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(54) **IMPEDANCE BLOCKING FILTER CIRCUIT**  
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(74) *Attorney, Agent, or Firm*—Gazdzinski & Associates  
(57) **ABSTRACT**

**Related U.S. Patent Documents**

Reissue of:  
(64) Patent No.: **6,181,777**  
Issued: **Jan. 30, 2001**  
Appl. No.: **09/370,137**  
Filed: **Aug. 9, 1999**

**U.S. Applications:**

(63) Continuation-in-part of application No. 09/195,522, filed on Nov. 19, 1998, now Pat. No. 6,188,750.

(51) **Int. Cl.**  
**H04M 1/24** (2006.01)  
**H04M 1/00** (2006.01)  
**H04M 9/00** (2006.01)  
**H04M 11/00** (2006.01)

(52) **U.S. Cl.** ..... **379/32.04**; 379/1.01; 379/8; 379/30; 379/168; 379/377

(58) **Field of Classification Search** ..... 379/1.01, 379/8, 30, 90.01, 93.01, 93.05, 93.09, 168, 379/377, 387.01, 390.02, 391–392, 394, 379/397, 399.01, 413.02, 413.04, 398, 414  
See application file for complete search history.

(56) **References Cited**

**U.S. PATENT DOCUMENTS**

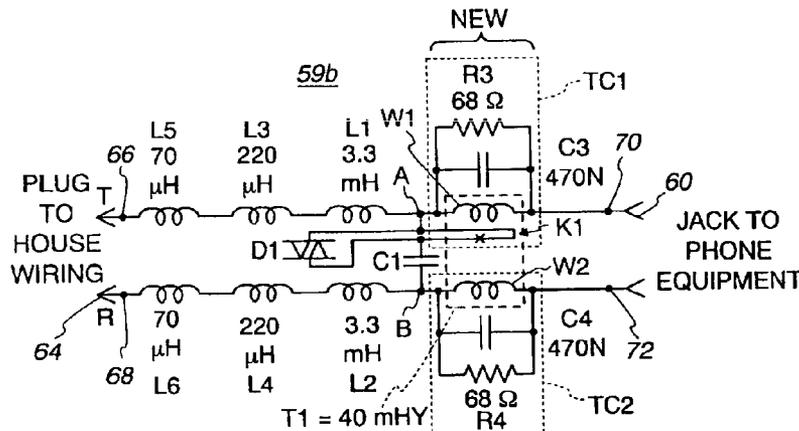
4,613,732 A \* 9/1986 Cwirzen et al.  
4,667,173 A \* 5/1987 Okochi ..... 333/177  
4,742,541 A \* 5/1988 Cwirzen et al. .... 379/412

(Continued)

*Primary Examiner*—Binh K. Tieu

[An impedance blocking filter circuit is provided for use in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances above 20 KHz due to the customer's terminal equipment from an ADSL network unit and/or home networking interface unit. The filter circuit includes first, second, and third inductors connected in series between a first input terminal and a first common point. A first resistor has its one end connected also to the first common point and its other end connected to a first output terminal. Fourth, fifth and sixth inductors are connected in series between a second input terminal and a second common point. A second resistor has its one end also connected to the second common point and its other end connected to a second output terminal. A capacitor has its ends connected across the first and second common points. In other aspects, the filter circuit also includes switching means for eliminating shunt additive capacitance and/or correction circuit means reducing significantly return loss.]  
*An impedance blocking filter circuit is provided for use in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to block impedances above a desired frequency range due to the customer's terminal equipment from a DSL network unit and/or home networking interface unit. In one exemplary embodiment, the filter circuit includes first, second, and third inductors connected in series between a first input terminal and a first common point. A first resistor has its one end connected also to the first common point and its other end connected to a first output terminal. Fourth, fifth and sixth inductors are connected in series between a second input terminal and a second common point. A second resistor has its one end also connected to the second common point and its other end connected to a second output terminal. A capacitor has its ends connected across the first and second common points. In other configurations, the filter circuit also includes switching means for eliminating shunt additive capacitance and/or correction circuit means reducing significantly return loss.*

