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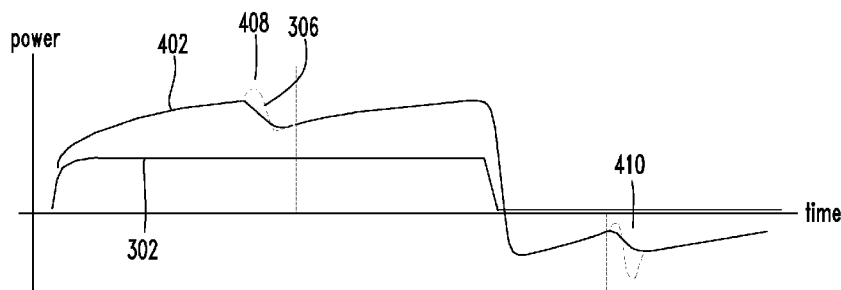


Fig. 4

(57) Abstract: A hybrid system includes a transmission control module, a power source, a transmission, and a drive train. The transmission control module partially operates the hybrid system and receives operating information from various components of the system, calculates power losses in the drive train, and calculates the driving torque needed to reach a target power profile determined from a driver's input.

SYSTEM AND METHOD FOR ENERGY RATE BALANCING IN HYBRID AUTOMATIC TRANSMISSIONS

CROSS REFERENCE TO RELATED APPLICATIONS

5 This application claims the benefit of U. S. Provisional Application No. 61/786,669 filed March 15, 2013, which is hereby incorporated by reference in its entirety.

BACKGROUND

10 The present disclosure generally relates to a hybrid vehicle drive train and, more particularly, to a method of adjusting the torque output of the drive train to match a target power profile.

 Over the past few years, there has been a growing concern over global climate change due to an increase in carbon dioxide levels as well as oil supply
15 shortages. As a result, automobile manufactures and consumers are developing a greater interest in motor vehicles having lower emissions and increased fuel efficiency. One viable option is a hybrid electric vehicle which allows the vehicle to be driven by electric motors, combustion engine, or a combination thereof.

 Transmissions in hybrid drive trains serve a number of functions by
20 transmitting and manipulating torque in order to provide torque to an output member. The driver, through actuation of the accelerator, brake pedal, and auxiliary braking selectors, commands the engine and/or electric motor to provide a desired power to the vehicle drive train. The transmission is expected to accurately implement the driver's command. As the transmission changes the gear
25 ratio, the driver's intent is not always achieved. Gear shifts within transmissions often result in disturbances in the drive train power output profile. The disturbances manifest as vibrations in the vehicle which are felt by the driver and passengers. Such disturbances can cause discomfort to the driver and passengers or otherwise create an undesirable driving experience.

30 Hybrid vehicle drive trains provide additional options for tailoring power output profiles based on a user's particular needs. For example, the power profile

can be tailored to provide many different functions such as optimizing fuel economy, maximizing acceleration, reducing or eliminating vibrations from gear shifts, or otherwise smoothing the drive train power profile for driver and passenger comfort. However, problems exist with transforming a drive train power
5 input to a desired drive train power.

Thus, there is a need for improvement in this field.

SUMMARY

The hybrid system described herein addresses several of the issues mentioned above as well as others. In one example, a method for operating a hybrid vehicle including a drive train having a transmission and a power source includes the actions of receiving a command input from a driver, determining a current state of the vehicle, determining loss parameters of the drive train, establishing a target drive train output power profile as a function of the command input, establishing power loss within the drive train as a function of the loss parameters, establishing a requisite input power needed to reach the target drive train output power profile as a function of the loss parameters and the target drive train output power profile, and supplying the requisite input power to the drive train. The loss parameters can include hydraulic power loss, kinetic power loss, and clutch power loss.

The hydraulic power loss can be calculated as a function of hydraulic loss parameters within the transmission. The hydraulic loss parameters can include the temperature of a hydraulic fluid, the pressure of the hydraulic fluid, and the flow rate of the hydraulic fluid.

The kinetic power loss can be calculated as a function of rotational inertia loss parameters within the drive train. The rotational inertia loss parameters include the rotational inertia of at least one body within the transmission, the rotational speed of the body, and the rotational acceleration of the body. The kinetic power loss (P_K) is calculated by the formula $P_K = \sum_1^N J_{i-N} \omega_{i-N} \dot{\omega}_{i-N}$ for $i=1-N$ bodies, where J is the rotational inertia of the body, ω is the rate of rotation of the body, and $\dot{\omega}$ is the rotational acceleration of the body.

The clutch power loss is calculated as a function of clutch loss parameters within the transmission. The clutch loss parameters include torque transmitted across the clutch during engagement between two clutch plates, and the rotational speed of each clutch plate. The clutch power loss (P_{clutch}) is calculated by the

formula $P_{clutch} = \sum_1^K T_{clutch_{m1-K}} |\omega_1 - \omega_2|_{m1-K}$ for $m=1-K$ bodies, where T_{clutch} is torque

transmitted across the clutch during engagement between two clutch plates and $|\omega_1 - \omega_2|$ is the absolute value of the difference between the rates of rotation of each clutch plate.

The power source can include an engine in the hybrid module. The requisite input power can be described as $P_{engine} + P_{hybrid}$ and is calculated by the

$$P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - \sum_{i=1}^N J_{i-N} \omega_{i-N} \alpha_{i-N} - \sum_{m=1}^K T_{clutch_{m-K}} |\omega_1 - \omega_2|_{m-K},$$

where P_{dl} is the target drive train output power profile, J is the rotational inertia of $i=1-N$ bodies in the transmission, ω is the rate of rotation of $i=1-N$ bodies in the transmission, α is the rotational acceleration of $i=1-N$ bodies in the transmission, T_{clutch} is the torque transmitted across $m=1-K$ clutches during engagement between two clutch plates, and $|\omega_1 - \omega_2|$ is the magnitude of the difference between the rates of rotation of two clutch plates in $m=1-K$ clutches. The calculations can be performed by a transmission/hybrid control module.

In one example, a method for operating a hybrid vehicle having a drive train including a transmission and a power source includes the actions of establishing a target drive train output power profile, establishing hydraulic power loss of the drive train as a function of hydraulic loss parameters within the transmission, establishing kinetic power loss of the drive train as a function of rotational inertia loss parameters within the drive train, establishing clutch power loss of the drive train as a function of clutch loss parameters within the transmission, establishing the drive train input power needed to reach the drive train output power profile as a function of the hydraulic loss parameters, the rotational inertia loss parameters, and the clutch loss parameters, and adjusting torque supplied by the power source to reach the target drive train output power profile.

The hydraulic loss parameters can include the temperature of a hydraulic fluid, the pressure of the hydraulic fluid, and the flow rate of the hydraulic fluid. The rotational inertia loss parameters can include the rotational inertia of a body within the transmission, the rotational speed of the body, and the rotational

acceleration of the body. The kinetic power loss (P_K) can be calculated by the

formula $P_K = \sum_{i=1}^N J_{i-1-N} \omega_{i-1-N} \alpha_{i-1-N}$ for $i=1-N$ bodies, where J is the rotational inertia of the body, ω is the rate of rotation of the body, and α is the rotational acceleration of the body.

5 The clutch loss parameters can include torque transmitted across the clutch during engagement between two clutch plates, and the rotational speed of each clutch plate. The clutch power loss (P_{clutch}) can be calculated by the formula

$$P_{clutch} = \sum_{m=1}^K T_{clutch_{m1-K}} |\omega_1 - \omega_2|_{m1-K} \text{ for } m=1-K \text{ bodies, where } T_{clutch} \text{ is the torque}$$

transmitted across the clutch during engagement between two clutch plates and
10 $|\omega_1 - \omega_2|$ is the absolute value of the difference between the rates of rotation of each clutch plate.

