



(11) (21) (C) **2,223,986**
(86) 1996/09/20
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(45) 2000/08/08

(72) KOMIYA, Kyosuke, JP

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(51) Int.Cl.⁶ C07C 69/96, C07D 213/63, C07C 255/55, C07C 205/43,
C07C 253/30, C07D 215/20, C07C 201/12, C07C 68/06, C07D 311/04

(30) 1995/09/22 (7-268036) JP

(54) **PROCEDE DE PRODUCTION D'UN CARBONATE
AROMATIQUE**

(54) **PROCESS FOR PRODUCING AN AROMATIC CARBONATE**

(57) L'invention concerne un procédé de préparation de carbonate aromatique qui consiste à utiliser un produit de départ choisi dans le groupe des carbonates de dialkyle, des carbonates d'alkylaryle et de leur mélange, ainsi qu'un réactif choisi dans le groupe des composés monohydroxyle, des carbonates d'alkylaryle et de leur mélange. Selon ce procédé, on soumet le produit de départ et le réactif à une transestérification en présence d'un catalyseur à base de métal. Ce procédé est caractérisé en ce que l'on effectue la transestérification tout en maintenant à 2 ou à une valeur inférieure le rapport en poids entre au moins une substance qui présente un groupe aromatique choisi dans la catégorie des composés aromatiques polyhydroxyle spécifiques résultant du produit de départ, le réactif et/ou les sous-produits de la transestérification et leurs résidus, d'une part et le métal constituant le catalyseur. On détermine ledit rapport en poids en analysant le mélange liquide du système de transestérification qui renferme le catalyseur. Le procédé en question permet d'éliminer les phénomènes indésirables comme le dépôt et l'adhérence du catalyseur sur les réacteurs ou la tuyauterie, et offre ainsi des conditions stables pour la préparation d'un carbonate aromatique pendant une longue période.

(57) A process for the preparation of an aromatic carbonate by subjecting a starting compound selected from the group consisting of dialkyl carbonates, alkyl aryl carbonates and mixtures thereof and a reactant selected from the group consisting of aromatic monohydroxyl compounds, alkyl aryl carbonates and mixtures thereof to transesterification in the presence of a metal-containing catalyst, characterized in that the transesterification is conducted while keeping the weight ratio (WR) of at least one substance having an aromatic group selected from the group consisting of specific aromatic polyhydroxyl compounds resulting from the starting compound, the reactant and/or by-products of the transesterification and residues of them to the metal constituting the catalyst-containing liquid mixture of the transesterification system. According to this process, undesirable phenomena such as the deposition of the catalyst in reactors or pipes and the adhesion of the catalyst to them can be inhibited to thereby permit a stable preparation of an aromatic carbonate for a long period.



NB

- SN

PATENT COOPERATION TREATY

From the INTERNATIONAL BUREAU

PCT

NOTIFICATION OF ELECTION
(PCT Rule 61.2)

To:

Canadian Patent Office
The Commissioner of Patents
50 Victoria Street
Ontario K1A 0C9
CANADA

in its capacity as elected Office

Date of mailing:

27 March 1997 (27.03.97)

International application No.:

PCT/JP96/02734

Applicant's or agent's file reference:

96-1057

International filing date:

20 September 1996 (20.09.96)

Priority date:

22 September 1995 (22.09.95)

Applicant:

ASAHI KASEI KOGYO KABUSHIKI KAISHA

1. The designated Office is hereby notified of its election made:

☒

in the demand filed with the International preliminary Examining Authority on:

25 October 1996 (25.10.96)

☐

in a notice effecting later election filed with the International Bureau on:

2. The election

☒

was

☐

was not

made before the expiration of 19 months from the priority date or, where Rule 32 applies, within the time limit under Rule 32.2(b).

The International Bureau of WIPO
34, chemin des Colombettes
1211 Geneva 20, Switzerland

Facsimile No.: (41-22) 740.14.35

Authorized officer:

J. Zahra

Telephone No.: (41-22) 730.91.11

PATENT COOPERATION TREATY

PCT

TRANSLATION

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference 96-1057	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/JP 96/02734	International filing date (day/month/year) 20.09.96	Priority date (day/month/year) 22.09.95
International Patent Classification (IPC) or national classification and IPC C07C69/96, C07C68/06		
Applicant ASAHI KASEI KOGYO KABUSHIKI KAISHA AS FILED / TEL QUE DÉPOSÉ		

1.	This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.
2.	This REPORT consists of a total of <u>3</u> sheets, including this cover sheet. ☐ This report is also accompanied by ANNEXES, i.e., sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT). These annexes consist of a total of _____ sheets.
3.	This report contains indications relating to the following items: I ☒ Basis of the report II ☐ Priority III ☐ Non-establishment of opinion with regard to novelty, inventive step and industrial applicability IV ☐ Lack of unity of the invention V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability: citations and explanations supporting such statement VI ☐ Certain documents cited VII ☐ Certain defects in the international application VIII ☐ Certain observations on the international application

Date of submission of the demand 25.10.96	Date of completion of this report 02.09.97
Name and mailing address of the IPEA/JP	Authorized officer
Facsimile No.	Telephone No.

I. Basis of the report

1. This report has been drawn on the basis of *(Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to the report since they do not contain amendments.)*:

☒ the international application as originally filed.

☐ the description,

pages

pages

pages

pages

, as originally filed,

, filed with the demand,

, filed with the letter of

, filed with the letter of

☐ the claims,

Nos.

Nos.

Nos.

Nos.

Nos.

, as originally filed,

, as amended under Article19,

, filed with the demand,

, filed with the letter of

, filed with the letter of

☐ the drawings,

sheets/fig

sheets/fig

sheets/fig

sheets/fig

, as originally filed,

, filed with the demand,

, filed with the letter of

, filed with the letter of

2. The amendments have resulted in the cancellation of:

☐ the description, pages

☐ the claims, Nos.

☐ the drawings, sheets/fig

3. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed, as indicated in the Supplemental Box (Rule 70.2(c)).

4. Additional observations, if necessary:

INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.
PCT/JP 96/02734

V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement

1.	Statement			
	Novelty (N)	Claims	1 - 8	YES
		Claims		NO
	Inventive step (IS)	Claims	1 - 8	YES
		Claims		NO
	Industrial applicability (IA)	Claims	1 - 8	YES
		Claims		NO

2. Citations and explanations

P C T

国際予備審査報告

(法第12条、法施行規則第56条)
〔PCT36条及びPCT規則70〕

REC 1 5 SEP 1997

WIPO

PC

出願人又は代理人 の書類記号 96-1057	今後の手続きについては、国際予備審査報告の送付通知（様式PCT/ IPEA/416）を参照すること。	
国際出願番号 PCT/J P 96/02734	国際出願日 (日.月.年) 20.09.96	優先日 (日.月.年) 22.09.95
国際特許分類 (IPC) Int.Cl ⁶ C07C69/96, C07C68/06		
出願人 (氏名又は名称) 旭化成工業株式会社		AS FILED / TEL QUE DÉPOSÉ

1. 国際予備審査機関が作成したこの国際予備審査報告を法施行規則第57条 (PCT36条) の規定に従い送付する。
2. この国際予備審査報告は、この表紙を含めて全部で 3 ページからなる。 ☐ この国際予備審査報告には、附属書類、つまり補正されて、この報告の基礎とされた及び/又はこの国際予備審査機関に対してした訂正を含む明細書、請求の範囲及び/又は図面も添付されている。 (PCT規則70.16及びPCT実施細則第607号参照) この附属書類は、全部で ページである。
3. この国際予備審査報告は、次の内容を含む。 I ☒ 国際予備審査報告の基礎 II ☐ 優先権 III ☐ 新規性、進歩性又は産業上の利用可能性についての国際予備審査報告の不作成 IV ☐ 発明の単一性の欠如 V ☒ PCT35条(2)に規定する新規性、進歩性又は産業上の利用可能性についての見解、それを裏付けるための文献及び説明 VI ☐ ある種の引用文献 VII ☐ 国際出願の不備 VIII ☐ 国際出願に対する意見

国際予備審査の請求書を受理した日 25.10.96	国際予備審査報告を作成した日 02.09.97	
名称及びあて先 日本国特許庁 (IPEA/J P) 郵便番号100 東京都千代田区霞が関三丁目4番3号	特許庁審査官 (権限のある職員) 渡辺 陽子 電話番号 03-3581-1101 内線 3443	4H 9279

I. 国際予備審査報告の基礎

1. この国際予備審査報告は下記の出願書類に基づいて作成された。（法第6条（PCT14条）の規定に基づく命令に
応答するために提出された差し替え用紙は、この報告書において「出願時」とする）

☒ 出願時の国際出願書類

☐	明細書	第	_____	ページ、	出願時のもの
	明細書	第	_____	ページ、	国際予備審査の請求書と共に提出されたもの
	明細書	第	_____	ページ、	_____ 付の書簡と共に提出されたもの
	明細書	第	_____	ページ、	_____ 付の書簡と共に提出されたもの
☐	請求の範囲	第	_____	項、	出願時に提出されたもの
	請求の範囲	第	_____	項、	PCT19条の規定に基づき補正されたもの
	請求の範囲	第	_____	項、	国際予備審査の請求書と共に提出されたもの
	請求の範囲	第	_____	項、	_____ 付の書簡と共に提出されたもの
	請求の範囲	第	_____	項、	_____ 付の書簡と共に提出されたもの
☐	図面	第	_____	ページ/図、	出願時に提出されたもの
	図面	第	_____	ページ/図、	国際予備審査の請求書と共に提出されたもの
	図面	第	_____	ページ/図、	_____ 付の書簡と共に提出されたもの
	図面	第	_____	ページ/図、	_____ 付の書簡と共に提出されたもの

2. 補正により、下記の書類が削除された。

☐	明細書	第	_____	ページ
☐	請求の範囲	第	_____	項
☐	図面	第	_____	ページ/図

3. ☐ この国際予備審査報告は、補充欄に示したように、補正が出願時における開示の範囲を越えてされたものと認めら
れるので、その補正がされなかったものとして作成した。（PCT規則70.2(c)）

4. 追加の意見（必要ならば）

V. 新規性、進歩性又は産業上の利用可能性についての法第12条（PCT35条(2)）に定める見解、それを裏付ける文献及び説明

1. 見解

新規性（N）	請求の範囲	1－8	有
	請求の範囲		無
進歩性（I S）	請求の範囲	1－8	有
	請求の範囲		無
産業上の利用可能性（I A）	請求の範囲	1－8	有
	請求の範囲		無

2. 文献及び説明

INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP96/02734

A. CLASSIFICATION OF SUBJECT MATTER

Int. Cl⁶ C07C69/96, C07C68/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

Int. Cl⁶ C07C69/96, C07C68/06

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JP, 4-9358, A (Asahi Chemical Industry Co., Ltd.), January 14, 1992 (14. 01. 92) & WO, 91/09832, A & EP, 461274, A & JP, 4-211038, A & US, 5210268, A & CN, 1064677, A & KR, 9405956, B1	1 - 8
A	JP, 4-224547, A (Asahi Chemical Industry Co., Ltd.), August 3, 1992 (03. 08. 92) (Family: none)	1 - 8
A	JP, 4-230242, A (Asahi Chemical Industry Co., Ltd.), August 19, 1992 (19. 08. 92) (Family: none)	1 - 8
A	JP, 4-235951, A (Asahi Chemical Industry Co., Ltd.), August 25, 1992 (25. 08. 92) (Family: none)	1 - 8
A	JP, 6-116210, A (Daicel Chemical Industries, Ltd.),	1 - 8

☒ Further documents are listed in the continuation of Box C.☐ See patent family annex.

* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

December 3, 1996 (03. 12. 96)

Date of mailing of the international search report

December 17, 1996 (17. 12. 96)

Name and mailing address of the ISA/

Japanese Patent Office

Authorized officer

Facsimile No.

Telephone No.

INTERNATIONAL SEARCH REPORT

International application No.

PCT/JP96/02734

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	April 26, 1994 (26. 04. 94) & EP, 591923, A & US, 5380908, A & TW, 239121, A & CN, 1089256, A JP, 7-227546, A (Nippon Shokubai Co., Ltd.), August 29, 1995 (29. 08. 95) & WO, 95/17371, A & EP, 685455, A & US, 5565605, A	1 - 8

A. 発明の属する分野の分類 (国際特許分類 (IPC)) Int. Cl ⁶ C07C69/96, C07C68/06		
B. 調査を行った分野 調査を行った最小限資料 (国際特許分類 (IPC)) Int. Cl ⁶ C07C69/96, C07C68/06		
最小限資料以外の資料で調査を行った分野に含まれるもの		
国際調査で使用した電子データベース (データベースの名称、調査に使用した用語)		
C. 関連すると認められる文献		
引用文献の カテゴリー*	引用文献名 及び一部の箇所が関連するときは、その関連する箇所の表示	関連する 請求の範囲の番号
A	JP, 4-9358, A (旭化成工業株式会社) 14. 1月. 1992 (14. 01. 92) & WO, 91/09832, A & EP, 461274, A & JP, 4-211038, A & US, 5210268, A & CN, 1064677, A & KR, 9405956, B1	1-8
A	JP, 4-224547, A (旭化成工業株式会社) 3. 8月. 1992 (03. 08. 92) (ファミリーなし)	1-8
A	JP, 4-230242, A (旭化成工業株式会社) 19. 8月. 1992 (19. 08. 92) (ファミリーなし)	1-8
A	JP, 4-235951, A (旭化成工業株式会社) 25. 8月. 1992 (25. 08. 92) (ファミリーなし)	1-8
A	JP, 6-116210, A (ダイセル化学工業株式会社) 26. 4月. 1994 (26. 04. 94) & EP, 591923, A & US, 5380908, A & TW, 239121, A & CN, 1089256, A	1-8
☒ C欄の続きにも文献が列挙されている。 ☐ パテントファミリーに関する別紙を参照。		
* 引用文献のカテゴリー 「A」 特に関連のある文献ではなく、一般的技術水準を示すもの 「E」 先行文献ではあるが、国際出願日以後に公表されたもの 「L」 優先権主張に疑義を提起する文献又は他の文献の発行日若しくは他の特別な理由を確立するために引用する文献 (理由を付す) 「O」 口頭による開示、使用、展示等に言及する文献 「P」 国際出願日前で、かつ優先権の主張の基礎となる出願 の日の後に公表された文献 「T」 国際出願日又は優先日後に公表された文献であって出願と矛盾するものではなく、発明の原理又は理論の理解のために引用するもの 「X」 特に関連のある文献であって、当該文献のみで発明の新規性又は進歩性がないと考えられるもの 「Y」 特に関連のある文献であって、当該文献と他の1以上の文献との、当業者にとって自明である組合せによって進歩性がないと考えられるもの 「&」 同一パテントファミリー文献		
国際調査を完了した日 03. 12. 96	国際調査報告の発送日 17.12.96	
国際調査機関の名称及びあて先 日本国特許庁 (ISA/J P) 郵便番号100 東京都千代田区霞が関三丁目4番3号	特許庁審査官 (権限のある職員) 脇村 善一 印	4 H 7 4 5 7
電話番号 03-3581-1101 内線 3443		

様式PCT/ISA/210 (第2ページの続き) (1992年7月)



(51) 国際特許分類6 C07C 69/96, 68/06	A1	(11) 国際公開番号 WO97/11049
		(43) 国際公開日 1997年3月27日(27.03.97)
(21) 国際出願番号 PCT/JP96/02734 (22) 国際出願日 1996年9月20日(20.09.96) (30) 優先権データ 特願平7/268036 1995年9月22日(22.09.95) JP (71) 出願人 (米国を除くすべての指定国について) 旭化成工業株式会社 (ASAHI KASEI KOGYO KABUSHIKI KAISHA)[JP/JP] 〒530 大阪府大阪市北区堂島浜1丁目2番6号 Osaka, (JP) (72) 発明者；および (75) 発明者／出願人 (米国についてのみ) 小宮強介(KOMIYA, Kyosuke)[JP/JP] 〒712 岡山県倉敷市神田2-7-12 Okayama, (JP) 東條正弘(TOJO, Masahiro)[JP/JP] 〒710 岡山県倉敷市東富井1005-1 旭化成大高アパート3-603 Okayama, (JP) 福岡伸典(FUKUOKA, Shinsuke)[JP/JP] 〒710 岡山県倉敷市吉岡359-11 Okayama, (JP)		(74) 代理人 弁理士 片桐光治(KATAGIRI, Mitsuji) 〒107 東京都港区赤坂4丁目3番1号 共同ビル赤坂312号 Tokyo, (JP) (81) 指定国 CA, CN, JP, KR, SG, US, 欧州特許 (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). 添付公開書類 国際調査報告書
(54)Title: PROCESS FOR THE PREPARATION OF AROMATIC CARBONATE (54)発明の名称 芳香族カーボネートの製造方法 (57) Abstract A process for the preparation of an aromatic carbonate by subjecting a starting compound selected from the group consisting of dialkyl carbonates, alkyl aryl carbonates and mixtures thereof and a reactant selected from the group consisting of aromatic mono-hydroxyl compounds, alkyl aryl carbonates and mixtures thereof to transesterification in the presence of a metal-containing catalyst, characterized in that the transesterification is conducted while keeping the weight ratio (WR) of at least one substance having an aromatic group selected from the group consisting of specific aromatic polyhydroxyl compounds resulting from the starting compound, the reactant and/or by-products of the transesterification and residues of them to the metal constituting the catalyst-containing liquid mixture of the transesterification system. According to this process, undesirable phenomena such as the deposition of the catalyst in reactors or pipes and the adhesion of the catalyst to them can be inhibited to thereby permit a stable preparation of an aromatic carbonate for a long period.		

(57) 要約

ジアルキルカーボネート、アルキルアリアルカーボネート及びそれらの混合物よりなる群から選ばれる出発物質と、芳香族モノヒドロキシ化合物、アルキルアリアルカーボネート及びそれらの混合物よりなる群から選ばれる反応物質とを金属含有触媒の存在下にエステル交換反応に付すことによって芳香族カーボネートを製造する方法において、出発物質、反応物質及び／又はエステル交換反応の副生成物に起因する特定の芳香族多価ヒドロキシ化合物及びその残基からなる群より選ばれる少なくとも1種の芳香族基含有物質の、触媒の金属に対する重量比(WR)を、エステル交換反応系内の触媒含有液相混合物について測定して2.0以下に維持しながら上記エステル交換反応を行うことを特徴とする方法が開示される。本発明の方法によれば、反応器や配管における触媒の析出や付着など、好ましくない現象の発生を防ぐことができ、それによって芳香族カーボネートを長期間安定に製造することができる。

情報としての用途のみ

PCTに基づいて公開される国際出願をパンフレット第一頁にPCT加盟国を同定するために使用されるコード

AL	アルバニア	EE	エストニア	LR	リベリア	RU	ロシア連邦
AM	アルメニア	ES	スペイン	LS	レソト	SD	スーダン
AT	オーストリア	FI	フィンランド	LT	リトアニア	SE	スウェーデン
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ABSTRACT

Disclosed is a process for producing an aromatic carbonate which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate, an alkyl aryl carbonate and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound, an alkyl aryl carbonate and a mixture thereof, wherein the transesterification is conducted while maintaining a weight ratio (WR) of at least one aromatic group-containing substance selected from the group consisting of a specific aromatic polyhydroxy compound and a residue thereof to the metal of the metal-containing catalyst at 2.0 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification, and wherein the aromatic group-containing substance originates from the starting material, the reactant and/or a by-product of the transesterification. According to the process of the present invention, the transesterification reaction can be conducted without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner walls of the reactor, pipes and the like, so that the desired aromatic carbonate can be produced stably for a prolonged period of time.

TITLE OF THE INVENTION

Process For Producing An Aromatic Carbonate

BACKGROUND OF THE INVENTIONField of The Invention

5 The present invention relates to a process for
producing an aromatic carbonate. More particularly,
the present invention is concerned with a process for
producing an aromatic carbonate which comprises transe-
sterifying, in the presence of a metal-containing
10 catalyst, a starting material selected from the group
consisting of a dialkyl carbonate, an alkyl aryl car-
bonate and a mixture thereof with a reactant selected
from the group consisting of an aromatic monohydroxy
compound, an alkyl aryl carbonate and a mixture there-
15 of, wherein the transesterification is conducted while
maintaining a weight ratio (WR) of at least one aromat-
ic group-containing substance selected from the group
consisting of a specific aromatic polyhydroxy compound
and a residue thereof to the metal of the metal-con-
20 taining catalyst at 2.0 or less, wherein the weight
ratio (WR) is measured with respect to a catalyst-
containing liquid-phase mixture in a system for the
transesterification, and wherein the aromatic group-
containing substance originates from the starting
25 material, the reactant and/or a by-product of the

transesterification. According to the process of the present invention, the transesterification reaction can be conducted without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner walls of the reactor, pipes and the like, so that the desired aromatic carbonate can be produced stably for a prolonged period of time.

10 Prior Art

An aromatic carbonate is useful as a raw material for, e.g., the production of an aromatic polycarbonate (whose utility as engineering plastics has been increasing in recent years) without using poisonous phosgene. With respect to the method for the production of an aromatic carbonate, a method for producing an aromatic carbonate or an aromatic carbonate mixture is known, in which a dialkyl carbonate, an alkyl aryl carbonate or a mixture thereof is used as a starting material and an aromatic monohydroxy compound, an alkyl aryl carbonate or a mixture thereof is used as a reactant, and in which a transesterification reaction is performed between the starting material and the reactant.

25 However, since this type of transesterification is

a reversible reaction in which, moreover, not only is the equilibrium biased toward the original system but the reaction rate is also low, the production of an aromatic carbonate by the above-mentioned method on an industrial scale is accompanied with great difficulties.