**41 Claims, 6 Drawing Sheets**





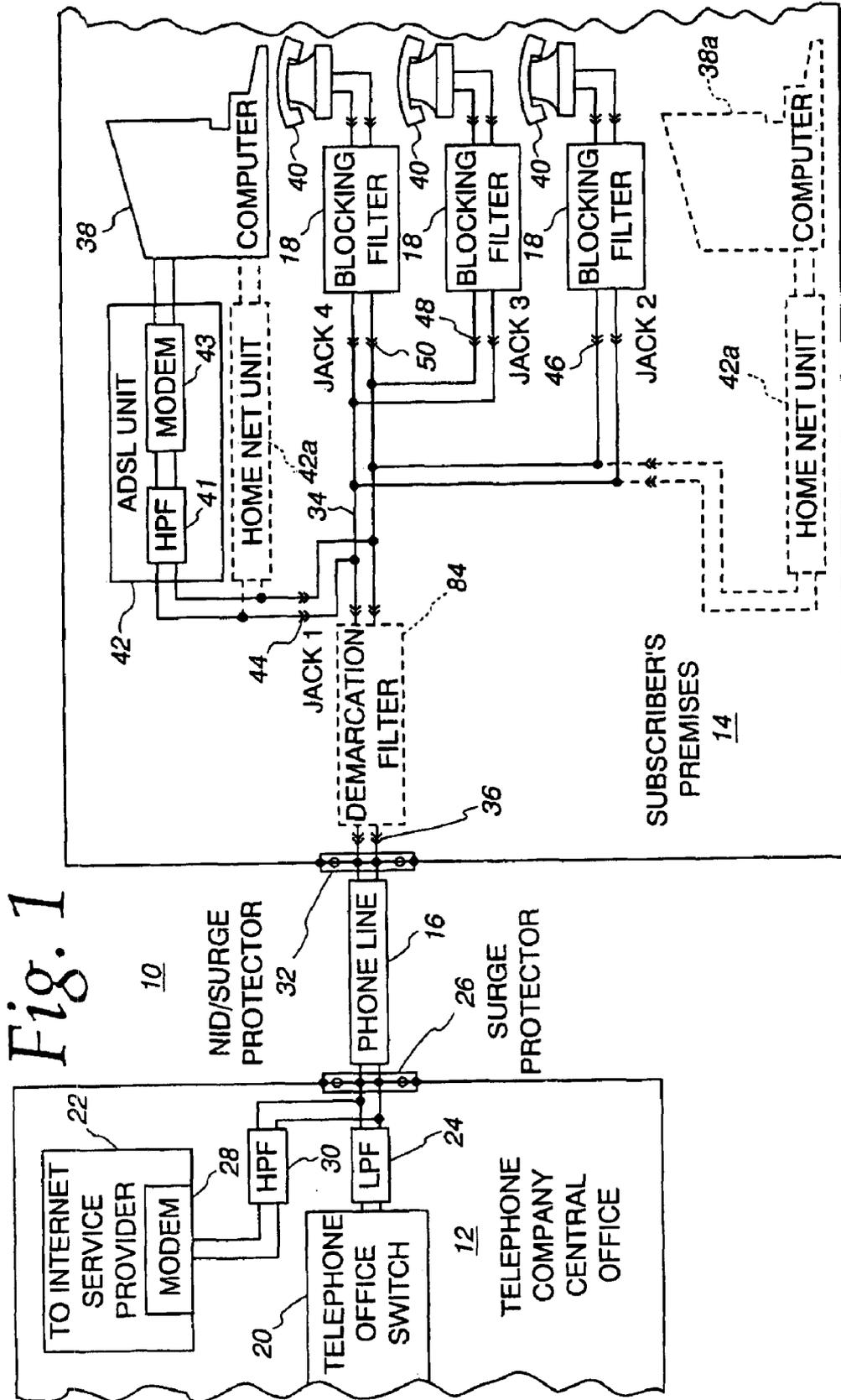


Fig. 1

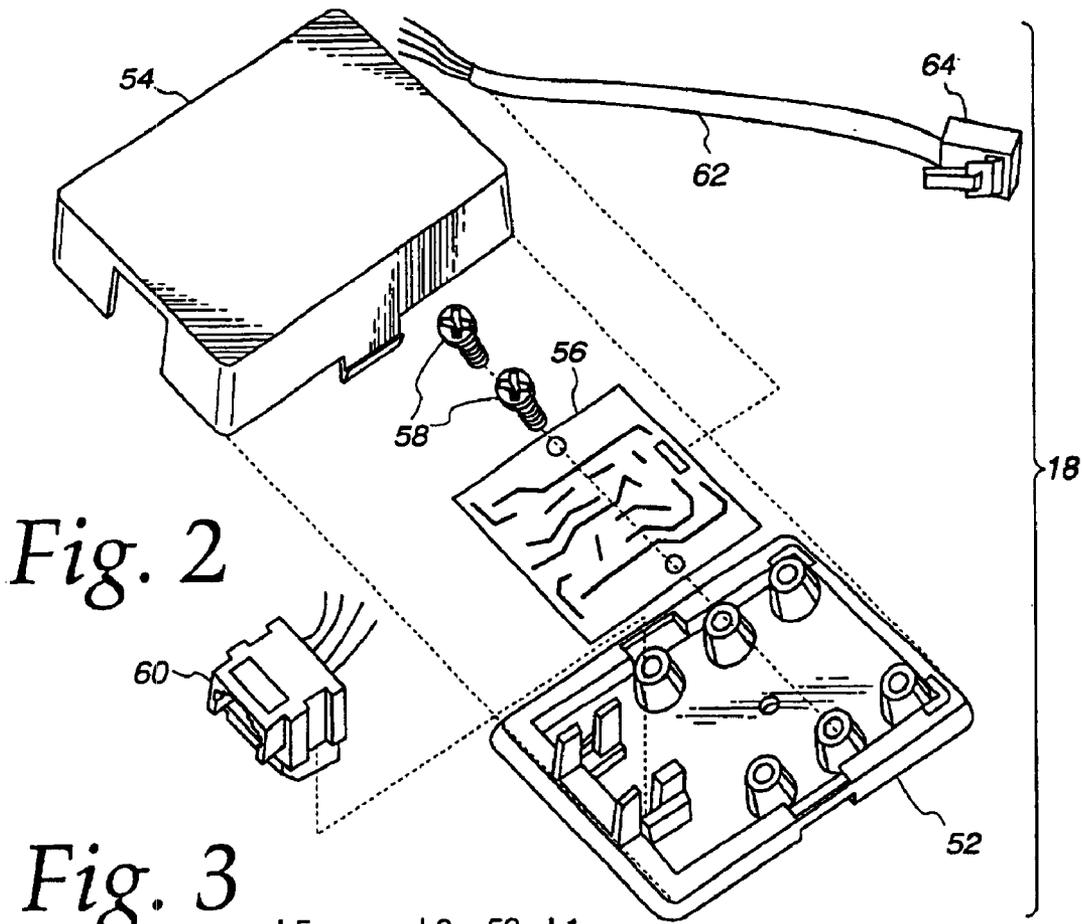


Fig. 2

Fig. 3

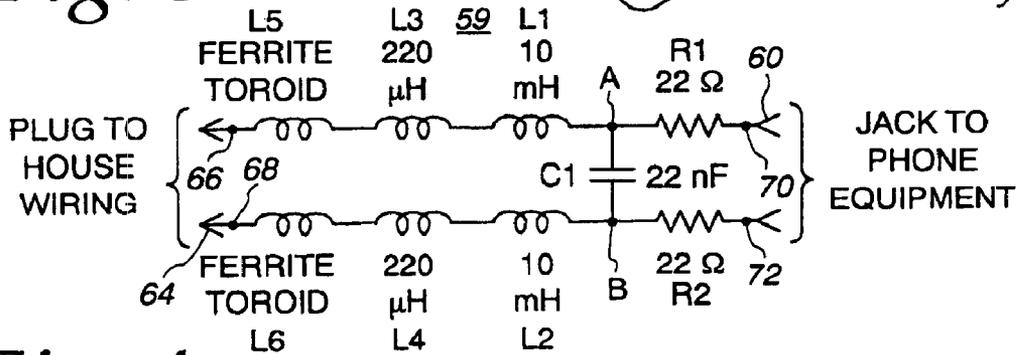


Fig. 4

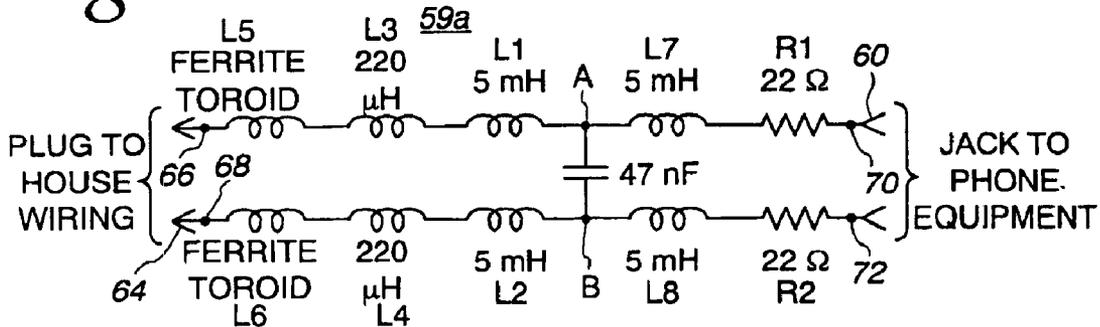


Fig. 5

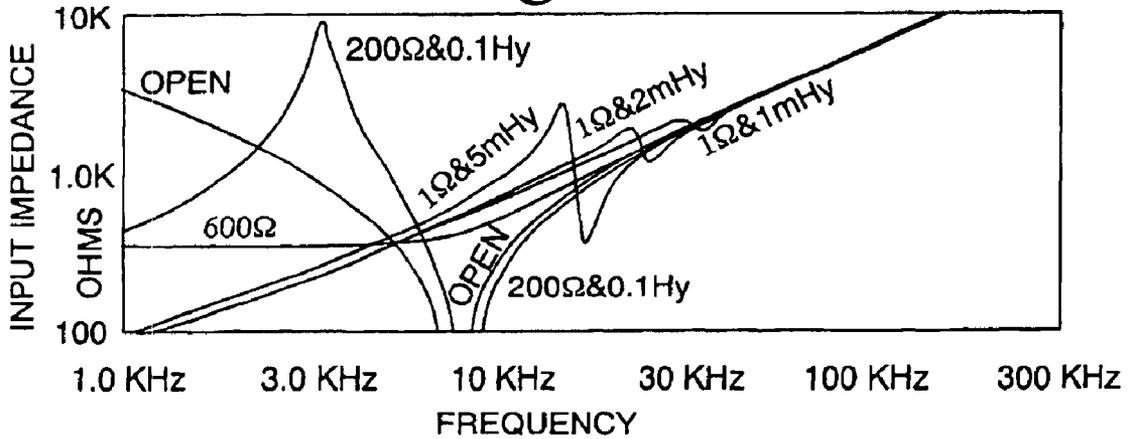


Fig. 6

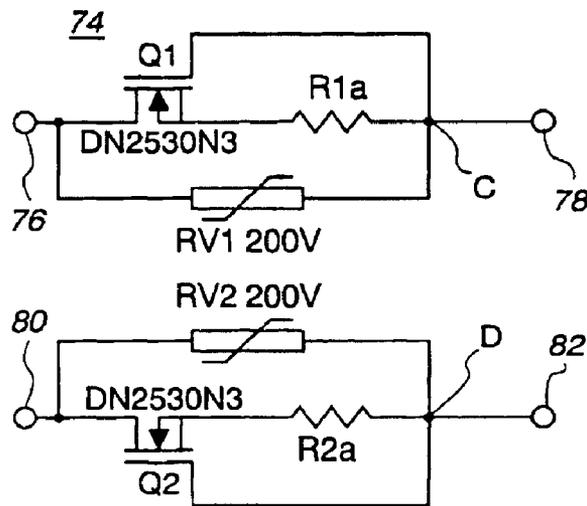
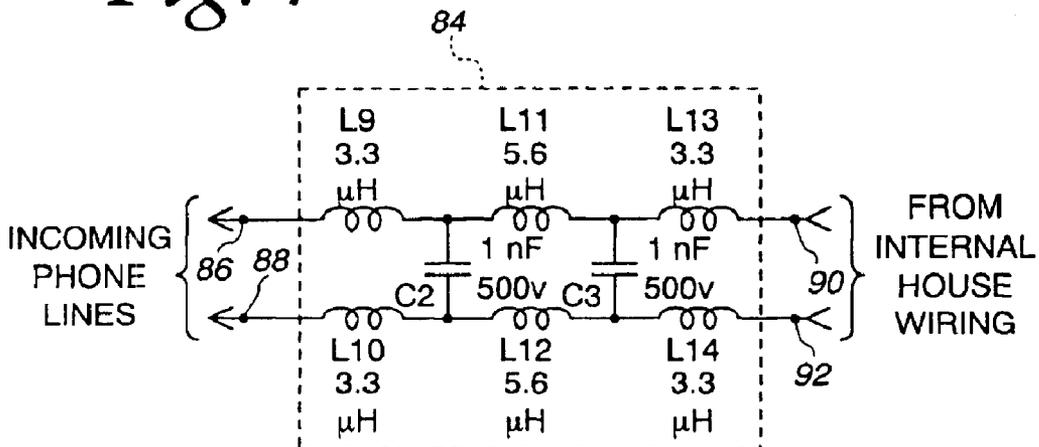
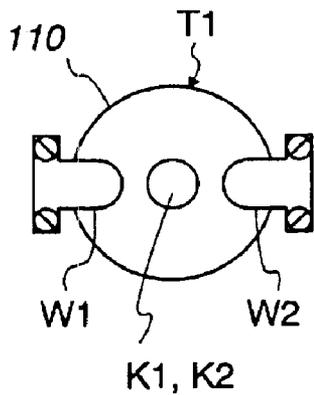


Fig. 7

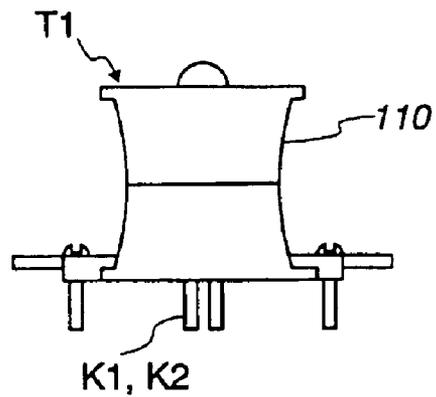




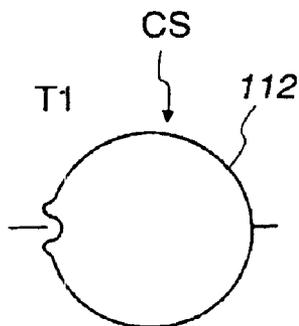
*Fig. 10(a)*



*Fig. 10(b)*



*Fig. 11(a)*



*Fig. 11(b)*

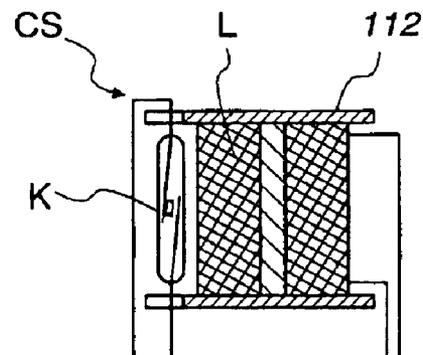


Fig. 12

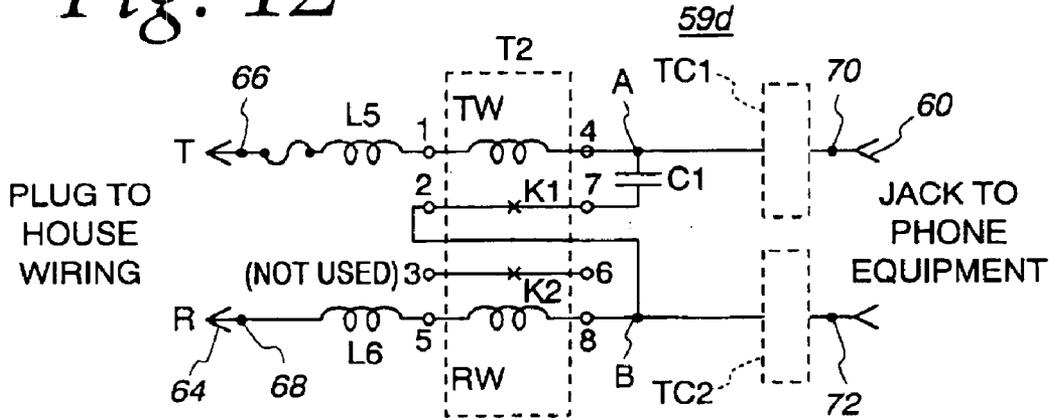


Fig. 13

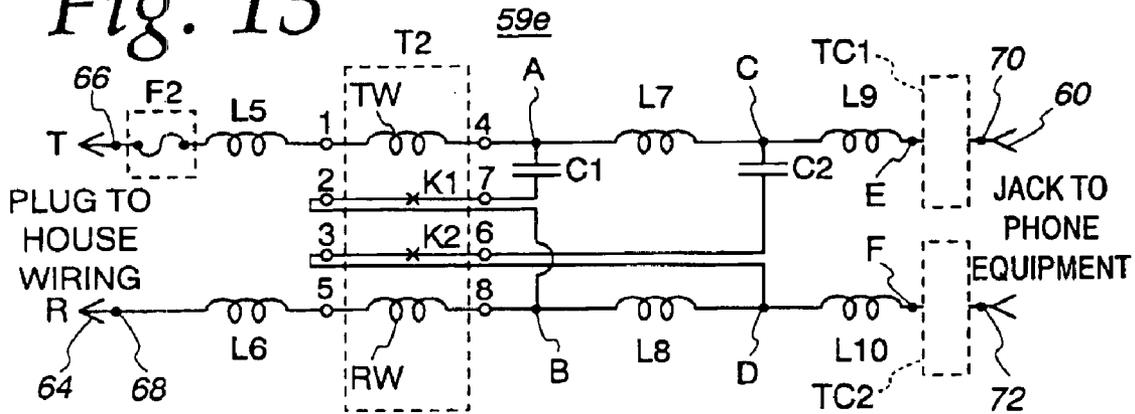


Fig. 14(a)

