Title: PHACOEMULSIFICATION HOOK TIP

Abstract: In various embodiments, a phacoemulsification cutting tip with a straight shaft and an angled portion off of the straight shaft may include a hook on the angled portion to move an axis of rotation of the cutting tip closer to alignment with an extended centerline of the shaft. The cutting tip may be configured to torsionally rotate back and forth on an axis perpendicular to a centerline of the shaft (e.g., rotation around a y-axis). In some embodiments, lateral vibrations (e.g., side to side along an x-axis or z-axis perpendicular to the y-axis) that result from torsional rotation around the y-axis in a cutting tip without the hook may be reduced through use of the hook to balance the otherwise eccentrically weighted hook.
PHACOEMULSIFICATION HOOK TIP

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FIELD OF THE INVENTION

The present invention generally pertains to phacoemulsification. More particularly, but not by way of limitation, the present invention pertains to phacoemulsification cutting tips.

DESCRIPTION OF THE RELATED ART

The human eye in its simplest terms functions to provide vision by transmitting light through a clear outer portion called the cornea, and focusing the image by way of the lens onto the retina. The quality of the focused image depends on many factors including the size and shape of the eye, and the transparency of the cornea and lens.

When age or disease causes the lens to become less transparent, vision deteriorates because of the diminished light which can be transmitted to the retina. This deficiency in the lens of the eye is medically known as a cataract. An accepted treatment for this condition is surgical removal of the lens and replacement of the lens function by an intraocular lens (IOL).

Cataractous lenses may be removed by a surgical technique called phacoemulsification. During this procedure, a thin phacoemulsification cutting tip may be inserted into the diseased lens and vibrated ultrasonically. The vibrating cutting tip may liquefy or emulsify the lens so that the lens may be aspirated out of the eye. The diseased lens, once removed, may be replaced by an artificial lens.
SUMMARY OF THE INVENTION

In various embodiments, a phacoemulsification tip with a straight shaft and an angled portion off of the straight shaft may include a hook on the angled portion to move an axis of rotation of the tip closer to alignment with a centerline of the shaft. The tip may be configured to torsionally rotate back and forth on an axis perpendicular to a centerline of the shaft (e.g., rotation around a y-axis). In some embodiments, lateral vibrations (e.g., side to side along an x-axis or z-axis perpendicular to the y-axis) that result from torsional rotation around the y-axis in a tip without the hook may be reduced through use of the hook to balance the otherwise eccentrically weighted hook.
BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present invention, reference is made to the following description taken in conjunction with the accompanying drawings in which:

FIGs. 1a-b illustrate a phacoemulsification tip with a distal end that is angled relative to centerline of the tip shaft;

FIG. 2a illustrates a phacoemulsification surgical console connected to a handpiece through an irrigation line and an aspiration line, according to an embodiment;

FIG. 2b illustrates an ultrasonic horn attached to the hooked tip, according to an embodiment;

FIGs. 3a-b illustrate an embodiment of the hooked tip;

FIG. 4 illustrates motion of the hooked tip, according to an embodiment;

FIG. 5 illustrates a hooked tip inserted into an incision in the eye, according to an embodiment; and

FIGs. 6a-c illustrate additional embodiments of the hooked tip.

It is to be understood that both the foregoing general description and the following detailed description are exemplary and explanatory only and are intended to provide a further explanation of the present invention as claimed.
DETAILED DESCRIPTION OF THE EMBODIMENTS

FIGs. 1a-b illustrate a phacoemulsification cutting tip 100 with a distal end that is angled relative to a tip shaft 108. The cutting tip 100 may include a predominantly straight shaft 108 with the far distal portion bent on an angle 102 (e.g., approximately a 20 degree bend). Other angles are also contemplated (e.g., 5 degree bend, 35 degree bend, etc). The distal portion may have a flared and/or beveled distal end. The cutting tip 100 may be used in conjunction with a phacoemulsification handpiece 204 (e.g., see FIG. 2). When used with the handpiece 204, the cutting tip 100 may use longitudinal movement and/or transverse movement. Cutting tip 100 may be eccentrically weighted with tip material on only one side of the extended shaft centerline 104 (because of angle 102). As used herein "extended shaft centerline" refers to a line that includes and is collinear with the shaft centerline (as illustrated in, for example, FIGs. 1a and 3a). The eccentrically weighted cutting tip may therefore have a center of rotation 106 that is displaced from the extended shaft centerline 104 of the shaft 108 through at least a portion of the cutting tip 100 (e.g., at least along the bottom 10% of the length of the cutting tip 100). Other portions of the length are also contemplated (e.g., the center of rotation 106 may be displaced from the extended shaft centerline 104 through 50% of the length or gradually over the entire length of the cutting tip 100). For example, as seen in FIG. 3a, the center of rotation 106 may follow an angle of approximately 0 to 10 degrees off parallel with the extended shaft centerline 104. Other angles and configurations of the center of rotation 106 are also contemplated (e.g., the center of rotation 106 may be displaced from and parallel to the extended shaft centerline 104). Rotating the eccentrically weighted tip and/or the resistance of fluid against the moving cutting tip 100 may cause lateral vibrations in the eccentrically weighted cutting tip 100 when the cutting tip 100 is vibrated (e.g., rotationally and/or longitudinally) through the shaft 108.

