## EXTENDED-SCALE INDICATORS

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## [57] <br> ABSTRACT

Novel extended-scale indicators of various types are disclosed, primarily for milling machine lead-screws. The described indicators include a sprocket on the lead-screw shaft, usually two looped or continuous tapes cogged to the sprocket, and a protective enclosure having idlers that guide the tapes in a compact serpentine path. The lengths of the tapes are related so that one tape precesses in relation to the other in successive sprocket rotations, including extendedscale indication in opposite directions of operation, starting at a common zero. One modification provides direct English-to-metric conversion. Another indicator provides turn-by-turn error calibration of the lead screw. Three identical individually adjustable indicators in tandem, having their zeros offset from each other, provide direct readings for centerline drawing dimensions and for drawing dimensions modified to allow plus and minus cutter off-set. Other tandem indicators are described.

16 Claims, 25 Drawing Figures


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SHEET 2 OF 5
$\rightarrow 9 \quad$ F/G. 8
FIG. 9



FIG. 10


FIG.//

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## FIG. 12



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## EXTENDED-SCALE INDICATORS

This invention relates to scale indicators, especially useful for the lead screws of milling machines.

In many respects, the present invention is an improvement over the indicator in my prior U.S. Pat. No. $3,198,165$ granted Aug. 3, 1965. That patent discloses an extended-scale indicator including two belts, one bearing small-scale-division numbers and the other bearing large-scale-division numbers. The two belts are operated in unison by a common sprocket at the viewing region. One belt is slightly longer than the other so that the large-division belt shifts incrementally in relation to the small-division belt for each cycle of the small-division belt. A mask forming part of the smalldivision belt covers most of the large-division belt, but apertures in the mask expose selected large-division numbers successively. Thus, while the numbers of the small-division belt as displayed at the viewing region advance from 0.000 to 0.990 and back to 0.000 , the related numbers of the large-division belt as revealed at intervals by the apertures of the mask are (large-division belt vs. small-division belt): $0: 0.000 ; 0: 0.250$; $0: 500 ; 0: 0.750 ; 1: 0.000$, continuing to 24:0.000.
In order to provide for the required incremental advance of the large-scale-division belt during a cycle of travel of the small-division belt, the two belts depend as loops of different lengths, held taut by the weight of respective idler pulleys whose axes are at different levels.
The two-belt indicator in that patent serves for indicating a distance from a starting position in one direction. To indicate operation in the reverse direction, both belts are lifted from a sprocket, reversed, and applied to the sprocket so as to display reverse-direction numbers. Pursuant to certain features of the invention, the two-belt indicator described in my patent is improved by making it more compact, by providing an enclosure that keeps the belts clean and protects them from damage, and by enabling operation of the indicator in either direction away from a starting " 0.000 " b without rearranging the belts on the sprocket.

The indicator in my patent was actually designed dimensionally as an attachment for a Bridgeport milling machine. One tape of the indicator in my patent gives a partial position reading, and the other tape completes a numerical reading each time an aperture of the mask appears at the viewing region. In the patent, an aperture of the mask appears at the viewing region at intervals representing a quarter-inch travel of the table. The table lead-screws of "the Bridgeport" have a pitch of 0.200 inch, so that $11 / 4$ turns of the "Bridgeport" tableposition lead-screws are needed to go from one complete numerical indicator reading to the next. Correspondingly, the lead-screw hand crank must be rotated an awkward $11 / 4$ turns from each complete numerical reading to the next. A feature of the present invention resides in providing an indicator that gives a complete numerical reading once (or at least once) for each rotation of the hand crank.

The vertical lead screw of "the Bridgeport" (for table adjustment) has a pitch of 10 turns per inch. A further feature of the invention involves a distinctively different scale concept than in the indicators for the horizontal lead-screws.

The invention also involves novel features of more general application, also being applicable (for example) to multiple-dial indicators. (That type of indicator involves expensive gear coupling between the dials that is avoided in the preferred multiple-belt indicator described below.) As a generic feature, while two series of small-division numbers are displayed corresponding to both operating directions, there is no need to conceal the series not in effect. Only one series of largedivision numbers is displayed, corresponding to the selected direction of displacement of the indicator from zero. The selectively displayed large-division numbers have an appearance that provides automatic visual identification with the series of small-division numbers that relate to the selected direction of displacement from zero.

A novel manipulatable reminder is provided, useful with the present extended-scale indicator and other scale indicators, to relate the table location to the reading of the indicator in a way that eliminates back-lash reading error. This is an extremely useful feature, which is added to standard machine tools of the type having inherent lead screw back-lash. Once a sequence of operations is decided, the setting of the reminder indicates the direction that the lead-screw crank should be operated in order to avoid a back-lash reading error, a very large and unacceptable error in many machine tools.
A still further distinctive and important feature of the invention resides in providing an indicator for a lead screw having a standard pitch in one system of units, especially inches, enabling adjustments of the lead screw to be made according to another system of units, especially metric. This is achieved here for "the Bridgeport" by a dual-tape indicator in which a smalldivision cyclic-number tape has a 500:127 ratio to the circumference of the sprocket, i.e., in which there are 500 sprocket holes (or an integral multiple of 500 ) and a sequence, effectively, of 127 sprocket teeth, as more fully explained below. The ratio $500: 127$ is a basic characteristic useful in indicators generally, and is not limited to the Bridgeport.
It will be recognized that, in an indicator having a sprocketed tape, highest standards of accuracy require the scale division marks to be carried by a dial, not by the tape. Lost-motion between the sprocket holes in the tape and the sprocket teeth would be but one source of error were the division marks carried by the tape. However, the circumference of the sprocket would have a number of division marks, equal to 127 times a small integer, e.g., 254 division marks about the sprocket circumference. The cyclic tape with its decimal numbers requires associated large or distinctive division marks every fifth or tenth one of the series of division marks, but the number " 254 " is obviously not divisible by 5 or by 10 . High precision of division marks is here obtained with a tape-to-sprocket ratio of $500: 127$ by applying 254 division marks to a dial united to the sprocket, together with a gage pattern on the tape associated with the decimal series of numbers on the tape. The gage pattern of the tape establishes the important emphasis for every tenth one of the uniform division marks of the dial on the sprocket, and it also provides subsidiary emphasis for the fifth and other division marks in each group of 10 .

