



(51) International Patent Classification:

G02F 1/377 (2006.01) G02B 6/293 (2006.01)

G02F 1/35 (2006.01) G02F 1/39 (2006.01)

G02F 1/37 (2006.01) G02F 1/21 (2006.01)

G02F 1/365 (2006.01) G02B 6/12 (2006.01)

UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

(21) International Application Number:

PCT/US2021/071723

(22) International Filing Date:

05 October 2021 (05.10.2021)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

63/088,220 06 October 2020 (06.10.2020) US

63/201,661 07 May 2021 (07.05.2021) US

63/201,664 07 May 2021 (07.05.2021) US

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(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DJ, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, IT, JO, JP, KE, KG, KH, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, WS, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ,

Published:

- with international search report (Art. 21(3))
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments (Rule 48.2(h))

(54) Title: OPTICAL WAVEGUIDE STRUCTURE WITH TRIPLE PARTIALLY OVERLAPPING LOOPS

(57) Abstract: A method, apparatus, and system for non-linear optical process. A first light (115) of a first wavelength (122) is routed in a first loop (142) in a main nonlinear optical waveguide (106). The first loop (142) has a first length (144) for the first light (115) of the first wavelength (122). A second light (124) of a second wavelength (126) is routed in a second loop (154) that includes portions of the main nonlinear optical waveguide (106) and a first extension optical waveguide (108). The second loop (154) has a second length (158) for the second light (124) of the second wavelength (126). A third light (128) of a third wavelength (130) is routed in a third loop (162) that include portions of the main nonlinear optical waveguide (106) and a second extension optical waveguide (110). The third loop (162) has a third length (164) for the third light (128) of the third wavelength (130).



**OPTICAL WAVEGUIDE STRUCTURE WITH TRIPLE PARTIALLY
OVERLAPPING LOOPS**

RELATED PROVISIONAL APPLICATION

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This application is related to and claims the benefit of priority of provisional U.S. Patent Application Serial No. 63/088,220, entitled "Directional Phase Matching (DPM) Optical Waveguide", filed on October 06, 2020, U.S. Patent Application Serial No. 63/201,661, entitled "Directional Phase Matching Optical Waveguide", filed on May 7, 2021, and U.S. Patent Application Serial No. 63/201,664, entitled "Nonlinear Optical Waveguide Structures for Light Generation and Conversion", filed on May 7, 2021, all of which are hereby incorporated by reference.

BACKGROUND INFORMATION

20 **1. Field:**

The present disclosure relates generally to optical waveguide structures and, in particular, to phase matching optical waveguide structures with partially overlapping loops to generate light using non-linear optical processes.

2. Background:

Optical waveguides are physical structures that guide electromagnetic waves in an optical spectrum. Optical waveguides can be used as components in integrated optical circuits. With respect to quantum communications and processing, nonlinear optical material structures can be used to create photon transmitters, repeaters, and other quantum devices for communications.

Nonlinear optical structures can be used to change the light passing through them depending on factors such as orientation, temperature, wavelength of light, polarization of light, and other factors. For example, a
5 waveguide with light of a blue wavelength passing through the waveguide can generate one or more photons of light that has a longer wavelength, such as green or red, and a correspondingly lower photon energy. This type of conversion can be performed using waveguides that
10 incorporate a material having a second order nonlinear optical susceptibility or a third order nonlinear optical susceptibility.

Current waveguides and structures that implement second order or third order nonlinear optical processes
15 are not as efficient as desired. Therefore, it would be desirable to have a method and apparatus that take into account at least some of the issues discussed above, as well as other possible issues. For example, it would be desirable to have a method and apparatus that overcome a
20 technical problem with increasing efficiency in generating light in nonlinear optical waveguide structures.

25

SUMMARY

An embodiment of the present disclosure provides an optical waveguide structure that comprises a main
5 nonlinear optical waveguide, a first extension optical waveguide, a second extension optical waveguide, a first wavelength selective optical coupler, and a second wavelength selective optical coupler. A first light of a first wavelength travels in a first loop that extends
10 through the main nonlinear optical waveguide. The first wavelength selective coupler couples the main nonlinear optical waveguide and the first extension optical waveguide to each other such that a second light of a second wavelength is coupled between the main nonlinear
15 optical waveguide and the first extension optical waveguide. The second light of the second wavelength travels in a second loop that extends through the main nonlinear optical waveguide and the first extension optical waveguide. The second loop has a second length
20 for the second light of the second wavelength. The second wavelength selective coupler couples the main nonlinear optical waveguide and the second extension optical waveguide to each other such a third light of a third wavelength is coupled between the main nonlinear
25 optical waveguide and the second extension optical waveguide. The third light of the third wavelength travels in a third loop that extends through the main nonlinear optical waveguide and the second extension optical waveguide. The third loop has a third length for
30 the third light of the third wavelength.

Another embodiment of the present disclosure provides an optical waveguide structure comprising a main nonlinear optical waveguide, an extension optical waveguide, and a wavelength selective coupler. A first

light of a first wavelength travels in a first loop that extends through the main nonlinear optical waveguide and the wavelength selective coupler, in which the first loop has a first length for the first light of the first
5 wavelength. The wavelength selective coupler couples a second light of a second wavelength between the main nonlinear optical waveguide and the extension nonlinear optical waveguide. The second light of the second wavelength travels in a second loop that extends through
10 the main nonlinear optical waveguide and the extension nonlinear optical waveguide, in which the second loop has a second length for the second light of the second wavelength.

Yet another embodiment of the present disclosure
15 provides a method for a non-linear optical process. A first light of a first wavelength is routed in a first loop that extends through a main nonlinear optical waveguide. The first loop has a first length for the first light of the first wavelength. A second light of a
20 second wavelength is routed in a second loop that extends through portions of the main nonlinear optical waveguide and a first extension optical waveguide, wherein the second loop has a second length for the second light of the second wavelength. A third light of a third
25 wavelength is routed in a third loop that extends through portions of the main nonlinear optical waveguide and a second extension optical waveguide, wherein the third loop has a third length for the third light of the third wavelength.

30 The features and functions can be achieved independently in various embodiments of the present disclosure or may be combined in yet other embodiments in which further details can be seen with reference to the following description and drawings.

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BRIEF DESCRIPTION OF THE DRAWINGS

The novel features believed characteristic of the illustrative embodiments are set forth in the appended
5 claims. The illustrative embodiments, however, as well as a preferred mode of use, further objectives and features thereof, will best be understood by reference to the following detailed description of an illustrative embodiment of the present disclosure when read in
10 conjunction with the accompanying drawings, wherein:
Figure 1 is an illustration of a block diagram of an optical waveguide structure in accordance with an illustrative embodiment;
Figure 2 is an illustration of a block diagram of a
15 configuration for nonlinear optical waveguides in accordance with an illustrative embodiment;
Figure 3 is an illustration of phase shifters used to obtain at least one of a resonance or roundtrip phase matching in accordance with an illustrative embodiment;
20 **Figure 4** is an illustration of a cross-section of an optical waveguide in accordance with an illustrative embodiment;
Figure 5 is an illustration of an optical waveguide structure with three optical waveguides in accordance
25 with an illustrative embodiment;
Figure 6 is an illustration of loops for light in an optical waveguide structure with three optical waveguides in accordance with an illustrative embodiment;
Figure 7 is an illustration of an optical waveguide
30 structure with three optical waveguides in accordance with an illustrative embodiment;
Figure 8 is an illustration of loops for light in an optical waveguide structure with three optical waveguides in accordance with an illustrative embodiment;

Figure 9 is an illustration of an optical waveguide structure with tuning electrodes in accordance with an illustrative embodiment;

Figure 10 is an illustration of an optical waveguide structure with wavelength selective couplers in accordance with an illustrative embodiment;

Figure 11 is an illustration of an optical waveguide structure with multiple sets of wavelength selective couplers for extension loops in accordance with an illustrative embodiment;

Figure 12 is an illustration of light coupling by a wavelength selective coupler in accordance with an illustrative embodiment;

Figure 13 is an illustration of light coupling by a wavelength selective coupler in accordance with an illustrative embodiment;

Figure 14 is an illustration of simulation results of light coupling by a wavelength selective coupler in accordance with an illustrative embodiment;

Figure 15 is an illustration of light coupling by a wavelength selective coupler in accordance with an illustrative embodiment;

Figure 16 is an illustration of simulation results of light coupling by a wavelength selective coupler in accordance with an illustrative embodiment;

Figure 17 is an illustration of a wavelength selective coupler in a form of a two-waveguide coupler in accordance with an illustrative embodiment;

Figure 18 is an illustration of a wavelength selective coupler in the form of a pulley coupler in accordance with an illustrative embodiment;

Figure 19 is an illustration of a wavelength selective coupler in the form of a 4-port micro-ring resonator coupler in accordance with an illustrative embodiment;

Figure 20 is an illustration of a wavelength selective coupler in the form of a multimode interference coupler in accordance with an illustrative embodiment;

Figure 21 is an illustration of a wavelength selective
5 coupler in the form of a Mach Zehnder interferometer comprising two multimode interference couplers connected to each other through two optical waveguide segments in accordance with an illustrative embodiment;

Figure 22 is an illustration of a flowchart of a process
10 for a nonlinear process in accordance with an illustrative embodiment;

Figure 23 is an illustration of a flowchart of a process for coupling the second light in accordance with an illustrative embodiment;

Figure 24 is an illustration of a flowchart of a process
15 for coupling the second light in accordance with an illustrative embodiment;

Figure 25 is an illustration of a flowchart of a process for applying activations to adjust a phase shift in a
20 first light in accordance with an illustrative embodiment;

Figure 26 is an illustration of a flowchart of a process for applying an activation to adjust a phase shift in a second light in accordance with an illustrative
25 embodiment;

Figure 27 is an illustration of a flowchart of a process for applying an activation to adjust a phase shift in a third light in accordance with an illustrative embodiment;

Figure 28 is an illustration of a flowchart of a process
30 for applying an activation to adjust a phase shift in light in accordance with an illustrative embodiment; and

Figure 29 is an illustration of a block diagram of a product management system in accordance with an illustrative embodiment.

DETAILED DESCRIPTION

The illustrative embodiments recognize and take into account one or more different considerations. For
5 example, the illustrative embodiments recognize and take into account that a nonlinear optical structure can function as a resonator such that a light of a particular wavelength in resonance with the resonator can travel over a longer distance in a nonlinear optical waveguide
10 of the nonlinear optical structure as compared to other light of other wavelengths that are not in resonance with the resonator.

The illustrative embodiments recognize and take into account that the loss of light from a resonator occurs
15 when the light exits the resonator instead of continuing to travel in the resonator. The resonator selects certain wavelengths of light to travel in the resonator. The illustrative embodiments recognize and take into account that different resonators can have different
20 resonances that match to different wavelengths of light. The illustrative embodiments recognize and take into account that the same resonator can have multiple resonances, with different resonances matching to different wavelengths of the light.

25 The illustrative embodiments recognize and take into account that currently used nonlinear optical waveguide structures employ a resonator that implements three-wave mixing and four-wave mixing processes to generate light. The illustrative embodiments recognize and take into
30 account that spontaneous parametric down conversion (SPDC) and spontaneous four-wave mixing (SFWM) are examples of three-wave mixing and four-wave mixing processes, respectively, for generating light, such as a signal light and an idler light, in response to the

introduction of source light, such as a pump light, into the nonlinear optical waveguide structure. The illustrative embodiments recognize and take into account that spontaneous parametric down conversion and
5 spontaneous four-wave mixing can generate a pair of photons, such as a signal photon and an idler photon, from one or more pump photons. Spontaneous parametric down conversion generates the signal and idler photons from a single pump photon. Spontaneous four-wave mixing
10 generates the signal photon and idler photon from two pump photons having the same wavelength.

The illustrative embodiments recognize and take into account that the nonlinear optical waveguide structure, in having a ring shape, can employ a nonlinear optical
15 waveguide in which light of three wavelengths involved in spontaneous parametric down conversion and spontaneous four-wave mixing propagates within the nonlinear optical waveguide structure. The illustrative embodiments recognize and take into account that the nonlinear
20 optical waveguide structure has a ring resonator with a closed path. The illustrative embodiments recognize and take into account that for current nonlinear optical waveguides structures, different wavelengths for the light must match resonances of the same resonator. The
25 illustrative embodiments recognize and take into account that this requirement results in severe limitation on allowable wavelengths for the signal light and the idler light that are generated.

The illustrative embodiments recognize and take into
30 account that current optical waveguide structures can have optical structures to input and output light from the ring resonator. The illustrative embodiments recognize and take into account that the addition of these input and output optical structures is unhelpful

for achieving the resonance match because the three wavelengths for the pump light, the signal light, and the idler light propagate through the ring resonator and are constrained to match the modes of the same ring resonator.

The illustrative embodiments recognize and take into account that current nonlinear optical waveguide structures can employ two ring resonators having different values for their circumferences. The illustrative embodiments recognize and take into account that these different values can result in different sets of resonance modes. The illustrative embodiments recognize and take into account that a first resonator can have all three wavelengths for the pump light, the signal light, and the idler light matched to the modes for the first resonator. The illustrative embodiments recognize and take into account that the second resonator can have modes matched to the wavelengths of the signal light and the idler light. The illustrative embodiments recognize and take into account that these two resonators still have the same limitations on resonance matching as a single ring resonator. The illustrative embodiments recognize and take into account that the use of three coupled ring resonators may provide some improvement, but still have limitations because at least some of the light from all of the three wavelengths travels through all three rings in the current nonlinear optical waveguide structure.

The illustrative embodiments recognize and take into account that current nonlinear optical waveguide structures employ multiple resonators that are coupled together directly through common wavelengths and not through a nonlinear optical process. The illustrative embodiments recognize and take into account that at least

some light for all of the wavelengths travel through all of the resonators. In other words, the illustrative embodiments recognize and take into account that the light with different wavelengths and traveling through all of the resonators in current nonlinear optical waveguide structures is resonant with each of the individual resonators that are coupled together. The optical waveguide structures in the illustrative examples are configured such that light of different wavelengths do not travel through all of the resonators. Instead, in the illustrative examples, the different wavelengths of light travel through different resonators.

In an illustrative example, the optical waveguide structure is configured such that each light of a particular wavelength can travel on a particular loop within the optical waveguide structure in which the loop is present for that particular light. In the illustrative examples, the loops are partially overlapping such that two different types of light of two different wavelengths are not required to travel along the same exact loop.

In one illustrative example, an optical waveguide structure comprises a main nonlinear optical waveguide, a first extension optical waveguide, a second extension optical waveguide, a first wavelength selective optical coupler, and a second wavelength selective optical coupler. A first loop in which a first light of a first wavelength travels extends through the main nonlinear optical waveguide, the first wavelength selective coupler and the second wavelength selective coupler. The first loop is a closed route in which the first light travels, forming a first resonator, and has a first length that is resonant for the first light of the first wavelength. In the illustrative example, a closed route is a route for

which a starting point and ending point are common or for which there is no distinct starting point that is separate from an ending point. The first wavelength selective coupler couples the main nonlinear optical waveguide and the first extension optical waveguide to each other such that a second light of a second wavelength is coupled between the main nonlinear optical waveguide and the first extension optical waveguide. The second light of the second wavelength travels in a second loop that extends through the main nonlinear optical waveguide, the second wavelength selective coupler, the first wavelength selective coupler, and the first extension optical waveguide. The second loop is a closed route, forming a second resonator, and has a second length that is resonant for the second light of the second wavelength. The second wavelength selective coupler couples the main nonlinear optical waveguide and the second extension optical waveguide to each other such that a third light of a third wavelength is coupled between the main nonlinear optical waveguide and the second extension optical waveguide. The third light of the third wavelength travels in a third loop that extends through the main nonlinear optical waveguide, the first wavelength selective coupler, the second wavelength selective coupler and the second extension optical waveguide. The third route has a closed route, forming a third resonator, and has a third length that is resonant for the third light of the third wavelength.

In the illustrative example, with this optical waveguide structure, the routes for the different lights of different wavelengths in the optical waveguides can have lengths that are selected such that at least one of resonance or round-trip phase matching is present for the

different lights of different wavelengths traveling on the different routes.