To improve the above-mentioned method, several proposals have been made, most of which relate to the development of a catalyst for increasing the reaction rate. As a catalyst for use in the method for producing an alkyl aryl carbonate, a diaryl carbonate or a mixture thereof by reacting a dialkyl carbonate with an aromatic hydroxy compound, there have been proposed various metal-containing catalysts, which include for example, a Lewis acid, such as a transition metal halide, or compounds capable of forming a Lewis acid, [see Unexamined Japanese Patent Application Laid-Open Specification No. 51-105032, Unexamined Japanese Patent Application Laid-Open Specification No. 56-123948 and Unexamined Japanese Patent Application Laid-Open Specification No. 56-123949 (corresponding to West German Patent Application Publication No. 2528412, British Patent No. 1499530 and U.S. Patent No. 4,182,726)], a tin compound, such as an organotin alkoxide or an organotin oxide [Unexamined Japanese Patent Application

Laid-Open Specification No. 54-48733 (corresponding to West German Patent Application Publication No. 2736062), Unexamined Japanese Patent Application Laid-Open Specification No. 54-63023, Unexamined Japanese Patent Application Laid-Open Specification No. 60-169444 (corresponding to U.S. Patent No. 4,554,110), Unexamined Japanese Patent Application Laid-Open Specification No. 60-169445 (corresponding to U.S. Patent No. 4,552,704), Unexamined Japanese Patent Application Laid-Open Specification No. 62-277345, and Unexamined Japanese Patent Application Laid-Open Specification No. 1-265063], salts and alkoxides of an alkali metal or an alkaline earth metal (Unexamined Japanese Patent Application Laid-Open Specification No. 56-25138), lead compounds (Unexamined Japanese Patent Application Laid-Open Specification No. 57-176932), complexes of a metal, such as copper, iron or zirconium (Unexamined Japanese Patent Application Laid-Open Specification No. 57-183745), titanilic acid esters [Unexamined Japanese Patent Application Laid-Open Specification No. 58-185536 (corresponding to U.S. Patent No. 4,410,464)], a mixture of a Lewis acid and protonic acid [Unexamined Japanese Patent Application Laid-Open Specification No. 60-173016 (corresponding to U.S. Patent No. 4,609,501)], a compound of Sc, Mo, Mn, Bi, Te or the

like [Unexamined Japanese Patent Application Laid-Open Specification No. 1-265064 (corresponding to European Patent Publication No. 0 338 760 A1 and U.S. Patent No. 5,034,557)], and ferric acetate (Unexamined Japanese Patent Application Laid-Open Specification No. 61-172852).

As a catalyst for use in the method for producing a diaryl carbonate by a same-species intermolecular transesterification, wherein an alkyl aryl carbonate is disproportionated to a diaryl carbonate and a dialkyl carbonate, there have been proposed various catalysts, which include for example, a Lewis acid and a transition metal compound which is capable of forming a Lewis acid [see Unexamined Japanese Patent Application Laid-Open Specification No. 51-75044 (corresponding to West German Patent Application Publication No. 2552907 and U.S. Patent No. 4,045,464)], a polymeric tin compound [Unexamined Japanese Patent Application Laid-Open Specification No. 60-169444 (corresponding to U.S. Patent No. 4,554,110 and West German Patent Application Publication No. 3445552)], a compound represented by the formula $R-X(=O)OH$ (wherein X is selected from Sn and Ti, and R is selected from monovalent hydrocarbon residues) [Unexamined Japanese Patent Application Laid-Open Specification No. 60-169445 (corresponding to U.S.

Patent No. 4,552,704)], a mixture of a Lewis acid and protonic acid [Unexamined Japanese Patent Application Laid-Open Specification No. 60-173016 (corresponding to U.S. Patent No. 4,609,501)], a lead catalyst (Unexamined Japanese Patent Application Laid-Open Specification No. 1-93560), a titanium or zirconium compound [Unexamined Japanese Patent Application Laid-Open Specification No. 1-265062 (corresponding to U.S. Patent No. 5,166,393)], a tin compound [Unexamined Japanese Patent Application Laid-Open Specification No. 1-265063 (corresponding to European Patent Publication No. 0 338 760 A1 and U.S. Patent No. 5,034,557)], and a compound of Sc, Mo, Mn, Bi, Te or the like [Unexamined Japanese Patent Application Laid-Open Specification No. 1-265064 (corresponding to European Patent Publication No. 0 338 760 A1 and U.S. Patent No. 5,034,557)].

Another attempt for improving the yield of aromatic carbonates in these reactions consists in biasing the equilibrium toward the product system as much as possible, by modifying the mode of the reaction process. For example, there have been proposed a method in which by-produced methanol is distilled off together with an azeotrope forming agent by azeotropic distillation in the reaction of a dimethyl carbonate with phenol [see Unexamined Japanese Patent Application Laid-Open Speci-

5 fication No. 54-48732 (corresponding to West German
Patent Application Publication No. 2736063 and U.S.
Patent No. 4,252,737) and Unexamined Japanese Patent
Application Laid-Open Specification No. 61-291545], and
a method in which by-produced methanol is removed by
adsorbing the same onto a molecular sieve [Unexamined
Japanese Patent Application Laid-Open Specification No.
58-185536 (corresponding to U.S. Patent No.
4,410,464)].

10 Further, a method is known in which an apparatus
comprising a reactor having provided on the top thereof
a distillation column is employed in order to separate
and distill off alcohols (by-produced in the course of
the reaction) from a reaction mixture obtained in the
15 reactor. [With respect to this method, reference can
be made to, for example, Unexamined Japanese Patent
Application Laid-Open Specification No. 56-123948
(corresponding to U.S. Patent No. 4,182,726), Unexam-
ined Japanese Patent Application Laid-Open Specifica-
20 tion No. 56-25138, Unexamined Japanese Patent Applica-
tion Laid-Open Specification No. 60-169444 (correspond-
ing to U.S. Patent No. 4,554,110), Unexamined Japanese
Patent Application Laid-Open Specification No. 60-
169445 (corresponding to U.S. Patent No. 4,552,704),
25 Unexamined Japanese Patent Application Laid-Open Speci-

fication No. 60-173016 (corresponding to U.S. Patent
No. 4,609,501), Unexamined Japanese Patent Application
Laid-Open Specification No. 61-172852, Unexamined
Japanese Patent Application Laid-Open Specification No.
5 61-291545, and Unexamined Japanese Patent Application
Laid-Open Specification No. 62-277345.]

As more preferred methods for producing an aromatic
carbonate, the present inventors previously developed
a method in which a dialkyl carbonate and an
10 aromatic hydroxy compound are continuously fed to a
continuous multi-stage distillation column to effect a
continuous transesterification reaction in the distil-
lation column, while continuously withdrawing a low
boiling point reaction mixture containing a by-produced
15 alcohol from an upper portion of the distillation
column by distillation and continuously withdrawing a
high boiling point reaction mixture containing a pro-
duced alkyl aryl carbonate from a lower portion of the
distillation column [see Unexamined Japanese Patent
20 Application Laid-Open Specification No. 3-291257
(corresponding to U.S. Patent No. 5,210,268 and Euro-
pean Patent Publication No. 0 461 274 B1)], and a
method in which an alkyl aryl carbonate is continuously
fed to a continuous multi-stage distillation column to
25 effect a continuous transesterification reaction in the

distillation column, while continuously withdrawing a low boiling point reaction mixture containing a by-produced dialkyl carbonate from an upper portion of the distillation column by distillation and continuously withdrawing a high boiling point reaction mixture containing a produced diaryl carbonate from a lower portion of the distillation column [see Unexamined Japanese Patent Application Laid-Open Specification No. 4-9358 (corresponding to U.S. Patent No. 5,210,268 and European Patent Publication No. 0 461 274 B1)]. These methods for the first time realized efficient, continuous production of an aromatic carbonate. Thereafter, various methods for continuously producing an aromatic carbonate have further been developed, based on the above-mentioned methods developed by the present inventors. Examples of these methods include a method in which a catalytic transesterification reaction is performed in a column reactor [see Unexamined Japanese Patent Application Laid-Open Specification No. 6-41022 (corresponding to West German Patent Application Publication No. 4218061, European Patent Publication No. 0 572 870 A1 and U.S. Patent No. 5,362,901), Unexamined Japanese Patent Application Laid-Open Specification No. 6-157424 (corresponding to West German Patent Application Publication No. 4226755, European Patent Publica-

tion No. 0 582 931 A1 and U.S. Patent No. 5,334,742),
Unexamined Japanese Patent Application Laid-Open Specifi-
cation No. 6-184058 (corresponding to West German
Patent Application Publication No. 4226756, European
5 Patent Publication No. 0 582 930 A1 and U.S. Patent No.
5,344,954)], a method in which use is made of a plural-
ity of reactors which are connected in series [Unexam-
ined Japanese Patent Application Laid-Open Specifica-
tion No. 6-234707 (corresponding to West German Patent
10 Application Publication No. 4301899, European Patent
Publication No. 0 608 710 A1 and U.S. Patent No.
5,463,102), and Unexamined Japanese Patent Application
Laid-Open Specification No. 6-263694], a method in
which a bubble tower reactor is used [Unexamined Ja-
15 panese Patent Application Laid-Open Specification No.
6-298700 (corresponding to West German Patent Applica-
tion Publication No. 4316428, European Patent Publica-
tion No. 0 614 877 A1 and U.S. Patent No. 5,523,451)],
and a method in which a vertically long reactor vessel
20 is used (Unexamined Japanese Patent Application Laid-
Open Specification No. 6-345697).

Also, there have been proposed methods for produc-
ing an aromatic carbonate stably for a prolonged period
of time on a commercial scale. For example, Unexamined
25 Japanese Patent Application Laid-Open Specification No.

6-157410 (corresponding to European Patent Publication
No. 0 591 923 A1 and U.S. Patent No. 5,380,908) dis-
closes a method for producing aromatic carbonates
from a dialkyl carbonate and an aromatic hydroxy com-
pound, which comprises continuously supplying a mixture
of raw materials and a catalyst to a reactor provided
with a distillation column thereon to effect a transe-
sterification reaction in the reactor, while continu-
ously withdrawing a by-produced aliphatic alcohol from
the reactor through the distillation column by distil-
lation so as to keep the aliphatic alcohol concentra-
tion of the reaction system at 2 % by weight or less.
This prior art document describes that, by this method,
continuous production of an aromatic carbonate can be
performed in a stable manner. The object of this
method is to avoid the deposition of the catalyst in
the distillation column. However, the reason for the
deposition of the catalyst in the distillation column
to be able to be avoided by this method is very simple
and resides in that the catalyst is not fed to the
distillation column. This prior art document describes
the effect that since the catalyst was fed only to the
reactor, no clogging was observed in the distillation
column. This document also describes that, when a
catalyst is fed to the distillation column, clogging of

a part of the distillation column occurs due to the deposition of the catalyst in the column. In view of the fact that, in this method, a catalyst is not fed to the distillation column, it is natural and not surprising that the deposition of the catalyst does not occur in the distillation column. In addition, in view of the fact that, in this method, a catalyst is not fed to the distillation column, it is also apparent that, by this method, it is impossible to efficiently conduct a reaction by feeding a catalyst to a distillation column (that is, it is impossible to conduct a reactive distillation by this method). Further, this prior art document does not teach or suggest any solution for the problem where a catalyst is deposited from a catalyst-containing liquid-phase mixture and the deposited catalyst adheres to a reactor, pipes, valves, means for separating the catalyst from the liquid phase, and the like in the system for transesterification. In this prior art document, the reason why the aliphatic alcohol concentration of the reaction system should be kept at 2 % by weight or less is not explained. However, it is presumed that the aliphatic alcohol concentration requirement of 2 % by weight or less is intended to bias the equilibrium toward the product system so that the reaction proceeds efficiently. In this prior art

document, there is no description regarding the relationship between the aliphatic alcohol concentration and the deposition of a catalyst.

Unexamined Japanese Patent Application Laid-Open Specification No. 6-116210 (corresponding to European Patent Publication No. 0 591 923 A1 and U.S. Patent No. 5,380,908) discloses a method for producing a diaryl carbonate from an alkyl aryl carbonate, which comprises continuously supplying a mixture of raw materials and a catalyst to a reactor provided with a distillation column thereon to effect a transesterification reaction in the reactor, while continuously withdrawing a by-produced dialkyl carbonate from the reactor through the distillation column by distillation so as to keep the dialkyl carbonate concentration of the reaction system at 2 % by weight or less. This prior art document describes that, by this method, continuous production of a diaryl carbonate can be performed in a stable manner. The object of this method is to avoid the deposition of the catalyst in the distillation column. However, the reason why the deposition of the catalyst in the distillation column is able to be avoided by this method is very simple and resides in that the catalyst is not fed to the distillation column. This prior art document describes the effect that since the

catalyst was fed only to the reactor, no clogging was observed in the distillation column. This document also describes that, when a catalyst is fed to the distillation column, clogging of a part of the distillation column occurs due to the deposition of the catalyst in the column. In view of the fact that, in this method, a catalyst is not fed to the distillation column, it is natural and not surprising that the deposition of the catalyst does not occur in the distillation column. In addition, in view of the fact that, in this method, a catalyst is not fed to the distillation column, it is also apparent that, by this method, it is impossible to efficiently conduct a reaction by feeding a catalyst to a distillation column (that is, it is impossible to conduct a reactive distillation by this method). Further, this prior art document does not teach or suggest any solution for the problem where a catalyst is deposited from a catalyst-containing liquid-phase mixture and the deposited catalyst adheres to a reactor, pipes, valves, means for separating the catalyst from the liquid phase, and the like in the system for transesterification.

When a catalyst is deposited from a catalyst-containing liquid-phase mixture and the deposited catalyst adheres to the inner walls of a reactor, pipes

and the like, the reaction is adversely affected. That is, the deposited catalyst which is adhered to the inner walls of the reactor, pipes and the like cannot exhibit effective catalyst activity, even if it is present in the reactor. The deposition of the catalyst and the adhesion of the deposited catalyst to portions in the system for the transesterification means that the amount of the effective catalyst present in the reactor is decreased, so that the reaction cannot achieve favorable results.

SUMMARY OF THE INVENTION

In these situations, for solving the above-mentioned problems accompanying the prior art, the present inventors made extensive and intensive studies with a view toward developing an improvement in a process for producing an aromatic carbonate which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate, an alkyl aryl carbonate and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound, an alkyl aryl carbonate and a mixture thereof. As a result, it has surprisingly been found that this task can be easily attained by conducting the transesterification while maintaining a weight ratio

(WR) of at least one aromatic group-containing substance selected from the group consisting of an aromatic polyhydroxy compound and a residue thereof to the metal of the metal-containing catalyst at 2 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification, and wherein the aromatic group-containing substance originates from the starting material, the reactant and/or a by-product of the transesterification. The present invention has been completed, based on the above finding.

Accordingly, it is a primary object of the present invention to provide an improved process for producing an aromatic carbonate, which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate, an alkyl aryl carbonate and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound, an alkyl aryl carbonate and a mixture thereof, which improved process can be used for producing an aromatic carbonate without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner walls of the

reactor, pipes and the like, so that the desired aromatic carbonate can be produced stably for a prolonged period of time.

The foregoing and other objects, features and advantages of the present invention will be apparent from the following detailed description and appended claims taken in connection with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

Fig. 1 is a diagram showing an example of systems for practicing the process of the present invention;

Fig. 2 is a diagram showing another example of systems for practicing the process of the present invention;

Fig. 3 is a diagram showing a further example of systems for practicing the process of the present invention; and

Fig. 4 is a diagram showing still a further example of systems for practicing the process of the present invention.

In Fig. 1 through Fig. 4, like parts or portions are designated by like numerals.

Description of Reference Numerals

1, 101: continuous multi-stage distillation

column

2, 102: top of the continuous multi-stage distillation column

6, 106: bottom of the continuous multi-stage distillation column

24: distillation column

100: reaction vessel

3, 5, 7, 9, 10, 12, 13, 15, 16, 18, 19, 20, 21, 23, 25, 27, 28, 29, 30, 32, 105, 113, 115, 116, 118, 119, 120, 121, 123, 124, 125, 127, 128, 129, 130, 132, 224: conduit

4: preheater

8, 14, 114: evaporator

11, 22, 26, 122, 126: condenser

17, 31, 117, 131: reboiler

DETAILED DESCRIPTION OF THE INVENTION

In the present invention, there is provided a process for producing an aromatic carbonate which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate represented by the following formula (1):



an alkyl aryl carbonate represented by the following

formula (2):



and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound represented by the following formula (3):



an alkyl aryl carbonate represented by the following formula (4):



and a mixture thereof,

wherein each of R^1 , R^2 and R^3 independently represents an alkyl group having 1 to 10 carbon atoms, an alicyclic group having 3 to 10 carbon atoms or an aralkyl group having 6 to 10 carbon atoms and each of Ar^1 , Ar^2 and Ar^3 independently represents an aromatic

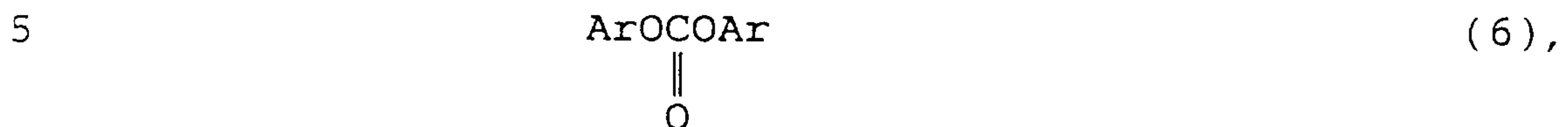
group having 5 to 30 carbon atoms,

to thereby produce at least one aromatic carbonate selected from the group consisting of an alkyl aryl carbonate and a diaryl carbonate, which is selected in correspondence to the starting material and the reactant and represented by at least one formula selected from the group consisting of the following formulae (5)

and (6):



and



wherein R and Ar are, respectively, selected from R^1 , R^2 and R^3 and selected from Ar^1 , Ar^2 and Ar^3 in correspondence to the starting material and the reactant,

characterized in that the transesterification is conducted while maintaining a weight ratio (WR) of at least one aromatic group-containing substance selected from the group consisting of an aromatic polyhydroxy compound and a residue thereof to the metal of the metal-containing catalyst at 2.0 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification, and wherein the aromatic group-containing substance originates from at least one member selected from the group consisting of the starting material, the reactant and a by-product of the transesterification,

the aromatic polyhydroxy compound being represented by the following formula (7):



wherein Ar^4 represents an aromatic group having a valence of m , m represents an integer of 2 or more, and each $-\text{OH}$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group, and the residue of the aromatic polyhydroxy compound being represented by the following formula (8):



wherein Ar^4 and m are as defined above, n represents an integer of from 1 to m , and each of the $-\text{OH}$ group and the $-\text{O}-$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group, and being present in such a form as chemically bonded to at least one member selected from the group consisting of the metal of the catalyst, an alkoxycarbonyl group derived from the dialkyl carbonate or the alkyl aryl carbonate, an aryloxycarbonyl group derived from the alkyl aryl carbonate or the diaryl carbonate, and a carbonyl group derived from the dialkyl carbonate, the alkyl aryl carbonate or the diaryl carbonate.

For an easy understanding of the present invention, the essential features and various preferred embodiments of the present invention are enumerated

below.

1. In a process for producing an aromatic carbonate which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate represented by the following formula (1):



an alkyl aryl carbonate represented by the following formula (2):



and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound represented by the following formula (3):



an alkyl aryl carbonate represented by the following formula (4):



and a mixture thereof,

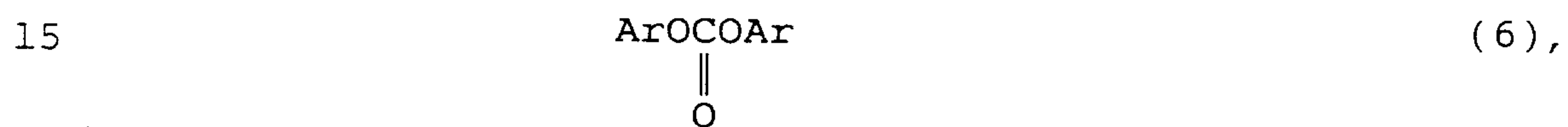
wherein each of R^1 , R^2 and R^3 independently represents an alkyl group having 1 to 10 carbon atoms, an alicyclic group having 3 to

10 carbon atoms or an aralkyl group having 6
to 10 carbon atoms and each of Ar^1 , Ar^2 and
 Ar^3 independently represents an aromatic
group having 5 to 30 carbon atoms,

5 to thereby produce at least one aromatic carbonate
selected from the group consisting of an alkyl aryl
carbonate and a diaryl carbonate, which is selected in
correspondence to the starting material and the react-
ant and represented by at least one formula selected
10 from the group consisting of the following formulae (5)
and (6):



and



wherein R and Ar are, respectively, selected
from R^1 , R^2 and R^3 and selected from Ar^1 ,
 Ar^2 and Ar^3 in correspondence to the start-
20 ing material and the reactant,
the improvement being that the transesterification is
conducted while maintaining a weight ratio (WR) of at
least one aromatic group-containing substance selected
from the group consisting of an aromatic polyhydroxy
25 compound and a residue thereof to the metal of the

metal-containing catalyst at 2.0 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification, and wherein the aromatic group-containing substance originates from at least one member selected from the group consisting of the starting material, the reactant and a by-product of the transesterification,

the aromatic polyhydroxy compound being represented by the following formula (7):



wherein Ar^4 represents an aromatic group having a valence of m , m represents an integer of 2 or more, and each $-\text{OH}$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group, and

the residue of the aromatic polyhydroxy compound being represented by the following formula (8):



wherein Ar^4 and m are as defined above, n represents an integer of from 1 to m , and each of the $-\text{OH}$ group and the $-\text{O}-$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group,

and being present in such a form as chemically bonded

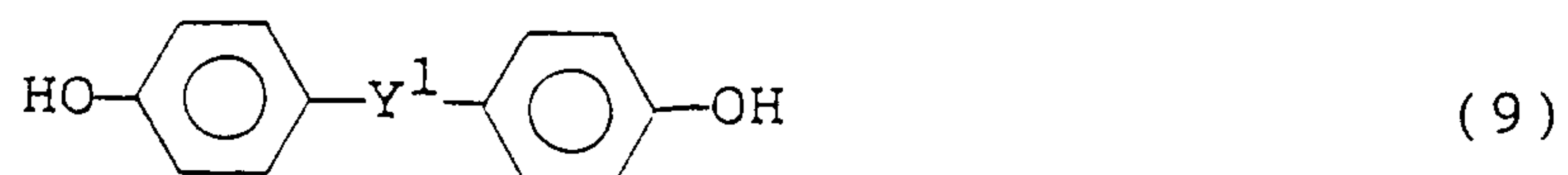
to at least one member selected from the group consisting of the metal of the catalyst, an alkoxycarbonyl group derived from the dialkyl carbonate or the alkyl aryl carbonate, an aryloxycarbonyl group derived from the alkyl aryl carbonate or the diaryl carbonate, and a carbonyl group derived from the dialkyl carbonate, the alkyl aryl carbonate or the diaryl carbonate.

