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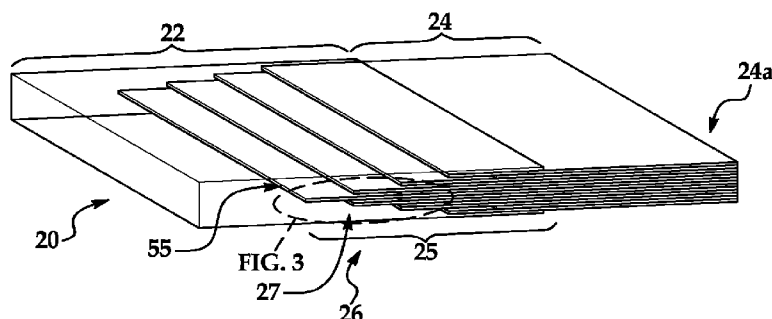
**Declarations under Rule 4.17:**

- as to the identity of the inventor (Rule 4.17(i))
- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii))
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(54) Title: COMPOSITE STRUCTURES HAVING COMPOSITE-TO-METAL JOINTS AND METHOD FOR MAKING THE SAME



**FIG. 2**

(57) Abstract: A composite structure comprises stacked sets of laminated fiber reinforced resin plies and metal sheets. Edges of the resin plies and metal sheets are interleaved to form a composite-to-metal joint connecting the resin plies with the metal sheets.



COMPOSITE STRUCTURES HAVING COMPOSITE-TO-METAL  
JOINTS AND METHOD FOR MAKING THE SAME

TECHNICAL FIELD

5           This disclosure generally relates to composite structures, especially to fiber reinforced resin laminates, and deals more particularly with a hybrid composite having a composite-to-metal joint.

BACKGROUND

10           Bonding techniques are often used to assemble composite structures. In applications where the composite structure also requires fasteners, the local thickness or gauge of the structure surrounding the fastener may need to be increased in order to withstand loads transmitted through the fastener joint. As the local thickness of the structure increases, the fastener may need to be lengthened, thereby adding weight to the structure. Additionally, the  
15   increased local thickness of the structure may increase the eccentricity of the load path across the fastener joint, which may place undesired bending loads on the fastener.

          One solution to the problems mentioned above consists of attaching metal fittings to the composite structure in the area of the fasteners. These metal fittings may be formed of  
20   titanium or similar metals that may not substantially chemically react with carbon fiber reinforced composites in which they are in contact. Titanium fittings, however may be relatively expensive, particularly when it is necessary to form them into complex shapes.

          Accordingly, there is a need for a composite resin-to-metal joint that may be used to  
25   connect substantially all metal fittings with substantially all composite resin structures, which

is relatively inexpensive and easy to manufacture, and which may withstand loads transferred around fastener connection points. There is also a need for a composite resin-to-metal joint that substantially avoids chemical reactions between the all metal fitting and the all composite resin structure.

5

## SUMMARY

The disclosed embodiments provide a hybrid-type composite structure that includes a fiber reinforced resin composite-to-metal joint that may be used to connect a substantially all-metal fitting with a substantially all composite resin structure. The joint provides a transition  
10 between the composite and metallic structures that is suitable for use in higher performance applications, such as aerospace vehicles. This transition from a substantially all composite to a substantially all metal material may reduce or eliminate the possibility of corrosion and/or problems stemming from eccentricity. During lay-up of the composite structure, sheets of metal are substituted for a number of composite plies, and the transition from composite plies  
15 to metal sheets occurs at staggered locations so as to provide adequate load transfer from the composite portion to the metal portion. The staggered transition results in an interleaving between the composite plies and the metal sheets and creates multiple bond lines that may reduce the occurrence and/or propagation of cracks or disbonds in the joint. An adhesive placed between the metal sheets binds and unitizes the sheets into a nearly solid metal fitting.

20

According to one disclosed embodiment, a composite structure is provided, comprising a laminated stack of fiber reinforced resin plies and a stack of metal sheets. The metal sheets have edges that are interleaved with the edges of the fiber reinforced resin plies to form a composite-to-metal joint connecting the fiber reinforced resin plies with the metal  
25 sheets.

According to another embodiment, a hybrid resin-metal structure is provided comprising a composite resin portion, a metal portion, and a transition section between the resin and metal portions. The resin portion includes laminated plies of fiber reinforced resin, and the metal portion includes bonded sheets of metal. The transition section includes staggered overlaps between the laminated plies and the metal sheets.

According to another embodiment, a hybrid composite metal part is provided. The part comprises a layup of fiber reinforced composite material that is terminated at an interface location. At the interface location, a metal ply of the same thickness as the composite material continues to the metal edge of the part, and the layup is repeated with a composite to metal interface that is staggered toward the edge of the part from the prior interface location. A ply of structural adhesive is placed between the metal plies, with the next metal to composite interface staggered away from the part edge to produce a nested splice, and the staggered interface stacking produces nested tabs is continued to the full thickness of the part with none of the composite plies extending fully to the edge of the part.

According to still another embodiment, a method is provided of fabricating a composite structure. The method comprises forming a multi-ply composite lay-up having a composite portion and a metal portion, and forming a composite-to-metal joint between the composite portion and the metal portion. The method further includes compacting and curing the layup.

According to a further embodiment, a method is provided to produce a hybrid metal part. The method comprises laying at least one fiber reinforced composite ply that is

terminated at a interface location, and laying an adjacent metal ply where the metal ply is of substantially the same thickness as the adjacent fiber reinforced composite ply. The steps of laying composite plies and adjacent metal plies are repeated to form a composite to metal interface that is staggered toward said an edge of the part from the prior interface location.

- 5 The method further comprises laying a ply of structural adhesive between the metal plies, and repeating the composite and metal ply layup where the next metal to composite interface is staggered away from the part edge to produce a nested splice.

9. A hybrid composite resin-metal structure, comprising:

a composite resin portion including laminated plies of fiber reinforced resin;

10 a metal portion including bonded sheets of metal; and

a transition section between the composite resin portion and the metal portion, the transition section including staggered overlaps between the laminated plies and the metal sheets.

15 10. The hybrid composite resin-metal structure of claim 9, wherein:

the laminated plies and the metal sheets are arranged in layers, and

each of the layers includes one of the metal sheets and a plurality of the fiber reinforced resin plies in substantially edge-to-edge abutment.

20 11. The hybrid composite resin-metal structure of claim 10, wherein the thickness of the plies in each of the layers is substantially equal to the thickness of the metal sheet in the layer.

