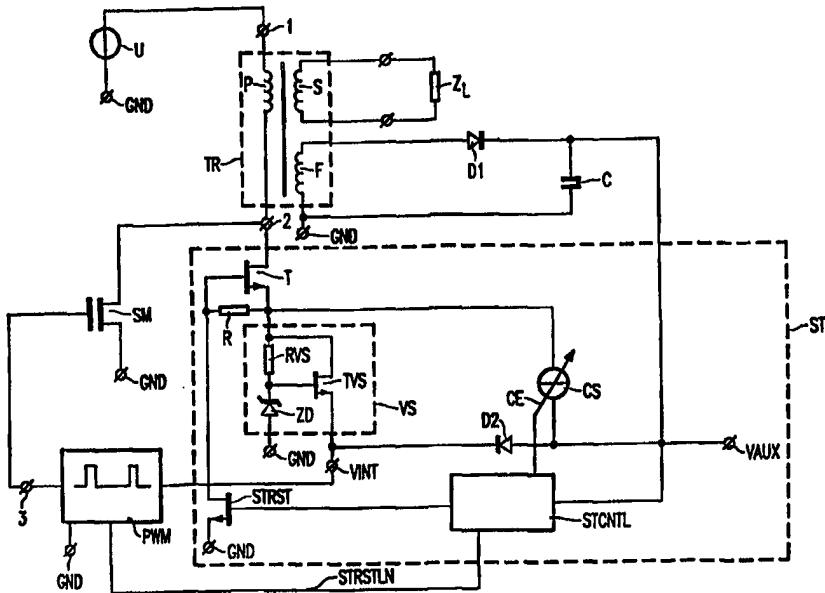




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(54) Title: SWITCHED-MODE POWER SUPPLY HAVING AN IMPROVED START-UP CIRCUIT



(57) Abstract

A switched-mode power supply comprises a transformer (TR) provided with a primary winding (P) having a first primary terminal (1), coupled to receive a voltage (U) with respect to a ground terminal (GND), and a second primary terminal (2); switching means (SM) coupled between the second primary terminal (2) and the ground terminal (GND); and a start-up circuit (ST) for starting up the switched-mode power supply. The start-up circuit (ST) comprises a field effect transistor (T) of the normally-on type having a drain coupled to the second primary terminal (2), a source, and a gate. The start-up circuit (ST) has been improved in that it comprises, interalia, a voltage stabilizer (VS), for supplying an internal supply voltage to an internal supply terminal (VINT), the voltage stabilizer (VS) being coupled to the source.

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Switched-mode power supply having an improved start-up circuit.

The invention relates to a switched-mode power supply comprising a transformer provided with a primary winding having a first primary terminal, coupled to receive a voltage with respect to a ground terminal, and a second primary terminal; switching means coupled between the second primary terminal and the ground terminal; and

5 a start-up circuit for starting up the switched-mode power supply, which start-up circuit comprises a field effect transistor of the normally-on type having a drain electrode coupled to the second primary terminal, a source electrode, and a gate electrode.

Such a switched-mode power supply is known from European Patent Specification EP 0 585 788 A1. Said Specification describes a switched-mode power supply

10 for use in an integrated circuit which does not require a separate IC terminal for supplying power to the start-up circuit. The start-up circuit is powered from the source of a junction field effect transistor, the junction field effect transistor being coupled in series between the switching means and the second primary terminal.

It is an object of the invention to provide a switched-mode power supply

15 having an improved start-up circuit.

To this end, according to the invention, the switched-mode power supply of the type defined in the opening paragraph is characterized in that the start-up circuit further comprises a voltage stabilizer, for supplying an internal supply voltage to an internal supply terminal, which voltage stabilizer is coupled to the source electrode. Thus, it is

20 achieved that the internal supply voltage is not unnecessarily high. An advantage of this is that it limits the dissipation of the necessary electronic circuitry coupled to the internal supply terminal.