The power source can include an engine and the hybrid module. The torque supplied by the power source can be characterized as $P_{engine} + P_{hybrid}$ and is calculated by the formula

$$15 \quad P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - \sum_{i=1}^N J_{i-1-N} \omega_{i-1-N} \alpha_{i-1-N} - \sum_{m=1}^K T_{clutch_{m1-K}} |\omega_1 - \omega_2|_{m1-K}, \text{ where } P_{dl} \text{ is}$$

the target drive train output power profile, J is the rotational inertia of $i=1-N$ bodies in the transmission, ω is the rate of rotation of $i=1-N$ bodies in the transmission, α is the rotational acceleration of $i=1-N$ bodies in the transmission, T_{clutch} is torque transmitted across $m=1-K$ clutches during
20 engagement between two clutch plates, and $|\omega_1 - \omega_2|$ is the magnitude of the difference between the rates of rotation of two clutch plates in $m=1-K$ clutches.

The disclosure further includes an apparatus for performing any of the actions described herein. Further forms, objects, features, aspects, benefits, advantages, and embodiments of the present disclosure will become apparent from
25 a detailed description and drawings provided herewith.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 illustrates a diagrammatic view of one example of a hybrid system.

FIG. 2 illustrates a general diagram of an electrical communication system in the FIG. 1 hybrid system.

5 FIG. 3 illustrates a power output profile of a hybrid system without energy balancing.

FIG. 4 illustrates a power output profile of a hybrid system with energy balancing.

10 FIG. 5 illustrates a power output profile of a hybrid system with increased energy balancing.

FIG. 6 illustrates a flow chart showing of actions of a method to balance energy within a hybrid vehicle.

DESCRIPTION OF THE SELECTED EMBODIMENTS

For the purpose of promoting an understanding of the principles of the disclosure, reference will now be made to the embodiments illustrated in the drawings and specific language will be used to describe the same. It will
5 nevertheless be understood that no limitation of the scope of the disclosure is thereby intended. Any alterations and further modifications in the described embodiments, and any further applications of the principles of the disclosure as described herein are contemplated as would normally occur to one skilled in the art to which the disclosure relates. One embodiment of the disclosure is shown in
10 great detail, although it will be apparent to those skilled in the relevant art that some features that are not relevant to the present disclosure may not be shown for the sake of clarity.

The reference numerals in the following description have been organized to aid the reader in quickly identifying the drawings where various components are
15 first shown. In particular, the drawing in which an element first appears is typically indicated by the left-most digit(s) in the corresponding reference number. For example, an element identified by a “100” series reference numeral will first appear in FIG. 1, an element identified by a “200” series reference numeral will first appear in FIG. 2, and so on. With reference to the Specification, Abstract, and
20 Claims sections herein, it should be noted that the singular forms “a”, “an”, “the”, and the like include plural referents unless expressly discussed otherwise. As an illustration, references to “a device” or “the device” include one or more of such devices and equivalents thereof.

FIG. 1 shows a diagrammatic view of a hybrid system 100 according to one
25 embodiment. The hybrid system 100 illustrated in FIG. 1 is adapted for use in commercial-grade trucks as well as other types of vehicles or transportation systems, but it is envisioned that various aspects of the hybrid system 100 can be incorporated into other environments. As shown, the hybrid system 100 includes a drive train 108 having a transmission 106, power sources in the form of an engine
30 102 and hybrid module 104, and a drive shaft 107. The drive train 108 is positioned to transfer power between the power sources and wheels 110. The hybrid module 104 incorporates an electrical machine, commonly referred to as an

eMachine 112, and a clutch that operatively connects and disconnects the engine 102 from the eMachine 112 and the transmission 106. An energy storage system 134 is operatively coupled to an inverter 132 and the eMachine 112.

5 The transmission 106 is an automatic transmission that is capable of automatically changing gear ratios as the vehicle moves. The transmission 106 has variable gear ratios which can be selected or changed in an automatic fashion during operation. The transmission 106 can be a variety of types, but commonly is a hydraulic transmission including one or more planetary gearsets and a plurality of clutches. The planetary gearset(s) is a compound epicyclic gearset having one or
10 more outer gears revolving about a central gear. The gearset(s) typically includes bands and clutches actuated by hydraulic servos. A hydraulic fluid (such as a lubricating or automatic transmission fluid) provides lubrication, corrosion prevention, and a hydraulic medium to convey mechanical power for operation of the transmission. In some embodiments, the transmission 106 includes a torque
15 converter for hydraulically connecting the power sources to the transmission 106. The transmission 106 can include a pump which draws the hydraulic fluid from a sump and circulates the fluid throughout the transmission 106 and/or pressurizes it for input to a torque converter housing. Transmission 106 can include a fluid cooling system for maintaining the temperature of the hydraulic fluid. The cooling
20 system can be shared with other components of the hybrid system 100 or it can be dedicated to the transmission 106. In some embodiments, the transmission 106 is fluidly connected with the hybrid module 104. The transmission 106 includes an input shaft which is coupled to the hybrid module 104 and an output shaft which is coupled to the drive shaft 107.

25 The hybrid system 100 incorporates a number of control systems for controlling the operations of the various components. For example, the engine 102 has an engine control module 146 that controls various operational characteristics of the engine 102 such as fuel injection and the like. A transmission/hybrid control module 148 substitutes for a traditional transmission control module and is
30 designed to control both the operation of the transmission 106 as well as the hybrid module 104. The transmission/hybrid control module 148 and the engine control module 146 along with the inverter 132, energy storage system 134, and a DC-DC

converter system 140 communicate along a communication link as is depicted in FIG. 1. In a typical embodiment, the transmission/hybrid control module 148 and engine control module 146 each comprise a computer having a processor, memory, and input/output connections. Additionally, other vehicle subsystems may also
5 contain computers having similar processors, memory, and input/output connections. During operation, the transmission/hybrid control module 148 receives information from various components of the vehicle, determines the appropriate gear ratio and implements changes, or shifts between gear ratios upon acceleration or braking demands from the driver. The system includes a shift
10 selector 152 for selecting whether the vehicle is in drive, neutral, reverse, etc.

FIG. 2 shows a diagram of one example of a communication system 200 that can be used in the hybrid system 100. While one example is shown, it should be recognized that the communication system 200 in other embodiments can be configured differently than what is shown. The hybrid/transmission control module
15 148 includes a hybrid data link and a vehicle data link through which most of the various components of the hybrid system 100 communicate. In particular, the data links facilitate communication between the transmission/hybrid control module 148, the engine control module 146, the energy storage system 134, the inverter 132, the shift selector 152, and the DC-DC converter system 140 as well as other
20 components.

Various information is exchanged or communicated between the transmission/hybrid control module 148 and other various components. In terms of general functionality, the transmission/hybrid control module 148 receives power limits, capacity available current, voltage, temperature, state of charge, status, and
25 fan speed information from the energy storage system 134 and the various energy storage modules within. The transmission/hybrid control module 148 in turn sends commands for connecting the various energy storage modules so as to supply voltage to and from the inverter 132. From the inverter 132, the transmission/hybrid control module 148 receives a number of inputs such as the
30 motor/generator torque that is available, the torque limits, the inverter's voltage current and actual torque speed. Based on that information, the transmission/hybrid

control module 148 controls the torque speed. From the inverter 132, the transmission/hybrid control module 148 also receives a high voltage bus power and consumption information. The transmission/hybrid control module 148 also communicates with and receives information from the engine control module 146 and in response controls the torque and speed of the engine 102 via the engine control module 146.