20. A method to produce a hybrid metal part comprising;

laying at least one fiber reinforced composite ply that is terminated at a interface location;

laying an adjacent metal ply where the metal ply is of the same thickness as the adjacent fiber reinforced composite ply;

- 5       repeating the steps of laying composite plies and adjacent metal plies to form a composite to metal interface that is staggered toward said an edge of the part from the prior interface location;

laying a ply of structural adhesive between the metal plies; and

- 10       repeating the composite and metal ply layup where the next metal to composite interface is staggered away from the part edge to produce a nested splice.

21.     The method of claim 20, further comprising:

- continuing the staggered interface stacking of the composite and metal plies to produces nested tabs to the full thickness of the part with none of composite plies extending  
15     fully to the edge of the part.

22.     The method of claim 21, further comprising:

- vacuum bag processing the part to remove air voids in the layup; and  
curing the laid up part.

20

23.     A hybrid composite resin-metal aircraft structure, comprising:

- a plurality of laminated layers forming a fiber reinforced, all composite portion, an all metal portion and a hybrid composite-metal finger joint connecting the composite portion with the metal portion,

each of the layers including a plurality of plies of composite resin and a titanium metal sheet, wherein the plies and the metal sheet are arranged in edge-to-edge abutment with each other forming a composite-to-metal transition point in the layer, and wherein the transition points in the layers are staggered relative to each other to form the finger joint; and

5 a layer of adhesive between the metal sheets for unitizing the metal sheets, and

wherein the thickness of the plies in each of the layers is substantially equal to combined thickness of one of the sheets and layer of the adhesive.

24. A method of making a hybrid composite resin-metal aircraft structure, comprising:

10 forming a lay-up including a fiber reinforced, all composite portion, an all metal portion and a hybrid composite-metal finger joint connecting the composite portion with the metal portion, forming the layup including laying up a plurality of layers wherein each of the layers is formed by placing a plurality of composite resin plies in edge-to-edge abutment with a titanium metal sheet forming a composite-to-metal transition point in the layer;

15 placing a layer of adhesive n=between the metal sheets to unitize the metal portion;

forming the joint between the composite portion and the metal portion by staggering the transition points in the layers relative to each other;

compacting the layup; and

curing the layup.

20

12. The hybrid composite resin-metal structure of claim 9, wherein the staggered overlaps form a composite-to-metal finger joint between the composite resin portion and the metal portion.

13. The hybrid composite resin-metal structure of claim 9, further comprising a layer of adhesive between each of the metal sheets for bonding the sheets together and unitizing the metal portion.

14. The hybrid composite resin-metal structure of claim 9, wherein each of the metal sheets is a titanium alloy.

15. A hybrid composite metal part, comprising:

a layup of fiber reinforced composite material that is terminated at an interface location, where a metal ply of the same thickness as the composite material continues to the metal edge of the part, and the layup is repeated with a composite to metal interface that is staggered toward the edge of the part from the prior interface location and includes a ply of structural adhesive between the metal plies, with the next metal to composite interface staggered away from the part edge to produce a nested splice, and the staggered interface stacking produces nested tabs is continued to the full thickness of the part with none of the composite plies extending fully to the edge of the part.

#### BRIEF DESCRIPTION OF THE ILLUSTRATIONS

FIG. 1 is an illustration of a sectional view of a composite structure having a composite-to-metal joint.

FIG. 2 is an illustration of a perspective view of the composite structure including the composite-to-metal joint.

FIG. 3 is an illustration of a perspective view of the area designated as FIG. 3 in FIG. 2.



FIG. 4 is an illustration of a cross sectional view of the joint, better showing interleaving between composite plies and the metal sheets.

FIG. 5 is an illustration of a cross sectional view of two separated layers of the joint shown in FIG. 4, also showing the application of a film adhesive on the metal sheets.

FIG. 6 is an illustration of an enlarged, cross sectional view of a portion of the joint formed by the two layers shown in FIG. 5.

FIG. 7 is an illustration of a broad flow diagram of a method of making a composite structure having the composite joint shown in FIGS. 2-4.

FIG. 8 is an illustration of a flow diagram showing additional details of the method  
15 shown in FIG. 7.

FIG. 9 is a flow diagram of another method of making a composite structure having the composite joint shown in FIGS. 2-4.

FIG. 10 is an illustration of a flow diagram of aircraft production and service methodology.

FIG. 11 is an illustration of a block diagram of an aircraft.

## 25 DETAILED DESCRIPTION

Referring first to FIG. 1, a hybrid composite structure 20 includes a composite resin portion 22 joined to a metal portion 24 by a transition section 25 that includes a composite-to-

metal joint 26. In the illustrated example, the composite structure 20 is a substantially flat composite sheet, however depending upon the application, the structure 20 may have one or more curves, contours or other geometric features. For example, composite structure 20 may comprise an inner and/or outer contoured skin of an aircraft (not shown) which is secured to a frame 28 portion of the aircraft by means of a lap joint 30 and fasteners 32 which pass through the skin 20 into the frame 28.

The frame 28 may comprise a composite, a metal or other rigid material, and the metal portion 24 of the structure 20 may serve as a rigid metal fitting 24 that is suited to transfer a range of loads and types of loadings between the frame 28 and the composite portion 20. As will be discussed below in more detail, the metal portion 24 may comprise any of various metals such as, without limitation, titanium that is substantially non-reactive to and compatible with the composite portion 20 and the structure 28. In one practical embodiment for example, and without limitation, the composite resin portion 22 may comprise a carbon fiber reinforced epoxy, the metal portion 24 may comprise a titanium alloy, and the frame 28 may comprise an aluminum alloy or a composite. The transition section 25 and the joint 26 are strong enough to carry the typical range and types of loads between the composite resin portion 22 and the metal portion 24, including but not limited to tension, bending, torsion and shear loads. Although the illustrated transition section 25 and joint 26 are formed between an all composite resin portion 22 and the all metal portion 24, it may be possible to employ them to join two differing composite structures (not shown) or two differing metal structures (not shown).

Referring to FIGS. 1-4, a layup of composite material plies 35 is terminated at a interface location 39 referred to later herein as a transition point 39, where a metal sheet or

ply 37 of the substantially the same thickness as the composite material plies 35 continues to the metal edge 24a of the metal portion 24, and the layup is repeated with a composite-to-metal interface 39 that is staggered toward the metal edge 24a from the prior interface location 39 and includes a ply of structural metal adhesive 45 (see FIGS. 5 and 6) between the metal plies 37, with the next metal-to-composite interface 39 staggered away from the part edge 24a to produce a nested splice 27. This staggered interface stacking, which produces nested tabs 29 (see FIG. 3), is continued to the full thickness of the hybrid composite structure 20 with none of the composite plies 35 extending fully to the metal edge 24a of the all metal portion 24

Referring now also to FIGS. 2-4, the composite portion 22 of the structure 20 comprises a laminated stack 34 of fiber reinforced resin plies 35, and the metal portion 24 of the structure 20 comprises a stack 36 of metal sheets or plies 37 that are bonded together to form a substantially unitized metal structure. As shown in FIGS. 5 and 6, the composite plies 35 and the metal sheets 37 are arranged in layers 38. Each of the layers 38 comprises one or more of the composite plies 35 in substantially edge-to-edge abutment with one of the metal sheets 37. Thus, each of the layers 38 transitions at a point 39 from a composite i.e. composite resin plies 35, to a metal, i.e. metal sheet 37.

