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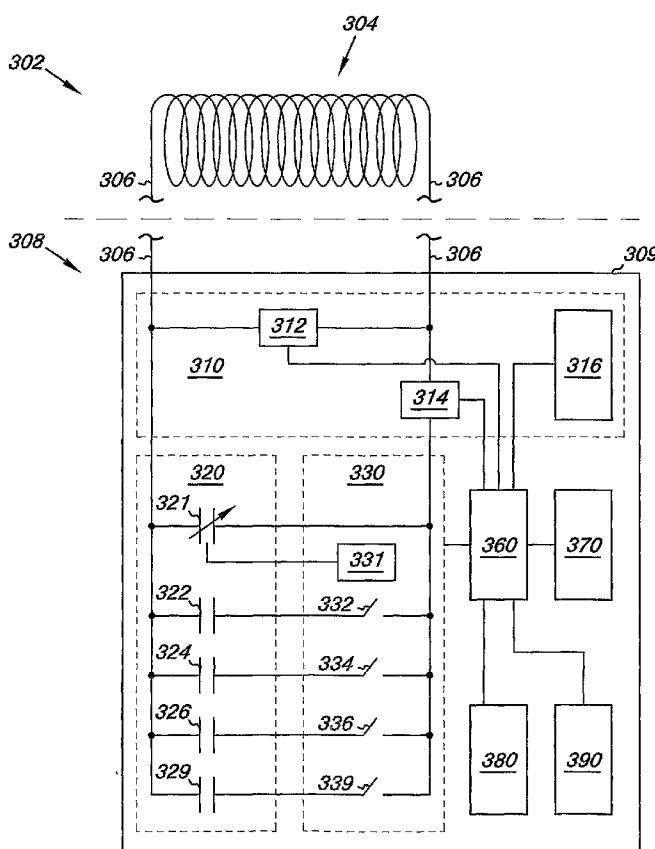
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**(54) Title: RESONATOR WITH ADJUSTABLE CAPACITANCE FOR MEDICAL DEVICE**

**(57) Abstract:** Systems and methods for a resonator with an adjustable capacitance for a medical device. In one embodiment, a resonator system includes a resonator device (202) with an LC resonator circuit that has an adjustable capacitance (321), an inductor coil (304) in series with the adjustable capacitance, and an adjustable capacitance control that can control the adjustable capacitance to obtain different particular capacitance values. The resonator device is used with a medical device so that at least a portion of the inductor coil surrounds a space that is surrounded by at least a portion of the medical device.





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## Resonator with Adjustable Capacitance for Medical Device

### Field of the Disclosure

The present disclosure relates generally to medical devices, medical device systems, and medical device methods; and more particularly to medical devices, medical device systems, and medical device methods for use during magnetic resonance imaging.

### Background

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Magnetic resonance imaging (MRI) can create images of internal aspects of structures by using magnetic fields of various field strengths. When performing MRI, sometimes it is desirable to enhance the visualization of a particular aspect of a structure or an object within a structure, for better signal-to-noise ratios in MRI images. For instance, sometimes it is desirable to enhance the visualization of a medical device when performing an MRI.

One way to enhance visualization when performing MRI is to use a resonator device. An LC circuit can form a basis for a resonator device. An LC circuit with a fixed inductance and a fixed capacitance can resonate at a particular frequency. However, an MRI can use magnetic fields with a range of field strengths to cause material in a structure or an object to resonate over a range of frequencies. Thus, a resonator device with a fixed inductance and a fixed capacitance may not resonate over a range of frequencies.

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### Brief Description of the Drawings

The illustrations provided in the Figures may not be to scale.

Figure 1 illustrates an exemplary embodiment of an MRI machine and a static magnetic field.

Figure 2A illustrates an exemplary embodiment of a hydrogen proton in a static magnetic field of an MRI machine.

Figure 2B illustrates an exemplary embodiment of a radio frequency pulse in relation to a static magnetic field of an MRI machine.

Figure 3A illustrates an embodiment of a resonator device with an adjustable capacitance according to the present disclosure.

Figure 3B illustrates another embodiment of a resonator device with an adjustable capacitance according to the present disclosure.

5 Figure 4A illustrates an embodiment of a resonator system with a medical device according to the present disclosure.

Figure 4B illustrates another embodiment of a resonator system with a medical device according to the present disclosure.

10 Figure 5 illustrates still another embodiment of a resonator system with a medical device according to the present disclosure.

### **Detailed Description**

The figures herein follow a numbering convention in which the first digit or digits correspond to the drawing figure number and the remaining digits

15 identify an element or component in the drawing. Similar elements or components between different figures may be identified by the use of similar digits. For example, 110 may reference element "10" in Figure 1, and a similar element may be referenced as 210 in Figure 2. As will be appreciated, elements shown in the various embodiments herein can be added, exchanged, and/or

20 eliminated so as to provide a number of additional embodiments. In addition, discussion of features and/or attributes for an element with respect to one figure can also apply to the element shown in one or more additional figures.

Embodiments of the present disclosure are directed to resonator devices, resonator systems, and methods of using the resonator devices. Generally, a 25 resonator device can be used in conjunction with a medical device, including a deliverable device, deliverable in a lumen of a body. One embodiment of the present disclosure includes a resonator with an adjustable capacitance for a medical device, which can enhance visualization when performing MRI.

Figure 1 illustrates an exemplary embodiment of an MRI machine and a 30 static magnetic field. Figure 1 is intended to illustrate basic concepts of an MRI machine and is not intended to show details of an MRI machine or to illustrate a particular MRI machine. Figure 1 includes an MRI scanner 110 with a coil 130 and terminals 120. Figure 1 also includes static magnetic field lines 140 and a magnetic field vector 150.

The MRI scanner 110 is a cylindrical tube. The coil 130 is electrically conductive. The coil 130 begins at one terminal 120, winds around the MRI scanner 110 in helical form, and ends at another terminal 120. Each terminal 120 is connected to the coil 130 so that electrical current can flow from the terminal 5 120 through the coil 130.

When electrical current flows through the coil 130 it can create a static magnetic field, which is represented by the static magnetic field lines 140. Each of the static magnetic field lines 140 has a direction, which is represented by arrows. The direction of the magnetic field lines 140 can depend upon the 10 direction in which electrical current flows through the coil 130.

The static magnetic field also has a magnetic field vector 150. The magnetic field vector 150 coincides with a central axis of the MRI scanner 110. The magnetic field vector 150 also has a direction which can depend upon the direction in which electrical current flows through the coil 130. In MRI, the static 15 magnetic field can cause hydrogen protons within the field to align with the magnetic field vector 150. The magnetic field vector 150 can also serve as a reference direction when performing MRI, as described in Figures 2A and 2B.

Figure 2A illustrates an exemplary embodiment of a hydrogen proton in a static magnetic field of an MRI machine. Figure 2A includes a magnetic field 20 vector 250 and an illustration of a precessing hydrogen proton 230. The magnetic field vector 250 corresponds with a static magnetic field of an MRI machine, such as the static magnetic field of Figure 1. The illustration of the precessing hydrogen proton 230 includes a hydrogen proton 238, a spin direction 232, a reference arrow 234, and a reference circle 236.

25 The presence of the static magnetic field causes the hydrogen proton 238 to precess in the spin direction 232. The hydrogen proton 238 precesses in the spin direction 232 around an axis that is parallel to the magnetic field vector 250. The reference arrow 234 indicates that the precessing of the hydrogen proton 238 creates the reference circle 236. The magnetic field vector 250 is perpendicular to 30 the reference circle 236.

Figure 2B illustrates an exemplary embodiment of a radio frequency pulse in relation to a static magnetic field of an MRI machine. Figure 2B includes a magnetic field vector 250, a transmitter coil 260, a radio frequency (RF) pulse 270, an RF pulse magnetic field vector 280, and an RF pulse electrical field vector

290. The magnetic field vector 250 corresponds with a static magnetic field of an MRI machine, such as the static magnetic field of Figure 1. The transmitter coil 260 can be part of the MRI machine and can create the RF pulse 270.