2. The process according to item 1 above, wherein the aromatic polyhydroxy compound is at least one member selected from the group consisting of:

(A) an oxidation product of an aromatic monohydroxy compound as the reactant,

(B) at least one member selected from the group consisting of a product produced by the Fries rearrangement of a diaryl carbonate obtained by the transesterification and an oxidation product of the product and

(C) at least one member selected from the group consisting of aromatic dihydroxy compounds derived from phenol as the reactant and represented by the following formula (9):



wherein Y^1 represents a single bond, a
divalent alkane group having 1 to 30 carbon
atoms or a divalent group selected from -O-,
5 -CO-, -S-, -SO₂-, -SO- and -COO-, and
oxidation products of the aromatic dihydroxy compounds.

3. The process according to item 1 or 2 above, wher-
ein the maintenance of the weight ratio (WR) at 2.0 or
10 less is performed by using as the reactant an aromatic
monohydroxy compound containing the aromatic polyhy-
droxy compound in a controlled concentration, and
withdrawing a part of the catalyst-containing liquid-
phase mixture out of the system for the transesterifi-
15 cation.

4. The process according to item 3 above, wherein the
aromatic monohydroxy compound has an aromatic polyhy-
droxy compound concentration of 400 ppm by weight or
20 less.

5. The process according to item 1 above, which is
for continuously producing the at least one aromatic
carbonate, wherein a transesterification reaction
25 mixture containing the at least one aromatic carbonate

and containing the catalyst is continuously withdrawn from a reactor for the transesterification.

5 6. The process according to item 5 above, wherein the aromatic monohydroxy compound as the reactant comprises a mixture of a feedstock aromatic monohydroxy compound and an unreacted aromatic monohydroxy compound recycled from the reactor, wherein the feedstock aromatic monohydroxy compound has an aromatic polyhydroxy compound
10 concentration of 400 ppm by weight or less.

 7. The process according to item 5 or 6 above, wherein a part of the reaction mixture, containing the catalyst, withdrawn from the reactor is subjected to
15 evaporation, and the resultant mixture having an increased catalyst concentration is at least partly withdrawn out of the system for the transesterification to thereby maintain the weight ratio (WR) at 2.0 or less.

20

 8. The process according to any one of items 5 to 7 above, wherein the starting material and the reactant are continuously fed to a continuous multi-stage distillation column to effect a transesterification reaction
25 therebetween in at least one phase selected from a

liquid phase and a gas-liquid phase in the presence of the metal-containing catalyst in the distillation column, while continuously withdrawing a high boiling point reaction mixture containing the at least one aromatic carbonate in a liquid form from a lower portion of the distillation column and continuously withdrawing a low boiling point reaction mixture containing a by-product in a gaseous form from an upper portion of the distillation column by distillation.

The present invention is described below in detail.

The dialkyl carbonate to be used as a starting material in the present invention is represented by formula (1):



wherein R^1 represents an alkyl group having 1 to 10 carbon atoms, an alicyclic group having 3 to 10 carbon atoms or an aralkyl group having 6 to 10 carbon atoms. Examples of R^1 include an alkyl group, such as methyl, ethyl, propyl (isomers), allyl, butyl (isomers), butenyl (isomers), pentyl (isomers), hexyl (isomers), heptyl (isomers), octyl (isomers), nonyl (isomers), decyl (isomers) and cyclohexylmethyl; an alicyclic

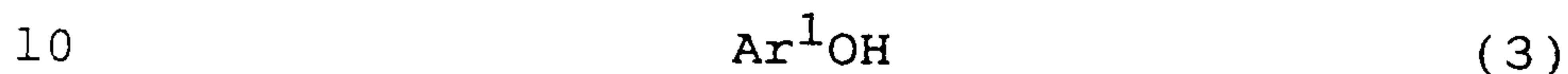
group, such as cyclopropyl, cyclobutyl, cyclopentyl, cyclohexyl and cycloheptyl; and an aralkyl group, such as benzyl, phenethyl (isomers), phenylpropyl (isomers), phenylbutyl (isomers) and methylbenzyl (isomers). The
5 above-mentioned alkyl group, alicyclic group and aralkyl group may be substituted with a substituent, such as a lower alkyl group, a lower alkoxy group, a cyano group and a halogen atom, as long as the number of carbon atoms of the substituted group does not exceed
10 10, and may also contain an unsaturated bond.

As a dialkyl carbonate having such R^1 , there may be mentioned for example, dimethyl carbonate, diethyl carbonate, dipropyl carbonate (isomers), diallyl carbonate, dibutenyl carbonate (isomers), dibutyl carbonate (isomers),
15 dipentyl carbonate (isomers), dihexyl carbonate (isomers), diheptyl carbonate (isomers), dioctyl carbonate (isomers), dinonyl carbonate (isomers), didecyl carbonate (isomers), dicyclopentyl carbonate, dicyclohexyl carbonate, dicycloheptyl carbonate,
20 dibenzyl carbonate, diphenethyl carbonate (isomers), di(phenylpropyl) carbonate (isomers), di(phenylbutyl) carbonate (isomers), di(chlorobenzyl) carbonate (isomers), di(methoxybenzyl) carbonate (isomers), di(methoxymethyl) carbonate, di(methoxyethyl) carbonate
25 (isomers), di(chloroethyl) carbonate (isomers) and

di(cyanoethyl) carbonate (isomers). These dialkyl carbonates can also be used in mixture.

Of these dialkyl carbonates, a dialkyl carbonate containing as R^1 a lower alkyl group having 4 or less carbon atoms is preferably used. Most preferred is dimethyl carbonate.

The aromatic monohydroxy compound used as the reactant in the present invention is represented by formula (3):



wherein Ar^1 represents an aromatic group having 5 to 30 carbon atoms, and the type of the compound is not limited as long as the hydroxyl group is directly bonded to the aromatic group.

15 Illustrative examples of Ar^1 in formula (3) include:

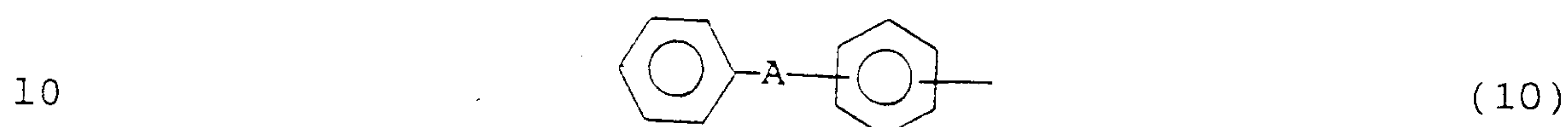
a phenyl group and various alkylphenyl groups, such as phenyl, tolyl (isomers), xylyl (isomers), trimethylphenyl (isomers), tetramethylphenyl (isomers), ethylphenyl (isomers), propylphenyl (isomers), butylphenyl (isomers), diethylphenyl (isomers), methylethylphenyl (isomers), pentylphenyl (isomers), hexylphenyl (isomers) and cyclohexylphenyl (isomers);

25 various alkoxyphenyl groups, such as methoxyphenyl (isomers), ethoxyphenyl (isomers) and butoxyphenyl

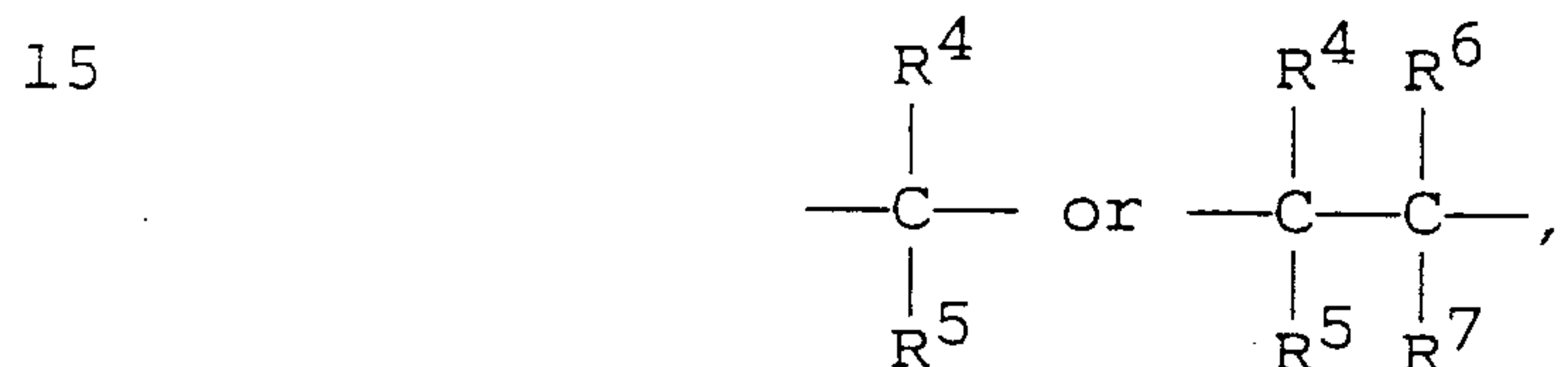
(isomers);

various halogenated phenyl groups, such as fluoro-phenyl (isomers), chlorophenyl (isomers), bromophenyl (isomers), chloromethylphenyl (isomers) and dichloro-phenyl (isomers);

various substituted phenyl groups represented by the formula (10):



wherein A represents a bond, a divalent group, such as -O-, -S-, -CO- or -SO₂-, an alkylene group, a substituted alkylene group of the following formula:



wherein each of R⁴, R⁵, R⁶ and R⁷ independently represents a hydrogen atom; or a lower alkyl group, a cycloalkyl group, an aryl group or an aralkyl group, which may be substituted with a halogen atom or an alkoxy group,

or a cycloalkylene group of the following formula:

25



5 wherein k is an integer of from 3 to 11, and
 the hydrogen atoms may be replaced by a
 lower alkyl group, an aryl group, a halogen
 atom or the like, and

 the aromatic ring in formula (3) may be substituted
 10 with a substituent, such as a lower alkyl group, a
 lower alkoxy group, an ester group, a hydroxyl group, a
 nitro group, a halogen atom and a cyano group;

 a naphthyl group and various substituted naphthyl
 groups, such as naphthyl (isomers), methylnaphthyl
 15 (isomers), dimethylnaphthyl (isomers), chloronaphthyl
 (isomers), methoxynaphthyl (isomers) and cyanonaphthyl
 (isomers); and

 various unsubstituted or substituted heteroaromat-
 ic groups, such as pyridyl (isomers), cumaryl
 20 (isomers), quinolyl (isomers), methylpyridyl (isomers),
 chloropyridyl (isomers), methylcumaryl (isomers) and
 methylquinolyl (isomers).

 Preferred examples of aromatic monohydroxy com-
 pounds of formula (3) include phenol; various alkyl-
 25 phenols, such as cresol (isomers), xlenol (isomers),

trimethylphenol (isomers), tetramethylphenol (isomers),
ethylphenol (isomers), propylphenol (isomers), butylphenol (isomers), diethylphenol (isomers), methylethylphenol (isomers), methylpropylphenol (isomers),
5 dipropylphenol (isomers), methylbutylphenol (isomers),
pentylphenol (isomers), hexylphenol (isomers) and
cyclohexylphenol (isomers); various alkoxyphenols, such
as methoxyphenol (isomers) and ethoxyphenol (isomers);
various substituted phenols represented by the follow-
10 ing formula (11):



wherein A is as defined above;

15 naphthol (isomers) and various substituted naphthols;
and heteroaromatic monohydroxy compounds, such as
hydroxypyridine (isomers), hydroxycumarine (isomers)
and hydroxyquinoline (isomers). These aromatic monohydroxy
compounds can also be used in mixture.

20 Of these aromatic monohydroxy compounds, an aromatic monohydroxy compound containing as Ar¹ an aromatic group having 6 to 10 carbon atoms is preferably used in the present invention, and phenol is most preferred.

The alkyl aryl carbonate used as the starting
25 material in the present invention is represented by the

following formula (2):



wherein R^2 may be identical with or different from R^1 ,
 5 and represents an alkyl group having 1 to 10 carbon
 atoms, an alicyclic group having 3 to 10 carbon atoms
 or an aralkyl group having 6 to 10 carbon atoms; and
 Ar^2 may be identical with or different from Ar^1 , and
 represents an aromatic group having 5 to 30 carbon
 10 atoms. As R^2 , there may be mentioned, for example, the
 same groups as set forth above for R^1 . As Ar^2 , there
 may be mentioned, for example, the same groups as set
 forth above for Ar^1 .

Representative examples of alkyl aryl carbonate
 15 having these R^2 and Ar^2 include methyl phenyl car-
 bonate, ethyl phenyl carbonate, propyl phenyl carbonate
 (isomers), allyl phenyl carbonate, butyl phenyl car-
 bonate (isomers), pentyl phenyl carbonate (isomers),
 hexyl phenyl carbonate (isomers), heptyl phenyl car-
 20 bonate (isomers), octyl tolyl carbonate (isomers),
 nonyl ethylphenyl carbonate (isomers), decyl butyl-
 phenyl carbonate (isomers), methyl tolyl carbonate
 (isomers), ethyl tolyl carbonate (isomers), propyl
 tolyl carbonate (isomers), butyl tolyl carbonate
 25 (isomers), allyl tolyl carbonate (isomers), methyl

xylyl carbonate (isomers), methyl trimethylphenyl carbonate (isomers), methyl chlorophenyl carbonate (isomers), methyl nitrophenyl carbonate (isomers), methyl methoxyphenyl carbonate (isomers), methyl cumyl carbonate (isomers), methyl naphthyl carbonate (isomers), methyl pyridyl carbonate (isomers), ethyl cumyl carbonate (isomers), methyl benzoylphenyl carbonate (isomers), ethyl xylyl carbonate (isomers), benzyl xylyl carbonate (isomers). These alkyl aryl carbonates can also be used in mixture. Of these alkyl aryl carbonates, one containing as R^2 an alkyl group having 1 to 4 carbon atoms and as Ar^2 an aromatic group having 6 to 10 carbon atoms is preferably used, and methyl phenyl carbonate is most preferred.

The alkyl aryl carbonate used as the reactant in the present invention is represented by the following formula (4):



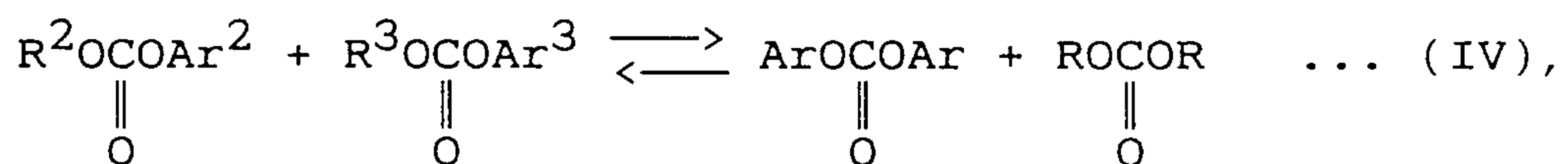
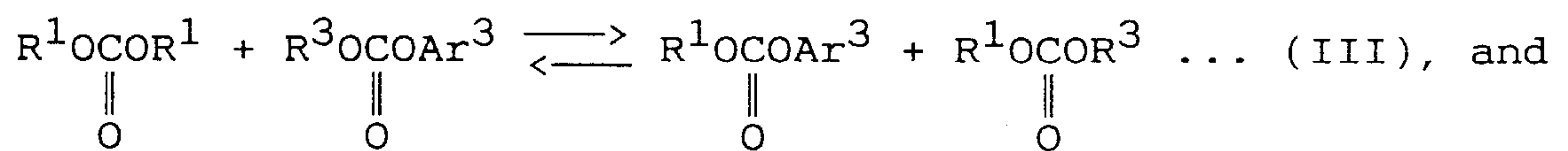
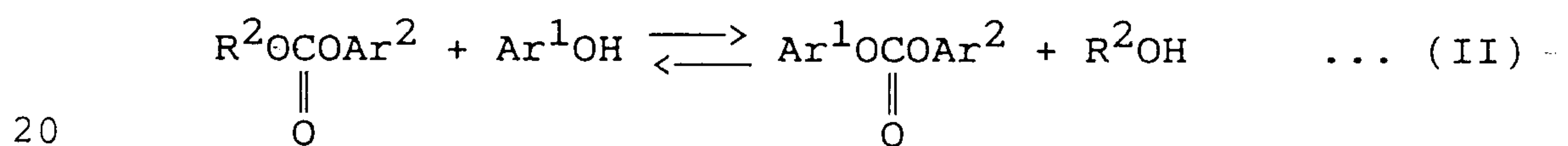
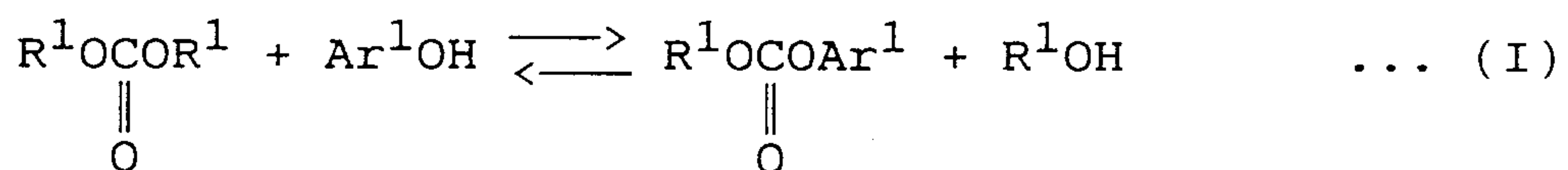
wherein R^3 may be identical with or different from R^1 and R^2 , and represents an alkyl group having 1 to 10 carbon atoms, as alicyclic group having 3 to 10 carbon atoms or an aralkyl group having 6 to 10 carbon atoms; and Ar^3 may be identical with or different from Ar^1 and Ar^2 , and represents an aromatic group having 5 to 30

carbon atoms. As R^3 , there may be mentioned, for example, the same groups as set forth above for R^1 . As Ar^3 , there may be mentioned, for example, the same groups as set forth above for Ar^1 .

5 As alkyl aryl carbonates having these R^3 and Ar^3 , there may be mentioned for example, those which are set forth above for alkyl aryl carbonates represented by the above-mentioned formula (2).

10 Of these alkyl aryl carbonates, one containing as R^3 an alkyl group having 1 to 4 carbon atoms and as Ar^3 an aromatic group having 6 to 10 carbon atoms is preferably used, and methyl phenyl carbonate is most preferred.

15 The typical reactions which are involved in the process of the present invention are represented by the following formulae:



25 wherein R^1 , R^2 , R^3 , Ar^1 , Ar^2 and Ar^3 are as defined

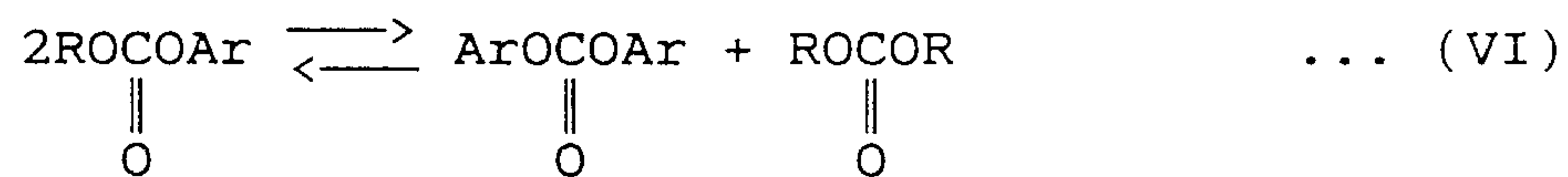
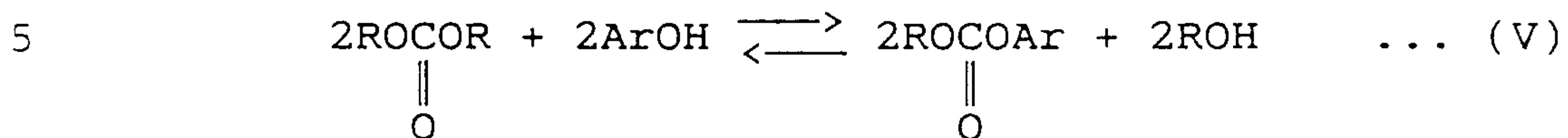
above, each of Ar's appearing in formula (IV) independently represents Ar^2 or Ar^3 , and each of R's appearing in formula (IV) independently represents R^2 or R^3 , and wherein when $\text{R}^2 = \text{R}^3$ and $\text{Ar}^2 = \text{Ar}^3$ in formula (IV), the reaction is a same-species intermolecular transesterification reaction generally known as a disproportionation reaction.

When each of the reactions of formulae (I), (II), (III) and (IV) is performed according to the process of the present invention, dialkyl carbonates or alkyl aryl carbonates as the starting materials for the reaction can be used individually or in mixture and aromatic monohydroxy compounds or alkyl aryl carbonates as the reactants for the reaction can be used individually or in mixture.

When $\text{R}^2 = \text{R}^3 = \text{R}$ and $\text{Ar}^2 = \text{Ar}^3 = \text{Ar}$ in the transesterification reaction of formula (IV), a diaryl carbonate and a dialkyl carbonate can be obtained by a same-species intermolecular transesterification reaction of a single type of alkyl aryl carbonate. This is a preferred embodiment of the present invention.