As used herein, the phrase "at least one of," when used with a list of items, means different combinations of one or more of the listed items can be used, and only one of each item in the list may be needed. In other words, "at least one of" means any combination of items and number of items may be used from the list, but not all of the items in the list are required. The item can be a particular object, a thing, or a category. For example, without limitation, "at least one of item A, item B, or item C" may include item A, item A and item B, or item B. This example also may include item A, item B, and item C or item B and item C. Of course, any combinations of these items can be present. In some illustrative examples, "at least one of" can be, for example, without limitation, two of item A; one of item B; and ten of item C; four of item B and seven of item C; or other suitable combinations.

In other words, the length can be selected for a loop such that resonance is achieved for the light traveling in a loop. This type of selection of the length can be made for each loop independently of the lengths for other loops in the optical waveguide structure. In the illustrative example, resonance occurs for each wavelength of the light separately from the other wavelengths of the light.

Round trip phase matching can be achieved for the combination of all three loops. Round trip phase matching involves all three wavelengths of the light. In the illustrative example, the lengths of all three loops are selected jointly such that round trip phase matching is achieved for the nonlinear optical interaction between the three wavelengths of the light.

In the illustrative example, an optical waveguide structure can be a resonator-enhanced structure for nonlinear optical (NLO) three-wave mixing processes. These nonlinear optical three-wave mixing processes can include difference frequency generation, sum frequency generation, and spontaneous parametric down conversion (SPDC). The optical structure can also be a resonator-enhanced structure for degenerately pumped or degenerate output nonlinear optical (NLO) four-wave mixing processes. These degenerate output nonlinear optical four-wave mixing processes can be, for example, difference frequency generation, sum frequency generation, and spontaneous four-wave mixing (SFWM). In this illustrative example, degenerate means at least two of the waves participating in the nonlinear optical process have the same wavelength. Further, a degenerate three-wave mixing process, such as second harmonic generation, can be used.

In the illustrative example, the nonlinear optical processes can involve three distinct wavelengths of light, a first wavelength, a second wavelength, and a third wavelength. The nonlinear optical waveguide structure in the different illustrative examples comprises triple partially overlapping loops for entanglement (TriPOLE). This optical waveguide structure comprises a main nonlinear optical waveguide, a first extension optical waveguide, a first wavelength selective coupler, a second extension optical waveguide, and a second wavelength selective coupler in which light of different wavelengths travels in loops that extend through different combinations of these different optical waveguides. A first loop extends through the main nonlinear optical waveguide. This first loop is overlapped by parts of two other loops, which are a

second loop and a third loop. The second loop extends through the main nonlinear optical waveguide and a first extension optical waveguide. The third loop extends through the main nonlinear optical waveguide and the
5 second extension optical waveguide. These loops can be closed routes that define optical resonators having resonances at specific sets of wavelengths.

The parts of the first loop, the second loop and the third loop that are in common with or that extend through
10 the main nonlinear optical waveguide in the optical waveguide structure are the portions of the optical waveguide structure in which the nonlinear optical three-wave mixing or four-wave mixing processes can occur. In the illustrative examples, the first extension optical
15 waveguide is physically separate from the main nonlinear optical waveguide and is connected to the main nonlinear optical waveguide by a first wavelength selective optical coupler that selectively couples only the second light of the second wavelength into that first extension optical
20 waveguide, but does not couple the first light of the first wavelength or the third light of the third wavelength into that first extension optical waveguide. In other words, the first wavelength selective optical coupler optically connects the first extension optical
25 waveguide to the main nonlinear optical waveguide.

In this illustrative example, the second extension optical waveguide is separate from the main nonlinear optical waveguide and is connected to the main nonlinear optical waveguide by a second wavelength selective
30 optical coupler that selectively couples the third light of the third wavelength into that second extension optical waveguide, but does not couple the first light of the first wavelength or the second light of the second wavelength into that second extension optical waveguide.

In other words, the second wavelength selective optical coupler optically connects the second extension optical waveguide to the main nonlinear optical waveguide.

The first light of the first wavelength travels in a

5 first loop that includes the main nonlinear optical waveguide. In this example, the first loop also can include the first wavelength selective coupler and the second wavelength selective coupler. The second light of the second wavelength light travels in a loop that

10 includes the main nonlinear optical waveguide and the first extension optical waveguide. The third wavelength of light travels in a third loop that includes the main nonlinear optical waveguide and the second extension optical waveguide. Each of the three loops has a length

15 that is designed to be resonant for the light that travels in the loop. The three loops can have different lengths.

The first wavelength selective optical coupler couples the second light of the second wavelength between

20 the main nonlinear optical waveguide and the first extension optical waveguide to travel in a second loop but does not couple light of the first or third wavelengths between the main nonlinear optical waveguide and the first extension optical waveguide. Likewise, the

25 second selective optical coupler couples the light of the third wavelength between the main nonlinear optical waveguide and the second extension optical waveguide to travel in a third loop but does not couple the light of the first or second wavelengths between the main

30 nonlinear optical waveguide and the second extension optical waveguide. Thus, only the second light of the second wavelength travels a second length through the entire second loop. Also, only the third light of the third wavelength travels a third length through the

entire third loop. The first light of the first wavelength travels only a first length through the first loop that includes the main nonlinear optical waveguide but does not include the first extension optical
5 waveguide or the second extension optical waveguide. The length of the first loop for the first light of the first wavelength can be selected such that the first light of the first wavelength is at a resonance of a first resonator comprising the main nonlinear optical
10 waveguide.

The length of the second loop for the second light of the second wavelength can be selected such that that second light of the second wavelength is at a resonance of a second resonator comprising the main nonlinear
15 optical waveguide and the first extension optical waveguide. The length of the third loop for the third light of the third wavelength can be selected so that the third light of the third wavelength is at a resonance of a third resonator formed by the main nonlinear optical
20 waveguide and the second extension nonlinear optical waveguide.

In the illustrative example, a loop may traverse one or more of these optical waveguides. The loops through these optical waveguides can partially overlap with each
25 other. In other words, the different loops are not identical to each other but may have overlaps within the optical waveguide structures.

Thus, although the propagation constants or wave vectors for the three wavelengths may be different from
30 each other, the light at the three different wavelengths can still be at resonances when propagating on their respective loops in the optical waveguide structure. The propagation can occur such that the light of the three wavelengths can propagate constructively over many cycles

through loops within the optical waveguide structure. This type of propagation can occur because the three loops have different lengths. Furthermore, the relative lengths of the three loops can be selected to meet the
5 phase-matching requirement to sustain the nonlinear optical process over an interaction distance that is greater than the circumference of the main nonlinear optical waveguide in the optical waveguide structure. The phase matching can be a feature distinct from the
10 resonance that occurs for a resonator in the optical waveguide structure. Thus, 5 constraints may be applied to the nonlinear optical interaction that occurs in the optical waveguide structure. One constraint is on "energy conservation" which constrains the relationship
15 between the 3 wavelengths. The other four constraints related to the propagation constants or wave vectors of the light of the 3 different wavelengths.

The phase-matching condition for the nonlinear optical process occurring in the main nonlinear optical
20 waveguide can be described by a phase walk-off and by a coherent interaction distance. The coherent interaction distance is the distance at which a phase walk-off for the nonlinear optical interaction between the light of the three wavelengths equals 180 degrees or π radians.
25 In some illustrative examples, the length of the main nonlinear optical waveguide, in which all three wavelengths travel, can be set to be no greater than the coherent interaction distance. This length of the main nonlinear optical waveguide can be the length of multiple
30 separate segments.

The length of the first extension optical waveguide and the length of the second extension optical waveguide can be set such that that the roundtrip phase walk-off for the nonlinear optical interaction between the light

of the three wavelengths is a specified value. This round-trip phase walk-off can be set equal to zero or as close to being zero as possible, or can be set as close as possible to being a multiple of 2π radians or 360
5 degrees.

In some examples, tuning electrodes can be located with optical waveguides. For example, the main nonlinear optical waveguide can have a set of tuning electrodes that operate to adjust the roundtrip phase of the light
10 of the first wavelength. The first extension optical waveguide can have a set of tuning electrodes that operates to adjust the roundtrip phase of the light of the second wavelength. The second extension optical waveguide can have a set of tuning electrodes that
15 operate to adjust the roundtrip phase of the light of the third wavelength. Thus, these tuning electrodes can enable adjusting the resonance conditions to compensate for changes in at least one of the wavelengths of the light, the cross-sectional dimensions of the optical
20 waveguides, and environmental conditions, such as temperature, or other factors. These tuning electrodes can also allow the optical waveguide structure to adjust the phase walk-off for the nonlinear optical interaction occurring in the main nonlinear optical waveguide.

25 In an illustrative example, the shortest wavelength of light involved in the nonlinear optical process can be the first light of the first wavelength. The next shortest wavelength of light involved in the nonlinear optical process can be the second light of the second
30 wavelength, and the longest wavelength of light involved in that nonlinear optical process can be the third light of the third wavelength.

For example, a structure for spontaneous parametric down conversion can have the light with the shortest

wavelength, the pump light, supplied to the main nonlinear optical waveguide through an input optical coupler and travel in the first loop. The optical coupler can be connected to an input optical waveguide that receives the pump light. The signal light and the idler light generated by the spontaneous parametric down conversion process would travel in the second loop and the third loop, respectively.

In another illustrative example, an optical waveguide structure that implements spontaneous four-wave mixing can have the pump light, whose frequency is intermediate between that of the generated light at the other wavelengths, supplied to the second loop through an additional optical coupler coupled to the first extension optical waveguide or coupled to the main nonlinear optical waveguide. The signal light generated by the spontaneous four-wave mixing process can travel through the main nonlinear optical waveguide and be coupled out of the waveguide structure through a first optical output coupler. The idler light generated by the spontaneous four-wave mixing process can travel in the third loop and can be coupled out of the optical waveguide structure through an additional, second, optical output coupler coupled to the second extension optical waveguide or coupled to the main nonlinear optical waveguide. These output optical couplers can be connected to output optical waveguides.

This optical waveguide structure can be a TriPOLE optical waveguide structure that is used in the illustrative examples to produce entangled photon pairs by nonlinear optical (NLO) processes. These nonlinear optical processes can be, for example, spontaneous parametric down conversion and spontaneous four-wave mixing. The two entangled photons produced by

spontaneous parametric down conversion can be entangled when those photons are produced from the same pump photon. In a similar fashion, the two entangled photons produced by spontaneous four-wave mixing can be entangled
5 when those photons are produced from the same two degenerate pump photons.

In this illustrative example, nonlinear optical waveguides in the form of ring resonators can be used to increase the generation rate of these entangled photon
10 pairs, comprising a signal photon and an idler photon. In a high-Q ring resonator, light can travel many times around the circumference of the ring resonator. Thus, the interaction length of a ring resonator can be many times greater than its physical size. In implementing
15 spontaneous parametric down conversion or spontaneous four-wave mixing with a ring resonator as currently used, all three wavelengths of light involved in the nonlinear optical process correspond to resonances of that resonator. For a resonator with high-Q, the allowable
20 amount that a wavelength can depart from the resonant condition and still be supported by the resonator can be smaller than desired.

Thus, with currently used spontaneous parametric down conversion or spontaneous four-wave mixing, all
25 three wavelengths involved in the nonlinear optical process are adjusted to match resonances of the ring. However, this type of adjustment of the wavelengths may not be possible if the entangled photon pairs are to be used in quantum photonic circuits that also contain other
30 sources of such photon pairs. The need in quantum photonics to perform optical interference functions involving photons produced by different sources of entangled photons may require those photons to have the

same wavelength, so that photons can be indistinguishable.

As a result, adjusting the wavelengths associated with a first ring resonator whose output photons are
5 involved in an optical interference function would impose a need to also adjust the wavelengths associated with a second ring resonator whose output photons are interfered with the photons from the first micro-ring resonator. However, if those two ring resonators are not identical,
10 such adjustment may be beyond what is permitted by the spectral width of the resonances of the two ring resonators.

For example, a departure of a dimension of the fabricated waveguide, such as the waveguide width, by
15 only 1-2 nm would shift the resonance wavelength beyond the spectral width associated with a quality factor or Q of 10^3 . Resonators with a higher Q have resonances with narrow spectral width, thereby making them impractical for use in quantum photonic circuits. Thus, if multiple
20 currently available ring resonators are used in a quantum photonic circuit, those resonators would need to have a low Q . As a result, the nonlinear optical interaction distance for producing the entangled photon pairs by spontaneous parametric down conversion or spontaneous
25 four-wave mixing would be much shorter and the photon-pair generation rates would be much lower.

The optical waveguide structure in the illustrative examples provides design flexibility to enable three loops through the waveguides to have resonances that
30 correspond to three pre-specified wavelengths. Also, if multiple optical waveguide structures are used together in a quantum photonic circuit, these optical waveguide structures can be adjusted to make resonances of the optical waveguide structures correspond to specified

wavelengths. This type of adjustment is in contrast to having all of the wavelengths adjusted to correspond to one resonator. Thus, the loops in the optical waveguide structures in a quantum photonic circuit can have a
5 higher Q , enabling those optical waveguide structures to generate photon pairs at higher generation rates. With reference now to the figures and, in particular, with reference to **Figure 1**, an illustration of a block diagram of an optical waveguide structure is depicted in
10 accordance with an illustrative embodiment. In this illustrative example, optical waveguide structure **100** comprises optical waveguides **102** in which at least one of optical waveguides **102** is comprised of nonlinear optical material **104**.

15 In this illustrative example, optical waveguides **102** comprise main nonlinear optical waveguide **106**, first extension optical waveguide **108**, and second extension optical waveguide **110**.

As depicted, main nonlinear optical waveguide **106** is
20 comprised of nonlinear optical material **104**. First extension optical waveguide **108** and second extension optical waveguide **110** can be comprised of nonlinear optical material **104**. In other words, in one illustrative example, first extension optical waveguide
25 **108** and second extension optical waveguide **110** are not constructed using nonlinear optical material **104**. In other illustrative examples, at least one of first extension optical waveguide **108** or second extension optical waveguide **110** can be constructed using nonlinear
30 optical material **104**.

In this illustrative example, optical waveguide structure **100** also comprises wavelength selective couplers such as first wavelength selective coupler **112** and second wavelength selective coupler **114**. These

wavelength selective couplers can selectively direct light **115** from one optical waveguide to another optical waveguide in optical waveguides **102**. In this example, first wavelength selective coupler **112** and second
5 wavelength selective coupler **114** can be selected from at least one of a two-waveguide coupler, a multi-mode interference coupler, a pulley coupler, a Mach-Zehnder interferometer, a 4-port micro-ring resonator coupler, or some other suitable wavelength selective coupler that can
10 couple light and determine which wavelengths of light are directed through coupling from one optical waveguide to another optical waveguide.

As depicted in this example, light **115** can comprise at least one of first light **120** having first wavelength
15 **122**, second light **124** having second wavelength **126**, or third light **128** having third wavelength **130**. In this particular example, first light **120**, second light **124**, and third light **128** can refer to a pump light, a signal light, and an idler light, but not necessarily in
20 any particular order. For example, first light **120** can also be the signal light, second light **124** can be the pump light, and third light **128** can be the idler light. As another example, first light **120** can also be the pump light, second light **124** can be the signal light, and
25 third light **128** can be the idler light.

In this illustrative example, optical waveguides **102** in optical waveguide structure **100** can support the propagation of light **115** through routes **131** in the form of loops **134**, which are closed routes. Light **115** travels
30 within optical waveguides **102** along routes **131**. In the illustrative example, a closed route is a route for which a starting point and ending point are common or for which there is no distinct starting point that is separate from

an ending point. The closed route is also referred to as a loop.

In this illustrative example, loops **134** can be triple partially overlapping loops for entanglement (TriPOLE) in which the loops overlap each other in portions of optical waveguides **102** in optical waveguide structure **100**. In other words, overlap is present between portions of loops **134** for the different wavelengths of light **115** traveling through optical waveguides **102**.

As depicted, wavelength selective couplers, such as first wavelength selective coupler **112** and second wavelength selective coupler **114**, can operate to produce different routes in routes **131** for the different wavelengths of light to have different lengths.

