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(71) Applicant: IVECO S.P.A. [IT/IT]; Via Puglia, 35, 10156 Torino (IT).

(72) Inventor: ROCCATO, Maurizio; Via Fiume, 17, 10024 Moncalieri (IT).

(74) Agent: FRANZOLIN, Luigi et al.; c/o Studio Torta S.p.A., Via Viotti, 9, 10121 Torino (IT).

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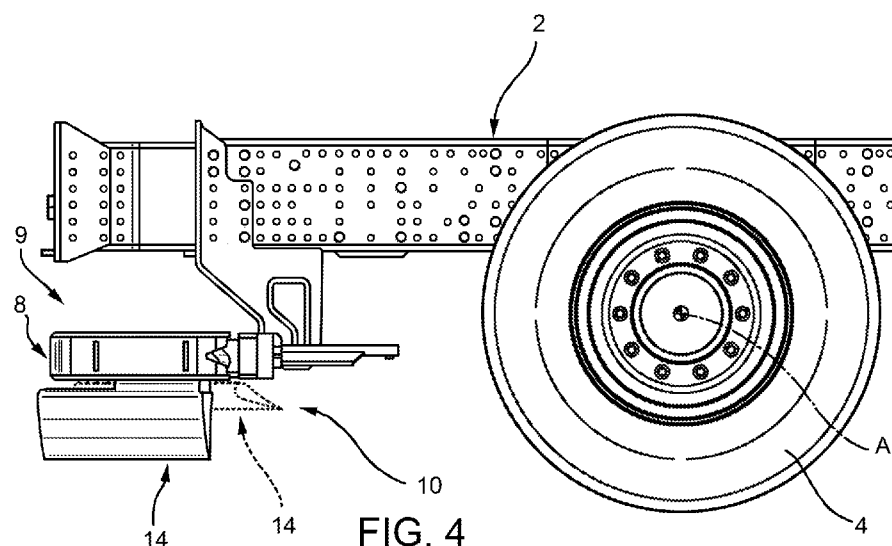
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(54) Title: ANTI-RUN OVER SAFETY DEVICE FOR A VEHICLE



(57) Abstract: Anti-run over safety device (10) for an industrial vehicle (1) comprising a plurality of bulkheads (14a, 14b) hinged to a lower front cross-member (8) of the vehicle (1) and movable, in case of impact, from a raised running position to a lowered activated position, in which they cantilever downward to reduce the free frontal space below the vehicle (1).



"ANTI-RUN OVER SAFETY DEVICE FOR A VEHICLE"

5

TECHNICAL FIELD

The invention relates to an anti-run over safety device
10 for a vehicle.

BACKGROUND ART

Recent changes to EU regulations allow derogations on
the maximum sizes of motor vehicles, in order to obtain a
greater (aerodynamic) energy efficiency and to improve
15 safety, though without compromising load capacity.

Therefore, manufacturers are allowed to elongate the
cabin front of B-trains and trailer trucks, compared to the
dimensions currently used, provided that the vehicle is
capable of moving inside a space defined by a circular crown
20 having predetermined inner and outer radii (12.5 m and 5.3
m, respectively).

A front elongation of the cabin leads to an increase of
the front projection of the cabin relative to the axis of
the front wheels. Given the same height of the cabin from

the ground, this would imply a reduction of the ramp angle of the vehicle.

Hence, in order to avoid a reduction of the ramp angle, the free front space below the cabin needs to be increased.

5 However, this would lead to a greater risk of running over vulnerable road users (pedestrians, cyclists, motorcyclists) in case of collision.

DISCLOSURE OF INVENTION

The object of the invention is to provide a safety device
10 for an industrial vehicle that is capable of solving the above-mentioned problem.

In order to do so, an anti-run over safety device for an industrial vehicle is provided, which comprises:

a support member, which is arranged in a lower front
15 area of the vehicle;

at least one bulkhead constrained to the support member and movable between a raised running position and a lowered activated position in which said bulkhead cantilevers downward to reduce the free front space below the vehicle;
20 and

means for activating the bulkhead in response to a signal indicating an impact.

The use of a movable bulkhead, which can be activated only in case of collision, allows manufacturers to have a
25 relatively great height of the cabin from the ground in running mode and, at the same time, to reduce the run-over

risk after a collision.

According to a preferred embodiment of the invention, plurality of simultaneously activatable movable bulkheads are provided. This solution allows manufacturers to reduce run-over risks even in case the cabin front is not straight but tapered, as the single bulkheads can follow the profile of the "face" of the vehicle.

Preferably, in case different bulkheads are used, the activating means are common.

10 According to an optional feature of the invention, the device comprises a manually operated reset device to bring the bulkhead(s) back to the running position after a collision.

BRIEF DESCRIPTION OF THE DRAWINGS

15 The invention will be best understood upon perusal of the following detailed description of a preferred embodiment, which is provided by mere way of non-limiting example, with reference to the accompanying drawings, in which:

20 figure 1 is a side view of a cabin of an industrial vehicle provided with a safety device according to the invention;

figure 2 is a partial front view of the cabin of figure 1;

25 figure 3 is a partial perspective view of the vehicle, with the cabin removed, showing the safety device of the

invention;

figure 4 is a partial side view of the vehicle, with the cabin removed, showing the device of the invention in two different operating positions;

5 figure 5 is a perspective view of the safety device of the invention in a running position;

figure 6 is a perspective view of a blocking mechanism of the device of figure 5, on a larger scale;

figure 7 is a diagram showing the operation of the
10 mechanism of figure 6;

figure 8 and figure 9 are two schematic views showing the mechanism of figure 6 in two different operating positions;

figure 10 is a partial and schematic elevation view of
15 a reset mechanism of the safety device of the invention; and

figure 11 is a schematic elevation view of a detail of the reset mechanism of figure 10.

BEST MODE FOR CARRYING OUT THE INVENTION

With reference to figure 1, number 1 indicates, as a
20 whole, an industrial vehicle comprising a frame 2 and a cabin 3, which is fitted on the frame in a known - and therefore not shown - manner. Furthermore, figures 1 and 2 show the front wheels 4 of the vehicle, with axis A, which are constrained to the frame by means of a suspension assembly,
25 which is known and not shown.