A still further feature of the invention involves the concurrent use of multiple interlocked direct-reading indicators for various distinctive results. For example, two direct-reading indicators may be locked together on a common lead screw, one having a "metric scale" in relation to the lead screw and the other having an inch-system scale in relation to the lead screw. These indicators can be used for converting dimensions between the metric and inch systems; and these two indicators can also be used for adjustment of a machine tool in machining operations following a drawing having dimensions in both metric and inch systems. In another example, three identical indicators on each of the table lead screws of a milling machine can be used together to avoid calculations involving center locations as well as dimensions of the extremities of a cut made by a milling cutter of specified diameter. One of the three indicators is set to indicate centerline dimensions, a second indicator is set to indicate centerline-plus-cutter-radius, and the third indicator is set to indicate centerline-minus-cutter radius. Depending on the particular drawing dimensions being followed, different indicators are available for use directly, avoiding calculations involving the cutter diameter. Multiple complements of indicators locked together can also serve in executing sequences of machining operations to make multiple parts successively using a common piece of stock clamped to the work table.

In these and many other uses of tandem indicators, it is usually desirable and sometimes vital for each indicator to be separately adjustable and then individually locked to the lead screw while another indicator is(or is not) locked to the lead screw.

Accordingly, a feature of the invention resides in providing a lead screw, especially a lead screw in a milling machine, with a succession of indicators that are individually adjustable relative to the lead screw and which can be individually locked to the lead screw in their respective adjustments.

Many machines using a lead screw and a dial or a direct-reading scale for positioning an element, especially the table of an old and worn milling machine, have an inherent cause of inaccuracy, namely, the variations in the pitch of the lead screw along its length. A feature of the invention resides in providing the lead screw with an indicator that can be calibrated by the machine attendant to provide a correction value at each turn of the lead screw, in this way providing ex-tended-scale, virtually continuous readings over all or any desired part of the operating range, to enable on old, worn or otherwise inaccurate machine to function with the accuracy of a new one. By this means, needed corrections in a worn milling machine of as much as 0.010 and more can be made known and available. The milling machine can then be operated to jig-borer accuracy, to a fraction of a thousandth.

The foregoing and other objects and novel features and their advantages are more clearly evident in the illustrative embodiment of the invention as shown in the accompanying drawings and described in detail below. In the drawing:

FIG. 1 is a fragmentary perspective of part of a milling machine drawn to reduced scale, showing a novel extended-scale indicator as an illustrative embodiment of the invention, coupled to the cross-feed operator.

FIG. 2 is a top plan view of a novel extended-scale indicator and the cross-feed operating handle of the milling machine of FIG. 1, drawn to approximately full scale.

FIG. 2A is a fragmentary top plan view of the viewing region of the indicator of FIGS. 1 and 2, including another form of scale useful for the vertical feed screw of the same milling machine, the indicator being shown in its "common zero" position in readiness for operation in either of two opposite directions.

FIG. 3 is a fragmentary cross-section of the novel ex-tended-scale indicator as seen from the plane $3-3$ of FIG. 2.

FIG. 4 is an enlarged fragmentary top plan view of a portion of a support for the transparent cover of the novel indicator, including a portion of a signal for indicating the direction of operation of the milling machine lead-screw to avoid back-lash error.

FIG. 5 is an enlarged fragmentary top plan view of a portion of the transparent cover of the novel indicator showing another portion of the signal for indicating the direction of lead-screw operation to avoid back-lash error.

FIGS. 6 and 7 are enlarged fragmentary views showing the parts of FIGS. 4 and 5 assembled so that the signal parts of FIGS. 3 and 4 complement each other to form direction signals to show operation of the novel extended-scale indicator to the right and to the left, respectively, in the direction required to avoid backlash error.

FIG. 8 is an enlarged front elevation of the cover support of FIG. 4.

FIG. 9 is a cross-section of the cover support of FIGS. 4 and 8 as viewed from the plane 9-9 in FIG. 8.

FIG. 10 is a front elevation of the novel indicator drawn to reduced scale and with the front half of a twopart enclosure removed.

FIG. 11 is a vertical cross-section of the novel indicator as viewed from the plane 11-11 in FIG. 10.

FIG. 12 is a fragmentary view of the two extendedscale belts shown side-by-side, for use assembled in the novel indicator as in FIG. 2A.

FIG. 13 is an approximately full-scale drawing of successive segments of the endless belts of FIG. 12 showing the entire length of the belts with some duplication, illustrating their relationships that become effective as the belts are advanced past the viewing region of FIG. 2A.

FIG. 14 is a fragmentary illustration of the continuous tapes to be incorporated in an extended-scale indicator like that of FIGS. 1-11, for providing a $0.200-$ inch lead screw with metric readings.

FIG. 15 is a fragmentary illustration of continuous tapes like those of FIG. 14, for providing a 0.100 -inch lead screw with metric readings.

FIG. 16 is an enlarged fragmentary cross-section of a modification of the dial-sprocket-pointer assembly for the extended-scale indicator of FIGS. 1-11.

FIGS. 17 and 18 are an enlarged fragmentary perspective and an enlarged top plan view, respectively, of the pointer and the dial in FIG. 16.

FIG. 19 is an enlarged fragmentary view of a small-scale-division tape shown in FIG. 15.

FIG. 20 is an enlarged plan view showing the parts of FIGS. 18 and 19 assembled in operative relationship.

FIG. 21 is a developed view of the cylindrical face of a modified sprocket for a further modification of the indicator of FIGS. 1-11.

FIG. 22 is an enlarged detail showing a portion of the sprocket of FIG. 21 together with associated parts of this further modification of the extended-scale indicator of FIGS. 1-11.

FIG. 23 is a side elevation of three tandem indicators like that of FIGS. 1-11, shown partly in cross-section along the shaft axis therein, illustrating still further aspects of the invention.

FIG. 24 is a cross-section of the assembly of FIG. 23 as viewed from the section line $24-24$ therein.

In the drawings, the illustrative form of extended scale indicator 10 is shown installed on a Bridgeport milling machine. Indicator 10 includes an enclosure 12 that is made of identical front and rear molded parts. A sprocket 14 (FIGS. 3, 10 and 11) has a groove 16 which receives a split or segmented ring 18 secured to enclosure 12 to exclude dirt. Sprocket 14 encloses the standard dial D of the milling machine cross feed, leaving exposed the original scale divisions. Sprocket 14 is adjusted in relation to the scale divisions of the dial $D$, and the two are held in adjustment by double-faced adhesive tape 15 (FIG. 11). Socket 14 and dial D as a unit are clamped to bushing $B$ and handle $H$ of the milling machine cross feed. At the rear, ring 20 bears a doublefaced adhesive overlay 21 that adheres the enclosure 12 to the fixed structure of the milling machine, with ring 18 concentrically in groove 16.

