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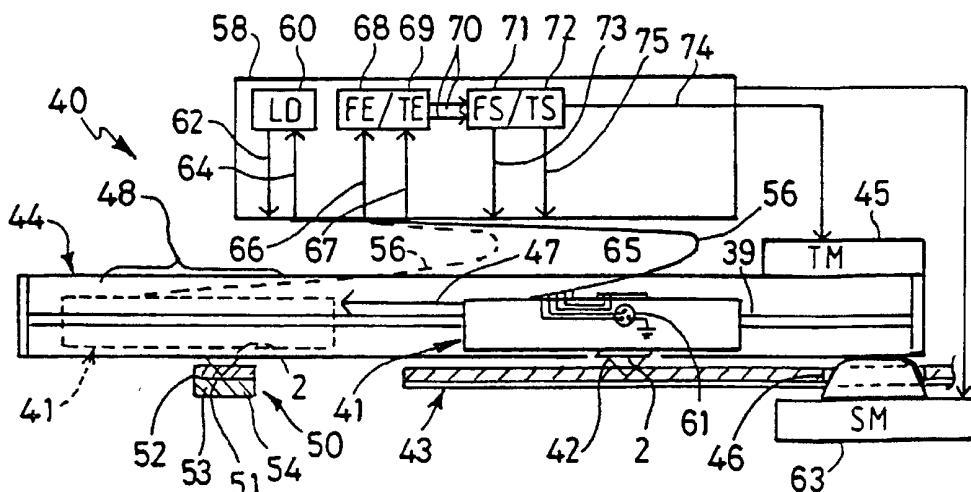
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(54) Title: OPTICAL MEDIA PICKUP ANTI-RATTLE



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Optical Media Pickup Anti-rattle

The present invention relates to an optical media system for suppressing externally induced rattle of an optical media pickup.

Optical media, such as optical discs, card or tape, are usually read and/or written to by an optical pickup containing an objective lens mounted in a voice coil actuator which performs focus and optionally tracking on the optical media. The objective lens is normally mounted in a carriage on a suspension, for example at the ends of flexible or hinged arms, with a biasing means that biases the lens to a neutral position often at the centre of a focussing range of about ± 1 mm. The focus motor is usually a voice coil actuator which moves between limits such as end stops that protect the focus actuator or lens from potential mechanical damage.

During normal operation in focussing on optical media, the end stops should never be reached, as a focus servo will keep the pickup focussed on the optical media. When the optical pickup is not being used, it may be moved off to one side of the optical media, so that the lens is no longer in position to read/write to/from the media.

The inventors have noted a problem with Compact Disc (CD) optical pickups in motor vehicles. Engine, road and wind noise reduction and rattle elimination is always desirable to provide for a quieter ride. In a very quiet car, rattles were noted in a CD player when the car was driven on a bumpy surface. The source of the noise was traced to the CD pickup hitting the focus end stops when the pickup was in a parked position, owing to vertical vehicle movement and vibrations.

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It is an object of the present invention to provide an optical media pickup with improved rattle characteristics.

Accordingly, the invention provides an optical media system comprising: an optical pickup for reading from and/or writing to an optical storage medium, the optical pickup having one or more sources of light, an objective lens, a focus and/or tracking actuator for moving the lens to focus and/or track the light on the optical medium and 5 mechanical limits to limit the focus and/or tracking movement of the lens; and an actuator controller for controlling the actuator and hence the focus and/or tracking position of the lens, characterised in that the actuator controller actively controls the lens position 10 when the optical pickup is not being used with the optical medium.

Because the focus lens position is controlled, rattling of the actuator is suppressed or eliminated.

20 The mechanical limits may be defined by the construction of the optical pickup, for example being provided by end stops about the lens and separated by a spacing along an axial focus direction of the lens, or along a tracking direction transverse to the axial position.

25 The light may be any suitable visible or invisible light source, for example, near infra-red laser light or LED light.

30 The term optical media systems includes optical disc, tape and card systems. These include read-only systems such as those using compact disc media and read/write/erase systems such as those using magneto-optic data disc media.

35 The optical pickup will in general include focus detection means which generates a focus error signal when the pickup

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is used to read from or write to the optical medium. The optical disc system will then contain focus servo electronics so that the focus actuator can be moved to keep the objective lens positioned correctly for focus on 5 the optical medium.