The cabin 6 is frontally delimited, moving from the top

to the bottom, by a windshield 5, a body member 6, a front bumper 7, and a fixed lower anti-run over band 8. These elements are shaped so as to form a laterally tapered front prolongation 9 of the cabin, as it can be assumed from the shape of the lower band 8 shown in figure 5.

The body member 6, the bumper 7 and the lower band 8 are manufactured so as to be yielding, in a known manner not forming part of the subject-matter of the invention, in order to increase passive safety in case of collision against a vulnerable road user.

According to the invention, the vehicle 1 comprises an anti-run over safety device 10 (hereinafter simply referred to as the "the device 10"), which is shown in figures 3 to 11.

The device 10 comprises one or more bulkheads, collectively indicated with numeral 14, in the example described herein a central bulkhead 14a and a pair of lateral bulkheads 14b, which are constrained to the lower band 8 and are movable between a raised running position, in which they substantially do not limit the ramp angle α of the vehicle, and a lowered activated position (figures 1, 2 and 4), in which the project below the lower band 8 so as to reduce the free front space below the cabin front.

By so doing, the risk that a vulnerable user, following a collision, can be run over by the front wheels 4 of the

vehicle is eliminated.

The central bulkhead 14a (figure 5) is hinged to an intermediate portion 8a of the lower band 8, which is substantially transverse to a longitudinal axis of the vehicle; the lateral bulkheads 14b are hinged to respective lateral portions 8b of the lower band 8 bent backwards starting from the central portion 8a.

The hinge constraint between the bulkheads 14a, 14b and the lower band 8 is obtained by means of respective axes 15a, 15b, which are supported in a rotary manner in a horizontal position close to an inner side of the respective portions 8a, 8b of the lower band 8 within respective supports 16a, 16b secured to the lower band 8. In particular, there are three supports 16a for the axis 15a of the central bulkhead 14a and two supports 16b for the lateral bulkheads 14b.

The bulkheads 14a, 14b (figures 5, 6) are rigidly connected to the respective axes 15a, 15b, so as to rotate with them by means of respective appendages 17a, 17b, which are integral to the bulkheads, are as many as the supports 16a, 16b and are secured to the respective axes 15a, 15b in the area of the supports.

The bulkheads 14 are subjected to an elastic force that tends to rotate them downward. This elastic force is generated, for example, by means of helical torsion springs

19a, 19b, which are wound around the axes 15a, 15b and have respective portions that are constrained to the lower band 8 and to an appendage 17a, 17b of the respective bulkhead 14.

5 The bulkheads 14 can be blocked in the raised running position by means of respective blocking mechanisms 20, which are associated with one of the supports 16a, 16b of each bulkhead.

10 Figures 6, 8 and 9 show the blocking mechanism 20 of the central bulkhead 14a; similar mechanisms, which are not shown herein, are provided for the lateral bulkheads 14.

15 As it can be clearly seen in the aforesaid figures, the central appendage 17a of the central bulkhead 14a, in its rotation movement, slides on a vertical plane P between two brackets 21, which are spaced apart from one another and form, as a whole, the central support 16a. The blocking mechanism 20 comprises two cams 22, which are hinged to the respective brackets 21 around respective horizontal axes B, B', which are parallel to one another and symmetrical
20 relative to the plane P.

25 The cams 22 are provided with respective pairs of projections 23, 24 with a substantially triangular shape, which are arranged above and below the axes B, B', respectively. As it can be seen in figure 8, in the blocking position the cams 22 are rotated so that the upper

projections 23 are close to one another and block the appendage 17a, thus preventing the bulkhead 14a from moving downward.

The cams 22 are controlled, by means of respective Bowden
5 cables 38, by an actuator 39, for example a single-acting
pneumatic cylinder, conveniently carried by a cross-member
35 fixed to the frame 2 of the vehicle (figure 5).

The actuator 39 (figure 7) is operated, by means of a
solenoid valve 49, by a control unit 41 of the vehicle, which
10 detects an impact condition in a known manner based on signal
Si received from on-board sensors that are not shown.

In response to an activation signal sent by the control
unit 41 to the solenoid valve 41, the actuator 39 controls
the rotation of the cams 22 so as to move the projections 23
15 away from one another and move the projections 24 close to
one another. In the position in which the distance between
the vertices of the projections 23 is equal to the one
between the projections 24, this distance is slightly greater
than the thickness of the appendage 17a, which, therefore,
20 is free to move between the cams 22, thus allowing the
bulkhead 14a to move downward towards the activated position
shown.

Figure 9 shows the position of the cams 22 at the end of
the downward movement of the bulkhead 14a: the cams 22 are
25 rotated so as to move the projections 24 close to one another

in order to block the appendage 17a in the lowered position.

As you can see in figure 5, in the running position the lateral bulkheads 14b partially overlap the central bulkhead 14a and they are also normally blocked in the raised position
5 by the respective blocking mechanisms 20, which are controlled by the same actuator 39.

After the detection of an impact condition, and similarly to what described above for the central bulkhead 14a, the lateral bulkheads 14b are also controlled by the actuator 39
10 so as to move to the lowered position.

Figures 5, 10 and 11 schematically show a mechanism 25 for resetting the device 10 after a collision.

The mechanism 25 (figures 5 and 10) comprises a lever 26 having a lower end 27 hinged to an end of the axis 15a and
15 an upper end where a handgrip 28 is obtained. Furthermore, the lever 26 is constrained to an intermediate support 29, which is carried by the cross-member 37 (figure 5). The intermediate support 29 is conveniently provided with a slot 30 engaged by a pin 31 integral to the lever 26, so as to
20 permit a limited rotation of the lever.

The lower end 27 of the lever 30 can be selectively coupled to the axis 15a by means of a known unidirectional pawl joint 32, which is schematically shown in figure 10. The joint 32, when deactivated, allows the axis 15a to freely
25 rotate relative to the lever 30; when it is active, the joint

32 causes the axis 15a to be integral to the lever 30 in the rotation direction corresponding to the raising of the bulkhead 14a from the lowered position to the raised position.