As depicted in this illustrative example, nonlinear optical material **104** has nonlinear coefficient **116**. In the illustrative example, nonlinear coefficient **116** can be a second order nonlinear coefficient or a third order nonlinear coefficient depending on the type of optical process implemented in optical waveguide structure **100**. Nonlinear polarization can occur in nonlinear optical material **104** in which the material polarization no longer varies linearly with the electric field amplitude. This nonlinear relationship can be expressed as follows:

$$P = \chi^{(1)}E + \chi^{(2)}EE + \chi^{(3)}EEE + \dots$$

where E is the electric field, $\chi^{(1)}$ is the linear optical susceptibility, $\chi^{(2)}$ is the second order nonlinear optical susceptibility, etc. The nonlinear susceptibilities, such as $\chi^{(2)}$ and $\chi^{(3)}$, represent the nonlinear parts of the material dipolar characteristics. In this example, the electric field amplitude is the electric field amplitude of the light wave, which is an electromagnetic field. An electromagnetic field has a

traveling (or propagating) electric field and a traveling (or propagating) magnetic field.

In this illustrative example, nonlinear optical process **132** can be nonlinear optical mixing processes that can occur within optical waveguide structure **100**. These nonlinear optical mixing processes can be used to generate light **115**. For example, the propagation of first light **120** can result in the generation of at least one of second light **124** or third light **128** using one or more nonlinear optical waveguides employing nonlinear optical mixing processes in optical waveguides **102**. In the illustrative example, nonlinear optical mixing processes can include nonlinear optical three-wave mixing processes and nonlinear optical four-wave mixing processes. In this illustrative example, the nonlinear optical three-wave mixing processes and the nonlinear optical four-wave mixing processes can include difference frequency generation (DFG) and sum frequency generation (SFG). The nonlinear optical three-wave mixing processes can also include spontaneous parametric down conversion (SPDC). The nonlinear optical four-wave mixing can also include spontaneous four-wave mixing (SFWM).

In this illustrative example, nonlinear optical wave-mixing processes can include three types of light with three distinct wavelengths such as first light **120** having first wavelength **122**, second light **124** having second wavelength **126**, and third light **128** having third wavelength **130**.

For example, nonlinear optical process **132** such as spontaneous four-wave mixing is a third order nonlinear optical process that can occur in main nonlinear optical waveguide **106**. In this process, a pair of output photons **172** is generated from a pair of input photons **174** in main nonlinear optical waveguide **106**. The pair of output

photons **172** have different wavelengths from each other and have the different wavelengths from a pair of input photons **174**.

In another illustrative example, nonlinear optical process **132**, such as a spontaneous parametric down conversion, is a second order nonlinear optical process that can occur in main nonlinear optical waveguide **106** in which a pair of output photons **172** is generated from an input photon in input photons **174**. In this example, the pair of output photons **172** can have different wavelengths from each other and have different wavelengths from the input photon in input photons **174**.

In another example, spontaneous four-wave mixing occurs can in main nonlinear optical waveguide **106** in which a pair of output photons **172** is generated from a pair of input photons **174**. The pair of output photons **172** have different wavelengths from each other and have the different wavelengths from the pair of input photons **174**.

In this illustrative example, light generation **133** can be improved for optical waveguide structure **100** using optical waveguides **102** with loops **134** through optical waveguides **102**. In the illustrative example, loops **134** are defined as the course of travel of light **115** within one or more of optical waveguides **102**. In other words, loops **134** are defined as where light **115** travels within optical waveguides **102**.

The manner in which optical waveguides **102** are coupled to each other through mechanisms such as first wavelength selective coupler **112** and second wavelength selective coupler **114** can be used to define loops **134** along which light **115** can travel. In the illustrative example, loops **134** can use different portions of optical waveguides **102** and wavelength selective couplers in

optical waveguide structure **100**. In this illustrative example, lengths **138** for loops **134** can be selected such that at least one of resonance matching **165** or roundtrip phase matching **166** is present for different wavelengths of light **115**.

In this illustrative example, "resonance matching" means a given wavelength is matched to a resonance of a resonator. A resonator can have many resonances. Also, a resonator can be designed such that different lengths can still produce resonance matching for a particular wavelength of light. Resonance is achieved every time the round-trip phase is a multiple of 2π .

In this illustrative example, first light **120** of first wavelength **122** travels in first loop **142** extending through main nonlinear optical waveguide **106** first wavelength selective coupler **112** and second wavelength selective coupler **114**, in which first loop **142** has first length **144** in lengths **138** that is resonant for first light of **120** of first wavelength **122**.

As depicted, first wavelength selective coupler **112** couples main nonlinear optical waveguide **106** and first extension optical waveguide **108** to each other such that second light **124** of second wavelength **126** is coupled between main nonlinear optical waveguide **106** and first extension optical waveguide **108**. Second light **124** of second wavelength **126** travels in second loop **154** in loops **134**, with second loop **154** extending through main nonlinear optical waveguide **106** and first extension optical waveguide **108**. In a depicted example, second loop **154** is a closed route, in which second loop **154** has second length **156** in lengths **138** that is resonant for second light **124** of second wavelength **126**.

In this illustrative example, second wavelength selective coupler **114** couples main nonlinear optical

waveguide **106** and second extension optical waveguide **110** to each other such that third light **128** of third wavelength **130** is coupled between main nonlinear optical waveguide **106** and second extension optical waveguide **110**.
5 Third light **128** of third wavelength **130** travels in third loop **162** in loops **134** extending through main nonlinear optical waveguide **106** and second extension optical waveguide **110** in which third loop **162** is a closed route and has third length **164** in lengths **138** that is resonant
10 for third light **128** of third wavelength **130**.

In this illustrative example, loops **134** extending through optical waveguides **102** are closed routes in routes **131**. These loops **134** can have a shape selected from at least one of a ring, a figure 8, a circle, an
15 oval, a racetrack, an irregular ring, or some other suitable shape.

In this illustrative example, loops **134** for different light in light **115**, such as first light **120**, second light **124**, and third light **128**, can have loops **134**
20 with different lengths in lengths **138**. For example, first length **144** for first loop **142**, second length **156** for second loop **154**, and third length **164** for third loop **162** can have different lengths in lengths **138** for loops **134**.

25 First loop **142**, second loop **154**, and third loop **162** are loops **134** that have lengths **138** selected to cause at least one of resonance matching **165** or roundtrip phase matching **166**. In other words, the length of each loop can be selected such that resonance matching **165** is
30 present, roundtrip phase matching **166** is present, or both resonance matching **165** and roundtrip phase matching **166** are obtained. The resonance in a loop can be matched to the wavelength of the light traveling in the loop in these examples.

For example, in optical waveguide structure **100**, first length **144** of first loop **142** can be selected such that resonance matching **165** is present for first light **120** of first wavelength **122**. As another example, in
5 optical waveguide structure **100**, second length **156** of second loop **154** can be selected such that resonance matching **165** is obtained for second light **124** of second wavelength **126**. As yet another example, in optical waveguide structure **100**, third length **164** of third loop
10 **162** can be selected such that resonance matching **165** is obtained for third light **128** of third wavelength **130**. Thus, the length of each loop can be selected to obtain resonance matching **165** for that loop and that wavelength. Multiple lengths can be selected for a given loop that
15 will result in resonance matching **165**.

When roundtrip phase matching **166** is present, a generation of photons for at least one of first light **120**, second light **124**, or third light **128** continues along a set of loops **134** selected from at least one of first
20 loop **142**, second loop **154**, or third loop **162** as travel distance increases for first light **120**, second light **124**, and third light **128** along the set of loops **134**. As depicted, optical waveguide structure **100** can also include a set of input optical waveguides **178** that
25 provides input light **180** to one or more of optical waveguides **102**. Optical waveguide structure **100** can also include a set of output optical waveguides **182** that emits output light **184** from one or more of the set of optical waveguides **102**. In one illustrative example, an input
30 optical waveguide in the set of input optical waveguides **178** can operate to provide input light **180** to one of main nonlinear optical waveguide **106**, first extension optical waveguide **108**, and second extension optical waveguide **110**. As another example, an output optical waveguide in

the set of output optical waveguides **182** can operate to emit output light **184** from one of main nonlinear optical waveguide **106**, first extension optical waveguide **108**, and second extension optical waveguide **110**.

5 In this illustrative example, a set of optical couplers **186** can couple input light **180** from the set of input optical waveguides **178** to one or more of optical waveguides **102**. A set of optical couplers **186** can also couple output light **184** from one or more of optical
10 waveguides **102** to the set of output optical waveguides **182**. Routes for light traveling through these optical couplers can also be part of a loop in some illustrative examples.

 In one illustrative example, an output optical
15 coupler in the set of optical couplers **186** can couple light **115** to an output optical waveguide in the set of output optical waveguides **182**. A first output optical coupler in the set of optical couplers **186** can have a configuration that results in a desired Q factor for
20 second loop **154** and a second output optical coupler in the set of optical couplers **186** can have a configuration that results in a desired Q factor for third loop **162**. In this example, the Q factor equals 2π times the number of oscillation periods of a light wave required for the
25 stored energy of that light wave in the resonator to decay to $1/e$ ($\approx 37\%$) of its initial value.

 Additionally, first loop **142**, second loop **154**, and third loop **162** are loops **134** that have lengths **138** that can be selected to cause roundtrip phase matching **166** in
30 which a generation of photons for at least one of first light **120**, second light **124**, or third light **128** continues along a set of loops **134**. In this example, the set of loops **134** is selected from at least one of first loop **142**, second loop **154**, or third loop **162** as for first

light **120**, second light **124**, and third light **128** in the set of loops **134**.

With reference next to **Figure 2**, an illustration of a block diagram of a configuration for nonlinear optical waveguides is depicted in accordance with an illustrative embodiment. In the illustrative examples, the same reference numeral may be used in more than one figure. This reuse of a reference numeral in different figures represents the same element in the different figures.

10 In illustrative example, at least one of resonance matching **165** or roundtrip phase matching **166** for optical waveguides **102** can be achieved through the selection of dimensions **202** for optical waveguides **102**. This selection of dimensions **202** can be made in addition to

15 the selection of lengths **138** in **Figure 1** for loops **134** in optical waveguides **102** to achieve at least one of resonance matching **165** or roundtrip phase matching **166** for optical waveguides **102**.

For example, main nonlinear optical waveguide **106**

20 can have cross-section **204** with dimensions **206** selected to achieve resonance condition **208** for first light **120** of first wavelength **122** traveling in main nonlinear optical waveguide **106**. As another example, first extension optical waveguide **108** can have first cross-section **210**

25 with first dimension **212** selected to achieve resonance condition **208** for second light **124** of second wavelength **126** traveling in first extension optical waveguide **108**. Further, second extension optical waveguide **110** can have second cross-section **214** with second dimension **216**

30 selected to achieve resonance condition **208** for third light **128** of third wavelength **130** traveling in second extension optical waveguide **110**.

With reference now to **Figure 3**, an illustration of phase shifters used to obtain at least one of a resonance

matching or roundtrip phase matching is depicted in accordance with an illustrative embodiment. At least one of manufacturing deviations from specifications, environmental factors, or other influences can affect whether resonance condition **208** is present during the operation of optical waveguide structure **100** in **Figure 1**. When roundtrip phase matching **166** is not present during operation of optical waveguide structure **100**, a set of phase shifters **300** can be used to adjust a set of phases **302** for light **115** propagating within optical waveguides **102**. In one illustrative example, the set of phase shifters **300** can be structures that are located adjacent to one or more of optical waveguides **102**; connected to one or more of optical waveguides **102**; include part of one or more of optical waveguides **102**; or a combination thereof.

The set of phase shifters **300** can operate to ensure a desired level of roundtrip phase matching **166** is achieved for light **115** that is generated within optical waveguides **102** in optical waveguide structure **100**. As depicted, light **115** can be generated in an optical waveguide in optical waveguides **102** that is comprised of nonlinear optical material **104** in **Figure 1**. In the illustrative example, main nonlinear optical waveguide **106** is comprised of nonlinear optical material **104**. Optionally, first extension optical waveguide **108** and second extension optical waveguide **110** can be comprised of nonlinear optical material **104**.

In one illustrative example, a set of phase shifters **300** can be connected to a set of optical waveguides **102** comprising at least one of main nonlinear optical waveguide **106**, first extension optical waveguide **108**, or second extension optical waveguide **110**. The set of phase shifters **300** can apply a set of activations **304** such that

a set of phases **302** in at least one of first light **120** of first wavelength **122**, second light **124** of second wavelength **126**, or third light **128** of third wavelength **130** changes in light **115** traveling in the set of optical waveguides **102** to which the set of activations **304** is applied.

In one illustrative example, the set of phase shifters **300** comprises a set of elements that can be located adjacent to a waveguide. The set of phase shifters **300** can take a number of different forms. For example, the set of phase shifters **300** can be selected from at least one of a tuning electrode, a thermal element, shape memory alloy element, piezo electric element, or some other element that can change the phase of a light particular wavelength propagating through the optical waveguide. These elements for the set of phase shifters **300** can be at least one of adjacent to part an optical waveguide, connected to part an optical waveguide, or include part an optical waveguide.

The set of activations **304** can take a number of different forms. For example, the set of activations **304** can be selected from at least one of a voltage, a current, a thermal energy, an electrically induced strain, or some other type of energy that can be applied to an optical waveguide to affect the manner in which light **115** propagates through the optical waveguide. In particular, the energy can be used to affect the phase of a light of the particular wavelength propagating through the optical waveguide.

In other words, the set of phase shifters **300** can selectively apply the set of activations **304** to adjust the phase for a particular wavelength of light **115** traveling within loops **134** and optical waveguides **102**. This adjustment can be made by applying the activations

304 using a particular phase shifter located adjacent to an optical waveguide in the set of optical waveguides **102** in a loop in loops **134** for a particular wavelength of light to maintain or reach resonance matching **165** for
5 that particular wavelength of light.

For example, when the set of phase shifters **300** is a set of tuning electrodes that apply a set of activations **304** as a set of voltages **314**, first phase shifter **308** in the set of phase shifters **300** can be first tuning
10 electrode **309** located adjacent to a portion of main nonlinear optical waveguide **106**. Second phase shifter **310** in the set of phase shifters **300** can be second tuning electrode **311** located adjacent to a portion of first extension optical waveguide **108**, and third phase shifter
15 **312** in the set of phase shifters **300** can be third tuning electrode **313** located adjacent to a portion of second extension optical waveguide **110**. First tuning electrode **309**, second tuning electrode **311**, and third tuning electrode **313** can apply the set of activations **304** in the
20 form of a set of voltages **314** to adjust the set of phases **302** in first light **120** of first wavelength **122**, second light **124** of second wavelength **126**, or third light **128** of third wavelength **130** traveling on a set of loops **134** through optical waveguides **102**. This shift in the set of
25 phases **302** can be made to maintain or reach resonance matching **165** for one or more of the wavelengths of light **115**, such as one or more of first light **120** of first wavelength **122**, second light **124** of second wavelength **126**, or third light **128** of third wavelength **130**.
30 In the illustrative example, when an optical waveguide in the set of optical waveguides **102** comprises an electro-optic material, the activation can take the form of a voltage. When the optical waveguide does not comprise an electro-optic material, other forms of energy such as,

for example, thermal energy, such as heat or strain, can be used as the set of activations **304**. In this illustrative example, heat can be generated by applying electrical current to a resistor that forms a phase shifter in the set of phase shifters **300** such that heat is generated. As another example, a voltage can be applied to a piezo electric element for phase shifter in the set of phase shifters **300** to change the dimensions of the tuning electrode to cause strain in the portion of the optical waveguide adjacent to the phase shifter in the set of phase shifters **300**.

The illustration of optical waveguide structure **100** in the different components in **Figures 1-3** is not meant to imply physical or architectural limitations to the manner in which an illustrative embodiment may be implemented. Other components in addition to or in place of the ones illustrated may be used. Some components may be unnecessary. Also, the blocks are presented to illustrate some functional components. One or more of these blocks may be combined, divided, or combined and divided into different blocks when implemented in an illustrative embodiment.

For example, optical waveguide structure **100** can include additional waveguides selected to provide additional flexibility selecting a desired length in lengths **138** for a loop in loops **134**. As another example, more than one nonlinear process can operate at the same time in optical waveguide structure **100**.

As another example, first wavelength selective coupler **112** can couple two portions of main nonlinear optical waveguide **106** to each other such that first light **120** is coupled from a first portion of main nonlinear optical waveguide **106** to a second portion of main nonlinear optical waveguide **106**. In yet another example,

second wavelength selective coupler **114** can couple two portions of main nonlinear optical waveguide **106** to each other such that first light **120** is coupled from the second portion of main nonlinear optical waveguide **106** to the first portion of main nonlinear optical waveguide **106**.