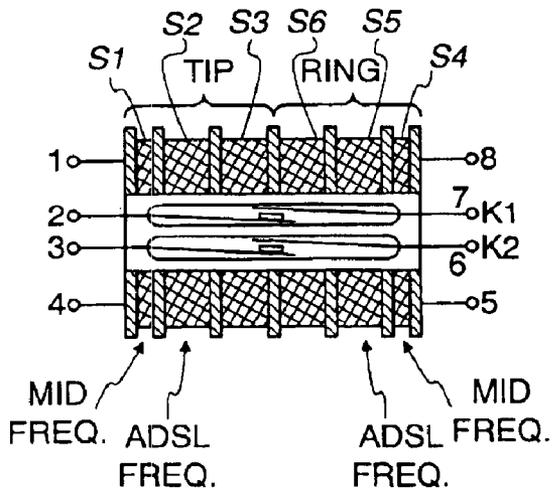
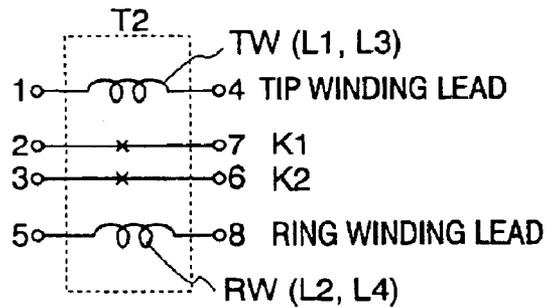


Fig. 14(b)



## IMPEDANCE BLOCKING FILTER CIRCUIT

**Matter enclosed in heavy brackets [ ] appears in the original patent but forms no part of this reissue specification; matter printed in italics indicates the additions made by reissue.**

### CROSS-REFERENCE TO RELATED APPLICATIONS

[The present invention is a continuation-in-part application based on prior application Ser. No. 09/195,222 filed on Nov. 19, 1998, and entitled "Impedance Blocking Filter Circuit."] *The present application is a reissue of U.S. Pat. No. 6,181,777 issued Jan. 30, 2001 of the same title, which is a continuation-in-part of application Ser. No. 09/195,522, now U.S. Pat. No. 6,188,750. This application is also related to co-pending reissue application Ser. Nos. 10/737,736 filed Dec. 12, 2003, 10/366,656 filed Feb. 12, 2003, 10/408,030 filed Apr. 3, 2003, and 10/748,729 filed Dec. 29, 2003, all of the same title.*

### BACKGROUND OF THE INVENTION

#### 1. Field of the Invention

This invention relates generally to telecommunication systems and more particularly, it relates to an impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines from a telephone company's central office (C.O.) and subscriber or customer telephone equipment such as a telephone set located at a subscriber's premises so as to unconditionally block telephone impedance above 20 KHz.

#### 2. Description of the Prior Art

The prior art appears to be best exemplified in the following U.S. Letters Patent which were developed in a search directed to the subject matter in this application:

4,613,732	4,823,383
4,742,541	5,642,416
4,743,999	5,802,170

In U.S. Pat. No. 4,823,383 issued to Cardot et al. on Apr. 18, 1989, there is disclosed a protection device for terminal equipment on telephone subscriber premises which includes a voltage surge protection circuit and/or a filter for providing protection against radio frequencies and interference. The filter is comprised of series inductors L1, L2, L3 and L5 interconnected between terminals E1 and S1 and series inductors L'1, L'2, L'4 and L'5 interconnected between terminals E2 and S2. A capacitor C5 is connected between the junction of the inductors L2, L3 and the inductors L'2, L'4. The surge protection circuit includes thermistors TH1, TH2 and voltage limiters D1-D3.

In U.S. Pat. No. 5,802,170 issued to Smith et al. on Sep. 1, 1998, there is disclosed a customer bridge module for connecting telephone company wiring and subscriber telephone wiring in a telephone network interface apparatus. In one embodiment, the customer bridge module includes overcurrent protection and an RFI filter. The overcurrent protection is formed by positive temperature coefficient resistors 220, 222 and inductors. The RFI filter is formed by inductors 224a-224c, 226a-226c and capacitors 236a-236c. The inductors and capacitors are used to form a multi-pole low pass filter.

In U.S. Pat. No. 5,642,416 issued to Hill et al. on Jun. 24, 1997, there is disclosed an electromagnetic interference

by-pass filter which suppresses RF noise currents conducted over the tip and ring leads of a telephone line-powered instrument. The filter includes first and second inductors 51, 53 and first and second capacitors 41, 43.

It is generally well-known these days that many telephone subscribers or customers also have a personal computer located on their premises. At times, the computer user receives ADSL (an acronym for Asymmetric Digital Subscriber Line) signals from the Internet over the same telephone lines via an Internet Server Provider (ISP). In order to increase the speed of downloading of information from the Internet, an ADSL network interface is typically purchased and installed between the incoming telephone lines and the user's computer. However, since one or more telephone subscriber terminal equipment such as telephone sets, facsimile machines and/or answering devices are also connected to the same incoming telephone lines via internal house wiring, ADSL interference problems may be caused by the terminal equipment which can significantly limit or reduce the data rate. In one situation, it has been experienced that the change of state from "on-hook" to "off-hook" of the telephone equipment and sometimes the telephone terminal equipment even being "on-hook" can create a resonance effect to occur so as to drop the impedance value to less than 10Ω (Ohms) at a frequency as high as 500 KHz.

Accordingly, it would be desirable to provide an impedance blocking filter circuit for connection to the telephone terminal equipment causing the erratic input impedances. The impedance blocking filter circuit of the present invention is of a modular design so as to be easily connected by the subscriber in series with the offending telephone terminal equipment. The impedance blocking filter circuit blocks unconditionally any telephone impedances (e.g., open, short, capacitive, inductive, resonant, or any combination thereof) above the frequency of 20 KHz.

### SUMMARY OF THE INVENTION

Accordingly, it is a general object of the present invention to provide an impedance blocking filter circuit which effectively and efficiently eliminates ADSL interference caused by telephone terminal equipment.

It is an object of the present invention to provide an impedance blocking filter circuit for connection to telephone terminal equipment causing the erratic input impedances.

It is another object of the present invention to provide an impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone line and customer's terminal equipment so as to unconditionally block impedance above 20 KHz due to the customer's terminal equipment form an ADSL network interface unit and/or home networking interface unit.

It is still another object of the present invention to provide an impedance blocking filter circuit which is of a modular design so as to be easily connected in series with the offending telephone terminal equipment by the subscriber.

It is still yet another object of the present invention to provide an impedance blocking filter circuit which is comprised of six inductors, two resistors, and a capacitor.

[In accordance with a preferred embodiment of the present invention, there is provided an impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances above 20 KHz due to the customer's terminal equipment from an ADSL network interface unit and/or home networking interface unit. The filter circuit includes

first, second and third inductors connected in series between a first input terminal and a first common point. The first inductor has its one end connected to the first input terminal and its other end connected to one end of the second inductor. The second inductor has its other end connected to one end of the third inductor. The third inductor has its other end connected to the first common point. A first resistor has its one end also connected to the first common point and its other end connected to a first output terminal.]

*In accordance with one exemplary embodiment of the present invention, there is provided an impedance blocking filter circuit used in telecommunication systems for inter-connecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances above 20 KHz due to the customer's terminal equipment from an ADSL network interface unit and/or home networking interface unit. The filter circuit includes first, second and third inductors connected in series between a first input terminal and a first common point. The first inductor has its one end connected to the first input terminal and its other end connected to one end of the second inductor. The second inductor has its other end connected to one end of the third inductor. The third inductor has its other end connected to the first common point. A first resistor has its one end also connected to the first common point and its other end connected to a first output terminal.*

The filter circuit further includes fourth, fifth and sixth inductors connected in series between a second input terminal and a second common point. The fourth inductor has its one end connected to the second input terminal and its other end connected to one end of the fifth inductor. The fifth inductor has its other end connected to one end of the sixth inductor. The sixth inductor has its other end connected to the second common point. A second resistor has its one end also connected to the second common point and its other end connected to a second output terminal. A capacitor has its one end connected to the first common point and its other end connected to the second common point. [The foregoing applies specifically to the disclosure of the parent application Ser. No. 09/195,522. A third embodiment of an impedance blocking filter circuit of the present invention added by way of this continuation-in-part application is quite similar to the schematic diagram of FIG. 3, except that the filter circuit therein has been modified so that the resistors R1 and R2 are replaced with first and second tank circuits TC1 and TC2, respectively and a reed switch K1 is connected in series with the capacitor C1. As a result, this third embodiment represents an improvement over the embodiment of FIG. 3 since it overcomes the shunt additive capacitance problem and eliminates the deterioration in the return loss at the phone.]