5 The RF pulse 270 can be an oscillating electro-magnetic field, propagating in a direction perpendicular to the magnetic field vector 250. The RF pulse 270 includes the RF pulse magnetic field vector 280 and the RF pulse electrical field vector 290. RF pulse magnetic field vector 280 and the RF pulse electrical field vector 290 can be perpendicular to each other and perpendicular to the direction in which the RF pulse 270 propagates.

10 An MRI machine can create an RF pulse at a certain frequency called the Larmor frequency. The Larmor frequency is a frequency at which certain protons resonate. The Larmor frequency differs for protons of different elements and for static magnetic fields of different strengths. Many MRI machines create RF pulses for hydrogen protons, and this is assumed throughout this document unless 15 otherwise indicated. For hydrogen protons, the Larmor frequency is 42.9 MHz for each Tesla of static magnetic field strength.

20 Some MRI machines can create static magnetic fields with flux ranging from 0.3 Teslas to 7.0 Teslas. Many MRI machines create static magnetic fields with flux ranging from 1.5 Teslas to 3.0 Teslas. Thus, MRI machines that create static magnetic fields with flux between 0.3 and 7.0 Teslas operate at Larmor frequencies between 13 and 300 MHz. Similarly, MRI machines that create static magnetic fields with flux between 1.5 and 3.0 Teslas operate at Larmor frequencies between 64 and 129 MHz.

25 In MRI, a resonator device can enhance visualization of images by resonating at the Larmor frequency. In some instances, a resonator device can enhance visualization of images by resonating at a frequency close to a Larmor frequency, depending on the frequency response of the device. A resonator device based on an LC circuit with a fixed inductance and a fixed capacitance may not resonate over a range of frequencies. Additionally, an inductance of an LC circuit 30 may change under certain conditions or may change in certain applications, such as an inductor coil with a radius that changes when used with an expandable stent. As examples, a resonator device can be used with a balloon expandable stent or a self-expandable stent. However, a resonator device with an adjustable capacitance can resonate over a range of frequencies, as described in Figures 3A and 3B.

Figure 3A illustrates an embodiment of a resonator device with an adjustable capacitance according to the present disclosure. In Figure 3A the resonator device 301 includes an inductor coil 304, connecting conductors 306, and a circuit package 308. The connecting conductors 306 are shown as broken lines to indicate that the inductor coil 304 and the circuit package 308 as shown, 5 may have different scales. The sizes of elements in the Figure 3A are merely illustrative and are not intended to indicate any particular size or relationship in size.

The inductor coil 304 is external to the circuit package 308, in the 10 resonator device 301. The circuit package 308 encapsulates electrical components, including sensors 310, an adjustable capacitance 320, and an adjustable capacitance control 330. The inductor coil 304, the connecting conductors 306, at least a portion of the adjustable capacitance 320, and at least a portion of the adjustable capacitance control 330 together form an LC resonator 15 circuit. In the resonator device 301, the circuit package also encapsulates a processor 360, a memory, 370, a power source 380, and a selector 390, which relate to the LC resonator circuit, as described herein.

In the embodiment of Figure 3A, the adjustable capacitance 320 can have different particular capacitance values. The adjustable capacitance 320, as a 20 whole, is electrically in series with the inductor coil 304. In other words, the inductor coil 304 and the adjustable capacitance 320 respectively form L and C components of the LC resonator circuit, as will be understood by one of ordinary skill in the art. The adjustable capacitance 320 is electrically connected to the adjustable capacitance control 330.

25 In the resonator device 301 of Figure 3A, the processor 360 is connected to the LC resonator circuit through the adjustable capacitance control 330. The processor 360 executes logic and/or program instructions that allow it to perform functions, including a function of adjusting the adjustable capacitance 320 by directing the adjustable capacitance control 330. The processor 360 directs the 30 adjustable capacitance control 330 to control the adjustable capacitance 320 to obtain different particular capacitance values. Since the processor 360 directs the adjustable capacitance control 330, in various embodiments, the processor 360 can also be considered as part of the adjustable capacitance control 330. The processor 360 is also connected to the sensors 310. For simplicity, Figure 3A

does not show details of the sensors 310, the adjustable capacitance 320, or the adjustable capacitance control 330. These details are described in Figure 3B.

In the resonator device 301, the processor 360 is also connected to the memory 370, the power source 380, and the selector 390. The memory 370 can 5 store data which can be used by the processor 360. The processor 360 can communicate with the memory 370 through its connection to the memory 370. The power source 380 can provide the processor 360 with electrical power so the processor 360 can perform its functions, as described in Figure 2. The selector 390 can be set to different settings, which represent various user inputs, as 10 described herein.

The power source 380 can have different forms in various embodiments. In one embodiment, the power source 380 can generate electrical power from an electro-magnetic field. As examples, the power source 380 can be the inductor coil 304, another conducting coil, or a secondary resonator circuit. In this 15 embodiment, the powering electro-magnetic field can be an RF pulse from an MRI machine or some other field. In various embodiments, an RF pulse can provide power over longer distances. In one embodiment, the power source 380 can be a battery or a rechargeable capacitor. In various embodiments, the power source 380 can also generate electrical power from an alternating magnetic field, 20 such as a field within a transformer, for powering by induction over shorter distances.

In one embodiment, the processor 360 of Figure 3A automatically adjusts the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance, in response to an RF pulse from an MRI machine. The processor 360 25 performs this automatic adjustment by determining a resonant capacitance and then adjusting the adjustable capacitance 320 to the resonant capacitance. As described herein, the resonant capacitance is a capacitance at which the LC resonator circuit will resonate in response to the RF pulse, as will be understood by one of ordinary skill in the art. The processor 360 directs this adjustment in 30 various ways by executing logic and/or program instructions in response to known, sensed, and/or calculated values, as described in Figure 3B.

A range of adjustable capacitance for an LC resonator circuit of a resonating device can be estimated, based upon a potential range of MRI Larmor frequencies of and an estimated range of inductor coil inductances. A potential

range of MRI Larmor frequencies can be determined as described above. An estimated range of inductor coil inductances can be estimated by mathematically modeling an ideal inductance coil.

An inductance for an ideal inductance coil can be mathematically modeled 5 by using an ideal inductor formula. In that formula,  $L = (\mu * N^2 * \pi * r^2) / l$  where L is inductance in Henries,  $\mu$  is a factor equal to  $1.26 \times 10^{-7}$  Henries per meter, N is a number of windings in an inductor coil, r is a radius of the inductor coil in meters, and l is a length of the inductor coil in meters. For example, the ideal inductor formula can be used to mathematically model an inductance for an 10 ideal inductor coil sized to match various dimensions of a stent. In this example a stent can range in radius from 0.001 meters to .005 meters and in length from 0.008 meters to 0.07 meters. Also in this example, an inductor can have 1 winding for every 0.001 meter of inductor length or 1 winding for every 0.002 meter of inductor length. Using these example numbers for an ideal inductance 15 coil yields an estimated range of inductor coil inductances from 0.79 nanoHenries to 0.69 microHenries.

A range of adjustable capacitance for an LC resonator circuit of a resonating device can be estimated, based upon a potential range of MRI Larmor frequencies, a potential range of inductor coil inductances and an LC circuit 20 resonance formula. In the LC circuit resonance formula,  $f = 1 / (2 * \pi * \sqrt(L * C))$  where f is a resonant frequency of the LC resonator circuit, L is an inductance of the LC resonator circuit at the resonant frequency, and C is the capacitance of the LC resonator circuit at the resonant frequency. Since a potential range of MRI Larmor frequencies can be determined and a range of inductor coil inductances 25 can be estimated, as described herein, the LC circuit resonance formula can be solved for a range of adjustable capacitance. As an example, using a potential range of MRI Larmor frequencies from 13 to 300 MHz and a potential range of inductor coil inductances from 0.79 nanoHenries to 0.69 microHenries in the LC circuit resonance formula yields an estimated range of adjustable capacitance from 30 0.41 picoFarads to 0.19 microFarads, which can be created as described in Figure 3B.