The set of phase shifters **300** are shown as separate functional blocks from optical waveguides **102**. The physical structures forming a phase shifter in the set of phase shifters **300** can also include a portion of the structure in a waveguide in optical waveguides **102**. With reference now to **Figure 4**, an illustration of a cross-section of an optical waveguide is depicted in accordance with an illustrative embodiment. In this illustrative example, waveguide **400** is shown in a cross-sectional view. This cross-section can be used in the optical waveguides in optical waveguide structure **100** in **Figure 1**.

As depicted, waveguide **400** comprises core region **402** and cladding region **404**. Core region **402** can be comprised of a material such as silicon nitride (Si_3N_4), silicon (Si) or silicon carbide (SiC) for optical processes based on four-wave mixing. Core region **402** can be comprised of a material such as lithium niobate (LiNbO_3), gallium phosphide (GaP), aluminum nitride (AlN) or silicon carbide (SiC) for optical processes based on three-wave mixing. Cladding region **404** is comprised of silicon dioxide (SiO_2) or other material whose refractive index is lower than the refractive index of the material comprising core region **402**. The particular material used in waveguide **400** can vary in other illustrative examples depending on the optical process used.

In this illustrative example, core region **402** has width w **406** and height tw **408**. Cladding region **404** has height tox **410**.

Waveguide **400** can achieve a phase matching condition
5 by adjusting the effective refractive indices (n_{eff}). The effective refractive indices can be adjusted through the selection of the material refractive index at a specific wavelength and varying the waveguide dimensions such as width w **406** and height tw **408**, and top oxide thickness,
10 height tox **410**.

The selection of at least one of the material and dimensions for waveguide **400** can be based on the conditions for momentum conservation and phase matching. In the illustrative example, momentum conservation **165** in
15 **Figure 1** is an automatic consequence of the nonlinear optical interaction. Whether the phase matching associated with the particular waveguide structure is consistent with momentum conservation **165** determines the degree of phase walk-off that results as the light
20 travels in the waveguide over some distance.

For example, an effective refractive index can be a function of the height and width of core region **402**. The coherence length is the propagation length at which the phase walk-off equals π radians. The coherence length is
25 inversely proportional to the phase mismatch. In an illustrative example, the length of the main nonlinear optical waveguide should be no larger than the coherence length that can be achieved for the main nonlinear optical waveguide. This constraint can be used when the
30 length of the loop in which the nonlinear optical interaction occurs is the main loop for the example described in **Figure 5** below.

Additionally, the cross-section shown for waveguide **400** is provided as an example and is not meant to limit

the manner in which other illustrative examples can implement cross-sections for waveguides. For example, waveguide **400** is shown with side **420** and side **422** that are angled. In other illustrative examples, these two
5 sides can be perpendicular rather than angled. As another example, other components may be present in this cross-section such as side regions that may be located adjacent to side **420** and side **422**. In yet another illustrative example, the cross-section of waveguide **400**
10 may also include a phase shifter such as a tuning electrode. As another example, waveguide **400** can include a second core region in addition to core region **402** when waveguide **400** is used to implement a two-waveguide optical coupler.

15 With reference to **Figure 5**, an illustration of an optical waveguide structure with three optical waveguides is depicted in accordance with an illustrative embodiment. In this illustrative example, optical waveguide structure **500** is an example of one
20 implementation for optical waveguide structure **100** shown in block form in **Figure 1**.

As depicted, optical waveguide structure **500** comprises optical waveguides in the form of main nonlinear optical waveguide **502**, first extension optical
25 waveguide **504**, and second extension optical waveguide **506**. As depicted, these optical waveguides in optical waveguide structure **500** have a racetrack shape. In this illustrative example, main nonlinear optical waveguide **502** is an example of main nonlinear optical waveguide
30 **106**; first extension optical waveguide **504** is an example of first extension optical waveguide **108**; and second extension optical waveguide **506** is an example of second extension optical waveguide **110** in **Figures 1-3**.

In this example, first extension optical waveguide **504**, and second extension optical waveguide **506** may or may not be nonlinear optical waveguides.

In this illustrative example, light can travel within
5 optical waveguide structure **500**. In this illustrative example, first light **508**, second light **510**, and third light **512**. First light **508** has the shortest wavelength in this example. In other words, first light **508** has the highest photon energy. Further, third light **512** as the
10 longest wavelength, meaning that third light **512** has the lowest photon energy. Second light **510** has an intermediate wavelength between first light **508** and third light **512**. In this example, second light **510** has an intermediate wavelength, meaning that second light **510**
15 has an intermediate photon energy.

In this illustrative example, optical waveguide structure **500** can operate to implement a third order nonlinear optical process such as spontaneous four-wave mixing (SFWM). In this example, for spontaneous four-
20 wave mixing with a degenerate pump light, pump photons in the pump light are for second light **510** having an intermediate wavelength with respect to the wavelengths of the photons for other lights in optical waveguide structure **500**. In this illustrative example, first light
25 **508** is a signal light and third light **512** is an idler light.

As depicted, the pump light, which is second light **510**, can be supplied to main nonlinear optical waveguide **502** through input optical waveguide **514**. Output optical
30 waveguide **516** emits the idler light, which is third light **512** in this example. Output optical waveguide **518** can emit the signal light, which is first light **508** in this example.

In this illustrative example, the pump light can be supplied to main nonlinear optical waveguide **502** from input optical waveguide **514** using optical coupler **520**. As depicted, the signal light can be coupled to output optical waveguide **518** from main nonlinear optical waveguide **502** using optical coupler **522** to be emitted as output light from output optical waveguide **518**. The idler light, third light **512**, can be coupled to output optical waveguide **516** from main nonlinear optical waveguide **502** using output optical coupler **524** to be emitted as output light from output optical waveguide **516**.

In this illustrative example, photons for the three types of light, first light **508**, second light **510**, and third light **512**, can travel on different routes through main nonlinear optical waveguide **502**, first extension optical waveguide **504**, and second extension optical waveguide **506** through wavelength selective coupler **526** and wavelength selective coupler **528**. These wavelength selected couplers can direct light of a particular wavelength from between a first optical waveguide and a second optical waveguide while other wavelengths of light are not directed between these two optical waveguides. These wavelength selective couplers can direct or couple light based on the wavelengths of the light.

For example, wavelength selective coupler **528** can couple second light **510** between main nonlinear optical waveguide **502** and first extension optical waveguide **504**. First light **508** and third light **512** are not directed between these two optical waveguides by wavelength selective coupler **528**. As another example, wavelength selective coupler **526** can couple third light **512** between main nonlinear optical waveguide **502** and second extension optical waveguide **506**. However, first light **508** and

second light **510** are not coupled between these two optical waveguides by wavelength selective coupler **526**. Turning next to **Figure 6**, an illustration of loops for light in an optical waveguide structure with three
5 optical waveguides is depicted in accordance with an illustrative embodiment. Photons for the three types of light having these three wavelengths travel through optical waveguide structure **500** through three different loops. In other words, the three loops traveled by the
10 three types of light can have partially overlapping portions and can also have portions that do not overlap. In the illustrative example, the photons for first light **508**, second light **510**, and third light **512** travel through loops that extend through the main nonlinear optical
15 waveguide **502**. In this illustrative example, each of the loops has a length. As depicted, main nonlinear optical waveguide **502** has a length L , first extension optical waveguide **504** has a length L_1 , and second extension optical waveguide **506** has a length L_2 .

20 As depicted, first light **508**, a signal light, travels along first loop **600**. In this example, first loop **600** is only located in main nonlinear optical waveguide **502** and has a length L_{L1} , which is the length of the path through main nonlinear optical waveguide **502** and
25 optical coupler **520**, optical coupler **522**, wavelength selective coupler **526**, and wavelength selective coupler **528** connected to the main nonlinear optical waveguide **502** if those couplers are distinct from the main nonlinear optical waveguide **502**. If the optical couplers are
30 assumed to have negligible length, the length of first loop **600** equals the length L of the main nonlinear optical waveguide **502**.

In this illustrative example, second loop **602** for second light **510**, a pump light, travels through main

nonlinear optical waveguide **502** and first extension optical waveguide **504**, as well as through optical coupler **520**, optical coupler **522**, wavelength selective coupler **526**, and wavelength selective coupler **528** if those
5 couplers are distinct from the optical waveguides. Second loop **602** has a "figure 8" shape. The length of second loop **602** includes the lengths of the main nonlinear optical waveguide **502** and first extension optical waveguide **504**, assuming one can neglect the
10 lengths of the optical couplers. As a result, the length of second loop **602** is $L+L_1$.

As shown in this figure, third loop **604** is for third light **512**, which is the idler light in this example. In this example, third loop **604** includes main nonlinear
15 optical waveguide **502** and second extension optical waveguide **506**, as well as through optical coupler **520**, optical coupler **522**, wavelength selective coupler **526**, and wavelength selective coupler **528** if those optical couplers are distinct from the optical waveguides. The
20 length of second loop **602** includes the lengths of the main nonlinear optical waveguide **502** and second extension optical waveguide **506**, assuming one can neglect the lengths of the optical couplers. Third loop **604** also has a "figure 8" shape and has a length $L+L_2$.

25 Including the two extension optical waveguides, first extension optical waveguide **504** and second extension optical waveguide **506**, with main nonlinear optical waveguide **502** enables mode resonance conditions for the three wavelengths for first light **508**, second
30 light **510**, and third light **512** to be achieved separately by adjusting the values for L , L_1 , and L_2 . As depicted, first loop **600** for first light **508** has length L , second loop **602** for second light **510** has length $L+L_1$, and third loop **604** for third light **512** has length $L+L_2$, assuming the

lengths of the optical couplers are sufficiently short such that those lengths do not need to be taken into account. These loops can be selected to provide resonance conditions for each of the three types of light
 5 having different wavelengths in a manner that is more flexible than current configurations.

Besides the mode resonance conditions for the three wavelengths, optical waveguide structure **500** also can satisfy the energy conservation condition and the
 10 momentum conservation condition for the nonlinear optical process. In degenerately pumped third order nonlinear parametric scattering such as spontaneous four-wave mixing (SFWM) can be implemented in optical waveguide structure **500**. With degenerate light, two photons can
 15 have the same wavelength. These two photons can be either input or output photons. For degenerately pumped spontaneous four-wave mixing, the two input photons involved in the four-wave mixing process have the same wavelength.

20 In this illustrative example of degenerately pumped spontaneous four-wave mixing (SFWM), the energy conservation condition is:

$$\frac{2}{\lambda_p} = \left(\frac{1}{\lambda_s} + \frac{1}{\lambda_i} \right)$$

and the momentum conservation condition is:

25
$$\frac{2n_p}{\lambda_p} = \left(\frac{n_s}{\lambda_s} + \frac{n_i}{\lambda_i} \right),$$

where n_p is the effective refractive index at the wavelength of the pump light, second light **510**; n_s is the effective refractive index at the wavelength of the signal light, first light **508**; n_i is the effective
 30 refractive index at the wavelength of the idler light, third light **512**; λ_p is the wavelength of the pump light, second light **510**; λ_s is the wavelength of the signal light,

first light **508**; and λ_i is the wavelength of the idler light, third light **512**.

These two conditions can be satisfied by a suitable selection of the transverse (or cross-sectional) profiles in the optical waveguides for at least one of main nonlinear optical waveguide **502**, first extension optical waveguide **504**, or second extension optical waveguide **506**. In this simplified illustrative example that neglects the effects of the optical couplers on the resonance matching and the phase matching, the nonlinear optical interaction takes place in main nonlinear optical waveguide **502**. Main nonlinear optical waveguide **502** is a nonlinear optical waveguide designed to achieve a phase matching condition. For optical waveguide structure **500**, the mode resonance conditions for the three wavelengths of light can be approximately described by $L + L_1 = m_p \lambda_p / n_{eff,p}$, $L = m_s \lambda_s / n_{eff,s}$, $L + L_2 = m_i \lambda_i / n_{eff,i}$, where m_p , m_s and m_i are integer numbers. These simplified expressions do not take into account the effects of the wavelength selective couplers and the phase of the light traveling through those couplers. With optical waveguide structure **500**, the resonance conditions are now not as restrictive as in the case of a single ring without extension optical waveguides and wavelength selective couplers. The length L of main nonlinear optical waveguide **502** can be selected to achieve the resonance condition for the signal wavelength. The length L_1 of first extension optical waveguide **504** for the pump photons in second light **510** can be selected to achieve the resonance condition for the pump wavelength.

Additionally, the length L_2 of second extension optical waveguide **506** for the idler photons in third light **512** can be selected to achieve the resonance condition for the idler wavelength λ_i .

In this depicted example, the optical waveguides in each of the extension optical waveguides can have electrodes that enable a bias voltage or other type of activation to be applied for electro optical tuning of the optical-phase shift that occurs in those extension optical waveguides. These additional adjustments can facilitate independent compensation of dimensional variations in the waveguide structure caused by fabrication inaccuracies.

Turning now to **Figure 7**, an illustration of an optical waveguide structure with three optical waveguides is depicted in accordance with an illustrative embodiment. In this illustrative example, optical waveguide structure **700** is an example of one implementation for optical waveguide structure **100** shown in block form in **Figure 1**.

As depicted, optical waveguide structure **700** comprises nonlinear optical waveguides in the form of main nonlinear optical waveguide **702**, signal extension optical waveguide **704**, and idler extension optical waveguide **706**. As depicted in this example, the optical waveguides in optical waveguide structure **700** have a racetrack shape. In this illustrative example, main nonlinear optical waveguide **702** is an example of main nonlinear optical waveguide **106**; signal extension optical waveguide **704** is an example of first extension optical waveguide **108**; and idler extension optical waveguide **706** is an example of second extension optical waveguide **110** respectively in **Figures 1-3**.

Additionally, optical waveguide structure **700** includes input optical waveguide **708**, output optical waveguide **710**, and output optical waveguide **712**. Further, input optical coupler **714**, output optical coupler **716**, and output optical coupler **718** are present.

Input optical coupler **714** couples pump light **724** from input optical waveguide **708** to main nonlinear optical waveguide **702**. Output optical coupler **718** couples signal light **726** from signal extension optical waveguide **704** to
5 output optical waveguide **712**. Output optical coupler **716** couples idler light **728** from idler extension optical waveguide **706** to output optical waveguide **710**.

In this illustrative example, pump light **724** has the shortest wavelength and idler light **728** has the longest
10 wavelength. Signal light **726** has an intermediate wavelength that is between the wavelength of pump light **724** and the wavelength of idler light **728**.

Additionally, signal wavelength selective coupler **720** and idler wavelength selective coupler **722** are present and
15 are wavelength selective couplers in optical waveguide structure **700**. In this illustrative example, signal wavelength selective coupler **720** can couple signal light **726** between main nonlinear optical waveguide **702** and signal extension optical waveguide **704**. Idler wavelength
20 selective coupler **722** can couple idler light **728** between main nonlinear optical waveguide **702** and idler extension optical waveguide **706**.

In this illustrative example, optical waveguide structure **700** can implement a second order nonlinear
25 optical process such as spontaneous parametric down conversion (SPDC). The three optical waveguides in optical waveguide structure **700** can define three partially overlapping loops for the light at the three wavelengths involved in the nonlinear optical process of
30 spontaneous parametric down conversion.

As depicted, signal wavelength selective coupler **720** can be designed to maximize the coupling of light at the wavelength of signal light **726** between main nonlinear optical waveguide **702** and signal extension optical

waveguide **704**. Signal wavelength selective coupler **720** can be designed to minimize the coupling of light at the pump wavelength for pump light **724** and the idler wavelength for idler light **728** between main nonlinear optical waveguide **702** and signal extension optical waveguide **704**. Instead, signal wavelength selective coupler **720** can be designed to maximize the coupling of light at the pump wavelength for pump light **724** and the idler wavelength for idler light **728** between a first portion of main nonlinear optical waveguide **702** and a second portion of main nonlinear optical waveguide **702**. In this illustrative example, idler wavelength selective coupler **722** can be designed to maximize the coupling of light at the idler wavelength for idler light **728** between main nonlinear optical waveguide **702** and idler extension optical waveguide **706**. Idler wavelength selective coupler **722** can minimize the coupling of light at the pump wavelength for pump light **724** and the signal wavelength for signal light **726**. Instead, idler wavelength selective coupler **722** can maximize the coupling of light at the pump wavelength for pump light **724** and the signal wavelength for signal light **726** between a second portion of main nonlinear optical waveguide **702** and a first portion of main nonlinear optical waveguide **702**.

