001 watts and about 5 watts and can be between about 0.05 watts and about 3 watts. In some embodiments, the time average electrical power can be approximately 0.6 watts or 1.2 watts to a pair of ultrasound radiating members. In other embodiments, the time average electrical power over treatment time can be approximately 0.45 watts or 1.2 watts to a pair of ultrasound radiating members.

The duty cycle can be between about 1% and 50%. In some embodiments, the duty cycle can be between about 5% and 25%. In certain embodiments, the duty ratio can be approximately 7.5% or 15%. In other embodiments, the duty cycle can be between about 0.01% and about 90% and can be between about 0.1% and about 50%. In certain embodiments, the duty ratio can be approximately 7.5%, 15% or a variation between 1% and 30%. In some embodiments, the pulse averaged power to a pair of ultrasound radiating members can be between about 0.1 watts and 20 watts and can further be between approximately 5 watts and 20 watts. In certain embodiments, the pulse averaged power to a pair of ultrasound radiating members can be approximately 8 watts and 16 watts. In some embodiments, the pulse averaged electrical power to a pair of ultrasound radiating members can be between about 0.01 watts and about 20 watts and can be between approximately 0.1 watts and 20 watts. In other embodiments, the pulse averaged electrical power to a pair of ultrasound radiating members is approximately 4 watts, 8 watts, 16 watts, or a variation of 1 to 8 watts. The amplitude during each pulse can be constant or varied.

As described above, the amplitude, pulse width, pulse repetition frequency, average acoustic pressure or any combination of these parameters can be constant or varied during each pulse or over a set of portions. In a non-linear application of acoustic parameters the above ranges can change significantly. Accordingly, the overall time average electrical power over treatment time may stay the same but not real-time average power.

In some embodiments, the pulse repetition rate can be between about 5 Hz and 150 Hz and can further be between about 10 Hz and 50 Hz. In some embodiments, the pulse repetition rate is approximately 30 Hz. In other embodiments, the pulse repetition can be between about 1 Hz and about 2 kHz and more can be between about 1 Hz and about 50 Hz. In certain embodiments, the pulse repetition rate can be approximately 30 Hz, or a variation of about 10 to about 40 Hz. The pulse duration can be between about 1 millisecond and 50 milliseconds and can be between about 1 millisecond and 25 milliseconds. In certain embodiments, the pulse duration can be approximately 2.5 milliseconds or

5 milliseconds. In other embodiments, the pulse duration or width can be between about 0.5 millisecond and about 50 milliseconds and can be between about 0.1 millisecond and about 25 milliseconds. In certain embodiments, the pulse duration can be approximately 2.5 milliseconds, 5 or a variation of 1 to 8 milliseconds. In certain embodiments, the average acoustic pressure can be between about 0.1 to about 20 MPa or in another embodiment between about 0.5 or about 0.74 to about 1.7 MPa. In one particular embodiment, the transducers can be operated at an average power of approximately 0.6 watts, a duty cycle of approximately 7.5%, a pulse repetition rate of 30 Hz, a pulse average electrical power of approximately 8 watts and a pulse duration of approximately 2.5 milliseconds. In one particular embodiment, the transducers can be operated at an average power of approximately 0.45 watts, a duty cycle of approximately 7.5%, a pulse repetition rate of 30 Hz, a pulse average electrical power of approximately 6 watts and a pulse duration of approximately 2.5 milliseconds. The ultrasound radiating member used with the electrical parameters described herein can have an acoustic efficiency greater than 50%. In some embodiments, the acoustic efficiency can be greater than 75%. The ultrasound radiating member can be formed a variety of shapes, such as, cylindrical (solid or hollow), flat, bar, triangular, and the like. The length of the ultrasound radiating member can be between about 0.1 cm and about 0.5 cm. The thickness or diameter of the ultrasound radiating members can be between about 0.02 cm and about 0.2 cm.

FIGS. 11A through 11D illustrate a method for using the ultrasonic catheter 10. As illustrated in FIG. 11A, a guidewire 84 similar to a guidewire used in typical angioplasty procedures can be directed through a patient's vessels 86 to a treatment site 88 which includes a clot 90. The guidewire 84 can be directed through the clot 90. Suitable vessels 86 can include, but are not limited to, the large periphery blood vessels of the body. Additionally, as mentioned above, the ultrasonic catheter 10 also has utility in various imaging applications or in applications for treating and/or diagnosing other diseases in other body parts.

