Processes for the recovery of ruthenium from materials containing ruthenium or ruthenium oxides or from ruthenium-containing noble metal ore concentrates, with the steps of:

A. the introduction of the material into a highly alkaline alkali hydroxide melt in the presence of nitrate as oxidising agent with the formation of an oxidised melt residue with water-soluble ruthenate (RuO₄)²⁻.

B. the dissolution of the oxidised melt residue obtained in water,

C. the addition of a reducing agent,

D. the precipitation of the metals formed, can also be used for separating off selenium.

Optionally, ruthenium is separated off by distillation, instead of precipitation, following step B, with the steps of:

5C the treatment of the ruthenate-containing solution with an oxidising agent,

5D distilling off of the RuO₄ obtained,

5E taking up of the RuO₄ from step 5D in hydrochloric acid.

By way of further subsequent purification steps, processes for the recovery of ruthenium targets are obtained.
PROCESSES FOR THE RECOVERY OF RUTHENIUM FROM MATERIALS CONTAINING RUTHENIUM OR RUTHENIUM OXIDES OR FROM RUTHENIUM-CONTAINING NOBLE METAL ORE CONCENTRATES

[0001] The invention relates to processes for the recovery of ruthenium from materials containing ruthenium or ruthenium oxides or from ruthenium-containing noble metal ore concentrates, if necessary with further purification steps for processing ruthenium targets.

STATE OF THE ART

[0002] Ruthenium-containing materials in which the ruthenium is present in the metallic or oxidic form (ore concentrates, target materials produced by powder metallurgy from ruthenium metal and ruthenium alloys, other cementates) need to be activated for further purification operations and converted into a water-soluble form.

[0003] Various processes are known for mobilising and/or separating off ruthenium:

[0004] melt flow with KOH/KNO₃ and subsequent formation of RuO₄ by the oxidation of the alkaline solution with chlorine gas (JP39019951; C. Claus, J. prakt. Chem. 79 [1860] 28),

[0005] oxidation and dissolution in HCl or HNO₃ with potassium chloride as oxidising agent (F. Krauss, Z. anorg. Ch. 117 [1921] 115),

[0006] exploiting the solubility in hypochlorite solution (Howe, JACS 47 [1925] 2928),


[0008] stressing ruthenium solutions in sequence with chloride and bromide (EP 1 114 795 A1),

[0009] heating ruthenium-containing hydrochloric acid noble metal solutions and subsequent addition of chloride and further heating of the suspension/solution formed to 80 to 90° C. and collection of the ruthenium tetroxide formed (U.S. Pat. No. 4,390,366),

[0010] Oxidation of alkali ruthenate in aqueous solutions (DE 39 35 798 A1) in the case of which the oxidation with ozone is carried out at pH values above 8. Alternatively, the ruthenium-containing noble metal solution present can be distilled with sodium chloride and/or chlorine gas.

OBJECT

[0011] Processes according to the state of the art have the following disadvantages: aqua regia or concentrated acids/chlorine gas used as oxidising agent do not dissolve ruthenium or only very slowly. Ruthenium is soluble in sodium hypochlorite liquor; however, volatile ruthenium(VIII) oxide is partly formed in this case directly. As a result, the digestion step cannot be separated from the separation step. The selenium contained in ore concentrates interferes with the purification of the noble metals in the further steps such that its rapid elimination, if possible at the beginning of the partitioning process, is desirable.

SUMMARY OF THE INVENTION

[0012] By introducing ruthenium-containing material and nitrate as oxidising agent into a highly alkaline potassium hydroxide melt, it is possible to achieve a satisfactory mobilisation of the ruthenium. Subsequently, ruthenium is present as water-soluble ruthenate (RuO₂⁺²). Subsequent partitioning operations permit a rapid removal of the ruthenium and the separation of selenium. Further subsequent purification steps permit the processing of ruthenium targets.

DETAILED DESCRIPTION

[0013] The invention relates to processes according to claims 1, 2, 5 and 9. Further advantageous characteristics can be found in the further claims.

[0014] Ruthenium contained in parting products is converted into the water-soluble ruthenate form by oxidation in an alkaline melt. As a result of the corrosivity of the melt, not every crucible material is suitable for this process. Crucibles consisting of a nickel base alloy with a high proportion of chromium such as e.g.