Further, when $\text{R}^1 = \text{R}^2 = \text{R}^3 = \text{R}$ and $\text{Ar}^1 = \text{Ar}^2 = \text{Ar}^3 = \text{Ar}$ in formulae (I) and (IV), by combining the reaction of formula (I) with the reaction of formula (IV), a diaryl carbonate can be obtained from a dialkyl carbonate and

an aromatic monohydroxy compound through an alkyl aryl carbonate as shown in formulae (V) and (VI). This is an especially preferred embodiment of the present invention.



10 Recycling of the dialkyl carbonate by-produced in the reaction of formula (VI) as the starting material for the reaction of formula (V) results in the formation of 1 mol. of a diaryl carbonate and 2 mol. of an aliphatic alcohol from 1 mol. of a dialkyl carbonate and 2 mol. of an aromatic monohydroxy compound.

15 When $\text{R}=\text{CH}_3$ and $\text{Ar}=\text{C}_6\text{H}_5$ in the above formulae (V) and (VI), diphenyl carbonate, which is an important raw material for a polycarbonate and an isocyanate, can be readily obtained from dimethyl carbonate, which is the simplest form of a dialkyl carbonate, and phenol. This
20 is especially important.

The metal-containing catalyst used in the present invention is one capable of promoting the reactions of formulae (I) to (IV). As such metal-containing catalysts, there may be mentioned for example:

(lead compounds)

lead oxides, such as PbO , PbO_2 and Pb_3O_4 ; lead sulfides, such as PbS and Pb_2S ; lead hydroxides, such as $\text{Pb}(\text{OH})_2$ and $\text{Pb}_2\text{O}_2(\text{OH})_2$; plumbites, such as Na_2PbO_2 , K_2PbO_2 , NaHPbO_2 and KHPbO_2 ; plumbates, such as Na_2PbO_3 , $\text{Na}_2\text{H}_2\text{PbO}_4$, K_2PbO_3 , $\text{K}_2[\text{Pb}(\text{OH})_6]$, K_4PbO_4 , Ca_2PbO_4 and CaPbO_3 ; lead carbonates and basic salts thereof, such as PbCO_3 and $2\text{PbCO}_3 \cdot \text{Pb}(\text{OH})_2$; lead salts of organic acids, and carbonates and basic salts thereof, such as $\text{Pb}(\text{OCOCH}_3)_2$, $\text{Pb}(\text{OCOCH}_3)_4$ and $\text{Pb}(\text{OCOCH}_3)_2 \cdot \text{PbO} \cdot 3\text{H}_2\text{O}$; organolead compounds, such as Bu_4Pb , Ph_4Pb , Bu_3PbCl , Ph_3PbBr , Ph_3Pb (or Ph_6Pb_2), Bu_3PbOH and Ph_3PbO wherein Bu represents a butyl group and Ph represents a phenyl group; alkoxylead compounds and aryloxylead compounds, such as $\text{Pb}(\text{OCH}_3)_2$, $(\text{CH}_3\text{O})\text{Pb}(\text{OPh})$ and $\text{Pb}(\text{OPh})_2$; lead alloys, such as Pb-Na, Pb-Ca, Pb-Ba, Pb-Sn and Pb-Sb; lead minerals, such as galena and zinc blende; and hydrates of these lead compounds;

(copper family metal compounds)

salts or complexes of copper family metals, such as CuCl , CuCl_2 , CuBr , CuBr_2 , CuI , CuI_2 , $\text{Cu}(\text{OAc})_2$, $\text{Cu}(\text{acac})_2$, copper oleate, Bu_2Cu , $(\text{CH}_3\text{O})_2\text{Cu}$, AgNO_3 , AgBr , silver picrate, $\text{AgC}_6\text{H}_6\text{ClO}_4$, $\text{Ag}(\text{bullvalene})_3\text{NO}_3$, $[\text{AuC}\equiv\text{C}-\text{C}(\text{CH}_3)_3]_n$ and $[\text{Cu}(\text{C}_7\text{H}_8)\text{Cl}]_4$ wherein OAc represents an acetyl group and acac represents an acetylac-

tone chelate ligand;

(alkali metal complexes)

alkali metal complexes, such as $\text{Li}(\text{acac})$ and
 $\text{LiN}(\text{C}_4\text{H}_9)_2$;

5 (zinc complexes)

zinc complexes, such as $\text{Zn}(\text{acac})_2$;

(cadmium complexes)

cadmium complexes, such as $\text{Cd}(\text{acac})_2$;

(iron family metal compounds)

10 iron family metal complexes, such as

$\text{Fe}(\text{C}_{10}\text{H}_8)(\text{CO})_5$, $\text{Fe}(\text{CO})_5$, $\text{Fe}(\text{C}_3\text{H}_6)(\text{CO})_3$, $\text{Co}(\text{mesitylene})_2(\text{PEt}_2\text{Ph})_2$, $\text{CoC}_5\text{F}_5(\text{CO})_2$, $\text{Ni}-\pi-\text{C}_5\text{H}_5\text{NO}$ and ferrocene;

(zirconium complexes)

15 zirconium complexes, such as $\text{Zr}(\text{acac})_4$ and zirconocene;

(Lewis acids and Lewis acid-forming compounds)

Lewis acids and Lewis acid-forming transition metal compounds, such as AlX_3 , TiX_3 , TiX_4 , VOX_3 , VX_5 ,
 20 ZnX_2 , FeX_3 and SnX_4 wherein X represents a halogen atom, an acetoxy group, an alkoxy group or an aryloxy group; and

(organotin compounds)

organotin compounds, such as $(\text{CH}_3)_3\text{SnOCOCH}_3$,

25 $(\text{C}_2\text{H}_5)_3\text{SnOCOC}_6\text{H}_5$, $\text{Bu}_3\text{SnOCOCH}_3$, $\text{Ph}_3\text{SnOCOCH}_3$,

$\text{Bu}_2\text{Sn}(\text{OCOCH}_3)_2$, $\text{Bu}_2\text{Sn}(\text{OCOC}_{11}\text{H}_{23})_2$, $\text{Ph}_3\text{SnOCH}_3$,
 $(\text{C}_2\text{H}_5)_3\text{SnOPh}$, $\text{Bu}_2\text{Sn}(\text{OCH}_3)_2$, $\text{Bu}_2\text{Sn}(\text{OC}_2\text{H}_5)_2$, $\text{Bu}_2\text{Sn}(\text{OPh})_2$,
 $\text{Ph}_2\text{Sn}(\text{OCH}_3)_2$, $(\text{C}_2\text{H}_5)_3\text{SnOH}$, Ph_3SnOH , Bu_2SnO ,
 $(\text{C}_8\text{H}_{17})_2\text{SnO}$, Bu_2SnCl_2 and $\text{BuSnO}(\text{OH})$.

5 These catalysts are effective even when they are
reacted with an organic compound present in the reac-
tion system, such as an aliphatic alcohol, an aromatic
monohydroxy compound, an alkyl aryl carbonate, a diaryl
carbonate and a dialkyl carbonate. Those which are
10 obtained by heat-treating these catalysts together with
a starting material, a reactant and/or a reaction
product thereof prior to the use in the process of the
present invention can also be used.

 It is preferred that the metal-containing catalyst
15 have high solubility in the liquid phase of the reac-
tion system. Preferred examples of metal-containing
catalysts include Pb compounds, such as PbO , $\text{Pb}(\text{OH})_2$
and $\text{Pb}(\text{OPh})_2$; Ti compounds, such as TiCl_4 and $\text{Ti}(\text{OPh})_4$;
Sn compounds, such as SnCl_4 , $\text{Sn}(\text{OPh})_4$, Bu_2SnO and
20 $\text{Bu}_2\text{Sn}(\text{OPh})_2$; Fe compounds, such as FeCl_3 , $\text{Fe}(\text{OH})_3$ and
 $\text{Fe}(\text{OPh})_3$; and reaction products of the above metal
compounds with the starting material, the reactant or a
product formed by the transesterification reaction of
the starting material with the reactant.

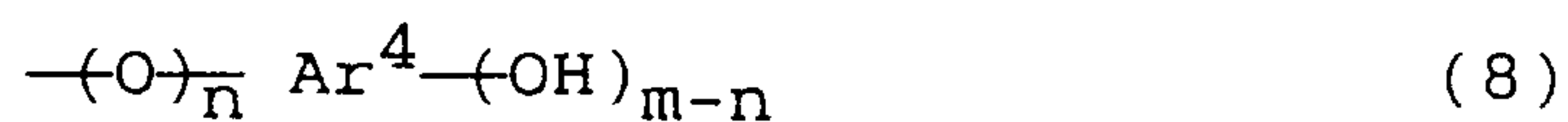
25 In the present invention, it is possible to use a

metal-containing catalyst which is not completely soluble in the liquid phase of the reaction system. In this case, from a practical viewpoint, it is important that the catalyst be in a form (for example, a slurry form) such that the catalyst can exert satisfactory catalyst activity in the reaction system.

As mentioned above, in the present invention, the aromatic polyhydroxy compound and a residue thereof (which originate from at least one member selected from the group consisting of the starting material, the reactant and a by-product of the transesterification) are, respectively, represented by the following formulae (7) and (8):



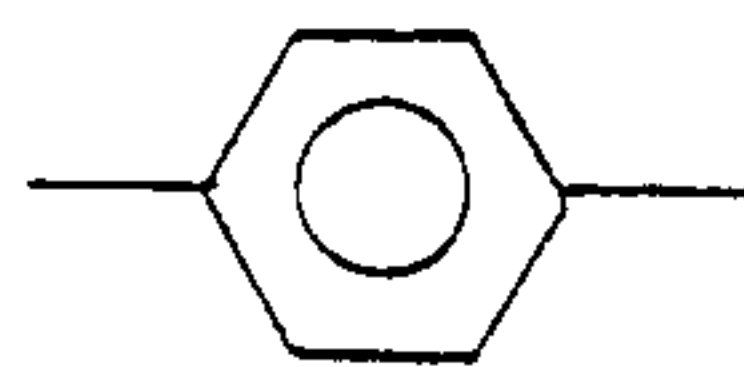
wherein Ar^4 represents an aromatic group having a valence of m , m represents an integer of 2 or more, and each $-\text{OH}$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group, and



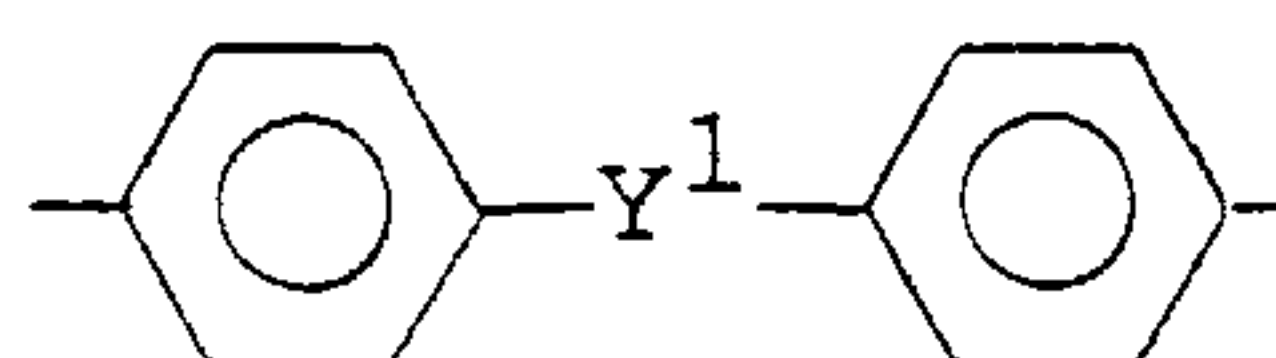
wherein Ar^4 and m are as defined above, n represents an integer of from 1 to m , and each of the $-\text{OH}$ group and the $-\text{O}-$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group.

The residue of the aromatic polyhydroxy compound.
 is present in such a form as chemically bonded, at the
 -O- group thereof, to at least one member selected from
 the group consisting of the metal of the catalyst, an
 5 alkoxy carbonyl group derived from the dialkyl carbonate
 or the alkyl aryl carbonate, an aryloxy carbonyl group
 derived from the alkyl aryl carbonate or the diaryl
 carbonate, and a carbonyl group derived from the dia-
 lkyl carbonate, the alkyl aryl carbonate or the diaryl
 10 carbonate.

Illustrative examples of the Ar^4 groups in formu-
 lae (7) and (8) above include aromatic groups repre-
 sented by the following formulae (12), (13), (14), (15)
 and (16):



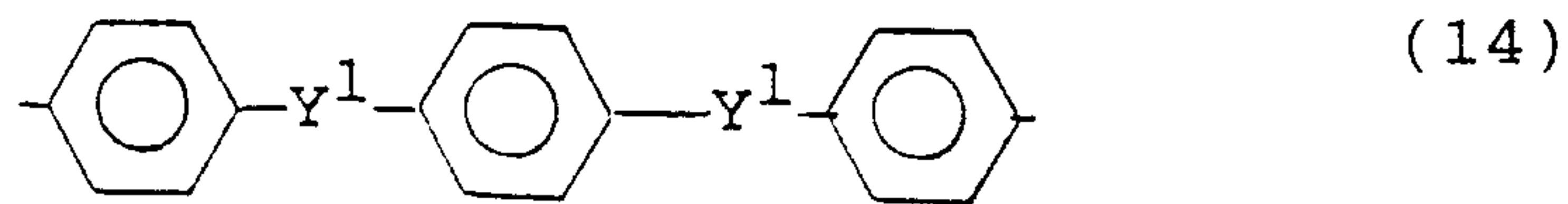
(12);



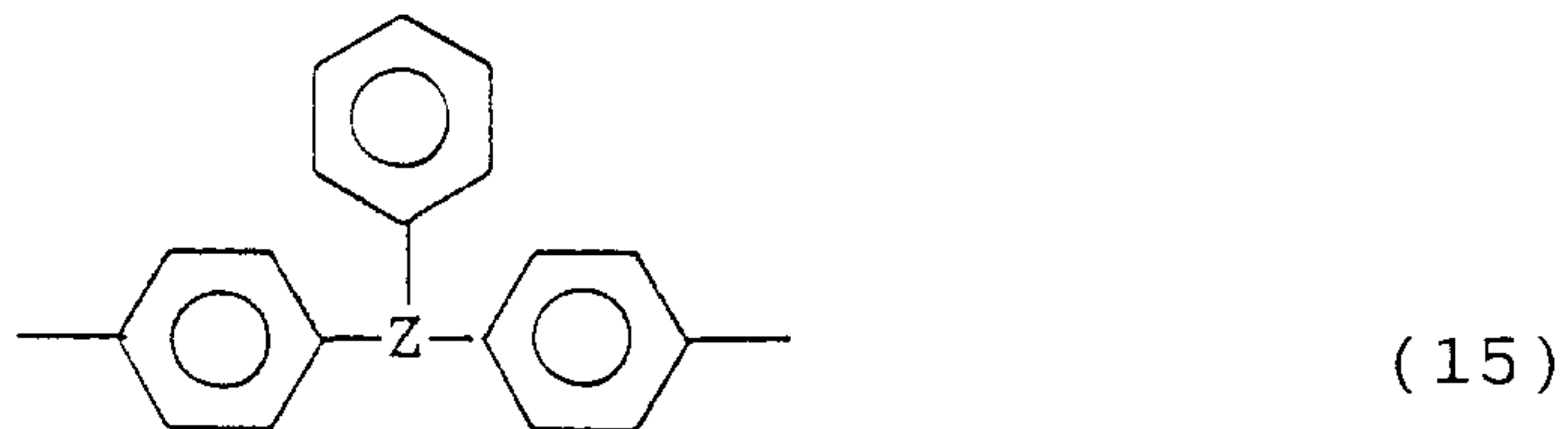
(13)

wherein Y^1 is as defined above;

44



wherein each of two Y¹'s is as defined
 above, and two Y¹'s may be the same or
 different;



wherein Z represents a trivalent group, such
 as a C₁-C₃₀ trivalent alkane group or a
 trivalent aromatic group; and at least one
 hydrogen atom of each aromatic ring may be
 replaced with a substituent, such as a
 halogen atom, a C₁-C₃₀ alkyl group, a C₁-C₃₀
 alkoxy group, a phenyl group, a phenoxy
 group, a vinyl group, a cyano group, an
 ester group, an amido group, a nitro group
 or the like; and



Examples of these aromatic polyhydroxy compounds include hydroquinone, resorcin, catechol, trihydroxybenzene (isomers), bis(hydroxyphenyl)propane (isomers), bis(hydroxyphenyl)methane (isomers), bis(hydroxyphenyl)ether (isomers), bis(hydroxyphenyl)ketone (isomers), bis(hydroxyphenyl)sulfone (isomers), bis(hydroxyphenyl)sulfide (isomers), dihydroxy diphenyl (isomers), bis(dihydroxyphenyl)methane (isomers), 2-hydroxyphenyl hydroxypropyl phenol, dihydroxy (hydroxyphenyl diphenyl) (isomers), tri-(hydroxyphenyl)ethane (isomers), tri-(hydroxyphenyl)benzene (isomers), dihydroxynaphthalene (isomers) and trihydroxynaphthalene (isomers).

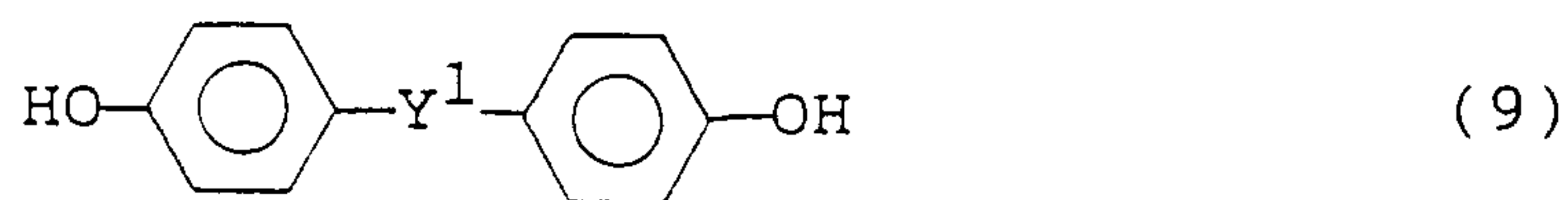
Of these aromatic polyhydroxy compounds and residues thereof, those which are likely to be present in the system for the transesterification for the production of an aromatic carbonate are especially important in the present invention. As such an important aromatic polyhydroxy compound, there can be mentioned at least one member selected from the group consisting of:

(A) an oxidation product of an aromatic monohy-

droxy compound as the reactant,

(B) at least one member selected from the group consisting of a product produced by the Fries rearrangement of a diaryl carbonate obtained by the transesterification and oxidation products of the product and

(C) at least one member selected from the group consisting of aromatic dihydroxy compounds derived from phenol as the reactant and represented by the following formula (9):

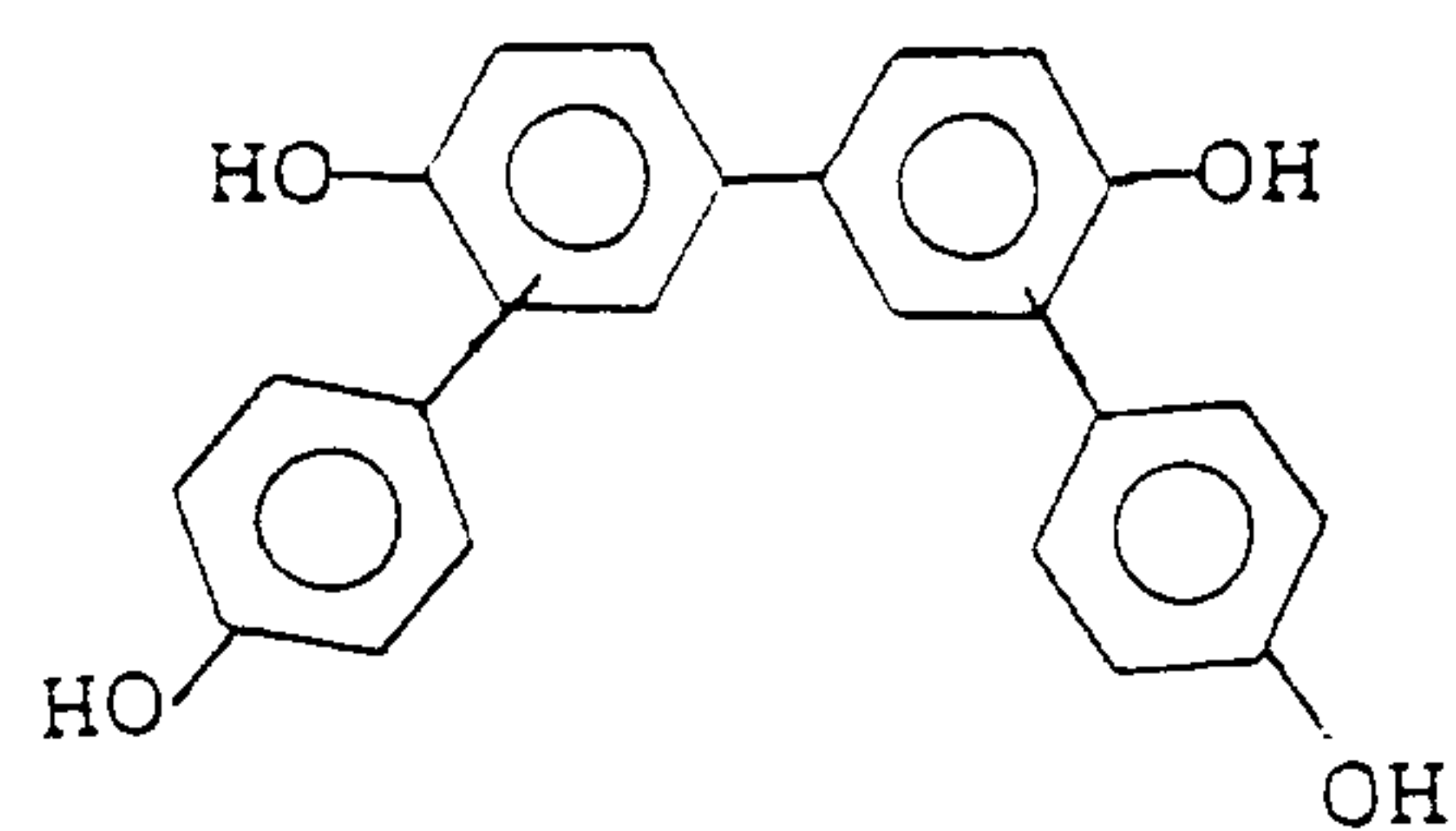


wherein Y^1 represents a single bond, a divalent alkane group having 1 to 30 carbon atoms or a divalent group selected from $-O-$, $-CO-$, $-S-$, $-SO_2-$, $-SO-$ and $-COO-$, and oxidation products of the aromatic dihydroxy compounds.

