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CA 2333517 C 2004/01/20

(11)(21) **2 333 517**

(12) **BREVET CANADIEN
CANADIAN PATENT**

(13) **C**

(22) Date de dépôt/Filing Date: 2001/02/01

(41) Mise à la disp. pub./Open to Public Insp.: 2001/08/07

(45) Date de délivrance/Issue Date: 2004/01/20

(30) Priorité/Priority: 2000/02/07 (09/499,593) US

(51) Cl.Int.⁷/Int.Cl.⁷ C22B 9/05

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(54) Titre : COUVERTURE DE METAUX ET ALLIAGES NON FERREUX EN FUSION AVEC DES GAZ AYANT UN
POTENTIEL REDUIT DE RECHAUFFEMENT DE LA PLANETE

(54) Title: BLANKETING MOLTEN NON-FERROUS METALS AND ALLOYS WITH GASES HAVING REDUCED
GLOBAL WARMING POTENTIAL

(57) **Abrégé/Abstract:**

An improved method of processing a molten non-ferrous metal and alloys of said metal using a blanketing gas having a global warming potential is provided. The improvement involves reducing said global warming potential of said blanketing gas by blanketing said molten non-ferrous metal and alloys with a gaseous mixture including at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .



ABSTRACT OF THE DISCLOSURE

An improved method of processing a molten non-ferrous metal and alloys of said
5 metal using a blanketing gas having a global warming potential is provided. The
improvement involves reducing said global warming potential of said blanketing gas by
blanketing said molten non-ferrous metal and alloys with a gaseous mixture including at
least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 ,
 SOF_4 , NOF and SF_4 .

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TITLE OF THE INVENTION:

BLANKETING MOLTEN NONFERROUS METALS AND ALLOYS
WITH GASES HAVING REDUCED GLOBAL WARMING POTENTIAL

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BACKGROUND OF THE INVENTION

10 The present invention pertains to the blanketing of molten metals and alloys with gaseous mixtures, and in particular to a method of blanketing molten nonferrous metals and alloys using gases having reduced global warming potentials relative to the prior art.

Open top vessels such as induction furnaces used to remelt metals are operated so that the surface of metal during melting and the surface of the molten bath are
15 exposed to ambient atmosphere. Air in the atmosphere tends to oxidize the melt, thereby: causing loss of metal, loss of alloying additions and formation of slag that causes difficulty in metal processing; shortening refractory life; and promoting nonmetallic inclusions in final castings, pickup of unwanted gases in the metals, porosity, and poor metal recovery. One solution is to enclose the induction furnace in a vacuum or
20 atmosphere chamber for melting and/or processing of the metals. However, completely enclosed systems are very expensive and limit physical and visual access to the metals being melted.

As alternatives, liquid fluxing salts, synthetic slag, charcoal covers, and similar methods and compounds have been used in the high-volume, cost-sensitive field of metal reprocessing for minimizing metal oxidation, gas pickup, and loss of alloying additions. For example, the prior art teaches that rapid oxidation or fire can be avoided
5 by the use of fluxes that melt or react to form a protective layer on the surface of the molten metal. However, this protective layer of thick slag traps good metal, resulting in a loss of up to 2% of the melt. It also can break up and be incorporated into the melt, creating damaging inclusions. In addition, metal in the slag is leachable and creates a hazardous waste product.

10 These prior art techniques also necessitate additional handling and processing, and cause disposal problems. These techniques often reduce furnace life or ladle refractory life, increase frequency of shutdowns for relining or patching of refractories, and produce non-metallic inclusions that have to be separated from the metal bath prior to pouring of the metal into a cast shape.

15 In searching for solutions to the above-described problems, metallurgical industries turned to inert gas atmosphere blanketing. One type of gas blanketing system is based on gravitational dispersion of cryogenically-liquified inert gas over the surface of a hot metal to be blanketed. For example, such cryogenic blanketing systems are disclosed and claimed in U.S. Pat. No. 4,990,183.