The transition points 39 are staggered relative to each other according to a predetermined lay-up schedule such that the plies 35 and the metal sheets 37 overlap each other in the transition section 25 (FIG. 1). Staggering of the transition points 39 creates multiple bond lines that may reduce the occurrence and/or propagation of cracks or disbonds in the joint 26. The staggering of the transition points 39 also results in a form of interleaving of the composite plies 35 and the metal sheets 37 within the joint 26 which forms a nested

splice 27 between the all composite portion 22 and the all metal portion 24. This nested splice 27 may also be referred to as a finger bond 26, a finger joint 26 or a multiple step lap joint 26. The adjacent ones of the transition points 39 are spaced from each other in the in-plane direction of the structure 20 so as to achieve a bonded joint 26 that exhibits optimum performance characteristics, including strength and resistance to disbonds and propagation of inconsistencies such as cracks. In the illustrated example, the nested splice 27 forming the joint 26 is a form of a double finger joint 26 in which the transition points 39 are staggered in opposite directions from a generally central point 55 of maximum overlap. However, other joint configurations are possible including but not limited to a single finger joint in which the multiple transition points 39 are staggered in a single direction.

The composite plies 35 may comprise a fiber reinforced resin, such as without limitation, carbon fiber epoxy, which may be in the form of unidirectional prepreg tape or fabric. Other fiber reinforcements are possible, including glass fibers, and the use of non-prepreg materials may be possible. The composite plies 35 may have predetermined fiber orientations and are laid up according to a predefined ply schedule to meet desired performance specifications. As previously mentioned, the bonded sheets 37 may comprise a metal such as titanium that is suitable for the intended application. In the illustrated example, the stack 36 of metal sheets 37 has a total thickness  $t_1$  which is generally substantially equal to the thickness  $t_2$  of the laminated stack 34 of plies 35. In the illustrated example however,  $t_2$  is slightly greater than  $t_1$  by a factor of the thickness of several overwrap plies 43 on opposite sides of the stack 37.

FIGS. 5 and 6 illustrate details of two adjoining layers 38 of the joint 26 shown in FIGS. 2-4. In this example, each layer 38 comprises four plies 35 having a collective total

thickness  $T_1$ . The individual metal sheets 37 of the adjacent layers 38 are bonded together by means of a layer of structural adhesive 45, which may comprise a commercial film adhesive or other forms of a suitable adhesive that is placed between the metal sheets 36 during the lay-up process.

5

The combined thickness of each metal sheet 37 and one layer of adhesive 45 represented as  $T_2$  in FIG. 5 is substantially equal to the thickness  $T_1$  of the composite plies 35 in the layer 38. Although not shown in the Figures, a thin film of adhesive may be placed between the plies 35 to increase the interlaminar bond strength. In one practical embodiment, titanium alloy metal sheets 37 may be used which each have a thickness of approximately 0.0025 inches, the film adhesive 45 may be approximately 0.005 inches thick, and four composite carbon fiber epoxy plies 35 may be used in each layer 38 having a collective total thickness of about 0.30 inches. Depending on the application, the use of metals other than titanium may be possible. The distance between adjacent transition points 39, and thus the length of the overlap between the layers 38, as well as the thickness and number of composite plies 35 and the thickness of the metal sheets 37 will depend on the requirements of the particular application, including the type and magnitude of the loads that are to be transmitted through the joint 26, and possibly other performance specifications.

20 The differing layers 38 of the joint 26 between the two differing materials of the composite and metal portions 22, 24 respectively (FIG. 1), render the structure 20 well suited to nondestructive evaluations of bond quality using embedded or mounted sensors (not shown). Ultrasonic structural waves (not shown) may be introduced into the structure 20 at the edge of the metal portion 24, at the composite portion 22 or in the transition section 25.

25 These ultrasonic waves travel through what amounts to a waveguide formed by the metal 37

sheets and the interfaces (not shown) between the composite plies 35 and the metal sheets 37. MEMS-based (microelectromechanical) sensors, thin piezo-electric sensors (not shown) or other transducers placed in the structure 20 may be used to receive the ultrasonic structural waves for purposes on analyzing the condition of the bondlines in the joint 26.

5

Referring now to FIG. 7, one method of making the composite structure 20 comprises forming a multi-layer composite lay-up as shown at 65. Forming the lay-up includes laying up a composite resin portion 22 at step 67, and laying up a metal portion 24 at 69. The step 65 of forming the layup further includes forming a composite-to-metal joint between the  
10 composite resin portion and the metal portion of the lay-up, shown at 71.

FIG. 8 illustrates additional details of the method shown in FIG. 7. Beginning at step 40, individual metal sheets 37 are trimmed to a desired size and/or shape. Next at 42, the surfaces of the metal sheets 37 are prepared by suitable processes that may include cleaning  
15 the sheets 37 with a solvent, drying them, etc. then at 44, the lay-up is assembled by laying up the metal sheets 36 and the composite plies 35 in a sequence that is determined by a predefined ply schedule (not shown) which includes a predetermined staggering of the transition points 39 between the plies 35 and the metal sheet 36 in each layer 38.

20 During the lay-up process, the metal sheets 37 are sequenced like plies into the lay-up, much like composite plies are sequenced into a lay-up in a conventional lay-up process. As shown at step 46, adhesive may be introduced between the metal sheets 37 in order to bond them together into a unitized metal structure. Similarly, although not shown in FIG. 8, a bonding adhesive may be introduced between the individual composite plies 35 in order to  
25 increase the bond strength between these plies 35. Next, at 48, the lay-up may be compacted

using any of several known compaction techniques, such as vacuum bagging following which the lay-up is cured at step 50 using autoclave or out-of-autoclave curing processes. At step 52, the cured composite structure 20 may be trimmed and/or inspected, as necessary.