An embodiment of a switched-mode power supply in accordance with the invention is characterized in that the gate electrode is coupled to the source electrode via a

25 resistor, and the start-up circuit further comprises a switching transistor having a main current path coupled between the gate electrode and the ground terminal. During a start-up phase of the switched-mode power supply the field effect transistor must be conductive. During the start-up phase the main current path of the switching transistor is not conductive. As a result of this, the resistor does not carry current so that there is no voltage difference

between the gate and the source of the field effect transistor. Since the field effect transistor is of the normally-on type, for example a junction field effect transistor, the field effect transistor is conductive. After the start-up phase the main current path of the switching transistor is conductive. The resistor consequently carries current, as a result of which there

5 is a voltage difference between the gate and the source of the field effect transistor. This has the advantage that the field effect transistor is substantially fully cut off, thereby further reducing the dissipation of the switched-mode power supply.

A further embodiment of a switched-mode power supply in accordance with the invention is characterized in that the transformer further comprises a feedback winding, which feedback winding is coupled to a series arrangement of a rectifier element and a buffer capacitor, which rectifier element and buffer capacitor are connected in an external supply terminal for supplying an external supply voltage, and the start-up circuit further comprises a current source coupled between the source electrode and the external supply terminal, to receive the external supply voltage. During the start-up phase the current

10 source charges the buffer capacitor, as a result of which the external supply voltage continually increases. The required electronic control circuitry for controlling the switching means, which control circuitry is coupled to the internal supply terminal, becomes operative once the external supply voltage has become sufficiently high. The electronic control circuitry ensures that the switching means are alternately turned on and turned off. This

15 results in an alternating current through the primary winding of the transformer, thereby causing a voltage to be induced in the feedback winding. The induced voltage is rectified by means of a rectifier element and thus forms the external supply voltage on the external supply terminal. This completes the start-up phase. After the start-up phase the start-up circuit is disabled in order to achieve a further reduction of the dissipation.

20 The invention will be described in more detail with reference to the accompanying drawing, in which the sole Figure shows an electrical circuit diagram of an embodiment of a switched-mode power supply in accordance with the invention.

The embodiment of a switched-mode power supply as shown in the Figure comprises a transformer TR having a primary winding P, a secondary winding A coupled to

25 a load Z_L , and a feedback winding F coupled to a series arrangement of a rectifier element D1 and a buffer capacitor C, said rectifier element D1 and buffer capacitor C being connected in an external supply terminal VAUX for supplying an external supply voltage with respect to a ground terminal GND. The first primary terminal 1 is coupled to receive a voltage U with respect to the ground terminal GND. The second primary terminal 2 is

coupled to the drain of the MOSFET SM forming the switching means. The MOSFET SM has its source coupled to the ground terminal GND. The switched-mode power supply further comprises a start-up circuit ST, which supplies an internal supply voltage to the internal supply terminal VINT. For this purpose, the start-up circuit ST comprises a field effect 5 transistor T of the normally-on type, for example a JFET, which has its drain connected to the second primary terminal 2. A resistor R is coupled between the gate and the source of the field effect transistor T.

To stabilize the internal supply voltage with respect to the ground terminal GND a voltage stabilizer VS is coupled to the source of the field effect transistor T and to 10 the internal supply terminal VINT. The voltage stabilizer VS may comprise, for example, a series arrangement of a resistor RVS and a zener diode ZD, which series arrangement is connected to the gate of a field effect transistor TVS in a common node, which field effect transistor has its drain connected to the source of the field effect transistor T and has its source connected to the internal supply terminal VINT. The resistor RVS has one electrode 15 connected to the source of the field effect transistor T. The zener diode ZD has one electrode connected to the ground terminal GND. The field effect transistor TVS is arranged as a source follower, as a result of which the internal voltage is equal to the voltage across the zener diode ZD minus the gate-source voltage of the field effect transistor TVS.