In a preferred embodiment of the invention, the optical pickup is moved to a park position away from the optical medium when not being used with such an optical medium.

10 Then, the system can include a focus object at the park position so that the actuator controller can focus the light on the focus object when the optical pickup is not being used with the optical medium in order to hold the lens focus position within the mechanical limits.

15 The focus object may advantageously be made to have similar optical characteristics to those of the optical medium. For example, if the optical medium has a transparent substrate through which the light is focussed to an information-bearing layer, then the lens will normally be adapted to focus light through this substrate in order to read and/or write to the optical medium. This is because focussing light through a planar substrate will introduce spherical aberration, which would result in an 20 increase in focus spot size. The light from the focus lens is therefore pre-aberrated with an opposite spherical aberration so that this aberration is cancelled after the light has traversed the correct thickness of substrate.

25 30 The focus object may then include a substrate similar to that of the optical medium. This gives the advantage of reducing any adverse affects on focus due to dust or dirt on the focus object.

35 Because in practice the focus object cannot be perfectly reflective, the light on the focus object will generate heat where this is focussed. Therefore, the focus actuator

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may control the lens position when the optical pickup is not being used with the optical medium so that the focus of light on the focus object is defocused in order to reduce the illuminance on the focus object. In this way, 5 the heat generated by the focussed light may be reduced.

Such an optical defocus may be obtained by injecting a focus offset signal into the electronic focus servo loop to the focus actuator.

10 Alternatively or additionally, the light may be pulsed on the focus object in order to reduce the average illuminance. When the focus servo uses light returned from the focus object to generate a focus error signal for a 15 feedback servo to the focus actuator, the pulsing of light should be set so that a sufficiently strong focus error signal may still be generated. Because the focus object is fixed, unlike the optical medium, the average light intensity on the focus object may be less than that on 20 the optical medium.

The focus object may contain thermally conductive material for dissipating heat absorbed from the focus light. For 25 example, the focus object may include a reflective layer on which the focus actuator focuses, the thermally conductive material being a thickness of the reflective layer significantly beyond that needed for bulk reflectivity.

30 For example, in the case of an aluminium reflector layer, about 40 nm to 50 nm thickness is needed in order to achieve a bulk reflectivity of about 95% at 830 nm. If the thickness is increased to about 250 nm, then the aluminium 35 layer will be able to conduct about five times as much heat from the focus area.

The focus or tracking actuator may be a voice coil

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actuator, the actuator controller being connected to the voice coil actuator and including circuitry that detects a voltage or a current generated by externally induced movement of the voice coil when the optical pickup is not being used with the optical medium in order to generate a compensating voltage or current in order to control the lens position.

10 The optical pickup may have at least one end stop that defines a limit to the focus and/or tracking movement of the lens. The actuator controller can then bias the lens towards an end stop when the optical pickup is not being used with the optical medium so that the lens position is held at the end stop.

15 Alternatively, when the optical pickup has a pair of end stops that define a limit to the focus (or tracking) movement of the lens, the actuator controller may control the lens position to a median position between the end 20 stops.

25 The optical media system may be used in a vehicle, such as a motor car, comprising a motive means by which the vehicle may be energised to move. The vehicle will in general have an electrical power source to power the optical media system. The actuator controller then actively controls the focus position of the lens when, and preferably only when, the vehicle is energised to move.

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The invention will now be further described, by way of example, with reference to the accompanying drawings, in which:

5 Figure 1 is a schematic view of a focus and tracking actuator of an optical pickup as seen from inside the pickup along the optical axis of an objective lens;

10 Figure 2 is a cross-section through the actuator of Figure 1, taken along line II-II;

Figure 3 is a cross-section through the actuator of Figure 1, taken along line III-III;

15 Figure 4 is a schematic drawing of an optical media system according to a first embodiment of the invention, showing an optical pickup with the actuator of Figure 1, with associated control electronics and an optical disc;

20 Figure 5 is a plot of focus error signal against defocus distance;

25 Figure 6 is a schematic drawing showing how defocus and a relatively thick reflector layer can be used to reduce heat absorbed from a focus spot of the optical pickup;

30 Figure 7 is a schematic drawing of an optical media system according to a second embodiment of the invention; and

35 Figure 8 is a schematic drawing of an optical media system according to a third embodiment of the invention.

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Figures 1, 2 and 3 show a focus and tracking voice coil actuator 1 of conventional design for an optical pickup. The actuator has an objective lens 2 with a numerical aperture of 0.6 held in a surrounding cradle 4. The cradle 4 supports pairs of coils 6,8. One pair of coils 6 has a common axis 10 transverse to an optical axis 12 of the lens, and serves as a tracking actuator. The other pair of coils 8 has a common axis coincident with the optical axis 12 and serves as a focus actuator.