Figure 3B illustrates another embodiment of a resonator device with an adjustable capacitance according to the present disclosure. The embodiment of Figure 3B is a specific embodiment of Figure 3A and includes elements

corresponding with elements of the embodiment of Figure 3A. In Figure 3B the resonator device 302 includes the inductor coil 304, the connecting conductors 306, and the circuit package 308. As with Figure 3A, the sizes of elements in Figure 3B are merely illustrative and are not intended to indicate any particular 5 size or relationship of size.

The inductor coil 304 is external to the circuit package 308, in the resonator device 302. The circuit package 308 encapsulates electrical components, including the sensors 310, the adjustable capacitance 320, and the adjustable capacitance control 330. The inductor coil 304, the connecting 10 conductors 306, at least a portion of the adjustable capacitance 320, and at least a portion of the adjustable capacitance control 330 together form an LC resonator circuit. The circuit package also encapsulates a processor 360, a memory, 370, a power source 380, and a selector 390, which relate to the LC resonator circuit, as described herein.

15 In the resonator device 302 of Figure 3B, the adjustable capacitance 320 includes a varactor 321, and capacitors 322, 324, 326, and 329. The varactor 321, and the capacitors 322, 324, 326, and 329 are electrically connected parallel to each other. The adjustable capacitance 320 can have different particular 20 capacitance values based on the capacitance value of the varactor 321, the capacitance values of the capacitors 322, 324, 326, and 329, and the adjustable capacitance control 330, as described herein.

The adjustable capacitance 320, as a whole, is electrically in series with the inductor coil 304. One side of the inductor coil 304 is electrically connected to one side of the adjustable capacitance 320 through one of the connecting 25 conductors 306. Another side of the inductor coil 304 is electrically connected to another side of the adjustable capacitance 320 through another of the connecting conductors 306 and through the adjustable capacitance control 330. Thus, while the varactor 321, and the capacitors 322, 324, 326, and 329 are electrically parallel to each other, the adjustable capacitance 320, with its particular capacitance value, 30 is electrically in series with the inductor coil 304. In other words, the inductor coil 304 and the adjustable capacitance 320 respectively form L and C components of the LC resonator circuit, as will be understood by one of ordinary skill in the art. The adjustable capacitance 320 is electrically connected to the adjustable capacitance control 330.

In the resonator device 302, the adjustable capacitance control 330 includes a varactor controller 331, and electrical switches 332, 334, 336, and 339. The varactor controller 331 controls an adjustable capacitance of the varactor 321. Each of the electrical switches 332, 334, 336, and 339 has an open state and a closed state. In the closed state, an electrical switch forms an electrical connection that allows electrical current to flow through that switch. In the open state, an electrical switch forms an electrical break that prevents electrical current from flowing through that switch. Each of the electrical switches of Figure 3B is shown in the open state, so the locations of the switches can be clearly identified.

10 In the embodiment of Figure 3B, there is an electrical switch for each of the capacitors 322, 324, 326, and 329. The electrical switches 332, 334, 336, and 339 correspond with the capacitors 322, 324, 326, and 329. Thus, each electrical switch can connect its corresponding capacitor to the LC resonator circuit or disconnect its corresponding capacitor from the LC resonator circuit, depending 15 on the state of the switch. For example, if the electrical switch 332 is in its closed state, it connects the capacitor 322 to the LC resonator circuit. Alternatively, if the electrical switch 332 is in its open state, then the capacitor 322 is disconnected from the LC resonator circuit. Since the capacitors 322, 324, 326, and 329 are electrically parallel to each other, each electrical switch can connect or disconnect 20 its corresponding capacitor individually. As a result, the adjustable capacitance 320, as a whole, can be adjusted to different particular capacitance values depending on which capacitors are connected to the LC resonator circuit. In the embodiment shown, the LC resonator circuit is electrically connected to some of the sensors 310.

25 In the resonator device 302 of Figure 3B, the sensors 310 include a voltage sensor 312, a current sensor 314, and a flux sensor 316. In this embodiment, some of the sensors 310 are electrically connected to the LC resonator circuit and each of the sensors 310 are connected to the processor 360. The voltage sensor 312 is electrically connected across the adjustable capacitance 312 and can sense an 30 electrical voltage differential across the adjustable capacitance 312. The voltage sensor 312 is also connected to the processor 360 and can transmit a signal that represents a sensed voltage through that connection to the processor 360. The current sensor 314 is electrically connected in line with a path of the LC resonator circuit and can sense an electrical current flow through the path of the LC

resonator circuit. The current sensor 314 is also connected to the processor 360 and can transmit a signal that represents a sensed current through that connection to the processor 360. The flux sensor 316 can sense a flux of a magnetic field, such as a flux of a static magnetic field from an MRI machine. The flux sensor 5 316 is also connected to the processor 360 and can transmit a signal that represents a sensed flux through that connection to the processor 360.

In the embodiment of Figure 3B, the processor 360 is connected to the LC resonator circuit through the adjustable capacitance control 330. The processor 360 can execute logic and/or program instructions that allow it to perform 10 functions, including a function of adjusting the adjustable capacitance 320 by directing the adjustable capacitance control 330. The processor 360 directs the adjustable capacitance control 330 to control the adjustable capacitance 320 to obtain different particular capacitance values. Specifically, the processor 360 directs the adjustable capacitance control 330 to open or close particular electrical 15 switches which connect or disconnect particular capacitors, to obtain different particular capacitance values in the LC resonator circuit. Additionally, the processor 360 directs the varactor controller 331 to control the adjustable capacitance of the varactor 321, to obtain different particular capacitance values in the LC resonator circuit. Since the processor 360 directs the adjustable 20 capacitance control 330, in various embodiments, the processor 360 can also be considered as part of the adjustable capacitance control 330. For simplicity, Figure 3B shows a connection between the processor 360 and the adjustable capacitance control 330, as a whole, but does not show individual control connections for elements of the adjustable capacitance control 330.

25 The processor 360 is also connected to the memory 370, in the resonator device 302. The memory 370 can store data such as logic and/or program instructions and/or values. The processor 360 can transmit such data to the memory 370 and receive such data from the memory 370 through its connection to the memory 370. The processor 360 can use data stored in the memory 370 to 30 perform functions. For example, the memory 370 can store program instructions that the processor 360 can use to direct the adjustable capacitance control 330 to adjust the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance in a magnetic field, as described herein. The memory 370 can store values that represent signals that the processor 360 receives from one or more of

the sensors 310. For example, the memory 370 can store values that represent an electrical voltage differential across the adjustable capacitance 312, as sensed by the voltage sensor 312. The memory 370 can also store known values, such as a known inductance of the LC resonator circuit, including an inductance of the  
5 inductor coil 304.

The processor 360 is also connected to the power source 380 and the selector 390. The power source 380 provides the processor 360 with electrical power so the processor 360 can perform its functions, as described in Figure 2. The selector 390 can be set to different settings, which represent various user  
10 inputs, as described herein. The processor 360 can detect the different settings of the selector 390 through its connection to the selector 390.

In one embodiment, the processor 360 of Figure 3B automatically adjusts the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance, in response to a flux from a magnetic field. The processor 360  
15 performs this automatic adjustment by determining a resonant capacitance and then adjusting the adjustable capacitance 320 to the resonant capacitance. As described herein, the resonant capacitance is a capacitance at which the LC resonator circuit will resonate in response to an RF pulse of an MRI machine, as will be understood by one of ordinary skill in the art. The processor 360 can  
20 adjust the adjustable capacitance 320 to the resonant capacitance by directing the adjustable capacitance control 330 to change a number of the parallel capacitors 322, 324, 326, and 329 that are connected to the LC resonator circuit and/or to adjust a capacitance of the varactor 321. The processor 360 directs this  
25 adjustment in various ways by executing logic and/or program instructions in response to known, sensed, and/or calculated values.

The processor 360 can direct the adjustment of the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance by executing logic and/or program instructions in response to known, sensed, and/or calculated values for a flux of a magnetic field and an inductance of the LC resonator circuit. Known  
30 values can be provided to the processor 360 from the memory 370, from the selector 390, or from directing the adjustable capacitance 310 to adjust to a known capacitance. The flux sensor 316 can sense a flux of a magnetic field, such as a flux of a static magnetic field from an MRI machine. In various embodiments of

the present disclosure, flux values, inductance values, and capacitance values can be calculated as described herein.