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have proved to be particularly suitable.

[0015] They exhibit a very low level of material abrasion.

[0016] A possible embodiment is a melt based on ore concentrate. Following the oxidation and dissolution of the cooled melt in water, the ruthenium obtained has dissolved to a level of >80%. Following filtration or siphoning off from the insoluble residue, the ruthenium can be easily precipitated by reduction (e.g. with ethanol) and separated off in this way. All noble metals, apart from ruthenium, are contained in the precipitate. During this process, selenium which may possibly be present and interferes strongly with the further purification steps of the other noble metals, is dissolved quantitatively as selenate and separated off together with ruthenium.

[0017] Apart from ethanol, other alcohols such as methanol, 1-propanol, 2-propanol or sugars such as e.g. glucose, are suitable as reducing agents.

[0018] In a further embodiment, ruthenium fines treated in a KOH melt with NaNO₃ are processed further by being leached with water, chlorine gas is introduced into the solution while the ruthenate is oxidised to ruthenium(VIII) oxide which is distilled off together with the gas stream and absorbed in concentrated hydrochloric acid.

[0019] The processes according to the invention have the following advantages:

[0020] Large proportions of the ruthenium content of parting products are activated and mobilised within a brief period, ruthenium being converted into a water-soluble form. For materials with a low ruthenium content, it is possible to
achieve an increase in the concentration of the ruthenium by subsequent alcohol precipitation. Subsequent purification operations then permit a rapid separation of further noble and non-ferrous metals contained in the parting products.

[0021] Osmium contained in ore concentrates follows the route of ruthenium as a result of its very similar chemical properties and can be easily partitioned from ruthenium by a further reaction step following the distillation described above (other digestion routes giving the noble metals in acid solution would lead to very high losses of osmium as a result of the easy formation and great volatility of osmium(VIII) oxide).

[0022] Following the dissolution, in water, of the melt obtained according to the invention from ore concentrate, ruthenium is usually present in solution to an amount of >80% and, following filtration or siphoning off from insoluble residue, can be precipitated easily by reduction (e.g. with ethanol) and thus separated off. Similarly, the selenium which has a strongly interfering effect in the further purification steps of the other noble metals is dissolved quantitatively as selenite and can thus be separated off easily from the noble metals contained in the precipitate. This provides an effective way of eliminating selenium by the formation of water-soluble selenates. These remain in solution if Ru (and, if applicable, Os) are precipitated with the reducing agent, e.g. ethanol.

[0023] The digestion according to the invention can advantageously be used for processing Ru targets. This includes further purification steps. The following process sequence is obtained, for example:

[0024] melt oxidising by alkaline oxidation with used targets;
[0025] dissolution in water;
[0026] distillation of RuO_4 using chlorine as oxidising agent;
[0027] absorption of RuO_4 in HCl;
[0028] concentration of the solution;
[0029] NH_4Cl precipitation;
[0030] calcination of the ammonium salt at approximately 600°C, e.g. in a chamber furnace;
[0031] rolling;
[0032] reduction under hydrogen;
[0033] grinding, e.g. in a fluid bed jet mill.

[0034] The invention thus also relates to processes for the recovery of ruthenium from ruthenium targets, the comminuted targets being passed directly to a melt undergoing alkaline oxidation as described above. The targets may contain substantial proportions of non-noble metals such as chromium.

[0035] The invention is elucidated further by way of the following examples. Parts and percentages relate to the weight, as they do in the remainder of the description, unless indicated otherwise.

EXAMPLE 1

[0036] In a crucible consisting of a nickel base alloy, 300 kg of potassium hydroxide are melted at 400-450°C. Once a clear melt has been formed, 100 kg of dried ore concentrate containing approximately 4.5% (w/w) of ruthenium—premixed with 75 kg of sodium nitrate—are slowly introduced into the melt with stirring. On completion of the addition, the temperature is increased to 600°C and stirring is carried out for a further 5 hours. The melt is allowed to cool before further treatment.

EXAMPLE 2

[0037] In a crucible consisting of a nickel base alloy, 300 kg of potassium hydroxide are melted at 400-450°C. Once a clear melt has been formed, 100 kg of oxide-containing ruthenium fines containing approximately 30-40% (w/w) of ruthenium premixed with 50 kg of sodium nitrate are slowly introduced into the melt with stirring. On completion of the addition, the temperature is increased to 600°C and stirring is carried out for a further 6 hours. The melt is allowed to cool before further treatment.