FIGS. 3-9 illustrate the construction of the ex-tended-scale indicator at the region where the scale numbers are to be viewed. Resilient sheet-metal face member 22 has upstanding flanges 24 that form longitudinal guides for a transparent cover plate or bezel 28. Member 22 has resilient panels 30 that are curved upward and have upstanding flanges 26 at their extremities. Flanges 26 limit the lengthwise shift of cover plate 28. Because the cover plate is a little shorter than the distance between flanges 26, the cover plate can shift a short distance lengthwise.

As seen in FIG. 4, part 32 of a direction signalling arrow is printed on panel 30 . Arrow part 32 has each of its ends notched to suggest an arrow tail. Transparent plate 28 has two oppositely directed arrow heads 34 . The arrow part 32, arrow heads 34 and the extend of longitudinal shift of plate 28 between flanges 26 are proportioned so that, with plate 28 shifted to the right against one flange 26 (FIG. 6), the right-hand arrow head 34 and arrow part 32 form a composite arrow pointing to the right. The left-hand arrow head 34 is virtually unnoticeable because it overlies and blends with arrow part 32, both being dark. Shift of plate 28 to the extreme left as limited by the other flange 26 results in a composite arrow 32, 34 pointing to the left. As will be seen, this direction signal will be found useful in indicating to the machinist the direction he should operate the cross feed for reaching any given position. Panels 30 are resilient, and they bias plate 28 against the inside surface of the enclosure, sealing the viewing opening 36 of the enclosure against dirt. As seen in FIG. 3, member 22 rests against a pair of ribs 38. Groove 40 is wide enough to allow panels 30 to be deflected downward far enough to remove flange 26 from the lengthwise path of cover plate 28. This ar-
rangement facilitates assembly of plate 28 into position over member 22; it makes easy the removal and replacement of the cover plate (in case it should become badly scratched) and it provides spring bias to hold cover plate 28 in its sealing position covering the frame opening 36 of the enclosure.
Two endless belts 42 and 44 band overlie sprocket 14 in the space between the front and rear walls of enclosure 12. Preferably, both belts are of transparent plastic film, and the portion of sprocket 14 behind the indicia-bearing areas of the belts in a bright color such as yellow or white. Face member or plate 22 has a beltdisplay opening 46 (FIG. 2) partially framed by parts 48 and $48 a$ that are bent down out of the body of member 22. A pointer 50 is struck out of part 48. Pointer 50 extends close to the dial division marks of dial $D$, so that the original accuracy obtainable with the dial is preserved in the illustrated indicator. Part $48 a$ has arcuate clearance from tape 42, but only a little clearance, so that part $48 a$ prevents the tapes from losing registration with the sprocket teeth.

An indicator containing belts or tapes 42 and 44 is especially useful for each of the table lead screws of the Bridgeport, which have a lead-screw pitch of 0.200 inch. Tape 42 has two series of numbers 52 and 54 that are of contrasting appearance. The numerals of these two series extend in two rows (as shown) all the way around the tape. The circumference or loop-length of tape $\mathbf{4 2}$ is five times the circumference of sprocket 14 , so that one-fifth of each series of numbers travels past pointer 50 in the viewing region each time sprocket 14 completes one full rotation. Each number series extends from zero to 1,000 , at intervals of " 10 ," thus: $000,010,020,040 \ldots 970,980,990$ and back to 000 . Consequently, if 000 is located at pointer 50 and sprocket 14 is rotated five times, the numbers 200,400 , 600,800 and 000 appear at pointer 50 at the completion of the successive sprocket rotations. One series increases for one direction of rotation and the other series increases for the opposite direction of rotation. Beyond five sprocket rotations, the number series repeats, and hence the numeral series of belt 42 are cyclic.

Tape 42 has an opaque stripe 60 that overlies two series of numbers arranged in a row on tape 44. There are apertures 62 in strips 60 adjacent numbers 000,200 , 400,600 and 800 of tape 42 at the ends of successive complete sprocket rotations. There are 100 sprocket holes in tape 42, one hole opposite each number, and there are 20 sprocket teeth on sprocket 14.

Tape 44 has two series of numbers arranged in a row underlying stripe 60 . There are three sprocket holes in tape 44 in the linear space allocated to one sprocket hole of tape 42. There is one sprocket hole opposite each number of tape 44 . The length of tape 44 is greater than that of tape 42 by the pitch of one sprocket hole of tape 44 . Consequently, when tape 42 is advanced one complete cycle past the viewing region, tape 44 advances less than one complete rotation, to the extent of the space allocated to one sprocket hole of tape 44, that is, the small pitch of the sprocket holes of tape 44. In the course of repeated rotations of sprocket 14, tape 44 precesses one small sprocket-hole pitch. There are 301 sprocket holes in tape 44.

At the end (or start) of successive rotations of sprocket 14 , starting with number 000 of tape 42 located opposite to pointer 50 , apertures 62 expose successive numbers of tape 44. This occurs once for each full rotation of handle 14 , and is especially convenient to the machinist. Starting with "*" which represents a common zero of two series of numbers in a row on tape 44, there are two series of numerals of contrasting appearance. Any one of these numbers complements the particular number of tape 42 that is opposite pointer 50 . Thus, number 3 (for example) on tape 44 may be located opposite pointer 50 adjacent number 600 of tape 42, and this represents number 3.600 or a table position 3.600 inches away from that which existed when the "*" common zero was opposite pointer 50. Two series of numbers can appear in apertures 62, one series corresponding in appearance to numbers 52 and the other series corresponding to series 54. Each series includes the following numbers, listed in the order of their display through apertures 62 : *, $0,0,0,0,1,1,1,1,1,2,2,2,2,2,3 \ldots 28,28,29$, $29,29,29,29$ and then arrow. In the course of many rotations of the sprocket, the sprocket teeth enter every hole in tape 42 and every third hole in tape 44, 25 and yet the sprocket holes that are "skipped" in one complete traverse of tape 44 past the viewing region are entered by sprocket teeth in the next two complete traverses of tape 44 past the viewing region. The indicator thus covers 30 inches of table travel in each direction from * as a continuous scale complemented by the scale divisions of dial $D$.