*In another exemplary embodiment, the telecommunications filter circuit comprises: at least one first inductor electrically disposed between a first input terminal and a first common point; at least one second inductor electrically disposed between a second input terminal and a second common point; a first switch responsive to DC loop current; first and second tank circuits disposed in parallel and between respective ones of the first and second common points and output terminals, the tank circuits being adapted to reduce return loss when equipment connected to the filter circuit changes state; third and fourth inductors disposed electrically between respective ones of the first and second common points, and the first and second tank circuits; a second switch responsive to DC loop current; and a capacitor disposed in electrical series with the second switch, the second switch and capacitor being disposed substantially between the third and fourth inductors.*

[In addition, a fourth embodiment of an impedance blocking filter circuit of the present invention also added by way of this continuation-in-part application includes all of the components of the third embodiment and further has added successively seventh and eighth inductors L7,L8; a second capacitor C2 and a second reed switch K2 connected in series; and ninth and tenth inductors L9,L10. This produces a fifth-order filter circuit.]

*In yet another embodiment, the telecommunications filter circuit comprises: at least one first inductor electrically disposed between a first input terminal and a first common point; at least one second inductor electrically disposed between a second input terminal and a second common point; a first switch responsive to DC loop current; a varistor connected in series with at least one capacitor and in parallel with the first switch; and a correction circuit interconnected between the common points and output terminals, the correction circuit being adapted to reduce return loss when equipment connected to the filter circuit changes state. [In a fifth embodiment, there is provided an impedance blocking filter circuit which is quite similar to the schematic circuit diagram of FIG. 3, except that the filter circuit therein has been modified so as to eliminate the resistors R1 and R2 and a reed switch K1 is connected in series with the capacitor C1. The four inductors L1-L4 and the reed switch K1 are all housed within a multi-sectioned wound bobbin inductor structure so as to significantly reduce the inductors' interwinding capacitance.]*

*In another embodiment, the filter circuit comprises: at least one first inductor electrically disposed between a first input terminal and a first common point; at least one second inductor electrically disposed between a second input terminal and a second common point; a correction circuit adapted to reduce return loss when equipment connected to the filter circuit changes state, the correction circuit comprising first and second tank circuits disposed in parallel and interconnected between the common points and output terminals, the first and second tank circuits each comprising at least one winding; a first reed switch responsive to DC loop current, the first switch being disposed in a dual winding inductor structure comprising the at least one winding of the first and second tank circuits; and a second reed switch disposed in the dual winding inductor structure.*

[ In a sixth embodiment, there is provided an impedance blocking filter circuit which includes all of the components of the fifth embodiment and further has added successively seventh and eighth inductors L7,L8; a second capacitor C2 and a second reed switch K2 connected in series; and ninth and tenth inductors L9,L10. The second reed switch K2 is also housed within the multi-sectioned wound bobbin inductor structure. This produces a fifth-order filter circuit.]

*In still another embodiment, the filter circuit comprises: at least one first inductor disposed in electrical series between a first input terminal and a first common point; at least one second inductor disposed in electrical series between a second input terminal and a second common point; a first switch being responsive to DC loop current; at least one capacitor disposed in electrical series with the first switch between the first and second common points; at least one bobbin onto which are wound corresponding ones of the at least one first and second inductors, the bobbin(s) being adapted to reduce interwinding capacitance so as to increase the useful frequency range of the filter circuit, the bobbin(s) further receiving at least a portion of the first switch; at least one correction circuit interconnected between the common points and respective output terminals*

*of the filter circuit, the correction circuit(s) being adapted to reduce return loss caused by inductive impedance when terminal equipment connected to the filter circuit changes state; and a second switch and a second capacitor, the second capacitor and second switch being disposed in electrical series between third and fourth common points of the filter circuit.*

#### BRIEF DESCRIPTION OF THE DRAWINGS

These and other objects and advantages of the present invention will become more fully apparent from the following detailed description when read in conjunction with the accompanying drawings with like reference numerals indicating corresponding parts throughout, wherein:

FIG. 1 is an overall block diagram of a telecommunication system for interconnecting a central office and a subscriber's premises, employing an impedance blocking filter circuit of the present invention;

FIG. 2 is an exploded, perspective view of one form of a module housing the impedance blocking filter circuit;

FIG. 3 is a schematic circuit diagram of an impedance blocking filter circuit, constructed in accordance with the principles of the present invention;

FIG. 4 is a schematic circuit diagram of a second embodiment of an impedance blocking filter circuit, in accordance with the principles of the present invention;

FIG. 5 is a plot of input impedances of the impedance blocking filter circuit of FIG. 3 for various telephone equipment impedances as a function of frequency;

FIG. 6 is a schematic circuit diagram of current limiting protection circuitry for use with the filter circuit of FIG. 3;

FIG. 7 is a schematic circuit diagram of a home network demarcation filter for use with the filter circuit of FIG. 3;

FIG. 8 is schematic circuit diagram of a third embodiment of an impedance blocking filter circuit in accordance with the present invention;

FIG. 9 is schematic circuit diagram of a fourth embodiment of an impedance blocking filter circuit in accordance with the present invention;

FIG. 10(a) is a top plan view of a dual winding inductor device housing one or two reed switches for use in the filter circuits of FIGS. 8 and 9.

FIG. 10(b) is a side elevational view of the dual winding inductor device of FIG. 10(a);

FIG. 11(a) is a top plan view of a current sensor unit for housing a single inductor and a single reed switch for alternate use in the filter circuits of FIGS. 8 and 9;

FIG. 11(b) is a side elevational view of the current sensor unit of FIG. 11(a);

FIG. 12 is a schematic circuit diagram of a fifth embodiment of an impedance blocking filter circuit utilizing a multi-sectioned bobbin structure;

FIG. 13 is a schematic circuit diagram of a sixth embodiment of an impedance blocking filter circuit utilizing a multi-sectioned bobbin structure;

FIG. 14(a) is a side view of a multi-sectioned bobbin structure for use in the filter circuits of FIGS. 12 and 13; and

FIG. 14(b) is schematic diagram of the multi-sectioned bobbin structure of FIG. 14(a).

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now in detail to the drawings, there is illustrated in FIG. 1 an overall block diagram of a telecommunication

system 10 for interconnecting a telephone company's central office (CO) 12 and a subscriber's premises 14 over a transmission media such as a conventional twisted pair of telephone lines 16. The telecommunication system 10 employs a plurality of impedance blocking filter circuits, constructed in accordance with the principles of the present invention, in which each is contained in a modular housing 18.

The central office 12 includes a telephone office switch 20 and an Internet Service Provider (ISP) 22. The telephone office switch 20 is used to send voice signals via a low-pass filter 24 and a surge protector 26 to the telephone line 16. The ISP 22 transmits ADSL data signals to a modem 28 which are then sent to the telephone lines 16 via a high-pass filter 30 and the surge protector 26. It should be understood that the voice signals from the telephone office switch 20 and the ADSL data signal from the ISP 22 can be transmitted simultaneously to the telephone lines 16. Further, the voice signals (speech) are in the frequency band between 30 and 3400 Hz, and the ADSL data signals are in the frequency band between 20 KHz and 1.1 MHz.

The subscriber's premises 14 includes a Network Interface Device (NID)/surge protector unit 32 which is connected to the incoming telephone lines 16 on its input side and is connected to the subscriber's internal wiring or house wiring 34 on its output side via a demarcation RJ-11 jack and plug unit 36. As can be seen, the subscriber's premises further includes a number of terminal equipment such as a plurality of telephone sets 40. At times, the computer user will be downloading information to a personal computer 38 from the Internet by receiving ADSL data signals transmitted by the ISP 22.

In order to optimize the downloading of this information from the Internet, the user can purchase and install an ADSL network interface unit 42 for connection between the computer 38 and a RJ-11 jack and plug unit 44. The ADSL network interface unit 42 includes a high-pass filter 41 connected to the RJ-11 unit 44 and an internal modem 43 connected to the computer 38. The RJ-11 unit 44 is connected to the house wiring 34 for receiving the ADSL signals from the telephone lines 16. However, it will be observed that the plurality of telephone sets 40 are also connected to the same house wiring 34 via RJ-11 units 46, 48 and 50, respectively.

If it were not for the impedance blocking filter circuits 18 in the present invention, the output impedance from each of the telephone sets 40 would be connected in parallel with the input impedance of the ADSL unit 42. Since the output impedances from the telephone sets are subject to wide variations due to, for example, changing from "on-hook" to "off-hook" so as to present either an open, a short, capacitive, inductive, resonant, or any combination thereof at frequencies above 20 KHz, this erratic impedance can significantly affect the rate of the ADSL data signals being received by the computer 38 via the ADSL network interface unit 42.

Therefore, the main purpose of the impedance blocking filter circuit of the present invention is to isolate the terminal equipment (telephone sets) impedances from the ADSL unit 42 and the house wiring 34 so as to eliminate degradation of the performance of the ADSL unit 42. Further, the impedance blocking filter circuit serves to attenuate the ADSL data signal from being receiving by the telephone sets 40 in order to prevent non-linear conversion to voice band signals. Moreover, to facilitate the installation required by the customer, the filter circuit is contained in the modular housing 18.

As can be seen from FIG. 2, one form of the modular housing 18 includes a base 52 and a snap-on removable cover 54. The base has a printed circuit board 56 which is fixedly secured thereto by screws 58 and has mounted thereon the electrical circuit components for the filter circuit 59. One end of the modular housing 18 has a RJ-11 jack 60 formed integrally therewith for connection to the telephone set. This connection is achieved by plugging a RJ-11 plug (not shown) from a telephone set into the jack 60. The other end of the modular housing 18 has a short length of cable 62 extending therefrom and terminating in a RJ-11 plug 64 which is connectable to the house wiring. In particular, the plug 65 is connected to the house wiring 34 by plugging the same into a wall socket (not shown) having a RJ-11 jack.

In FIG. 3, there is shown a detailed schematic circuit diagram of the impedance blocking filter circuit 59 of the present invention for connection in series between the house wiring 34 and the terminal equipment (telephone set) of FIG. 1. The filter circuit 59 includes two input (tip and ring) terminals 66, 68 which are connectable to the house wiring 34 via the RJ-11 plug 64 and two output (tip and ring) terminals 70, 72 which are connectable to the telephone set 40 via the RJ-11 jack 60. The filter circuit 59 is comprised of inductors L1-L6, a capacitor C1, and resistors R1, R2.

The inductors L5, L3, L1 and the resistor R1 are connected in series between the first or tip input terminal 66 and the first or tip output terminal 70. Similarly, the inductors L6, L4, L2 and the resistor R2 are connected in series between the second or ring input terminal 68 and the second or ring output terminal 72. The inductors L5 and L6 are each preferably formed of a ferrite toroid. The inductors L3 and L4 have the same inductance values, and the inductors L1 and L2 have the same inductance values. The inductor L1 and the first resistor R1 are connected together at a common point A and to one side of the capacitor C1. The inductor L2 and the second resistor R2 are connected together at a common point B and to the other side of the capacitor C1. The resistors R1 and R2 also have the same values.