In one embodiment of Figure 3B, the processor 360 can execute logic and/or program instructions to direct the adjustment of the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance in response to a known or sensed flux of a particular magnetic field and a known inductance of the circuit. .

5 For example, if the processor 360 receives a signal from the flux sensor 316 that the particular magnetic field has a flux of 1.5 Teslas then the processor 360 can use a Larmor frequency formula, as described herein, to determine that the

10 particular magnetic field has a Larmor frequency of 64 MHz. Further, in this example, if the LC resonator circuit has a known inductance of 0.69 microHenries, which can be known, for example, based on a known configuration of the inductor of the LC resonator circuit, then the processor can use the LC circuit resonance formula to determine that the resonant capacitance for that

15 circuit is 8.9 picoFarads. Finally, in this example, in response to the known flux of a particular magnetic field and a known inductance of the circuit the processor can then direct the adjustable capacitance control 330 to adjust the adjustable capacitance 320 to 8.9 picoFarads.

The processor 360 can also direct the adjustment of the adjustable capacitance 320 of the LC resonator circuit to a resonant capacitance by executing logic and/or program instructions in response to sensed voltages across the adjustable capacitance 320 and/or sensed currents through the resonator circuit, for particular magnetic fields. For example, for a particular magnetic field, the processor 360 can direct the adjustable capacitance 320 to adjust to a particular 25 capacitance, receive a signal from the voltage sensor 312 that represents a sensed voltage across the adjustable capacitance 320, and repeat this adjusting and sensing to determine a resonant capacitance at which a voltage across the adjustable capacitance 320 is a maximum voltage that can be obtained across the adjustable capacitance 320 in that particular magnetic field. In an alternative 30 example, the processor 360 can perform a similar adjusting and sensing using a signal from the current sensor 314 to determine a resonant capacitance at a maximum current that can be obtained through the resonator circuit in a particular magnetic field. For these examples, the processor 360 can store sensed values in the memory 370, as necessary. The processor 360 can also repeat the adjusting of

the adjustable capacitance 320 by adjusting through all possible capacitance values, by performing a bracketing approach, or by using some other technique.

In various embodiments of the present disclosure, a resonant capacitance for the LC resonator circuit of the resonator device 302 of Figure 3B can be 5 determined in other ways. In one embodiment, the adjustable capacitance 320 can be adjusted to a known capacitance, an inductance of the LC resonator circuit can be calculated, and a resonant capacitance for the LC resonator circuit can also be calculated, based on a known or sensed flux value and the calculated inductance. The inductance of the LC resonator circuit can be calculated by using various 10 general circuitry formulas such as Kirchoff's voltage law, Kirchoff's current law, and other defined relationships for resistance, reactance, impedance, and frequency response for LC circuits, as will be understood by one of ordinary skill in the art. In another embodiment, a resonant capacitance for the LC resonator circuit can be determined from a frequency response of the LC resonator circuit as 15 sensed by the voltage sensor 312, the current sensor 314, and/or another type of sensor.

Various embodiments of the inductor coil 304 of the resonator device 302 of Figure 3B can be made as described herein. In one embodiment, the inductor coil 304 can be a commercially available inductor coil with a number of windings, 20 a radius, and a length chosen to suit a particular application. In another embodiment, the inductor coil 304 can be fabricated from a flexible conductive material, such as copper or a copper alloy, with an adjustable radius, such as a radius that can increase when used with an expandable stent. In various other embodiments of Figure 3B, more than one inductor coil can be used in the LC 25 resonator circuit. In an alternate embodiment of the present disclosure, a core inductor can be used in place of an inductor coil.

Various embodiments of the adjustable capacitance 320 of the resonator device 302 of Figure 3B can also be made as described herein. In one embodiment, the adjustable capacitance 320 can include the varactor 320, which 30 is sized to have a range similar to a lower end of a range of estimated adjustable capacitance. For example, if a lower end of a range of estimated adjustable capacitance is 0.41 picoFarads, as described in Figure 3A, then the varactor 320 can have a capacitance range of 1 picoFarad.

In various embodiments of the resonator device 302, capacitors in the adjustable capacitance 320 can be of increasing size, to provide for a continuous range of possible capacitance. For example, in one embodiment of the present disclosure, the adjustable capacitance 320 can include a varactor with a 1 5 picoFarad adjustable capacitance, and capacitors with values of 1, 2, 4, 8, 16, 32, 64, 128, 256, 512, 1012, 2048, and 4096 picoFarads. Using combinations of capacitors in this example can provide adjustable capacitance values from zero Farads to 8.2 nanoFarads, which is a sufficient range to provide resonant 10 capacitance in a resonator device for MRI from 1.5 to 3.0 Teslas and inductor coil inductances from 0.79 nanoHenries to 0.69 microHenries, as described herein. In various embodiments, the adjustable capacitance 320 can also include various other combinations of capacitors. Although the embodiment of Figure 3B shows one varactor and four capacitors in parallel, other numbers of varactors and/or capacitors can be used, in various embodiments of the present disclosure. 15 Additionally, resistors and other electrical components can be added to the LC resonator circuit of the resonator device 302 to provide different resonant frequency responses, as will be understood by one of ordinary skill in the art.

Figure 4A illustrates an embodiment of a resonator system with a medical device according to the present disclosure. The system embodiment of Figure 4A 20 includes a stent 402, and a resonator device including an inductor coil 404, connecting conductors 406 and a circuit package 408. In the embodiment shown in Figure 4, the inductor coil 404 surrounds the stent 402 and extends beyond both ends of the stent 402. In various embodiments, the inductor coil 404 can relate to an implantable medical device, such as the stent 404, in various ways. In one 25 embodiment, a portion of the inductor coil 404 can surround a space that is surrounded by at least a portion of a medical device. For example, a portion of the inductor coil 404 can surround a portion of a passageway of a stent. In another embodiment, a portion of the inductor coil 404 can surround the medical device.

30 As in Figures 3A and 3B, electrical components encapsulated by the circuit package 408 include sensors, an adjustable capacitance, an adjustable capacitance control, a processor, a memory, a power source, and a selector. The inductor coil 404, the connecting conductors 406, at least a portion of the adjustable capacitance, and a portion of the adjustable capacitance control

together form an LC resonator circuit. In this embodiment, the processor automatically adjusts the adjustable capacitance of the LC resonator circuit to a resonant capacitance, in response to a flux from a magnetic field, as described in Figures 3A and 3B. Thus, the system embodiment of Figure 4A can resonate over 5 a range of MRI frequencies, enhancing the visualization of the stent 402, when performing MRI.

Figure 4B illustrates another embodiment of a resonator system with a medical device according to the present disclosure. The system embodiment of Figure 4B includes a stent with a meandering coil 422, connecting conductors 426 10 and a circuit package 428. As in Figures 3A and 3B, electrical components encapsulated by the circuit package 428 include sensors, an adjustable capacitance, an adjustable capacitance control, a processor, a memory, a power source, and a selector. The meandering coil of the stent 422, the connecting conductors 406, at least a portion of the adjustable capacitance, and a portion of 15 the adjustable capacitance control together form an LC resonator circuit, with the meandering coil of the stent 422 forming the L component of the LC resonator circuit. In this embodiment, the processor automatically adjusts the adjustable capacitance of the LC resonator circuit to a resonant capacitance, in response to a flux from a magnetic field, as described in Figures 3A and 3B. Thus, the system 20 embodiment of Figure 4A can resonate over a range of MRI frequencies and stent diameters, enhancing the visualization of the stent 422, when performing MRI. Similarly, a resonator system can be made with other implantable medical devices such as a graft, a shunt, and a vena cava filter, as will be understood by one of ordinary skill in the art.