The vertical lead screw of a Bridgeport milling machine has a pitch of 0.100 inch. An indicator having tapes as shown in FIG. 2A and in FIGS. 12 and 13 cover a 20 -inch range of that lead screw. Numbers for the parts of this indicator are the same as the numbers of corresponding parts of the 0.200 -inch-pitch indicator, but here they are primed. Belt 42 ' has two series of numbers $52^{\prime}$ and $54^{\prime}$ that are of contrasting appearance. Belt 44' has two series of numbers and other indicia that also contrast in appearance. Series 52' matches the appearance of series $56^{\prime}$, and series $54^{\prime}$ matches the appearance of another series 58 '. In FIGS. 12 and 13 , the belts are shown side-by-side, but they have the same relative positions (lengthwise) that they would have when assembled in the indicator with belt $42^{\prime}$ overlying belt $44^{\prime}$. An opaque strip $60^{\prime}$ on belt $42^{\prime}$ overlies the indicia $56^{\prime}$ and $58^{\prime}$ of belt $44^{\prime}$ when the belts are assembled. Stripe $\mathbf{6 0}^{\prime}$ is a mask that conceals indicia 56' and 58' except at intervals where the stripe has mask openings $62{ }^{\prime}$. These openings occur, in the case of the belts shown, opposite the zeros of both series of numbers $52^{\prime}$ and $54^{\prime}$. Belts $42^{\prime}$ and $44^{\prime}$ have sprocket holes $64^{\prime}$ and $66^{\prime}$, respectively, identical in number, distribution, etc., as has already been described in the case of tapes 42 and 44.

Two broken-line representations of display opening 46 of member 22 are shown in FIG. 12, representing the condition shown in FIG. 2A. In this condition pointer 50 is opposite " 00 " and "oo" and it is also opposite the "*." This last symbol is the "common zero" or starting point for both directions of motion of the belts or tapes past display opening 46.

It may now be assumed that the belts or tapes are operated from left to right past viewing opening 46,
utilizing the ascending large-size series of numerical indicia. The sprocket causes both belts to advance equally, in unison. The large-face numbers advance from " 00 " to " 45 " near the imaginary break B in belt $42^{\prime}$ 'at the left of FIG. 12, continuing from B at the right in FIG. 13, to " 50 " and back to a new " 00 ." As belt 42' advances past display opening 46, mask aperture $6^{\prime}$ initially exposes the common-zero symbol "*" and mask 60 then conceals all of small-face number series $58^{\prime}$, "off-scale" arrows $68^{\prime}$ and $70^{\prime}$, and most of largeface number series $56^{\prime}$. When the belt $44^{\prime}$ arrives at ". 1 " of number series 56 ', the next aperture 62 ' exposes that number. Thus, for the first group of numbers " 00 " to " 00 " of series 52 ' on belt 42 ', the numbers of series 56' advance from zero to .1 , for a change in the composite reading from ". 000 " to ". 100 ." Accordingly, both belts are advanced in unison, and group ( 00 to 95 ) after group ( 00 to 95 ) of numbers in series 52 ' pass the viewing opening 46, one such group for each rotation of the hand crank. Mask apertures $62^{\prime}$ successively display "*", ". 1 ", ". 2 ", ". 3 ", ". 4 ", and ". 5 " of the large-scale-division series of numbers 56 ". In this sequence from "*" to ". 5 ", tape or belt 42 ' has completed one cycle past viewing opening 46, and longer tape belt 44' has advanced only one increment less (in the illustrated example). Continued advance of the belts brings numbers .6 to 1.0 and so on up to 9.9 into view for a maximum scale reading of 9.900 at that point and effectively to a reading of 9.995 in the course of the further advance of the belts. As shown in FIGS. 2 and 11, the sprocket drum 14 complements the dial $D$ of the Bridgeport milling machine which bears index marks subdividing the readings at pointer 50 from " 00 " to " 05 " into five places. Thus the extended scale reading here reaches 9.999 , representing 10 inches of vertical feed, shown by 90 feet of travel of belt 42 whose circumference, in an example, is substantially $41 / 2$ feet long. Reverse operation of the extended scale indicator produces a further indication from "*" to 9.999 in another 90 feet of belt travel. When both extremes of " 9.9 " are exceeded, the scale shows "overshoot" arrows 68 and 70 , pointing the direction needed to manipulate the extended-scale indicator back into the numerical range. If a range greater than 9.9 of the large-scale-division tape were wanted, then 10.0 etc. or equivalent could be provided to the limit 15.0 for this tape.
The points in the belt represented by breaks $A$ and $a$ at the right of FIG. 12 (to the right of " 90 " and " 3.5 ", respectively) incur a relative shift by the time ". 5 " is advanced into position opposite " 00 " as represented at the bottom of FIG. 13. This shift is represented by the relative off-set between broken-line markers $A^{\prime}$ and $a^{\prime}$ at the bottom of FIG. 13, representing the same points A and $a$ of FIG. 12. The The reverse relative shift would occur in one full reverse cycle of belt 42, so that points J and $j$ at the bottom of FIG. 13 would be related as $J^{\prime}$ and $j^{\prime}$ in FIG. 12. Belt 44 has a sprocket hole opposite each significant number or other index mark that is to be located opposite 00 of belt 42 .

The depending lengths of belts 42 and 44 in the example above, if draped over sprocket 14 , would be about 2 feet. Enclosure 12 contains common idler pulleys 72 on respective pins 74 . These pulleys shape belts 42 and 44 into a compact serpentine or labyrinth-like
configuration, and pulley 76 takes up the slack of the slightly greater length of belt 44 . Plate 78 is a lateral guide for the edges of the belts, directing the belts into proper position for cooperation with the teeth of sprocket 14.

The belts move in unison past the viewing opening 46 in face member 22, but because of the difference in their loop lengths the longer (inner) belt 44 advances an "increment" less than one full cycle each time belt 42 completes a cycle. This relative shift results in a change of the scale number that is displayed, but the shift does not involve relative sliding between the belts in their serpentine or labyrinth-like path over idlers 72. Even though belts 42 and 44 are in face contact along nearly their whole lengths (excluding the short part of belt 44 that is diverted by idler 76) there is no serious wear problem.

The extended-scale indicator that is added to the milling machine does not degrade the precision of the original milling-machine dial. As already noted, the divisions of dial D are utilized, and the dial and the sprocket are united in a way that precludes both erratic and progressive errors.

The common zero "*" or any other scale reading can be set in position for any job being done by loosening nut N (FIG. 11), and manipulating knob portion $14 a$ of the sprocket to set the indicator to the desired position and then locking sprocket 14 to the milling machine cross-feed by tightening nut N . With the nut N loose, the handle $H$ can be manipulated for operating the table to any desired position without materially changing the indicator reading. This is because a limited amount of friction inherently present in the indicator resists shift of the indicator tapes out of any given reading. This friction will be found at many places, notably at the tape supporting parts including the sprocket 14 , rollers 72, etc. In this way the table can be set at a desired starting position in relation to a given reading of the indicator.
The reversible arrows $\mathbf{3 2}, 34$ form an important adjunct to the extended scale indicator for the milling machine lead screws. A certain amount of looseness or play is characteristic of lead screws. This play can be nullified as a source of error in many sequences of operations requiring exact setting of the table position by consistently approaching each required table setting by operating the lead screw consistently in the same direction for approaching and reaching each new setting. In the course of a series of such settings, it may be necessary to reverse the motion of the lead screw to reach a particular setting, but even then, the lead screw should be operated more than required in that reverse motion, completing the adjustment by operating the lead screw in the adopted consistent direction used in the other settings of a sequence. That direction is used consistently, with the aid of the direction-of-adjustment signal arrows.
A slightly modified structure compared with that already shown and described can be used in the Bridgeport, and for English-system lead screws generally, in converting such machines to settings according to the metric system. For example, it has already been noted that the table lead screws of the Bridgeport have a pitch of 0.200 and that the leadscrew indicator makes precisely one complete rotation
in operating the table through a distance of 0.200 inch. In accordance with a feature of the invention, a metric extended-scale indicator can be formed largely as shown in FIGS. 1-11 and thus far described, to replace or to supplement the existing dial.