FIG. 2a illustrates a phacoemulsification surgical console 214 connected to a handpiece 204 through an irrigation line 206 and an aspiration line 208. In some
embodiments, power may be supplied to handpiece 204 through electrical cable 210 and flow through lines 206 and 208 may be controlled by a user (e.g., via footswitch 212) to perform a phacoemulsification procedure. One example of a handpiece for a phacoemulsification procedure is described in U.S. Patent Application Publication entitled "Ultrasound Handpiece," Publication No. 2006/0041220, Serial No. 11/183,591, by Mikhail Boukhny, James Y. Chon, and Ahmad Salehi filed July 18, 2005, which is hereby incorporated by reference in its entirety as though fully and completely set forth herein.

In some embodiments, the handpiece 204 may include at least one set of piezoelectric elements 227 polarized to produce longitudinal motion when excited at a relevant resonant frequency. As seen in FIG. 2b, the piezoelectric crystals 227 may be connected to an ultrasonic horn 216 to which a cutting tip 202 is attached. The horn 216 and/or the cutting tip 202 may include a plurality of diagonal slits or grooves 224. The slits or grooves 224 may produce torsional movement in the cutting tip 202 when the piezoelectric crystals are excited at a resonant frequency. Movement of the cutting tip 202 caused by the grooves 224 engaging fixed elements in the handpiece 204 may include a torsional rotational component relative to an axis of rotation collinear with a centerline of the horn 216.

In some embodiments, handpiece 204 may be coupled to a phacoemulsification cutting tip 202. As seen in FIG. 3a, the phacoemulsification cutting tip 202 may include a hook 310 located near angle 312 in a shaft 304 of the cutting tip 202. In some embodiments, the hook 310 may include a curve, a bump, or an elbow geometry that may act as a counterweight by placing tip material on an opposing side of the extended shaft centerline 316 than tip material angled away from the extended shaft centerline below angle 312. In some embodiments, the cutting tip may have a diameter in a range of approximately 0.5 mm to 2 mm (e.g., 1.5 mm). In some embodiments, the cutting tip may have a flared tip with a diameter at a top of the tip of approximately 1.5 mm and a diameter near a distal end of the tip of 0.5 mm.
(other diameters and configurations are also contemplated). In one embodiment, the cutting tip 202 may have a length of approximately 1 and 3/8 inches with a hook portion length of approximately 5/32 inches. Other dimensions are also contemplated. Hook 310 may act to move a center of rotation 306 to lie near (e.g., within a distance 314 of 0.25 * shaft diameter) or on extended shaft centerline 316. Other distances between the center of rotation 306 and the extended shaft centerline 316 are also contemplated (e.g., within a distance of 0.5 * shaft diameter, within a distance equal to the shaft diameter, etc). In some embodiments, motion of a top portion of the cutting tip 100 may be constrained due to its close proximity to the horn gripping the cutting tip 100 such that an axis of rotation of the top of the cutting tip 100 may lie along the extended shaft centerline 316 while a distal end of the cutting tip 100 (e.g., along approximately 10% of the bottom length of the cutting tip 100) may be distanced from the extended shaft centerline 316. In some embodiments, there may be a gradual displacement of the center of rotation 306 relative to the extended shaft centerline 316 from the top of the cutting tip 100 to the bottom of the cutting tip 100. As noted above, the hook 310 may effectively move the center of rotation 306 to lie near (e.g., within a distance 314 of 0.25 * shaft diameter) or on extended shaft centerline 316 at the bottom portion of the cutting tip 100.

The hook 310 may include various geometries of varying angle, length or depth of bend, etc. (e.g., see FIG. 3a and 6a-6c). The geometry of the hook 310 may also be configured to move a line through the center of mass of the tip and parallel to the extended shaft centerline of the cutting tip 202 closer to the extended shaft centerline 316 to reduce eccentric movement (including lateral vibrations) in the cutting tip 202 during rotational and/or longitudinal movements.