When electrical current is passed through a pair of coils 6,8, this generates a magnetic field which then interacts with a permanent magnetic field produced by a pair of permanent magnets 14 on opposite sides of the optical axis 12, in order to drive the cradle and objective lens along either the tracking axis 10 or the focus axis 12.

The cradle is supported by four straight suspension wires 16,17,18,19, which are arranged in pairs 16,17 and 18,19. As shown in Figure 2, one pair 16,17 is generally above the coils 6,8 and the other pair 18,19 is generally below the coils 6,8. The wires all terminate at one end away from the cradle at corresponding electrical terminals 20 on a terminal block 22, and at the other end to corresponding terminals 24 to which ends of the coils 6,8 are wired. Therefore, current to drive the focus and tracking actuator 1 is supplied to the coils through the suspension wires 16-19.

Tension in the wires 16-19 when these are moved away from a neutral position creates biasing forces, which will tend to return the cradle 4 to a neutral position.

The terminal block supports a frame 26 that extends fully around the cradle 4 in a plane transverse to the optical axis 12 of the lens 2.

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The frame 26 in turn supports a pair of end stops 28,30 shown most clearly in Figure 2, one of which 28 extends frame-like about the optical axis 12 above the cradle, and the other of which 30 consists of a pair of ledges 31,32 that are inwardly directed towards the lens 2 in a plane generally below the cradle 4.

When the focus actuator is driven fully inwards, a top surface 34 of the cradle 4 contacts the upper stop 28, and when the focus actuator is driven fully outwards, a bottom surface 35 of the cradle 4 contacts the lower stop 30.

The frame 26 has a pair of inwardly directed projections 36,37, which act as stops in the tracking direction.

The focus and tracking stops 28,30,36,37 act to protect the focus and tracking actuator 1, and particularly the suspension wires 16-19, from mechanical damage which would occur at an extreme movement of the cradle 4 relative to the terminal block 22.

It has been discovered that in a motor car vibrations from the road cause a rattling between the cradle and focus end stops 28,30, but not between the cradle and tracking end stops. There are two reasons for this. One is that vibrations tend to be strongest in a vertical direction, which normally coincides with the optical axis 12, and the other is that the stiffness of the suspension wire to movement of the cradle in the tracking direction can be greater than in the focus direction. This difference in stiffness is due to the fact that the required frequency response of the tracking actuator is less than that required from the focus actuator.

Figure 4 shows a first embodiment of the invention 40, in which the focus and tracking actuator 1 is incorporated in a conventional optical disc pickup 41. The pickup is shown

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focussing a beam of laser light 42 from the lens 2 onto a compact disc (CD) 43. The pickup 41 is mounted on rail 39 of a conventional linear tracking actuator 44 driven by a coarse tracking motor (TM) 45. The tracking motor 45 can move the optical pickup 41 so that the lens 2 can focus on an innermost portion 46 the CD 43. When the pickup is not being used to read from the CD, the tracking motor 45 can move 47 the optical pickup away from the CD 43 to a park position 48, as shown by the optical pickup 41 drawn in phantom.

A focus object 50 is provided at the park position 48 on which the lens 2 may focus. The focus object consists of a an aluminium reflector layer 51 encapsulated by a transparent substrate 52 of 1.1 mm thick polycarbonate, a lacquer backing layer 53, held in a surrounding moulded plastic cup 54.

When the lens 2 is focussed on the focus object 50, the position of the cradle 4 along the focus axis 12 is actively controlled so that the cradle is restrained from rattling against the focus end stops 28,30.