Turning next to **Figure 8**, an illustration of loops for light in an optical waveguide structure with three optical waveguides is depicted in accordance with an illustrative embodiment. With this configuration of optical waveguide structure **700**, the photons for pump light **724**, signal light **726**, and idler light **728** can travel in different loops within optical waveguide structure **700**. These loops can be selected to obtain

desired propagation characteristics for pump light **724**, signal light **726**, and idler light **728**.

With the configuration of signal wavelength selective coupler **720** and idler wavelength selective coupler **722**,
5 pump light **724** travels in loop **800** having an oval shape or race-track shape only through main nonlinear optical waveguide **702** and does not travel through signal extension optical waveguide **704** and idler extension optical waveguide **706**. With this configuration, signal
10 light **726** travels in loop **804** having a "figure 8" shape through main nonlinear optical waveguide **702** and signal extension optical waveguide **704**. In this example, idler light **728** travels in loop **802** having a "figure 8" shape around main nonlinear optical waveguide **702** and idler
15 extension optical waveguide **706**.

Tuning electrodes (not shown in this figure) for thermal or electro-optic (E-O) tuning can be implemented on signal extension optical waveguide **704** and idler extension optical waveguide **706**. These tuning electrodes
20 (not shown) can also be used with main nonlinear optical waveguide **702**.

For a second order nonlinear optical parametric scattering process such as spontaneous parametric down conversion, energy conservation can be described by the
25 expression:

$$\frac{1}{\lambda_p} = \left(\frac{1}{\lambda_s} + \frac{1}{\lambda_i} \right),$$

where λ_p is the wavelength of pump light **724**; λ_s is the wavelength of signal light **726**; and λ_i is the wavelength of idler light **728**.

30 This energy-conservation condition constrains the wavelengths for pump light **724**, signal light **726**, and idler light **728**. In some examples, optical waveguide structure **700** can implement a nonlinear optical process

such as spontaneous parametric down conversion. This process can operate to generate a photon pair comprising one signal photon and one idler photon in a node of a quantum network. The signal and idler wavelengths can be
 5 determined by additional constraints imposed by the node and the network. Thus, the pump wavelength also can be determined, as constrained by the energy-conservation condition. The momentum conservation condition for the spontaneous parametric down conversion process can be
 10 described by the expression:

$$\frac{n_p}{\lambda_p} = \left(\frac{n_s}{\lambda_s} + \frac{n_i}{\lambda_i} \right),$$

where n_p is the effective refractive index at the wavelength of pump light **724**, n_s is the effective refractive index at the wavelength of signal light **726**,
 15 and n_i is the effective refractive index at the wavelength of idler light **728** for the wave-guided modes at the pump, signal, and idler wavelengths, respectively. In this expression, λ_p is the wavelength of pump light **724**; λ_s is the wavelength of signal light **726**; and λ_i is idler light
 20 **728**.

In some illustrative examples, the cross-sectional structure of the waveguide in main nonlinear optical waveguide **702** can be designed to achieve the momentum-conservation condition.

25 In a simplified illustrative example, the lengths of the optical waveguides in optical waveguide structure **700** can be selected to achieve resonance matching **165** or roundtrip phase matching **166**. This simplified example ignores the effects of the lengths of the wavelength
 30 selective couplers and the input and output couplers on the resonance matching or the round trip phase matching.

The length L of main nonlinear optical waveguide **702** can be selected to satisfy the resonance-mode condition:

$$L = \frac{m_p \lambda_p}{n_p},$$

where m_p is an integer value and represents the azimuthal mode number of the light at the pump wavelength that propagates in loop **800** extending through main nonlinear optical waveguide **702**; λ_p is the wavelength of pump light **724**; and n_p is the effective refractive index at the wavelength of pump light **724**.

The signal-loop extension can have a length L_s that is selected to satisfy the resonance-mode condition:

$$L_s = \frac{m_s \lambda_s}{n_s} - L,$$

where m_s is an integer value and represents the resonance-mode number of signal light **726** at the signal wavelength that propagates around loop **804** extending through main nonlinear optical waveguide **702**, signal wavelength selective coupler **720**, and signal extension optical waveguide **704**; λ_s is the wavelength of signal light **726**; n_s is the effective refractive index at the wavelength of signal light **726**; and L is the length of main nonlinear optical waveguide **702**. The idler-loop extension can have a length L_i that is selected to satisfy the resonance-mode condition:

$$L_i = \frac{m_i \lambda_i}{n_i} - L,$$

where m_i is an integer value and represents the resonance-mode number of idler light **728** at the idler wavelength that propagates around loop **802** extending through main nonlinear optical waveguide **702**, idler wavelength selective coupler **722**, and idler extension optical waveguide **706**; λ_i is the wavelength of idler light

728; n_i is the effective refractive index at the wavelength of idler light **728**; and L is the length of main nonlinear optical waveguide **702**.

With respect to the wavelength selective optical
5 couplers used in optical waveguide structure **100** in **Figure 1**, optical waveguide structure **500** in **Figure 5** and optical waveguide structure **700** in **Figure 7** can be configured to direct light between waveguides in the structures for selected wavelengths.

10 In one illustrative example, each of the two wavelength selective couplers in an optical waveguide structure can be designed to direct as close as possible to 100 percent of the light at the selected wavelength from the main nonlinear optical waveguide **702** into an
15 extension optical waveguide for that wavelength. The wavelength selective coupler can also be designed to direct as close as possible to zero percent of the light at the other two wavelengths into that extension optical waveguide, such that the light at the other two
20 wavelengths is directed to continue traveling in the main nonlinear optical waveguide **702**.

Additionally, each of those two wavelength selective couplers can be designed to direct as close to 100 percent of the light at the selected wavelength back from
25 the extension optical waveguide for that wavelength into the main nonlinear optical waveguide **702** after the light has propagated through the extension optical waveguide. As a result, the light of the selected wavelength can travel in a "figure 8" shaped loop through the
30 combination of main nonlinear optical waveguide **702** and the extension optical waveguide using the wavelength selective coupler.

In an illustrative example, the shortest wavelength λ_1 of the three wavelengths involved in a nonlinear

optical process remains in the main nonlinear optical waveguide. A first wavelength selective coupler selects the second longest wavelength λ_2 of the wavelengths involved in the nonlinear optical process for coupling
5 between the main nonlinear optical waveguide and the first extension optical waveguide which extends the route for light of that wavelength λ_2 . A second wavelength selective coupler selects the longest wavelength λ_3 of the wavelengths involved in the nonlinear optical process
10 for coupling between the main nonlinear optical waveguide and the second extension optical waveguide which extends the route for light of that wavelength λ_3 .

For example, in optical waveguide structure **700** in **Figure 7** and **Figure 8**, signal extension optical waveguide
15 **704** is located to the left side of main nonlinear optical waveguide **702** and extends the length of loop **804** for signal light **726**. As another example, in optical waveguide structure **500** in **Figure 5**, first extension optical waveguide **504** is shown as being above main
20 nonlinear optical waveguide **502** and extends second loop **602** in **Figure 6** for pump light **724**, which is second light **510** in **Figure 5**. In optical waveguide structure **700** in **Figure 7**, the loop extension path, idler extension optical waveguide **706**, is located to the right side of
25 main nonlinear optical waveguide **702** and extends the length of the loop for idler light **728** beyond the length provided by just main nonlinear optical waveguide **702**. For the example depicted in **Figure 5**, this loop extension path provided by second extension optical waveguide **506**
30 is located below main nonlinear optical waveguide **502** and extends the length of the loop for idler light **728**, which is third light **512** in **Figure 5**.

The first wavelength selective coupler is configured to selectively couple light of wavelength λ_2 between the main nonlinear optical waveguide and the first extension optical waveguide and to not couple light of wavelengths λ_1, λ_3 . The second wavelength selective coupler is configured to selectively couple light of wavelength λ_3 between the main nonlinear optical waveguide and the second extension optical waveguide and to not couple light of wavelengths λ_1, λ_2 . The first wavelength selective coupler and the second wavelength selective coupler can be selected from at least one of a two-waveguide coupler, a multi-mode interference coupler, a pulley coupler, a Mach-Zehnder interferometer, and a 4-port micro-optical waveguide resonator coupler.

In an illustrative example, the first wavelength selective coupler and the second wavelength selective coupler are implemented as two-guide couplers or directional couplers. For this example, the first wavelength selective coupler can be described by a coupling coefficient $\kappa_1(\lambda)$ and by a coupling distance d_1 . The parentheses in the expression for κ_1 indicates that the coupling coefficient is a function of a wavelength λ . The value of coupling coefficient κ_1 that applies for wavelength λ_1 is different from the value of κ_1 that applies for the other wavelengths λ_2 or λ_3 . The width of the two waveguide-core regions in a two-guide coupler and the gap between those two core regions can be designed to achieve relative values for $\kappa_1(\lambda_1)$, $\kappa_1(\lambda_2)$ and $\kappa_1(\lambda_3)$ that together with a selected value for the coupling distance d_1 can achieve transfer between the main nonlinear optical waveguide **702** and the first extension optical waveguide **704** for light of wavelength λ_2 and no or minimal

transfer for light of wavelengths λ_1 and λ_3 . For example, the following relations can be satisfied: $\kappa_1(\lambda_2) \cdot d_1 = \pi$, $\kappa_1(\lambda_3) \cdot d_1 = 2 \cdot N \cdot \pi$ and $\kappa_1(\lambda_1) \cdot d_1 \approx 0$.

In this illustrative example, the second wavelength selective coupler likewise can be described by a coupling distance d_2 and a coupling coefficient $\kappa_2(\lambda)$, with the coupling coefficient κ_2 being a function of a wavelength λ . The width of the two waveguide-core regions in a two-guide coupler and the gap between those two core regions can be designed to achieve relative values for $\kappa_2(\lambda_1)$, $\kappa_2(\lambda_2)$ and $\kappa_2(\lambda_3)$ that together with a selected value for the coupling distance d_2 can achieve transfer between the main nonlinear optical waveguide **702** and the second extension optical waveguide **706** for light of wavelength λ_3 and no or minimal transfer for light of wavelengths λ_1 and λ_2 . For example, the following relations can be satisfied: $\kappa_2(\lambda_3) \cdot d_2 = \pi$, $\kappa_2(\lambda_1) \cdot d_2 \approx 0$ and $\kappa_2(\lambda_2) \cdot d_2 \approx 0$.

For example, the first coupler, signal wavelength selective coupler **720** can selectively couple signal light **726** at 1130 nm from main nonlinear optical waveguide **702** to signal extension optical waveguide **704**. Minimal net coupling of idler light **728** at 1550 nm can occur. The second coupler, idler wavelength selective coupler **722**, can selectively couple idler light **728** at 1550 nm but minimally couples signal light **726** at 1130 nm.

For example, in simulations, photons for signal light **726** at 1130 nm can be coupled from main nonlinear optical waveguide **702** to signal extension optical waveguide **704** with 96 percent efficiency, and the photons for idler light **728** at 1550 nm can be coupled from main nonlinear optical waveguide **702** to signal extension optical waveguide **704** with lower than 0.1 percent efficiency. In simulations, the photons for idler light **728** at 1550 nm

can be coupled from main nonlinear optical waveguide **702** to idler extension optical waveguide **706** with 96 percent efficiency, and the photons for signal light **726** at 1130 nm can be coupled from main nonlinear optical waveguide
5 **702** to idler extension optical waveguide **706** with 0.1% efficiency.

In **Figure 9**, an illustration of an optical waveguide structure with tuning electrodes is depicted in accordance with an illustrative embodiment. In this
10 illustrative example, optical waveguide structure **900** is an example of an implementation of optical waveguide structure **100** shown in block form in **Figure 1**.

As depicted, optical waveguide structure **900** comprises main nonlinear optical waveguide **902**, signal extension
15 optical waveguide **904**, and idler extension optical waveguide **906**. In this illustrative example, main nonlinear optical waveguide **902**, signal extension optical waveguide **904**, and idler extension optical waveguide **906** have a racetrack shape. As depicted, optical waveguide
20 structure **900** also includes signal wavelength selective coupler **908** and idler wavelength selective coupler **910**.

In this illustrative example, optical waveguide structure **900** also includes pump input waveguide **912**, signal output optical waveguide **914**, and idler output optical waveguide
25 **916**. Input optical coupler **918** couples pump input waveguide **912** to main nonlinear optical waveguide **902**.

Output optical coupler **920** couples signal output waveguide **914** to signal extension optical waveguide **904**, and output optical coupler **922** couples idler output
30 waveguide **916** to idler extension optical waveguide **906**.

As depicted, different wavelengths of light can travel within optical waveguide structure **900**. In this example, pump light **924**, signal light **926**, and idler light **928** can travel in optical waveguide structure **900** along different

loops in which the loops have different lengths selected to increase momentum conversation in phase matching conditions for the nonlinear optical process in optical waveguide structure **900**.

5 Further, optical waveguide structural **900** can also include phase shifters such as tuning electrodes that can operate to shift the phase of at least one of pump light **924**, signal light **926**, or idler light **928**. As depicted, optical waveguide structure **900** includes main tuning
10 electrode **930**, signal tuning electrode **932**, and idler tuning electrode **934**. Main tuning electrode **930** is located adjacent to main nonlinear optical waveguide **902**. Signal tuning electrode **932** is located adjacent to signal extension optical waveguide **904**, and idler tuning
15 electrode **934** is located adjacent to idler extension optical waveguide **906**.

 In optical waveguide structure **900**, pump light **924** travels in a loop that includes main nonlinear optical waveguide **902** but that does not include signal extension
20 optical waveguide **904** or idler extension optical waveguide **906**. For example, pump light **924** travels in a clockwise direction within main nonlinear optical waveguide **902**.

 In this illustrative example, signal light **926**
25 travels in a "figure 8" shaped loop that includes main nonlinear optical waveguide **902** and signal extension optical waveguide **904**. In this example, signal light **926** travels in a clockwise direction in main nonlinear optical waveguide **902** and in a counterclockwise direction
30 in signal extension optical waveguide **904**.

 Idler light **928** travels in a "figure 8" shaped loop that includes main nonlinear optical waveguide **902** and idler extension optical waveguide **906**. Idler light **928** travels in a clockwise direction within main nonlinear

optical waveguide **902** and in a counterclockwise direction within idler extension optical waveguide **906**.

The loops traveled by pump light **924**, signal light **926**, and idler light **928** have different lengths in this
5 illustrative example. The lengths of these loops can be designed to increase at least one of efficiency in propagation or light generation in optical waveguide structure **900**.

As depicted, signal wavelength selective coupler **908**
10 is configured to be in a "through" state for wavelengths of pump light **924** and idler light **928**. With this selectiveness, pump light **924** and idler light **928** remain in main nonlinear optical waveguide **902** without being directed to signal extension optical waveguide **904**. In
15 this illustrative example, signal wavelength selective coupler **908** is configured to be in a "cross" or "drop" state for wavelength of signal light **926**. Thus, signal light **926** supplied to signal wavelength selective coupler **908** from main nonlinear optical waveguide **902** (lower
20 right port) is coupled to signal extension optical waveguide **904** (upper left port). Likewise, signal light **926** supplied from signal extension optical waveguide **904** (lower left port) is coupled to main nonlinear optical waveguide **902** (upper right port).

25 In a similar fashion, idler wavelength selective coupler **910** is configured to be in a "through" state for wavelengths of pump light **924** and signal light **926**. As a result, pump light **924** and signal light **926** remain in main nonlinear optical waveguide **902** when traveling by
30 idler wavelength selective coupler **910**. Idler wavelength selective coupler **910** is configured to be in a "cross" or "drop" state for the wavelength of idler light **928**. Thus, idler light **928** supplied to idler wavelength selective coupler **910** from main nonlinear optical

waveguide **902** (upper left portion) is coupled to idler extension optical waveguide **906** (lower right portion). Additionally, idler light **928** supplied from idler extension optical waveguide **906** (upper right portion) is
 5 coupled to main nonlinear optical waveguide **902** (lower left portion).