The various components of the hybrid system 100 as well as their function are discussed in further detail in US Patent Application No. 13/527,953, filed June 20, 2012 and International Application No. PCT/US2011/041018, filed September 9, 2011, published as WO 2012/034031 A2, which are hereby incorporated by reference.

Disclosed herein is a method of controlling the drive train power profile. As used herein “power profile” refers to the torque profile delivered to wheels 110 over a given period of time. A target drive train output power profile (target power profile) is tailored to produce a specific power profile in response to a command from the driver. Driver commands can include actuating the accelerator, releasing the accelerator, actuating the brake pedal, releasing the brake pedal, engaging auxiliary braking selectors, or any combination, degree, or variance of the same. The method generally includes setting a target power profile in response to a driver command, determining the cumulative power losses of the drive train, and adjusting the power input from the power sources so that the actual power delivered to wheels 110 (i.e. actual power profile) matches the target power profile. The target power profile is monitored continuously or during set intervals over time and adjusted based on new or different driver commands. Various operating parameters of the drive train 108 are likewise monitored continuously or during set intervals in order to calculate the power losses and actual power delivered to wheels 110 at any given moment. Power losses are generally defined as energy losses over a period of time. Power losses are commonly dependent on a several loss parameters at any given moment and change with variance in the loss parameters. Power losses do not necessarily occur linearly, and various relationships between energy loss and time are described below.

During operation, various operating parameters of the drive train 108 are known, monitored, and/or calculated by the transmission/hybrid control module 148 and used when determining the amount of torque that is necessary to achieve the target power profile. Operating parameters are divided herein into the vehicle data and loss parameters. Loss parameters include hydraulic power loss, kinetic power loss, and clutch power loss. Vehicle data includes in part the rotational speed of the engine 102 output shaft, the rotational speed of the hybrid module 104, and the speed and acceleration of the vehicle (including the rotational speed of the drive shaft 107. Examples of loss parameters include the gear configuration of the transmission 106, the rotational speeds of each part of the transmission 106 (i.e. various groupings of gears), the temperature and pressure of the hydraulic fluid in the transmission, and the state of engagement of all of the clutches in transmission 106. The sampled values are transmitted to or obtained by the transmission/hybrid control module 148.

More specifically, several losses occur in the transmission 106 hydraulic system. Certain parameters of the transmission 106 hydraulic system are known (i.e. hydraulic loss parameters). A sensor positioned along the fluid flow path of the hydraulic fluid monitors and reports the temperature of the hydraulic fluid. Similarly, a sensor monitors and reports the pressure of the hydraulic fluid. The flow rate of the hydraulic fluid is also monitored and reported. Energy losses occur due to fluid friction from moving parts and moving fluid as well as losses from oil pressure changes. Efficiency of the hydraulic system varies with variances in the temperature of the fluid. Energy dissipated (and therefore lost) within the transmission 106 due to the transmission hydraulic system have been determined through testing and are generally well known for any given values of these loss parameters. Such losses for any given values of these loss parameters are denoted herein as equation (1):

$$(1) \quad P_{loss} = \text{transmission hydraulic system losses}$$

Other loss parameters include the rotational rates and acceleration of all rotating parts in the drive train 108. Generally, energy losses occur when rotating parts maintain, change, or reverse rotational speeds. The kinetic energy of a rotating body is described mathematically as $E = \frac{1}{2} J \omega^2$, where J is the rotational inertia of the body, and ω is the angular velocity of the body. The rotational inertia (or polar moment of inertia) is the property of the body that measures its resistance to rotational acceleration about an axis, i.e. the degree of outside force necessary to reduce the rotation rate of the body. The rotational inertia of various parts of the transmission 106 for every possible gear and clutch configuration have been determined through testing and are well known. Generally, for each configuration one or more groups of components rotate in unison (not including transitory periods of clutch engagement and disengagement), and the rotational inertia of each group is determined. Power is defined as the time rate of change of energy, so the power of a rotating body can be found by taking the time derivative of E .

Therefore the power is $P = \frac{dE}{dt} = J \omega \alpha$, where α is the time derivative of ω (i.e. $\frac{d\omega}{dt}$), or the rotational acceleration of the body. Practically, the rotational acceleration can be determined from or quantified as the surplus of power versus the load, or in the case of the drive train, the rotational acceleration is dependant on the power available and the weight of the vehicle and can be determined accordingly. The rotational speed of bodies in the drive train are known through sensors and/or known relationships between input values and various gear configurations. Thus, the total power loss due to kinetic energy dissipation (kinetic power loss) can be expressed and calculated according to equation (2):

$$(2) \quad P_K = \sum_{i=1}^N J_{i-N} \omega_{i-N} \alpha_{i-N}$$

for N groups of components rotating in unison (i.e. $i=1-N$), where J , ω , and α are known values for any given set of loss parameters.

Other loss parameters are related to engagement of the clutches in the transmission 106. A clutch is a mechanical device for controlling the connection between two rotating bodies. Clutches generally include two metal plates that are pressed together by hydraulic force. When pressed together, frictional forces couple the two plates and connect the bodies so that they rotate in unison. During the coupling, energy is dissipated in the form of heat due to the friction between the two plates. Solenoids are included in the transmission 106. A solenoid includes a helically-wound coil which creates a magnetic field upon excitation of the coil. Such magnetic fields are harnessed and used to apply a linear hydraulic force to one or both plates in a clutch. The torque transmitted across the clutch during engagement is denoted by T_{clutch} . The slip across the clutch is denoted as $|\omega_1 - \omega_2|$, where $\omega_1 - \omega_2$ is the difference between the rates of rotation of the two clutch plates. The power dissipated during engagement of a clutch (i.e. transmission clutch power loss, or clutch losses) is then described according to equation (3):

$$(3) \quad P_{clutch} = \sum_1^K T_{clutch_{m_1-K}} |\omega_1 - \omega_2|_{m_1-K}$$

for K clutches (i.e. $m=1-K$). Through testing, the torque transmitted across various clutches in transmission 106 has been determined as a function of the current applied to the coil(s). Therefore, the power loss in each clutch is known as a function of the current applied to the coil and the angular rotation rates of the two plates. Clutch losses occur when changing gears, as clutches either engage or disengage. When gears are not changing during operations, the clutch losses are zero and need not be calculated.

When all the power losses are known, the power needed from the power sources to maintain or achieve the target power profile are calculated according to equation (4):

$$(4) \quad P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - P_K - P_{clutch}$$

or, alternatively as equation (5):

$$(5) \quad P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - \sum_1^N J_{i_{1-N}} \omega_{i_{1-N}} \dot{\omega}_{i_{1-N}} - \sum_1^K T_{clutch_{m_{1-K}}} |\omega_1 - \omega_2|_{m_{1-K}}$$

5 where P_{dl} is the target power profile, P_{engine} is the engine 102 power, and P_{hybrid} is the hybrid module 104 power.