As examples of the oxidation product (A) of an aromatic monohydroxy compound, compounds represented by the following formulae (17) and (18) can be mentioned.

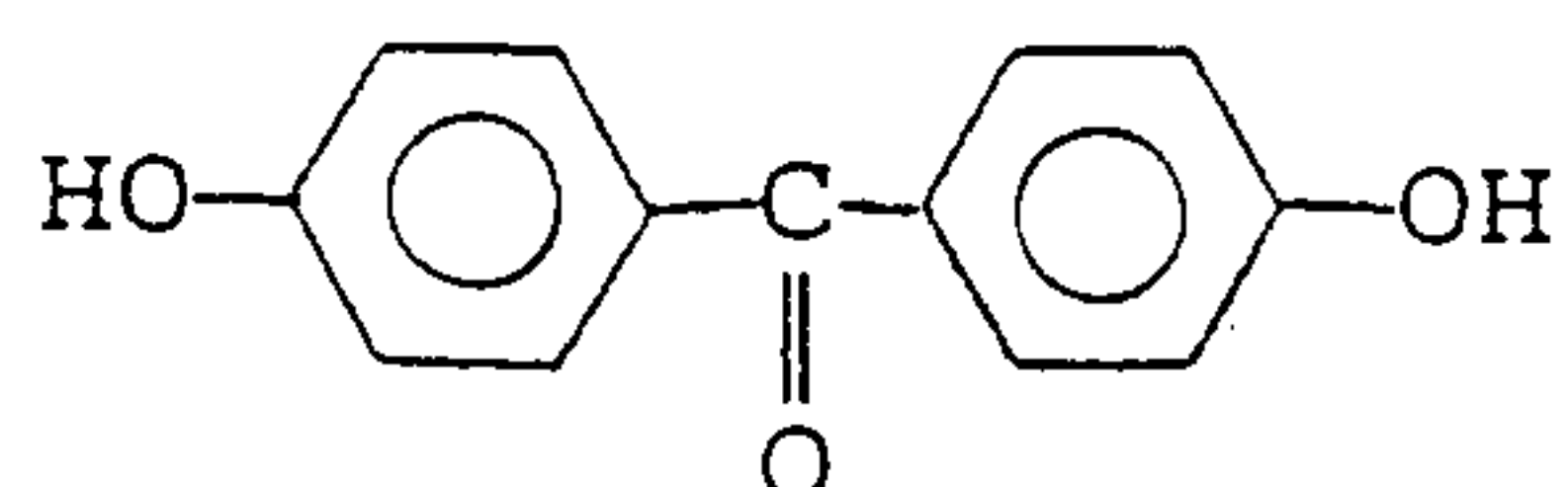


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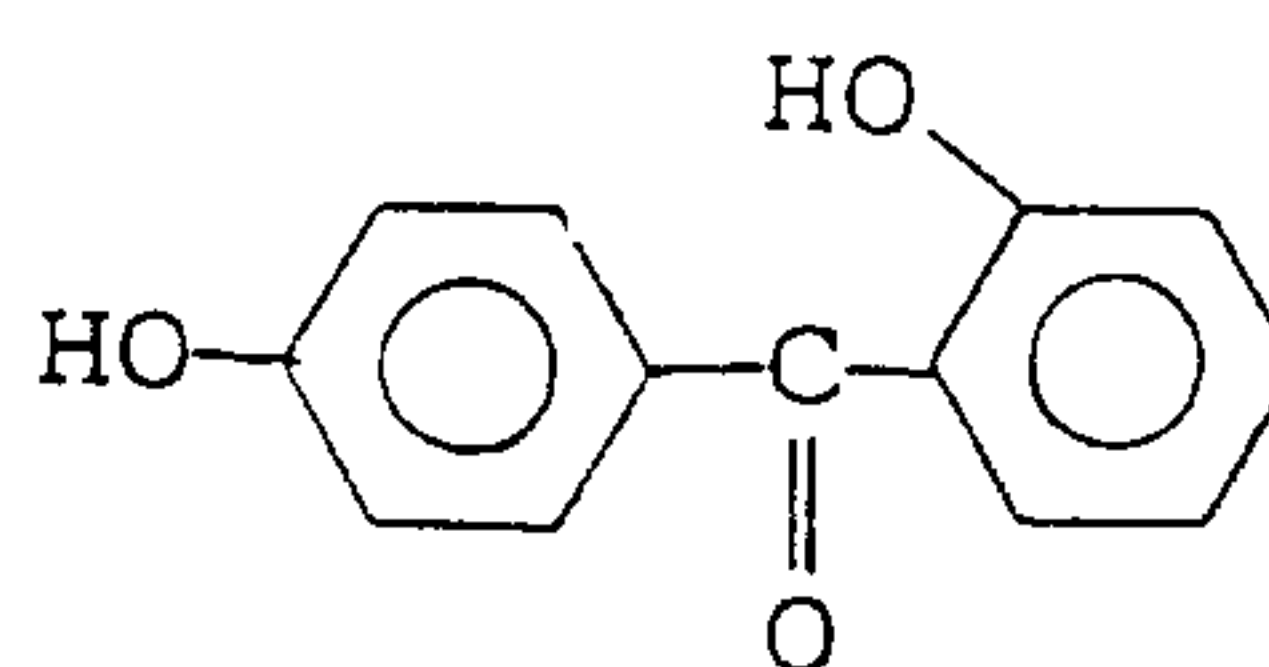


(18)

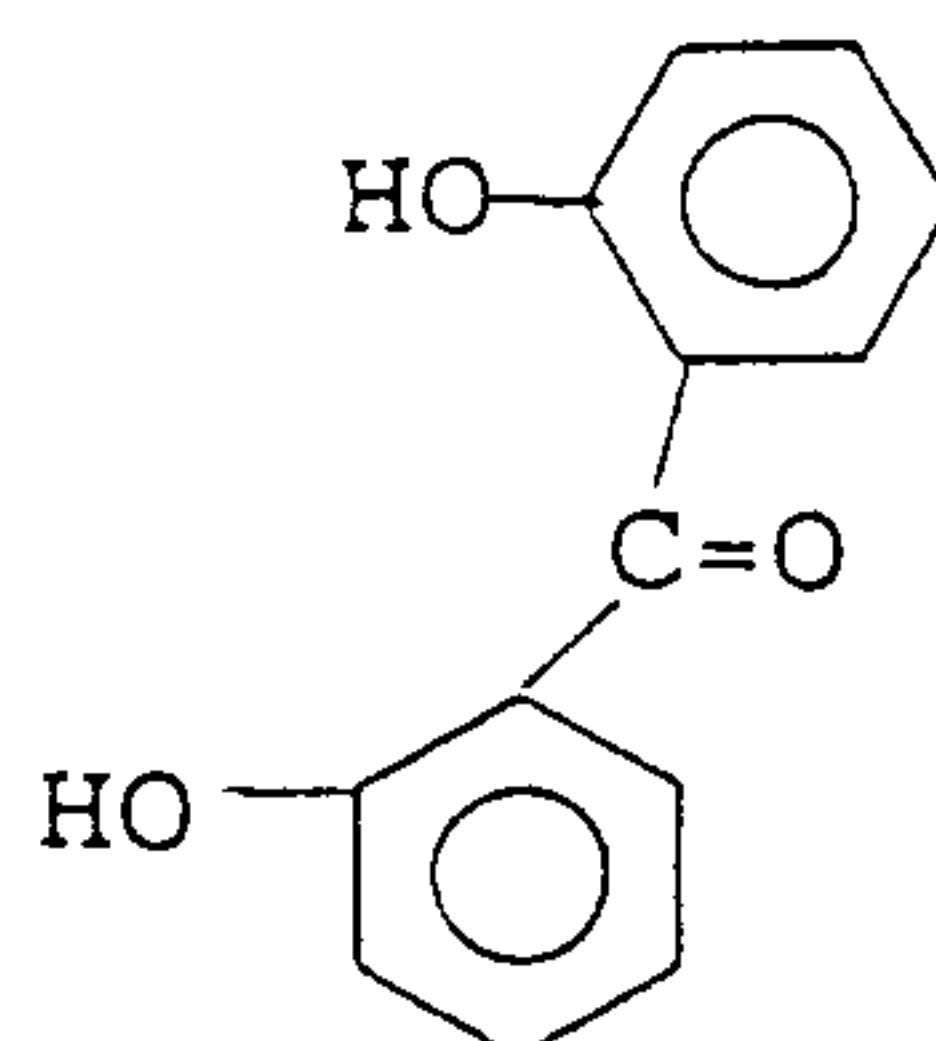
As examples of the product (B) produced by the Fries rearrangement of a diaryl carbonate, compounds represented by the following formulae (19), (20) and (21) can be mentioned.



(19)



(20)

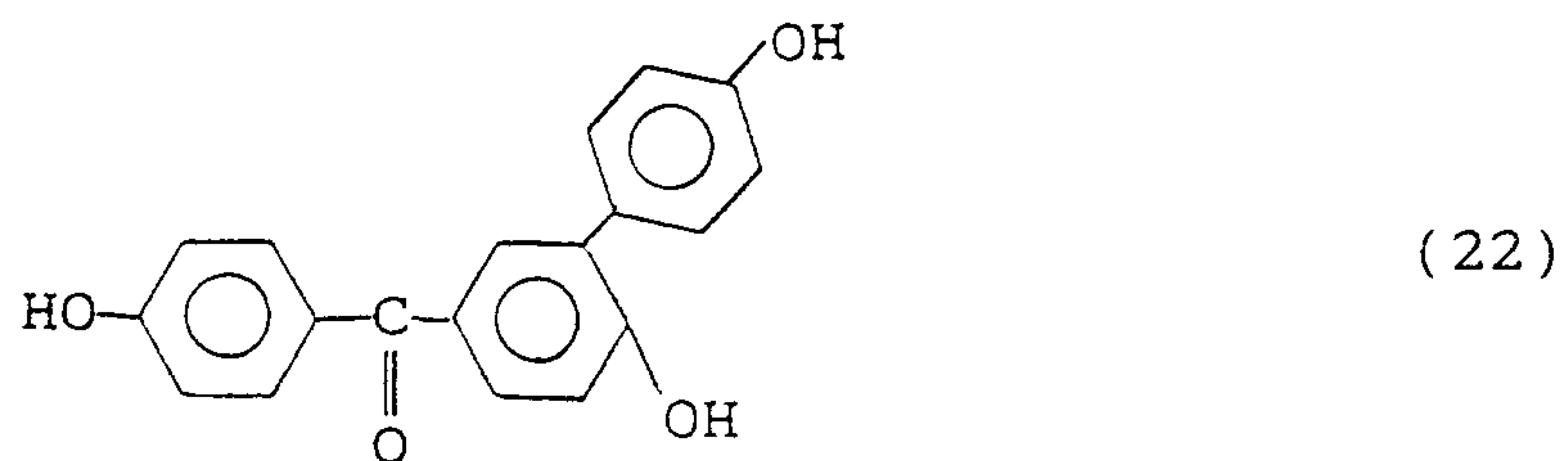


(21)

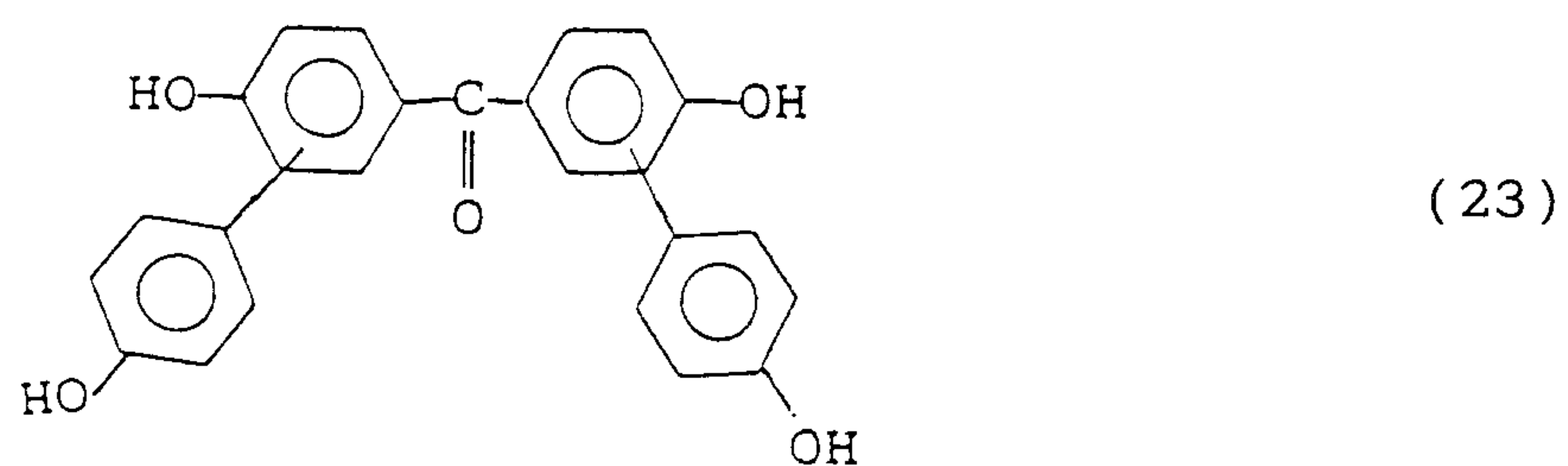
As examples of oxidation products of the above-mentioned product (B) produced by the Fries rearrangement of a diaryl carbonate and represented by formula (19), compounds represented by the following formulae (22) and (23) can be mentioned. Also, as examples of

respective oxidation products of the above-mentioned products (B) represented by formulae (20) and (21), compounds represented by the following formulae (24) and (25) can be mentioned.

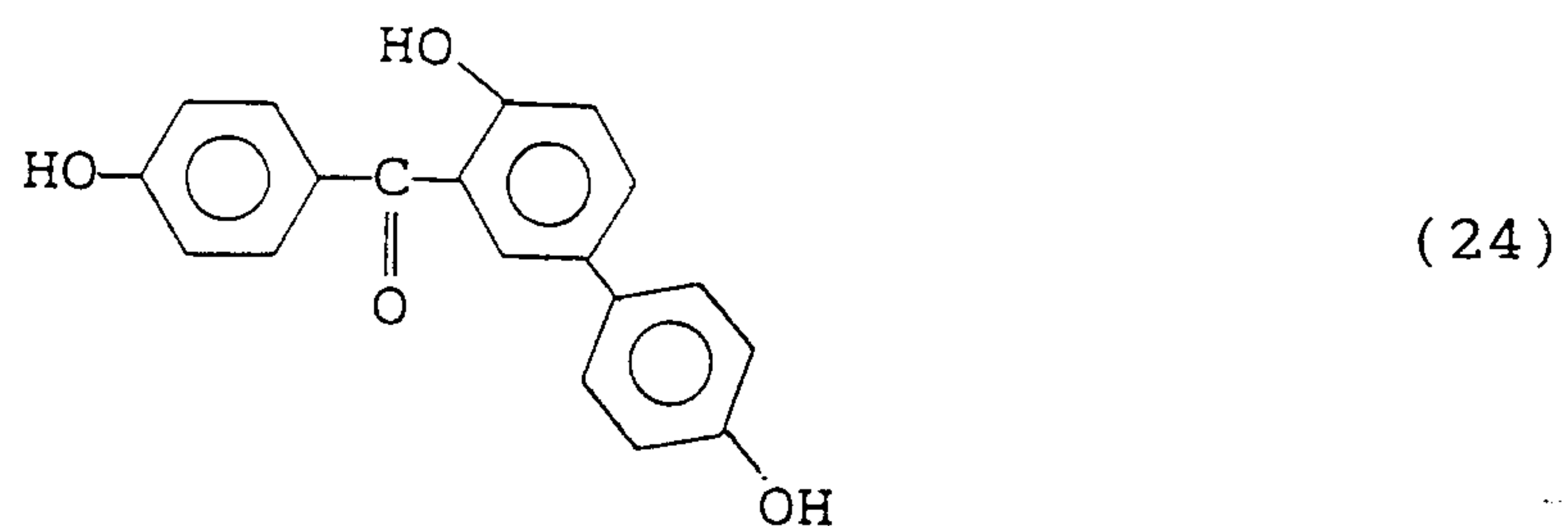
5



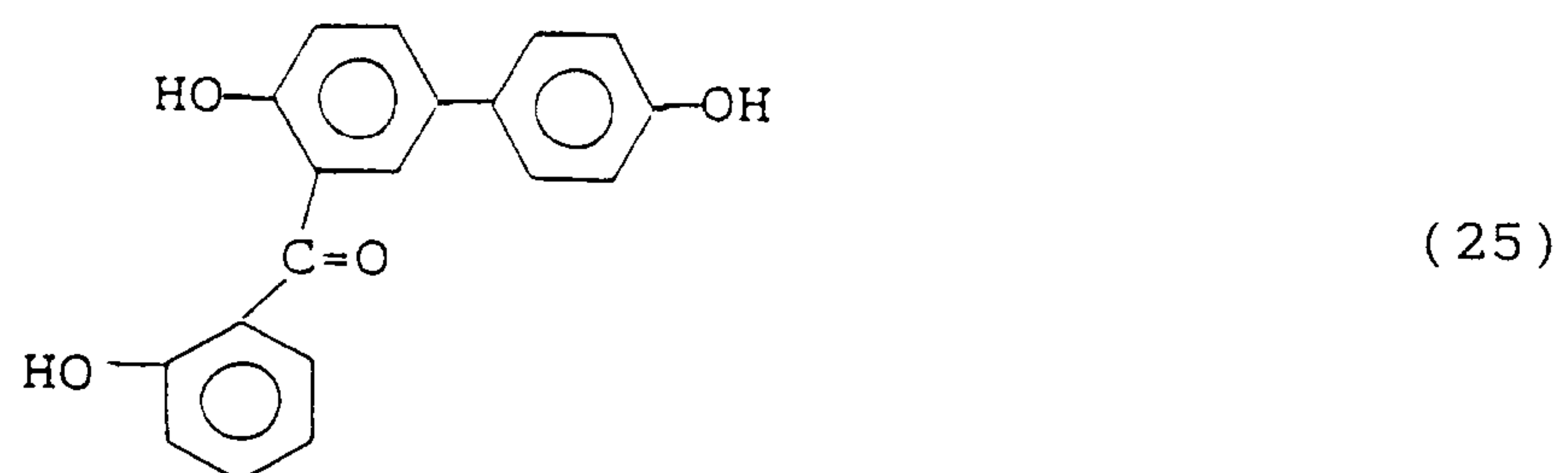
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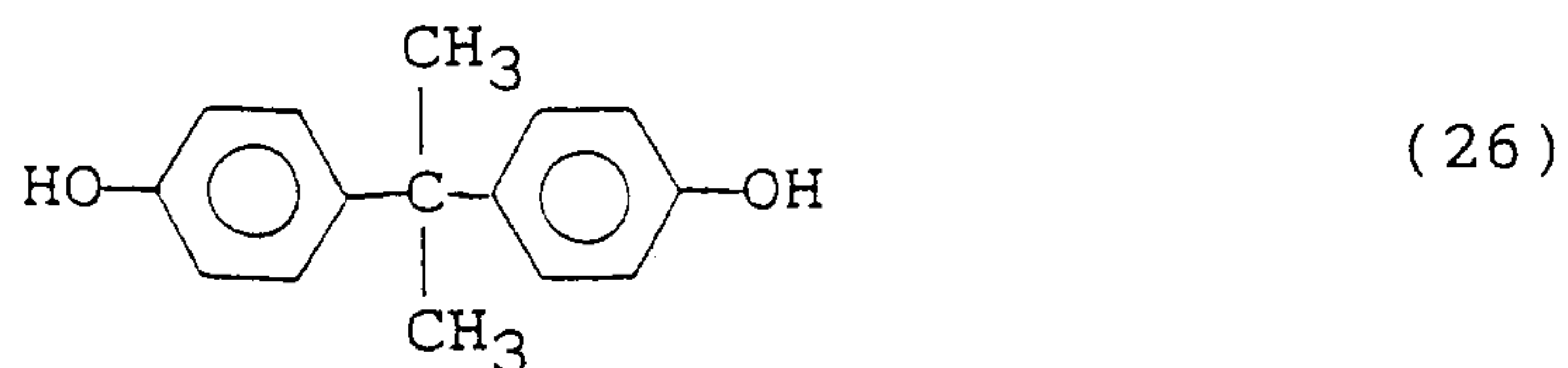
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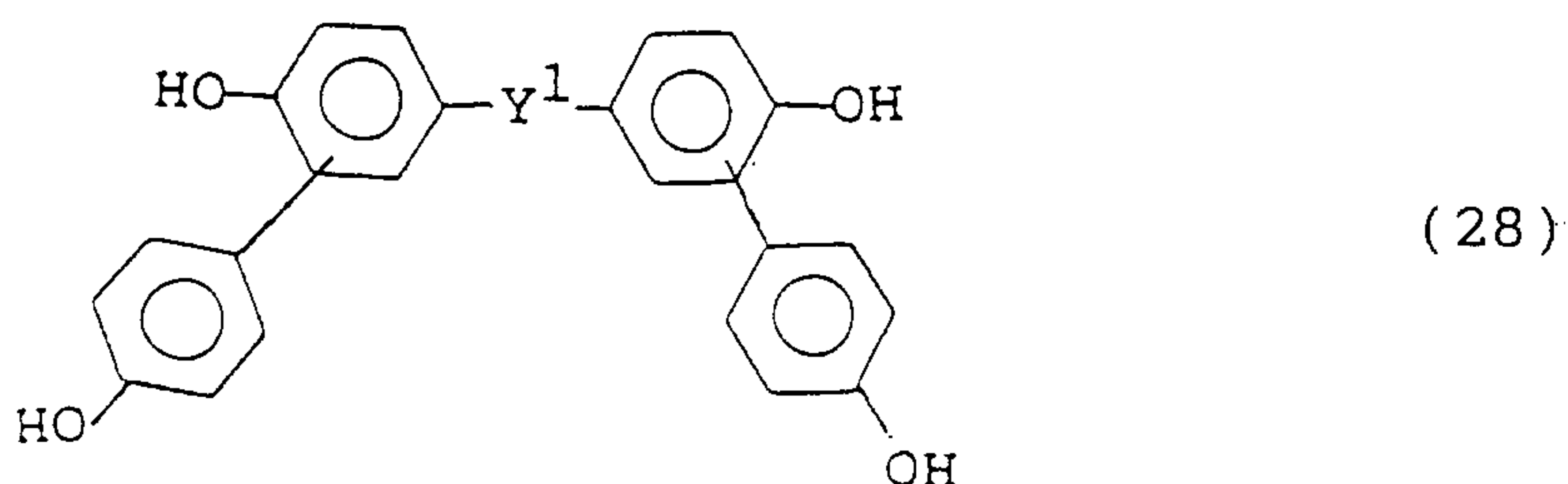
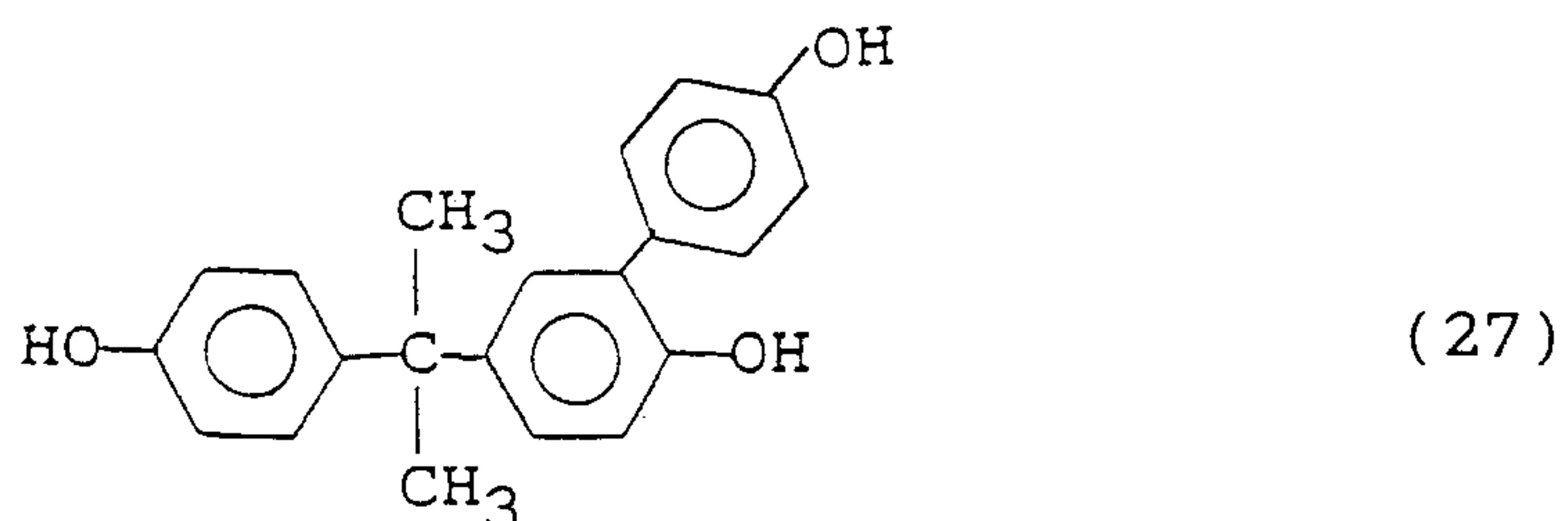
As an example of the aromatic dihydroxy compound