5 The unidirectional joint 32 is normally deactivated by means of elastic means, which are not shown, and it can be activated through an auxiliary lever 33 arranged on the handgrip 28 of the lever 26 by means of a Bowden cable 34.

10 The reset mechanism 25 comprises, furthermore, a non-return device 35, which is schematically shown in figure 11 in the form of a ratchet means, which selectively constrains an opposite end of the axis 15a to the relative support 16a. The reset device 35, when it is deactivated, allows the axis 14a to freely move in both directions; when it is active, it
15 prevents the axis 15a from rotating in the direction corresponding to the downward movement of the bulkhead 14a.

20 The non-return device 35 is normally deactivated by means of elastic means, which are not shown, and it can be activated through the auxiliary lever 33 by means of a further Bowden cable 36.

 The lever 33 is further adapted to operate a microswitch 42 adapted to send to the control unit 31 a reset consent signal when the lever 33 is pressed.

25 The operation of the device 10, which is already partly evident from the description above, is the following.

In a running condition, the bulkheads 14a, 14b are blocked in the raised running position by the blocking mechanisms 20. Therefore, the space between the lower band 8 and the ground is such as to ensure an adequate ramp angle.

5 In case of collision, the cams 22 are "opened" by the actuator, thus allowing the bulkheads 14a, 14b to rotate towards the lowered position due to the thrust of the relative springs 19a, 19b. The cams 22, after having reached the position of figure 9, block the bulkheads 14a, 14b in
10 the lowered position.

By so doing there is no risk of running over a vulnerable user.

The rotation of the central bulkhead 14a towards the activated position is possible because the axis 15a is
15 decoupled from the lever 30 by means of the unidirectional joint 32 and from the support 16a by means of the non-return device 35.

After a collision, the bulkheads 14 are in lowered position. In order to move them back to the raised running
20 position, you need to act upon the lever 30, which is accessible by lifting the body member 6, which is conveniently manufactured so as to be folded upwards.

In particular, by acting upon the auxiliary lever 32 you generate, by means of the microswitch 42, the reset consent
25 signal, in response to which the control unit 41 controls

the actuator 39 so as to move the cams 22 back to the position of figure 8.

By keeping the auxiliary lever 33 pressed, you can engage both the unidirectional joint 32 and the non-return device
5 35.

In this way, by means of the lever 30, the axis 15a can be rotated by the angle needed to move the bulkhead 14a from the lowered position to the raised position (for example by 70°) with an alternative movement of the lever with a reduced
10 amplitude (equal to the angle subtended by the slot 36). With every travel of the lever 30 towards the vehicle front, the bulkhead 14a rotates upwards by a corresponding angle, whereas during the return travels of the lever 30 towards the inside of the cabin the unidirectional joint 32 does not
15 transmit the motion. During return travels, when the lever 30 is idle relative to the axis 15a, the latter is blocked by the non-return device 35, thus preventing the bulkhead 14a from moving downward.

Given the partially overlapped position of the lateral
20 bulkheads 14b relative to the central bulkhead 14a, the latter drags the two lateral bulkheads 14b upward during the reset operation.

During the reset step, the appendages 17a, 17b are forcedly wedged in between the cams 22 of the respective
25 blocking mechanisms 20, thus spreading the projections 23

against the elastic force exerted by the actuator 39 by means of the Bowden cables 38. Once the appendages 17a, 17b have moved upward past the cams 22, the latter close elastically, thus blocking the bulkheads 14a, 14b.

5 Finally, the device 10 described herein can be subjected to changes and variants, which do not go beyond the scope of protection set forth in the appended claims.

 In particular, the number and arrangement of the bulkheads as well as the way in which they are constrained
10 can change. Furthermore, the control of the bulkheads towards the activated position can be carried out in a different way.

 The reset mechanism 25 can be manufactured differently; in particular, the unidirectional joint 32 and the non-return
15 device 35 can be replaced by different elements.

 The controls through Bowden cables can be replaced by different transmission devices or by electric controls; the actuator 39 can be electric instead of pneumatic.

CLAIMS

1.- Anti-run over safety device for an industrial vehicle

(1) comprising:

a support member (8) adapted to be secured to a front area
5 of the vehicle (1);

at least one bulkhead (14a, 14b) constrained to the support
member (8) and movable between a raised running position and
a lowered activated position in which said bulkhead (14a)
cantilevers downward to reduce the free frontal space below
10 the vehicle (1); and

means (10) for activating the bulkhead (14a, 14b) in response
to a signal (Si) indicating an impact.

2. A device as claimed in claim 1, characterized in that
the bulkhead (14a, 14b) is hinged to the support member (8).

15 3. A device as claimed in claim 1 or 2, characterized by
comprising a plurality of simultaneously activatable
bulkheads (14a, 14b).

4. A device as claimed in claims 2 or 3, characterized
in that the support member is a lower cross-member (8)
20 located in the vicinity of a front bumper (7) of the vehicle
(1) and comprising a central portion (8a) and a pair of
lateral portions (8b) bent backwards starting from the
central portion (8a), said device (10) comprising a central
bulkhead (14a) constrained to the central portion (8a) of
25 the lower cross-member (8) and a pair of side bulkheads (8b)

constrained to the lateral portions (8b) of said lower cross-member.

5 5. A device as claimed in claim 4, characterized in that the side bulkheads (14b) are partially overlapping the central bulkhead (14a) in said running position.

6. A device as claimed in any of the preceding claims, characterized in that said means (10) for activating the at least one bulkhead (14a, 14b) includes elastic means (19) biasing the bulkhead (14a, 14b) towards the activated
10 position and a blocking mechanism (20) for maintaining the bulkhead (14a, 14b) in the running position against the action of said elastic means (19), said blocking mechanism (20) being releasable in response to said signal (Si) indicating an impact.

15 7. Device as claimed in claim 6, characterized in that said elastic means (19) include at least one torsion spring (19a, 19b) wound around a hinge axis (15a, 15b) of said bulkhead (14a, 14b).