FIGs. 3, 4, and 5 illustrate example implementations of different power profiles. FIG. 3 illustrates an example power profile according to current methods in which no target power profile is applied. The horizontal axis represents time and the vertical axis represents power. A user command profile 302 represents the users application of the accelerator. The profile of the user command profile 302 shows an initial steep slope beginning at zero which tapers off into a line having zero slope. The user command profile 302 can be characterized as a command for smooth acceleration until a desired vehicle speed is achieved. At 304, the desired speed is achieved and the user releases the accelerator and correspondingly the user command profile 302 returns to zero, indicating a desire to maintain or reduce the speed of the vehicle. Although the user command profile 302 indicates a desire for smooth acceleration, the vehicle does not deliver the desired power profile. Rather, the exemplary power profile 306 is achieved. The regions 308 and 310 indicate areas where gear changes occur. The region 308 indicates an upshift, and the region 310 indicates a downshift. In each of the regions 308 and 310, the power profile exhibits a disturbance. Generally, gear changes in automatic transmissions cause variances in torque applied to the wheels of the vehicle. This is due in part to a continuous supply of power from the power source even while the gear is disengaged. As a clutch disengages, the continuous supply of power causes an upsurge 312 in the power profile. Subsequently the re-engagement of the gears in the higher gear causes a downsurge 314 in the power profile. The continuous supply of power from the power source then causes the power profile to continue an upward trend in the new gear. A similar result happens during a downshift as shown in the region 310. The upsurge and downsurge in the regions 308 and 310

create disturbances in the drive train 108 which manifest as vibrations or other unwanted characteristics to the driver.

The details disclosed herein provide a method to precisely control the power profile of the vehicle and to create a driving experience that is more comfortable and/or custom tailored to the user's wishes. FIG. 4 illustrates a further example of a power profile. The user command profile 302 again illustrates a command for smooth acceleration to a desired vehicle speed. A target power profile 402 diverges from the exemplary power profile 306 in the regions 408 and 410. The target power profile is chosen to minimize the disturbance in the drive train 108 during gear shifts by reducing the magnitude of the profile disturbances in regions 408 and 410.

FIG. 5 illustrates a further example showing a target power profile 502. The figure again illustrates the user command profile 302 which calls for a smooth acceleration to a desired vehicle speed at 504. The exemplary power profile 306 is shown again for comparison. The target power profile 502 continues without significant disturbance throughout the gear shifts in the regions 508 and 510. Such a power profile creates a significantly smoother acceleration experience than that provided by the exemplary power profile 306.

Realization of the target power profile 502 is achieved according to the methods described herein, including obtaining the loss parameters, calculating the power losses in the drive train 108, and determining the level of torque that is needed at the transmission input shaft in order to maintain the target power profile 502 at the wheels 110 of the vehicle. Values for each of the loss parameters described herein are sampled regularly for each operating state (i.e. gear positions, speed of motors, speed of wheels, etc) and received by the transmission/hybrid control module 148. When the engine 102 and/or the hybrid module 104 are already rotating and/or supplying torque to the drive train 108, that speed or torque information is conveyed to the transmission/hybrid control module 148 along with the speed of wheels 110. In some cases the values of the loss parameters are sampled at specific intervals (e.g. 50-100 samples per second). Each sampling produces a result set of values.

An algorithm describing the method disclosed herein will now be described according to FIG. 6. In a typical operation, the vehicle may be at any number of operational states (stopped, constant velocity, accelerating, decelleraing, etc.). The driver executes a driver input (or command input) which could be acuation of the accelerator, brake, or auxiliary brake command. The transmission/hybrid control module 148 receives the driver input at action 600.

Current vehicle operational data is transferred to the transmission/hybrid control module 148 at action 602. This includes information related to the current operation of the engine 102, the hybrid module 104, energy storage system 134, and the vehicle. The engine 102 speed, power (or torque produced), and limits associated with speed and power are obtained from the engine control module 146 over the vehicle data link. Data is also obtained regarding the speed, power (or torque produced), for all hybrid motors (i.e. hybrid module 104). Information related to the hybrid power capabilities is obtained from the energy storage system 134 over the hybrid data link. Data related to the vehicle such as wheel 110 speed and/or acceleration is also obtained. The transmission/hybrid control module 148 stores these values. In some embodiments, the transmission/hybrid control module 148 measures operational data directly. In other embodiments, any data described herein is measured and/or obtained by any of a variety of sensors and controllers, with the data ultimately being obtained by a single controller for processing.

At action 604, the transmission/hybrid control module 148 obtains the loss parameters necessary to calculate the losses according to equations (1), (2), and (3). The loss parameters (as already described above) include the gear configuration of the transmission 106, the current configuration of gears in the transmission including rotational speeds (ω), acceleration (α), and rotational inertia (J) of each. If a gear change is in progress, then loss parameters for each clutch undergoing change are obtained, such as angular rotation speeds (ω_1 and ω_2) of each clutch plate and the value of the torque across the clutch (T_{clutch}). The temperature of the hydraulic fluid in the transmission 106 as well as the pressure and flow rate of the hydraulic fluid are obtained. The three values of the pressure

losses are then calculated (equations (1), (2), and (3)) and stored by the transmission/hybrid control module 148.

At action 606, the transmission/hybrid control module 148 calculates a target power profile (P_{dl}) based on the driver input received in action 600. The target power profile (P_{dl}) is determined based on a user's specific preference and can be tailored in a variety of ways. For example, the target power profile can be chosen to optimize fuel economy, maximize acceleration, cancel power fluctuations from transmission shifts, or smooth the drive line power profile for driver comfort. For example, the smooth slope of the target power profile 502 of FIG. 5 is optimized to cancel power fluctuations from transmission shifts and/or to increase fuel efficiency. A target power profile optimized for increased acceleration would have a steeper initial slope that tapered off earlier than the point 504. Some of these objectives may exclude others. For example, a profile chosen to optimize fuel economy is generally incompatible with a profile chosen to maximize acceleration. The strategy behind the profile selection may change at various times during the service life of the vehicle. In some cases, the profile can be user-selectable. For example, in some embodiments, an interface is placed within the cab or elsewhere on the vehicle so that the user can choose a target power profile based on an immediate or changed need during operation. In other embodiments, the target power profile is not selectable by the user (e.g. in situations where an owner prefers to maximize fuel economy in contrast to the driver who prefers to maximize driver comfort or acceleration).

At action 608, the transmission/hybrid control module 148 calculates the power requirement from the engine 102 and the hybrid module 104 ($P_{engine} + P_{hybrid}$) that is needed to meet the target power profile according to equation (4), which includes consideration of the difference between the actual power profile and the target power profile. In other words, equation (4) is solved for $P_{engine} + P_{hybrid}$. The transmission/hybrid control module 148 sends torque commands to the engine control module 146 and the hybrid module 104, and the

engine 102 and hybrid module 104 are set to best achieve $P_{engine} + P_{hybrid}$. The torque commands are executed, and the target power profile is achieved.

Operation of the engine 102 and hybrid module 104 are tailored to make the actual power profile match the target power profile, as described below.

5 Because the sampling and calculations are performed many times per second, any commands sent to the power sources which are needed to maintain the target power profile are immediately conveyed. Similarly, because the sampling occurs frequently, any changes to the state of the vehicle or driver inputs (e.g. change from acceleration to brake or change in incline of a road) are immediately
10 considered. In this way, the target power profile can change and still be maintained by the vehicle.

Generally, a determination is made as to the appropriate split in power between the two power sources in order to make the actual power profile match the target power profile with the user's goal in mind, as each power source has
15 different efficiencies and/or operating limits at any given operating condition. For example, the state of charge of the energy storage system 134 informs the transmission/hybrid control module 148 as to how much of the power can be provided by hybrid module 104 at any given moment and at what efficiency.