As illustrated in FIG. 11B, the catheter 10 can be slid over and advanced along the guidewire 84 using conventional over-the-guidewire techniques with the guidewire extending through the interior tubular body 13. The catheter 10 can be advanced until the energy delivery section 18 of the exterior tubular body 12 is positioned at the clot 90. In certain embodiments, radiopaque markers (not shown) are positioned along the energy delivery section 18 of the exterior tubular body 12 to aid in the positioning of the exterior tubular body 12 of the catheter 10 within the treatment site 88.

As illustrated in FIG. 11C, the guidewire 84 can then be withdrawn from the catheter 10 by pulling the guidewire 84 from the proximal region 14 of the catheter 10 while holding the catheter stationary. This leaves catheter 10 (exterior body 12 shown in FIG. 11C) positioned at the treatment site 88.

As illustrated in FIG. 11D, the inner core 34 can then be inserted into interior tubular body 13 until the ultrasound assembly 42 is positioned at least partially within the energy delivery section 18 of the exterior tubular body 12. Once the inner core 34 is properly positioned, the ultrasound assembly 42 can be activated to deliver ultrasonic energy through the energy delivery section 18 to the clot 90. As described above, suitable ultrasonic energy is delivered with a frequency between about 20 kHz and about 20 MHz.

In a certain embodiment, the ultrasound assembly 42 comprises sixty ultrasound radiating members 40 spaced

over a length of approximately 30 to 50 cm. In such embodiments, the catheter 10 can be used to treat an elongate clot 90 without requiring movement of or repositioning of the catheter 10 during the treatment. However, in some embodiments, the inner core 34 can be moved or rotated within the catheter 10 during the treatment. Such movement can be accomplished by maneuvering the proximal hub 37 of the inner core 34 while holding the backend hub 33 stationary.

Referring again to FIG. 11D, arrows 48 indicate that a cooling fluid flows through the cooling fluid lumen 44 and out the distal exit port 29. Likewise, arrows 49 indicated that a therapeutic compound flows through gap 52 in the fluid delivery lumen 30 and out the fluid delivery ports 58 to the treatment site 88. In the schematic illustrations of FIGS. 11A and 11D, the fluid delivery ports 58 are shown in a different location than illustrated in FIG. 8.

The cooling fluid can be delivered before, after, during or intermittently with the delivery of ultrasonic energy. Similarly, the therapeutic compound can be delivered before, after, during or intermittently with the delivery of ultrasonic energy. Consequently, the steps illustrated in FIGS. 11A through 11D can be performed in a variety of different orders than that described above. The therapeutic compound and ultrasonic energy can be applied until the clot 90 is partially or entirely dissolved. Once the clot 90 has been dissolved to the desired degree, the exterior tubular body 12 and the inner core 34 are withdrawn from the treatment site 88.

Pulmonary Embolism Treatment

In some embodiments, the ultrasonic catheter 10 can be configured to be introduced into the major blood vessels leading from the heart to the lungs (e.g., the pulmonary artery). In one embodiment of use, femoral venous access may be used to place the ultrasonic catheter 10 into such vessels. In such embodiments, the ultrasonic catheter 10 can be advanced through femoral access site, through the heart and into the pulmonary artery. The dimensions of the ultrasonic catheter 10 are adjusted based on the particular application for which the ultrasonic catheter 10 is to be used.

As noted above, the ultrasound catheter 10 can, also be used for treating PE. The ultrasound catheter 10 can be introduced into a patient's pulmonary artery over a guidewire. The distal region 15 of the ultrasound catheter 10 is then advanced to the treatment site within the pulmonary artery. The ultrasound energy delivery section 18 of the ultrasound catheter can be positioned across the treatment site using fluoroscopic guidance via radiopaque marker located near the proximal end and the distal end of the ultrasound energy delivery section 18. Once the ultrasound catheter 10 is successfully placed, the guidewire may be removed from the ultrasound catheter 10. In the embodiments depicted in FIGS. 1-11, the elongate inner core 34 comprising at least one ultrasound radiating member 40 can then be inserted into the central lumen 51 of the ultrasound catheter 10. The at least one ultrasound radiating member 40 can be positioned along the energy delivery section 18 of the ultrasound catheter 10. In some embodiments, at least one cooling lumen 44 is formed between an outer surface 39 of the inner core 34 and an inner surface of the interior tubular body 13. The coolant infusion pump is attached to the cooling fluid inlet port 46, which is in communication with the at least one cooling fluid lumen 44. The drug infusion pump can then be connected to the fluid inlet port 32, which is in communication with the asymmetric gap 52 in the at least one fluid delivery lumen 30.