5           FIG. 9 illustrates still another embodiment of a method of making a hybrid composite part 20. The method begins at step 73 with laying at least one composite ply 35 that is terminated at an interface location 39 on a suitable layup tool (not shown). At 75, an adjacent metal ply 37 is laid up which is substantially the same thickness as the adjacent composite material ply 35. As shown at 77, the layup process is repeated with a composite-to-metal  
10   interface 39 that is staggered toward the metal edge 24a of the part 20 from the prior interface location 39. At 79, a ply 45 of structural adhesive is laid between the metal plies 37. Steps 73-79 are repeated successively to produce a nested splice 27 and a staggered interface stacking forming nested tabs 29 to the full thickness of the hybrid part 20, with none composite plies 35 extending fully to the metal edge 24a of the part 20. Although not shown  
15   in FIG. 9, the completed layup is vacuum bagged processed to remove voids, and is subsequently cured using any suitable curing method.

Embodiments of the disclosure may find use in a variety of potential applications, particularly in the transportation industry, including for example, aerospace, marine and  
20   automotive applications. Thus, referring now to FIGS. 10 and 11, embodiments of the disclosure may be used in the context of an aircraft manufacturing and service method 60 as shown in FIG. 10 and an aircraft 62 as shown in FIG. 11. Aircraft applications of the disclosed embodiments may include, for example, a wide variety of structural composite parts and components, especially those requiring the use of fasteners during the assembly  
25   process. During pre-production, exemplary method 60 may include specification and design

64 of the aircraft 62 and material procurement 66. During production, component and subassembly manufacturing 68 and system integration 70 of the aircraft 62 takes place. Thereafter, the aircraft 62 may go through certification and delivery 72 in order to be placed in service 74. While in service by a customer, the aircraft 62 is scheduled for routine  
5 maintenance and service 76 (which may also include modification, reconfiguration, refurbishment, and so on).

Each of the processes of method 60 may be performed or carried out by a system integrator, a third party, and/or an operator (e.g., a customer). For the purposes of this  
10 description, a system integrator may include without limitation any number of aircraft manufacturers and major-system subcontractors; a third party may include without limitation any number of vendors, subcontractors, and suppliers; and an operator may be an airline, leasing company, military entity, service organization, and so on.

15 As shown in FIG. 11, the aircraft 62 produced by exemplary method 60 may include an airframe 78 with a plurality of systems 80 and an interior 82. Examples of high-level systems 82 include one or more of a propulsion system 84, an electrical system 86, a hydraulic system 88, and an environmental system 90. Any number of other systems may be included. The disclosed method may be employed to fabricate parts, structures and  
20 components used in the airframe 78 or in the interior 82. Although an aerospace example is shown, the principles of the disclosure may be applied to other industries, such as the marine and automotive industries.

Systems and methods embodied herein may be employed during any one or more of  
25 the stages of the production and service method 60. For example, parts, structures and



components corresponding to production process 68 may be fabricated or manufactured in a manner similar to parts, structures and components produced while the aircraft 62 is in service. Also, one or more apparatus embodiments, method embodiments, or a combination thereof may be utilized during the production stages 68 and 70, for example, by substantially  
5 expediting assembly of or reducing the cost of an aircraft 62. Similarly, one or more of apparatus embodiments, method embodiments, or a combination thereof may be utilized while the aircraft 62 is in service, for example and without limitation, to maintenance and service 76.

10           Although the embodiments of this disclosure have been described with respect to certain exemplary embodiments, it is to be understood that the specific embodiments are for purposes of illustration and not limitation, as other variations will occur to those of skill in the art.

## CLAIMS

What is claimed:

1. A composite structure, comprising:

a laminated stack of fiber reinforced resin plies; and

5 a stack of metal sheets having edges interleaved with edges of the fiber reinforced resin plies to form a composite-to-metal joint connecting the fiber reinforced resin plies with the metal sheets.

2. The composite structure of claim 1, wherein:

10 the stacks of fiber reinforced resin plies and metal sheets are arranged in layers, wherein each of the layers includes a metal sheet and at least one of the fiber reinforced resin plies.

3. The composite structure of claim 2, wherein the thickness of the fiber reinforced resin  
15 plies in each of the layers is generally equal to the thickness of the metal sheet in the layer.

4. The composite structure of claim 2, wherein:

the fiber reinforced resin plies and the metal sheet in each of the layers having substantially abutting edges forming a resin-to-metal transition point.

20

5. The composite structure of claim 4, wherein the transition points of the layers are staggered relative to each other.

6. The composite structure of claim 2, wherein the layers form a fiber reinforced resin-  
25 to-composite finger joint between the stack of resin plies and the stack of metal sheets.

7. The composite structure of claim 1, further comprising:

a layer of adhesive between adjacent ones of the metal sheet for bonding the sheets together.

5

8. The composite structure of claim 1, wherein:

the metal sheets are a titanium alloy, and

the fiber reinforcement of the plies includes carbon.

10 9. A method of fabricating a composite structure, comprising:

forming a multi-layer composite lay-up having a fiber reinforced composite resin portion and a metal portion, including forming a composite-to-metal joint between the composite resin portion and the metal portion of the lay-up.

15 10. The method of claim 9, wherein forming the lay-up includes forming each of the layers by placing at least one fiber reinforced composite resin ply and one metal sheet in substantially edge-to-edge abutment with each other to form a transition point between the fiber reinforced composite resin and the metal in the layer.

20 11. The method of claim 10, wherein forming the lay-up includes staggering the transition points in the layers relative to each other.

12. The method of claim 10, further comprising:

unitizing the metal portion by placing a layer of adhesive between the metal sheets.

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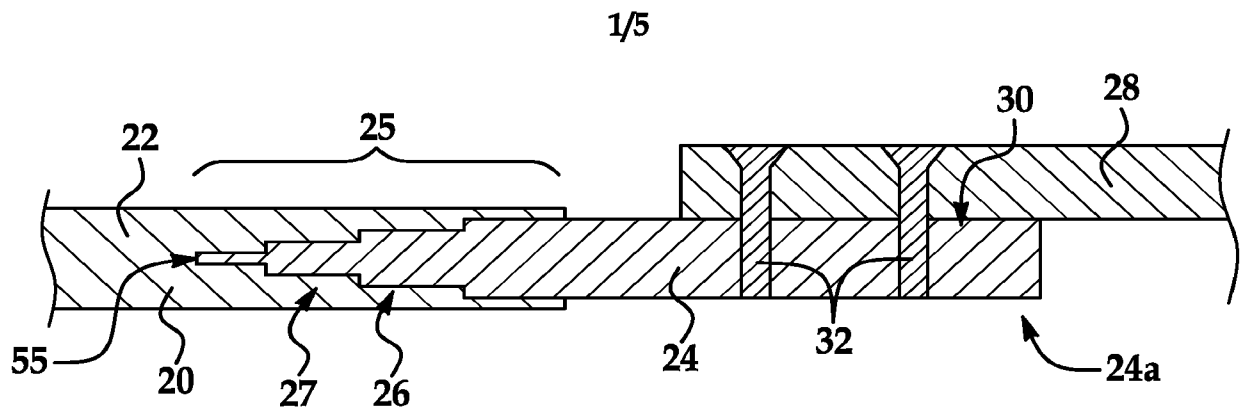