In some embodiments, the cutting tip 202 may be ultrasonically torsionally vibrated along a small arc (e.g., +/- 5 degrees). The torsional vibrations of cutting tip 202 may result in lateral motions in the shaft 304 and cutting tip 202. The whipping motion may include a side to side torsional motion of the cutting tip 202
perpendicular to the extended shaft centerline 316 (e.g., rotation around the y-axis as seen in FIG. 3a). In some embodiments, lateral vibrations (e.g., side to side along the x-axis or z-axis as seen in FIG. 3a) that result from the eccentrically weighted cutting tip and/or fluid resistance against the back and forth torsional rotation around the y-axis (e.g., cutting tip 100 in FIG. 1a) may be reduced through use of the hook 310 to balance the otherwise eccentrically weighted hook.

As seen in FIG. 4, in some embodiments, the cutting tip 202 may torsionally rotate back and forth through approximately a 10 degree arc (e.g., plus or minus 5 degrees off center (see middle diagram 2)). In some embodiments, the cutting tip 202 may rotate back and forth at a rate of approximately 31 kHz. Other arcs and rates are also contemplated. For example, an arc of plus or minus 20 degrees and/or a rate of 10-60 kHz may be used. The arc shown in FIG. 4 is exaggerated to show movement (i.e., the total arc shown is 180 degrees, whereas the cutting tip may have limited back and forth rotation on a 10 degree arc).

As seen in FIG. 5, when used to perform phacoemulsification, the ends of the cutting tip 202 and an irrigating sleeve 226 may be inserted into a small incision in the cornea 501, sclera 507, or other location in the eye tissue to gain access to, for example, the anterior chamber 503 of the eye 509. In various embodiments, a portion or all of the cutting tip 202 may be inside the irrigating sleeve 226. The cutting tip 202 may be ultrasonically torsionally vibrated along its longitudinal axis within the irrigating sleeve 226 by a crystal-driven ultrasonic horn 216, thereby emulsifying upon contact the selected tissue in situ. The hollow bore of the cutting tip 202 may communicate with the bore in the horn that in turn may communicate with the aspiration line from the handpiece 204 to the console 214 (e.g., see FIG. 2a). A reduced pressure or vacuum source in the console 214 may draw or aspirate the emulsified tissue from the eye 509 through an open end of the cutting tip 202, the bore of the cutting tip 202, the horn bore, and the aspiration line 208 and into a collection device. The aspiration of emulsified tissue may be aided by a saline
flushing solution or irrigant that may be injected into the surgical site through the small annular gap between the inside surface of the irrigating sleeve 226 and an outside surface of the cutting tip 202.

Cutting tip 202 may be made from stainless steel or titanium (other materials may also be used). Cutting tip 202 may have an overall length of between 0.50 inches and 1.50 inches (e.g., 1.20 inches). Other lengths are also contemplated. Cutting tip 202 may be formed using conventional metalworking technology and may be electropolished. Shaft 304 may be generally tubular, with an outside diameter of between 0.005 inches and 0.100 inches and an inside diameter of between 0.001 inches and 0.090 inches (other diameters are also contemplated).

Various modifications may be made to the presented embodiments by a person of ordinary skill in the art. Other embodiments of the present invention will also be apparent to those skilled in the art from consideration of the present specification and practice of the present invention disclosed herein. It is intended that the present specification and examples be considered as exemplary only with a true scope and spirit of the invention being indicated by the following claims and equivalents thereof.
WHAT IS CLAIMED IS:

1. A cutting tip for a surgical handpiece, comprising:
   a shaft;
   an angled portion coupled to the shaft;
   wherein the angled portion further comprises a hook; and
   wherein the shaft, angled portion, and hook are comprised in a single piece;
   wherein a distal portion of the cutting tip has an axis of rotation relative to the
   shaft that is substantially aligned with an extended shaft centerline.

2. The cutting tip as recited in claim 1, wherein substantially aligned comprises
   the axis of rotation being offset from the extended shaft centerline by a distance less
   than 0.25 * shaft diameter.

3. The cutting tip as recited in claim 1, wherein substantially aligned comprises
   the axis of rotation being offset from the extended shaft centerline by a distance less
   than 0.5 * shaft diameter.

4. The cutting tip of claim 1, wherein a shortest distance between the axis of
   rotation of the cutting tip without the hook and the extended shaft centerline would be
   greater than a shortest distance between the axis of rotation of the cutting tip with the
   hook and the extended shaft centerline.

5. The cutting tip of claim 1, wherein the cutting tip is configured to be vibrated
   torsionally back and forth at approximately plus 5 degrees to minus 5 degrees from
   center.