In this illustrative example, signal wavelength selective coupler **908** applies a phase shift of ϕ_{1p} , ϕ_{1i} to the "through" coupled light, pump light **924** and idler
 10 light **928**, respectively. Signal wavelength selective coupler **908** applies a phase shift of ϕ_{M1s} or ϕ_{1Ms} to the "cross" coupled light, signal light **926**. Idler wavelength selective coupler **910** applies a phase shift of ϕ_{2p} , ϕ_{2s} to the "through" coupled light, pump light **924** and
 15 signal light **926**, respectively. Idler wavelength selective coupler **910** applies a phase shift of ϕ_{M2i} or ϕ_{2Mi} to the "cross" coupled light, idler light **928**.

In this illustrative example, the tuning electrodes for main nonlinear optical waveguide **902**, signal extension
 20 optical waveguide **904**, and idler extension optical waveguide **906** can operate to add a phase shift to the light traveling through the portions of the structure with the tuning electrodes. For example, signal tuning electrode **932** for the signal-loop extension can add a
 25 phase shift of $\Delta\phi_{1Es}$ to signal light **926**. This phase shift can be a positive or negative value.

In this example, tuning electrode **930** in main nonlinear optical waveguide **902** can add phase shifts to $\Delta\phi_{MEp}$, $\Delta\phi_{MEs}$ and $\Delta\phi_{MEi}$ to pump light **924**, signal light **926**,
 30 and idler light **928**, respectively. These phase shifts can have a positive or negative value. The roundtrip phase shift for the pump light, is given by:

$$\phi_{Mp} + \phi_{1p} + \phi_{2p} + \Delta\phi_{MEp} , \text{ where } \phi_{Mp} = 2\pi n_{Mp} L_M / \lambda_p$$

The parameter n_{Mp} is the effective refractive index of the wave-guided pump light in main nonlinear optical waveguide **902** and L_M is the length of the portions of main nonlinear optical waveguide **902** that are not part of signal wavelength selective coupler **908** or idler wavelength selective coupler **910**.

In this illustrative example, pump light **924** only circulates within main nonlinear optical waveguide **902**. For pump light **924** to remain circulating for many roundtrips in main nonlinear optical waveguide **902**, the roundtrip phase shift should equal a multiple of 2π . This condition can be met by designing optical waveguide structure **900** to have suitable values for the length L_M and the effective refractive index n_{Mp} . The value for n_{Mp} is determined by the detailed cross-sectional structure of the waveguide comprising the main nonlinear optical waveguide **902**. This cross-section can be implemented using the cross-section shown for waveguide **400** in **Figure 4**.

Signal light **926** propagates in a loop having a "figure 8" shape. This loop includes main nonlinear optical waveguide **902**, signal wavelength selective coupler **908**, idler wavelength selective coupler **910**, and signal extension optical waveguide **904**. For signal light **926**, a roundtrip phase shift of signal light **926** traveling the entire loop is given by:

$$\phi_{Ms} + \Delta\phi_{MEs} + \phi_{M1s} + \phi_{1s} + \Delta\phi_{1Es} + \phi_{1Ms} ,$$

where $\phi_{Ms} = 2\pi n_{Ms} L_M / \lambda_s$ and n_{Ms} is the effective refractive index of the signal light **926** in main nonlinear optical waveguide **902** and L_M is the length of the portions of main nonlinear optical waveguide **902** that are not part of signal wavelength selective coupler **908** or idler

wavelength selective coupler **910**. Also, $\phi_{1s} = 2\pi n_{1s} L_1 / \lambda_s$ and n_{1s} is the effective refractive index of signal light **926** in signal extension optical waveguide **904** and L_1 is the length of the portion of signal extension optical waveguide **904** that is not part of signal wavelength selective coupler **908**.

For signal light **926** to remain circulating many roundtrips in the "figure 8" shaped loop, the roundtrip phase shift should equal a multiple of 2π . This condition can be met by designing optical waveguide structure **900** to have suitable values for the length L_1 and the effective refractive index n_{1s} . The value for n_{1s} is determined by the detailed cross-sectional structure of the waveguide comprising the signal-loop extension. The value for n_{Ms} is determined by the detailed cross-sectional structure of the waveguide comprising the main nonlinear optical waveguide **902**. Idler light **928** propagates in a loop having a "figure 8" shape. This loop includes main nonlinear optical waveguide **902**, signal wavelength selective coupler **908**, idler wavelength selective coupler **910**, and idler extension optical waveguide **906**. The roundtrip phase shift of idler light **928** is given by:

$$\phi_{Mi} + \Delta\phi_{MEi} + \phi_{M2i} + \phi_{2i} + \Delta\phi_{2Ei} + \phi_{2Mi},$$

where $\phi_{Mi} = 2\pi n_{Mi} L_M / \lambda_i$ and n_{Mi} is the effective refractive index of the wave-guided idler light **928** in main nonlinear optical waveguide **902** and L_M is the length of the portions of main nonlinear optical waveguide **902** that are not part of signal wavelength selective coupler **908** or idler wavelength selective coupler **910**. Also, $\phi_{2i} = 2\pi n_{2i} L_2 / \lambda_i$ and n_{2i} is the effective refractive index of signal light **926** in signal extension optical waveguide **904** and L_2 is the length of the portion of idler

extension optical waveguide **906** that is not part of idler wavelength selective coupler **910**.

For idler light **928** to remain circulating for many roundtrips in the "figure 8" shaped loop, the roundtrip
 5 phase shift should equal a multiple of 2π . This requirement can be met by designing optical waveguide structure **900** to have suitable values for the length L_2 and the effective refractive index n_{2i} . The value for n_{2i} is determined by the detailed cross-sectional
 10 structure of the waveguide comprising signal extension optical waveguide **904**. The value for n_{Mi} is determined by the detailed cross-sectional structure of waveguide comprising main nonlinear optical waveguide **902**.

It is desirable to increase the interaction distance
 15 over which the nonlinear optical process, such as spontaneous parametric down conversion, occurs coherently. Increasing the interaction distance can increase generation rate or efficiency of the signal and idler photons from the pump photons. Additionally, the
 20 round trip phase shifts for the pump light, signal light and idler light should match the momentum conservation condition of the nonlinear optical process. The condition includes the roundtrip phase shift of pump light **924** from its travel in main nonlinear optical
 25 waveguide **902**, the roundtrip phase shift of signal light **926** from its travel in its "figure 8" shaped loop, and the roundtrip phase shift of idler light **928** from its travel in its "figure 8" shaped loop. Thus:

$$\phi_{Mp} + \phi_{1p} + \phi_{2p} + \Delta\phi_{MEp} - (\phi_{Ms} + \Delta\phi_{MEs} + \phi_{M1s} + \phi_{1s} +$$

$$30 \quad \Delta\phi_{1Es} + \phi_{1Ms}) - (\phi_{Mi} + \Delta\phi_{MEi} + \phi_{M2i} + \phi_{2i} + \Delta\phi_{2Ei} + \phi_{2Mi}) = 0.$$

The adjustable phase shifts can be achieved by applying activations such as bias voltages using at least one of main tuning electrode **930**, signal tuning electrode **932**, or idler tuning electrode **934**. These electrodes depicted

for optical waveguide structure **900** can be used to adjust the roundtrip phase shifts for pump light **924** by adjusting $\Delta\phi_{MEp}$, signal light **926** by adjusting $\Delta\phi_{1Es}$, and idler light **928** by adjusting $\Delta\phi_{2Ei}$.

5 These in-situ adjustments to the phase of at least one of pump light **924**, signal light **926**, or idler light **928** can be used to correct or compensate for departures of the other parameters from as-designed values for optical waveguide structure **900** in an actually fabricated
10 and operating implementation of optical waveguide structure **900**.

The phase shift that can be obtained for a given electric field in the electro-optic material (due to a voltage applied to a set of electrodes) can be described
15 by the relation:

$$\Delta\phi_{Ej} = 2\pi r_j n_j^3 E \Gamma_j L_E / \lambda_j$$

where $j = p, s, i$ representing pump light **924**, signal light **926**, and idler light **928**, respectively. Other parameters in this expression are the electric field E ,
20 the electro-optic coefficient r_j , the effective refractive index n_j , the overlap of the optical field of pump light **924**, signal light **926**, or idler light **928** with the electro-optic material Γ_j , the electrode length (or electro-optic interaction distance) L_E , and the
25 wavelength λ_j of pump light **924**, signal light **928**, or idler light **928**. For an electro-optic material such as lithium niobate and for an electric field applied across the waveguide of 10^6 V/m, the electrode length needed to achieve a phase shift of 2π is about 3–10 mm.

30 As depicted, optical waveguide structure **900** includes input optical coupler **918** that supplies pump light **924**; output optical coupler **920** extracts some of signal light **926**; and output optical coupler **922** extracts

some of idler light **928**. As depicted, input optical coupler **918** for pump light **924** is coupled to main nonlinear optical waveguide **902**. Output optical coupler **920** for signal light **926** is coupled to signal extension optical waveguide **904**, and output optical coupler **922** for idler light **928** is coupled to idler extension optical waveguide **906**.

In some examples, input optical coupler **918** can be operated in a condition of critical coupling. In this critical coupling condition, as much of pump light **924** is coupled into main nonlinear optical waveguide **902** as is lost from main nonlinear optical waveguide **902**. The loss of pump light **924** can occur in main nonlinear optical waveguide **902** from conversion of the pump photons in pump light **924** into signal photons in signal light **926** and idler photons in idler light **928** through the nonlinear optical process. In the illustrative examples, output optical coupler **920** for signal light **926** can be operated in a condition that determines a desired value for the Q of the resonator for the signal wavelength for signal light **926**. In some examples, output optical coupler **922** for idler light **928** can be operated in a condition that determines a desired value for the Q of the resonator for the idler wavelength for idler light **928**.

Turning next to **Figure 10**, another illustration of an optical waveguide structure with wavelength selective couplers is depicted in accordance with an illustrative embodiment. In this illustrative example, optical waveguide structure **1000** is an example of an implementation of optical waveguide structure **100** shown in block form in **Figure 1**. In this illustrative example, optical waveguide structure **1000** implements spontaneous parametric down conversion.

As depicted, optical waveguide structure **1000** comprises main nonlinear optical waveguide **1002**, first extension optical waveguide **1004**, and second extension optical waveguide **1006**. In this illustrative example, 5 main nonlinear optical waveguide **1002**, first extension optical waveguide **1004**, and second extension optical waveguide **1006** have irregular elongate shapes. As depicted, optical waveguide structure **1000** also includes wavelength selective optical coupler **1008** and 10 wavelength selective coupler **1010**.

In this illustrative example, pump light **1022**, signal light **1024**, and idler light **1026** can travel within optical waveguide structure **1000**. Additionally, optical waveguide structure **1000** also includes pump input 15 waveguide **1028**, signal output waveguide **1030**, and idler output waveguide **1032**. In this illustrative example, input optical coupler **1034** can couple pump light **1022** from pump input waveguide **1028** to main nonlinear optical waveguide **1002**. Output optical coupler **1036** can couple 20 signal light **1024** from first extension optical waveguide **1004** to signal output waveguide **1030**, and output optical coupler **1038** can couple idler light **1026** from second extension optical waveguide **1006** to idler output optical waveguide **1032**.

25 In this illustrative example, optical waveguide structure **1000** also includes tuning electrode **1050**, and tuning electrode **1056**. These tuning electrodes can be used to adjust the phase of light traveling through the optical waveguides in optical waveguide structure **1000**. 30 For example, tuning electrode **1050** can adjust the phase of signal light **1024** traveling through first extension optical waveguide **1004**. In this illustrative example, tuning electrode **1056** adjusts the phase of idler light

1026 traveling through second extension optical waveguide **1006**.

In this illustrative example, optical waveguide structure **1000** also includes tuning electrode **1052** and
5 tuning electrode **1054**. These tuning electrodes can be used to adjust the wavelength selective coupling of light between the optical waveguides in optical waveguide structure **1000**. For example, tuning electrode **1052** can be used to adjust the coupling of signal light **1024**
10 between main nonlinear optical waveguide **1002** and first extension optical waveguide **1004** and the retention of pump light **1022** and idler light **1026** in main nonlinear optical waveguide **1002**. Also, tuning electrode **1054** can be used to adjust the coupling of idler light **1026**
15 between main nonlinear optical waveguide **1002** and second extension optical waveguide **1006** and the retention of pump light **1022** and idler light **1026** in main nonlinear optical waveguide **1002**.

With reference now to **Figure 11**, an illustration of
20 an optical waveguide structure with multiple sets of wavelength selective couplers for extension loops is depicted in accordance with an illustrative embodiment. In this illustrative example, optical waveguide structure **1100** is an example of an implementation of optical
25 waveguide structure **100** shown in block form in **Figure 1**. In this illustrative example, optical waveguide structure **1100** implements spontaneous parametric down conversion.

In this illustrative example, optical waveguide structure **1100** comprises a number of different optical
30 waveguides. As depicted, optical waveguide structure **1100** comprises main nonlinear optical waveguide **1102**, first inner extension optical waveguide **1104**, first outer extension optical waveguide **1106**, second inner extension

optical waveguide **1108**, and second outer extension optical waveguide **1110**.

These optical waveguides in optical waveguide structure **1100** have a rounded rectangle shape. In this illustrative example, main nonlinear optical waveguide **1102** is an example of main nonlinear optical waveguide **106**; first inner extension optical waveguide **1104** is an example of first extension optical waveguide **108**; and first outer extension optical waveguide **1106** is an example of second extension optical waveguide **110** in **Figures 1-3**. Also, second inner extension optical waveguide **1108** is an example of first extension optical waveguide **108**; and second outer extension optical waveguide **1110** is an example of second extension optical waveguide **110** in **Figures 1-3**.

In this illustrative example, light can travel within optical waveguide structure **1100**. In this illustrative example, light traveling within optical waveguide structure **1100** comprises pump light **1112**, signal light **1114**, and idler light **1116**. In this illustrative example, optical waveguide structure **1100** can operate to implement nonlinear optical processes than can generate photons. These nonlinear optical processes can be, for example, spontaneous parametric down conversion (SPDC) or spontaneous four-wave mixing (SFWM). In this illustrative example, pump light **1112** can be supplied to main nonlinear optical waveguide **1102** from pump input optical waveguide **1120** using input optical coupler **1121**. Pump light **1112** can be output from main nonlinear optical waveguide **1102** to pump output optical waveguide **1122** using output optical coupler **1123**. As depicted, signal output optical waveguide **1124** emits signal light **1114** in which signal light **1114** enters signal output optical waveguide **1124** from first inner

extension optical waveguide **1104** using output optical coupler **1125**. In this illustrative example, idler output optical waveguide **1126** outputs idler light **1116**.

In this example, idler output optical waveguide **1126**

5 emits idler light **1116** in which idler light **1116** enters idler output optical waveguide **1127** from second outer extension optical waveguide **1110** using output optical coupler **1127**. In this illustrative example, idler output optical waveguide **1126** outputs idler light **1116**.

10 In this illustrative example, photons for the three types of light, pump light **1112**, signal light **1114**, and idler light **1116**, can travel on different routes through main nonlinear optical waveguide **1102**, first inner extension optical waveguide **1104**, first outer extension
15 optical waveguide **1106**, second inner extension optical waveguide **1108**, and second outer extension optical waveguide **1110**.

Wavelength selected couplers, such as wavelength selective optical coupler **1130**, wavelength selective
20 optical coupler **1132**, wavelength selective optical coupler **1134**, and wavelength selective optical coupler **1136**, can direct light of a particular wavelength between a first optical waveguide and a second optical waveguide while other wavelengths of light are not directed between
25 these two optical waveguides. These wavelength selective couplers can direct or couple light based on the wavelengths of the light. As depicted in this example, wavelength selective coupler **1130** and wavelength selective optical coupler **1132** are different locations on
30 the opposite sides of main nonlinear optical waveguide **1102**. In other words, the locations are not symmetric or a mirror image of each other.

In this illustrative example, wavelength selective coupler **1130** can couple both signal light **1114** and idler

light **1116** between main nonlinear optical waveguide **1102** and first inner extension optical waveguide **1104**. In this example, wavelength selective optical coupler **1130** does not couple pump light **1112**.