20 U.S. Pat. No. 5,518,221 discloses a method and apparatus for inerting the interior space of a vessel containing hot liquids or solids in induction furnaces, crucible furnaces or ladles during charging, melting, alloying, treating, superheating, and pouring or tapping of metals and metal alloys. The method and apparatus employ a swirl of inert gas to blanket or cover the surface of the metal from the time of charging of the furnace
25 until the furnace is poured or tapped or inerting of the molten metal contained in a

furnace or ladle or other vessel. The gas swirl is confined by a unique apparatus mounted on top of the furnace or vessel containing the material to be protected. Any inert gas that is heavier than air can be used to practice the invention. In addition to argon and nitrogen, depending upon the material being blanketed, gases such as carbon
5 dioxide and hydrocarbons may be used.

While some cryogenic blanketing systems are quite effective, use of such systems is limited to metallurgical facilities and vessels that can be supplied by well-insulated cryogenic pipelines or equipped with cryogenic storage tanks in close proximity to the point of use of the liquid cryogen. This is not always practical, and some cryogenic
10 blanketing systems have been plagued by poor efficiency due to premature boil-off of the cryogenic liquid and oversimplified design of dispersing nozzles that wasted the boiled-off gas.

Moreover, cryogenic dispensers often fail to uniformly disperse the cryogenic liquid over the blanketed surface, leading to a transient accumulation or entrapment of
15 the liquid in pockets under the slag or dross, which may result in explosions in a subsequent rapid boil-off.

Other approaches have been taken for different molten metals and alloys in further attempts to solve the above-described problems. For example, U.S. Pat. No. 4,770,697 discloses a process for protecting an aluminum-lithium alloy during melting,
20 casting and fabrication of wrought shapes by enveloping the exposed surfaces with an atmosphere containing an effective amount of a halogen compound (e.g., dichlorodifluoromethane) having at least one fluorine atom and one other halogen atom; the other halogen atom is selected from the group consisting of chlorine, bromine, and iodine, and the ratio of fluorine to the other halogen atom in the halogen compound is
25 less than or equal to one. A passivating and self-healing viscous liquid layer is formed

which protects the alloy from lithium loss due to vaporization, oxidation of the alloy, and hydrogen pick-up by the alloy.

Another approach for some molten metals, such as magnesium, is to use inhibitors in the air. The early practice was to burn coke or sulfur to produce a gaseous agent, CO₂ or SO₂. An atmosphere of CO₂ was found to be superior to the commonly used commercial atmospheres of N₂, Ar, or He because of the absence of vaporization of the magnesium, the absence of excessive reaction products, and the reduced necessity for the enclosure above the molten metal to be extremely air tight.

However, the use of these inhibitors has several drawbacks. For example, both CO₂ and SO₂ pose environmental and health problems, such as breathing discomfort for personnel, residual sludge disposal, and a corrosive atmosphere detrimental to both plant and equipment. Furthermore, SO₂ is toxic and can cause explosions.

While BF₃ has been mentioned as being a very effective inhibitor, it is not suitable for commercial processes because it is extremely toxic and corrosive. Sulfur hexafluoride (SF₆) also has been mentioned as one of many fluorine-containing compounds that can be used in air as an oxidation inhibitor for molten metals, such as magnesium. A summary of industry practices for using SF₆ as a protective atmosphere, ideas for reducing consumption and emissions, and comments on safety issues related to reactivity and health are provided in *"Recommended Practices for the Conservation of Sulfur Hexafluoride in Magnesium Melting Operations,"* published by the International Magnesium Association (1998) as a "Technical Committee Report" (hereinafter "IMA Technical Committee Report").

The use of pure SF₆ was generally discarded because of its severe attack on ferrous equipment. In addition, the use of pure SF₆ for protecting molten metals such as magnesium has been reported to have caused explosions. Although sulfur hexafluoride

(SF₆) is considered physiologically inert, it is a simple asphyxiant which acts by displacing oxygen from the breathing atmosphere.

Later, it was found that at low concentrations of SF₆ in air (<1%), a protective thin film of MgO (and MgF₂) is formed on the magnesium melt surface. Advantageously, even at high temperatures in air, SF₆ showed negligible or no reactions.