A ratio of 25.4 to 10.000 has been accepted as a valid approximation for conversion of inch dimensions to millimeters. This is basic to the metric extendedscale indicator now to be described.
In an embodiment of a metric indicator for an "inchsystem" lead screw, sprocket 14 is equipped with 127 sprocket teeth and outer small-scale-division tape $42 a$ has 500 sprocket holes, and the ratio of the circumference of the sprocket to the loop-length of tape $42 a$ is 127 to 500 (equal to 254 to 1,000 ). It is not necessary for all 127 sprocket teeth to be present, since obviously the operation of the sprocket and belt or tape would not change if many of the 127 teeth were removed. As a practical approximation, 20 sprocket teeth properly distributed around the sprocket at points chosen to simulate a 127 -tooth sprocket will adequately serve for cogging the tapes to the sprocket. The second tape $44 a$ in this illustrative metric indicator is made two sprocket holes longer than tape $42 a$, in order to allow a space of two sprocket teeth for the large-division-scale numbers, and accordingly "windows" or apertures 62 in stripe $\mathbf{6 0}$ are two sprocket teeth long.

An indicator tape $42 a$ for the metric lead-screw indicator described to this point for a 0.200 -inch lead screw has two cycles of fifty numbers from 0.0 to 9.8 by mm ., by 0.2 mm . jumps. The large-scale-division tape $44 a$ "*" representing "common zero" for two series of numbers enabling operation of the indicator in either desired direction with numbers increasing from'zero. The numbers of each series on the large-division tape, starting with common "*" are: $0,1,1,2,2, \ldots 60,60$, 61 , with windows 62 occurring opposite the " 0.0 "s and the " 0.5 "'s. These numbers complement the same-scale-division numbers on tape $42 a$, e.g., $61 / 0.0$ to represent 610 mm . FIG. 14 is an illustration of the numbers of tapes $42 a$ and $44 a$ of a metric indicator for a " 0.200 -inch" lead screw.
A metric indicator for a " 0.100 -inch" lead screw, in an example, has one cycle of 100 numbers from 0.0 through 9.9 in sequence, by 0.1 mm . jumps, on tape $42 a^{\prime}$. The large-scale-division markings are ${ }^{*}, 0,0,0,1$, $1,1,1,2, \ldots 30,30,30,30,31$, in each direction as before. These numbers are exposed by four windows 62 , respectively, opposite the numbers $0.0,2.5,5.0$ and 7.5 of the small-scale-division tape 42a'. The range of the indicator for each direction of operation from "*" is 310 mm . FIG. 15 shows the numbers of illustrative met-ric-scale tapes $42 a$ ' and $44 a$ ' for a " 0.100 -inch" lead screw.
The metric-scale tapes obviously cannot be used with the original scale divisions on dial $D$. It is not even practical for a substitute for dial $D$ to be used here, directly. This is because 254 dial marks are needed around the sprocket for providing 0.02 mm . division marks with the tapes described in connection with a metric indicator for a " 0.200 -inch" lead screw, and every tenth scale mark requires emphasis for easy and positive identification with a number on the small-scale-division tape. Likewise, 254 scale divisions are needed for providing 0.01 mm . division marks with metric tapes for the
" 0.100 -inch" lead screw, and every 10 th division mark requires emphasis.

It would be possible to apply the scale division marks to the edge of the small-scale-division tapes. This would introduce inaccuracy due to various causes. For example, any looseness of the sprocket teeth in the sprocket holes would introduce error, and some looseness here is useful for easy operation and non-critical manufacture. The basic accuracy of the lead-screw dial is preserved and emphasis of the tenth-scale-marks is realized by means of the arrangement shown in FIGS. 16-20.

In FIG. 16, dial $D a$ is a ring on the original dial $D$, centered on dial D by a resilient tube 79 (as of rubber) and cemented to the edge of sprocket 14, here equipped with 127 -pitch sprocket teeth. Dial Da has new and precisely formed uniform scale markings 80 , there being 254 of them around the dial circumference. Pointer $50 a$ is a modified form of pointer 50 but the structure supporting the pointer here is otherwise unchanged. FIGS. 17 and 18 show the relationship of pointer $50 a$ and division marks 80 of dial $D a$.

As seen in FIG. 19, tape 42a' (for example) is equipped with a marginal gating pattern 82 , including deep gate apertures 84 (measured from the edge of the tape). There are shallow and progressively deeper steps between apertures 84 , the deepest step 86 being midway between apertures 84. In FIGS. 16 and 20, tape $42 a^{\prime}$ overlies part of the width of the ring in which scale marks 80 are formed. Tape $42 a^{\prime}$ is transparent and gating pattern 82 is opaque. Apertures 84 are spaced apart at centers equal to the space between teeth marks 80 . In this way, when the gating pattern of tape $42 a^{\prime}$ overlies scale markings 80 , every scale mark opposite a number on the tape appears long, the "fifth" scale marks between the "tenth" scale marks are emphasized, and the stepped pattern facilitates reading the scale markings between the "fifth" and "tenth" scale markings. In FIG. 20 it is eminently easy to recognize the reading " 9.23 " opposite pointer $50 a$.
Each of the steps of the gating pattern, and apertures 84 as well, are as wide as the pitch of scale markings 80. In this way, even if there is slight shift or drift of the tape in relation to the sprocket, within the latitude of one space between dial marks 80 , the dial reading remains unaffected. Every tenth mark 80 is emphasized in relation to different ones of those 254 marks in the course of successive rotations of the sprocket.

The precise structure thus far described is utilized in yet another important feature of the invention. In a further modification of the indicator, a means is provided for vastly improving the accuracy of "the Bridgeport" and of machines generally, that depend on accurate setting of an element by means including a lead screw equipped with a dial or an extended scale. The readings of an indicator such as a dial or a scale are linear, so the system presumes strict linearity of the adjustment effected by the lead-screw. This assumption may be inaccurate when a machine tool is new, but it is not valid after the machine has become worn. The invention, in one of its aspects, provides a virtually continuous means of knowing the reading error of the indicator in a machine of this kind.