A person skilled in the art will be familiar with the conventional operation of an optical pickup, and so this will be described only briefly. The optical pickup 41 is connected by a ribbon cable 56 to control electronics 58. The control electronics 58 includes a laser diode driver (LD) 60 that supplies a current 62 to a laser diode 61 in the optical pickup, and receives from the laser diode 61 a power monitor signal 64. When the CD 43 is set spinning by a spindle motor 63 under the control of the control electronics 58, and the CD 43 is in view of the lens 2, a quadrant photodiode 65 sends a focus error signal 66 and a tracking error signal 67 to a corresponding focus error circuit 68 and tracking error circuit 69, which in turn are connected 70 to a focus servo circuit 71 and a

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tracking servo circuit 72. The focus servo circuit generates an appropriate focus correction signal 73, and the tracking servo circuit 72 generates both a coarse tracking correction signal 74 that is fed to the tracking 5 motor 45, and a fine tracking correction signal 75. The focus and tracking correction signals 73,75 are then fed back to the focus and tracking coils 8,6 to keep the optical pickup 41 correctly focused and on track.

- 10 When the optical pickup 41 is in the park position 48, the control electronic can be used to keep the lens focussed on the focus object, and so avoid rattling of the optical pickup 41. This control can be activated whenever rattles might be expected. For example, if the optical media 15 system 40 is part of a CD played in a motor car (not shown), then the active control of focus in the parking position may be activated as soon as the motor vehicle is energised by the driver.
- 20 In use with a CD, the laser power will be typically 1 mW. In order to reduce power consumption, and the heat absorbed by the focus object 50, the laser power at the focus position may be reduced to about 0.1 mW or less, either by pulsing the laser at a 10% duty cycle, or by 25 reducing the laser power, or by a combination of these. Because the focus object is not moving relative to the optical pickup 41, this reduced power should not unduly affect focus operation.
- 30 Figures 5 and 6 show another way in which the heat absorbed by the focus object 50 may be reduced. Figure 5 shows a plot of an S-shaped focus error signal 47 against defocus distance. The focus error signal 47 is zero outside ± 40 nm of best focus. It is possible by 35 introducing an offset into the derived focus error signal to lock onto focus at any point on the curve 47 with a sufficiently high slope, for example at a defocus distance

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d_0 of 20 nm. As can be seen in Figure 6, at this defocus distance, the focus spot size S will be about 10 μm , which implies an energy density about 100 fold less than at the best focus at the focus waist W of about 1 μm .

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In addition, the reflector layer 51 is about 250 μm thick in order to increase the ability of the reflector layer 51 to conduct heat away from the focus spot S.

10 Figure 7 shows a second embodiment of an optical media system 80. This differs from the first embodiment 40 in that there is no focus object, and in that once the optical pickup 41 is in the park position 48, the focus coils 8 are energised to retract fully the lens 2 so that the cradle 4 is held securely against the upper stop 28. This is done with modified control electronics 81 in which a focus offset 82 is added to the focus servo 71. The cradle 4 can then be held against the upper end stop 28 with sufficient force so that expected vibration does not cause rattling of the cradle 4 against the end stops 28,30. An advantage of this embodiment is that there is no need to provide a focus object 50 which, although potentially quite inexpensive, does use a volume within the optical media system and add some small mechanical complexity.

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Figure 8 shows a third embodiment of an optical media system 90. This differs from the first embodiment 40 in that there is no focus object, and from the second embodiment 80 in that the position of the lens 2 and cradle 4 is not controlled so that the cradle is held against one of the end stops 28,30. There are two advantages to this approach. The first is that there is no need to provide a focus object 50 and the second is that the focus actuator is not biased fully in one direction, thereby avoiding any induced distortion over time to the wire suspension of the focus and tracking actuator.

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In the park position 48 of Figure 8, the position of the lens 2 is held away from the end stops 28,30 by the detection of currents induced in the focus coil 8 by movement of the focus coil in the static magnetic field of the permanent magnets 14. The currents are detected by modifying the control electronics 91 so that this includes a focus current detection circuit (FC) 92. An output 93 from the focus current detection circuit 92 is fed to the focus servo, which then generates with a current mirror an opposite current which is fed back into the focus coils 8 to cancel partially the induced movement of the lens 2 and cradle 4. Although it is not possible to cancel entirely the movement of the lens owing to inevitable lags between the detection of the induced current and the generation of a cancelling current, the movement can be controlled sufficiently to keep the cradle 4 from hitting the end stops owing to vibration in a moving motor car.