6. The cutting tip of claim 1,
   wherein the cutting tip is configured to be torsionally rotated back and forth
   about an axis that is parallel with an extended shaft centerline; and
wherein the third portion balances the cutting tip to reduce lateral vibrations back and forth perpendicular to the axis.

7. The cutting tip of claim 1, wherein substantially aligned with the extended shaft centerline includes parallel with the extended shaft centerline to 5 degrees off parallel with the extended shaft centerline.

8. The cutting tip of claim 1, wherein substantially aligned with the extended shaft centerline comprises a range of parallel with the extended shaft centerline to 10 degrees off parallel with the extended shaft centerline.

9. The cutting tip of claim 1, wherein the distal portion of the cutting tip is approximately 10% of a length of an end of the cutting tip farthest from the handpiece.

10. A cutting tip for a surgical handpiece, comprising:
  a first portion comprising a shaft;
  a second portion forming an angle with the first portion;
  a third portion forming a hook; and
  a distal end;
  wherein the first portion, second portion, third portion and distal end are comprised in a single piece;
  wherein the second portion, third portion, and distal end together have an axis of rotation relative to the shaft that is substantially aligned with the extended shaft centerline.

11. The cutting tip as recited in claim 10, wherein substantially aligned comprises the axis of rotation being offset from the extended shaft centerline by a distance less than 0.25 * shaft diameter.
12. The cutting tip as recited in claim 10, wherein substantially aligned comprises the axis of rotation being offset from the extended shaft centerline by a distance less than 0.5 * shaft diameter.

13. The cutting tip of claim 10, wherein a shortest distance between the axis of rotation of the cutting tip without the hook and the extended shaft centerline would be greater than a shortest distance between the axis of rotation of the cutting tip with the hook and the extended shaft centerline.

14. The cutting tip of claim 10, wherein the cutting tip is configured to be vibrated torsionally back and forth at approximately plus 5 degrees to minus 5 degrees from center.

15. The cutting tip of claim 10, wherein the cutting tip is configured to be torsionally rotated back and forth on an axis that is parallel with the extended shaft centerline; and wherein the third portion balances the cutting tip to reduce lateral vibrations back and forth perpendicular to the axis.

16. The cutting tip of claim 10, wherein substantially aligned comprises a range of parallel with the extended shaft centerline to 5 degrees off parallel with the extended shaft centerline.

17. The cutting tip of claim 10, wherein substantially aligned with the extended shaft centerline comprises a range of parallel with the extended shaft centerline to 10 degrees off parallel with the extended shaft centerline.

18. The cutting tip of claim 10, wherein the second portion, third portion, and distal end of the cutting tip are approximately 10% of a length of the cutting tip.
19. The cutting tip of claim 10, wherein the hook configuration changes directions at least three times relative to the extended shaft centerline.
**FIG. 1a**

Tip material on one side of extended centerline.

**FIG. 1b**
**FIG. 3a**

Tip material on one side of extended centerline

Tip material on opposing side of extended centerline

**FIG. 3b**
### A. CLASSIFICATION OF SUBJECT MATTER

INV. A61F9/007  
ADD. A61B17/32

According to International Patent Classification (IPC) or to both national classification and IPC

### B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

A61F   A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database consulted during the international search (name of data base and, where practical, search terms used)

**EPO-Internal, WPI Data**

### C. DOCUMENTS CONSIDERED TO BE RELEVANT

<table>
<thead>
<tr>
<th>Category</th>
<th>Citation of document, with indication, where appropriate, of the relevant passages</th>
<th>Relevant to claim No</th>
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</table>
| X        | US 2004/127887 A1 (ZINKEL JOHN L [US])  
1 July 2004 (2004-07-01)  
paragraph [0028]  
figure 7 | 1-3,7,  
10-12,  
16,17 |
| X        | US 6 458 143 B1 (SUGAI TOSHIYA [JP])  
1 October 2002 (2002-10-01)  
column 3, line 32 - column 4, line 18  
figure 1 | 1,4-6,9,  
10,  
13-15,  
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**X** Further documents are listed in the continuation of Box C  

**X** See patent family annex

1. Special categories of cited documents

   "A" document defining the general state of the art which is not considered to be of particular relevance
   "B" earlier document but published on or after the international filing date
   "L" document which may throw doubts on novelty claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
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   "P" document published prior to the international filing date but later than the priority date claimed

2. "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

3. "X" document of particular relevance, the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

4. "Y" document of particular relevance, the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

5. "S" document member of the same patent family

- **Date of the actual completion of the international search**: 7 September 2010
- **Date of mailing of the international search report**: 16/09/2010

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- **Authorised officer**: Grochol, Jana
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Form PCT/ISA/210 (patent family annex) (April 2005)