In FIGS. 1-11, it may be considered that tape 42 is omitted and that tape 44 and the sprocket are
modified, as indicated in FIGS. 21 and 22. Sprocket $14 b$ is made black or any dark color, and has a number of isolated bright-colored areas. Tape $44 b$ as supplied has a series of printed numbers 90 . The circumference of sprocket $14 b$ relative to the loop length of tape $44 b$ is such that precession occurs, being other than an integral multiple of the sprocket circumference. One bright-colored area 92 on the sprocket will underlie one number 90 as the bright area 92 and the number move across the viewing region of the indicator (There may be two diametrically opposite areas 92 , or more, depending on the proportions.) In successive rotations, successive numbers 90 overlie bright area 92 and become effective visually. The other dark-colored numbers are effectively obliterated, visually, by the dark color of the sprocket. These numbers form an ex-tended-scale indicator.

Adjacent area 92 on sprocket $14 b$ there is additional bright area 94, having two ears 96 and 98 . The areas of tape 42 b that overlie the additional bright area upon successive rotations of the sprocket are available to the user for inscribing correction factors. This is done in the following way.

At some point in the range of the lead screw, the mid-point for example, the sprocket and the lead screw are operated in a selected direction to bring a preprinted number over bright area 92, accurately positioned as determined by pointer 50. Bezel 28 is removed, by flexing one panel 30 downward. This deflects edge 26 from the removal path of the bezel, which is then slipped out of the indicator leaving the tape $44 b$ exposed and accessible for writing-in the applicable correction notations. A symbol representing "plus" or "minus" representing the direction of the error or the required correction may be written directly; or it may be recorded (as shown) by applying a dark mark on the tape over ear 96 or 98 , and " 0 " is recorded on the tape over the additional bright area on the sprocket. Then the sprocket is rotated exactly one revolution to bring the additional bright area 94 opposite pointer 50, operating the lead screw in the adopted direction in approaching the end-point of the adjustment so as to eliminate the back-lash error considered previously. This can be done by rotating the lead screw and the sprocket in the decided direction and stopping at the $360^{\circ}$ point; or the lead screw and the sprocket can be rotated in the reverse direction more than $360^{\circ}$, to be followed by rotation of the sprocket in the decided direction to the $360^{\circ}$ end-point of the adjustment. The distance moved by the millingmachine table or other element operated by the lead screw can be measured accurately in a routine way, and compared with the distance indicated by the new number over bright area 92 as compared with the previous number. Any error is recorded as a number 100 on tape $44 b$ over bright area 94 and once again a mark is applied to tape $44 b$ over ear 96 or 98 as a symbol representing the sign of the error to be added or subtracted in the adjustment. This procedure is continued until all (or any desired part) of the continuous scale readings 90 have an accompanying correction notation 100. Bezel 28 is then slipped into place, and it is adjusted so that the proper arrow (FIG. 6 or FIG. 7) is formed to show the direction of operation of the indicator and of the lead screw for which the correction
is valid. Considering back-lash, and the opposite driving surfaces of the lead screw, a very different calibration would be needed for the opposite direction of operation.
As shown in FIG. 22, the error notation is "6.3." This represents the precise departure of the lead screw from linearity, when number 90 is opposite the pointer $\mathbf{5 0}$. If some other setting is desired in the routine use of the machine, then the proper correction factor is determined by interpolating between the two error notations to either side of the desired setting. Interpolation is aided by nine uniformly distributed bright points 102 along the edge of sprocket $14 b$ and by a 10 th such point forming part of bright patch 92. For example, if two correction notations at opposite sides of a desired setting are " 6.3 " and " 4.6 ," then the difference is to be apportioned between the extremes. If the indicated setting is three "points" away from the " 6.3 " error reading, then the correction is 6.3 minus 0.3 (6.34.6) or 5.8. The absolute scale markings " 28.2 " for which the calibration error is 6.3 in this example means " 28.200 "; and so, if the required setting turns out to be about 0.3 of a dial rotation away, e.g., 28.231, and if the applicable correction is 5.8 , and if this correction is "minus" as indicated by an entry over "ear" 98 adjacent the correction value " 6.3 ", then the dial is set at 28.2252. Care must be taken to reach this setting by operating the hand crank in the right direction toward this end-point, as indicated by the arrows of bezel 28 for which the calibration is valid. The arrangement makes possible a degree of accuracy that may well exceed that of the new machine. A milling machine that is worn significantly can be operated with jig borer accuracy with the described extended-scale error calibration.

After all the desired error notations have been entered, bezel 28 is slipped into place, and it is set to indicate the direction of lead-screw operation for which the error notations are valid. The error notations can be revised from time to time, when further wear of the lead screw is noted.

A separate extended-scale indicator precisely like that in FIGS. 1-11 may be used with the calibration indicator just described, by uniting the separate ex-tended-scale indicator to the calibration indicator in a manner described below. The added extended scale indicator can be adjusted to have any desired zero point, as may be appropriate to the job being done. That adjustment does not upset the calibration indicator.
Space permitting (as through the use of a wider sprocket) two bright areas 94 may be provided side-byside, and in that modification two sequences of error notations might be inscribed as error calibrations applicable to the two directions of lead-screw operation, respectively, one being that represented by the selectively set arrows of bezel 28 and the other being applicable to the reverse direction of lead-screw operation.

FIGS. 23 and 24 show extended scale indicators assembled in tandem. As an example, two tandem indicators can be used together where one is of the form in FiGS. 1-13 giving "English" readings and the other is "metric" as represented in FIGS. 16-20. This assembly is useful for a milling machine, in following a drawing having mixed "English" and "metric" dimensions, or
for checking drawings involving a conversion from either system of dimensions to the other, and for various other uses. A calibration indicator can be fixed to a lead-screw shaft and used with a separate extended-
5 scale indicator (FIGS. 1-11) that is adjustable to establish a desired zero for each new job. Two or more identical extended scale indicators can be used for maintaining separate zeros in machining duplicate parts or multiple different parts out of a single piece of stock. A single lead-screw calibration indicator as described above can be used together with these multiple indicators.
The tandem lead-screw extended-scale indicators of FIGS. 23 and 24 include one such indicator 10 that is identical to that in FIGS. 1-11. Two additional indicators $10 a$ and $10 b$ are of the same construction externally but are modified internally in particulars to be described. In this example, three extended-scale indicators are used in tandem for each of the two horizontal lead screws of the table in a Bridgeport milling machine. One of the three is adjusted so that its common zero indicates a drawing coordinate related to hole centerlines. A second identical indicator has its 5 zero off-set from that of the first indicator in one direction so that it represents "plus" cutter off-set, and the third identical indicator has its zero off-set from the first indicator in the opposite direction so that it represents "minus" cutter off-set. In this way, the first indicators of the table lead screws show the relative position of the cutter axis, while the other two represent the desired positions of the cutter axis to make a cut whose edge or outline dimensions are shown on the drawing. The inclusion of three extendedscale indicators thus avoids the need for cutter off-set calculations, as a further expediting and error-reducing advantage. As with a single such indicator, the bezels 28 are set to provide arrows showing the adopted direction of operation, to be used consistently in order to avoid error due to lead-screw back-lash. Additionally, it is to be understood that a lead-screw calibration indicator can be added in precisely the same manner as will be described for the two added ex5 tended-scale indicators shown in FIGS. 23 and 24.