If tracking rattle is a problem, then the three embodiments described above may be modified so that instead of or in addition to the focus position being controlled, the tracking position is controlled. For example, in Figure 4, the focus object 50 may have tracking grooves arranged essentially parallel with similar grooves on the optical disc 43. The tracking servo 72 could then control the position of the lens 2 and cradle 4 to suppress or eliminate rattle in the tracking direction. In Figure 7, the cradle 4 could be moved left or right so that this came up against one or the other of the tracking end stops 36,37. In Figure 8, circuitry similar to that described for focus current detection and cancellation could be used to control tracking movement of the cradle 4 owing to vibration in the tracking direction.

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The invention therefore provides a number of ways in which rattling of a focus and/or tracking actuator may be

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controlled in order to suppress or eliminate rattle induced by external vibrations of the optical media system. This is particularly useful in an automotive application, where in-vehicle rattles can be annoying to a 5 driver or passengers.

Claims

1. An optical media system (40) comprising: an optical pickup (41) for reading from and/or writing to an optical storage medium (43), the optical pickup (41) having one or more sources of light (61), an objective lens (2), a focus and/or tracking actuator (1) for moving the lens (2) to focus and/or track the light (61) on the optical medium (43) and mechanical limits (28,30,36,37) to limit the focus and/or tracking movement of the lens (2); and an actuator controller (58) for controlling the actuator (1) and hence the focus and/or tracking position of the lens (2), characterised in that the actuator controller (58) actively controls the lens position when the optical pickup (41) is not being used with the optical medium (43).
2. An optical media system (40) as claimed in Claim 1, in which the optical pickup (41) is moved to a park position away from the optical medium (43) when not being used with such an optical medium (43).
3. An optical media system (40) as claimed in Claim 2, in which the system includes a focus object (50) at the park position so that the actuator controller (58) can focus the light (61) on the focus object (50) when the optical pickup (41) is not being used with the optical medium (43) in order to hold the lens position within the mechanical limits (28,30).
4. An optical media system (40) as claimed in Claim 3, in which the lens (2) is adapted to focus light (61) through an optical substrate in order to read and/or write to the optical medium (43), and the focus object includes a similar substrate (52).

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5. An optical media system (40) as claimed in Claim 3 or
Claim 4, in which the actuator controls the lens position
when the optical pickup (41) is not being used with the
optical medium (43) so that the focus of light (61) on the
5 focus object is defocused in order to reduce the
illuminance on the focus object (50).

6. An optical media system (40) as claimed in any of
Claims 3 to 5, in which the light (61) is pulsed on the
10 focus object (50).

7. An optical media system (40) as claimed in any of
Claims 3 to 6 in which the focus object (50) contains
thermally conductive material (51) for dissipating heat
15 absorbed from the focus light (61).

8. An optical media system (40) as claimed in Claim 7,
in which the focus object (50) includes a reflective layer
(51) on which the focus actuator (1) focuses, the
thermally conductive material being a thickness of the
20 reflective layer significantly beyond that needed for bulk
reflectivity.

9. An optical media system (40) as claimed in Claim 1 or
Claim 2, in which the actuator is a voice coil actuator
(1), the actuator controller (58) being connected to the
voice coil actuator (1) and including circuitry (92) that
detects a voltage or a current generated by externally
induced movement of the voice coil when the optical pickup
30 (41) is not being used with the optical medium (43) in
order to generate a compensating voltage or current (71)
in order to control the lens position.

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10. An optical media system (40) as claimed in Claim 1 or
Claim 2, in which the optical pickup (41) has at least one
end stop (28,30,36,37) that defines a limit to the focus
and/or tracking movement of the lens (2), and the actuator
5 controller (58) biases the lens (2) towards an end stop
(28,30,36,37) when the optical pickup (41) is not being
used with the optical medium (43) so that the lens
position is held at the end stop (28,30,36,37).

10 11. An optical media system (40) as claimed in any of
Claims 1 to 9, in which the optical pickup (41) has a pair
of end stops (28,30,36,37) that define a limit to the
focus and/or tracking movement of the lens (2), and the
actuator controller (58) controls the lens position to a
15 median position between the end stops (28,30,36,37).