A pulse-width modulator PWM is supplied with voltage in that the pulse-width modulator PWM is coupled between the internal supply terminal VINT and the ground terminal GND. The pulse-width modulator PWM has an output terminal 3 coupled to the 20 gate of the MOSFET SM. Furthermore, to charge the buffer capacitor C during the start-up phase, a controllable current source CS is coupled between the source of the field effect transistor T and the external supply terminal VAUX. The value of the current supplied by 25 the controllable current source CS is dependent upon the external supply voltage on the external supply terminal VAUX. For this purpose, the current source CS has a control electrode CE coupled to a start-up control circuit STCRTL, which is coupled to the external supply terminal VAUX. In dependence upon the external supply voltage the start-up control circuit STCRTL determines the voltage on the control electrode CE of the current source 30 CS. The start-up circuit ST further comprises a switching transistor STRST having a main current path coupled between the gate of the field effect transistor T and the ground terminal (GND). The switching transistor STRST has its control electrode coupled to the start-up control circuit STCRTL to receive a SET/RESET signal.

The start-up circuit ST further comprises a unidirectional element formed

by a diode D2 coupled between the internal supply terminal VINT and the external supply terminal VAUX.

The circuit operates as follows. It is assumed that initially the respective voltages on the internal supply terminal and the external supply terminal VINT, VAUX are 5 equal to the voltage on the ground terminal GND and that the switching transistor STRST and the MOSFET SM do not conduct. The field effect transistor T conducts, as a result of which the internal supply voltage on the internal supply terminal VINT rises rapidly to a given value. Since only a small constant current flows through the primary winding P of the transformer T the voltage on the second primary terminal 2 is substantially equal to the 10 voltage U. Although the value of the internal supply voltage is adequate to power the pulse-width modulator PWM the pulse-width modulator PWM does not yet become operative. As a matter of fact, the pulse-width modulator PWM does not become operative until the value of the external supply voltage on the external supply terminal VAUX has become sufficiently large, which is achieved under control of a control signal on a communication line 15 STRSTLN coupled between the start-up control circuit STCRTL and the pulse-width modulator PWM. The reason for this is as follows. When the MOSFET SM is conductive the voltage on the second primary terminal 2 is substantially equal to the ground terminal GND. As a consequence of this, the switching transistor T is turned off immediately, so that the internal supply voltage again becomes equal to the voltage on the ground terminal GND. 20 As a result, the pulse-width modulator PWM and, consequently, the MOSFET SM would be turned off immediately. In order to preclude this, the buffer capacitor C is allowed to be charged to a sufficient extent by means of the current source CS. The time required for charging the buffer capacitor C is independent of the voltage U. Since the start-up time of the switched-mode power supply is mainly determined by the time required for charging the 25 buffer capacitor C the start-up time of the switched-mode power supply is also substantially independent of the voltage U. It is not until the buffer capacitor C has been charged to a sufficient extent that the pulse-width modulator PWM becomes operative. The internal voltage will then remain sufficiently large because the internal supply terminal receives power from the charged buffer capacitor C, which is coupled to the internal supply terminal 30 VINT by means of the diode D2.

The pulse-width modulator PWM will now remain operative, so that the MOSFET SM is alternately turned on and turned off, thereby producing an alternating current through the primary winding P of the transformer TR. As a result of this, a voltage is induced both in the secondary winding S and in the feedback winding F. The buffer

capacitor C is further charged by means of the feedback winding F.

The start-up phase has now been completed. The start-up circuit STCRTL supplies a RESET signal to the control electrode of the switching transistor STRST, causing this transistor to be turned on. As a result, the field effect transistor T remains cut off 5 permanently, so that the current source CS is also turned off permanently. This precludes unnecessary dissipation of the switched-mode power supply. If a minimal dissipation of the switched-mode power supply is considered to be less important, the resistor and the switching transistor STRST may be dispensed with. The gate of the field effect transistor T should then be connected to the source of the field effect transistor T or to the ground 10 terminal GND. The field effect transistor T will then not be turned off permanently after the start-up phase but it will merely be turned off automatically when the MOSFET SM is conductive, because the voltage on the second primary terminal 2, with respect to the voltage on the ground terminal GND, is then substantially zero.

The internal supply voltage is derived from the external supply voltage by means of the 15 coupling via the diode D2.