As mentioned previously, the drive train 108 couples the power sources
20 (i.e. the engine 102 and the hybrid module 104) to the wheels 110. Torque can be transferred to an input shaft of transmission 106 independently by either the engine 102 or the hybrid module 104. Alternatively, the engine 102 and the hybrid module 104 can work in conjunction to transfer torque to the transmission 106. The hybrid module clutch allows the hybrid module 104 to couple or decouple with the engine
25 102 so that the hybrid module 104 can be turned by the engine 102, independently supply torque to the input shaft of the transmission 106, or work in conjunction with the engine 102 to supply torque to the input shaft of the transmission 106. Each power source has particular efficiency advantages and missions for a variety of different operating conditions. An algorithm executed by the
30 transmission/hybrid control module is used to maintain a balance of the power

sources that most efficiently realizes both the target power profile and other operating considerations.

While the disclosure has been illustrated and described in detail in the drawings and foregoing description, the same is to be considered as illustrative and not restrictive in character, it being understood that only the preferred embodiment
5 has been shown and described and that all changes, equivalents, and modifications that come within the spirit of the disclosures defined by following claims are desired to be protected. All publications, patents, and patent applications cited in this specification are herein incorporated by reference as if each individual
10 publication, patent, or patent application were specifically and individually indicated to be incorporated by reference and set forth in its entirety herein.

What is claimed is:

1. A method, comprising:

controlling a power profile for a hybrid vehicle using a control module,
wherein the hybrid vehicle has a power source and a drive train, and wherein the
control module controls the drive train and the power source;

establishing a target drive train output power profile using the control
module, wherein the target drive train output power profile is determined using a
command input; and

establishing an input power using the control module, wherein the input
power is sufficient to supply the target drive train output power profile, and
wherein the control module establishes the input power using one or more loss
parameters and the target drive train output power profile.

2. The method of claim 1, further comprising:

determining a current state of the vehicle using the control module;

calculating a power loss within the drive train using the control module, the
control module calculating the power loss using the one or more loss parameters;
and

controlling the power source to provide the input power to the drive train
using the control module.

3. The method of claim 1 or 2, wherein the loss parameters include a
hydraulic power loss, and wherein the hydraulic power loss is calculated as a
function of hydraulic loss parameters.

4. The method of claim 3, wherein the hydraulic loss parameters include a
temperature of a hydraulic fluid in the drive train.

5. The method of claim 3 or 4, wherein the hydraulic loss parameters include
a pressure of the hydraulic fluid in the drive train.

6. The method of any one of claims 3 through 5, wherein the hydraulic loss parameters include a flow rate of a hydraulic fluid in the drive train.

7. The method of any preceding claim, wherein the one or more loss parameters include a kinetic power loss, and wherein the kinetic power loss is calculated as a function of rotational inertia loss parameters within the drive train.

8. The method of claim 7, wherein the rotational inertia loss parameters include a rotational inertia of at least one body in the drive train.

9. The method of claim 7 or 8, wherein the rotational inertia loss parameters include a rotational speed of at least one body in the drive train.

10. The method of any one of claims 7 through 9, wherein the rotational inertia loss parameters include a rotational acceleration of at least one body in the drive train.

11. The method of any one of claims 7 through 10, wherein the kinetic power loss is represented by the following equation:

$$P_K = \sum_{i=1}^N J_{i-N} \omega_{i-N} \alpha_{i-N}$$

where:

P_K = Kinetic Power Loss;

N = Number of groups of components rotating in unison;

J_{i-N} = A rotational inertia of a body;

ω_{i-N} = A rate of rotation of the body; and

α_{i-N} = A rotational acceleration of the body.

12. The method of any preceding claim, wherein the loss parameters include a clutch power loss for a clutch, wherein the drive train has at least one clutch,

wherein the clutch has a plurality of clutch plates, and wherein the clutch power loss is calculated as a function of clutch loss parameters.

13. The method of claim 12, wherein the clutch loss parameters include a torque transmitted between the plurality of clutch plates during engagement of the clutch.

14. The method of claim 12 or 13, wherein the clutch loss parameters include a rotational speed of each clutch plate in the plurality of clutch plates.

15. The method of any one of claims 12 through 14, wherein the clutch power loss is represented by the equation:

$$P_{clutch} = \sum_{1}^K T_{clutch_{m1-K}} |\omega_1 - \omega_2|_{m1-K}$$

where:

P_{clutch} = Clutch Power Loss;

K = Number of bodies;

$T_{clutch_{m1-K}}$ = A torque transmitted between clutch plates of the clutch during engagement;

$|\omega_1 - \omega_2|_{m1-K}$ = an absolute value of a difference between rates of rotation of each clutch plate.

16. The method of any preceding claim, wherein the target drive train output power profile is represented by the following equation:

$$P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - P_K - P_{clutch}$$

where:

P_{dl} = A target drive train output power profile;

P_{engine} = Engine power;

P_{hybrid} = Hybrid module power;

P_{loss} = A hydraulic power loss;

P_K = A kinetic power loss;

$$P_{clutch} = A \text{ clutch power loss.}$$

17. The method of any one of claims 2 through 16, wherein the act of calculating a power loss is performed before the control module controls the power source to provide the input power to the drive train.

18. The method of any one of claims 2 through 16, wherein the act of calculating a power loss is performed at substantially the same time the control module controls the power source to provide the input power to the drive train.

19. The method of the preceding claims, wherein the power source includes an engine and a hybrid module.

20. The method of claim 19, wherein the hybrid module includes an electric motor.

21. A method, comprising:
controlling a power source output power of a vehicle using a controller, wherein the vehicle has a drive train and a power source, and wherein the controller controls the power source and the drive train;
determining a target drive train output power using the controller, wherein the target drive train output power is determined using a command input;
determining the power source output power using the controller, wherein the target drive train output power is derived from the power source output power;
and wherein the controller determines the power source output power using one or more loss parameters and the target drive train output power.

22. The method of claim 21, further comprising:
calculating a power loss within the drive train using the controller, the controller calculating the power loss using the one or more loss parameters, and
controlling the power source output power provided to the drive train using the controller.

23. The method of claim 21 or 22, wherein the loss parameters include a hydraulic power loss, and wherein the hydraulic power loss is calculated as a function of hydraulic loss parameters.

5

24. The method of any one of claims 21 through 23, wherein the loss parameters include a kinetic power loss, and wherein the kinetic power loss is calculated as a function of rotational inertia loss parameters within the drive train.

10 25. The method of claim 24, wherein the kinetic power loss is represented by the following equation:

$$P_K = \sum_1^N J_{i_{1-N}} \omega_{i_{1-N}} \alpha_{i_{1-N}}$$

where:

P_K = Kinetic Power Loss;

15 N = Number of groups of components rotating in unison;

$J_{i_{1-N}}$ = A rotational inertia of a body;

$\omega_{i_{1-N}}$ = A rate of rotation of the body; and

$\alpha_{i_{1-N}}$ = A rotational acceleration of the body.

20 26. The method of any preceding claim, wherein the loss parameters include a clutch power loss for a clutch, wherein the drive train has at least one clutch, wherein the clutch has a plurality of clutch plates, and wherein the clutch power loss is calculated as a function of clutch loss parameters.

25 27. The method of claim 26, wherein the clutch power loss is represented by the following equation:

$$P_{clutch} = \sum_1^K T_{clutch_{m_{1-K}}} |\omega_1 - \omega_2|_{m_{1-K}}$$

where:

P_{clutch} = Clutch Power Loss;

K = Number of bodies;

$T_{clutch_{m_1-K}}$ = A torque transmitted between clutch plates of the clutch during engagement;

$|\omega_1 - \omega_2|_{m_1-K}$ = an absolute value of a difference between rates of rotation of each clutch plate.