8. Device as claimed in claim 6 or 7, characterized in
20 that said blocking mechanism (20) includes cam means (22) cooperating with a portion (17a, 17b) integral with said bulkhead (14a, 14b).

9. Device as claimed in claim 8, characterized in that said cam means (22) are movable between a first position in
25 which said cam means (22) block said bulkhead (14a, 14b) in

the running position and a second position in which said cam means (22) block said bulkhead (14a, 14b) in the activated position.

10. Device as claimed in claim 9, characterized in that
5 said cam means includes a pair of cams (22) facing one another and symmetrically set with respect to a plane of motion (P) of said portion (17a), said cams (22) including first cam profile (23) configured to cooperate with said portion (17a) in said first position and second cam profiles
10 (24) configured to cooperate with said portion (17a) in said second position.

11. Device as claimed in any of claims 6 to 10, characterized in that said blocking mechanism (20) includes an actuator actuating said cam means (22) in response to
15 said signal.

12. Device as claimed in claim 11, characterized by including a reset mechanism (25) for resetting said safety device (9).

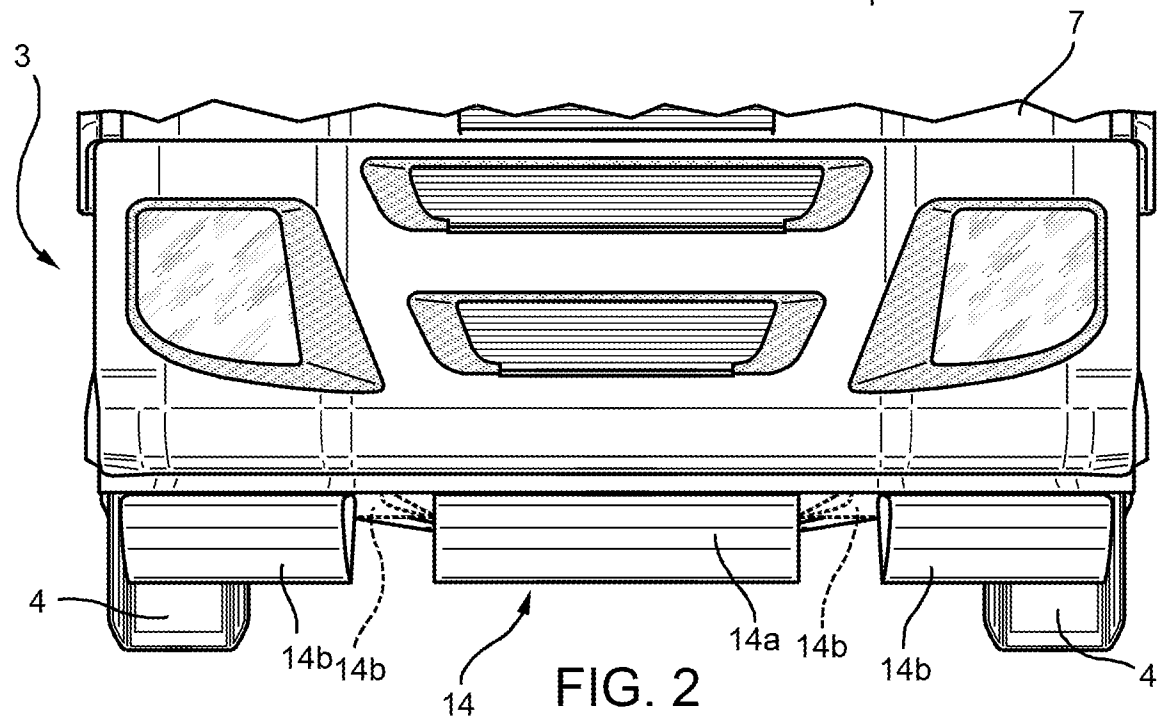
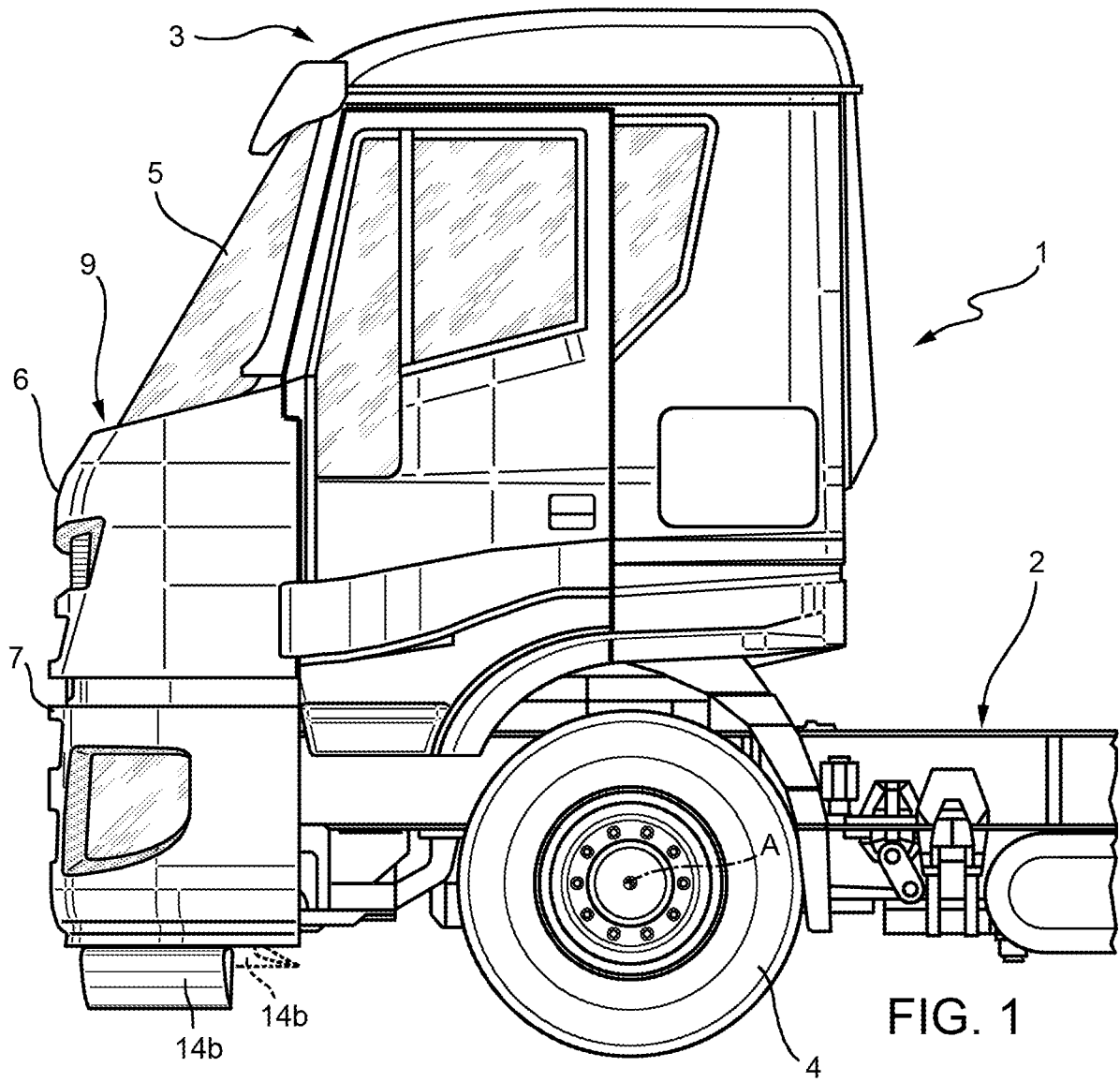
13. Device as claimed in claim 12, characterized in that
20 said reset device (25) includes a lever (26) for rotating said hinge axis (15a) so as to displace said at least one bulkhead (14a, 14b) from said activated position to said running position.