As previously pointed out, the primary purpose of the impedance blocking filter circuit 59 is to block the impedances from the telephone set at above the frequency of 20 KHz from reaching the house wiring 34, thereby preventing adverse performance of the ADSL network unit 42 (FIG. 1). In particular, the ADSL data signals being in the frequency range of 20 KHz and 1.1 MHz are mainly blocked by the inductors L1 and L2. However, it has been experienced that some telephone sets have an input capacitance of less than 5 of which can cause resonant impedances to occur within the ADSL band. In order to eliminate this underside effect, the capacitor C1 is used to lower any resonance into an acceptable dead band at around 10 KHz frequency. Further, the capacitor C1 also provides additional attenuation of the ADSL signals so as to prevent driving the telephone impedance into a non-linear region and converting the high frequency ADSL signals into audible signals which can be heard by the subscriber or converted to another ADSL band and cause ADSL interference. While there may still exist other minor resonances in the telephone set in the frequency range of between 20 KHz and 60 KHz, their undesirable effect is significantly reduced by the resistors R1 and R2 which produce a de-Q effect. It should be noted that the inductors L1 and L2 are formed as separate inductors so as to avoid longitudinal impedance problems as well as blocking differential impedances.

Since the inductors L1 and L2 have their own frequency limitations (e.g., self-resonance frequency), the inductors L3 and are provided so as to block the telephone impedances in

the frequency band of 1 MHz to 20 MHz. These inductors L3, L4 are necessary when phoneline home networking interface units (FIG. 1), are being used in conjunction with the ADSL network interface unit 42, as will be explained hereinafter. The inductors L4 and L6 are provided so as to block the telephone set impedances in the frequency band of 20 MHz to 500 MHz, which will prevent any problems caused by TV/FM interface.

For completeness in the disclosure of the above-described filter circuit but not for purposes of limitation, the following representative values and component identification are submitted. These values and components were employed in a filter circuit that was connected and tested, and which provides high quality performance.

PART	TYPE or VALUE
L1, L2	10 mH
L3, L4	220 $\mu$ H
L5, L6	ferrite toroid, 75 $\mu$ H
C1	22 nf
R1, R2	22 $\Omega$

With these above values being used, the input impedance of the impedance blocking filter circuit 59 was plotted for various telephone equipment impedances (e.g., open, short, capacitive, inductive, resonant, or a combination of these conditions) as a function of frequency and is illustrated in FIG. 5. As can be seen from the various curves, the input impedance across the input terminals 66, 68 of the impedance blocking filter circuit 59 for any telephone impedances connected across its output terminals 70, 72 is equal to or greater than 2K Ohms at frequencies above 40 KHz.

The impedance blocking filter circuit 59 of FIG. 3 is basically a second-order filter and has been found to minimize adequately voice band transmission effects when up to eight (8) filter circuits are installed into the telecommunication system of FIG. 1. In order to provide higher attenuation at frequencies above 20 KHz, there is shown in FIG. 4 a schematic circuit diagram of a second embodiment of a third-order impedance blocking filter circuit 59a of the present invention. The third-order filter circuit of FIG. 4 is substantially identical to the second-order filter circuit of FIG. 3, except there has been added an inductor L7 and an inductor L8. The inductor L7 is interconnected between the common point A and the first resistor R1, and the inductor L8 is connected between the common point B and the second resistor R2. The inductors L7 and L8 have the same inductance values.

Based upon tests conducted on the third-order filter circuit of FIG. 4, it was observed that higher attenuation was provided at frequencies above 20 KHz. However, it was found that the number of such third-order filter circuits which could be connected to the telecommunication system of FIG. 1 was limited to three or four. This is due to the fact that the inductor values of L1, L2, L7 and L8 of FIG. 4 are smaller (on the order of 5-10 mH) than the ones in FIG. 3, the capacitor value of C1 of FIG. 4 is larger (on the order of 33-47 nf) than the one in FIG. 3, and the adaptive capacitive loading caused by each added filter circuit will adversely affect the voice band performance. Thus, the optimized operation between voice performance and ADSL performance was found to exist when only three or four filter circuits 59a were installed.

While the filter circuit of FIG. 3 performed adequately, the inventor has found based upon further testing that a transient

problem will occur when the telephone set goes "off-hook" at the peak of the ring signal. This "off-hook" transient condition may cause current pikes to occur which are higher than 600 mA. As a result, the high current will tend to saturate the inductors, thereby momentarily lowering the input impedance of the filter circuit and thus adversely affects the data on the ADSL signal being transmitted to the interface unit 42.

In order to overcome this current transient problem, the inventors have developed fast current limiting protection circuitry 74 for providing protection against the "off-hook" transients. In FIG. 6 of the drawings, there is shown a schematic circuit diagram of the current limiting protection circuitry 74 which is comprised of depletion mode N-channel field-effect transistors (FET) Q1, Q2; resistors R1a, R2a; and varistors RV1, RV2. The FET Q1 has its drain electrode connected to a first input terminal 76, its source electrode connected to one end of the resistor R1a, and its gate electrode connected to the other end of the resistors R1a. The common point C of the gate electrode of the transistor Q1 and the resistor R1a is also joined to the first output terminal 78. Similarly, the FET Q2 has its drain connected to a second input terminal 80, its source connected to one end of the resistors R2a, and its gate electrode connected to the other end of the resistor R2a. The component point D of the gate of the transistors Q2 and the resistors Q2a is also joined to a second output terminal 82. One end of the varistor RV1 is connected to the drain of the transistors Q1, and the other end thereof is connected to the common point C. One end of the varistor RV2 is connected to the drain of the transistor Q2, and the other end thereof is connected to the common point D.

In use, the current limiting protection circuitry 74 replaces the resistors R1 and R2 of FIG. 3. The first and second input terminals 76, 80 of the protection circuitry 74 are connectable to the common points A and B of FIG. 3, and the first and second output terminals 78, 82 thereof are connected to the tip and ring output terminals 70, 72 of FIG. 3. The transistors Q1, Q2 may be similar to the ones commercially available from Supertex Corporation under their Part No. DN2530N3. The varistors may be similar to the type ZNR which are manufactured and sold by Panasonic Corporation. The resistors R1a and R2a have the same resistance value and are on the order of 5–20 Ohms depending on the thresholds of the transistors Q1, Q2. It should be understood that the transistors Q1, Q2 have a large tolerance on current limit and the resistors R1a, R2a permit the desired current limit value to be adjusted. Alternatively, the resistors R1a, R2a may have a value of zero Ohms or be entirely eliminated.

In normal on-hook operation, the transmission Q1 and Q2 are rendered conductive and have an on-resistance value of about 10 Ohms. When the telephone set goes "off-hook" into high ringing voltage, the gate-to-source voltage of the forward conducting FET will become more negative due to the resistors R1a, R2a. As a result, the resistance of the transistors Q1, Q2 will go very high which will limit the current spikes to approximately 70–100 mA. The transistor Q1 serves to limit the current flowing in a first direction, and the transistor Q2 serves to limit the current flow in a reverse direction. Further, the varistors RV1, RV2 defining transient protection means function to clamp transients caused by lightning and power shorts from damaging or destroying the FETs Q1, Q2.

In view of continuing increased use of host computers and the high demand for accessing of information from the Internet in the last decade or so, many of the subscribers will

be multi-PC homes. As shown in FIG. 1, the subscriber's premises or small business will typically have a second computer 38a also connected to the same internal house wiring 34. In order to effect high-speed data transfer in the multi-PC environment, there will be required phoneline home networking interface units 42a for using the internal house wiring in the frequency band above 5 MHz so as to interconnect the multiple computers 38, 38a or other devices at data rates above 10 MB/s as illustrated. While the impedance filter circuit of the present invention adequately filters and blocks the telephone impedances from the home networking signals, which are in the frequency band of 5–10 MHz, it will be noted that the home networking signals from the telephone company's C.O. are however still connected to the housing wiring via the NID/surge processor unit 32.

In order to solve this problem, the invention has developed a home network demarcation filter 84 as shown in desired (NID/surge protection unit 32) between the telephone company's incoming lines 16 and the subscriber's internal house wiring 34 via the demarcation unit 36. A schematic circuit diagram of the home network demarcation network is depicted in FIG. 7. The demarcation filter 84 includes two input (tip and ring) terminals 85, 88 which are connectable to the incoming lines via the jack side of the demarcation unit 36 in the NID/surge protector unit 32 and two output (tip and ring) terminals 90, 92 which are connectable to the internal house wiring via the plug side of the demarcation unit 36. The demarcation filter is comprised of six inductors L9–L14 and two capacitors C2, C3. In use, the demarcation filter is transparent to the ADSL data signals having the frequencies between 20 KHz and 1.1 MHz but will produce an attenuation of more than 40 dB for frequencies above 5.5 MHz. The demarcation filter will also provide an inductive input impedance for above 5 MHz frequency based so as to prevent loading down the home networking signals on the incoming phone lines and also adds data security benefits.

From the foregoing detailed description, it can thus be seen that the present invention provides an impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedance above 20 KHz due to the customer's terminal equipment from an ADSL network interface unit and/or home networking interface unit. The impedance blocking filter circuit is comprised of six inductors, two resistors, and a capacitor.

While the second-order impedance blocking filter 59 of FIG. 3 and the third-order impedance blocking filter 59a of FIG. 4 both perform adequately for unconditionally blocking telephone impedances above 20 KHz, the inventor has found that based upon additional testing they suffer from the disadvantages of causing (1) a shunt additive capacitance problem and (2) a deterioration in the return loss at a phone set, when the number of such filter circuits are added increasingly in parallel into the telecommunication system of FIG. 1.

The shunt capacitance problem is caused by the added capacitance from all of the filter circuits connected to the on-hook phones. The return loss problem is due to the fact that the series inductances of the impedance blocking filter circuit connected to the telephone set going "off-hook" will cause a resonance to occur in the frequency range of 2–5 KHz with the total capacitance seen, which is equal to the sum of the line capacitance plus the capacitance from the filter circuits. Further, as the total capacitance is increased this will also cause a lower resonant frequency which will

create a phase shift so to unbalance the telephone hybrid. As a result, the side tone levels of the "off-hook" telephone set is caused to increase.

In order to overcome this problem, there is provided in FIG. 8 a third embodiment of a second-order impedance blocking filter circuit 59b of the present invention. The third embodiment includes all of the circuit elements used in the filter circuit of FIG. 3, except for the resistors R1 and R2, and further includes a reed switch K1 and a return loss correction circuit consisting of a first tank circuit TC1 and a second tank circuit TC2.