Figure 5 illustrates another embodiment of a resonator system with a medical device according to the present disclosure. The resonator system 500 of Figure 5 includes an inductor coil 504, connecting conductors 506 and a circuit package 508. As in Figures 3A and 3B, electrical components encapsulated by the circuit package 508 include sensors, an adjustable capacitance, an adjustable 25 capacitance control, a processor, a memory, a power source, and a selector. The inductor coil 504, the connecting conductors 506, a portion of the adjustable capacitance, and a portion of the adjustable capacitance control together form an LC resonator circuit. In this embodiment, the processor automatically adjusts the adjustable capacitance of the LC resonator circuit to a resonant capacitance, in

response to a flux from a magnetic field, as described in Figures 3A and 3B.

Thus, the system embodiment of Figure 5 can resonate over a range of MRI frequencies, enhancing the visualization of a distal end 580 of a catheter 574, when performing MRI.

5       Figure 5 also illustrates the catheter 574 with an elongate body 576, an inflatable balloon 578 positioned adjacent the distal end 580, and a lumen 582 longitudinally extending in the elongate body 576 of the catheter 574 from the inflatable balloon 578 to a proximal end 584. The catheter 574 can further include a guidewire lumen 586 to receive a guidewire 588. The inflatable balloon  
10      578 can be inflated through the use of an inflation pump 590 that can releasably couple to a lumen 582. In various embodiments, the inductor coil 504 can be placed inside a temporarily implantable medical device, such as the catheter 574, in various ways. In one embodiment, the inductor coil 504 can be connected to a temporarily implantable medical device. The resonator system 500 of Figure 5  
15      5 can be used with various temporarily implantable medical devices, such as a guiding catheter, a guiding wire, a catheter for stent delivery, or a catheter for dilation without a stent.

As discussed herein, embodiments of a resonator device or system can also be implanted into a body. As will be understood by one of ordinary skill in the  
20      art, a variety of procedures can be used to implant an embodiment of a resonator device or system with an implantable medical device. For example, certain embodiments of a resonator device can be implanted adjacent to a stent that has already been implanted in a body. Alternatively, both a stent and certain  
25      embodiments of a resonator device can be implanted simultaneously. For example, both a stent and a resonator device could be loaded onto a catheter (e.g., a balloon catheter) for implanting in a body. In various embodiments of the present disclosure a medical device can be a deliverable device, deliverable in a lumen of a body.

In the foregoing Detailed Description, various features are grouped  
30      together in several embodiments for the purpose of streamlining the disclosure. This method of disclosure is not to be interpreted as reflecting an intention that the embodiments of the disclosure require more features than are expressly recited in each claim. Rather, as the following claims reflect, inventive subject matter lies in less than all features of a single disclosed embodiment. Thus, the following

claims are hereby incorporated into the Detailed Description, with each claim standing on its own as a separate embodiment.

WHAT IS CLAIMED IS:

1. A resonator system for detecting a deliverable device, comprising:
  - a resonator device with an LC resonator circuit, including:
    - an adjustable capacitance;
    - an inductor coil in series with the adjustable capacitance; and
    - an adjustable capacitance control that can control the adjustable capacitance to obtain different particular capacitance values; and
  - a deliverable device, positioned with the resonator device, so that at least a portion of the inductor coil surrounds a space that is surrounded by at least a portion of the deliverable device.
2. The resonator system of claim 1, wherein:
  - the deliverable device is an implantable medical device; and
  - the resonator device includes a power source that can generate electrical power from a field for use by the adjustable capacitance control, wherein the field is selected from the group including:
    - an electro-magnetic field; and
    - an alternating magnetic field.
3. The resonator system of any of claims 1-2, wherein the adjustable capacitance includes capacitors and a varactor in parallel.
4. The resonator system of any of claims 1-3, wherein the resonator device includes a current sensor that can sense an electrical current flow through a path of the LC resonator circuit.
5. The resonator system of any of claims 1-4, wherein the resonator device includes a voltage sensor that can sense an electrical voltage differential across the adjustable capacitance.
6. The resonator system of any of claims 1-5, wherein:
  - at least a portion of the inductor coil has an adjustable radius; and

at least a portion of the inductor coil surrounds at least a portion of a passageway of an implantable medical device.

7. The resonator system of claim 6, wherein the implantable medical device is a permanently implantable medical device selected from the group including:

- a balloon expandable stent;
- a self-expandable stent;
- a graft;
- a shunt; and
- a vena cava filter.

8. The resonator system of claim 6, wherein the implantable medical device is a temporarily implantable medical device selected from the group including:

- a guiding catheter;
- a guiding wire;
- a catheter for stent delivery; and
- a catheter for dilation without a stent.

9. The resonator system of claim 1, wherein:

the deliverable device is a temporarily implantable medical device; and  
the resonator device is inside the temporarily implantable medical device.

10. A resonator system, comprising:

- a resonator circuit that includes an inductor coil in series with an adjustable capacitance;
- an adjustable capacitance control that can automatically adjust the adjustable capacitance to a resonant capacitance in response to magnetic fields of different strength;
- a power source connected to the adjustable capacitance; and
- an implantable medical device, wherein at least a portion of the implantable medical device is surrounded by the inductor coil.

11. The resonator system of claim 10, including a selector that manually adjusts the adjustable capacitance, at least in part, by changing a number of the parallel capacitors that are connected to the resonator circuit.
12. The resonator system of claim 10, wherein:  
the adjustable capacitance includes capacitors that are:  
in parallel; and  
connectable to the resonator circuit; and  
the adjustable capacitance control automatically adjusts the adjustable capacitance, at least in part, by changing a number of the parallel capacitors that are connected to the resonator circuit.
13. The resonator system of claim 12, wherein:  
the adjustable capacitance includes a varactor that is:  
parallel to the parallel capacitors; and  
connectable to the resonator circuit; and  
the adjustable capacitance control automatically adjusts the adjustable capacitance, at least in part, by adjusting a capacitance of the varactor.
14. The resonator system of any of claims 10-13, including a sensor:  
connected to a processor; and  
selected from the group including:  
a magnetic flux sensor;  
a voltage sensor connected across the adjustable capacitance; and  
a current sensor connected in line with a path of the resonator circuit.
15. The resonator system of any of claims 10-14, wherein the power source is selected from the group including:  
the inductor coil;  
a coil;  
a battery;  
a capacitor; and  
a secondary resonator circuit.

16. A method comprising:

providing a resonator circuit with an inductor coil in series with an adjustable capacitance to a deliverable device, deliverable in a lumen of a body, so that at least a portion of the inductor coil surrounds at least a portion of the deliverable device;

determining a resonant capacitance, at which the resonator circuit will resonate in a particular magnetic field; and

adjusting the adjustable capacitance to the resonant capacitance in the lumen.

17. The method of claim 16, wherein determining the resonant capacitance includes calculating the resonant capacitance of the resonator circuit, based on a known flux of the particular magnetic field and a known inductance of the resonator circuit.

18. The method of claim 16, wherein determining the resonant capacitance includes:

adjusting the adjustable capacitance to a known capacitance;

calculating an inductance of the resonator circuit, based on the known capacitance and a known flux of the particular magnetic field; and

calculating the resonant capacitance of the resonator circuit, based on the known flux and the calculated inductance of the resonator circuit.

19. The method of claim 16, wherein determining the resonant capacitance includes:

sensing a flux of the particular magnetic field; and

calculating the resonant capacitance of the resonator circuit, based on the sensed flux and a known inductance of the resonator circuit.

20. The method of claim 16, wherein determining the resonant capacitance includes:

sensing a flux of the particular magnetic field;

adjusting the adjustable capacitance to a known capacitance;

calculating an inductance of the resonator circuit, based on the known capacitance and a sensed flux of the particular magnetic field; and  
calculating the resonant capacitance of the resonator circuit, based on the sensed flux and the calculated inductance of the resonator circuit.

21. The method of claim 16, wherein determining the resonant capacitance includes:

adjusting the adjustable capacitance to a particular capacitance;  
sensing a voltage across the adjustable capacitance; and  
repeating the adjusting and the sensing to determine a particular capacitance at which the voltage across the adjustable capacitance is a maximum voltage that can be obtained by the adjustable capacitance in the particular magnetic field.