5 As depicted, wavelength selective optical coupler **1134** can couple idler light **1116** between first inner extension optical waveguide **1104** and first outer extension optical waveguide **1106**. Wavelength selective optical coupler **1134** does not couple signal light **1114**.
10 As another example, wavelength selective optical coupler **1132** can couple signal light **1114** and idler light **1116** between main nonlinear optical waveguide **1102** and second inner extension optical waveguide **1108**. Wavelength selective optical coupler **1132** does not couple pump light
15 **1112**.

 In yet another example, wavelength selective optical coupler **1136** can couple idler light **1116** between second inner extension optical waveguide **1108** and second outer extension optical waveguide **1110**. In this particular
20 example, wavelength selective optical coupler **1136** does not couple signal light **1114**.

 In this depicted example, pump light **1112** travels along a loop in main nonlinear optical waveguide **1102**, which is the resonator for pump light **1112**. A signal
25 loop is present for signal light **1114** and comprises the combination of two inner extension loops, first inner extension optical waveguide **1104** and second inner extension optical waveguide **1108**, and main nonlinear optical waveguide **1102**. The idler loop for idler light
30 **1116** comprises the combination of main nonlinear optical waveguide **1102**, first inner extension optical waveguide **1104**, second inner extension optical waveguide **1108**, and the two outer extension loops, first outer extension

optical waveguide **1106** and second outer extension optical waveguide **1110**.

As depicted, optical waveguide structure **1100** can combine the nonlinear optical generation from a first
5 portion **1103** of main nonlinear optical waveguide **1102** ring that has one sign of the nonlinear optical coefficient with the nonlinear optical generation from a second portion **1105** of main nonlinear optical waveguide **1102** that has an opposite sign of the nonlinear optical
10 coefficient. First portion **1103** can be referred to as an upper portion and second portion **1105** can be referred to as a lower portion in this depicted illustration of optical waveguide structure **1100**.

In this illustrative example, the nonlinear optical
15 generation occurs mainly in first portion **1103** and in second portion **1105** of main nonlinear optical waveguide **1102**.

In this illustrative example, optical waveguide structure **1100** also includes tuning electrodes. As
20 depicted, tuning electrode **1150** and tuning electrode **1152** are located adjacent to main nonlinear optical waveguide **1102**. Tuning electrode **1154** and tuning electrode **1156** are located adjacent to first inner extension optical waveguide **1104**, and tuning electrode **1160** and tuning
25 electrode **1162** are located adjacent to first outer extension optical waveguide **1106**.

As depicted, tuning electrode **1164** and tuning electrode **1166** are located adjacent to second inner extension optical waveguide **1108**, and tuning electrode
30 **1168** and tuning electrode **1170** are located adjacent to second outer extension optical waveguide **1110**.

In this illustrative example, pump light **1112** travels in a first loop in a clockwise direction within main nonlinear optical waveguide **1102**. Signal light **1114**

travels in second loop in a counterclockwise direction within first inner extension optical waveguide **1104**, in a clockwise direction within main nonlinear optical waveguide **1102**, and in a counterclockwise direction within second inner extension optical waveguide **1108**. In this example, idler light **1116** travels in a third loop that is clockwise in first outer extension optical waveguide **1106**, counterclockwise within first inner extension optical waveguide **1104**, clockwise direction within main nonlinear optical waveguide **1102**, counterclockwise within second inner extension optical waveguide **1108**, and clockwise within second outer extension optical waveguide **1110**.

In **Figure 11**, some of the wavelength selective couplers in optical waveguide structure **1100** are not connected directly to main nonlinear optical waveguide **1102**. For example, wavelength selective optical coupler **1134** is connected between first inner extension optical waveguide **1104** and first outer extension optical waveguide **1106**. As another example, wavelength selective optical coupler **1136** is connected between second inner extension optical waveguide **1108** and second outer extension optical waveguide **1110**.

With reference to **Figure 12**, an illustration of light coupling by a wavelength selective coupler is depicted in accordance with an illustrative embodiment. In this illustrative example, signal light **1202** and idler light **1204** travel through optical waveguide **1206** and are input into wavelength selective coupler **1208**. As depicted, at the output of wavelength selective coupler **1208**, idler light **1204** continues through optical waveguide **1206** and signal light **1202** crosses over to optical waveguide **1210**.

This crossover of signal light **1202** is caused by the design of wavelength selective coupler **1208**. In illustrative examples, wavelength selective coupler **1208** can be used for signal wavelength selective coupler **720** in optical waveguide structure **700** to selectively couple signal light **726** from main nonlinear optical waveguide **702** to signal extension optical waveguide **704** in **Figure 7**. Wavelength selective coupler **1208** can also be used for signal wavelength selective coupler **908** in optical waveguide structure **900** to selectively couple signal light **926** from main nonlinear optical waveguide **902** to signal extension optical waveguide **904**.

With reference next to **Figure 13**, an illustration of light coupling by a wavelength selective coupler is depicted in accordance with an illustrative embodiment. In this illustrative example, pump light **1302**, signal light **1304**, and idler light **1306** travel through optical waveguide **1308** into wavelength selective optical coupler **1310**. Pump light **1312** also travels through optical waveguide **1314** and is input into wavelength selective optical coupler **1310**.

As depicted, at the output of wavelength selective optical coupler **1310**, signal light **1304** and idler light **1306** continue to travel through optical waveguide **1308**. Pump light **1302** traveling into wavelength selective optical coupler **1310** from optical waveguide **1308** crosses over to optical waveguide **1314** at the output of wavelength selective optical coupler **1310**. In a similar fashion, pump light **1312** traveling through optical waveguide **1314** into wavelength selective optical coupler **1310** crosses over to optical waveguide **1308** at the output of wavelength selective optical coupler **1310**. Wavelength selective optical coupler **1310** is illustrative example of input optical coupler **714** of optical waveguide structure

700 in **Figure 7** or input optical coupler **918** for optical waveguide structure **900** in **Figure 9**. Wavelength selective optical coupler **1310** also is illustrative of input optical coupler **1121** and output optical coupler **1123** for optical waveguide structure **1100** in **Figure 11**.

In **Figure 14**, an illustration of simulation results of light coupling by a wavelength selective coupler is depicted in accordance with an illustrative embodiment. As depicted, simulation results **1400** comprises plots for signal extraction plot **1402** and idler retention plot **1404**. Simulation results **1400** are plots of the optical-field distributions for a signal light and an idler light having different wavelengths from each other. Simulation results **1400** are generated using a wavelength selective coupler such as wavelength selective coupler **1208** in **Figure 12**. This wavelength selective coupler can be as a two-waveguide coupler. In this illustrative example, simulation results **1400** are for a first light, signal light **1202**, that is coupled and exits from the "cross" output of wavelength selective coupler **1208** has a larger guided-mode effective index of refraction n_{eff} and is confined more strongly than the second light, idler light **1204**, that exits from the "through" output of wavelength selective coupler **1208**.

As depicted, signal extraction plot **1402** depicts the electric-field magnitude of the signal light **1202**. Plot **1402** has x-axis **1406** that represents the longitudinal direction of the two-guide wavelength selective coupler structure and y axis **1408** that represents the transverse direction of the two-guide wavelength selective coupler structure. Signal extraction plot **1402** in simulation results **1400** shows that signal light **1202** is coupled from the lower left waveguide to the upper right waveguide.

In this illustrative example, idler retention plot **1404** depicts the electric-field magnitude of the idler light **1204**. Plot **1404** has x-axis **1410** that represents the longitudinal direction of the two-guide wavelength selective coupler structure and y axis **1412** that represents the transverse direction of the two-guide wavelength selective coupler structure. As depicted, idler retention plot **1404** shows that the idler light **1204** couples from the lower waveguide to the upper waveguide in a few portions of the coupling region but eventually remains in the lower waveguide away from that coupling section.

In this example, these simulation results can be obtained using a wavelength selective coupler that comprises two curved waveguides that are coupled by a section of straight waveguide of a length and a gap for wavelength selective coupler that are selected to result in the coupling of the signal light from a first optical waveguide to a second optical waveguide when passing through the wavelength selective coupler.

Thus, if light of both signal light **1202** and idler light **1204** are supplied to wavelength selective coupler **1208** through optical waveguide **1206**, signal light **1202** exits wavelength selective coupler **1208** via optical waveguide **1210** and idler light **1204** exits wavelength selective coupler **1208** via optical waveguide **1206**. For this example, an example length $d_{s|i}$ for the coupling section for wavelength selective coupler **1208** can be described by the following relation: $\kappa_{s|i}(\lambda_s) \cdot d_{s|i} = \pi$, where $\kappa_{s|i}$ is the coupling coefficient. To achieve the desired wavelength selectivity, wavelength selective coupler **1208** can also be constrained by another relation: $\kappa_{s|i}(\lambda_l) \cdot d_{s|i} = 2 \cdot \pi \cdot X$, where λ_l is the longer wavelength and X is an

integer. In the illustrative example, the value of X is 2, such that the photons of wavelength λ_s have 100% coupling between the two waveguides being coupled, while the photons of wavelength λ_i are coupled back again to the starting waveguide.

Turning to **Figure 15**, an illustration of light coupling by a wavelength selective coupler is depicted in accordance with an illustrative embodiment. In this illustrative example, pump light **1502**, signal light **1504**, and idler light **1506** travel through optical waveguide **1508** and are input into wavelength selective coupler **1510**. As depicted, at the output of wavelength selective coupler **1510**, pump light **1502** continues through optical waveguide **1508**. In this example, signal light **1504** and idler light **1506** cross over to optical waveguide **1512** at the output of wavelength selective coupler **1510**. Wavelength selective coupler **1510** is an illustration of an implementation for of wavelength selective coupler **1130** and wavelength selective optical coupler **1132** in optical waveguide structure **1100** in Figure 11.

With reference now to **Figure 16**, an illustration of simulation results of light coupling by a wavelength selective coupler is depicted in accordance with an illustrative embodiment. Simulation results **1600** comprise plots that illustrate light coupling using a wavelength selective coupler such as a two-waveguide coupler.

As depicted, simulation results **1600** are for pump light in pump plot **1602**, signal light in signal plot **1604**, and idler light in idler plot **1606**. These simulation results are plots of the electric field magnitude distributions of light at the pump, signal and idler wavelengths. Pump plot **1602** is a plot for field magnitude distribution in linear scale. As depicted,

pump plot **1602** has x-axis **1618** that represents the longitudinal direction of the two-guide wavelength selective coupler structure and y axis **1608** that represents the transverse direction of the two-guide wavelength selective coupler structure.

In this illustrative example, Signal plot **1604** and idler plot **1606** are plots for the signal and idler field magnitude distributions in a logarithmic scale. As depicted, signal plot **1604** has x-axis **1610** that represents the longitudinal direction of the two-guide wavelength selective coupler structure and y axis **1612** that represents the transverse direction of the two-guide wavelength selective coupler structure. Idler plot **1606** has x-axis **1614** that represents the longitudinal direction of the two-guide wavelength selective coupler structure and y axis **1616** that represents the transverse direction of the two-guide wavelength selective coupler structure.

In this depicted example, the optical waveguide at the lower portion of the plots for simulation results **1600** has a smaller radius of curvature than the optical waveguide at the upper portion of those plots. The light travels from left to right in these plots for simulation results **1600**. Pump light enters in the upper guide from the upper left of pump plot **1602**. Signal light and idler light enter in the lower, curved guide from the lower left of signal plot **1604** and idler plot **1606**.

In this example, the pump light experiences primarily the "cross" state of this coupler and is coupled into the curved, lower guide and exits from the lower right of the plot. The signal and idler light experience the "through" state of this coupler and remain in the curved guide to also exit from the lower right of the plots. For this example, the pump light is carried

by a higher-order transverse mode of the curved guide. Thus, the field magnitude distribution of the pump light in that curved guide has several brighter regions. The signal and idler light, however, are carried by the
5 fundamental transverse modes at those wavelengths. Thus, the intensity distributions for the signal and idler light have just one bright region that is brighter near the center of the guide.

Figures 17-21 are some illustrative examples of
10 implementations for wavelength selective couplers that can be used to couple light of selected wavelengths to travel in loops that include more than one optical waveguide. These example wavelength selective couplers can be used to couple light between a main nonlinear
15 optical waveguide and an extension optical waveguide in an optical waveguide structure. In these illustrative examples, wavelength selective optical couplers in **Figure 17-21** are an implementation for first wavelength selective coupler **112** in **Figure 1**, second wavelength
20 selective coupler **114** in **Figure 1**, wavelength selective coupler **526** in **Figure 5**, wavelength selective coupler **528** in **Figure 5**, signal wavelength selective coupler **720** in **Figure 7**, idler wavelength selective coupler **722** in **Figure 7**, signal wavelength selective coupler **908** in
25 **Figure 9**, idler wavelength selective coupler **910** in **Figure 9**, wavelength selective optical coupler **1008** in **Figure 10**, and wavelength selective coupler **1010** in **Figure 10**.

Turning next to **Figure 17**, an illustration of a
30 wavelength selective coupler in a form of a two-waveguide coupler is depicted in accordance with an illustrative embodiment. As depicted, wavelength selective coupler **1700** is an example of a wavelength selective coupler in the form of a two-waveguide coupler that can be used to

couple light between a main nonlinear optical waveguide and an extension optical waveguide in an optical waveguide structure. This two-waveguide coupler can also be referred to as a directional coupler.

5 In this example, wavelength selective coupler **1700** comprises optical waveguide **1702** and nonlinear optical waveguide **1704**. These two waveguides are spaced apart from each other by a gap **1706**. In **Figure 17**, optical waveguide **1702** and nonlinear optical waveguide **1704** are
10 denoted by their core regions, which have higher refractive index than the surrounding cladding region. Gap **1706** is the portion of the cladding region between optical waveguide **1702** and nonlinear optical waveguide **1704**.

15 As depicted in **Figure 17**, the distance of gap **1706** and the dimensions for optical waveguide **1702** and nonlinear optical waveguide **1704** can be selected to selectively couple light of a particular wavelength between the two waveguides.

20 In an illustrative example, a wavelength selective coupler has a coupling section that comprises two waveguide core regions that are separated by a gap. In this illustrative example, the coupling coefficient decays exponentially with the size of the gap. In other
25 words, the coupling coefficient decays as the size of the gap increases. The coupling coefficient also depends on the effective index of the light of a particular wavelength.

 In an illustrative example, the first wavelength
30 selective coupler and the second wavelength selective coupler of nonlinear optical waveguide structure are implemented as two-guide couplers or directional couplers. The length d_1 of the coupling section of the first waveguide selective coupler for selectively

coupling light of the second longest wavelength λ_2 can be described by the following relation:

$$\kappa_1(\lambda_2) \cdot d_1 = \pi,$$

where κ_1 is the coupling coefficient between the main
 5 nonlinear optical waveguide and the associated extension
 optical waveguide for wavelength λ_2 . The parentheses in
 this expression indicates that κ_1 is a function of λ_2 .

To achieve the desired wavelength selectivity, the
 first waveguide selective coupler also is constrained by
 10 another relation:

$$\kappa_1(\lambda_3) \cdot d_1 = 2 \cdot N \cdot \pi,$$

where κ_1 is the coupling coefficient between the main
 nonlinear optical waveguide and the associated extension
 optical waveguide; λ_3 is the longest wavelength of the
 15 three wavelengths involved in the nonlinear optical
 process; N is an integer; and d_1 is the length of the
 coupling section of the first waveguide selective
 coupler. The value of coupling coefficient κ_1 that
 applies for the longest wavelength λ_3 is different from
 20 the value of κ_1 that applies for the other wavelengths λ_2
 and λ_1 .

In this illustrative example, when N is an integer,
 the photons of wavelength λ_3 are coupled back again to the
 starting waveguide. Furthermore, the gap of the first
 25 coupler is sufficiently large such that the shortest
 wavelength λ_1 is not coupled between the two waveguides,
 such as $\kappa_1(\lambda_1)$ which is small relative to the values for
 $\kappa_1(\lambda_2)$ and $\kappa_1(\lambda_3)$. In other words, this coupler is
 wavelength selective and can direct 100 percent of the
 30 light of wavelength λ_2 to transfer between the main
 nonlinear optical waveguide and the signal extension
 optical waveguide while directing the photons for the

light having wavelength λ_3 or the light having wavelength λ_1 to not transfer between those two waveguides.