If the current source CS is a controllable current source the current supplied by the current source CS can be low, for example under control of the start-up control circuit STCRTL, as long as the external voltage does not exceed a threshold value, for example 0.5 V. If the external voltage exceeds the threshold value the current supplied 20 by the current source CS can then be substantially larger in order to ensure rapid starting of the switched-mode power supply. An advantage of this is that in the case of overloading of the switched-mode power supply, for example owing to a short-circuit of the external supply terminal VAUX to the ground terminal GND, so that the external supply voltage VAUX cannot exceed the threshold value, the current supplied by the current source CS remains 25 low, thereby avoiding unnecessary dissipation. Another advantage is that by means of a comparatively cheap switch, for example by means of a transistor, the switched-mode power supply can simply be set to a standby mode by short-circuiting the external supply terminal VAUX deliberately to the ground terminal GND by means of the switch, as a result of which the current supplied by the current source CS is small. Thus, it is achieved that the 30 dissipation of the switched-mode power supply in the standby mode is low.

Except for the field effect transistor T, other types than the types shown in the Figure can be used for the transistors. Furthermore, other electrical components than transistors, such as for example thyristors, can be used for the switching means SM. The current source CS need not necessarily be controllable and can even be realized by means of

a resistor. The switched-mode power supply can be implemented in an integrated circuit but also by means of discrete components.

