



(12) UK Patent (19) GB (11) 2 151 866 (13) B

(54) Title of invention

Switched capacitor s-correction circuit

(51) INTCL⁴; H04N 3/233

(21) Application No
8431540

(22) Date of filing
13 Dec 1984

(30) Priority data

(31) 562246

(32) 16 Dec 1983

(33) United States of America
(US)

(43) Application published
24 Jul 1985

(45) Patent published
25 Mar 1987

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(52) Domestic classification
(Edition I)
H3T 2B3 2B4 2RX 2T2X 2W2 2W3
30C 30R 3V 40S 4D 4E2N 5E LAA

(56) Documents cited
None

(58) Field of search
H3T

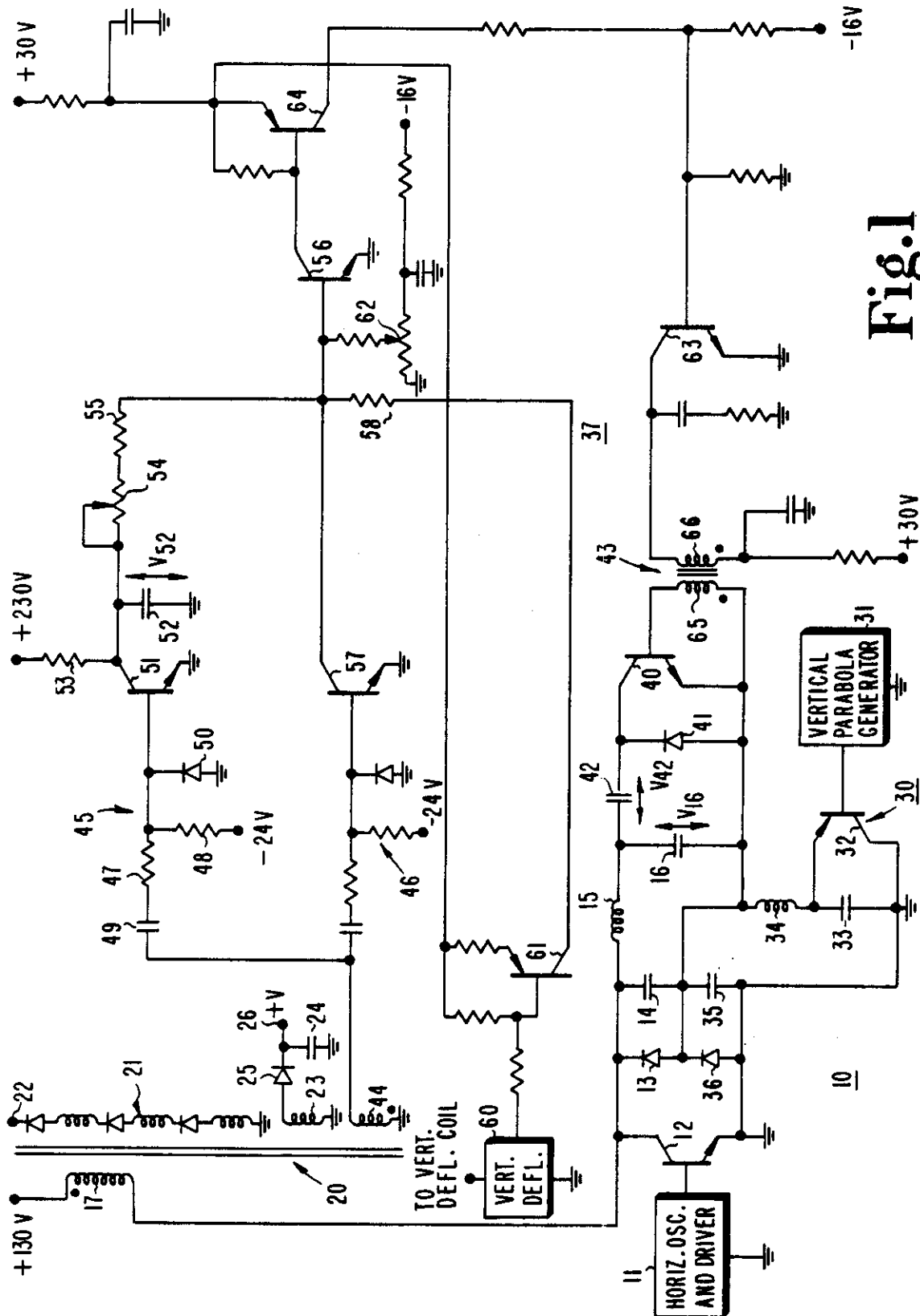
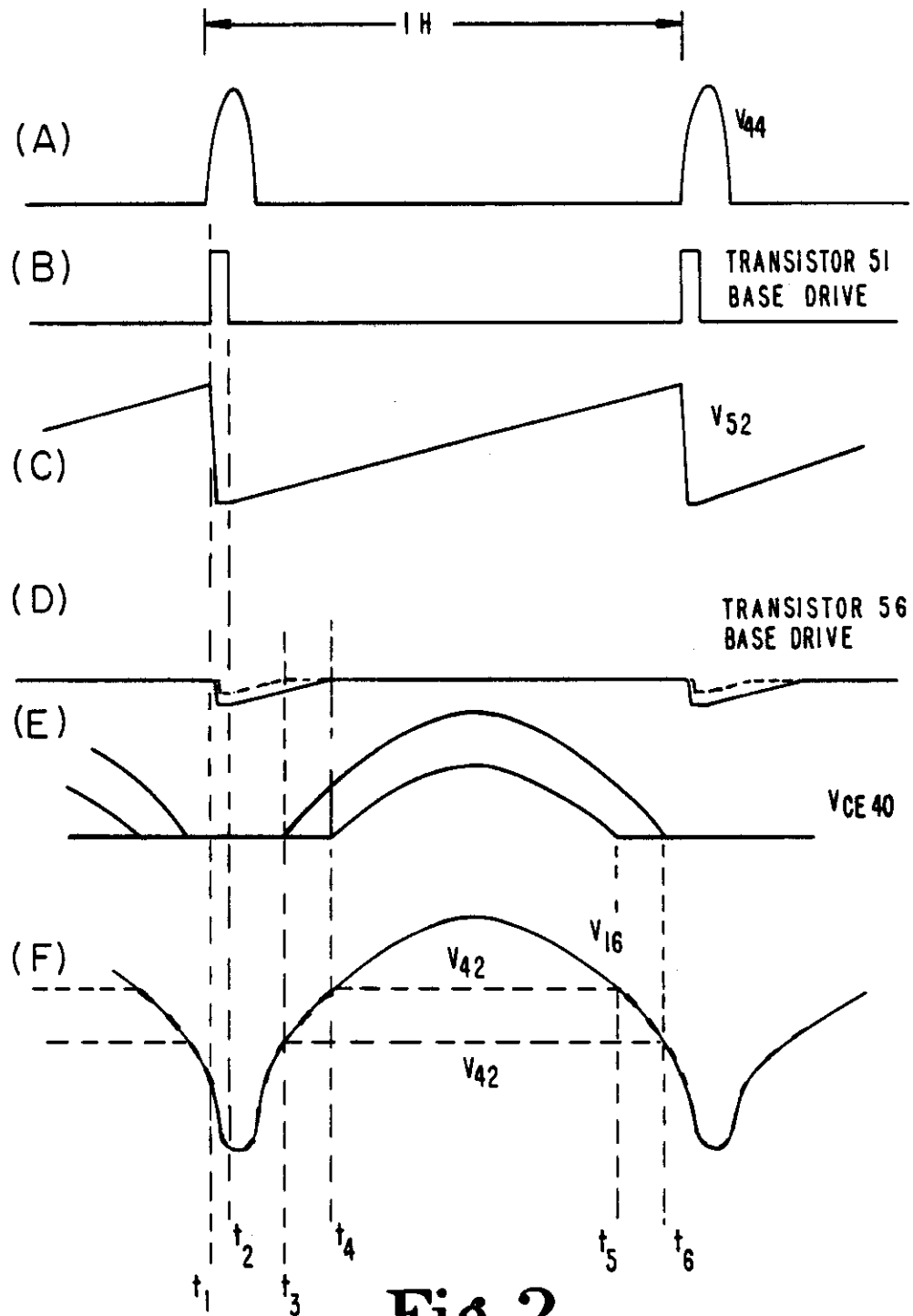
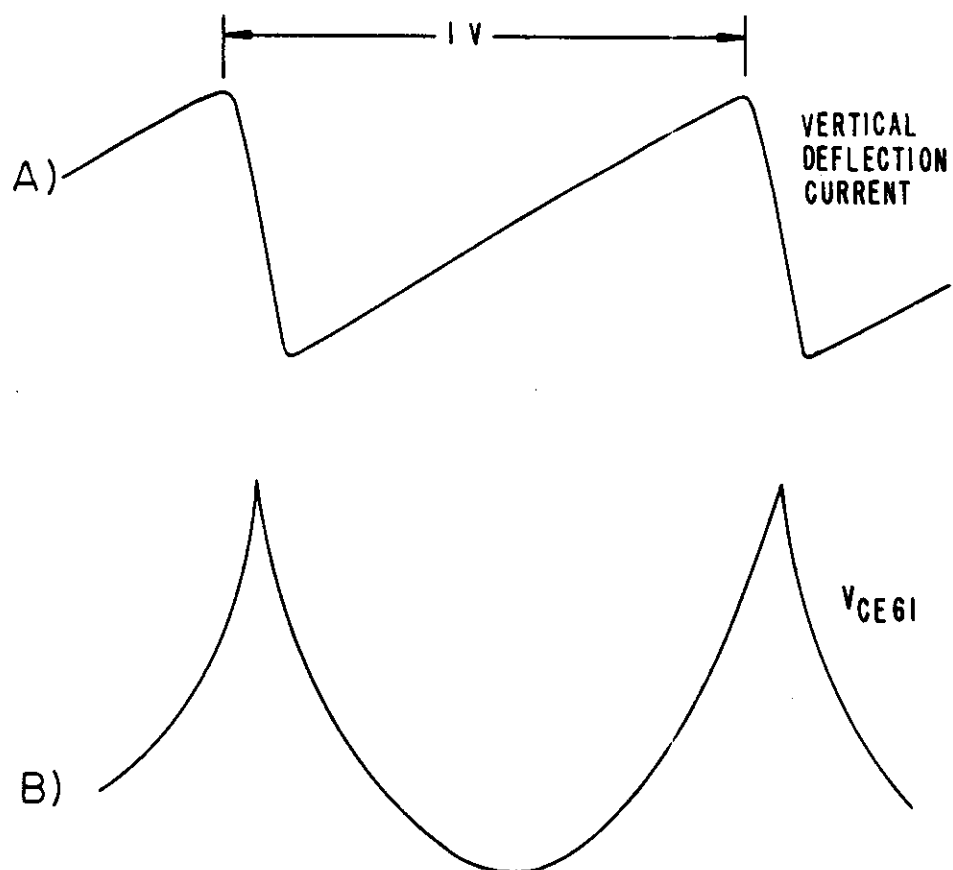