However, the use of SF₆ and air has some drawbacks. The primary drawback is the release to the atmosphere of material having a high global warming potential (GWP).

It also was found that CO₂ could be used together with SF₆ and air. A gas atmosphere of air, SF₆, and CO₂ has several advantages. First, this atmosphere is non-toxic and non-corrosive. Second, it eliminates the need to use salt fluxes and the need to dispose of the resulting sludge. Third, using such an atmosphere results in lower metal loss, elimination of corrosion effects, and clean castings. Fourth, a casting process using such an atmosphere provides a clean operation and improved working conditions. Fifth, the addition of CO₂ to the blanketing atmosphere reduces the concentration of SF₆ at which an effective inerting film is formed on the metal. In sum, the addition of CO₂ to an air/SF₆ atmosphere provides much improved protection compared to the protection obtained with an air/SF₆ atmosphere.

However, using an atmosphere of SF₆ and CO₂ also has disadvantages. Both SF₆ and CO₂ are greenhouse gases, *i.e.*, each has a global warming potential over 100 years (GWP₁₀₀). Thus, there is a need to reduce the amounts of SF₆ and CO₂ released into the atmosphere. SF₆ has a 100-year global warming potential (GWP₁₀₀) of 23,900 relative to CO₂. International concern over global warming has focused attention on the long atmospheric life of SF₆ (about 3,200 years, compared to 50-200 years for CO₂) together with its high potency as a greenhouse gas (23,900 times the GWP₁₀₀ of CO₂ on a mole basis) and has resulted in a call for voluntary reductions in emissions. Because

of this, the use of SF_6 is being restricted and it is expected to be banned in the near future. In addition, SF_6 is a relatively expensive gas.

Some of the best alternatives to SF_6 for blanketing gases would be perfluorocarbons, such as CF_4 , C_2F_6 , and C_3F_8 , but these materials also have high
5 GWP's. Other alternatives would be chlorofluorocarbons (CFC's) or partially fluorinated hydrocarbons (HCFC's). However, the use of CFC's and HCFC's also is restricted; most of these materials are banned as ozone depleters under the Montreal Protocol.

Another alternative to SF_6 for a blanketing gas is SO_2 . When SO_2 is used as a blanketing gas, the effective concentration over a melt is typically in the range of about
10 30% to 70% SO_2 , with about 50% being normal. However, as discussed earlier, SO_2 poses environmental and health problems, is toxic, and can cause explosions. In addition, the use of SO_2 in such relatively high concentrations can cause corrosion problems on crucible walls.

It is desired to have a process for preventing oxidation of molten nonferrous
15 metals and alloys which overcomes the difficulties and disadvantages of the prior art to provide better and more advantageous results.

It is further desired to have an improved method of processing molten nonferrous metals and alloys using blanketing gases having lower global warming potentials than the gases used in prior art methods.

20 It also is desired to have an improved method of processing molten nonferrous metals and alloys using blanketing gases which overcomes the difficulties and disadvantages of the prior art to provide better and more advantageous results.

BRIEF SUMMARY OF THE INVENTION

A first embodiment of the present invention is an improvement in a method of processing a molten non-ferrous metal and alloys of said metal using a blanketing gas having a global warming potential. The improvement comprises reducing said global warming potential of said blanketing gas by blanketing said molten non-ferrous metal and alloys with a gaseous mixture including at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .

There are several variations of the first embodiment of the improvement in the method. In one variation, the at least one compound is provided at a first concentration of less than about 10% on a mole basis of said gaseous mixture. In addition, there may be several variants of that variation. In one variant, the first concentration is about 1% to about 6%. In another variant, the first concentration is about 3% to about 6%.

In yet another variant, the gaseous mixture further comprises at least one member selected from the group consisting of N_2 , Ar , CO_2 , SO_2 and air. In a variant of that variant, said at least one member is CO_2 provided at a second concentration of about 30% to about 60% on a mole basis. In a variant of that variant, said at least one compound is SO_2F_2 provided at said first concentration of less than about 3% on a mole basis. In a variant of that variant, said first concentration of SO_2F_2 is about 0.5% to about 2.9%.