The thrombolytic drug can then be delivered to the treatment site through at least one fluid delivery lumen 30.

In some embodiments, a plurality of fluid delivery ports **58** is in fluid communication with the fluid delivery lumen **30** can be located on, the ultrasound catheter at the ultrasound energy delivery section **18**. The drug can be infused through the fluid delivery ports **58** to the treatment site.

The ultrasound energy may be delivered to the treatment site simultaneously or intermittently with the infusion of the thrombolytic drug. In some embodiments, the ultrasound energy is emitted to the treatment site prior to the thrombolytic drug being delivered. In some embodiments, the thrombolytic drug is delivered to the treatment site prior to the ultrasound energy being emitted. The ultrasound energy may be emitted according to the manner described above. In some embodiment, the power parameter and the physiological parameter of at least one ultrasound radiating member **40** may be varied as described above.

In some embodiments, the elongate, inner core **34** may comprise five or less (i.e., one, two, three, four, or five) ultrasound radiating members **40**. In some variants, by limiting the number of the ultrasound radiating members **40**, it is possible to drive the ultrasound radiating members at a higher power for PE treatments.

High intensity ultrasound catheter may also be especially effective in treating pulmonary embolism. In some embodiments, the size of one or more ultrasound radiating members **40** positioned in the elongate inner core **34** can be increased to generate high intensity ultrasound. In other words, larger ultrasound radiating members can be used for this purpose. In some embodiments, positioning the ultrasound radiating members less than 1 cm apart can result in higher intensity ultrasound output.

Without being bound to the theory, the ultrasound can prepare the clot by unwinding the fibrin strands and increasing the permeability of the clot. Acoustic pressure waves and micro-streaming force the delivered drug into the clot, quickly permeating the clot with drug. As the drug is absorbed into the clot it binds with exposed plasminogen receptor sites. Once bound in the clot, the drug is no longer in free circulation, does not pass through the liver and is not metabolized.

In some embodiments, recombinant tissue plasminogen activator (rt-PA or Actilyse®) can be used with the ultrasound catheter **10** for the treatment of pulmonary embolism. The effective infusion dosage may range from about 0.12 mg/hr to about 2 mg/hr, from about 0.2 mg/hr to about 1.5 mg/hr, from about 0.5 mg/hr to about 1.5 mg/hr, or from about 1 mg/hr to about 2 mg/hr. The rt-PA maximum total infusion dose may be from about 10 mg to about 30 mg, from about 10 mg to about 20 mg, or about 25 mg. In some embodiment, as rt-PA is infused at a rate of about 1 mg/hr to about 2 mg/hr for about 3 to about 5 hours, then the infusion rate is decreased to about 0.5 mg/hr for 10 hours. In some embodiments, rt-PA is infused at a rate of about 1 mg/hr to about 2 mg/hr for about 5 hours, and then the infusion rate is decreased to about 0.5 mg/hr for 10 hours.

Other potential drugs that may be used with the ultrasound catheter for treating pulmonary embolism may include fibrinolytic compounds such as urokinase (Abbokinase®, Abbott laboratories, USA), streptokinase (Streptase®, Behringwerke AG), and reteplase (Retavase™, Centocor, Inc.). The enzymatic activity and stability of these fibrinolytics (including rt-PA) are not changed after exposure to therapeutic ultrasound.

In general, digital angiographic equipment is used to aid the performance of the ultrasound catheter treatment procedure. Continuous invasive pressure monitoring and ECG-monitoring can be used for obtaining baseline hemodynamic

parameters, including heart rate, right atrial, right ventricular, and pulmonary artery pressures, as well as the mixed-venous oxygen saturation from the pulmonary artery. A systemic arterial blood pressure and a systemic oxygen saturation can also be measured if an arterial line is in place. Otherwise, the systemic cuff blood pressure is measured and the oxygen saturation is obtained by pulse oximetry. In one embodiment, a blood pressure sensor is integrated into the ultrasound catheter.