Fig. 1

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**Fig.2**

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**Fig.3**

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1 SWITCHED CAPACITOR S-CORRECTION CIRCUIT

2 This invention relates to correction of cathode
3 ray tube geometry distortion, and in particular, to
4 deflection current S-correction for cathode ray tubes
5 having complex correction requirements.

6 The cathode ray tube of a video display apparatus
7 incorporates an electron gun assembly which produces an
8 electron beam or beams. The beams are deflected or
9 scanned to form a raster on a phosphor display screen
10 located on the inside surface of the front panel of the
11 tube. The radius of curvature of the front panel is
12 greater than the distance from the deflection center of
13 the electron beams to the center of the display screen
14 (i.e., the deflection distance). Because of the
15 difference in radii, the electron beams travel a greater
16 distance to the edges of the display screen than to the
17 center of the screen. For a given amount of deflection,
18 therefore, the beams will traverse a greater distance on
19 the display screen near the edges than at the center of
20 the screen. This causes the picture on the screen to
21 appear stretched at the edges compared to the center. The
22 solution to this problem has previously been the inclusion
23 of a capacitor in series with the horizontal or line
24 deflection winding. This capacitor has the effect of
25 varying the amplitude of the horizontal deflection
26 current, so that the sawtooth deflection current waveform
27 resembles an "S" shape. This S-correction reduces the
28 amount of deflection of the electron beams near the edges
29 of the screen, thereby compensating for the previously
30 described tube geometry distortion.

31 For picture tubes having large deflection angles,
32 e.g., 110° or greater, or for tubes having an
33 unconventional faceplate curvature, the previously
34 described geometry correction may not be sufficient. For
35 example, insufficient correction may occur with tubes
36 having a front panel with a spherical radius of curvature
37 greater than a conventional tube, or with tubes having a
38 complex or compound faceplate curvature with multiple

1 radii, such as is described in U.S. Patent Application
Serial Number 469,775, filed February 25, 1983, in the
names of D'Amato et al. and entitled "Cathode Ray Tube
Having Different Curvatures Along Major and Minor Axes"
5 corresponding to German OLS 3406787 and GB 2136199A.

With these tubes, a single S-shaping capacitor may
not be able to provide the desired amount of correction at
all screen locations, and may provide too much or too little
correction at different regions of the screen.

10 The present invention is directed to an
S-correction circuit that provides effective correction
for tubes having large deflection angles or complex
faceplate contours.

15 In accordance with the present invention, a
horizontal or line deflection circuit comprises a horizontal
deflection winding and a circuit for providing a deflection
current in the winding, which current defines a trace and a
retrace interval. A first capacitor is coupled to the
deflection winding and provides linearity distortion correction to the
deflection current. A second capacitor is selectively coupled to the
deflection winding during portions of each of said deflection intervals
for supplying additional amounts of linearity distortion correction to
the deflection current during each of those portions.

25 In the accompanying drawing, FIGURE 1 is a
schematic and block diagram of a portion of a television
receiver incorporating a correction circuit in accordance
with an aspect of the present invention; and

FIGURES 2 and 3 illustrate waveforms associated
with the circuit of FIGURE 1.

30 Referring to FIGURE 1, there is shown a portion
of a video display apparatus, such as a television
receiver, incorporating a horizontal or line deflection
circuit 10. The horizontal deflection circuit 10 includes
horizontal oscillator and driver circuits 11 which apply
35 switching signals to the base of a horizontal output
transistor 12. Coupled to the horizontal output
transistor 12 is a damper diode 13, a retrace
capacitor 14, a horizontal deflection winding 15 and an

1 S-shaping capacitor 16. Power is provided to the horizontal output circuit 10 from a power supply of the order of +130 volts via a primary winding 17 of a power transformer 20.

5 Transformer 20 generates a source of high voltage at a terminal 22 via windings 21. The high voltage potential, of the order of 30 KV, is applied to the anode or ultor terminal of a kinescope (not shown).

10 Transformer 20 also provides power to other receiver circuits. This is illustratively shown in FIGURE 1 by secondary winding 23, filter capacitor 24 and rectifying diode 25, which provides a voltage level designated +V at a terminal 26.

Horizontal deflection circuit 10 generates a
15 sawtooth current in horizontal deflection winding 15 which in turn produces a deflection field which deflects the electron beams of the kinescope. The electron beams are deflected to form a raster on the display screen of the kinescope. Since the electron beams are deflected farther
20 to the corners of the raster than to the edges, the sides of the raster will appear inwardly bowed or pincushion shaped.