Another aspect of the present invention is a method as in the first embodiment of the improvement in the method, wherein at least one operation is performed on said non-ferrous metal and alloys, said at least one operation being selected from the group consisting of melting, holding, alloying, ladling, stirring, pouring, casting and transferring of said non-ferrous metal and alloys.

The present invention also includes an improvement in a method of processing a melt comprising at least one molten non-ferrous metal using a blanketing gas having a global warming potential. The improvement comprises reducing said global warming potential of said blanketing gas by blanketing said melt with a gaseous mixture including
5 at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .

The present invention also includes a process for preventing oxidation of a molten non-ferrous metal and alloys of said metal. A first embodiment of the process includes blanketing said molten non-ferrous metal and alloys with an atmosphere
10 containing an effective amount of at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .

There are several variations of the first embodiment of the process. In one variation, said at least one compound is provided at a first concentration of less than about 10% on a mole basis of said atmosphere. In addition, there may be several
15 variants of that variation. In one variant, said first concentration is about 1% to about 6%. In another variant, said first concentration is about 3% to about 6%.

In yet another variant, said atmosphere further comprises at least one member selected from the group consisting of N_2 , Ar , CO_2 , SO_2 and air. In a variant of that variant, said at least one member is CO_2 provided at a second concentration of about
20 30% to about 60% on a mole basis. In a variant of that variant, said at least one compound is SO_2F_2 provided at said first concentration of less than about 3% on a mole basis. In a variant of that variant, said first concentration of SO_2F_2 is about 0.5% to about 2.9%.

Another aspect of the present invention is a process as in the first embodiment of
25 the process, wherein at least one operation is performed on said non-ferrous metal and

alloys, said at least one operation being selected from the group consisting of melting, holding, ladling, stirring, pouring, casting and transferring of said non-ferrous metals and alloys.

The present invention also includes a process for preventing oxidation of a melt comprising at least one molten non-ferrous metal, said process comprising blanketing said melt with an atmosphere containing an effective amount of at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2ClF , SOF_2 , SOF_4 , NOF and SF_4 .

BRIEF DESCRIPTION OF SEVERAL VIEWS OF THE DRAWINGS

Not Applicable.

DETAILED DESCRIPTION OF THE INVENTION

The invention provides a process for preventing oxidation of molten nonferrous metals or alloys by blanketing the molten metals or alloys with an atmosphere containing an effective amount of at least one compound having a reduced GWP, preferably selected from the group consisting of SO_2F_2 , SOF_2 , SOF_4 , NF_3 , SO_2ClF , NOF and SF_4 . The invention also provides an improved method of processing molten nonferrous metals and alloys using a blanketing gas having a reduced GWP (relative to the prior art) by blanketing the molten nonferrous metal or alloy with a gaseous mixture including at least one compound having a reduced GWP, preferably selected from the group consisting of SO_2F_2 , SOF_2 , SOF_4 , NF_3 , SO_2ClF , NOF and SF_4 .

The invention may be applied in many types of operations, including but not limited to the melting, holding, alloying, ladling, stirring, pouring, casting and transferring

of nonferrous metals and alloys thereof. Additional applications include such operations as protecting scrap when compacting, preparing powder for improved alloying, protecting reactive metals during electric arc spray coating, and improving the corrosion and wear resistance of articles of Magnesium or Magnesium based alloys. Persons
5 skilled in the art will recognize other operations where the invention also may be applied.

The gases used in the present invention have lower GWP's and/or are less toxic than the gases used in the prior art. Since the gases used in the present invention are more reactive than SF_6 , these gases can be used at concentrations supplying an equivalent or lower fluorine level. In other words, if SF_6 can be beneficially used at a
10 concentration of 1%, then SO_2F_2 will have a similar utility at concentrations of approximately $\leq 3\%$.

In a preferred embodiment, the selected compound is provided at a concentration of less than about 10% (on a mole basis) of said gaseous mixture. It is more preferable that the concentration be in the range of about 1% to about 6%, and it is
15 even more preferable that it be in the range of about 3% to about 6%.