(C) represented by formula (9), a compound represented by the following formula (26) can be mentioned.



As examples of oxidation products of the above-mentioned aromatic dihydroxy compound (C) represented by formula (26), compounds represented by the following formulae (27) and (28) can be mentioned.

10



wherein Y^1 is as defined above.

The reason why the above-mentioned oxidation product (A) of an aromatic monohydroxy compound is

25

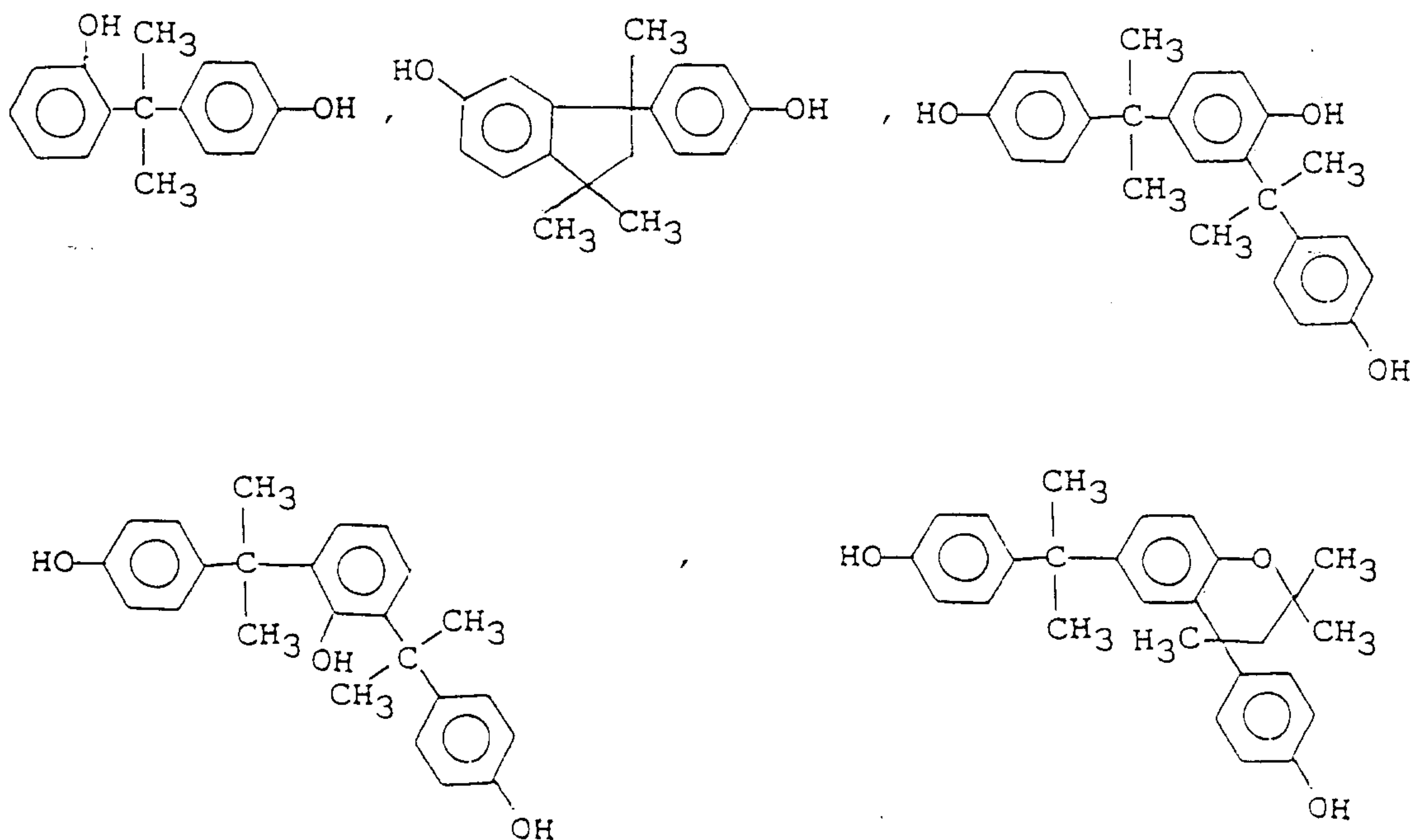
likely to be present in the system for the transesterification for the production of an aromatic carbonate, for example, is that such an oxidation product is formed by the oxidation of an aromatic monohydroxy compound with a very small amount of oxygen which occasionally enters the system for the transesterification, or that such an oxidation product is occasionally present as a contaminant of an aromatic monohydroxy compound as a raw material and enters the system together with the raw material. Representative examples of type (A) oxidation products, namely, oxidation products of aromatic monohydroxy compounds include dihydroxybenzene (isomers), dihydroxy diphenyl (isomers), and the like.

Product (B) produced by the Fries rearrangement of a diaryl carbonate is likely to be formed as a by-product in the production of the diaryl carbonate. Examples of products (B) include 2,2'-dihydroxybenzophenone, 2,4'-dihydroxybenzophenone and 4,4'-dihydroxybenzophenone.

The aromatic dihydroxy compound (C) is a compound which is usually used as a monomer for the production of an aromatic polycarbonate. An aromatic polycarbonate can be produced by a transesterification of the above-mentioned aromatic dihydroxy compound (C) with a

diaryl carbonate, wherein an aromatic monohydroxy compound is by-produced. When such a by-produced aromatic monohydroxy compound is used as a raw material in the process of the present invention, the aromatic dihydroxy compound (C) is likely to be introduced into the system for the transesterification for the production of an aromatic carbonate. Examples of aromatic dihydroxy compounds (C) include 2,2-bis-(4-hydroxyphenyl)propane, and the like.

Further, 2,2-bis-(4-hydroxyphenyl)propane usually contains aromatic polyhydroxy compounds represented by the following formulae, which compounds are also included in the aromatic polyhydroxy compound defined in the present invention.



In the process of the present invention, it is essential to conduct a transesterification while maintaining a weight ratio (WR) of at least one aromatic group-containing substance selected from the group consisting of an aromatic polyhydroxy compound and a residue thereof to the metal of the metal-containing catalyst at 2.0 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification. The above-mentioned weight ratio (WR) is preferably 1.0 or less, more preferably 0.5 or less. The term "system for the transesterification" means a system which includes not only the reactor, but also the pipes and devices provided in connection with the reactor, such as a device for the recovering and recycling or recirculating of the catalyst, and the like. In the present invention, the term "catalyst-containing liquid-phase mixture" means a catalyst-containing liquid material to be fed to the reactor, a catalyst-containing reaction mixture in the reactor, a catalyst-containing reaction mixture withdrawn from the reactor, a liquid material having an increased catalyst concentration which is obtained by subjecting to evaporation a part of the catalyst-containing reaction mixture withdrawn from the reactor, and the like. In the

catalyst-containing liquid-phase mixture, either the catalyst may be completely dissolved, or it need not be completely dissolved. In the case of the latter, the catalyst-containing liquid-phase mixture is in the form of a slurry. In the present invention, when the catalyst-containing reaction mixture is in the form of a slurry (which contains insoluble matters), such a slurry including insoluble matters is also referred to as a "catalyst-containing liquid-phase mixture". With respect to the above-mentioned weight ratio (WR), it has been found that, when the WR exceeds 2.0, disadvantageous phenomena, such as the deposition of the metal-containing catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner walls of the reactor, pipes and the like occur, so that the reaction becomes unstable and hence cannot achieve favorable results. The reason for this has not yet been elucidated, but is considered to be as follows. When the above-mentioned weight ratio (WR) exceeds 2.0, an insoluble substance having a crosslinked structure is formed by a crosslinking reaction between the metal of the metal-containing catalyst and the aromatic polyhydroxy compound and deposited from the liquid-phase mixture, wherein the deposited substance has strong adhesiveness to the

inner walls of the reactor, pipes, and the like.

In the process of the present invention for producing an aromatic carbonate, the aromatic monohydroxy compound used as a reactant frequently comprises two types of compounds, i.e., a fresh feedstock aromatic monohydroxy compound and an unreacted aromatic monohydroxy compound recycled from the reactor. There is no particular limitation with respect to the ratio of the fresh feedstock aromatic monohydroxy compound to the unreacted aromatic monohydroxy compound recycled from the reactor; however, the weight ratio of the fresh feedstock aromatic monohydroxy compound to the unreacted aromatic monohydroxy compound recycled from the reactor is generally in the range of from 100 : 0 to 0.0001 : 99.9999. In the present invention, for maintaining the weight ratio (WR) of the at least one aromatic group-containing substance to the metal of the metal-containing catalyst at 2.0 or less as measured with respect to a catalyst-containing liquid-phase mixture in the system for the transesterification, it is preferred that the fresh feedstock aromatic monohydroxy compound have an aromatic polyhydroxy compound concentration of 400 ppm by weight or less, more preferably 300 ppm by weight or less, most preferably 200 ppm by weight or less.

As a method for controlling the concentration of the at least one aromatic group-containing substance in the catalyst-containing liquid-phase mixture so as to maintain the weight ratio (WR) within the range as defined in the present invention, it is preferred to withdraw a part of the catalyst-containing liquid-phase mixture out of the system for the transesterification. For example, when the process of the present invention comprises the steps of subjecting to evaporation a part of the catalyst-containing liquid-phase mixture withdrawn from the reactor and recycling the resultant catalyst-containing liquid-phase mixture having an increased catalyst concentration to the reactor, the accumulation of the aromatic group-containing substance in the system can be effectively avoided by withdrawing at least a part of the resultant evaporation-concentrated liquid-phase mixture (having an increased catalyst concentration) out of the system for the transesterification. Further, the accumulation of the aromatic group-containing substance in the system for the transesterification can also be avoided by a method in which occasional entry of air into the system is suppressed to a level as low as possible, to thereby suppress the formation of an aromatic polyhydroxy compound as an oxidization product of the aromatic

monohydroxy compound.

In the process of the present invention, it is preferred that the amount of the aromatic polyhydroxy compound in each of the starting material and the reactant be as small as possible.

Further, when the amount of such an aromatic group-containing substance in the system for the transesterification is considerably large (due to the introduction of such a substances as impurities of the starting material to the system together with the starting material or the reactant, or due to the formation of such a substance in the system by side reactions), for example, in the process for continuously producing a desired aromatic polycarbonate, it is preferred to start the above-mentioned withdrawal of at least a part of the evaporation-concentrated, catalyst-containing liquid-phase mixture out of the system for the transesterification at an early stage and/or to increase the withdrawal amount, depending on the amount of aromatic group-containing substance present in the system, so as to avoid the accumulation of the aromatic group-containing substance in the system. For enabling such a withdrawal of the evaporation-concentrated, catalyst-containing liquid-phase mixture to be conducted properly, it is preferred to use, for example, the

following method. A sampling nozzle is provided on a pipe connected to the outlet of the reactor, and samples of a catalyst-containing liquid-phase mixture withdrawn from the reactor are taken at predetermined intervals through the sampling nozzle. By measuring the amount of the aromatic group-containing substance in each sample and monitoring the changes in the amount of the aromatic group-containing substance in the samples, suitable timing for starting the withdrawal and a suitable withdrawal amount can be determined so that the weight ratio (WR) of the aromatic group-containing substance to the metal of the metal-containing catalyst in the catalyst-containing liquid-phase mixture can be maintained within the range defined in the present invention.

An example of the above-mentioned operation for withdrawing the catalyst-containing liquid-phase mixture out of the system for the transesterification is explained below, referring to Fig. 1. Fig. 1 shows an example of systems for practicing the process of the present invention for producing an aromatic carbonate using a continuous multi-stage distillation column. In the system shown in Fig. 1, a mixture of dimethyl carbonate, phenol and a catalyst is continuously fed in liquid form from conduit 3 to continuous multi-stage

distillation column 1 at top 2 thereof (which column 1 has sieve trays therein) through preheater 4 and conduit 5, thereby allowing the mixture to flow down inside of multi-stage distillation column 1. Simultaneously, dimethyl carbonate is introduced from conduit 7 into evaporator 8, in which the evaporation of the dimethyl carbonate is performed, and the resultant gas is continuously fed to bottom 6 of distillation column 1 through conduit 9, so that a transesterification reaction is conducted while effecting distillation. Gas (containing methanol and dimethyl carbonate) distilled from column top 2 is led into condenser 11 through conduit 10, in which the gas is condensed. The resultant condensate is continuously withdrawn through conduit 12. A reaction mixture (containing the produced methyl phenyl carbonate, the catalyst, and an aromatic polyhydroxy compound and a residue thereof, which residue is chemically bonded to, for example, carbonyl groups derived from the carbonates and/or to the metal of the catalyst) is continuously withdrawn from column bottom 6, and led through conduit 13 into evaporator 14, in which the methyl phenyl carbonate is evaporated to thereby obtain an evaporation-concentrated liquid (containing the catalyst, the aromatic polyhydroxy compound and the residue thereof). A part of

the obtained concentrated liquid is led into reboiler. 17 through conduits 15 and 16 and recycled into evaporator 14 through conduit 18. The rest of the concentrated liquid is recycled into distillation column 1 through conduits 15 and 19. An evaporated gas (containing the methyl phenyl carbonate) from evaporator 14 is led into condenser 22 through conduit 21, in which the gas is condensed. The resultant condensate is withdrawn from condenser 22 through conduit 23. The concentrated liquid, which is being recycled into distillation column 1 through conduit 19 as mentioned above, is partly withdrawn out of the system for the transesterification through conduit 20. By the withdrawal of a part of the concentrated liquid through conduit 20, the aromatic group-containing substance is at least partly withdrawn out of the system for the transesterification, so that the weight ratio (WR) of the aromatic group-containing substance to the metal of the catalyst in the catalyst-containing liquid-phase mixture in the system for the transesterification can be maintained at 2.0 or less. In the above system, the catalyst is fed to distillation column 1 through conduit 3 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 20, so that the catalyst concentration of the catalyst-con-

taining liquid-phase mixture in the system for the transesterification is maintained at a predetermined level. There is no particular limitation with respect to the amount of the concentrated liquid withdrawn out of the system for the transesterification. However, the concentrated liquid is generally withdrawn in such an amount that the weight ratio of the concentrated liquid withdrawn out of the system for the transesterification to an aromatic carbonate to be produced is in the range of from 10^{-8} to 0.1, preferably from 10^{-6} to 0.05.

With respect to the lower limit of the content of the aromatic group-containing substance in the catalyst-containing liquid-phase mixture in the system for the transesterification, there is no particular limitation. However, when it is attempted to obtain a catalyst-containing liquid-phase mixture having an extremely small content of the aromatic group-containing substance, disadvantages arise in that a burden on the separation and purification equipment for the starting material and reactant to be fed to the system for the transesterification becomes large, and that the amount of the catalyst-containing liquid-phase mixture which must be withdrawn out of the system becomes too large. Therefore, the weight ratio (WR) of the aromatic group-

containing substance to the metal of the catalyst in the catalyst-containing liquid-phase mixture in the system for the transesterification is generally not smaller than 10^{-9} , preferably not smaller than 10^{-8} .

5 The process of the present invention for producing an aromatic carbonate may either be conducted in a batchwise manner or in a continuous manner. It is preferred that an aromatic carbonate be produced in a continuous manner. For example, an aromatic carbonate
10 can be continuously produced by a method in which a starting material and a reactant are continuously fed to a reactor to effect a transesterification reaction therebetween in at least one phase selected from a liquid phase and a gas-liquid phase in the presence of
15 a metal-containing catalyst in the reactor, while continuously withdrawing a high boiling point reaction mixture containing the produced aromatic carbonate or aromatic carbonate mixture in liquid form from a lower portion of the reactor and continuously withdrawing a
20 low boiling point reaction mixture containing a by-product in gaseous form from an upper portion of the reactor by distillation.

 One illustrative example of systems for practicing the process for continuously producing an aromatic
25 carbonate is shown in Fig. 2, wherein reaction vessel

100 equipped with a stirrer is used. In the process
using the system of Fig. 2, a starting material and a
reactant are continuously fed to reaction vessel 100
from conduit 3 to thereby effect a transesterification
5 reaction therebetween in at least one phase selected
from a liquid phase and a gas-liquid phase in the
presence of a metal-containing catalyst in reaction
vessel 100, while continuously withdrawing a high
boiling point reaction mixture containing a produced
10 aromatic carbonate and the catalyst from a bottom
portion of reaction vessel 100 through conduit 13 and
continuously withdrawing a low boiling point reaction
mixture containing a by-product in gaseous form from an
upper portion of reaction vessel 100 through conduit
15 30, distillation column 24 and conduit 29.

Another illustrative example of systems for prac-
ticing the process for continuously producing an aro-
matic carbonate is shown in Fig. 1, wherein continuous
multi-stage distillation column 1 is used as a reactor.
20 In the process using the system of Fig. 1, a starting
material and a reactant are continuously fed to contin-
uous multi-stage distillation column 1 at top 2 thereof
and/or bottom 6 thereof to effect a transesterification
reaction therebetween in at least one phase selected
25 from a liquid phase and a gas-liquid phase in the

presence of a metal-containing catalyst in continuous multi-stage distillation column 1, while continuously withdrawing a high-boiling point reaction mixture containing a produced aromatic carbonate and the catalyst from a lower portion of distillation column 1 through conduit 13 and continuously withdrawing a low boiling point reaction mixture containing a by-product in gaseous form from an upper portion of distillation column 1 through conduit 10, condenser 11 and conduit 12 by distillation.

As apparent from the above, there is no particular limitation with respect to the type of the reactor to be used in the process of the present invention, and various types of conventional reactors, such as an agitation type reactor, a multi-stage agitation type reactor and a multi-stage distillation column, can be used. These types of reactors can be used individually or in combination, and may be used either in a batch-wise process or a continuous process. From the viewpoint of efficiently biasing the equilibrium toward the product system, a multi-stage distillation column is preferred, and a continuous process using a multi-stage distillation column is especially preferred. There is no particular limitation with respect to the multi-stage distillation column to be used in the present

invention as long as it is a distillation column having a theoretical number of stages of distillation of two or more and which can be used for performing continuous distillation. Examples of such multi-stage distillation columns include plate type columns using a tray, such as a bubble-cap tray, a perforated tray, a valve tray and a counterflow tray, and packed type columns packed with various packings, such as a Raschig ring, a Lessing ring, a Pall ring, a Berl saddle, an Intelox saddle, a Dixon packing, a McMahon packing, a Heli pack, a Sulzer packing and Mellapak. In the present invention, any of the columns which are generally used as a multi-stage distillation column can be utilized. Further, a mixed type of plate column and packed column comprising both a plate portion and a portion packed with packings, can also be preferably used. With respect to a process for continuously producing an aromatic carbonate using a multi-stage distillation column, reference can be made to, for example, U.S. Patent No. 5,210,268 and EP Patent Publication No. 0 461 274 B1 corresponding to the above U.S. patent.