EXAMPLE 3

[0038] In a crucible consisting of a nickel base alloy, 275 kg of potassium hydroxide and 14 kg of sodium nitrate are melted at 400-450°C. Once a clear melt has been formed, 53 kg of metallic ruthenium fines containing approximately 98% (w/w) of ruthenium premixed with 41 kg of sodium nitrate are slowly introduced into the melt with stirring. On completion of the addition, the temperature is increased to 600°C and stirring is carried out for a further 6 hours. The melt is allowed to cool before further treatment.

EXAMPLE 4

[0039] A melt obtained according to example 1 is dissolved in 800 l of water and allowed to settle at room temperature. It is siphoned off and washed repeatedly with water, all the solutions being combined to give a total volume of approximately 1200 l. By adding 20 l of ethanol to the solution, ruthenium is precipitated as water-containing ruthenium(IV) oxide and can be filtered off via a suction filter. 25 kg of moist ruthenium(IV) oxide are obtained.

EXAMPLE 5

[0040] Analogous to example 3, 84 kg of sputter targets due for recycling and consisting of 70 kg ruthenium with 17% chromium are melted in a crucible with 400 kg of potassium hydroxide and 84 kg of sodium nitrate. After cooling, the melt is dissolved in 1600 l of water and, by introducing chloride gas, ruthenium(VI) oxide is distilled off and this is absorbed in concentrated hydrochloric acid. The absorber solution thus obtained contains 68.87 kg of ruthenium as pure ruthenium chloride solution.

1. Process for the recovery of ruthenium from materials containing ruthenium or ruthenium oxides or from ruthenium-containing noble metal ore concentrates with the steps of
   A. the introduction of the material into an alkaline hydroxide melt in the presence of nitrate as oxidising agent with the formation of an oxidised melt residue with water-soluble ruthenate (RuO_4)_2^-
   B. the dissolution, in water, of the oxidised melt residue obtained,
   C. the addition of a reducing agent,
   D. the precipitation of the metals formed.

2. Process for the separation of ruthenium from materials containing ruthenium or ruthenium oxides or from ruthenium-containing noble metal ore concentrates with the steps of
2A. the introduction of the material into an alkali hydroxide melt in the presence of nitrate as oxidising agent with the formation of an oxidised melt residue with watersoluble ruthenate (RuO₄)²⁺.

2B. the dissolution, in water, of the oxidised melt residue obtained; the solution subsequently contains ruthenate (RuO₄)²⁺ and selenate (SeO₄)²⁻.

2C. the addition of a reducing agent,

2D. the precipitation of water-containing ruthenium(IV) oxide, selenium being dissolved quantitatively in step 2B as selenate.

3. Process according to claim 1 or 2 characterised in that step 1A or 2A is carried out in an apparatus consisting of nickel base alloy.

4. Process according to claim 3, the nickel base alloy having a Cr content of at least 10% by wt.

5. Process for the recovery of ruthenium from materials containing ruthenium or ruthenium oxides and for the subsequent separation of ruthenium with the steps of

5A. the introduction of the material into an alkali hydroxide melt in the presence of nitrate as oxidising agent with the formation of water-soluble ruthenate (RuO₄)²⁺,

5B. the dissolution, in water, of the oxidised melt residue obtained to give a ruthenate-solution,

5C. the treatment of the ruthenate-containing solution with an oxidising agent,

5D. distilling off of the RuO₄ obtained,

5E. absorbing the RuO₄ from step 5D in hydrochloric acid.

6. Process according to claim 5, the materials containing ruthenium or ruthenium oxides being ruthenium targets.

7. Process according to one of the preceding claims, the alkali hydroxide melt being a KOH melt.

8. Process according to one of the preceding claims, the nitrate being NaNO₃.

9. Process according to claim 6 with the additional purification steps of

6F. the concentration of the hydrochloric acid solution,

6G. the precipitation of an ammonium ruthenate with NH₄Cl,

6H. the calcination of the ammonium ruthenate,

6I. rolling,

6J. reduction under hydrogen,

6K. grinding.

10. Process according to claim 9, step 6F taking place at 450-700°C.

11. Process according to claim 9, step 6F taking place at 600°C.