In addition, in a preferred embodiment, the gaseous mixture further comprises at least one member selected from the group consisting of N_2 , Ar, CO_2 and air as a diluent. (SO_2 also could be used as the diluent, but is less desirable because of potential corrosion problems associated with SO_2 .) The most efficacious mixtures for blanketing
20 nonferrous metals contain significant concentrations of CO_2 , preferably in the range of about 30% to about 60%. Some nonferrous metals also could benefit from the addition of chlorine or chlorine-containing species (such as $\text{SO}_2\text{-ClF}$) to the blanketing gas mixture.

For example, in one embodiment, CO_2 is the diluent in the blanketing atmosphere at a concentration of about 30% to about 60% on a mole basis, and SO_2F_2 is provided at
25 a concentration of less than about 3% on a mole basis, and preferably at about 0.5% to

about 2.9%.

Table 1 compares the preferred gases used in the present invention to various gases used in the prior art with regard to GWP and other characteristics.

TABLE 1

Name	Formula	CAS Number ⁽¹⁾	OSHA PEL/ Ceiling/ Max Peak ⁽²⁾	ACGIH TWA/STEL ⁽³⁾	GWP ₁₀₀ ⁽⁴⁾	Atmospheric Lifetime years
Sulfur Hexafluoride	SF ₆	2551-62-4	1,000/x/x	1,000/1,250	24,900	3,200
Sulfur Dioxide	SO ₂	7446-09-5	2/5/x	10/15	-1 ⁽⁵⁾	NK ⁽⁶⁾
Carbon Dioxide	CO ₂	124-38-9	5,000/30,000	asphyxiant	1	50-200
Perfluoromethane	CF ₄	75-73-0	x	asphyxiant	6,500	50,000
Perfluoroethane	C ₂ F ₆	76-16-4	X	asphyxiant	9,200 to 12,500	10,000
Perfluoropropane	C ₃ F ₈	76-19-7	X	asphyxiant	6,950	7,000
Sulfuryl Fluoride	SO ₂ F ₂	2699-79-8	5/10/x	toxic	~1	NK
Thionyl Fluoride Sulfinyl Fluoride	SOF ₂	7783-84-8	X	toxic	~1	NK
Sulfur Oxifluoride	SOF ₄	13709-54-1	X	toxic	~1	NK
Sulfur Tetrafluoride	SF ₄	7783-60-0	x/0.1/x	0.1/0.3	~1	NK
Nitrogen Trifluoride	NF ₃	7783-54-2	10/x/x	10/15	8,000 to 9,720	180 to 740
Nitrosyl Fluoride	NOF	7789-25-5	X	toxic	~1	NK
Sulfuryl Chloride Fluoride	SO ₂ ClF	13637-84-8	X	toxic	~1	NK

5

(1) "CAS" is Chemical Abstract Services.

(2) "OSHA" is Occupational Safety and Health Administration; and "PEL" is Permissible Exposure Limit in parts per million (ppm), 29 CFR 1910.1000.

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- (3) "ACGIH" is American Conference of Governmental Industrial Hygienists; "TWA" is Time Weighted Average in parts per million (ppm); and "STEL" is Short Term Exposure Limit in parts per million (ppm).
- 5 (4) "GWP₁₀₀" is Global Warming Potential relative to that of CO₂ estimated over 100 years; for example, the GWP₁₀₀ of SF₆ is 24,900 times the GWP₁₀₀ of CO₂. Applicants are not aware of any published data regarding the GWP's for the compounds for which the GWP₁₀₀ is indicated to be ~1.
- 10 (5) Atmospheric reactions of SO₂ produce sulfate aerosols. These aerosols result in negative radiative forcing, *i.e.* tend to cool the earth's surface, but also are a major source of acid rain.
- 15 (6) "not known (NK)"; the atmospheric lifetime of these species are not known to the applicants, but are believed to be comparable to that of CO₂.