All three extended-scale indicators $10,10 a$ and $10 b$ of FIG. 23 have enclosures 12 which contain the same form of sprocket 14 with its knob $14 a$ projecting out of the enclosure 12. On each sprocket there is a pair of 0 continuous or looped extended-scale tapes 42 and 44 as previously described.

Shaft $S$ of the Bridgeport, being an extension of the lead screw, bears bushing $B$ of the Bridgeport that supports the Bridgeport dial D, bearing sprocket 14 in unit 10. A special clamping nut 106 locks sprocket 14 to bushing B, or releases the sprocket for adjusting the common zero of indicator 10 , as desired. Nut 106 has four arms 108 for operating nut 106. The spaces between each of the units 10 and $10 a$, and between units $10 a$ and $10 b$ are available for operating knobs $14 a$, and the spaces between the arms 108 are available for the operator's fingers in adjusting the sprockets as desired.
Indicators $10 a$ and $10 b$ lack the original Bridgeport dial D. Rings 110 which bear scale division marks replace dial $D$ in units $10 a$ and $10 b$. These rings 110 are united as by cement to the edges of the respective
sprockets 14 of units $10 a$ and $10 b$. A bearing ring 112 is fixed to ring 20. Bearing ring 112 is journalled at its center hole on a bushing 114, accurately supporting enclosure 12 at the proper axis. A centrally flanged annular bearing 116 fits in the scale-division-marked ring 110 and is journalled on bearing ring 112 , providing a support for the sprocket. Bushing 114 is threaded to fit another locking nut 106 (or original nut N of the Bridgeport) to clamp the sprocket in its desired adjustment. The center hole of the sprocket fits a cylindrical centering surface of the bushing, providing another bearing support for the sprocket spaced axially from annular plate 116. This structure in units $10 a$ and $10 b$ provides stable centered support for the sprocket in any indicator that lacks dial $D$ of the Bridgeport.

The shaft S of the Bridgeport, bearing the dial D , is long enough to carry the handle $H$ and a further nut $n$. A key $K$ is received in a keyway in shaft $S$ and in a keyway in bushing $B$ and (ordinarily) in a keyway in handle $H$. Here, however, key $K$ extends in keyways in bushing B and in shaft S, and in a keyway in bushing 114. Another key 118 is greatly elongated and extends along keyways in bushings 114 and 114' so that these bushings are constrained against independent rotation Likewise a greatly elongated key 118 ' extends along keyways in bushing 118' and handle H .

Shaft $S$ is elongated a modular distance by hollow internally threaded extension shaft $\mathbf{1 2 0}$. Its length is equal to that required for one added tandem extendedscale indicator. A screw $\mathbf{1 2 2}$ is received and tightened in the right-hand end of shaft 120 , the internal threads extending only far enough for receiving half of the length of screw 122. The part of screw 122 that projects (virtually integrally) from hollow shaft $\mathbf{1 2 0}$ simulates the threaded end $s$ of original shaft $S$ of the Bridgeport.

A duplicate hollow shaft $\mathbf{1 2 0}^{\prime}$ and screw 122' extend as a unit from shaft-and-screw unit 120, 122. Its length is appropriate for the added indicator $10 b$. Handle H is held on extension shaft unit $\mathbf{1 2 0}^{\prime}, \mathbf{1 2 2}^{\prime}$ by nut $n$. Hollow shaft 120' is threaded on screw 122 and tightened against shaft 120. Shaft $S$ and units $120-122,120^{\prime}-\mathbf{1 2 2}$ ' behave as if it were a unitary shaft, in supporting indicators $10 a$ and $10 b$, additionally carrying handle H . Bushings 114 and $114^{\prime}$ are carried by the extended shaft in just the same way as dial $D$ is carried by shaft $S$, with the incidental exception that it is unnecessary for keys 118 and $118^{\prime}$ to be received in keyways in the modular shaft extension units 120-122 and 102'-122'.

Shaft S, bushings 13, 114 and $114^{\prime}$ and handle H are all keyed together so that they cannot rotate independently. The keyed interconnection is not depended on for holding them together as a unit. The keyed interconnection would introduce some possible looseness. However, these parts are held together to act dependably as a unit when nut $n$ is tightened.

The three indicators $10,10 a$ and $10 b$ are separately adjustable by virtue of the individual clamping nuts 112, 112' and N which are loosened individually to adjust the respective sprockets 14 individually and tightened to lock the respective sprockets individually. In another construction, nuts 112 and $\mathbf{1 1 2}^{\prime}$ can be omitted so as to depend on nut N when tightened to lock all the sprockets or to allow them to be manually rotated individually. However, in the preferred con-
struction shown, there is no chance of a previous perhaps critical setting of one indicator being disturbed accidentally during the adjustment of a second indicator. This is an advantage realized through the use of separate clamping nuts for the sprockets of the respective indicators.
The enclosure 12 of indicator 10 is adhered to the frame of the milling machine by double-faced adhesive ring 21, as shown in FIG. 11 and described previously. A clamp 124 unites the enclosures 12 of units 10 and 10a, and another identical clamp 124 unites enclosures 12 of units $10 a$ and $10 b$. Clamp 124 includes sides 126 and 128, and ends 130 . Sides 126 and 128 are received between two enclosures 12 , but ends 130 include gripping portions 130a that slope toward enclosure 12; and these gripping portions have edges that dig into enclosures $\mathbf{1 2}$ when screw 132 and nut 134 of side 128 are tightened.

The three tandem extended-scale indicators 10, 10a and 10 b are especially useful in connection with parts drawings having both centerline locations from a zero reference and locations of edges to be cut on a milling machine by a cutter having a chosen radius. An individual extended-scale indicator $\mathbf{1 0}$ has important advantages, notably in avoiding calculations and in avoiding turns-counting of a standard Bridgeport dial. The three duplicate tandem indicators avoid still further calculations when set individually to read centerline dimensions and dimensions modified to incorporate plus and minus cutter off-set dimensions, respectively.