In some embodiments, a feedback control loop configured to monitor the baseline hemodynamic parameters and/or mixed-venous oxygen saturation can be integrated into the control system **100**. The output power of the energy source can then be adjusted according to the readings. A physician can override the closed or open loop system if so desired.

In some embodiments, an unilateral filling defect in one main or proximal lower lobe pulmonary artery by contrast-enhanced chest CT indicates that only one ultrasound catheter is to be placed into the pulmonary artery. In case of bilateral filling defect is detected in both main or proximal lower lobe pulmonary arteries by contrast-enhancing chest CT, two ultrasound catheters may be placed.

As noted above, in some embodiments, femoral venous access may be used for placing the ultrasound catheter in the pulmonary arteries. For example, a 6F introducer sheath is inserted in the common femoral vein. An exchange-length 0.035-inch (0.089-cm) angled guidewire, for example the Terumo□ soft wire, may be used for probing the embolic occlusion under fluoroscopy. A 5F standard angiographic catheter, such as a multipurpose catheter or pigtail catheter or any other pulmonary angiographic catheter may be used with small manual contrast injections for localizing the embolic occlusion and for positioning the catheter such that the energy delivery section **18** of the ultrasound catheter spans the thrombus. If the distal extent of the embolus is not visible angiographically or if it is difficult to probe the embolic occlusion, a 4F Terumo glide catheter may be used for obtaining very small selective contrast injections beyond the presumed thrombotic occlusion after transiently removing the 0.035 wire. After the wire is successfully placed beyond the thrombotic occlusion in a lower lobe segmental branch, the angiographic catheter is exchanged for the ultrasound catheter.

Finally, in embodiments wherein the ultrasound catheter including elongate inner core with ultrasound catheter (as shown in FIGS. **1-11**) is used, the 0.035-inch (0.089-cm) guidewire can be removed and the elongate inner core with ultrasound radiating member(s) **40** is inserted into the ultrasound catheter. The therapeutic compound can be introduced through the at least one fluid delivery lumen **30** and out of the fluid delivery port(s) **58** to the treatment site.

After about 12 to about 15 hours of drug infusion, the rt-PA infusion can be replaced with heparinized saline infusion (about 1 µg/ml) at an infusion rate of 5 ml/hr. Sometime between about 16 and about 24 hours after the start of the rt-PA infusion, follow-up hemodynamic measurements (heart rate, systemic arterial pressure, right atrial, right ventricular and pulmonary artery pressures, mixed venous and pulse oximetric oxygen saturations, cardiac output, pulmonary vascular resistance) and controlled removal of the ultrasound catheter can be performed. The decision on the exact duration of the ultrasound-assisted thrombolysis infusion is at the discretion of the physician, but in one embodiment it is recommended to continue the treatment for 15 hours (or until 20 mg of rt-PA has been delivered) if well tolerated by the patient.

In certain embodiments, it can be beneficial to keep the catheter centered in the pulmonary artery during the treatment process. For example, centering the ultrasound radiating member 40 in the pulmonary artery may improve the uniform exposure at the treatment site. In some embodiments, the ultrasound catheter 10 also includes a centering mechanism for keeping the catheter centered during the treatment. In some embodiments, the centering mechanism of the catheter 10 can be provided with one or more balloons disposed around the catheter 10 toward the distal region 15.

As described above, in some embodiments, the ultrasound assembly 42 comprises a plurality of ultrasound radiating members 40 that are divided into one or more groups. For example, FIGS. 5 and 6 are schematic wiring diagrams illustrating one technique for connecting five groups of ultrasound, radiating members 40 to form the ultrasound assembly 42. As illustrated in FIG. 5, the ultrasound assembly 42 comprises five groups G1, G2, G3, G4, and G5 of ultrasound radiating members 40 that are electrically connected to each other. The five groups are also electrically connected to the control system 100. In some embodiments, two, three, or four or more than five groups of ultrasound radiating member 40 may be electrically connected to each other and the control system 100. Each group (G1-G5) may comprise one or more individual ultrasound elements. For example, in one embodiment, each group comprises five or less (i.e., one, two, three, four, or five) ultrasound radiating members 40. In other embodiments, more than 5 ultrasound elements can be provided, in each group. Modified embodiments may also include different numbers of elements within each group.