12. A vehicle comprising a motive means by which the
vehicle may be energised to move, an optical media system
(40), and an electrical power source to power the optical
20 media system (40), the optical media system being as
claimed in any preceding claim, in which the actuator
controller (58) actively controls the focus and/or
tracking position of the lens (2) when the vehicle is
energised to move.

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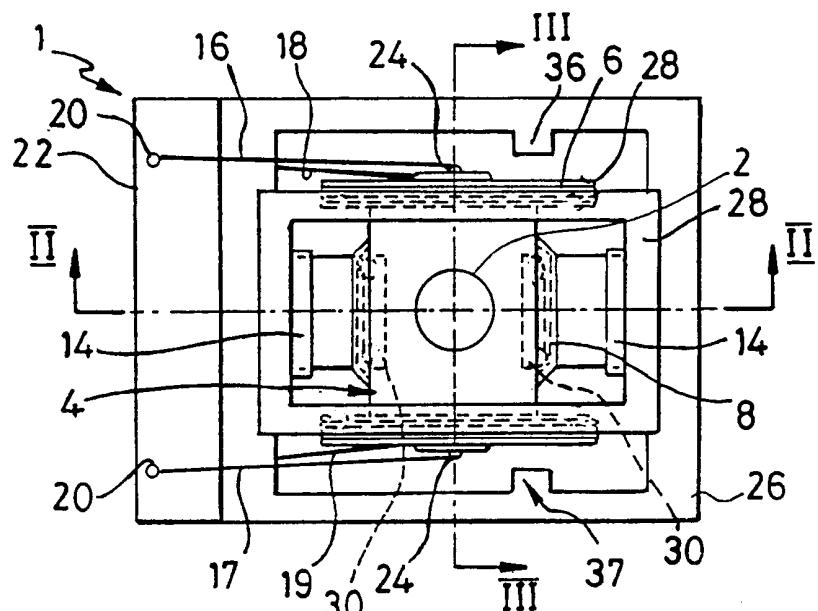