22. The method of claim 16, wherein determining the resonant capacitance includes:

adjusting the adjustable capacitance to a particular capacitance;  
sensing a current through the resonator circuit at the particular capacitance;  
and  
repeating the adjusting and the sensing to determine a particular capacitance at which the current through the resonator circuit is a maximum current that can be obtained by the adjustable capacitance in the particular magnetic field.

23. A method, comprising:

fabricating a resonator device that includes:  
a resonator circuit with an inductor coil in series with an adjustable capacitance; and  
an adjustable capacitance control that can automatically adjust the adjustable capacitance to a resonant capacitance in response to magnetic fields of different strength; and  
connecting the resonator device to a medical device so that at least a portion of the inductor coil surrounds at least a portion of the medical device.

24. The method of claim 23 wherein:

fabricating the resonator device includes fabricating an inductor coil out of a flexible conductive material so that the coil has an adjustable radius; and

connecting the resonator includes securing the inductor coil around a stent so that the adjustable radius can increase as the stent expands.

25. The method of any of claims 23-24, wherein connecting the resonator includes securing the resonator device in a distal end of a catheter.

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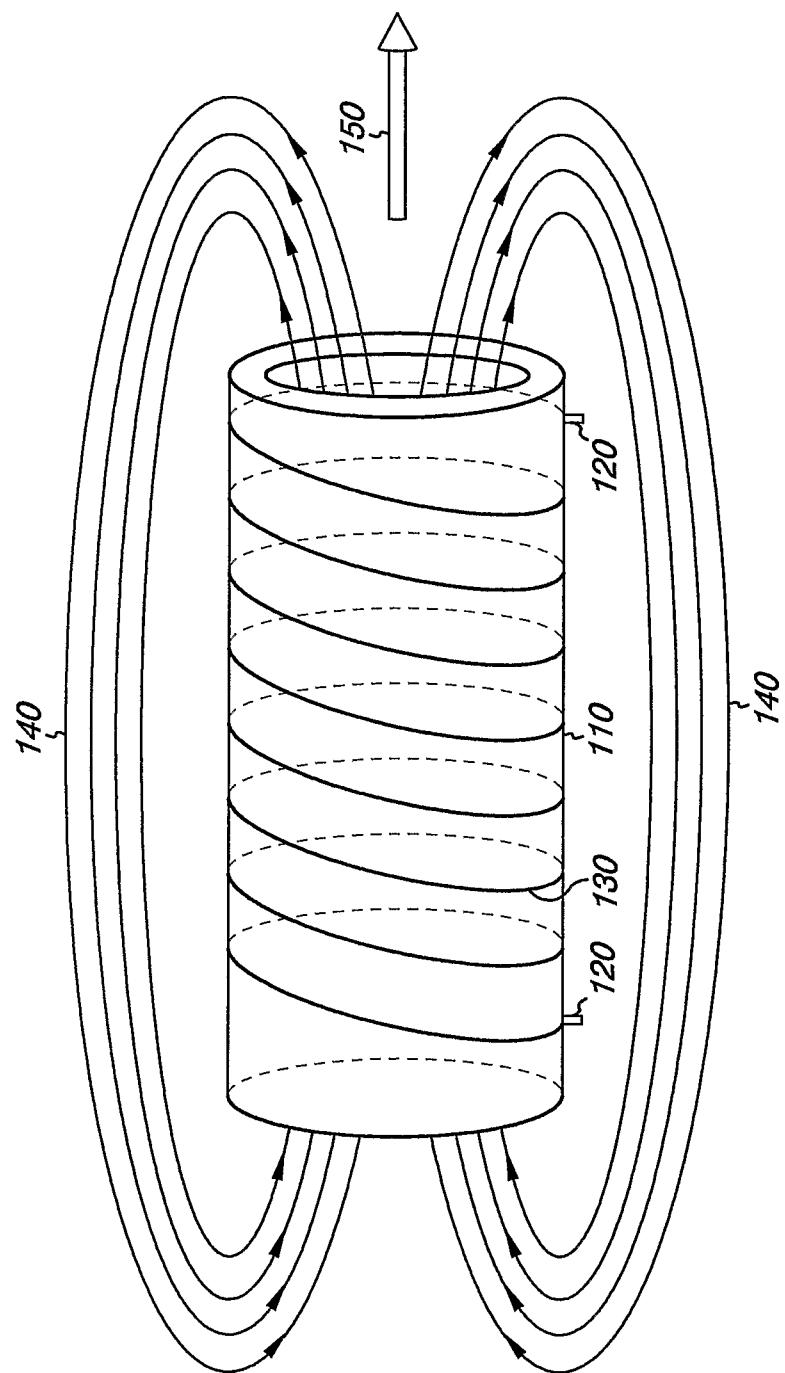


Fig. 1

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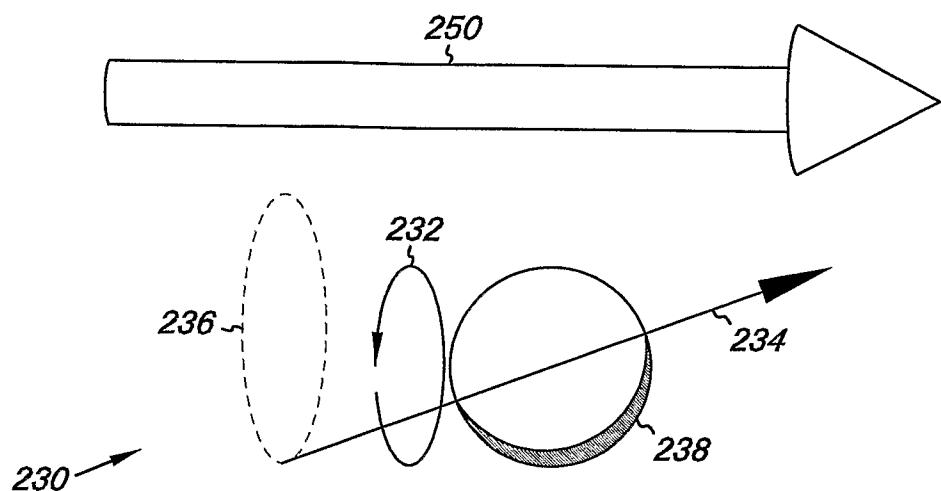