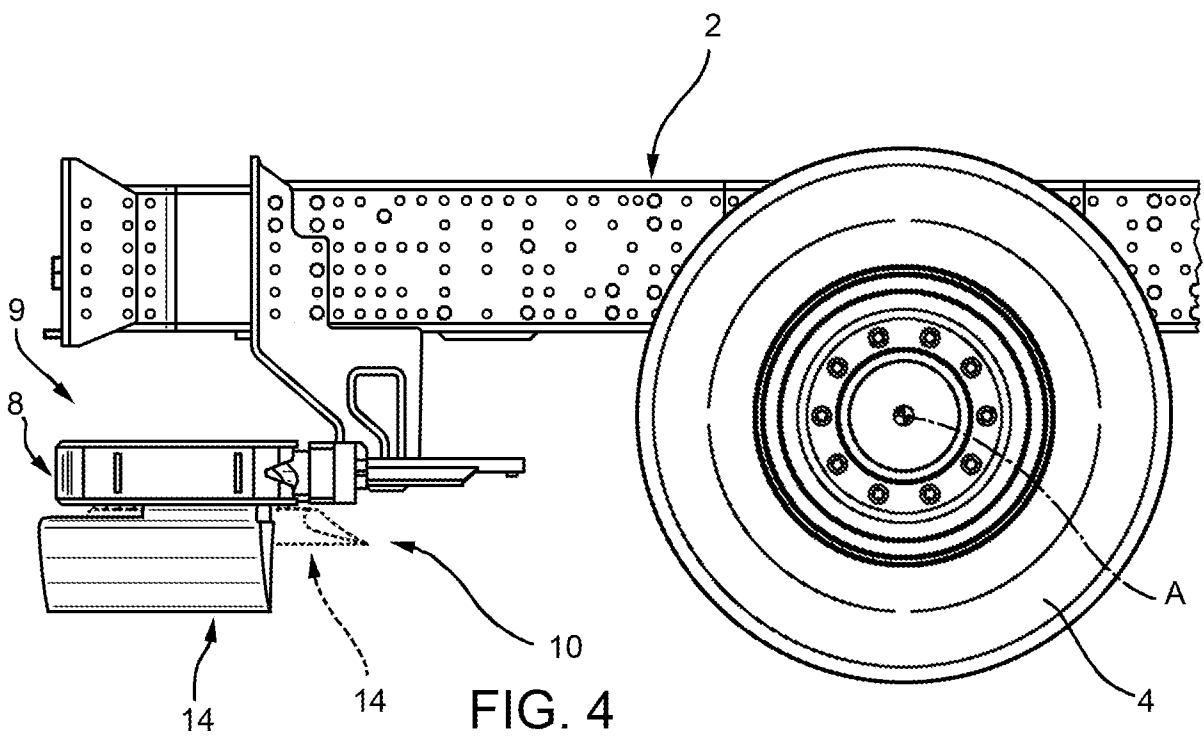
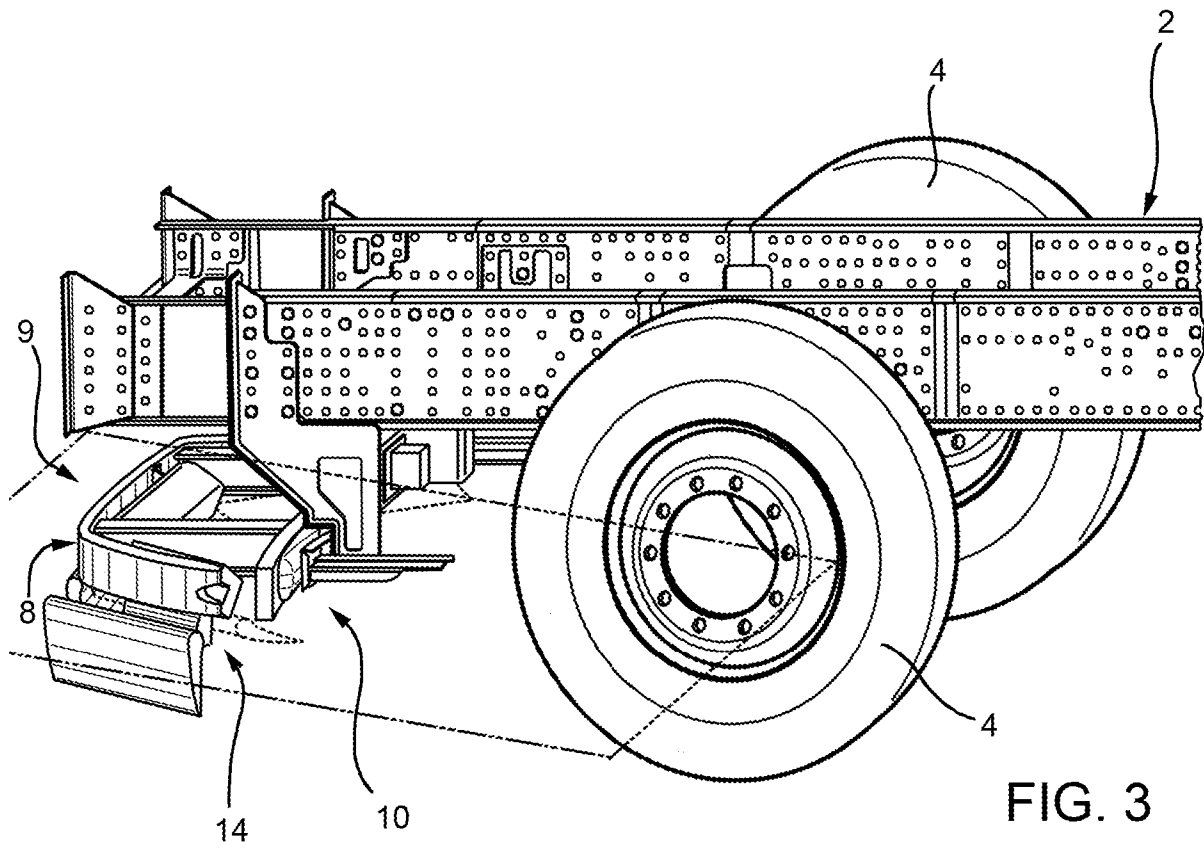
14. Device as claimed in claim 13, characterized in that
25 said lever (26) includes means (33, 42) for manually