FIG. 1

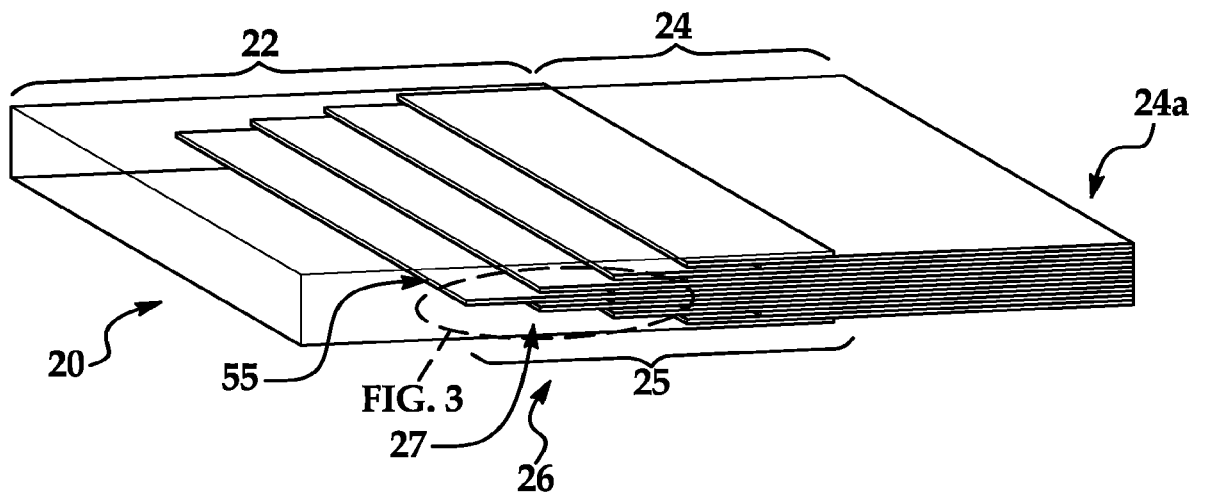


FIG. 2

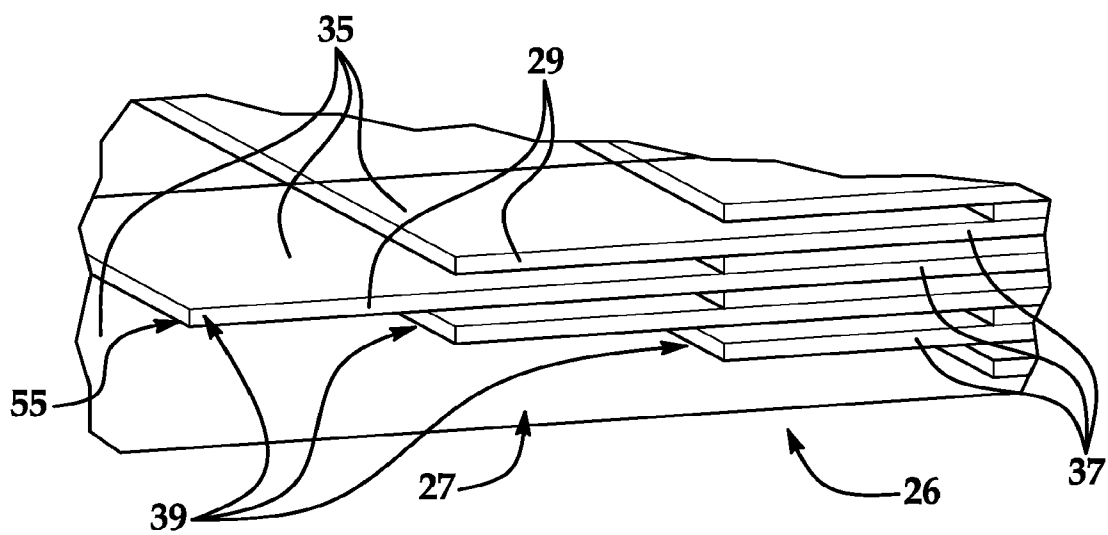
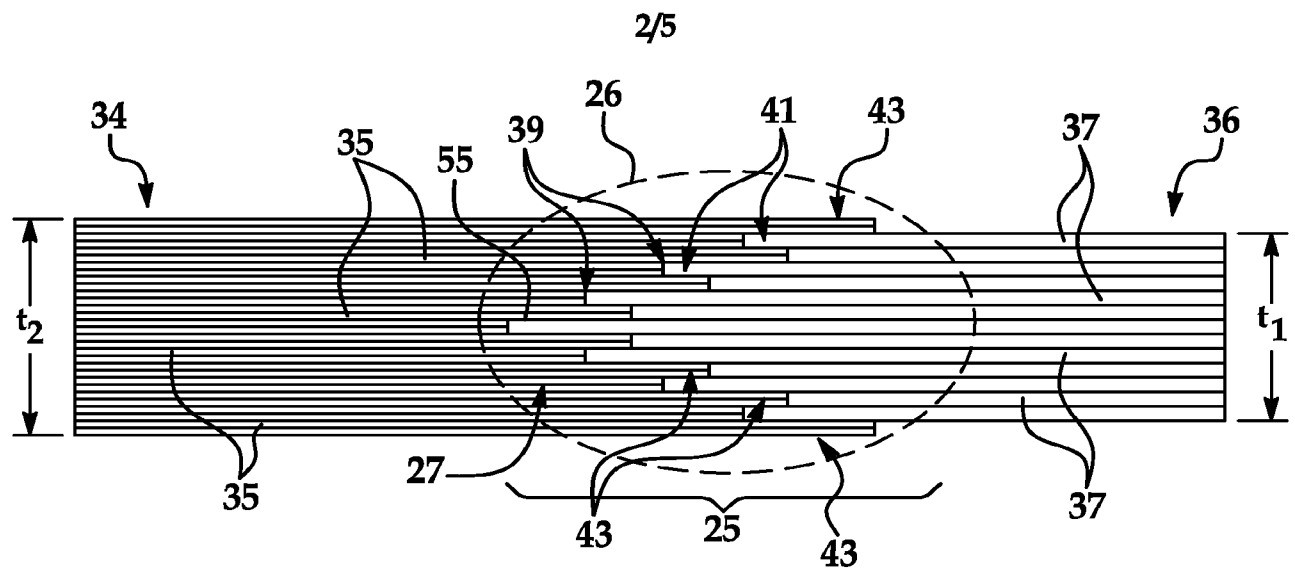
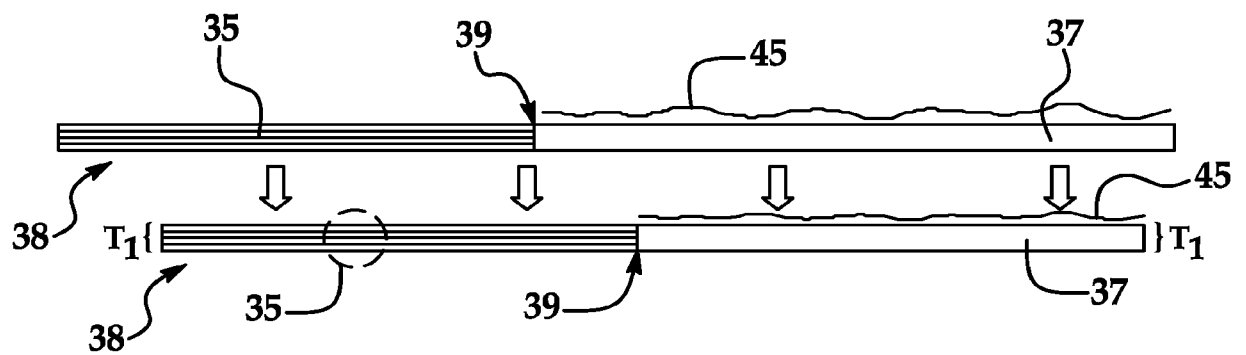