In particular, the reed switch KC1 connected in series with the capacitor C1 is connected between the common points A and B. Further, the first tank circuit TC1 is comprised of a first winding inductor W1, a capacitor C3, and a resistor R3 all connected together in parallel and between the common point A and the output tip terminal 70. Similarly, the second tank circuit TC2 is comprised of a second winding inductor W2, a capacitor C4, and a resistor R4 all connected together in parallel and between the common point B and the output ring terminal 72. In addition, there provided optionally a metal-oxide varistor D1 connected in series with the capacitor C1 and in parallel with the reed switch K1. The varistor D1 serves to protect the reed switch K1 from being damaged by transients when the telephone set is in the on-hook condition.

In use, when a telephone set goes "off-hook" DC loop current will flow which creates a DC magnetic field in the first and second winding inductors W1, W2. This will cause only the reed switch K1 of the filter circuit 59b connected to the "off-hook" telephone set to become actuated or closed by the DC magnetic field. As a consequence, the shunt additive capacitance from all of the filter circuits connected to the "on-hook" phones have been eliminated.

Moreover, the first winding inductor W1 and the capacitor C3 of the first tank circuit TC1 will cause a resonance to occur at the frequency of about 2 KHz. The impedance of the first tank circuit TDC1 above the resonance frequency will appear as a capacitance reactance, which will substantially cancel the inductive reactance of the filter circuit 59b. The resistor R3 sets the Q or the slope of the resonance so as to best match the effects of the inductive impedance of the filter circuit. In this manner, the return loss at the "off-hook" phone is significantly improved, thereby reducing the side tone level of the telephone set. Similarly, the second winding inductor W2, the capacitor C4, and the resistor R4 of the second tank circuit TC1 operate in an identical manner to first winding inductor W1, the capacitor C3, and the resistor R3 of the first tank circuit TC1.

In FIG. 9, there is illustrated a fourth embodiment of an impedance blocking filter circuit 59c of the present invention. The fourth embodiment includes all of the circuit components of the filter circuit 59c of FIG. 8 and has added an inductor L7 and an inductor L8. The inductor L7 is interconnected between the common point A and the first tank circuit TC1, and the inductor L8 is interconnected between the common point B and the second tank circuit TC2. The filter circuit 59c as described thus far is essentially a third-order filter circuit which provides a better stop band performance than the second-order filter circuit 59b of FIG. 8.

Referring still to FIG. 9, a second reed switch K2 and a capacitor C2 have been successively added to convert the third-order filter circuit to a fourth-order filter circuit which is optimized for better operation for full rate ADSL modem. In particular, the reed switch K2 connected in series with the

capacitor C2 is joined between common points C and D. In addition, there is provided optionally a metal-oxide varistor D2 connected in series with the capacitor C2 and in parallel with the reed switch K2. Likewise, the varistor D2 is used to protect the reed switch K2 from being destroyed by transients when the telephone set is in the on-hook condition.

Further, an inductor L9 and an inductor L10 are added successively so as to produce a fifth-order filter circuit. Specifically, the inductor L9 is interconnected between the inductor L7 at the common point C and the first tank circuit TC1. The inductor L10 is interconnected between the inductor L8 at the common point D and the second tank circuit TC2.

In addition, a thermo-fuse F1 may be optionally connected in series the inductors L5, L3, L1, L7, L9 and the tank circuit TC1 which are arranged between the input tip terminal 66 and the output tip terminal 70. For example, the thermo-fuse F1 may be electrically interconnected between the input tip terminal 66 and the inductor L5. Typically, the thermo-fuse F1 is located physically adjacent to one of the inductors or the resistor in order to sense the highest temperature within the filter circuit. The fuse F1 provides a safety feature and will open when the second temperature of the filter circuit exceed a specified trip temperature. The fuse functions as a safety protection means for preventing the filter circuit from overheating and causing a fire due to a power cross on the phone lines.

In FIG. 10(a), there is shown a top plan view of a dual winding inductor device T1 for use in the filter circuits of FIGS. 8 and 9. FIG. 10(b) is a side elevational view of the dual winding inductor device. As can be seen, inductor device Ti includes a cylindrical-shaped housing 110 which contains the first wiring inductor W1 of the first tank circuit TC1, the second winding inductor W2 of the second tank circuit TC2, the reed switch K1, and the reed switch K2.

In FIG. 11(a), there is depicted a top plan view of an alternate current sensor unit CS for use in the filter circuits of FIGS. 8 and 9. FIG. 11(b) is a side elevational view of the current sensor unit CS. The current sensor unit CS is forward of cylindrical housing 112 and contains a single inductor L and a single reed switch K. It should be apparent to those skilled in the art the dual winding inductor device T1 can be replaced with two such current sensor units CS so as to render the same operation. Since the windings W1, W2 or the inductor L is used to drive the reed switches K1, K2(K), the reed switch is selected to be actuatable on a loop current threshold of approximately 14–20 mA. If the loop current threshold is below 14 mA, the reed switch may chatter during ringing on a 1 REN telephone and may thus shorten the useful life of the reed switch. On the other hand, if the loop current threshold is above 20 mA, then the amount of loop current may be insufficient to be actuatable in the worst case condition (e.g., the longest cable).

In FIG. 12, there is illustrated a fifth embodiment of an impedance blocking filter circuit 59d of the present invention. The fifth embodiment is substantially identical to the first embodiment of the second-order filter circuit of FIG. 3, except that the resistors R1 and R2 have been eliminated and a reed switch K1 has been added in series with the capacitor C1 located between the common points A and B. Further, the four stage inductors L1, L2 and L3, L4 of FIG. 3 have replace by a multi-sectioned wound bobbin inductor structure T2. It will be noted that the bobbin structure T2 includes a tip winding TW (corresponding to replace inductors L1, L3) connected between the inductor L5 and the common

point A, and a ring winding RW (corresponding to replace inductors L2,L4) connected between the inductor L6 and the common point B. Further, the bobbin structure T2 houses the reed switches K1,K2. The tip(ring) winding TW(RW) combines the inductor L1(L2) for the ADSL frequency band (20 KHz to 1.1 MHz) and the inductor L3(L4) for the mid-frequency band (1 MHz to 20 MHz) into a single coil. It has been found that the filter circuit 59d is more economical to manufacture and assemble, but yet eliminates the shunt additive capacitance problem of the filter circuits connected the "on-hook" phone sets. Optionally a return loss correction circuit consisting of a first tank circuit TC1 and a second tank circuit TC2 may be interconnected between the common points A,B and the output terminals 70,72.

In FIG. 13, there is shown a sixth embodiment of an impedance filter circuit 59e of the present invention, the sixth embodiment includes all of the circuit components of the filter circuit 59d of FIG. 12 and has added an inductor L7 and an inductor L8. The inductor L7 is interconnected between the common point A and the output terminal 70, and the inductor L8 is interconnected between the common point B and the output ring terminal 72. The filter circuit thus far described is essentially a third-order filter circuit for producing a better stop band.

Referring still to FIG. 13, a second reed switch K2 and a second capacitor C2 have been further added to as to convert the third-order filter circuit to a fourth-order filter circuit which is optimized for better operations for full rate ADSL modems. In practice, the second reed switch K2 connected in series with the second capacitor C2 are joined between modes C and D. It will be noted that the second reed switch K2 is also incorporated into the bobbin structure. Further, an inductor L9 is added between the inductor L7 and the node E, and an inductor L10 is added between the inductor L8 and the node F in order to convert the fourth-order filter circuit to a fifth-order filter circuit. Optionally, a thermo-fuse F2 may be commenced in a manner similar to the one in FIG. 9.

In FIG. 14(a), there is shown a side view of a wiring bobbin structure T2 having multiple sections S1-S6 for use in the circuits of FIGS. 12 and 13 FIG. 14(b) is a schematic diagram of the bottom structure T2 of FIG. 14(a). The bobbin structure includes a first narrow section S1 on which is wound the inductor L3, first window sections S2,S3 on which are wound the inductor L1, a second narrow section S4 on which is wound the inductor L4, and second wider sections S5,S6 on which are wound the inductor L2. The inductors L2,L3 are combined on the same coil and is represented by the tip winding TW in FIG. 14(b). Similarly, the inductors L2,L4 are combined on the coil and is represented by the ring window RW.

The inventor has designed purposely the bobbin structure T2 to include the narrow section S1(S4) on which is wound the higher frequency of the coil (e.g., inductor L3,L4) since there will be less winding capacitance so as to obtain a maximum useful frequency range. Further, by dividing the bobbin structure into a plurality of sections the beginning of the tip(ring) winding TW(RW) of pin 1 (pin 5) will be farther removed from the end of the tip (ring) winding on pin 4 (pin 8). As result, the interwinding capacitance will be reduced, thereby increasing the useful frequency range of the coil. The first reed switch K1 with pins 2 and 7 is disposed within the center of the bobbin structure T2 so as to be actuable by the windings TW, RW. Further, the second reed switch K2 with pins 3 and 6 may be also for formed with the center of the bobbin structure and actuated by the same winding TW, RW.

While there has been illustrated and described what is at present considered to be a preferred embodiment of the present invention, it will be understood by those skilled in the art that various changes and modifications may be made, and equivalents may be substituted for elements thereof without departing from the true scope of the invention. In addition, many modifications may be made to adapt a particular situation or material to the teachings of the invention without departing from the central scope thereof. Therefore, it is intended that this invention not be limited to the particular embodiments disclosed as the best mode contemplated for carrying out the invention, but that the invention will include all embodiments falling within the scope of the appended claims.

What is claimed is:

[1. An impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances from above 20 KHz due to the customer's terminal equipment from ASDL network unit and/or home networking interface unit, said filter circuit comprising:

first, second, and third inductors connected in series between a first input terminal and a first common point,

said first inductor having its one end connected to said first input terminal and its other end connected to one end of said second inductor, said second inductor having its other end connected to one end of said third inductor, said third inductor having its other end connected to said first common point;

fourth, fifth, and sixth inductors connected in series between a second input terminal and a second common point;

said fourth inductor having its one end connected to said second input terminal and its other end connected to one end of said fifth inductor, said fifth inductor having its other end connected to one end of said sixth inductor, said sixth inductor having its other end connected to said second common point;

first switching means having a first end and a second end and being responsive to DC loop current for electrically connecting said first end to said second end;

a capacitor having a first end connected to said first common point and a second end connected to said first end of said switching means, said second end of said switching means being connected to said second common point; and

correction circuit means interconnected between said common points and said output terminals for significantly reducing return loss caused by inductive impedance when the customer's terminal equipment goes off-hook.]