controlling said blocking mechanism (20) to displace said
cams (22) from said second position to said first position.

15. Device as claimed in claim 13 or 14, characterized
in that said reset mechanism (25) includes a unidirectional
5 joint (32) to selectively connect said lever (26) to said
hinge axis (15a) of said bulkhead (14a).

16. Device as claimed in one of claims 13 to 15,
characterized in that said reset mechanism (25) includes a
non-return device (35) configured to block said hinge axis
10 (15a) unidirectionally during reset of said bulkhead (14a).





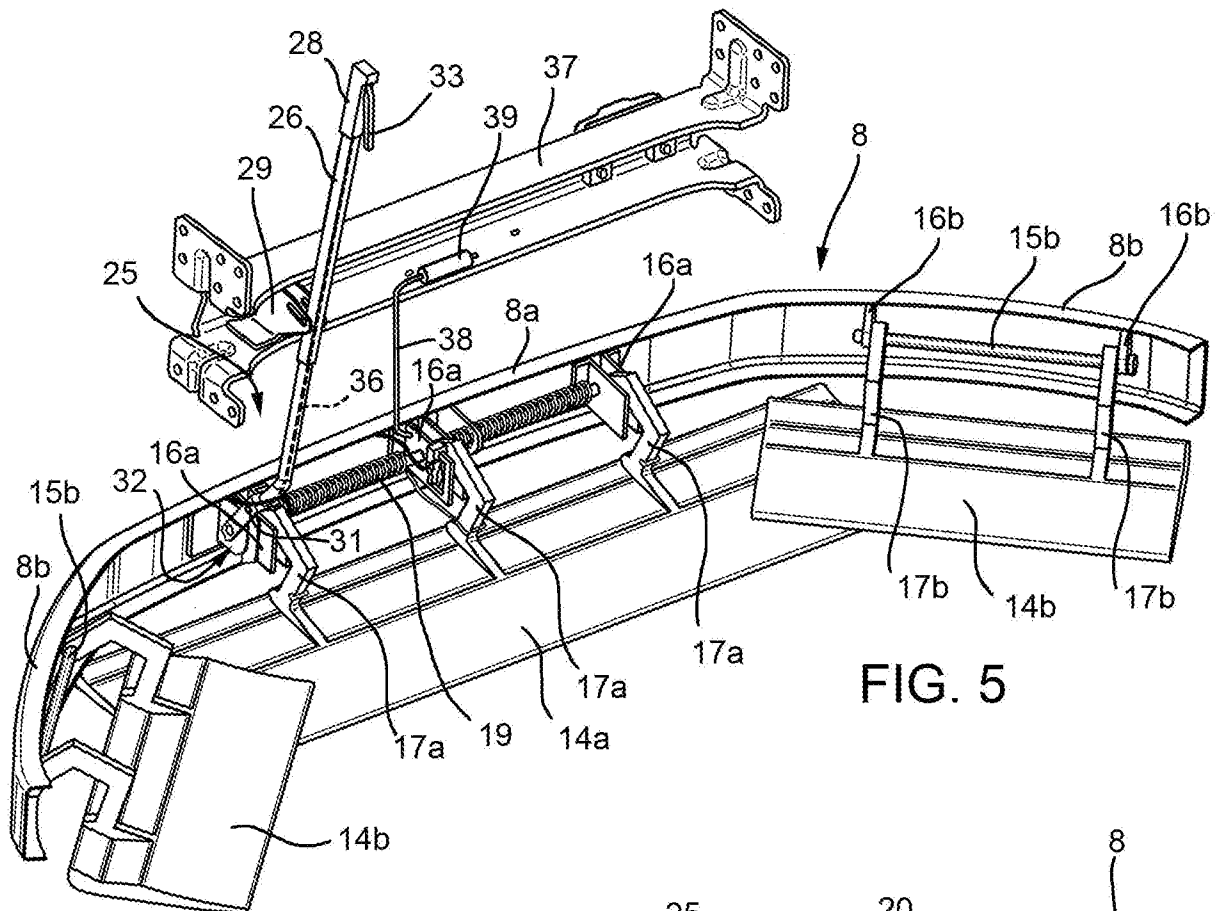


FIG. 5

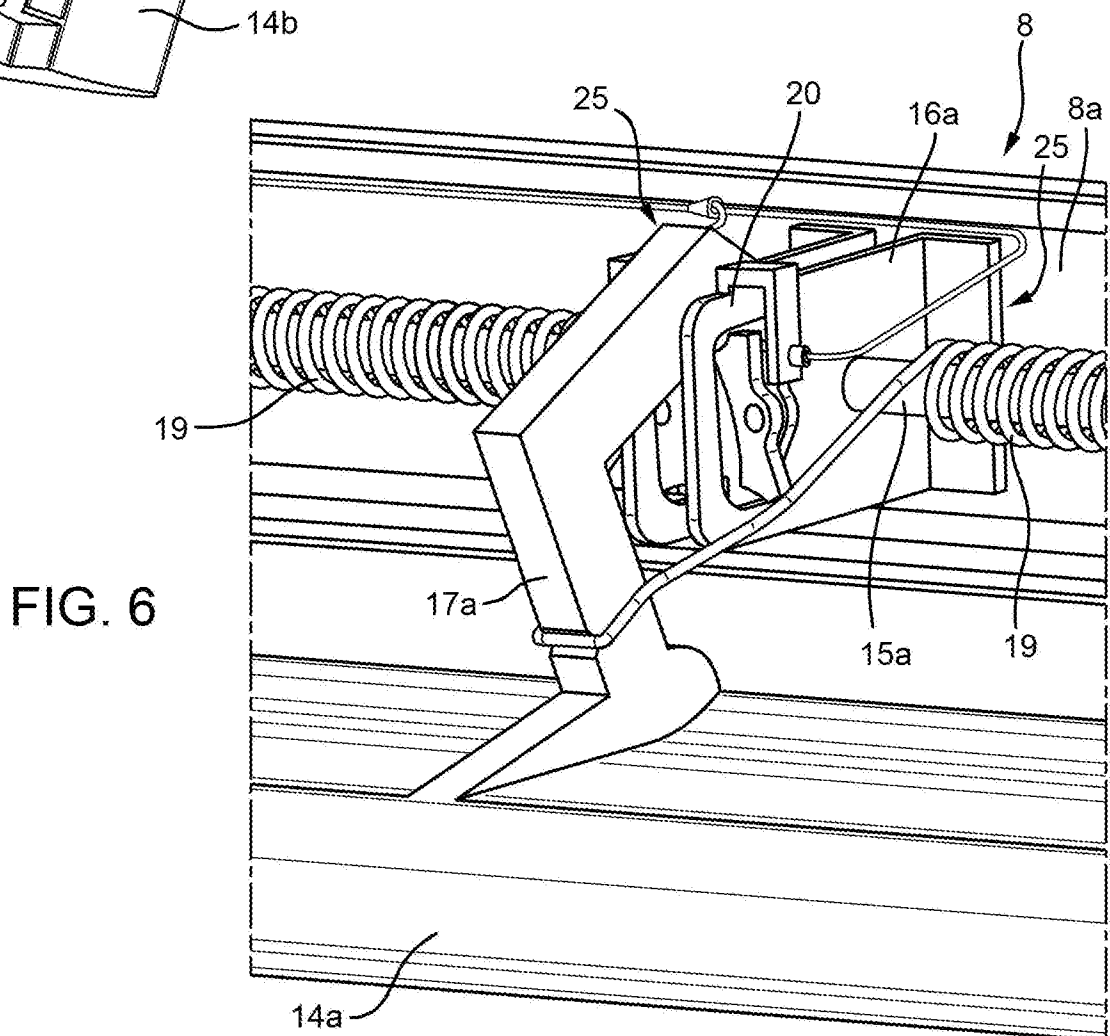


FIG. 6

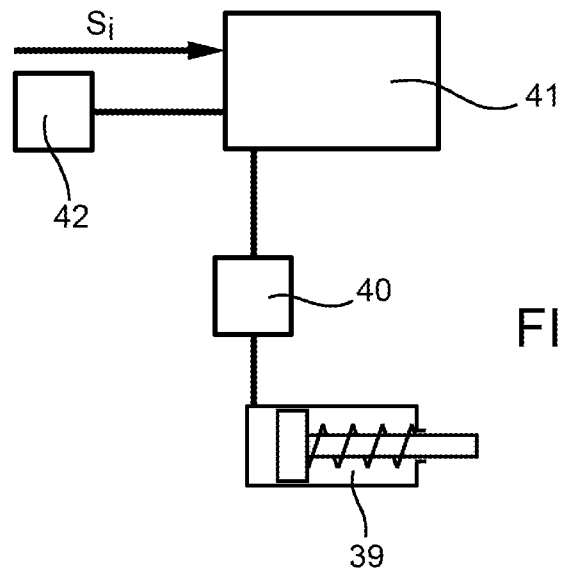