Fig. 2A

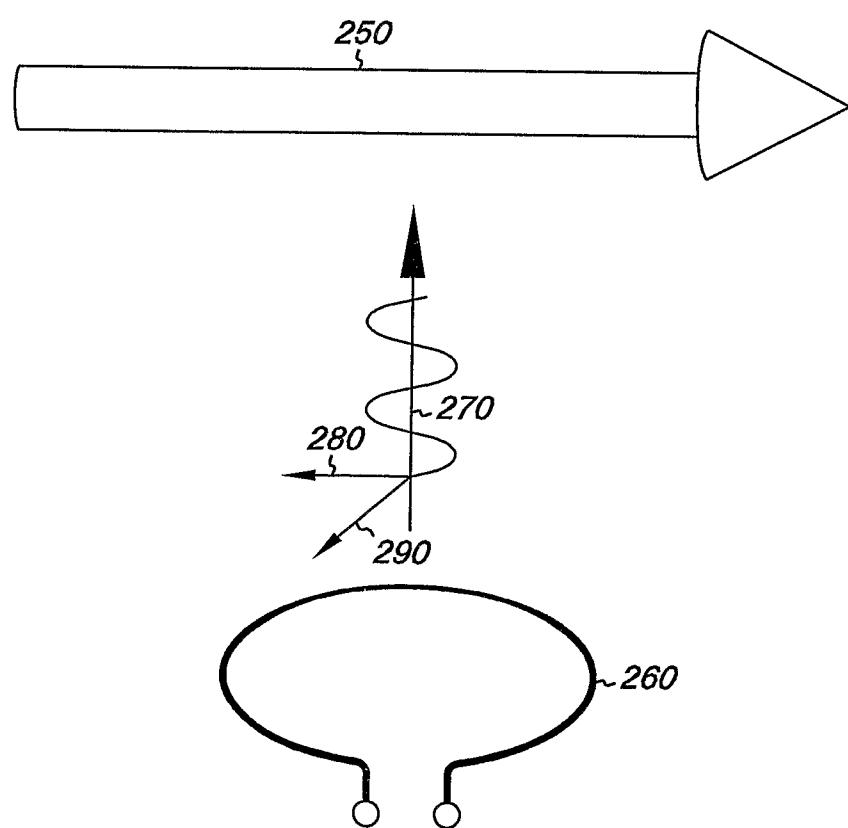


Fig. 2B

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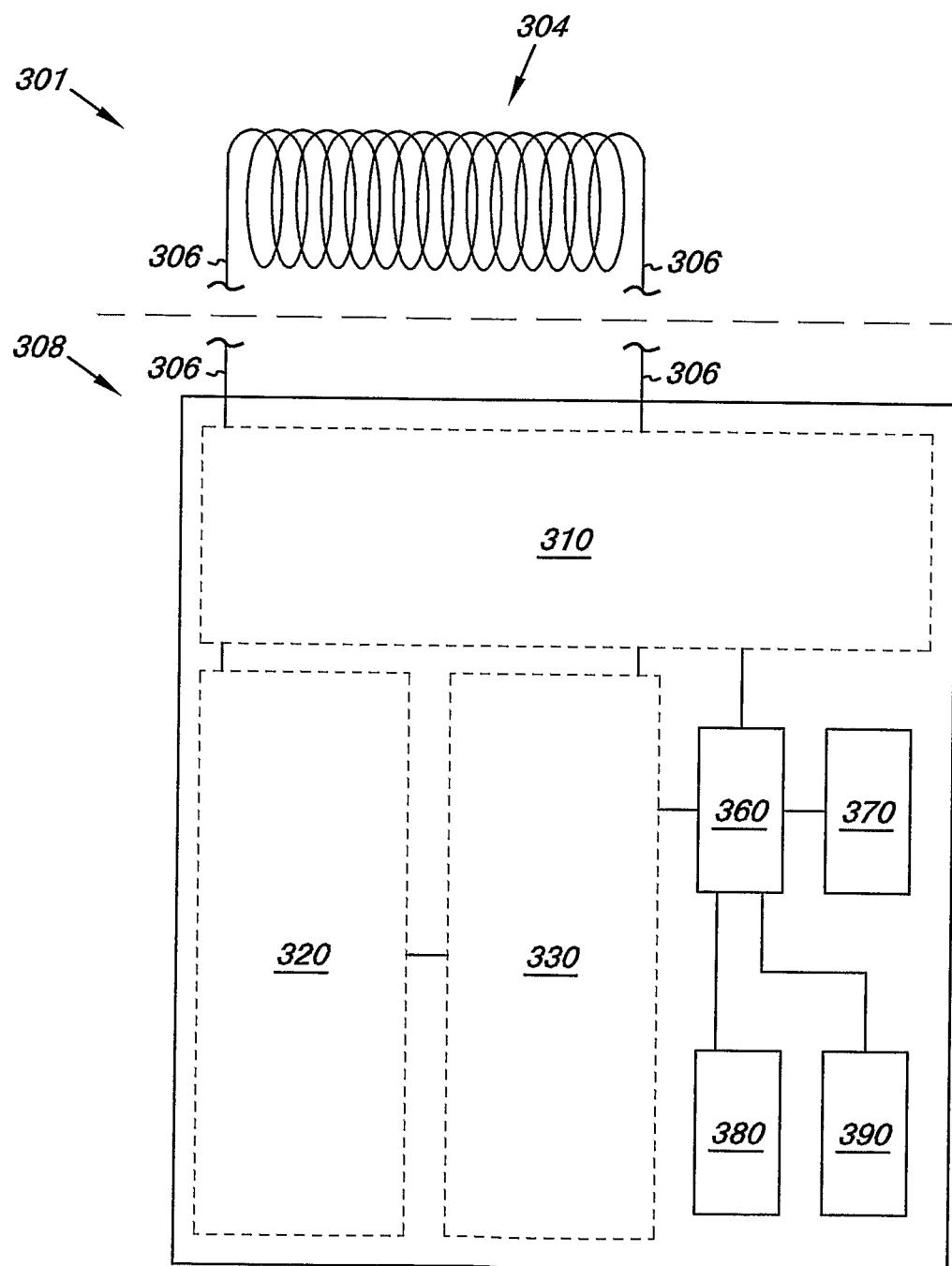


Fig. 3A

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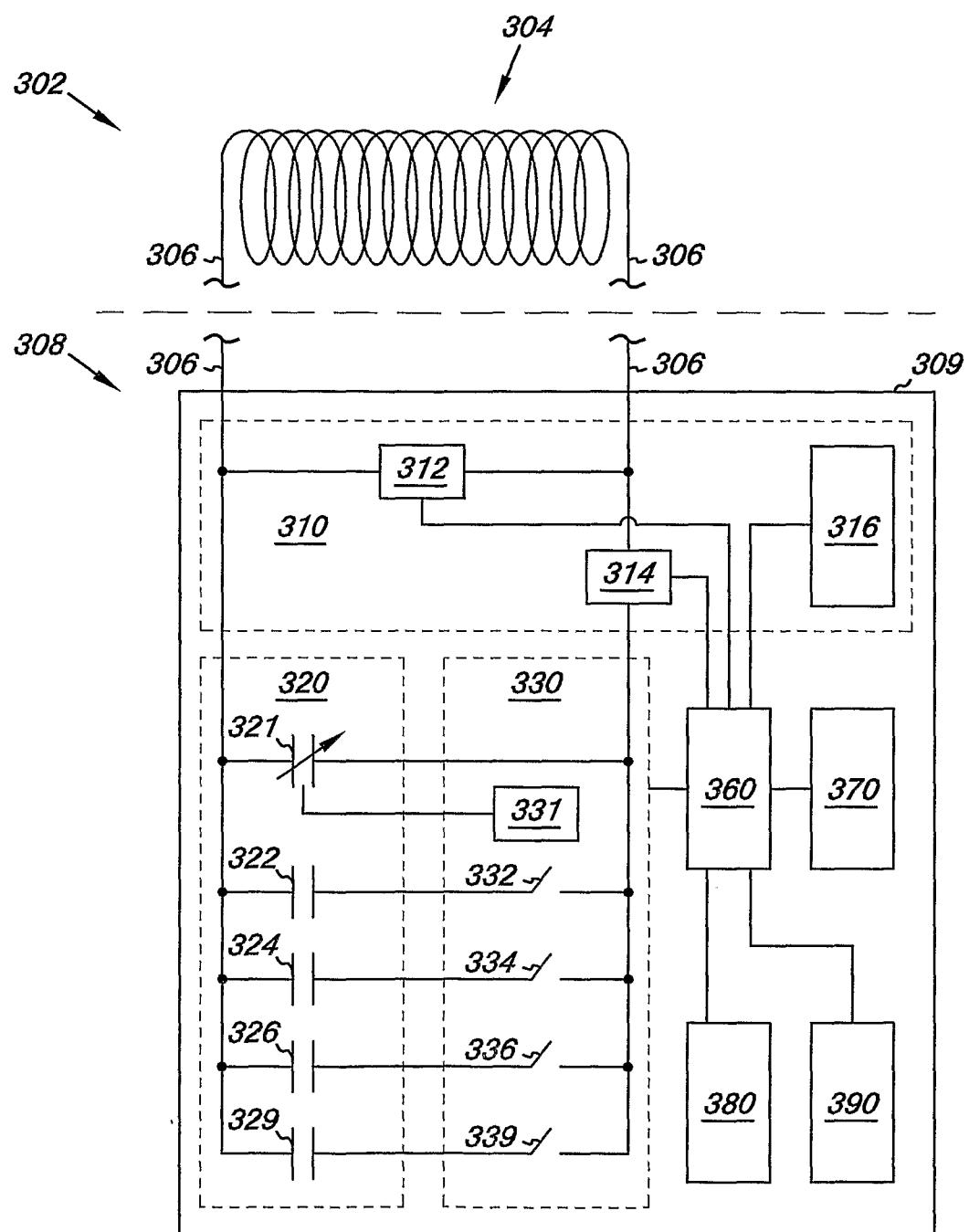