It has been indicated that a calibration indicator as in FIGS. 16-20 can be used individually, but it can also be used as one of two or more tandem units. When this is done, its clamping nut (corresponding to nut 106) should not include arms 108. This is to avoid any possibility of thoughtless release of the sprocket 14 of such calibration unit. When a calibration extended-scale indicator has once been calibrated to indicate the relative corrections required at each point along a lead screw for true linear indications, there is no occasion for releasing and readjusting its sprocket 14. An ordinary wrench-operated hexagonal nut would advantageously place nut 106, requiring the attendant to be quite deliberate in releasing the sprocket of the calibration unit if adjustment should become necessary on occasion.

What is claimed is:

1. An extended-scale indicator having
i. means defining a viewing region including means for indicating particular indicia in said viewing region,
ii. a first member cyclically operable in either of two opposite directions relative to said viewing region, said first member having first and second endless sequences of small-division numerical indicia, said sequences being divided into the same number of groups including at least one group in each sequence, the indicia within any one group of the first sequence as indicated by said indicating means increasing in one direction of operation of said first member and the indicia within any one group of the second sequence as indicated by said indicating means increasing in the opposite direction of operation of said first member, the indicia of said first and second sequences including
respective zeros aligned with each other for concurrent indication,
iii. a second member having two sequences of largedivision numbers operable past said viewing region for individually complementing said small-division numerical indicia to constitute composite readings of the extended-scale indicator, said two sequences of large-division numbers having a common zero arranged to be indicated in a starting position in said viewing region when two of said small-division aligned zeros are in indicated position,
iv. said extended-scale indicator having means coupling said first and second members together for coordinated advance past said indicating means,
v. the large-division indicia of one of said two sequences thereof being arranged to reach the indicating means successively in increasing order each time the small-division zeros reach the indicating means during operation of said first and second members in one direction from said starting position, and
vi. the large-division indicia of the other of said two sequences thereof being arranged to reach the indicating means successively in increasing order each time the small-division zeros reach said indicating means during the operation of said first and second members in the opposite direction from said starting position.
2. An extended-scale indicator in accordance with claim 1, wherein said first and second members are endless belts and including an enclosure for said endless belts; said coupling means including a common sprocket in said enclosure, each of said belts having sprocket holes cooperating with said sprocket, and plural guide rollers distributed in said enclosure, said belts extending for the most part in parallel paths about said guide rollers, and a further guide roller for part of only the longer one of said two belts, for taking up the slack thereof.
3. An extended-scale indicator in accordance with claim 1, further including means for obscuring the sequence of large-division numbers corresponding to the direction of operation of said members opposite to the operating direction.
4. An extended-scale indicator in accordance with claim 1 wherein said first and second small-division sequences of numerical indicia contrast in appearance from each other and correspond in appearance with respective ones of said two sequences of large-division indicia.
5. An extended-scale indicator in accordance with claim 1 wherein, when said members are displaced in a given direction from said starting point and are operated in said given direction, one of said two sequences of large-division numbers increases and the other inherently decreases as the small-division zeros recur at the indicating means, said extended-scale indicator further including means for obscuring said other of said two sequences of large-division numbers when said members are displaced in said given direction from said starting position.
6. An extended-scale indicator in accordance with claim 1 , wherein said indicating means includes an serical indicia and at least one sequence of large-division numerical indicia, a plurality of rollers in said enclosure, each of said rollers forming a guide for both of said belts, said rollers forming a labyrinth-path for both of said belts, and guide means forming an extendedlength guide path for the longer of said two belts at a definite location in said labyrinth path for taking up the slack in said longer belt and avoiding enforced sliding of one of the belts relative to the other along said labyrinth path, the difference in length between the belts being related to the spacing between the largedivision numerical indicia to cause step-wise change thereof at the viewing region.
7. A metric indicator for a machine tool including a lead screw having an indicator shaft for a cyclic inchsystem indicator, said metric indicator having means defining a viewing region, a sprocket for said indicator shaft, a small-scale-division cyclic continuous tape and a large-scale-division continuous tape having respective portions supported by the sprocket in the viewing region and having regular numerical sequences, the continuous tapes being of different lengths so that precession of the large-scale-division tape relative to the small-scale-division tape occurs in the course of successive cycles of the small-scale-division tape past the viewing region and so that successive readings of the large-scale-division tape are brought into the view-
ing region successively with successive zeros of the small-scalegdivision tape, the ratio of the circumference of the sprocket to the circumference of the small-scale-division tape being equal to 1.27 multiplied by the advance produced by the lead screw in inches per rotation of the indicator shaft, multiplied by a small integer greater than zero.
8. A metric indicator for a machine tool including a lead screw having an indicator shaft for a cyclic inchsystem indicator, said metric indicator having means defining a viewing region, a unitary dial and sprocket for said indicator shaft, said dial having uniform regularly distributed scale divisions, and a continuous indicator tape on said sprocket, the ratio of the circumference of the sprocket to the circumference of the small-scale-division tape being equal to 1.27 multiplied by the advance produced by the lead screw in inches per rotation of the indicator shaft, multiplied by a small integer greater than zero, said indicator tape having decimal-series numerals distributed thereon for alignment with only certain of said scale divisions and the scale divisions other than said certain divisions forming intervening subdivisions.
9. A metric indicator in accordance with claim 11, wherein said indicator tape has a gating pattern distinguishing said certain scale divisions from at least the scale divisions at opposite sides of each of said certain scale divisions.
10. A multiple indicator for a work-table lead screw of a machine tool having a lead-screw indicator shaft,
said multiple indicator including plural direct-reading indicators, each said indicator having an enclosure, a sprocket, and dual indicator tapes in said enclosure cogged to said sprocket and of different loop lengths, 5 all arranged to provide continuous direct readings over a range covering many sprocket rotations, means for securing the enclosures of said plural indicators to each other and to a stationary part of the machine tool, and means for releasably locking said sprockets to the irdicator shaft for rotation therewith and with each other and further adapting the sprockets to individual rotational adjustment relative to said shaft when the locking means is released.
11. A multiple indicator in accordance with claim 13 wherein said indicator shaft includes an individual modular shaft extension for each indicator in excess of one.
12. A multiple indicator in accordance with claim 13, wherein an individual locking means is provided for each indicator so that individual adjustment of each indicator is feasible while the other indicators are locked to retain the adjustment thereof.
13. A multiple indicator in accordance with claim 13, including three duplicate extended-scale indicators one of which provides direct readings of the work-table position while the other two provide "plus" and "minus" off-set readings corresponding to said direct readings modified to allow for cutter off-set.