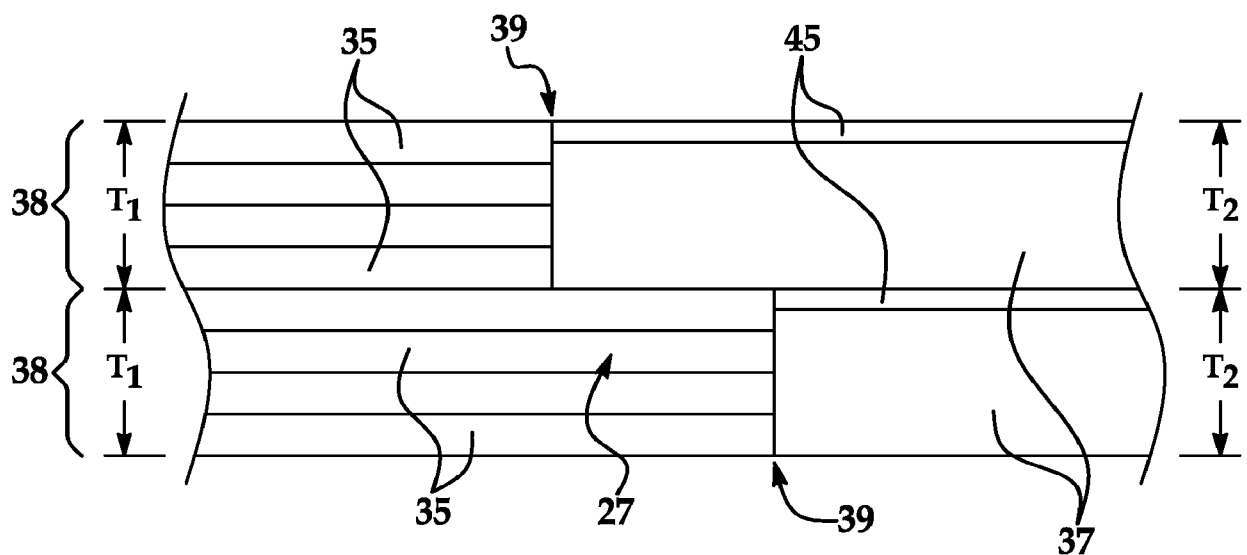
FIG. 3



**FIG. 4**



**FIG. 5**



**FIG. 6**

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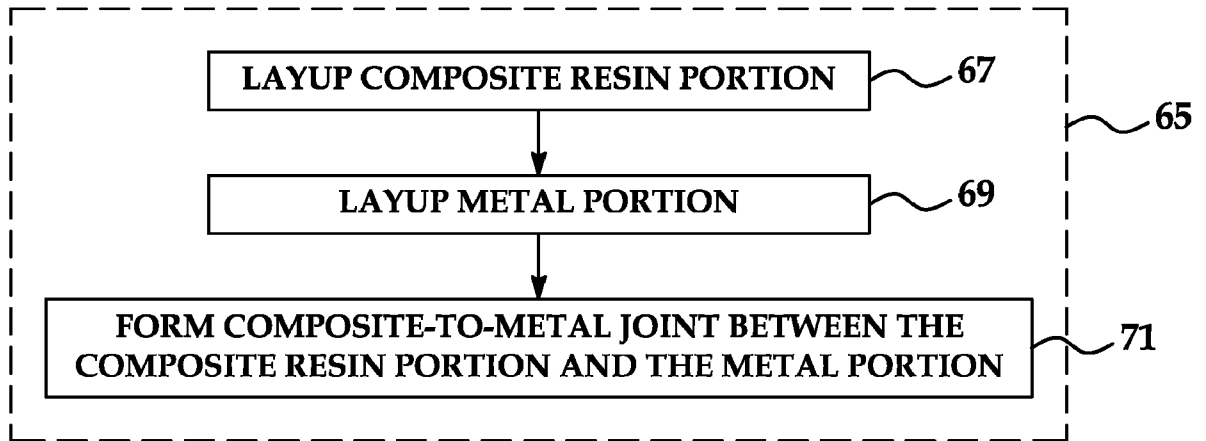