FIG. 7

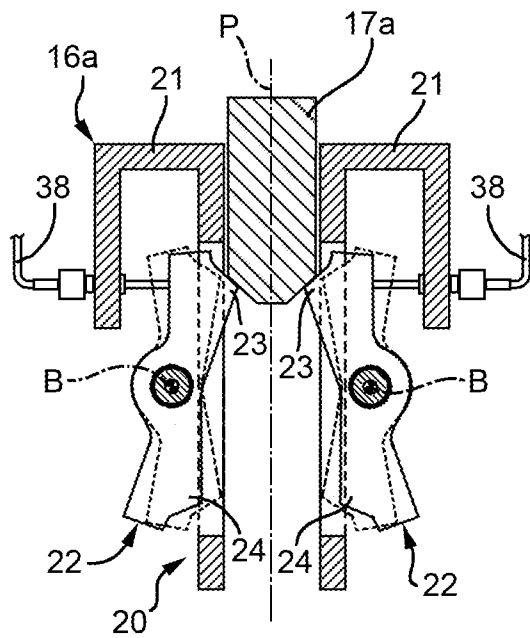


FIG. 8

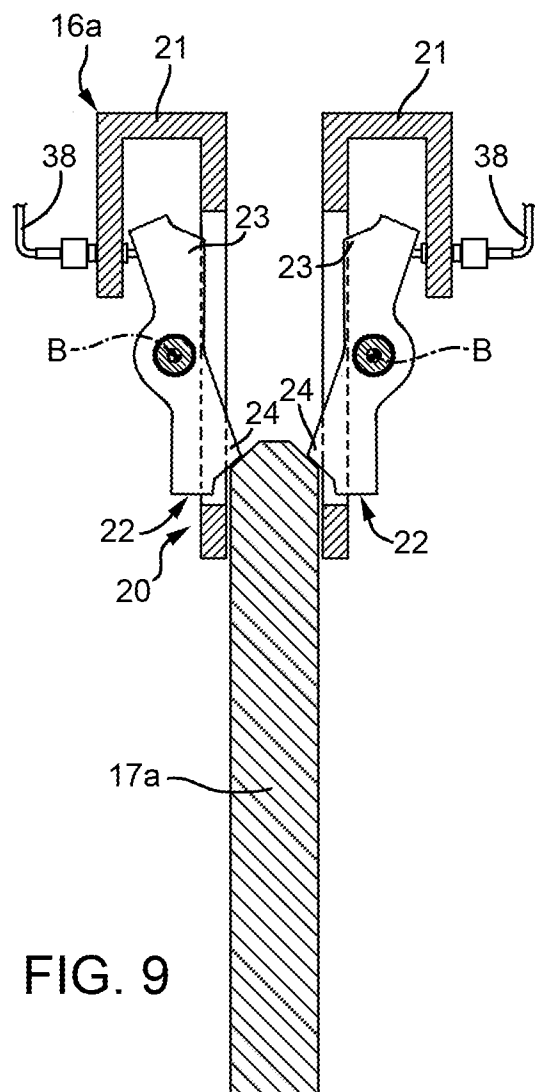


FIG. 9

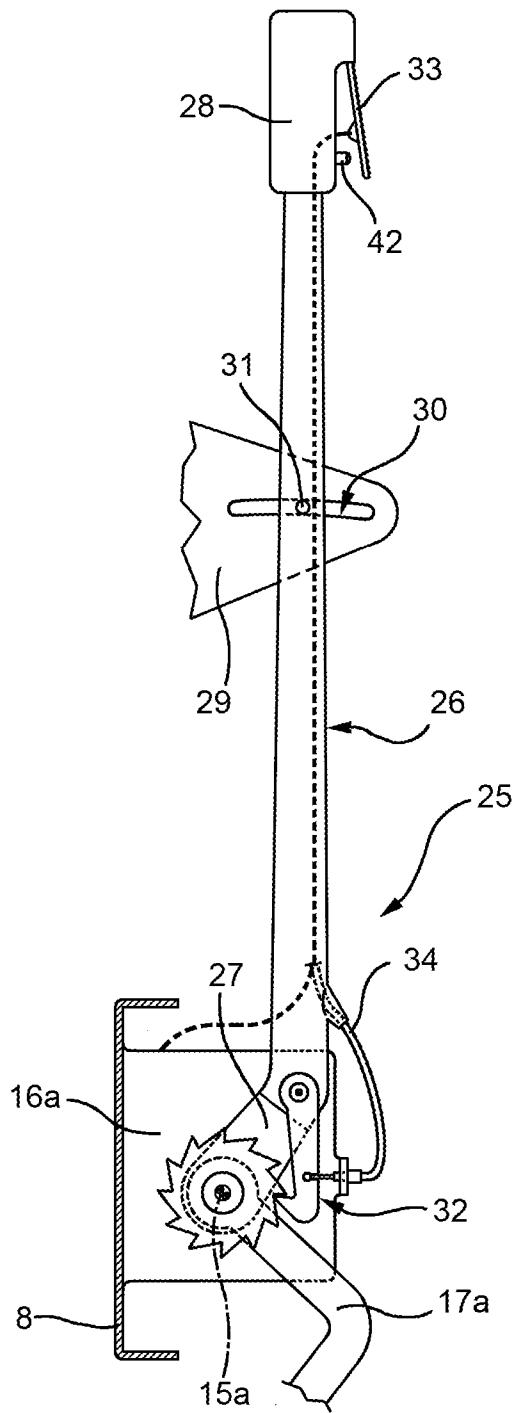


FIG. 10

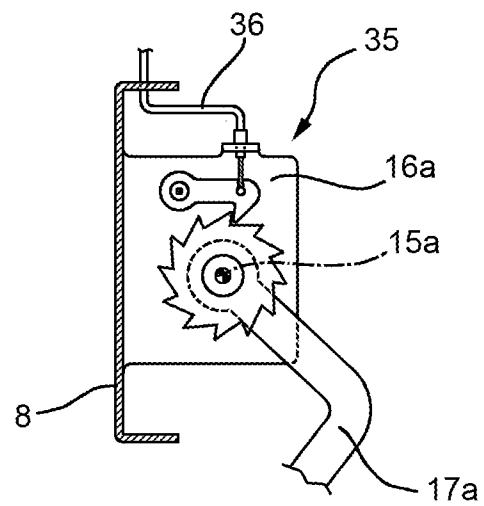


FIG. 11

INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2017/052608

A. CLASSIFICATION OF SUBJECT MATTER
INV. B60R19/56 B60R21/34
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
B60R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

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X	US 4 688 824 A (HERRING JOHN D [US]) 25 August 1987 (1987-08-25) claims 1-6; figures 3-9	1-16
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Further documents are listed in the continuation of Box C.



See patent family annex.

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Date of the actual completion of the international search

25 August 2017

Date of mailing of the international search report

06/09/2017

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040,
Fax: (+31-70) 340-3016

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Topolski, Jan

INTERNATIONAL SEARCH REPORT

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C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
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Information on patent family members

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