Fig. 3B

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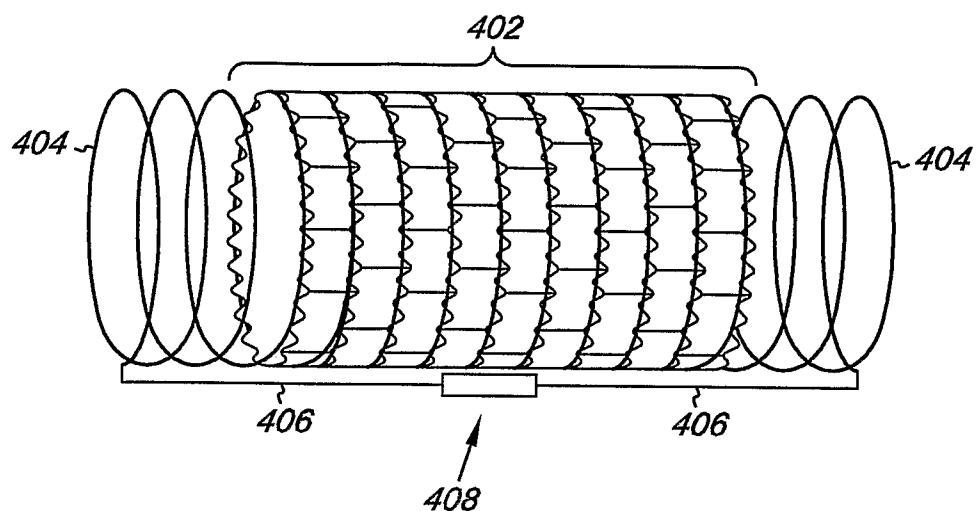


Fig. 4A

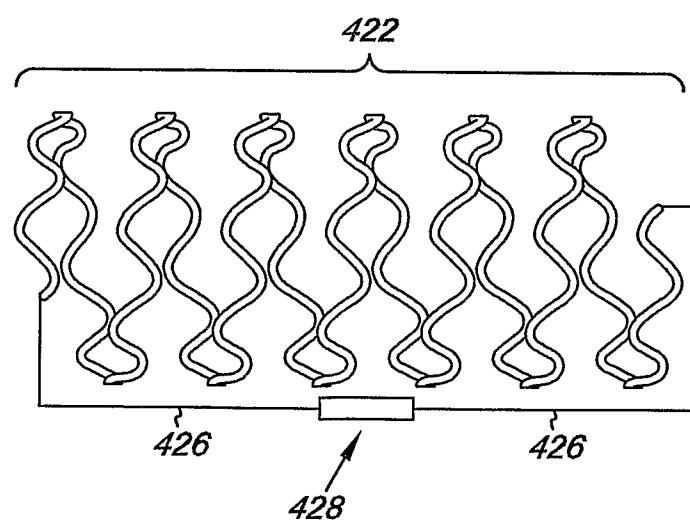


Fig. 4B

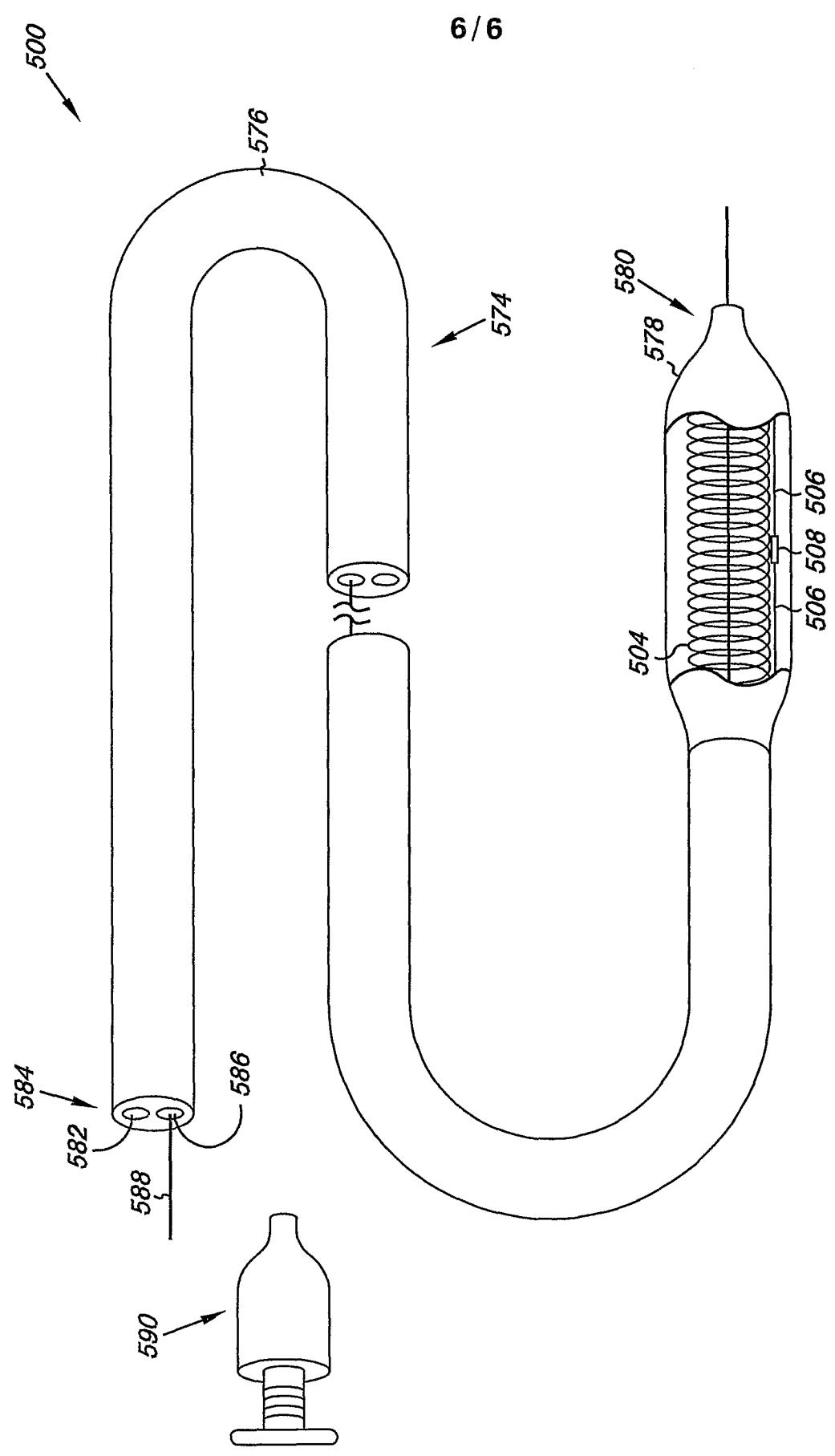


Fig. 5

# INTERNATIONAL SEARCH REPORT

International application No

PCT/US2006/041736

**A. CLASSIFICATION OF SUBJECT MATTER**  
INV. G01R33/28 G01R33/36

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
G01R A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, EMBASE, BIOSIS, COMPENDEX, INSPEC, WPI Data, MEDLINE

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

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|-----------|--|-----------------------|
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| X         | column 6, line 59 - column 9, line 62<br>column 10, line 46 - line 53<br>column 11, line 32 - line 37; claims 1,7  | 16,23-25              |
| Y         | VENOOK R D ET AL: "Automatic tuning of flexible interventional RF receiver coils"<br>MAGNETIC RESONANCE IN MEDICINE WILEY USA,<br>vol. 54, no. 4, October 2005 (2005-10),<br>pages 983-993, XP002419518<br>ISSN: 0740-3194<br>the whole document | 1-15,<br>17-22        |

Further documents are listed in the continuation of Box C.

See patent family annex.

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Date of the actual completion of the international search

Date of mailing of the international search report

12 February 2007

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Skalla, Jörg

## INTERNATIONAL SEARCH REPORT

|                              |
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| International application No |
| PCT/US2006/041736            |

| C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT |   |                       |
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Information on patent family members

International application No

PCT/US2006/041736

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