In one preferred embodiment of the present invention, in which the continuous production of an aromatic carbonate is conducted using a multi-stage distillation column, a starting material and a reactant are continu-

ously fed to a continuous multi-stage distillation column to effect a transesterification reaction therebetween in at least one phase selected from a liquid phase and a gas-liquid phase in the presence of a metal-containing catalyst in the distillation column, while continuously withdrawing a high boiling point reaction mixture containing a produced aromatic carbonate or aromatic carbonate mixture in liquid form from a lower portion of the distillation column and continuously withdrawing a low boiling point reaction mixture containing a by-product in gaseous form from an upper portion of the distillation column by distillation.

The amount of the catalyst used in the present invention varies depending on the type thereof, the types and weight ratio of the starting material and the reactant, the reaction conditions, such as reaction temperature and reaction pressure, and the like. Generally, the amount of the catalyst is in the range of from 0.0001 to 30 % by weight, based on the total weight of the starting material and the reactant.

The reaction time (or the residence time when the reaction is continuously conducted) for the transesterification reaction in the present invention is not specifically limited, but it is generally in the range

of from 0.001 to 50 hours, preferably from 0.01 to 10 hours, more preferably from 0.05 to 5 hours.

The reaction temperature varies depending on the types of the starting material and reactant, but is generally in the range of from 50 to 350 °C, preferably from 100 to 280 °C. The reaction pressure varies depending on the types of the starting material and reactant and the reaction temperature, and it may be any of a reduced pressure, an atmospheric pressure and a superatmospheric pressure. However, the reaction pressure is generally in the range of from 0.1 mmHg to 200 kg/cm².

In the present invention, it is not necessary to use a solvent. However, for the purpose of facilitating the reaction operation, an appropriate inert solvent, such as an ether, an aliphatic hydrocarbon, an aromatic hydrocarbon, a halogenated aliphatic hydrocarbon or a halogenated aromatic hydrocarbon, may be used as a reaction solvent.

20

25

BEST MODE FOR CARRYING OUT THE INVENTION

Hereinbelow, the present invention will be described in more detail with reference to the following Examples and Comparative Examples, but they should not
5 be construed as limiting the scope of the present invention.

In the following Examples and Comparative Examples, the metal concentration of the metal-containing catalyst was measured by means of an ICP (inductively
10 coupled plasma emission spectral analyzer) (JY38PII: manufactured and sold by Seiko Electronics Co., Ltd., Japan); the determination of the composition of the reaction mixture and the measurement of the respective concentrations of the components (such as an aromatic
15 polyhydroxy compound, and a residue thereof bonded to carbonyl-containing groups originating from aromatic polycarbonates as the starting material, the reactant and the desired product; an aromatic monohydroxy compound; an aromatic carbonate; and anisole) in the reac-
20 tion mixture were conducted by high performance liquid chromatography; and the measurement of the concentration of the aromatic polyhydroxy compound residue bonded to the catalyst in the reaction mixture was
25 conducted by a method in which a ligand exchange with trifluoroacetic acid is conducted, followed by analysis

by high performance liquid chromatography.

All of the concentrations are indicated by weight percentages.

5 Example 1

(Preparation of catalyst)

10 A mixture of 30 kg of phenol, 10 kg of methyl phenyl carbonate and 8 kg of dibutyltin oxide was heated to and maintained at 180 °C for 10 hours, thereby performing a reaction. After that period of time, water formed in the resultant reaction mixture was distilled off together with unreacted phenol. Then, most of the remaining phenol and the remaining methyl phenyl carbonate were distilled off from the reaction mixture under reduced pressure, and the resultant mixture was allowed to cool under nitrogen atmosphere, to thereby obtain catalyst A.

(Production of aromatic carbonate)

20 The production of an aromatic carbonate was conducted using an apparatus shown in Fig. 2, which comprises distillation column 24 having a height of 1 m and a diameter of 4 inches and containing Dixon packing (6 mm ϕ), and a reaction vessel 100 having a capacity of 200 liters and equipped with a stirrer.

25 A mixture of dimethyl carbonate, phenol [concen-

tration of 4,4'-dihydroxy diphenyl (i.e., an aromatic polyhydroxy compound) in phenol: 100 ppm] and catalyst A was continuously fed in liquid form from conduit 3 to reaction vessel 100 at a rate of 20 kg/hr, thereby performing a reaction. The weight ratio of the dimethyl carbonate to the phenol in the mixture was 50/50, and catalyst A was used in an amount such that the Sn concentration of the reaction mixture in conduit 13 became 0.4 % by weight, wherein the Sn concentration can be confirmed using a sample withdrawn through a sampling nozzle (not shown) provided on conduit 13. The reaction conditions of the above reaction were such that the temperature in reaction vessel 100 was 200 °C and the pressure at the top of distillation column 24 was 6.2 kg/cm²-G. Gas (containing methanol and dimethyl carbonate) formed in reaction vessel 100 was led into distillation column 24 through conduit 30. From distillation column 24, dimethyl carbonate was recycled to reaction vessel 100 through conduit 32, while the gas (containing methanol and dimethyl carbonate) distilled from the top of distillation column 24 was led into condenser 26 through conduit 25, in which the gas was condensed. A portion of the resultant condensate was recycled into distillation column 24 at a reflux ratio of 50 through conduits 27 and 28, and the rest of

the condensate was continuously withdrawn at a rate of 2.3 kg/hr through conduit 29. A reaction mixture [containing methyl phenyl carbonate (as a desired reaction product), the catalyst, and an aromatic polyhydroxy compound and a residue thereof] was continuously withdrawn from the bottom of reaction vessel 100 at a rate of 17.7 kg/hr and led into evaporator 14 through conduit 13, from which an evaporated gas containing the methyl phenyl carbonate was withdrawn and led through conduit 21 into condenser 22, in which the evaporated gas was condensed. The resultant condensate was withdrawn from condenser 22 through conduit 23 at a rate of 16.67 kg/hr. On the other hand, an evaporation-concentrated liquid containing the catalyst and the aromatic polyhydroxy compound and the residue thereof was formed in evaporator 14. A portion of the concentrated liquid was led into reboiler 17 through conduits 15 and 16 and recycled into evaporator 14 through conduit 18. The rest of the concentrated liquid in evaporator 14 was recycled into reaction vessel 100 at a rate of 1 kg/hr through conduits 15, 19 and 3. During the period of time of from 300 hours to 2,000 hours after the start of the operation, a portion of the concentrated liquid formed in evaporator 14 was continuously withdrawn through conduit 20 at a rate of 0.03 kg/hr.

Instead, catalyst A was added to reaction vessel 100 through conduit 3 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 20, so that the above-mentioned Sn concentration of 0.4 % by weight was able to be maintained in conduit 13. The operation was conducted for 2,000 hours. During this period of time, the operation could be stably conducted (for example, both the flow and the composition in each conduit were stable) without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner wall of the reaction vessel and the like. Samples were taken from the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time

of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Sn were, respectively, 0.19, 0.19, 0.2 and 0.2. The composition of the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle at the point in time of 2,000 hours after the start of the operation was as follows: phenol (PhOH): 51 % by weight; methyl phenyl carbonate (MPC): 6 % by weight; diphenyl carbonate (DPC): 0.4 % by weight; anisole (ANS): 0.6 % by weight; and Sn: 0.4 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, no adhesion of the catalyst to the inner wall of each of reaction vessel 100, evaporator 14, reboiler 17 and conduits was observed.

Comparative Example 1

The production of an aromatic carbonate was conducted in substantially the same manner as in Example 1 except that the withdrawal of the evaporation-concentrated liquid formed in evaporator 14 (containing the catalyst and the aromatic polyhydroxy compound and the residue thereof) through conduit 20 was not conducted. Samples were taken from the reaction mixture withdrawn

from reaction vessel 100 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzo-phenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Sn were, respectively, 0.4, 1.0, 1.5 and 2.1. The composition of the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle at the point in time of 2,000 hours after the start of the operation was as follows: PhOH: 53 % by weight; MPC: 3.5 % by weight; DPC: 0.1 % by weight; ANS: 0.5 % by weight; and Sn: 0.3 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, the adhesion of the catalyst to a part of the inner wall of each of reaction vessel 100, evaporator 14, reboiler 17 and

conduits was observed.

Comparative Example 2

The production of an aromatic carbonate was conducted in substantially the same manner as in Example 1, except that phenol having a 4,4'-dihydroxy diphenyl concentration of 600 ppm by weight was used.

Samples were taken from the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Sn were, respectively, 0.9, 1.5, 2.0 and 2.6. The composition of the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle

at the point in time of 2,000 hours after the start of the operation was as follows: PhOH: 53 % by weight; MPC: 3.3 % by weight; DPC: 0.1 % by weight; ANS: 0.5 % by weight; and Sn: 0.3 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, the adhesion of the catalyst to a part of the inner wall of each of reaction vessel 100, evaporator 14 and conduits was observed.

Example 2

(Preparation of catalyst)

A mixture of 40 kg of phenol and 8 kg of titanium tetrachloride was heated to and maintained at 50 °C for 10 hours, thereby performing a reaction. After that period of time, hydrogen chloride formed in the resultant reaction mixture was distilled off together with unreacted phenol. Then, most of the remaining phenol was distilled off from the reaction mixture under reduced pressure, and the resultant mixture was allowed to cool under nitrogen atmosphere, to thereby obtain catalyst B.

(Production of aromatic carbonate)

The production of aromatic carbonate was conducted in substantially the same manner as in Example 1 except

that catalyst B was used in an amount such that the Ti concentration of the reaction mixture in conduit 13 became 0.2 % by weight.

The operation was conducted for 2,000 hours.

5 During this period of time, the operation could be stably conducted (for example, both the flow and the composition in each conduit were stable) without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing
10 liquid-phase mixture and the adhesion of the deposited catalyst to the inner wall of the reaction vessel and the like. Samples were taken from the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle provided on conduit 13, which
15 samples were, respectively, withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-
20 containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,000 hours, 1,500 hours and 2,000 hours
25 after the start of the operation, the weight ratios

(WRs) of the aromatic group-containing substance to Ti were, respectively, 0.37, 0.38, 0.39 and 0.40. The composition of the reaction mixture withdrawn from reaction vessel 100 through the above-mentioned sampling nozzle at the point in time of 2,000 hours after the start of the operation was as follows: PhOH: 51 % by weight; MPC: 6 % by weight; DPC: 0.4 % by weight; ANS: 0.4 % by weight; and Ti: 0.2 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, no adhesion of the catalyst to the inner wall of each of reaction vessel 100, evaporator 14, reboiler 17 and conduits was observed.

Example 3

(Preparation of catalyst)

A mixture of 40 kg of phenol and 8 kg of lead monoxide was heated to and maintained at 180 °C for 10 hours, thereby performing a reaction. After that period of time, water formed in the resultant reaction mixture was distilled off together with unreacted phenol, to thereby obtain catalyst C.

(Production of aromatic carbonate)

The production of an aromatic carbonate was conducted using an apparatus shown in Fig. 1, which com-

prises continuous multi-stage distillation column 1 composed of a plate column having a height of 6 m and a diameter of 6 inches and equipped with 20 sieve trays.

5 A mixture of dimethyl carbonate, phenol [concentration of 4,4'-dihydroxy diphenyl (i.e., an aromatic polyhydroxy compound) in phenol: 150 ppm by weight] and catalyst C was continuously fed in liquid form from conduit 3 through preheater 4 and conduit 5 to continuous multi-stage distillation column 1 at a position of
10 0.5 m below top 2 thereof at a rate of 32 kg/hr, and was allowed to flow down inside multi-stage distillation column 1, thereby performing a reaction. The weight ratio of the dimethyl carbonate to the phenol in the mixture was 62/38, and catalyst C was used in an
15 amount such that the Pb concentration of the reaction mixture in conduit 13 became 0.1 % by weight, wherein the Pb concentration can be confirmed using a sample withdrawn through a sampling nozzle (not shown) provided on conduit 13. Dimethyl carbonate was fed from
20 conduit 7 to evaporator 8 thereby forming a gas and the formed gas was fed from conduit 9 to bottom 6 of continuous multi-stage distillation column 1 at a rate of 26 kg/hr. The reaction conditions of the above reaction were such that the temperature at the bottom of
25 continuous multi-stage distillation column 1 was 203 °C

and the pressure at the top of continuous multi-stage distillation column 1 was 6.5 kg/cm²-G. Gas distilled from top 2 was led into condenser 11 through conduit 10, in which the gas was condensed. The resultant condensate was continuously withdrawn at a rate of 25 kg/hr through conduit 12. A reaction mixture, containing methyl phenyl carbonate (as a desired reaction product), the catalyst, and an aromatic polyhydroxy compound and a residue thereof, was continuously withdrawn from bottom 6 at a rate of 34 kg/hr and led into evaporator 14 through conduit 13, from which an evaporated gas containing the methyl phenyl carbonate was withdrawn and led through conduit 21 into condenser 22, in which the gas was condensed. The resultant condensate was withdrawn from condenser 22 through conduit 23 at a rate of 32.95 kg/hr. On the other hand, an evaporation-concentrated liquid containing the catalyst and the aromatic polyhydroxy compound and the residue thereof was formed in evaporator 14. A portion of the concentrated liquid was led into reboiler 17 through conduits 15 and 16 and recycled into evaporator 14 through conduit 18. The rest of the concentrated liquid in evaporator 14 was recycled into continuous multi-stage distillation column 1 at a rate of 1 kg/hr through conduits 15, 19 and 3. During the period of

time of from 400 hours to 3,000 hours after the start of the operation, a portion of the concentrated liquid formed in evaporator 14 was continuously withdrawn through conduit 20 at a rate of 0.05 kg/hr. Instead, catalyst C was added to continuous multi-stage distillation column 1 through conduit 3 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 20, so that the above-mentioned Pb concentration of 0.1 % by weight was able to be maintained in conduit 13. The operation was conducted for 3,000 hours. During this period of time, the operation could be stably conducted (for example, both the flow and the composition in each conduit were stable) without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner wall of continuous multi-stage distillation column 1 and the like. Samples were taken from the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy

benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Pb were, respectively, 0.11, 0.11, 0.12 and 0.12. The composition of the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13 at the point in time of 3,000 hours after the start of the operation was as follows: PhOH: 31 % by weight; MPC: 9 % by weight; DPC: 0.5 % by weight; ANS: 0.1 % by weight; and Pb: 0.1 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, no adhesion of the catalyst to the inner wall of each of continuous multi-stage distillation column 1, evaporator 14, reboiler 17 and conduits was observed.

Comparative Example 3

The production of an aromatic carbonate was conducted in substantially the same manner as in Example

3, except that the withdrawal of the evaporation-concentrated liquid formed in evaporator 14 (containing the catalyst and the aromatic polyhydroxy compound and the residue thereof) through conduit 20 was not conducted. Samples were taken from the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Pb were, respectively, 0.2, 0.7, 1.4 and 2.1. The composition of the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle at the point in time of 3,000 hours after the start of the operation was as follows: PhOH: 33 % by

weight; MPC: 6.5 % by weight; DPC: 0.2 % by weight;
ANS: 0.1 % by weight; and Pb: 0.1 % by weight. After
the operation was stopped, the conditions of various
parts of the apparatus were examined. As a result, the
adhesion of the catalyst to a part of the inner wall of
each of continuous multi-stage distillation column 1,
evaporator 14 and conduits was observed.

Comparative Example 4

The production of an aromatic carbonate was conducted in substantially the same manner as in Example 3, except that a by-produced phenol formed during the transesterification of diphenyl carbonate with bisphenol A to produce a polycarbonate was used. The phenol contained 15 % by weight of diphenyl carbonate and 500 ppm by weight of bisphenol A.

Samples were taken from the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substanc-

es (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Pb were, respectively, 0.7, 1.7, 2.6 and 4.0. The composition of the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle at the point in time of 3,000 hours after the start of the operation was as follows: PhOH: 34 % by weight; MPC: 5.8 % by weight; DPC: 0.2 % by weight; ANS: 0.1 % by weight; and Pb: 0.1 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, the adhesion of the catalyst to a part of the inner wall of each of continuous multi-stage distillation column 1, evaporator 14 and conduits was observed.

Example 4

The production of diphenyl carbonate from methyl phenyl carbonate was conducted using catalyst C obtained in Example 3, and an apparatus shown in Fig. 3, which comprises continuous multi-stage distillation

column 1 comprised of a plate column which has a height of 6 m and a diameter of 4 inch, and is equipped with 20 sieve trays.

A mixture of methyl phenyl carbonate and catalyst C was continuously fed in liquid form from conduit 3 through preheater 4 and conduit 5 to continuous multi-stage distillation column 1 at a position of 2.0 m below top 2 thereof at a rate of 10 kg/hr, and was allowed to flow down inside multi-stage distillation column 1, thereby performing a reaction. Catalyst C was used in an amount such that the Pb concentration of the reaction mixture in conduit 13 became 0.1 % by weight, wherein the Pb concentration can be confirmed using a sample withdrawn through a sampling nozzle (not shown) provided on conduit 13. The reaction conditions of the above reaction were such that the temperature at the bottom of continuous multi-stage distillation column 1 was 195 °C and the pressure at the top of continuous multi-stage distillation column 1 was 194 mmHg. Gas distilled from top 2 was led into condenser 26 through conduit 25, in which the gas was condensed. A portion of the resultant condensate was recycled into top 2 through conduits 27 and 28, and the rest of the condensate was continuously withdrawn at a rate of 2.4 kg/hr through conduits 27 and 29. A portion of the

reaction mixture containing diphenyl carbonate (as a desired reaction product), the catalyst, and an aromatic polyhydroxy compound and a residue thereof, was withdrawn from bottom 6 of continuous multi-stage distillation column 1 and recycled to bottom 6 through conduit 30, reboiler 31 and conduit 32. The rest of the reaction mixture was continuously withdrawn from bottom 6 at a rate of 7.6 kg/hr and led into evaporator 14 through conduit 13, from which an evaporated gas containing the diphenyl carbonate was withdrawn and led through conduit 21 into condenser 22, in which the gas was condensed. The resultant condensate was withdrawn from condenser 22 through conduit 23 at a rate of 5.55 kg/hr. On the other hand, an evaporation-concentrated liquid containing the catalyst and the aromatic polyhydroxy compound and the residue thereof was formed in evaporator 14. A portion of the concentrated liquid was led into reboiler 17 through conduits 15 and 16 and recycled into evaporator 14 through conduit 18. The rest of the concentrated liquid in evaporator 14 was recycled into continuous multi-stage distillation column 1 at a rate of 2 kg/hr through conduits 15, 19 and 3. During the period of time of from 400 hours to 3,000 hours after the start of the operation, a portion of the concentrated liquid formed in evaporator 14 was

continuously withdrawn through conduit 20 at a rate of 0.05 kg/hr. Instead, catalyst C was added to continuous multi-stage distillation column 1 through conduit 3 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 20, so that the above-mentioned Pb concentration of 0.1 % by weight was able to be maintained in conduit 13. The operation was conducted for 3,000 hours. During this period of time, the operation could be stably conducted (for example, both the flow and the composition in each conduit were stable) without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner wall of continuous multi-stage distillation column 1 and the like. Samples were taken from the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13, which samples were, respectively, withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in

each sample was conducted by the above-mentioned method. With respect to the samples respectively withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Pb were, respectively, 0.20, 0.21, 0.21 and 0.21. The composition of the reaction mixture withdrawn from continuous multi-stage distillation column 1 through the above-mentioned sampling nozzle provided on conduit 13 at the point in time of 3,000 hours after the start of the operation was as follows: MPC: 24.1 % by weight; DPC: 75.6 % by weight; and Pb: 0.1 % by weight. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, no adhesion of the catalyst to the inner wall of each of continuous multi-stage distillation column 1, evaporator 14, reboiler 17 and conduits was observed.

Example 5

The production of diphenyl carbonate was conducted using catalyst C prepared in Example 3, and the apparatus shown in Fig. 4.