28. The method of any one of claims 21 through 27, wherein the target drive train output power is represented by the following equation:

$$P_{dl} = P_{engine} + P_{hybrid} - P_{loss} - P_K - P_{clutch}$$

10 where:

P_{dl} = A target drive train output power profile;

P_{engine} = Engine power;

P_{hybrid} = Hybrid module power;

P_{loss} = A hydraulic power loss;

15 P_K = A kinetic power loss;

P_{clutch} = A clutch power loss.

29. The method of any preceding claim, wherein determining the target drive train output power includes an acceleration vehicle data parameter.

20

30. The method of any preceding claim, wherein determining the target drive train output power includes a fuel economy vehicle data parameter.

31. The method of any preceding claim, wherein determining the target drive train output power includes an emissions vehicle data parameter.

25

32. The method of claim any one of claims 29 through 31, further comprising: selecting one or more vehicle data parameters, wherein the user selects the vehicle data parameters using an interface.

30

33. The method of any one of claims 21 through 32, wherein the power source includes an engine and a hybrid module.

34. The method of claim 33, wherein the hybrid module includes an electric motor.

35. A method for operating a vehicle having a controller and a drive train including a transmission and a power source wherein the controller is arranged and configured to:

- 10 determine a target drive train output power using a command input;
- determine hydraulic power loss of the drive train as a function of hydraulic loss parameters within the transmission;
- determining kinetic power loss of the drive train as a function of rotational inertia loss parameters within the drive train;
- 15 determining clutch power loss of the drive train as a function of clutch loss parameters within the transmission;
- establishing the input power needed to reach the target drive train output power as a function of the hydraulic loss parameters, the rotational inertia loss parameters, and the clutch loss parameters; and
- 20 adjusting the power supplied by the power source to reach the target drive train output power.

36. A method for operating a hybrid vehicle having a controller and a drive train including a transmission and a power source, comprising:

- 25 receiving a command input from a driver;
- determining a current state of the vehicle;
- determining loss parameters of the drive train;
- establishing a target drive train output power profile as a function of the command input;
- 30 establishing power loss within the drive train as a function of the loss parameters;

establishing a requisite input power needed to reach the target drive train output power profile as a function of the loss parameters and the target drive train output power profile; and
supplying the requisite input power to the drive train.