In the embodiment of FIG. 6, each group G1-G5 comprises a plurality of ultrasound radiating members 40. Each of the ultrasound radiating members 40 is electrically connected to the common wire 108 and to the lead wire 110 via one of two positive contact wires 112. Thus, when wired as illustrated, a constant voltage difference will be applied to each ultrasound radiating member 40 in the group. Although the group illustrated in FIG. 6 comprises twelve ultrasound radiating members 40, one of ordinary skill in the art will recognize that more or fewer ultrasound radiating members 40 can be included in the group. Likewise, more or fewer than five groups can be included within the ultrasound assembly 42 illustrated in FIG. 5.

The wiring arrangement described above can be modified to allow each group G1, G2, G3, G4, G5 to be independently powered. Specifically, by providing a separate power source within the control system 100 for each group, each group can be individually turned on or off, or can be driven with an individualized power. This provides the advantage of allowing the delivery of ultrasonic energy to be "turned off" in regions of the treatment site where treatment is complete, thus preventing deleterious or unnecessary ultrasonic energy to be applied to the patient.

The embodiments described above, and illustrated in FIGS. 5 through 7, illustrate a plurality of ultrasound radiating members grouped spatially. That is, in such embodiments, all of the ultrasound radiating members within a certain group are positioned adjacent to each other, such that when a single group is activated, ultrasonic energy is delivered at a specific length of the ultrasound assembly. However, in modified embodiments, the ultrasound radiating members of a certain group can be interdigitated with respect to ultrasound radiating members of a different group.

Method for Assembling a Catheter with a Temperature Sensor

As discussed above, the configuration of the temperature sensor 20 in the exterior tubular body 12 can provide for ease of assembly and manufacturability. In one aspect, the disclosure resides in a method of manufacturing a catheter comprising a flexible circuit and/or a ribbon thermocouple according to any of the embodiments described herein. In a particular embodiment of the disclosure, the flexible circuit is configured to form a thermocouple. In a particular embodiment of the disclosure, the thermocouple ribbon is configured to form a thermocouple. FIG. 13 illustrates a flow-chart of an example method for assembling a catheter with a flex circuit thermocouple and/or thermocouple ribbon.

The method for assembling a catheter with flex circuit thermocouple and/or thermocouple ribbon can first include block 410 which describes first inserting the interior tubular body 13 into the exterior tubular body 12. In some embodiments, the interior tubular body 13 can be inserted into the exterior tubular body 12 such that the outside surface of the interior tubular body 13 contacts the inside surface of the exterior tubular body 12. This can form an asymmetrical space within the exterior tubular body 12 to accommodate a temperature sensor 20.

Next, the method can include block 420 which describes inserting the flexcircuit temperature sensor 20 or and/or thermocouple ribbon 500, 600 through the first barb inlet 69 of the distal hub 65. As described above, the temperature sensor 20 can be the flexcircuit 220 of FIGS. 2A and 2B or flexcircuit 320 of FIGS. 12A-12B or ribbon thermocouple 500, 600 of FIGS. 2D-2I.

Once inserted, the temperature sensor 20 can be attached to the proximal and distal ends of the interior tubular body 13 as discussed in block 430 and block 440. The attachment of the temperature sensor 20 to the interior tubular body 13 can be done using an adhesive or a heat shrink.

At block 450, the remaining components of the catheter 10 are assembled. For example, in the catheter 10 described above, FIG. 1E illustrates an exploded view of the various components of the catheter 10 and the connections between each of the components.

Once the catheter 10 has been assembled, the method can include block 460 which describes attaching the fluid lines (e.g. fluid line 91 and cooling fluid line 92) to the catheter. As shown above, the fluid line 91 can be attached to the second barb inlet 75 while the cooling fluid line 92 is attached to the barb inlet 63.

To attach the temperature sensor 20 to an electrical source, block 470 describes connecting the temperature sensor 20 to a cable assembly. As illustrated in FIG. 1E, the cable 45 can attach to the temperature sensor 20 through first barb inlet 69. The distal end of the cable 45 can then attach to a control system 100. The various methods and techniques described above provide a number of ways to carry out the disclosure. Of course, it is to be understood that not necessarily all objectives or advantages described may be achieved in accordance with any particular embodiment described herein. Thus, for example, those skilled in the art will recognize that the methods may be performed in a manner that achieves or optimizes one advantage or group of advantages as taught herein without necessarily achieving other objectives or advantages as may be taught or suggested herein.