FIG. 7

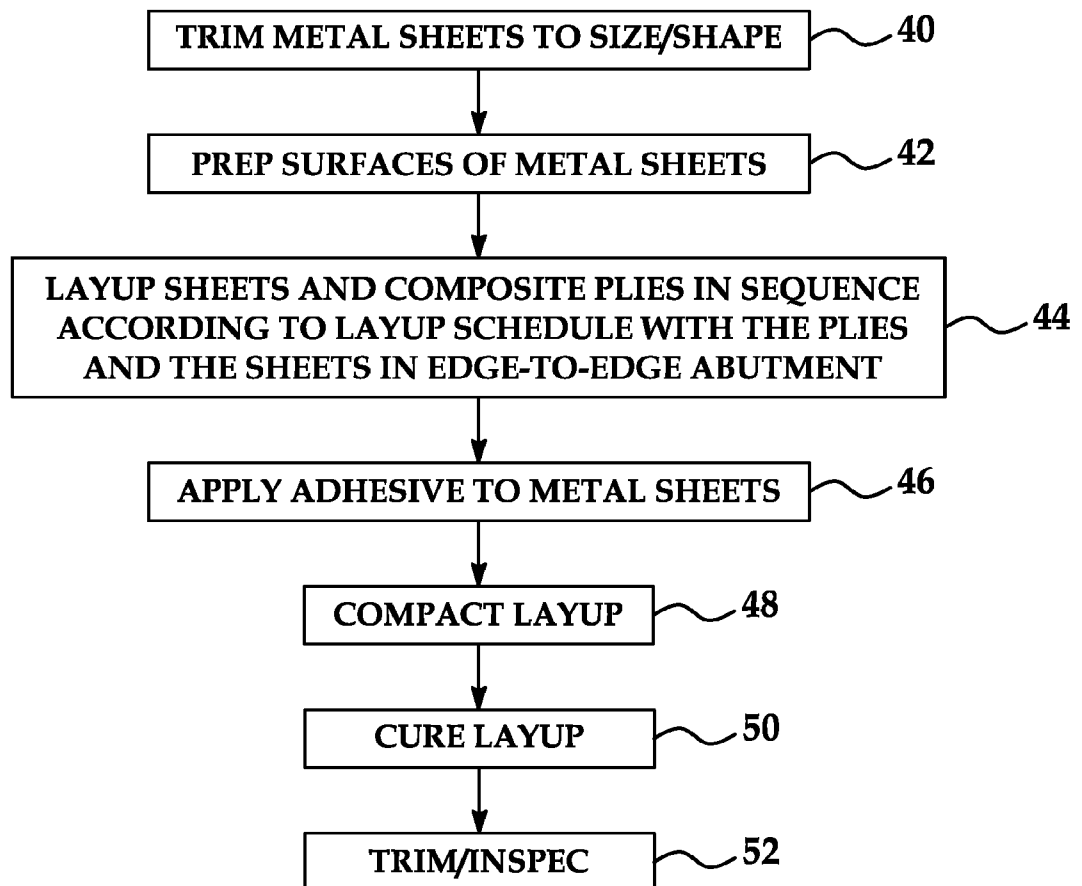


FIG. 8

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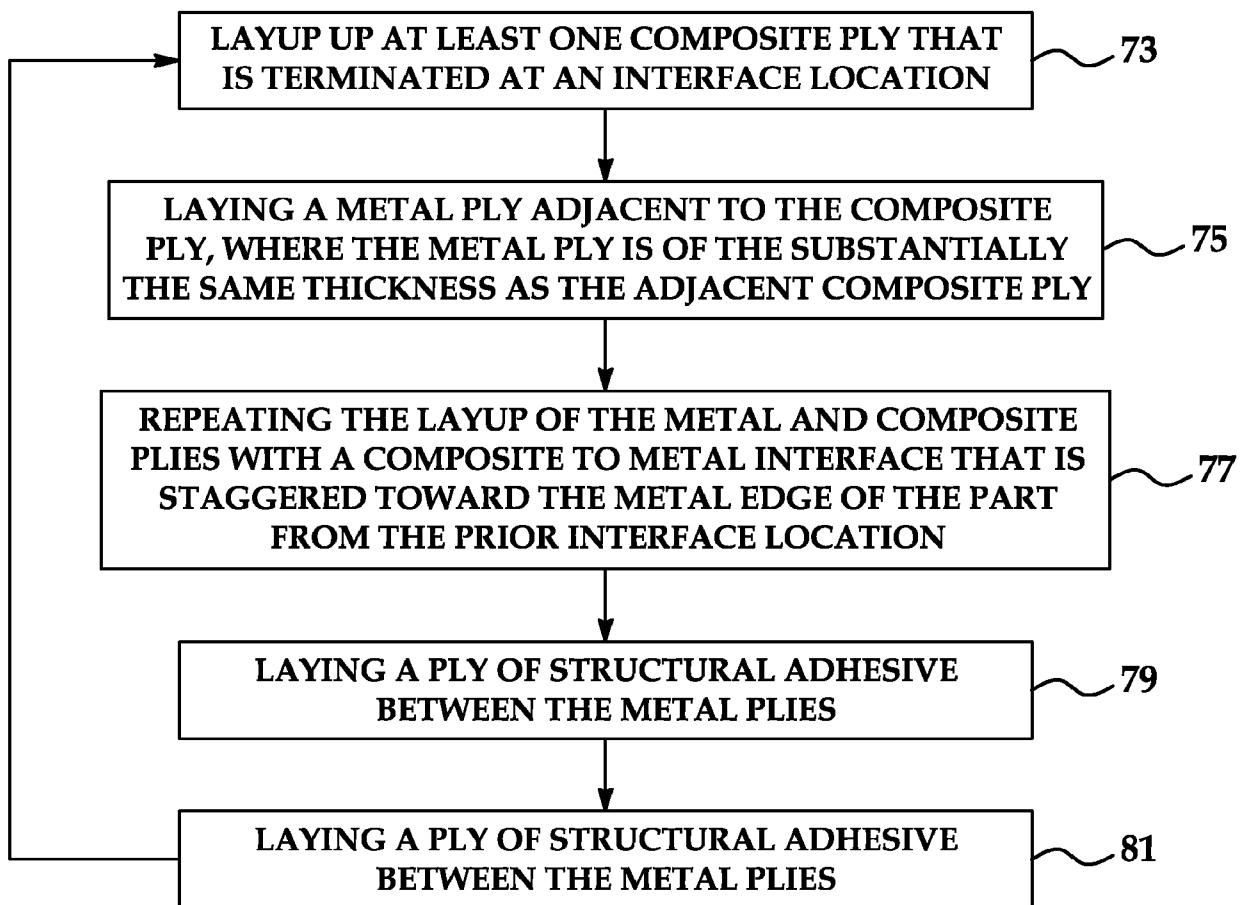