In order to correct the previously described side, or east-west, pincushion distortion, horizontal
25 deflection circuit 10 incorporates a diode modulator correction circuit 30 which modulates the horizontal deflection current at a vertical deflection rate in a parabolic manner. Diode modulator circuit 30 incorporates a vertical parabola generator 31 which applies a parabolic
30 vertical rate signal to a transistor 32. Diode modulator circuit 30 also comprises a modulator capacitor 33, a modulator inductor 34, a modulator retrace capacitor 35 and a modulator diode 36. Conduction of transistor 32 controls the voltage across modulator capacitor 33 in
35 order to vary the modulator capacitor voltage in a parabolic manner. This in turn varies the horizontal deflection trace voltage in order to provide correction of side pincushion distortion.

1 As previously described, picture tubes having
large deflection angles and/or compound curvature
faceplates may require a more complex form of S-correction
than is provided by the single S-shaping capacitor 16. In
5 accordance with an aspect of the present invention,
FIGURE 1 illustrates an S-correction circuit 37 which
provides effective S-correction for picture tubes having
complex S-correction requirements. S-correction
circuit 37 includes a switching transistor 40, a diode 41
10 and a capacitor 42. Switching of transistor 40 into
conduction has the effect of placing capacitor 42 in
parallel with S-shaping capacitor 16, thereby increasing
the amount of circuit S-shaping capacitance. Two values
of S-shaping capacitance may be presented to the
15 horizontal deflection circuit; namely, the value of
capacitor 16 and the value of the parallel combination of
capacitors 16 and 42. This allows the amount of S-shaping
correction to be changed for different portions of the
horizontal deflection interval.

20 Switching pulses are applied to the base of
transistor 40 via a transformer 43. Transformer 43
permits the application of a fixed amplitude pulse to the
base of transistor 40 independent of the emitter voltage,
which follows the pincushion correcting parabola voltage
25 produced by diode modulator correction circuit 30.

As previously described, certain cathode ray tube
geometries or tubes having large deflection angles may
require different amounts of S-correction during a given
horizontal scan line. With some tubes, it may be
30 sufficient to control the S-correction switching to occur
at the same time during each horizontal deflection
interval. Other tubes, for example those having a complex
curvature faceplate, may have a contour that requires the
S-correction switching to be advanced or retarded during
35 the course of the vertical or field deflection interval.
S-correction circuitry 37 of FIGURE 1 produces switching
pulses for transistor 40 which may be modulated with
respect to their time of occurrence within the horizontal

1 deflection interval.

Horizontal retrace derived pulses, shown in FIGURE 2A, produced across winding 44 of transformer 20, are applied to differentiator circuits 45 and 46.

5 Differentiator circuit 45, comprising capacitor 49, resistors 47 and 48, and diode 50, differentiates the leading edges of the horizontal rate pulses from winding 44 in order to produce a short duration pulse, illustratively shown in FIGURE 2B, that is used to turn
10 transistor 51 on for approximately 5 microseconds.

Capacitor 52, together with resistor 53 and the +230 volt supply, form a ramp generator. Turn-on of transistor 51 causes capacitor 52 to discharge through transistor 51 to ground, thereby resetting the ramp.
15 Capacitor 52 discharges very quickly, as shown in FIGURE 2C, so that it is completely discharged before transistor 51 is turned off. When transistor 51 is turned off, capacitor 52 charges through resistor 53 to form a horizontal rate ramp signal, shown in FIGURE 2C, that is
20 applied via variable resistor 54 and resistor 55 to the base of a transistor 56. Variable resistor 54 controls the amplitude of the ramp signal that is applied to transistor 56.

Differentiator 46 produces a short duration pulse
25 which turns transistor 57 on and off coincident with the switching of transistor 51. Conduction of transistor 57 rapidly removes the charge from the base region of transistor 56 so that transistor 56 turns off very quickly when the horizontal rate ramp is reset.