[2. An impedance blocking filter circuit as claimed in claim 1, wherein said correction circuit means is comprised of a first tank circuit and a second tank circuit, said first tank circuit being formed of a first winding inductor, a first tank capacitor and a first tank resistor all connected in parallel and between said first common point and said first output terminal, second tank circuit being formed of a second winding inductor, a second tank capacitor, and a second tank resistor all connected in parallel and between said second common point and said second output terminal.]

[3. An impedance blocking filter circuit as claimed in claim 2, further comprising a seventh inductor having a first end connected to said first common point and a second end connected to said first tank circuit, and an eighth inductor

having a first end connected to said second common point and a second end connected to said second tank circuit.]

[4. An impedance blocking filter circuit as claimed in claim 3, further comprising second switching means having a first end and a second end and being responsive to said DC loop current for electrically connecting said first end to said second end, and a second capacitor having a first end connected said eighth inductor at a first node and a second end connected to said first end of said second switching means, said second end of said second switching means being connected to said seventh inductor at a second node.]

[5. An impedance blocking filter circuit as claimed in claim 4, further comprising a ninth inductor having a first end connected to said seventh inductor at said first node and a second end connected to said first tank circuit, and a tenth inductor having a first end connected to said eighth inductor at said second node and a second end connected to said second tank circuit.]

[6. An impedance blocking filter circuit as claimed in claim 5, wherein said first switching means includes a first reed switch and said second switching means includes a second reed switch.]

[7. An impedance blocking filter circuit as claimed in claim 6, wherein said first winding of said first tank circuit, said second winding of said second tank circuit, said first reed switch, and said second reed switch are arranged in a dual winding inductor structure.]

[8. An impedance blocking filter circuit as claimed in claim 6, wherein said first winding of said first tank circuit and said first reed switch is arranged in a first current sensor unit, said second winding of said second tank circuit and said second reed switch is arranged in a second current sensor unit.]

[9. An impedance blocking filter circuit as claimed in claim 1, further comprising a metal-oxide varistor connected to series with said capacitor and in parallel with said first switching means.]

[10. An impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances from above 20 KHz due to the customer's terminal equipment from an ADSL network unit and/or home networking interface unit, said filter circuit comprising:

first, second, and third inductors connected in series between a first input terminal and a first common point; said first inductor having its one end connected to said first input terminal and its other end connected to one end of said second inductor, said second inductor having its other end connected to one end of said third inductor, said third inductor having its other end connected to said first common point;

fourth, fifth, and sixth inductors connected in series between a second input terminal and a second common point;

said fourth inductor having its one end connected to said second input terminal and its other end connected to one end of said fifth inductor, said fifth inductor having its other end connected to one end of said sixth inductor, said sixth inductor having its other end connected to said second common point;

first switching means having a first end and a second end and being responsive to DC loop current for electrically connecting said first end to said second end;

a capacitor having a first end connected to said first common point and a second end connected to said first

end of said switching means, said second end of said switching means being connected to said second common point; and

bobbin means including at least a first narrow section on which is wound said second inductor, first wider sections on which are wound said third inductor, a second narrow section on which is wound said fifth inductor; and second wider sections on which are wound said sixth inductor for reducing interwinding capacitance so as to increase the useful frequency range, said bobbin means having a center portion for receiving said first switching means.]

[11. An impedance blocking filter circuit as claimed in claim 10, further comprising correction circuit means interconnected between said common points and said output terminals for significantly reducing return loss caused by inductive impedance when the customer's terminal equipment goes off-hook.]

[12. An impedance blocking filter circuit as claimed in claim 11, wherein said correction circuit means is comprised of a first tank circuit and a second tank circuit, said first tank circuit being formed of a first winding inductor, a first tank capacitor, and a first tank resistor all connected in parallel and between said first common point and said first output terminal, second tank circuit being formed of a second winding inductor, a second tank capacitor, and a second tank resistor all connected in parallel and between said second common point and said second output terminal.]

[13. An impedance blocking filter circuit as claimed in claim 12, further comprising a seventh inductor having a first end connected to said first common point and a second end connected to said first tank circuit, and an eighth inductor having a first end connected to said second common point and a second end connected to said second tank circuit.]

[14. An impedance blocking filter circuit as claimed in claim 13, further comprising second switching means having a first end and a second end and being responsive to said DC loop current for electrically connecting said first end to said second end, and a second capacitor having a first end connected said eighth inductor at a first node and a second end connected to said first end of said second switching means, said second end of said second switching means being connected to said seventh inductor at a second node.]

[15. An impedance blocking filter circuit as claimed in claim 14, further comprising a ninth inductor having a first end connected to said seventh inductor at said first node and a second end connected to said first tank circuit, and a tenth inductor having a first end connected to said eighth inductor at said second node and a second end connected to said second tank circuit.]

[16. An impedance blocking filter circuit as claimed in claim 15, wherein said first switching means includes a first reed switch and said second switching means includes a second reed switch.]

[17. An impedance blocking filter circuit as claimed in claim 16, wherein said first winding of said first tank circuit, said second winding of said second tank circuit, said first reed switch, and said second reed switch are arranged in a dual winding inductor structure.]

[18. An impedance blocking filter circuit as claimed in claim 16, wherein said first winding of said first tank circuit and said first reed switch is arranged in a first current sensor unit, said second winding of said second tank circuit and said second reed switch is arranged in a second current sensor unit.]

[19. An impedance blocking filter circuit as claimed in claim 10, further comprising a metal-oxide varistor con-

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nected in series with said capacitor and in parallel with said first switching means.]

[20. An impedance blocking filter circuit as claimed in claim 10, further comprising a thermo-fuse connected in series with said first, second and third inductors.]

21. An impedance blocking filter circuit used in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances from above 20 KHz due to the customer's terminal equipment from an ADSL network unit and/or home networking interface unit, said filter circuit comprising:

first, second, and third inductors connected in series between a first input terminal and a first common point; said first inductor having its one end connected to said first input terminal and its other end connected to one end of said second inductor; said second inductor having its other end connected to one end of said third inductor; said third inductor having its other end connected to said first common point;

fourth, fifth, and sixth inductors connected in series between a second input terminal and a second common point;

said fourth inductor having its one end connected to said second input terminal and its other end connected to one end of said fifth inductor; said fifth inductor having its other end connected to one end of said sixth inductor; said sixth inductor having its other end connected to said second common point;

first switching means having a first end and a second end and being responsive to DC loop current for electrically connecting said first end to said second end;

a capacitor having a first end connected to said first common point and a second end connected to said first end of said switching means, said second end of said switching means being connected to said second common point; and

correction circuit means interconnected between said common points and said output terminals for significantly reducing return loss caused by inductive impedance when the customer's terminal equipment goes off-hook.

22. An impedance blocking filter circuit in telecommunication systems for interconnecting between incoming telephone lines and customer's terminal equipment so as to unconditionally block impedances from above 20 KHz due to the customer's terminal equipment from an ADSL network unit and/or home networking interface unit, said filter circuit comprising:

first, second, and third inductors connected in series between a first input terminal and a first common point; said first inductor having its one end connected to said first input terminal and its other end connected to one end of said second inductor; said second inductor having its other end connected to one end of said third inductor; said third inductor having its other end connected to said first common point;

fourth, fifth, and sixth inductors connected in series between a second input terminal and a second common point;

said fourth inductor having its one end connected to said second input terminal and its other end connected to one end of said fifth inductor; said fifth inductor having its other end connected to one end of said sixth inductor; said sixth inductor having its other end connected to said second common point;

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first switching means having a first end and a second end and being responsive to DC loop current for electrically connecting said first end to said second end;

a capacitor having a first end connected to said first common point and a second end connected to said first end of said switching means, said second end of said switching means being connected to said second common point; and

bobbin means including at least a first narrow section on which is wound said second inductor, first wider sections on which are wound said third inductor, a second narrow section on which is wound said fifth inductor, and second wider sections on which are wound said sixth inductor for reducing interwinding capacitance so as to increase the useful frequency range, said bobbin means having a center portion for receiving said first switching means.

23. An impedance blocking filter circuit as claimed in claim 21, wherein said correction circuit means is comprised of a first tank circuit and a second tank circuit, said first tank circuit being formed on a first winding inductor; a first tank capacitors and a first tank resistor all connected in parallel and between said first common point and said first output terminal, second tank circuit being of a second winding inductor, a second tank capacitor, and a second tank resistor all connected in parallel between said second common point and said second output terminal.

24. An impedance blocking filter circuit as claimed in claim 23, further comprising a seventh inductor having a first end connected to said first common point and a second end connected to said first tank circuit and an eighth inductor having a first end connected to said second common point and a second end connected to said second tank circuit.

25. An impedance blocking filter circuit as claimed in claim 24, further comprising second switching means having a first end and a second end and being responsive to said DC loop current for electrically connecting said first end to said second end, and a second capacitor having a first end connected to said eighth inductor at a first node and a second end connected to said first end of said switching means, said second end of said second switching means being connected to said seventh inductor at a second node.

26. An impedance blocking filter circuit as claimed in claim 25, further comprising a ninth inductor having a first end connected to said seventh inductor at said first node and a second end connected to said first tank circuit, and a tenth inductor having a first end connected to said eighth inductor at said second node and a second end connected to said second tank circuit.

27. An impedance blocking filter circuit as claimed in claim 26, wherein said first switching means includes a first reed switch and said second switching means includes a second reed switch.

28. An impedance blocking filter circuit as claimed in claim 27, wherein said first winding of said first tank circuit, and second winding of said second tank circuit, said first reed switch, and said second reed switch are arranged in a dual window inductor structure.

29. An impedance blocking filter circuit as claimed in claim 27, wherein said first switching of said first tank circuit and said first reed switch is arranged in a first current sensor unit, said second winding of said second tank circuit and said second reed switch is arranged in a second current sensor unit.

30. An impedance blocking filter circuit as claimed in claim 21, further comprising a metal-oxide varistor con-

nected in series with said capacitor and in parallel with said first switching means.

31. An impedance blocking filter circuit as claimed in claim 22, further comprising correction circuit means interconnected between said common points and said output terminals for significantly reducing return loss caused by inductive impedance when the customer's terminal equipment goes off-hook.

32. An impedance blocking filter circuit as claimed in claim 31, wherein said correction circuit means is comprised of a first tank circuit and a second tank circuit, said first tank circuit being formed of a first winding inductor, a first tank capacitor, and a first tank resistor all connected in parallel and between said first common point and said first output terminal, second tank circuit being formed of a second winding inductor, a second tank capacitor, and a second tank resistor all connected in parallel between said second common point and said second output terminal.