A mixture of dimethyl carbonate, phenol (the concentration of 4-,4'-dihydroxyphenyl as an aromatic

polyhydroxy compound in the phenol: 200 ppm by weight) and methyl phenyl carbonate was fed in liquid form to continuous multi-stage distillation column 1 at a position 0.5 m below the top 2 thereof (which column was comprised of a plate column having a height of 12 m and a diameter of 8 inches, and provided with 40 sieve trays) at a rate of 31 kg/hr from conduit 3 through preheater 4 and conduit 5, thereby allowing the mixture to flow down inside continuous multi-stage distillation column 1 so as to perform a reaction. The composition of the mixture fed from conduit 3 was controlled so that the mixture flowing through conduit 5 during the operation (the mixture flowing through conduit 5 was comprised of a liquid introduced from conduit 19, which was recycled from evaporator 14; a liquid introduced from conduit 129, which was recycled from continuous multi-stage distillation column 101; and the above-mentioned mixture fed from conduit 3) had a composition of 49.9 % by weight of dimethyl carbonate, 44.7 % by weight of phenol and 4.9 % by weight of methyl phenyl carbonate. Dimethyl carbonate was fed through conduit 7 to evaporator 8, in which the dimethyl carbonate was subjected to evaporation. The resultant gas was fed to bottom 6 of continuous multi-stage distillation column 1 through conduit 9 at a rate of 55 kg/hr. Catalyst C

was fed from conduit 224 in such an amount that the Pb concentration at conduit 13 became 0.2 % by weight, wherein the Pb concentration can be confirmed using the reaction mixture withdrawn from a sampling nozzle (not shown) provided on conduit 13. Continuous multi-stage distillation column 1 was operated under conditions such that the temperature at the column bottom was 203 °C and the pressure at the column top was 6.5 kg/cm²-G. Continuous multi-stage distillation column 1 was clothed with a heat insulating material and a part of the column was heated by a heater (not shown). Gas distilled from top 2 of the column was led through conduit 10 to condenser 11, in which the gas was condensed. The resultant condensate was continuously withdrawn at a rate of 55 kg/hr from conduit 12. A reaction mixture was withdrawn continuously from bottom 6 at a rate of 31 kg/hr, and was led to evaporator 14 through conduit 13. In evaporator 14, an evaporation-concentrated liquid containing the catalyst and the aromatic polyhydroxy compound and residue thereof was formed. A portion of the concentrated liquid was recycled to evaporator 14 through conduits 15 and 16, reboiler 17 and conduit 18. The rest of the concentrated liquid was recycled into continuous multi-stage distillation column 1 at a rate of 1 kg/hr

through conduits 15, 19 and 3. During the period of time from 400 hours to 3000 hours after the start of the operation, a portion of the concentrated liquid formed in evaporator 14 was continuously withdrawn from conduit 20 at a rate of 0.05 kg/hr. Instead, catalyst C was fed from conduit 224 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 20, so that the above-mentioned Pb concentration of 0.2 % by weight was able to be maintained in conduit 13. On the other hand, an evaporated gas formed in evaporator 14 was led into condenser 22 through conduit 21, in which the gas was condensed. The resultant condensate was fed to continuous multi-stage distillation column 101 at a position of 2.0 m below top 102 thereof through conduits 23 and 105, which column was comprised of a plate column having a height of 6 m and a diameter of 10 inches, and provided with 20 sieve trays, thereby performing a reaction. The composition of the mixture in conduit 105 was as follows: dimethyl carbonate: 43.1 % by weight; phenol: 24.5 % by weight; methyl phenyl carbonate: 27.1 % by weight; and diphenyl carbonate: 4.5 % by weight (the mixture at conduit 105 was comprised of a liquid introduced from conduit 23 and a liquid introduced from conduit 119, which was recycled from evaporator 114).

Catalyst C was fed from conduit 124 in an amount such that the Pb concentration at conduit 113 became 0.2 % by weight, wherein the Pb concentration can be confirmed using a sample withdrawn from a sampling nozzle (not shown) provided on conduit 113. Continuous multi-stage distillation column 101 was operated under conditions such that the temperature at the column bottom was 198 °C and the pressure at the column top was 280 mmHg. Gas distilled from column top 102 was led through conduit 125 to condenser 126, in which the gas was condensed. A portion of the resultant condensate was recycled into column top 102 through conduit 128, and the rest of the condensate was recycled into continuous multi-stage distillation column 1 through conduits 127 and 129, preheater 4 and conduit 5. After the start of the recycling of the condensate into continuous multi-stage distillation column 1 through conduit 129, phenol (having a concentration of 4,4'-dihydroxydiphenyl as an aromatic polyhydroxy compound of 200 ppm by weight) was added to the mixture fed from conduit 3 in an amount such that the above-mentioned composition of the mixture at conduit 5 can be maintained. A portion of the reaction mixture at bottom 106 of continuous multi-stage distillation column 101 was led into reboiler 131 through conduit 130, and

recycled into column bottom 106 through conduit 132, and the rest of the reaction mixture was led to evaporator 114 through conduit 113 at a rate of 6.9 kg/hr. In evaporator 114, an evaporation-concentrated liquid containing the catalyst and the aromatic polyhydroxy compound and the residue thereof was formed. A portion of the concentrated liquid was led into reboiler 117 through conduits 115 and 116 and recycled into evaporator 114 through conduit 118. The rest of the concentrated liquid in evaporator 114 was recycled into continuous multi-stage distillation column 101 through conduits 115, 119 and 105 at a rate of 2 kg/hr. During the period of time of from 400 hours to 3,000 hours after the start of the operation, a portion of the concentrated liquid formed in evaporator 114 was continuously withdrawn through conduit 120 at a rate of 0.1 kg/hr. Instead, catalyst C was fed from conduit 124 in such an amount as to compensate for the amount of the catalyst withdrawn from conduit 120, so that the above-mentioned Pb concentration of 0.2 % by weight can be maintained in conduit 113. On the other hand, an evaporated gas formed in evaporator 114 was led to condenser 122 through conduit 121 and withdrawn through conduit 123 at a rate of 6.8 kg/hr. The liquid-phase mixture withdrawn from conduit 123 had a diphenyl

carbonate content of 98 % by weight. The operation was conducted for 3,000 hours. During this period of time, the operation could be stably conducted (for example, both the flow and the composition in each conduit were stable) without suffering disadvantageous phenomena, such as the clogging of a conduit, which is liable to be caused by the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of catalyst to the inner wall of the conduit.

Samples were taken from the reaction mixtures withdrawn from continuous multi-stage distillation columns 1 and 101, respectively, through the sampling nozzle provided on conduit 13 and the sampling nozzle provided on conduit 113, which samples were withdrawn at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation. The determination of the concentrations of dihydroxy diphenyl, dihydroxy benzophenone, and residues thereof as aromatic group-containing substances (i.e., an aromatic polyhydroxy compound and a residue thereof) in each sample was conducted by the above-mentioned method. With respect to the samples withdrawn through conduit 13, respectively, at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic

group-containing substance to Pb were, respectively, 0.40, 0.41, 0.42 and 0.42. With respect to the samples withdrawn through conduit 113, respectively, at points in time of 500 hours, 1,200 hours, 2,100 hours and 3,000 hours after the start of the operation, the weight ratios (WRs) of the aromatic group-containing substance to Pb were, respectively, 0.16, 0.17, 0.17 and 0.18. After the operation was stopped, the conditions of various parts of the apparatus were examined. As a result, no adhesion of the catalyst to the inner wall of each of continuous multi-stage distillation column 1, evaporator 14, reboiler 17, and conduits was observed.

INDUSTRIAL APPLICABILITY

According to the present invention, in a process for producing an aromatic carbonate by transesterification of a starting material with a reactant in the presence of a metal-containing catalyst, the transesterification is conducted while maintaining a weight ratio (WR) of at least one aromatic group-containing substance selected from the group consisting of a specific aromatic polyhydroxy compound and a residue thereof to the metal of the metal-containing catalyst at 2.0 or less, wherein the weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for the transesterification, and wherein the aromatic group-containing substance originates from the starting material, the reactant and/or a by-product of the transesterification. By the process of the present invention, the transesterification reaction can be conducted without suffering disadvantageous phenomena, such as the deposition of the catalyst from the catalyst-containing liquid-phase mixture and the adhesion of the deposited catalyst to the inner walls of the reactor, pipes and the like, so that the desired aromatic carbonate can be produced stably for a prolonged period of time.

In conducting a transesterification reaction for

producing an aromatic carbonate, which is important, .
for example, as a raw material for producing an aromat-
ic polycarbonate, the process of the present invention
can be advantageously used either when the reaction is
5 performed in a batchwise manner or when the reaction is
performed in a continuous manner. According to the
present invention, especially when the production of an
aromatic carbonate is conducted in a continuous manner,
the continuous production of an aromatic carbonate can
10 be conducted extremely efficiently for a prolonged
period of time by withdrawing a part of the catalyst-
containing liquid-phase mixture out of a system for the
transesterification.

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CLAIMS

1. In a process for producing an aromatic carbonate which comprises transesterifying, in the presence of a metal-containing catalyst, a starting material selected from the group consisting of a dialkyl carbonate represented by the following formula (1):



an alkyl aryl carbonate represented by the following formula (2):



and a mixture thereof with a reactant selected from the group consisting of an aromatic monohydroxy compound represented by the following formula (3):



an alkyl aryl carbonate represented by the following formula (4):



and a mixture thereof,

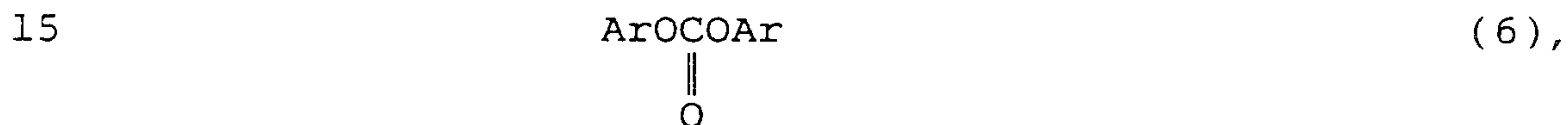
wherein each of R^1 , R^2 and R^3 independently represents an alkyl group having 1 to 10 carbon atoms, an alicyclic group having 3 to

10 carbon atoms or an aralkyl group having 6
to 10 carbon atoms and each of Ar^1 , Ar^2 and
 Ar^3 independently represents an aromatic
group having 5 to 30 carbon atoms,

5 to thereby produce at least one aromatic carbonate
selected from the group consisting of an alkyl aryl
carbonate and a diaryl carbonate, which is selected in
correspondence to the starting material and the react-
ant and represented by at least one formula selected
10 from the group consisting of the following formulae (5)
and (6):



and



wherein R and Ar are, respectively, selected
from R^1 , R^2 and R^3 and selected from Ar^1 ,
15 Ar^2 and Ar^3 in correspondence to the start-
20 ing material and the reactant,
the improvement in which said transesterification is
conducted while maintaining a weight ratio (WR) of at
least one aromatic group-containing substance selected
from the group consisting of an aromatic polyhydroxy
25 compound and a residue thereof to the metal of said

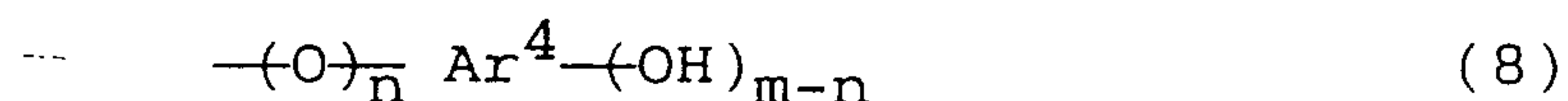
metal-containing catalyst at 2.0 or less, wherein said weight ratio (WR) is measured with respect to a catalyst-containing liquid-phase mixture in a system for said transesterification, and wherein said aromatic group-containing substance originates from at least one member selected from the group consisting of said starting material, said reactant and a by-product of said transesterification,

said aromatic polyhydroxy compound being represented by the following formula (7):



wherein Ar^4 represents an aromatic group having a valence of m , m represents an integer of 2 or more, and each $-\text{OH}$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group, and

said residue of the aromatic polyhydroxy compound being represented by the following formula (8):



wherein Ar^4 and m are as defined above, n represents an integer of from 1 to m , and each of the $-\text{OH}$ group and the $-\text{O}-$ group is individually bonded to an arbitrary ring-carbon position of the Ar^4 group,

and being present in such a form as chemically bonded

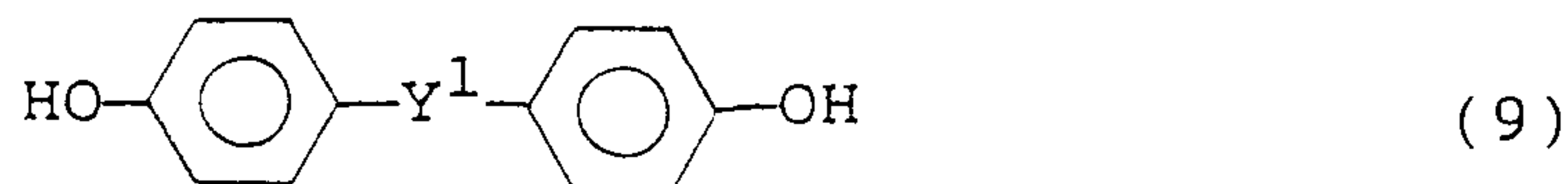
to at least one member selected from the group consisting of the metal of said catalyst, an alkoxycarbonyl group derived from said dialkyl carbonate or said alkyl aryl carbonate, an aryloxycarbonyl group derived from said alkyl aryl carbonate or said diaryl carbonate, and a carbonyl group derived from said dialkyl carbonate, said alkyl aryl carbonate or said diaryl carbonate.

2. The process according to claim 1, wherein said aromatic polyhydroxy compound is at least one member selected from the group consisting of:

(A) an oxidation product of an aromatic monohydroxy compound as said reactant,

(B) at least one member selected from the group consisting of a product produced by the Fries rearrangement of a diaryl carbonate obtained by said transesterification and an oxidation product of said product and

(C) at least one member selected from the group consisting of aromatic dihydroxy compounds derived from phenol as the reactant and represented by the following formula (9):



wherein Y^1 represents a single bond, a
divalent alkane group having 1 to 30 carbon
atoms or a divalent group selected from -O-,
-CO-, -S-, -SO₂-, -SO- and -COO-, and

5 oxidation products of said aromatic dihydroxy compounds.

3. The process according to claim 1 or 2, wherein the
maintenance of said weight ratio (WR) at 2.0 or less is
performed by using as the reactant an aromatic monohy-
10 droxy compound containing said aromatic polyhydroxy
compound in a controlled concentration, and withdrawing
a part of said catalyst-containing liquid-phase mixture
out of said system for the transesterification.

15 4. The process according to claim 3, wherein said
aromatic monohydroxy compound has an aromatic polyhy-
droxy compound concentration of 400 ppm by weight or
less.

20 5. The process according to claim 1, which is for
continuously producing said at least one aromatic
carbonate, wherein a transesterification reaction
mixture containing said at least one aromatic carbonate
and containing said catalyst is continuously withdrawn
25 from a reactor for said transesterification.

6. The process according to claim 5, wherein said aromatic monohydroxy compound as the reactant comprises a mixture of a feedstock aromatic monohydroxy compound and an unreacted aromatic monohydroxy compound recycled from said reactor, wherein said feedstock aromatic monohydroxy compound has an aromatic polyhydroxy compound concentration of 400 ppm by weight or less.

7. The process according to claim 5 or 6, wherein a part of said reaction mixture, containing said catalyst, withdrawn from said reactor is subjected to evaporation, and the resultant mixture having an increased catalyst concentration is at least partly withdrawn out of said system for the transesterification to thereby maintain said weight ratio (WR) at 2.0 or less.

8. The process according to any one of claims 5 to 7, wherein said starting material and said reactant are continuously fed to a continuous multi-stage distillation column to effect a transesterification reaction therebetween in at least one phase selected from a liquid phase and a gas-liquid phase in the presence of the metal-containing catalyst in said distillation column, while continuously withdrawing a high boiling

point reaction mixture containing said at least one
aromatic carbonate in a liquid form from a lower por-
tion of the distillation column and continuously with-
drawing a low boiling point reaction mixture containing
5 a by-product in a gaseous form from an upper portion of
the distillation column by distillation.

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FIG.1

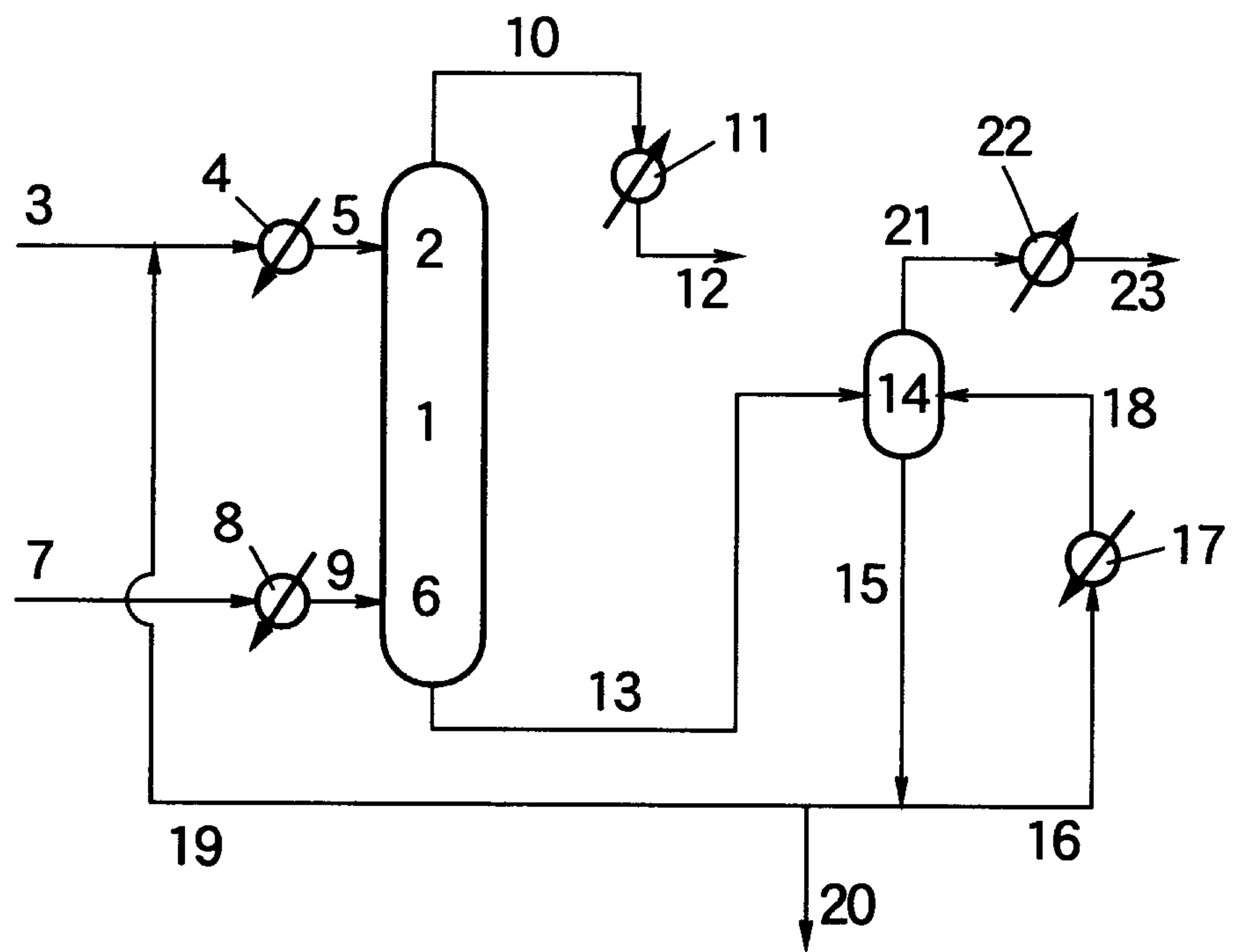


FIG.2

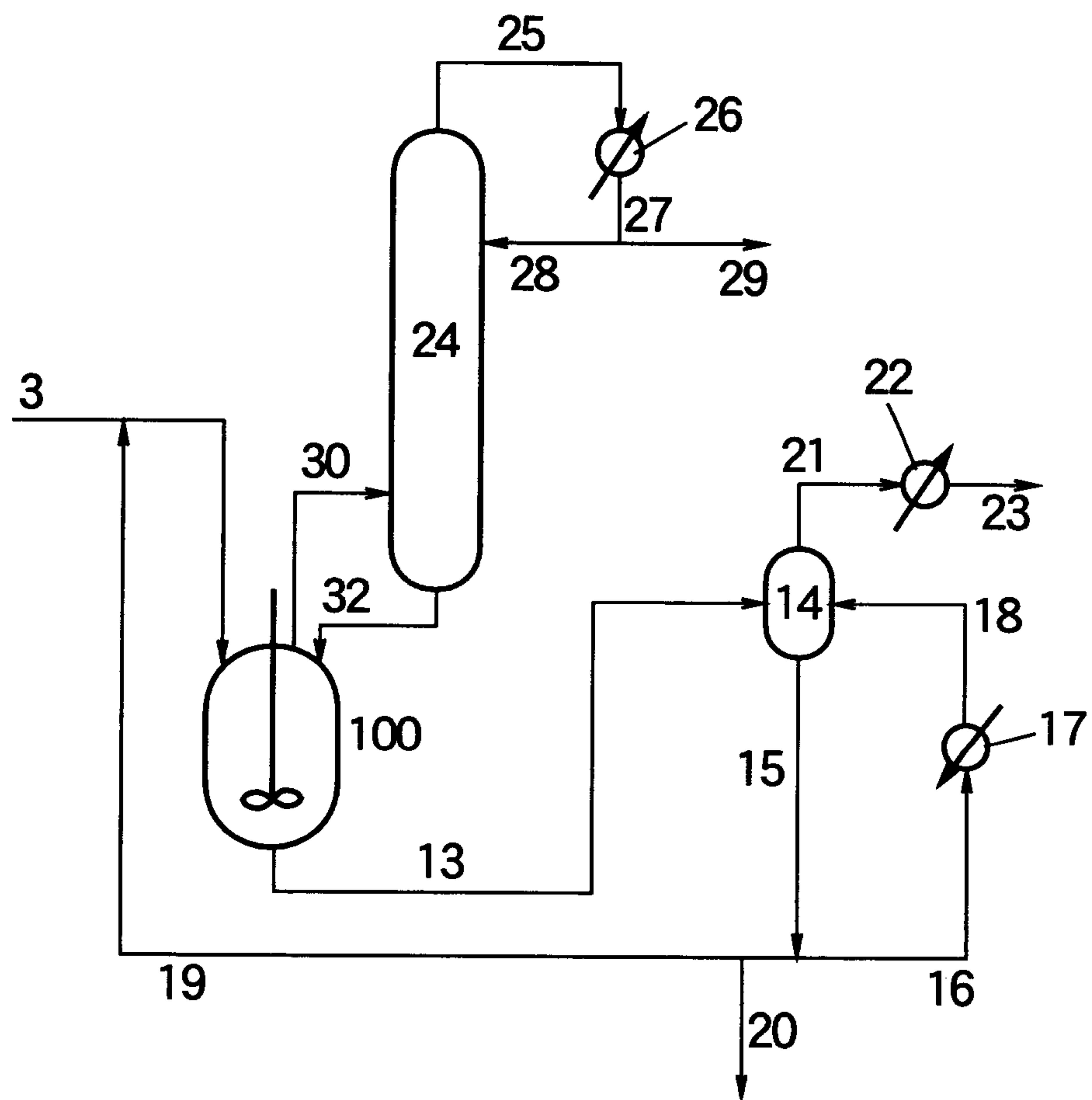


FIG.3