30 Vertical deflection circuit 60, in addition to generating a sawtooth vertical deflection current, shown in FIGURE 3A, for a vertical deflection winding (not shown), provides a vertical rate parabolic voltage signal which is inverted by transistor 61 to form a signal as
35 shown in FIGURE 3B. This vertical rate parabolic voltage is added to the horizontal rate ramp voltage to form a signal, as shown in FIGURE 2D, that is applied to the base of transistor 56 through resistor 58. The vertical parabola voltage has the

1 effect of changing the dc level of the horizontal ramp, as
illustrated by the solid and dashed waveforms of FIGURE
2D. This variation in dc level over the course of the
vertical deflection interval modulates the turn-on time of
5 transistor 56 at a vertical rate. Variable resistor 62 is
adjustable to set the dc bias on the base of transistor 56
in order to control the point at which transistor 56
switches. The circuit of FIGURE 1 is illustratively
10 configured to cause transistor 56 to turn on earlier in
the horizontal deflection interval near the top and bottom
of the scanned raster; i.e., where the vertical rate
parabolic voltage is greatest. This is shown by the
dashed waveform in FIGURE 2D. A different cathode ray
tube faceplate contour may, however, require a different
15 modulation in which transistor 56 would turn on later
during horizontal deflection intervals near the top and
bottom of the raster. Such a requirement could be
satisfied, for example, by removing transistor 61, which
would eliminate the inversion of the parabolic voltage
20 signal from vertical deflection circuit 60. Other circuit
modifications to satisfy particular modulation
requirements are, of course, possible.

Conduction of transistor 56 provides a low
impedance current path which clamps the base drive signal,
25 as shown in FIGURE 2D. Conduction of transistor 56 also
causes transistor 63 to conduct, via switching of
amplifying transistor 64. Conduction of transistor 63
causes current to flow in winding 66 of transformer 43
from the +30 volt supply, through winding 66 and
30 transistor 63 to ground. This causes a current to flow in
winding 65 of transformer 43 which, because of the
coupling polarity of windings 65 and 66, will turn
transistor 40 off. As can be seen in FIGURE 2E,
transistor 40 is turned off at time t_3 in response to
35 the dashed waveform of FIGURE 2D, and at time t_4 in
response to the solid waveform of FIGURE 2D. This
illustrates the modulation of the switching of transistor
40 in response to the level of the vertical parabola

1 voltage signal. The turn-off time of transistor 40 will
occur during the first half of the horizontal trace
interval. With transistor 40 turned off, the voltage
across capacitor 42 will remain constant, as shown in
5 FIGURE 2F, while the voltage across S-shaping capacitor 16
continues to rise, as shown also in FIGURE 2F. During the
second half of the horizontal trace interval, the voltage
across capacitor 16 begins to decrease. When the voltage
across capacitor 16 equals the voltage across capacitor
10 42, diode 41 will begin to conduct, and capacitor 42
begins to discharge, thereby influencing the S-correction
of the deflection current. Diode 41 will continue to
conduct until the center of the horizontal retrace
interval, when the direction of deflection current
15 reverses. Resetting of the horizontal rate ramp voltage
generated across capacitor 52 causes transistor 40 to
begin conducting which in turn causes capacitor 42 to
charge again, until transistor 40 is turned off as
previously described. It is important that transistor 40
20 be turned on when its collector voltage is near zero in
order to prevent a potentially damaging current surge in
the transistor when it is turned on. To accomplish this
objective, transistor 40 should be turned on when diode 41
is conducting.

25 The charge on capacitor 42, determined by the
length of conduction of transistor 40, will also determine
the time at which diode 41 begins to conduct after
transistor 40 is turned off. As can be seen in FIGURE 2F,
the charge and discharge intervals of capacitor 42, hence
30 the intervals when capacitor 42 contributes to
S-correction, are symmetrical about the center of the
horizontal trace interval for both transistor 40 turn off
times of either t_3 or t_4 . This occurs because the
time at which diode 41 begins to conduct will always occur
35 when the voltage level across capacitor 16 is equal to the
same level as it was when transistor 40 was turned off.
Symmetry of S-correction about the center of horizontal
trace is therefore achieved regardless of the time at

1 which transistor 40 is turned off.

 The previously described S-correction circuit
therefore provides switchable amounts of correction during
a given line deflection interval. The point at which the
5 S-correction switching occurs in a given line may be
controlled in order to increase the flexibility of the
correction circuit.