The comparison of GWP₁₀₀ shows that six of the seven preferred gases used in the present invention (SO₂F₂, NF₃, SO₂ClF, SF₄, SOF₂ NOF and SOF₄) have significantly lower GWP₁₀₀'s than the gases used in the prior art. (Of the seven gases, only NF₃ has a

20 GWP₁₀₀ greater than ~1; but the GWP₁₀₀ of NF₃ is still several fold lower than the GWP₁₀₀ of SF₆, and the atmospheric life of NF₃ also is shorter than that of SF₆). Furthermore, the prior art did not teach or even appreciate the possible use of these gases for blanketing. For example, the IMA Technical Committee Report shows that SO₂F₂ and SF₄ are by-products of the SF₆ protective chemistry for magnesium, but that report fails to realize

25 that both SO₂F₂ and SF₄ can be potent sources of fluorine for protection of the melt.

While the present invention has been described in detail with reference to certain specific embodiments, the invention is nevertheless not intended to be limited to the details described. Rather, it will be apparent to persons skilled in the art that various changes and modifications can be made in the details within the scope and range of the

30 claims and without departing from the spirit of the invention and the scope of the claims.

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CLAIMS

1. In a method of processing a molten nonferrous metal and alloys of said metal using a blanketing gas having a global warming potential, the improvement comprising reducing said global warming potential of said blanketing gas by blanketing
5 said molten nonferrous metal and alloys with a gaseous mixture including at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .
2. A method as in claim 1, wherein said at least one compound is provided
10 at a first concentration of less than about 10% on a mole basis of said gaseous mixture.
3. A method as in claim 2, wherein said first concentration is about 1% to about 6%.
- 15 4. A method as in claim 2, wherein said first concentration is about 3% to about 6%.
5. A method as in claim 2, wherein said gaseous mixture further comprises at least one member selected from the group consisting of N_2 , Ar, CO_2 , SO_2 and air.
20
6. A method as in claim 5, wherein said at least one member is CO_2 provided at a second concentration of about 30% to about 60% on a mole basis.
7. A method as in claim 6, wherein said at least one compound is SO_2F_2
25 provided at said first concentration of less than about 3% on a mole basis.

8. A method as in claim 7, wherein said first concentration of SO_2F_2 is about 0.5% to about 2.9%.

5 9. A method as in claim 1, wherein at least one operation is performed on said nonferrous metal and alloys, said at least one operation being selected from the group consisting of melting, holding, alloying, ladling, stirring, pouring, casting and transferring of said nonferrous metal and alloys.

10 10. A process for preventing oxidation of a molten nonferrous metal and alloys of said metal comprising blanketing said molten nonferrous metal and alloys with an atmosphere containing an effective amount of at least one compound selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .

15 11. A process as in claim 10, wherein said at least one compound is provided at a first concentration of less than about 10% on a mole basis of said atmosphere.

12. A process as in claim 11, wherein said first concentration is about 1% to about 6%.

20 13. A process as in claim 11, wherein said first concentration is about 3% to about 6%.

14. A process as in claim 11, wherein said atmosphere further comprises at
25 least one member selected from the group consisting of N_2 , Ar, CO_2 , SO_2 and air.

15. A process as in claim 14, wherein said at least one member is CO_2 provided at a second concentration of about 30% to about 60% on a mole basis.

5 16. A process as in claim 15, wherein said at least one compound is SO_2F_2 provided at said first concentration of less than about 3% on a mole basis.

17. A process as in claim 16, wherein said first concentration of SO_2F_2 is about 0.5% to about 2.9%.

10

18. A process as in claim 10, wherein at least one operation is performed on said nonferrous metal and alloys, said at least one operation being selected from the group consisting of melting, holding, alloying, ladling, stirring, pouring, casting and transferring of said nonferrous metal and alloys.

15

19. In a method of processing a melt comprising at least one molten nonferrous metal using a blanketing gas having a global warming potential, the improvement comprising reducing said global warming potential of said blanketing gas by blanketing said melt with a gaseous mixture including at least one compound
20 selected from the group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .

20. A process for preventing oxidation of a melt comprising at least one molten nonferrous metal, said process comprising blanketing said melt with an atmosphere containing an effective amount of at least one compound selected from the
25 group consisting of SO_2F_2 , NF_3 , SO_2CLF , SOF_2 , SOF_4 , NOF and SF_4 .