Fig. 1

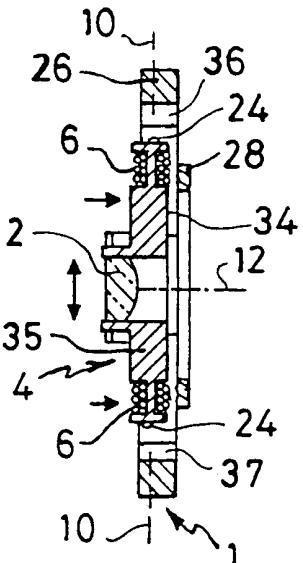


Fig. 3

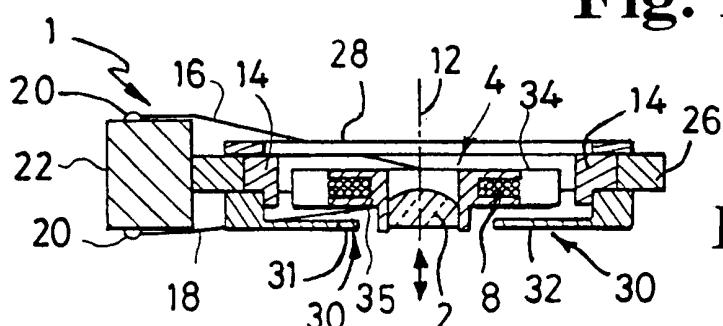


Fig. 2

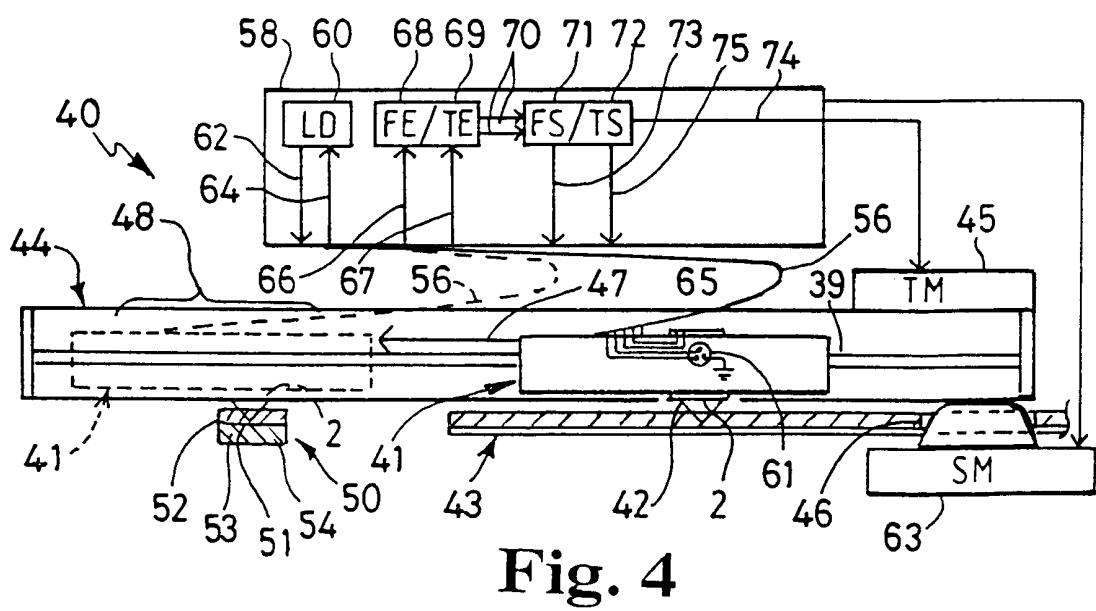
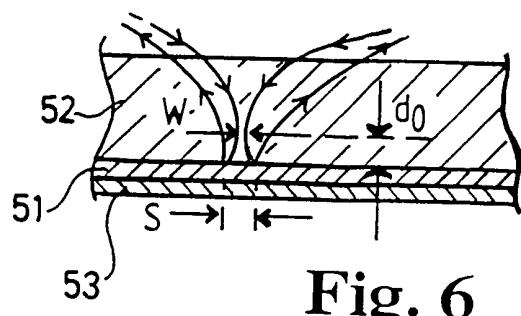
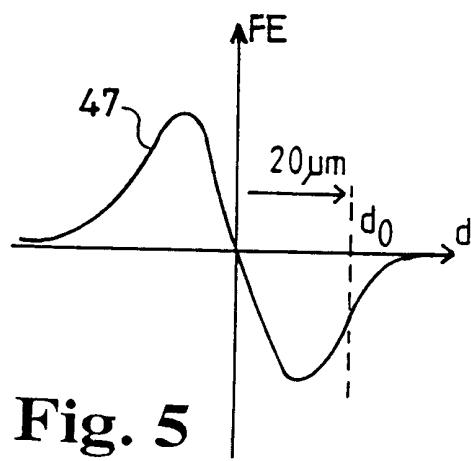
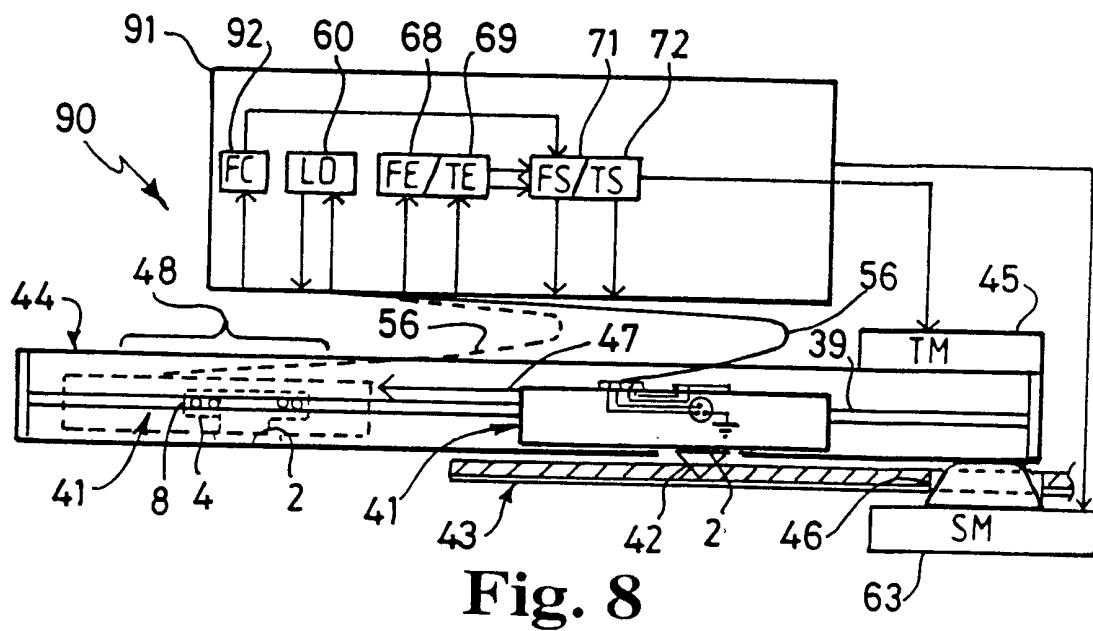
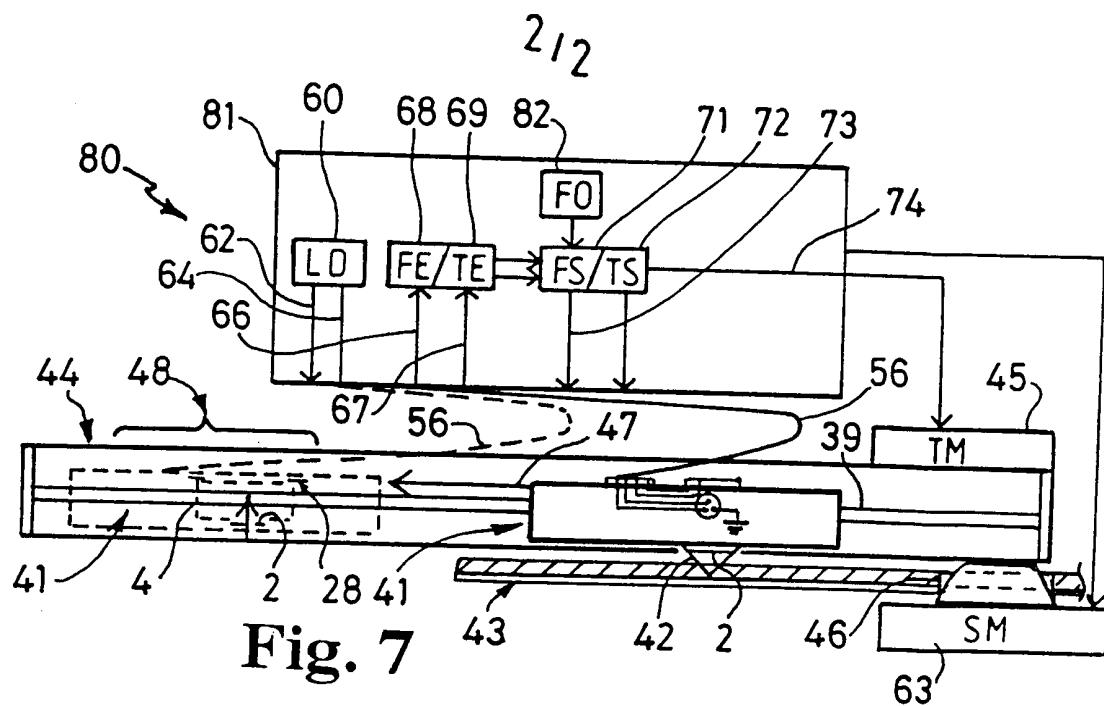


Fig. 4



INTERNATIONAL SEARCH REPORT

International Application No

PCT/GB 00/02595

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 G11B7/09

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 G11B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, PAJ

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	PATENT ABSTRACTS OF JAPAN vol. 1999, no. 08, 30 June 1999 (1999-06-30) & JP 11 066574 A (NIPPON CONLUX CO LTD), 9 March 1999 (1999-03-09) abstract ---	1
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A	US 5 020 045 A (SMART GERALD J ET AL) 28 May 1991 (1991-05-28) abstract ---	1
		-/-

Further documents are listed in the continuation of box C.

Patent family members are listed in annex.

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Date of the actual completion of the international search

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Name and mailing address of the ISA

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Quaranta, L

INTERNATIONAL SEARCH REPORT

Intern	na	Application No
PCT/GB 00/02595		

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

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