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1 CLAIMS

1. A line deflection circuit comprising:
a line deflection winding;
means for providing a deflection current in said
5 line deflection winding, said deflection current defining
deflection intervals having trace and retrace
intervals;

a first capacitor coupled to said deflection
winding for providing linearity distortion correction to
10 said deflection current;

a second capacitor; and
means for selectively coupling said second capacitor to said
deflection winding during portions of each of said deflection intervals
for supplying additional amounts of linearity distortion correction
15 to said deflection current during each of said portions of said
deflection intervals.

2. A circuit as defined in Claim 1, wherein
said means for coupling said second capacitor to said
20 deflection winding comprises means for controlling the
instant within said deflection interval that said coupling
occurs.

3. A circuit as defined in Claim 2, wherein
25 said controlling means controls the time of coupling of
said second capacitor to said deflection winding in
response to a field deflection rate signal.

4. A circuit as defined in Claim 1, wherein
30 said means for coupling said second capacitor to said
deflection winding comprises a switch coupled to said
second capacitor for selectively completing a current path
through said second capacitor when said switch is closed
for coupling said second capacitor to said deflection
35 winding and for preventing current flow through said
capacitor when said switch is open for causing said second
capacitor to be decoupled from said deflection winding.

1 5. A circuit as defined in Claim 4, wherein
said switch comprises a transistor, said transistor being
rendered conductive when said switch is closed for causing
the voltage level across said second capacitor to equal
5 the voltage level across said first capacitor, said
transistor being rendered nonconductive when said switch
is open for causing the voltage level across said second
capacitor to remain constant at the voltage level that is
across said second capacitor when said transistor is
10 rendered nonconductive.

6. A circuit as defined in Claim 1, wherein
said second capacitor is coupled in parallel with said
first capacitor.
15

7. A circuit as defined in Claim 1, wherein
said second capacitor is coupled to said deflection
winding during a first interval occurring during the first
half of said trace interval and a second interval
20 occurring during the second half of said trace interval.

8. A circuit as defined in Claim 7, wherein
said means for coupling said second capacitor to said
deflection winding comprises means for maintaining the
25 duration of said second interval substantially equal to
the duration of said first interval in order to maintain
symmetry of said linearity correction.

9. A circuit as defined in Claim 8, wherein
30 said means for maintaining said first and second interval
durations equal comprises a diode for coupling said second
capacitor to said deflection winding during one of said
first and second intervals.

35 10. A line deflection circuit substantially
as hereinbefore described with reference to the
accompanying drawings.

REGISTER ENTRY FOR GB2151866 ✓

Form 1 Application No GB8431540.7 filing date 13.12.1984 ✓

Priority claimed:

16.12.1983 in United States of America - doc: 562246

Title SWITCHED CAPACITOR S-CORRECTION CIRCUIT

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Classified to

H3T H4T

H04N

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Publication No GB2151866 dated 24.07.1985

Examination requested 02.01.1986

Patent Granted with effect from 25.03.1987 (Section 25(1)) with title SWITCHED
CAPACITOR S-CORRECTION CIRCUIT

30.05.1989 RCA LICENSING CORPORATION, Incorporated in USA - Delaware, Two
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by virtue of deed of assignment dated 08.12.1987. Certified copy
filed on GB2198311

Entry Type 8.4 Staff ID. WE1 Auth ID. F21

28.10.1991 Application under Section 32 filed on 21.10.91.

Entry Type 10.1 Staff ID. MM Auth ID. EO

- 31.10.1991 Notification of change of Applicant/Proprietor name of
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dated 21.10.1991. Official evidence filed on GB2215154
Entry Type 7.1 Staff ID. MM Auth ID. EO

**** END OF REGISTER ENTRY ****

OA80-01
FG

OPTICS - PATENTS

20/11/91 15:20:05
PAGE: 1

RENEWAL DETAILS

PUBLICATION NUMBER

GB2151866

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America

DATE FILED

13.12.1984

DATE GRANTED

25.03.1987

DATE NEXT RENEWAL DUE

13.12.1992

DATE NOT IN FORCE

DATE OF LAST RENEWAL

13.11.1991

YEAR OF LAST RENEWAL

08

STATUS

PATENT IN FORCE