5

37. An apparatus for performing the method of any one of the preceding claims.

10

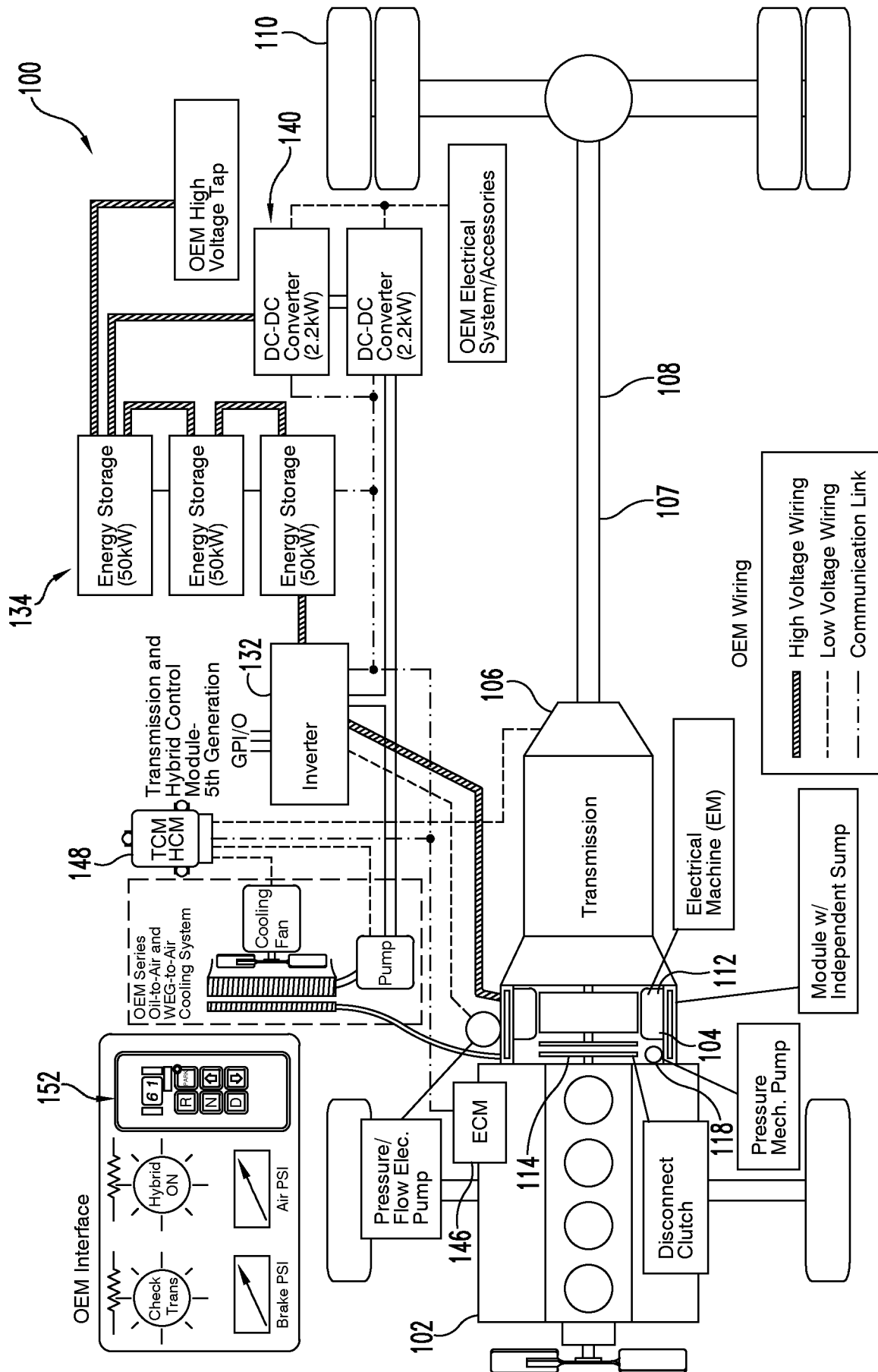


Fig. 1

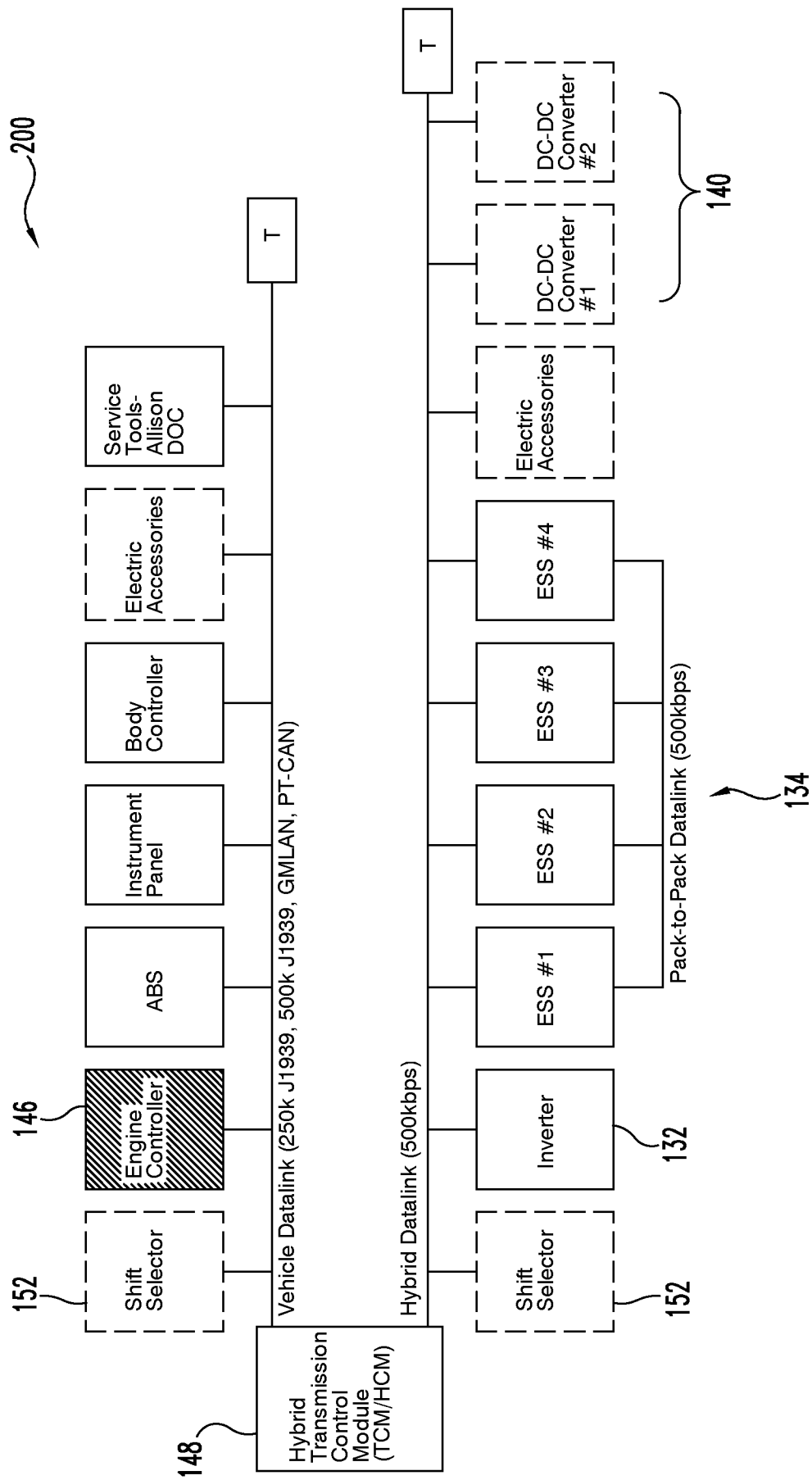
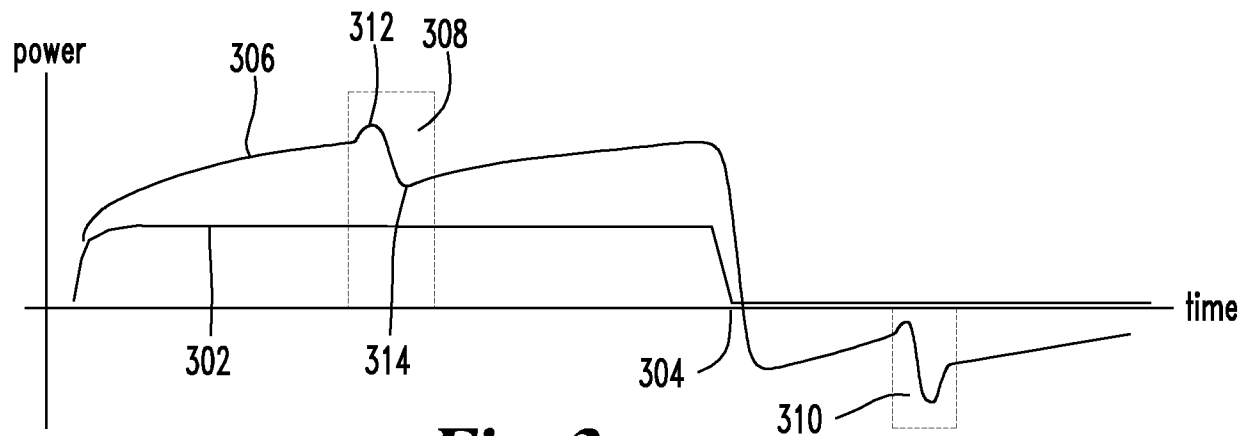
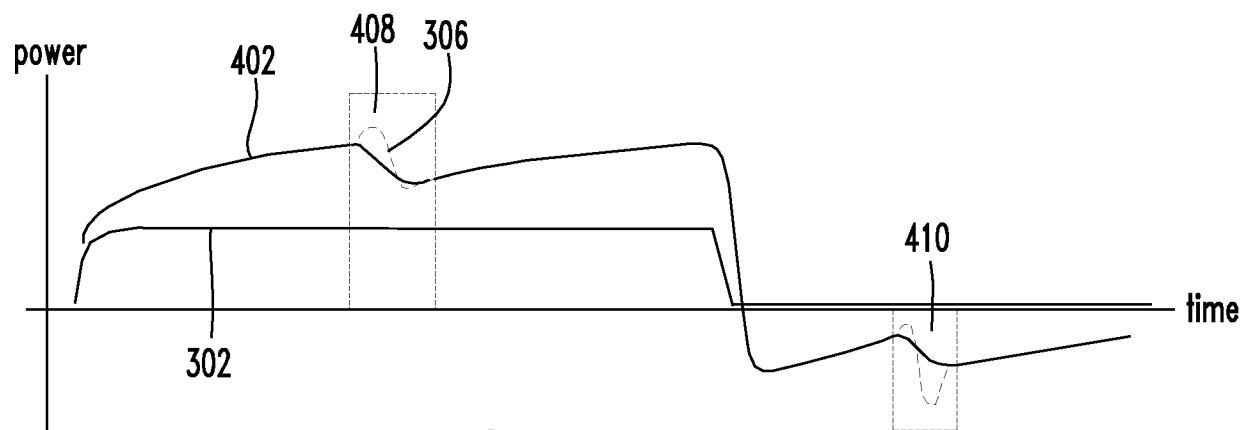
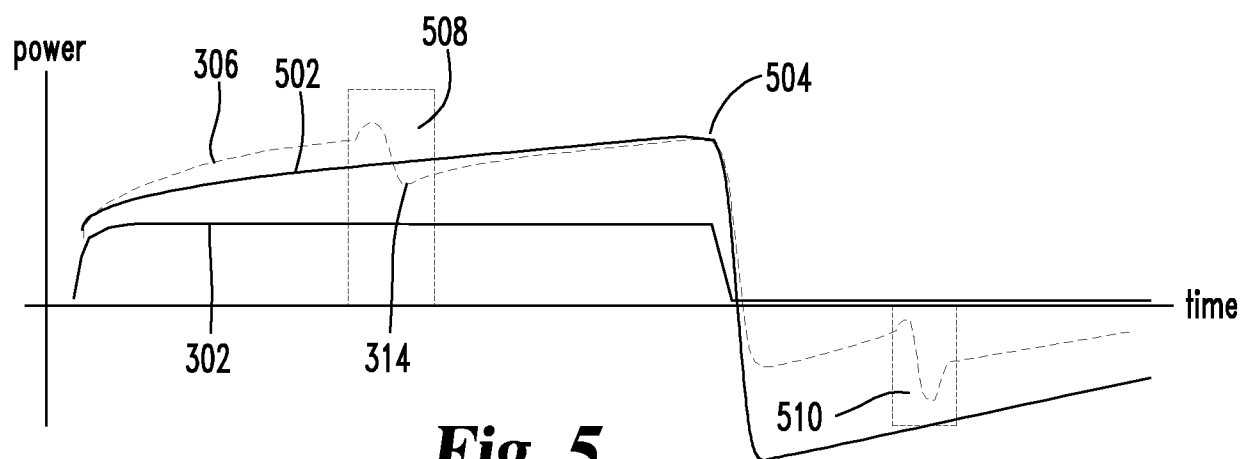
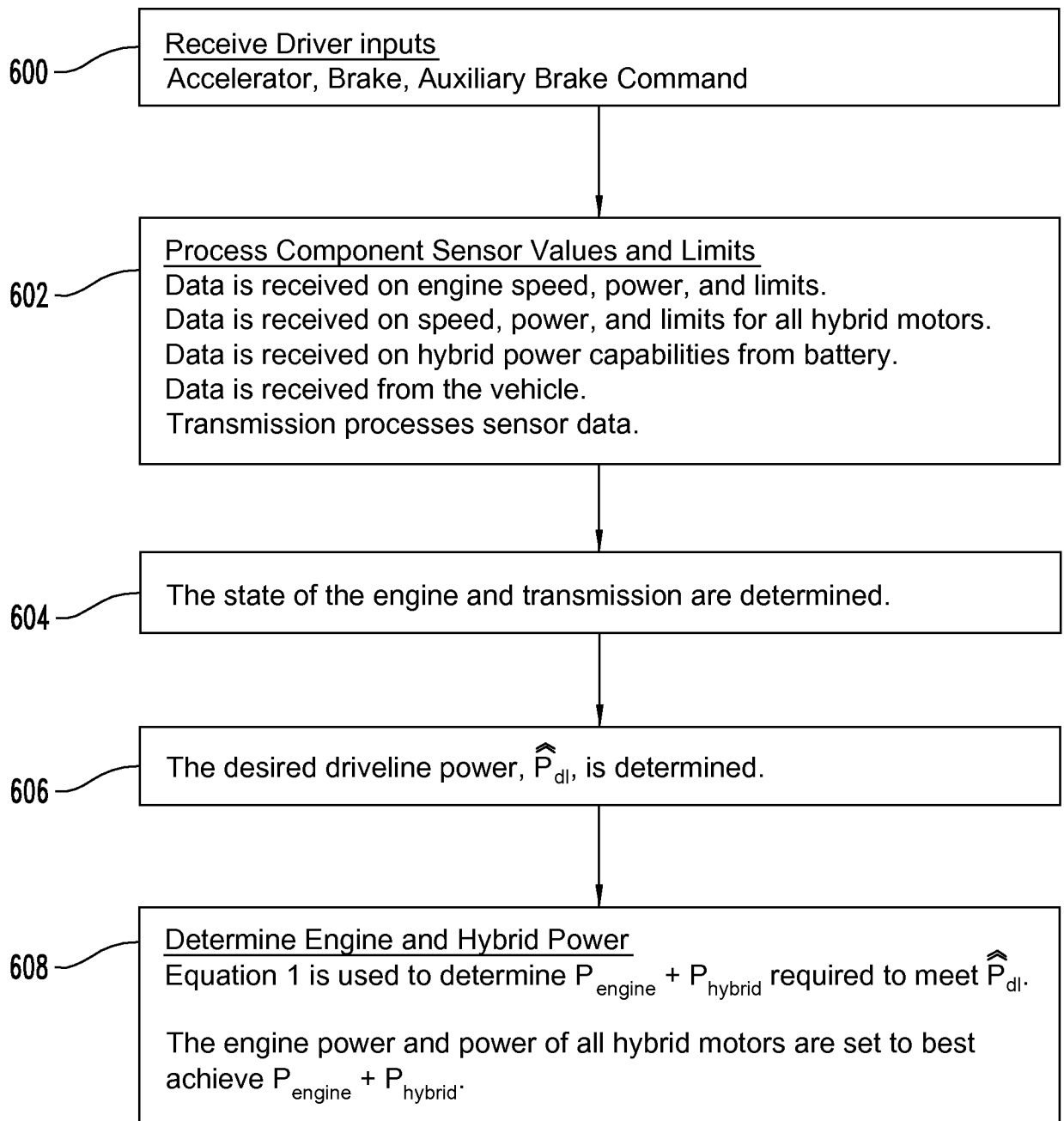