The disclosure includes the following additional embodiments:

- Embodiment 1. An ultrasound catheter comprising:
 - a first tubular body having a first longitudinal axis extending centrally through the tubular body, the first

tubular body including at least one delivery port extending through a wall of the first tubular body; a second tubular body having a second longitudinal axis extending centrally through the second tubular body, the first and second, longitudinal axes being displaced from each other such that an asymmetrical longitudinally extending gap is formed between an outer surface of the second tubular body and an interior surface of the first tubular body; a flexible circuit forming a thermocouple extending longitudinally within the gap between the first tubular body and the second tubular body; and an inner core positioned within the second tubular body, the inner core comprising at least one ultrasound element.

Embodiment 2: The ultrasound catheter of Embodiment 1, wherein the flexible circuit positioned in the widest portion of the asymmetrical gap.

Embodiment 3: The ultrasound catheter of any one of Embodiments 1-2, wherein the flexible circuit extends along the length of the first tubular body.

Embodiment 4: The ultrasound catheter of any one of Embodiments 1-3, wherein the flexible circuit is adjacent to an outer surface of the second tubular body.

Embodiment 5: The ultrasound catheter of any one of Embodiments 1-4, wherein the ultrasound catheter comprises a first fluid injection port in fluid communication with the gap.

Embodiment 6: The ultrasound, catheter of any one of Embodiments 1-5, wherein the apparatus further comprises a second fluid injection port in fluid communication with an interior of the second tubular body.

Embodiment 7: The ultrasound catheter of any one of Embodiments 1-6, wherein the flexible circuit is configured to measure temperature at different points along the length of ultrasound catheter.

Embodiment 8: The ultrasound catheter of any one of Embodiments 1-7, wherein the inner core comprises a plurality of ultrasound radiating members extending along a length of the ultrasound catheter.

Embodiment 9: The ultrasound catheter of Embodiment 8, wherein the flexible circuit comprises a plurality of joints between traces of dissimilar materials.

Embodiment 10: The ultrasound catheter of Embodiment 9, wherein the plurality of joints between traces of dissimilar materials extend along the length of the ultrasound catheter in which the plurality of ultrasound radiating members is positioned.

Embodiment 11: The ultrasound catheter of Embodiment 10, wherein the joints between traces of dissimilar materials are formed by a plurality traces of a first material connected to a single trace of second dissimilar material.

Embodiment 12: The ultrasound catheter of Embodiment 1, wherein the flexible circuit comprises a plurality of traces formed on the flexible circuit separated by insulating material, the plurality of traces comprising at least two traces of a first material connected to a single trace of second dissimilar material at different points along a length of the flexible circuit.

Embodiment 13: A method of manufacturing a catheter comprising:
 inserting an inner tubular body into an outer tubular body; and
 placing a flexible circuit between the outer and inner tubular body, wherein the temperature sensor is adjacent to an outer surface of the inner tubular body

such that the inner tubular body does not extend along the same longitudinal axis a the outer tubular body.

Embodiment 14: The method of manufacturing of Embodiment 13, wherein the flexible circuit is configured to form a thermocouple.

Embodiment 15: The method of manufacturing of Embodiment 13, further comprising: forming an inner core, wherein the inner core is configured to be insertable into the inner tubular body.

Embodiment 16: The method of manufacturing of Embodiment 13, wherein inserting the elongate fluid delivery body and inserting the temperature sensor forms an asymmetrical cross-section in the catheter.

Embodiment 17: An ultrasound catheter comprising:
 an elongate inner tubular body;
 an, elongate outer tubular;
 wherein the elongate inner tubular body is positioned within the elongate outer tubular body to form an asymmetrical gap between an outer surface of the inner tubular body and an interior surface of the elongate outer tubular body to form a fluid delivery lumen, and
 a temperature sensor extending along the outer surface of the inner tubular body within the gap; and
 an inner core positioned within the inner tubular body and comprising at least one ultrasound element.

Embodiment 18: The ultrasound catheter of Embodiment 17, wherein the temperature sensor is formed by a flexible circuit.

Embodiment 19: An ultrasound catheter of Embodiment 18, wherein the temperature sensor is located in the widest portion of the asymmetrical gap.