FIG. 9

5/5

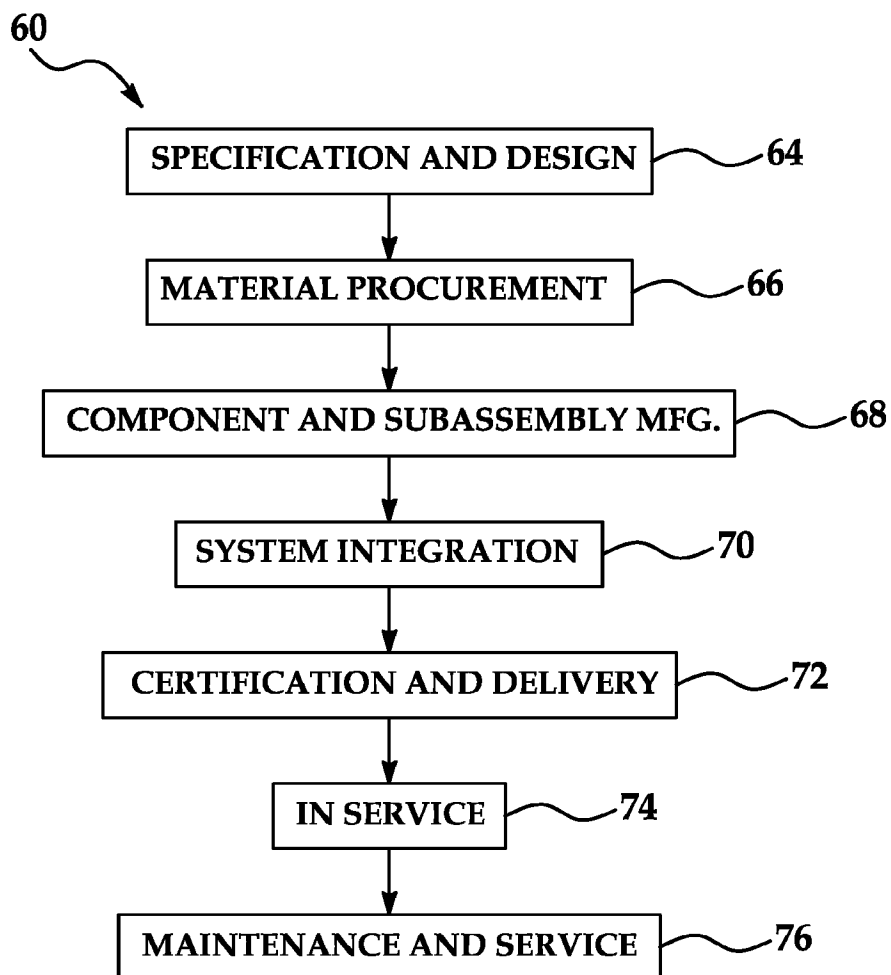


FIG. 10

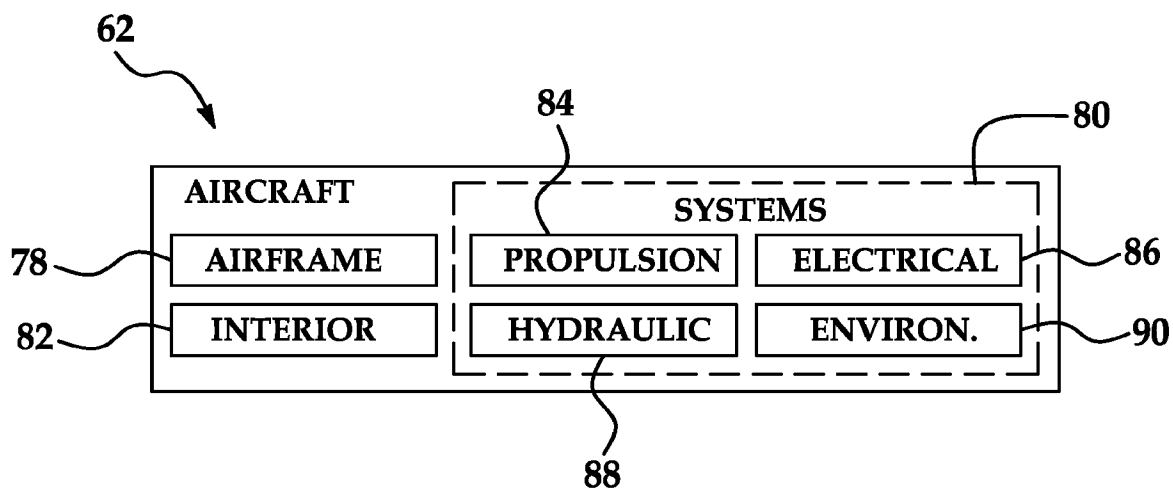


FIG. 11



## INTERNATIONAL SEARCH REPORT

International application No  
PCT/US2011/041519

A. CLASSIFICATION OF SUBJECT MATTER  
INV. B32B3/18 B32B15/08 B64C1/12  
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
B32B B64C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

| Category* | Citation of document, with indication, where appropriate, of the relevant passages                                                                                                                                                                                                                                                         | Relevant to claim No. |
|-----------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|
| X         | WO 00/56541 A1 (DLR EV [DE]; KOLESNIKOV BORIS [DE]; WILMES HOLGER [DE]; HERRMANN AXEL) 28 September 2000 (2000-09-28)<br>the whole document<br>page 2, line 6 - page 3, line 17; figures                                                                                                                                                   | 1-12                  |
| X         | -----<br>KOLESNIKOV ET AL: "CFRP/titanium hybrid material for improving composite bolted joints",<br>COMPOSITE STRUCTURES, ELSEVIER SCIENCE LTD, GB,<br>vol. 83, no. 4,<br>8 February 2008 (2008-02-08), pages<br>368-380, XP022473355,<br>ISSN: 0263-8223, DOI:<br>10.1016/J.COMPSTRUCT.2007.05.010<br>the whole document<br>-----<br>-/- | 1-12                  |



Further documents are listed in the continuation of Box C.



See patent family annex.

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"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

29 July 2011

Date of mailing of the international search report

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## INTERNATIONAL SEARCH REPORT

International application No

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C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

| Category* | Citation of document, with indication, where appropriate, of the relevant passages                                                                                                                                                                                                                                                                                                         | Relevant to claim No. |
|-----------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|
| X         | <p>FINK A ET AL: "Hybrid CFRP/titanium bolted joints: Performance assessment and application to a spacecraft payload adaptor",<br/>COMPOSITES SCIENCE AND TECHNOLOGY,<br/>ELSEVIER, UK,<br/>vol. 70, no. 2,<br/>1 February 2010 (2010-02-01), pages<br/>305-317, XP026824268,<br/>ISSN: 0266-3538<br/>[retrieved on 2009-11-06]<br/>the whole document<br/>abstract; figures<br/>-----</p> | 1-12                  |

## INTERNATIONAL SEARCH REPORT

### Information on patent family members

International application No

PCT/US2011/041519

| Patent document<br>cited in search report | Publication<br>date | Patent family<br>member(s) | Publication<br>date |            |
|-------------------------------------------|---------------------|----------------------------|---------------------|------------|
| WO 0056541                                | A1                  | 28-09-2000                 | DE 59901643 D1      | 11-07-2002 |
|                                           |                     |                            | EP 1082217 A1       | 14-03-2001 |
|                                           |                     |                            | ES 2178421 T3       | 16-12-2002 |
| -----                                     |                     |                            |                     |            |