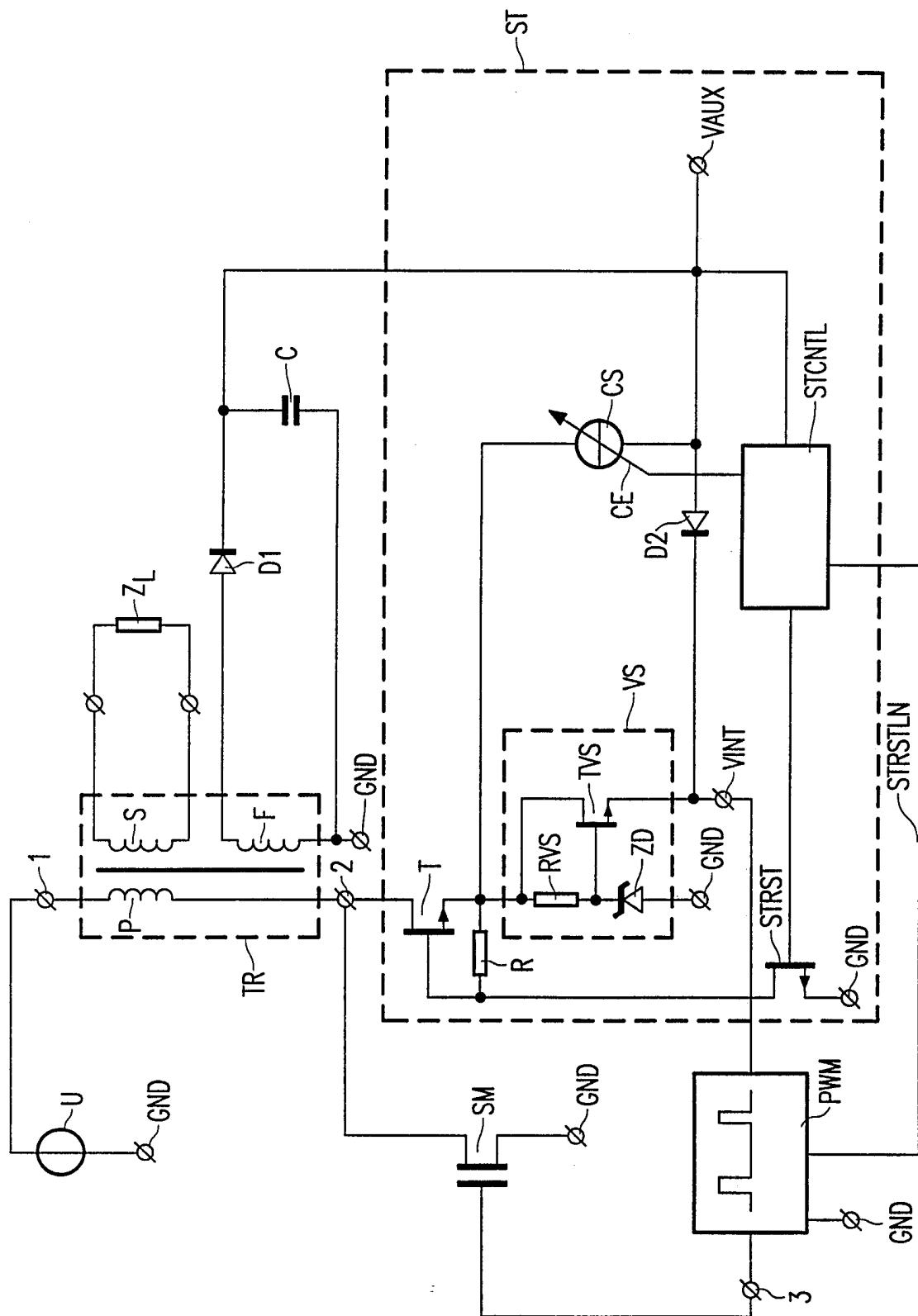
Claims

1. A switched-mode power supply comprising a transformer (TR) provided with a primary winding (P) having a first primary terminal (1), coupled to receive a voltage (U) with respect to a ground terminal (GND), and a second primary terminal (2); switching means (SM) coupled between the second primary terminal (2) and the ground terminal (GND); and a start-up circuit (ST) for starting up the switched-mode power supply, which start-up circuit comprises a field effect transistor (T) of the normally-on type having a drain electrode coupled to the second primary terminal (2), a source electrode, and a gate electrode, characterized in that the start-up circuit (ST) further comprises a voltage stabilizer (VS), for supplying an internal supply voltage to an internal supply terminal (VINT), which voltage stabilizer (VS) is coupled to the source electrode.
2. A switched-mode power supply as claimed in Claim 1, characterized in that the gate electrode is coupled to the source electrode.
3. A switched-mode power supply as claimed in Claim 1, characterized in that the gate electrode is coupled to the ground terminal (GND).
4. A switched-mode power supply as claimed in Claim 1, characterized in that the gate electrode is coupled to the source electrode via a resistor (R), and the start-up circuit (ST) further comprises a switching transistor (STRST) having a main current path coupled between the gate electrode and the ground terminal (GND).
5. A switched-mode power supply as claimed in Claim 1, 2, 3, or 4, characterized in that the transformer (TR) further comprises a feedback winding (F), which feedback winding (F) is coupled to a series arrangement of a rectifier element (D1) and a buffer capacitor (C), which rectifier element (D1) and buffer capacitor (C) are connected in an external supply terminal (VAUX) for supplying an external supply voltage.
6. A switched-mode power supply as claimed in Claim 5, characterized in that the start-up circuit (ST) further comprises a current source (CS) coupled between the source electrode and the external supply terminal (VAUX).
7. A switched-mode power supply as claimed in Claim 6, characterized in that the current source (CS) comprises a control electrode (CE), to receive a control signal for controlling the current source (CS), which control signal is dependent upon the external

supply voltage.

8. A switched-mode power supply as claimed in Claim 5, 6, or 7, characterized in that the start-up circuit (ST) comprises a unidirectional element (D2) coupled between the internal supply terminal (VINT) and the external supply terminal (VAUX).

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INTERNATIONAL SEARCH REPORT

International application No.

PCT/IB 98/00369

A. CLASSIFICATION OF SUBJECT MATTER

IPC6: H02M 1/08, H02M 3/35

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: H02M

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

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C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5041956 A (A.A.M. MARINUS), 20 August 1991 (20.08.91), column 3, line 49 - column 7, line 36, figures 1,2, abstract --	1-8
A	US 4737669 A (W.M. AUSTIN), 12 April 1988 (12.04.88), column 5, line 12 - line 47, figure 2, abstract --	1-8
A	US 4754387 A (J.G. KONOPKA), 28 June 1988 (28.06.88), column 2, line 19 - column 3, line 25, figure 1, abstract --	1-8

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C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5452195 A (S. LEHR ET AL.), 19 Sept 1995 (19.09.95), column 3, line 8 - column 6, line 17, figures 1,4,5, abstract --	1-8
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Information on patent family members

27/07/98

International application No.

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