Embodiment 20: A flexible circuit for a catheter, the flex, circuit comprising a plurality of traces formed on the flexible circuit separated by insulating material, the plurality of traces comprising at least two traces of a first material connected to a single trace of second dissimilar material at different points along a length of the flexible circuit.

Embodiment 22: The flexible circuit of Embodiment 20, wherein the second dissimilar material is Constantan and the first material is copper.

Furthermore, the skilled artisan will recognize the interchangeability of various features from different embodiments disclosed herein. Similarly, the various features and steps discussed above, as well as other known equivalents for each such feature or step, can be mixed and matched by one of ordinary skill in this art to perform methods in accordance with principles described herein. Additionally, the methods which is described and illustrated herein is not limited to the exact sequence of acts described, nor is it necessarily limited to the practice of all of the acts set forth. Other sequences of events or acts, or less than all of the events, or simultaneous occurrence of the events, may be utilized in practicing the embodiments of the invention.

Although the invention has been disclosed in the context of certain embodiments and examples, it will be understood by those skilled in the art that the invention extends beyond the specifically disclosed embodiments to other alternative embodiments and/or uses and obvious modifications and equivalents thereof. Accordingly, the invention is not intended to be limited by the specific disclosures of embodiments herein.

What is claimed is:

1. An ultrasound catheter comprising:

a first tubular body having a first longitudinal axis extending centrally through the tubular body, the first tubular body including at least one delivery port extending through a wall of the first tubular body;

a second tubular body having a second longitudinal axis extending centrally through the second tubular body, the first and second longitudinal axes being displaced from each other such that an asymmetrical longitudinally extending gap is formed between an outer surface of the second tubular body and an interior surface of the first tubular body;

a temperature sensor forming a thermocouple extending longitudinally within the gap between the first tubular body and the second tubular body; and

an inner core positioned within the second tubular body, the inner core comprising at least one ultrasound element, and the inner core having a third longitudinal axis extending centrally through the inner core, wherein the third longitudinal axis is displaced from the first and second longitudinal axes.

2. The ultrasound catheter of claim **1**, wherein the temperature sensor is positioned in a widest portion of the asymmetrical gap.

3. The ultrasound catheter of claim **1**, wherein the temperature sensor extends along a length of the first tubular body.

4. The ultrasound catheter of claim **1**, wherein the temperature sensor is adjacent to the outer surface of the second tubular body.

5. The ultrasound catheter of claim **1**, wherein the ultrasound catheter comprises a first fluid injection port in fluid communication with the gap.

6. The ultrasound catheter of claim **5**, wherein the ultrasound catheter further comprises a second fluid injection port in fluid communication with an interior of the second tubular body.

7. The ultrasound catheter of claims **1**, wherein the temperature sensor is configured to measure temperature at different points along a length of the ultrasound catheter.

8. The ultrasound catheter of claim **1**, wherein the inner core comprises a plurality of ultrasound radiating members extending along a length of the ultrasound catheter.

9. The ultrasound catheter of claim **8**, wherein the temperature sensor comprises a flexible circuit that comprises a plurality of joints between traces of dissimilar materials.

10. The ultrasound catheter of claim **9**, wherein the plurality of joints between traces of dissimilar materials extend along the length of the ultrasound catheter in which the plurality of ultrasound radiating members is positioned.

11. The ultrasound catheter of claim **10**, wherein the plurality of joints between traces of dissimilar materials are formed by a plurality of traces of a first material connected to a single trace of second dissimilar material.

12. The ultrasound catheter of claim **1**, wherein the temperature sensor comprises a plurality of traces formed on the temperature sensor separated by insulating material, the plurality of traces comprising at least two traces of a first material connected to a single trace of second dissimilar material at different points along a length of the temperature sensor.

13. The ultrasound catheter of claim **1**, wherein the second tubular body is asymmetrical and includes a plurality of indentations along an interior surface of the second tubular body.

14. The ultrasound catheter of claim **1**, wherein the temperature sensor comprises a flexcircuit.

15. The ultrasound catheter of claim **1**, wherein the temperature sensor comprises a plurality of filament pairs wherein each of the plurality of filament pairs is insulated; and at least one additional thermocouple wherein each of at least one additional thermocouple are formed between each of the plurality of filament pairs.

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