33. An impedance blocking filter circuit as claimed in claim 32, further comprising a seventh inductor having a first end connected to said first common point and a second end connected to said first tank circuit, and an eighth inductor having a first end connected to said second common point and a second end connected to said second tank circuit.

34. An impedance blocking filter circuit as claimed in claim 33, further comprising second switching means having a first end and a second end and being responsive to said DC loop current for electrically connecting said first end to said second end, and a second capacitor having a first end connected to said eighth inductor at a first node and a second end connected to said first end of said second switching means, said second end of said second switching means being connected to said seventh inductor at a second node.

35. An impedance blocking filter circuit as claimed in claim 34, further comprising a ninth inductor having a first end connected to said seventh inductor at said first node and a second end connected to said first tank circuit, and a tenth inductor having a first end connected to said eighth inductor at said second node and a second end connected to said second tank circuit.

36. An impedance blocking filter circuit as claimed in claim 35, wherein said first switching means includes a first reed switch and said second switching means includes a second reed switch.

37. An impedance blocking filter circuit as claimed in claim 36, wherein said first winding of said first tank circuit, said second winding of said second tank circuit, said first reed switch, and said second reed switch are arranged in a dual winding inductor structure.

38. An impedance blocking filter circuit as claimed in claim 36, wherein said first winding of said first tank circuit and said first reed switch is arranged in a first current sensor unit, said second winding of said second tank circuit and the second reed switch is arranged in a second current sensor unit.

39. An impedance blocking filter circuit as claimed in claim 22, further comprising a metal-oxide varistor connected in series with said capacitor and in parallel with said first switching means.

40. An impedance blocking filter circuit as claimed in claim 22, further comprising a thermo-fuse connected in series with said first, second and third inductors.

41. A telecommunications filter circuit comprising:

at least one first inductor electrically disposed between a first input terminal and a first common point;

at least one second inductor electrically disposed between a second input terminal and a second common point;

a first switch responsive to DC loop current for selectively passing therethrough;

first and second tank circuits, each of said circuits being formed of respective ones of a winding inductor, capacitor and resistor all disposed in parallel and between respective ones of said first and second common points and output terminals, said tank circuits being adapted to reduce return loss when equipment connected to said filter circuit changes state;

third and fourth inductors disposed electrically between respective ones of said first and second common points, and said first and second tank circuits;

a second switch responsive to DC loop current; and

a capacitor disposed in electrical series with said second switch, said second switch and capacitor being disposed substantially between said third and fourth output.

42. A telecommunications filter circuit as claimed in claim 41, further comprising fifth and sixth inductors disposed electrically between respective ones of said third and fourth inductors and said first and second tank circuits.

43. A telecommunications filter circuit as claimed in claim 42, wherein said first switch includes a first reed switch and said second switch includes a second reed switch.

44. A telecommunications filter circuit as claimed in claim 43, wherein said winding inductors of said first and second tank circuits and said first and second reed switches are arranged in a dual winding inductor structure.

45. A telecommunications filter circuit as claimed in claim 43, wherein said winding inductor of said first tank circuit and said first reed switch are arranged in a first current sensor unit, and said winding inductor of said second tank circuit and said second reed switch are arranged in a second current sensor unit.

46. A telecommunications filter circuit comprising:

at least one first inductor electrically disposed between a first input terminal and a first common point;

at least one second inductor electrically disposed between a second input terminal and a second common point;

a first switch responsive to DC loop current for selectively passing therethrough;

a varistor connected in series with at least one capacitor and in parallel with said first switch; and

a correction circuit interconnected between said common points and output terminals, said correction circuit being adapted to reduce return loss when equipment connected to said filter circuit changes state.

47. The telecommunications filter circuit as claimed in claim 46, wherein said varistor and first switch are disposed in electrical parallel with one another to form a first circuit, said first circuit being disposed in electrical series with at least one capacitor.

48. The telecommunications filter circuit as claimed in claim 46, wherein said first circuit and said at least one capacitor are disposed in electrical series substantially between said first and second common points.

49. The telecommunications filter circuit as claimed in claim 46, wherein said at least one first and second inductors each comprise three inductors disposed in electrical series between respective ones of said first and second input terminals and said first and second common points.

50. The telecommunications filter circuit as claimed in claim 48, wherein said at least one first and second inductors each comprise three inductors disposed in electrical series between respective ones of said first and second input terminals and said first and second common points.

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51. A telecommunications filter circuit comprising:  
 at least one first inductor electrically disposed between a  
 first input terminal and a first common point;  
 at least one second inductor electrically disposed between  
 a second input terminal and a second common point;  
 a correction circuit adapted to reduce return loss when  
 equipment connected to said filter circuit changes state,  
 said correction circuit comprising first and second tank  
 circuits disposed in parallel and interconnected  
 between said common points and output terminals, said  
 first and second tank circuits each comprising at least  
 one winding;  
 a first reed switch responsive to DC loop current for  
 selectively passing current therethrough, said first  
 switch being disposed in a dual winding inductor  
 structure comprising said at least one windings of said  
 first and second tank circuits; and  
 a second reed switch disposed in said dual winding  
 inductor structure.
52. The telecommunications filter circuit as claimed in  
 claim 51, wherein said at least one first and second induc-  
 tors each comprise three inductors disposed in electrical  
 series between respective ones of said first and second input  
 terminals and said first and second common points.
53. The telecommunications filter circuit as claimed in  
 claim 51, wherein said dual winding inductor structure  
 comprises a bobbin, and said first and second reed switches  
 are disposed substantially within a central region of said  
 bobbin.
54. A impedance blocking filter circuit comprising:  
 at least one first inductor disposed in electrical series  
 between a first input terminal and a first common point;  
 at least one second inductor disposed in electrical series  
 between a second input terminal and a second common  
 point;  
 a first switch being responsive to DC loop current;  
 at least one capacitor disposed in electrical series with  
 said first switch between said first and second common  
 points;  
 at least one bobbin including at least first and second  
 portions on which are wound corresponding ones of  
 said at least one first and second inductors, said at least  
 one bobbin being adapted to reduce intertwining  
 capacitances so as to increase the useful frequency  
 range of said filter circuit, said at least one bobbin  
 further having a center portion for receiving at least a  
 portion of said first switch;  
 at least one correction circuit interconnected between  
 said common points and respective output terminals of  
 said filter circuit, said at least one correction circuit  
 being adapted to reduce return loss caused by inductive  
 impedance when a customer's terminal equipment con-  
 nected to said filter circuit changes state; and  
 a second switch and a second capacitor, said second  
 capacitor and second switching being disposed in  
 electrical series between third and fourth common  
 points of said filter circuit.
55. An impedance blocking filter circuit as claimed in  
 claim 54, wherein said first switch comprises a first switch  
 magnetically coupled to at least one inductor of said at least  
 one correction circuit.
56. An impedance blocking filter circuit as claimed in  
 claim 54, wherein said at least one correction circuit com-  
 prises first and second tank circuits.
57. An impedance blocking filter circuit as claimed in  
 claim 54, wherein the filter circuit is used in telecommuni-

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- cation systems for interconnecting between incoming tele-  
 phone lines and customer's terminal equipment so as to  
 unconditionally block impedances from above 20 KHz due to  
 the customer's terminal equipment from an ADSL network  
 unit and/or home networking interface unit.
58. A telecommunications filter circuit comprising:  
 first inductor means electrically disposed between a first  
 input terminal and a first common point;  
 second inductor means electrically disposed between sec-  
 ond input terminal and a second common point;  
 first means, responsive to DC loop current, for selectively  
 passing current therethrough;  
 first and second tank circuits, each of said circuits being  
 formed of respective ones of a winding inductor,  
 capacitor and resistor all disposed in parallel and  
 between respective ones of said first and second com-  
 mon pints and output terminals, said tank circuit being  
 adapted to reduce return loss when equipment con-  
 nected to said filter circuit changes state;  
 third and fourth inductor means disposed electrically  
 between respective ones of said first and second com-  
 mon points, and said first and second tank circuits;  
 second means, responsive to DC loop current, for selec-  
 tively passing current; and  
 means for storing electrical charge disposed in electrical  
 series with said second switch, said second switch and  
 means for storing electrical charge being disposed  
 substantially between said third and fourth inductor  
 means.
59. A telecommunications filter circuit comprising:  
 first inductor means electrically disposed between a first  
 input terminal and a first common point;  
 second inductor means electrically disposed between a  
 second input terminal and a second communication  
 point;  
 first means, responsive to DC loop current, for selectively  
 passing current therethrough;  
 means for providing transient suppression connected in  
 series with at least one means for storing electrical  
 charge, and in parallel with said first means for selec-  
 tively passing current; and  
 correction circuit means interconnected between said  
 common points and output terminals, said correction  
 circuit means being adapted to reduce return loss when  
 equipment connected to said filter circuit changes state.
60. A telecommunications filter circuit comprising:  
 first means for providing inductance electrically disposed  
 between a first input terminal and a first common point;  
 second means for providing inductance electrically dis-  
 posed between a second input terminal and a second  
 common point;  
 means for reducing return loss when equipment connected  
 to said filter circuit changes state, said means for  
 reducing return loss comprising first and second tank  
 circuits disposed in parallel and interconnected  
 between said common points and output terminals, said  
 first and second tank circuits each comprising at least  
 one winding means;  
 first means for switching responsive to DC loop current  
 and adapted to selectively passing current  
 therethrough, said first means for switch being dis-  
 posed in a means for receiving at least two winding  
 means, said at least two winding means comprising  
 said at least one winding means of said first and second  
 tank circuits; and

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*a second means for switching disposed in said means for receiving.*  
*61. A impedance blocking filter circuit comprising:*  
*first inductive means disposed in electrical series between a first input terminal and a first common point;* 5  
*second inductive means disposed in electrical series between a second input terminal and a second common point;*  
*first means for switching, responsive to DC loop current;* 10  
*at least one capacitor disposed in electrical series with said first means for switching between said first and second common points;*  
*means for receiving including at least first and second portions on which are wound corresponding ones of* 15  
*said first and second inductive means, and means for receiving being adapted to reduce interwinding capaci-*

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*tance so as to increase the useful frequency range of said filter circuit, said at least one means for receiving further having means for receiving at least a portion of said first means for switching;*  
*at least one correction circuit means interconnected between said common points and respective output terminals of said filter circuit, said at least one correction circuit being adapted to reduce return loss caused by inductive impedance when a customer's terminal equipment connected to said filter circuit changes stage; and*  
*second means for switching and a second capacitor, said second capacitor and second means for switching being disposed in electrical series between third and fourth common points of said filter circuit.*

\* \* \* \* \*