Fig. 2

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**Fig. 3****Fig. 4****Fig. 5**

4/4

**Fig. 6**

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US2014/020499**A. CLASSIFICATION OF SUBJECT MATTER****B60W 20/00(2006.01)i, B60W 10/04(2006.01)i, B60W 10/06(2006.01)i, B60W 10/08(2006.01)i**

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

B60W 20/00; H02H 7/06; B60L 11/18; B60W 10/08; B60K 6/02; B60K 41/00; B60K 1/00; B60W 10/06; B60K 6/04; B60W 10/04

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Korean utility models and applications for utility models

Japanese utility models and applications for utility models

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

eKOMPASS(KIPO internal) & Keywords: hybrid, target, output, power, torque, request, input, and loss

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	US 7076356 B2 (HUBBARD, GREGORY A. et al.) 11 July 2006 See column 1, line 62 - column 14, line 22, and figures 2,4,11.	1-3,12,17,19-23,26 ,29,30,33,34,36,37 4-11,13-16,18,24 ,25,27,28,31,32,35
A	US 6799650 B2 (KOMIYAMA, SUSUMU et al.) 05 October 2004 See column 2, line 49 - column 3, line 38 and figures 1,2.	1-37
A	WO 2012-114430 A1 (SUZUKI MOTOR CORPORATION et al.) 30 August 2012 See abstract, paragraphs [0011],[0019]-[0024], and figures 1,4.	1-37
A	US 2003-0173934 A1 (ARIMITSU, MINORU) 18 September 2003 See paragraphs [0040]-[0042] and figures 1,3.	1-37
A	US 7532961 B2 (HOSHIBA, TAKESHI et al.) 12 May 2009 See column 2, line 48 - column 3, line 13, column 6, line 55 - column 7, line 17, claim 3, and figures 1,2.	1-37



Further documents are listed in the continuation of Box C.



See patent family annex.

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"P" document published prior to the international filing date but later than the priority date claimed

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"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

12 June 2014 (12.06.2014)

Date of mailing of the international search report

16 June 2014 (16.06.2014)

Name and mailing address of the ISA/KR

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/US2014/020499

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 7076356 B2	11/07/2006	CN 100467914 C CN 1654854 A DE 102005006369 A1 US 2005-0182526 A1	11/03/2009 17/08/2005 08/09/2005 18/08/2005
US 6799650 B2	05/10/2004	JP 03539406 B2 JP 2003-009305 A US 2002-0195288 A1	07/07/2004 10/01/2003 26/12/2002
WO 2012-114430 A1	30/08/2012	CN 103402840 A DE 112011104926 T5 US 2014-081500 A1	20/11/2013 24/12/2013 20/03/2014
US 2003-0173934 A1	18/09/2003	DE 60305549 D1 DE 60305549 T2 EP 1346865 A1 EP 1346865 B1 JP 03641245 B2 JP 2003-269594 A US 6751960 B2	06/07/2006 02/11/2006 24/09/2003 31/05/2006 20/04/2005 25/09/2003 22/06/2004
US 7532961 B2	12/05/2009	CN 1819933 A CN 1819933 B DE 602004030340 D1 EP 1644215 A1 EP 1644215 B1 JP 03894168 B2 JP 2005-039880 A US 2006-0161328 A1 WO 2005-005188 A1	16/08/2006 24/11/2010 13/01/2011 12/04/2006 01/12/2010 14/03/2007 10/02/2005 20/07/2006 20/01/2005