A second wavelength selective coupler in the optical waveguide structure can direct the light of the longest wavelength λ_3 of the three wavelengths involved in the nonlinear optical process. In one illustrative example, length d_2 of the coupling section for this second coupler is described by the following relation:

$$\kappa_2(\lambda_3) \cdot d_2 = \pi,$$

where κ_2 is the coupling coefficient between the main nonlinear optical waveguide and the second extension optical waveguide, the associated loop extension for light of wavelength λ_3 . The value of the coupling coefficient κ_2 is a function of the value of the wavelength of the light.

Consider, for example, a second wavelength selective coupler with a coupling coefficient κ_2 . Assume, for an illustrative example, that n_1 , n_2 and n_3 are the effective indices for light of wavelengths λ_1 , λ_2 and λ_3 , respectively. Assume that the values of the effective indices are described by the relation $n_1, n_2 \gg n_3$. Assume, also, the coupling coefficient at the three wavelengths has values described by the relation $\kappa_2(\lambda_1), \kappa_2(\lambda_2) \gg \kappa_2(\lambda_3)$. The coupling section of the second wavelength selective coupler has a length d_2 that is chosen to fulfill the condition: $\kappa_2(\lambda_3) \cdot d_2 = \pi$, so that the photons of the longest wavelength λ_3 have close to 100 percent coupling efficiency between the two waveguides being coupled. This choice of d_2 means that the condition for 100 percent coupling is not fulfilled for the other two wavelengths, λ_1 and λ_2 . Very little of the light at these other two wavelengths is coupled between the two waveguides because the coupling efficiency for

the other two wavelengths, with coupling coefficient values $\kappa_2(\lambda_2)$ and $\kappa_2(\lambda_1)$, are so much smaller than π radians.

The wavelength selective coupling can be performed to increase the length of a loop in which the light at
5 the particular wavelength can travel. For example, nonlinear optical waveguide **1704** can be part of a main nonlinear optical waveguide, such as main nonlinear optical waveguide **106** in **Figure 1**. Optical waveguide **1702** can be part of an extension optical waveguide, such
10 as first extension optical waveguide **108** or second extension optical waveguide **110** in **Figure 1**. In other illustrative examples, these waveguides can be considered separate components that are connected waveguides.

In another illustrative example, first end **1708** of
15 nonlinear optical waveguide **1704** can be connected to one end of main nonlinear optical waveguide **106**, and second end **1710** of nonlinear optical waveguide **1704** can be connected to a second end of main nonlinear optical waveguide **106**. This connection can result in main
20 nonlinear optical waveguide **106** having a closed path. In this example, first end **1712** of optical waveguide **1702** can be connected to a first end of first extension optical waveguide **108** and second end **1714** of optical waveguide **1702** can be connected to a second end of second
25 extension optical waveguide **110**.

When one component is "connected" to another component, the connection is a physical association. For example, a first component can also be considered to be physically connected to a second component by being
30 formed as part of the second component, an extension of the second component, or both. As another example, the first component can be considered to be physically connected to the second component by at least one of being secured to the second component, bonded to the

second component, mounted to the second component, welded to the second component, fastened to the second component, or connected to the second component in some other suitable manner. The first component also can be
5 connected to the second component using a third component.

With reference now to **Figure 18**, an illustration of a wavelength selective coupler in the form of a pulley coupler is depicted in accordance with an illustrative
10 embodiment. As depicted, pulley coupler **1800** is another example of a wavelength selective coupler that can be used to couple light between a main nonlinear optical waveguide and an extension optical waveguide in an optical waveguide structure.

As depicted, pulley coupler **1800** comprises optical waveguide **1802** and nonlinear optical waveguide **1804**. As depicted, optical waveguide **1802** can be a part of an extension optical waveguide, and nonlinear optical waveguide **1804** can be a part of a main nonlinear optical
15 waveguide or can be separate waveguides that are connected to the extension optical waveguide and the main nonlinear optical waveguide. Optical waveguide **1802** and nonlinear optical waveguide **1804** have a curved shape such that the wavelength selective coupler functions as pulley
20 coupler **1800**.

In this illustrative example, distance **1806** and dimensions of optical waveguide **1802** and nonlinear optical waveguide **1804** can be selected to selectively couple light of a particular wavelength between an
25 extension optical waveguide and a main nonlinear optical waveguide. This coupling can be performed to increase the length of a loop in which the light of the selected wavelength travels.

For example, pump light at 1310 nm can be coupled selectively into a first extension optical from the main nonlinear optical waveguide using pulley coupler **1800**. Pulley coupler **1800** can also be configured to couple
5 idler light at 1550 nm into a second extension optical waveguide from a main nonlinear optical waveguide. In other words, one pulley coupler can have a different radius of curvature and different value for distance **1806** from the second pulley coupler used to couple light
10 between a main nonlinear optical waveguide into extension optical waveguides. The configuration of the pulley couplers can be such that a signal light remains in main nonlinear optical waveguide.

The two different radii of curvature of the two
15 waveguide core regions in a pulley coupler provide an additional degree-of-freedom that can enable pulley coupler **1800** to have wavelength selectivity that is stronger than obtained with couplers that have straight sections such as wavelength selective coupler **1700** in
20 **Figure 17**.

For example, in simulations, photons in a pump light at a wavelength of 1310 nm can be coupled from a main nonlinear optical waveguide to a first extension optical waveguide with 99 percent efficiency, and idler photons
25 in idler light at a wavelength of 1550 nm can be coupled with an efficiency lower than 1 percent. In simulations, the photons in idler light at a wavelength of 1550 nm can be coupled with more than 99 percent efficiency while the photons in pump light at wavelength of 1310 nm couple
30 from main nonlinear optical waveguide to a second extension optical waveguide with 23 percent efficiency in this example.

In **Figure 19**, an illustration of a wavelength selective coupler in the form of a 4-port micro-ring

resonator coupler is depicted in accordance with an illustrative embodiment. In this illustrative example, 4-port micro-ring resonator coupler **1900** is another example of an implementation for a wavelength selective
5 coupler that can be used to couple light between a main nonlinear optical waveguide and an extension optical waveguide in the different illustrative examples.

In this illustrative example, 4-port micro-ring resonator is comprised of two pulley couplers with an
10 intervening ring resonator. As depicted in this example, 4-port micro-ring resonator coupler **1900** comprises micro-ring waveguide **1902**, optical waveguide **1904**, and optical waveguide **1906**. In this illustrative example, dimensions of micro-ring waveguide **1902**, optical waveguide **1904**, and
15 optical waveguide **1906** can be selected to provide a desired coupling light of particular wavelengths.

In one illustrative example, the two 4-port micro-ring resonator couplers in an optical waveguide structure such as optical waveguide structure **500** in **Figure 5** can be
20 designed to couple light of different wavelengths. For example, the radius of a first micro-ring resonator in a first 4-port micro-ring resonator coupler implemented using 4-port micro-ring resonator coupler **1900** for coupling the pump photons in pump light is 29.8 μm , and
25 the radius of a second micro-ring resonator in a second 4-port micro-ring resonator coupler implemented using 4-port micro-ring resonator coupler **1900** for coupling the photons in idler light is 25.0 μm . With this configuration, the first 4-port micro-ring resonator
30 coupler can couple photons in pump light at a wavelength of 1310 nm from a main nonlinear optical waveguide **502** to a first extension optical waveguide **504** with 100 percent efficiency. The coupling of photons for the idler light, having a wavelength of 1550 nm, and the photons for the

signal light, having a wavelength of 1130 nm, is lower than -20dB, which is only 1 percent coupling efficiency. The signal and idler photons are retained in the main nonlinear optical waveguide **502**.

5 Additionally, with this configuration, the second 4-port micro-ring resonator coupler can couple photons for the signal light with a wavelength of 1550 nm from main nonlinear optical waveguide **502** to a second extension optical waveguide **506** with a greater than 99 percent
10 efficiency. The photons for the signal light at a wavelength of 1130 nm and the photons for the pump light at a wavelength of 1310 nm can be coupled at a level that is lower than -20dB. This second 4-port micro-ring resonator retains the signal and pump photons in the main
15 nonlinear optical waveguide **502**.

 With reference next to **Figure 20**, an illustration of a wavelength selective coupler in the form of a multimode interference coupler is depicted in accordance with an illustrative embodiment. As depicted, multimode
20 interference (MMI) coupler **2000** is an example of an implementation for a wavelength selective coupler that can be used to couple light between a main nonlinear optical waveguide and an extension optical waveguide in the different illustrative examples.

25 As depicted, multimode interference coupler **2000** has region **2002**. Multimode interference coupler **2000** also has first input **2004**, second input **2006**, first output **2008**, and second output **2010**.

 In this illustrative example, first input **2004** can
30 be connected to a first end of an extension optical waveguide. First output **2008** can be connected to a second end of the extension optical waveguide. Second input **2006** can be connected to a first end of a main nonlinear extension optical waveguide, and second output

2010 can be connected to a second end of the main nonlinear optical waveguide.

The dimensions of multimode interference coupler **2000** can be selected to provide a desired selectivity of light of different wavelengths that are coupled between an extension optical waveguide and a main nonlinear optical waveguide. For example, width **2012** and length **2014** can be selected to enable selectively coupling light of a particular wavelength between a main nonlinear optical waveguide and an extension optical waveguide. Turning to **Figure 21**, an illustration of a wavelength selective coupler in the form of a Mach Zehnder interferometer comprising two multimode interference couplers connected to each other through two optical waveguide segments is depicted in accordance with an illustrative embodiment. One or both of the optical waveguide segments can be implemented as a phase shifter. In this illustrative example, Mach Zehnder interferometer **2100** is an example of an implementation a wavelength selective optical coupler that can be used to couple light between a main nonlinear optical waveguide and an extension optical waveguide in the different illustrative examples.

In this particular example, Mach Zehnder interferometer **2100** comprises first region **2102** and a second region **2104**. First input **2106** and second input **2108** are inputs to first region **2102**. First output **2110** and second output **2112** are outputs from second region **2104**. Mach Zehnder interferometer **2100** includes first optical waveguide **2114** and second optical waveguide **2116**. These optical waveguides connect first region **2102** and second region **2104** in Mach Zehnder interferometer **2100** to each other. In this illustrative example, Mach Zehnder interferometer **2100** also includes phase shifter **2118**. In

this illustrative example, a phase shifter **2118** is a voltage-controlled optical phase shifter that has one or more tuning electrodes. Phase shifter **2118** can shift the phases of light. This phase shifting can be used to
5 change the phase walk-off for different wavelengths of light passing through multimode interference coupler **2000**.

In this illustrative example, first input **2106** can be connected to a first end of an extension optical
10 waveguide. First output **2110** can be connected to a second end of the extension optical waveguide. Second input **2108** can be connected to a first end of a main nonlinear extension optical waveguide, and second output **2112** can be connected to a second end of the main
15 nonlinear optical waveguide.

Turning next to **Figure 22**, an illustration of a flowchart of a process for a nonlinear process is depicted in accordance with an illustrative embodiment. The process in **Figure 22** can be implemented in physical
20 components such as optical waveguide structure **100** in **Figure 1**.

The process begins by routing a first light of a first wavelength in a first loop in a main nonlinear optical waveguide having a first closed path (operation
25 **2200**). In operation **2200**, the first loop can have a first length that is resonant for the first light of the first wavelength.

The process routes a second light of a second wavelength in a second loop that includes portions of the
30 main nonlinear optical waveguide and a first extension optical waveguide having a second closed path (operation **2202**). In operation **2202**, the second loop can have a second length that is resonant for the second light of the second wavelength.

The process routes a third light of a third wavelength in a third loop that includes portions of the main nonlinear optical waveguide and a second extension optical waveguide having a third closed path (operation
5 **2204**). The process terminates thereafter. In operation **2204**, the third loop can have a third length that is resonant for the third light of the third wavelength. Furthermore, the first loop can have a first length, the second loop can have a second length, and the third loop
10 can have a third length for which round trip phase matching is present for a nonlinear optical process that occurs in the main nonlinear optical waveguide. In this illustrative example, round trip phase matching applies jointly to all three wavelengths and all three loops in
15 the optical waveguide structure.

Turning next to **Figure 23**, an illustration of a flowchart of a process for coupling a second light is depicted in accordance with an illustrative embodiment. The operation illustrated in this figure is an additional
20 operation that can be performed with the operations in **Figure 22**.

The process begins by coupling a second light of a second wavelength between a main nonlinear optical waveguide and a first extension optical waveguide with a
25 first wavelength selective coupler in a first region in which the main nonlinear optical waveguide and the first extension optical waveguide have a first distance from each other such that the first wavelength selective coupler couples the second light of the second wavelength
30 between the main nonlinear optical waveguide and the first extension optical waveguide causing the second light of the second wavelength to travel in a second loop (operation **2300**). The process terminates thereafter.

With reference now to **Figure 24**, an illustration of a flowchart of a process for coupling a second light is depicted in accordance with an illustrative embodiment. The operation illustrated in this figure is an additional
5 operation that can performed with the operations in **Figure 22**.

The process begins by coupling a third light of a third wavelength between a main nonlinear optical waveguide and a second extension optical waveguide with a
10 second wavelength selective coupler in a second region in which the main nonlinear optical waveguide and the second extension optical waveguide have a second distance from each other such that the second wavelength selective coupler couples the third light of the third wavelength
15 between the main nonlinear optical waveguide and the first extension optical waveguide causing the third light of the third wavelength to travel in a third loop (operation **2400**). The process terminates thereafter.

In **Figure 25**, an illustration of a flowchart of a
20 process for applying activations to adjust a phase shift in a first light is depicted in accordance with an illustrative embodiment. The operation illustrated in this figure is an additional operation that can performed with the operations in **Figure 22**.

25 The process begins by applying an activation to a portion of a main nonlinear optical waveguide, wherein a phase shifts occurs in a first light of a first wavelength to achieve a resonant condition for the first light of the first wavelength (operation **2500**). The
30 process terminates thereafter.

Turning now to **Figure 26**, an illustration of a flowchart of a process for applying an activation to adjust a phase shift in a second light is depicted in accordance with an illustrative embodiment. The

operation illustrated in this figure is an additional operation that can performed with the operations in **Figure 22**.

5 The process begins by applying an activation to a portion of a first extension optical waveguide, wherein a phase shifts occurs in a second light of a second wavelength to achieve a resonant condition for a first light of the second wavelength (operation **2600**). The process terminates thereafter.

10 Turning next to **Figure 27**, an illustration of a flowchart of a process for applying an activation to adjust a phase shift in a third light is depicted in accordance with an illustrative embodiment. The operation illustrated in this figure is an additional operation that can performed with the operations in **Figure 22**.

15 The process begins by applying an activation to a portion of a first extension optical waveguide, wherein a phase shifts occurs in a third light of a third wavelength to achieve a resonant condition for the third light of the third wavelength (operation **2700**). The process terminates thereafter.

20 With reference now to **Figure 28**, an illustration of a flowchart of a process for applying an activation to adjust a phase shift in light is depicted in accordance with an illustrative embodiment. The operation illustrated in this figure is an additional operation that can performed with the operations in **Figure 22**. The process begins by applying an activation to a portion of a main nonlinear optical waveguide, a first extension optical waveguide, and a second extension optical waveguide such that phase shifts in wavelengths of a light in the main nonlinear optical waveguide cause a value of a phase walk-off to change (operation **2800**).

The process terminates thereafter. In operation **2800**, the activation causes the phase walk-off to change to being as close to zero degrees as possible.

The flowcharts and block diagrams in the different
5 depicted embodiments illustrate the architecture, functionality, and operation of some possible implementations of apparatuses and methods in an illustrative embodiment. In this regard, each block in the flowcharts or block diagrams can represent at least
10 one of a module, a segment, a function, or a portion of an operation or step. For example, one or more of the blocks can be implemented as program code, hardware, or a combination of the program code and hardware. When implemented in hardware, the hardware can, for example,
15 take the form of integrated circuits that are manufactured or configured to perform one or more operations in the flowcharts or block diagrams. When implemented as a combination of program code and hardware, the implementation may take the form of
20 firmware. Each block in the flowcharts or the block diagrams can be implemented using special purpose hardware systems that perform the different operations or combinations of special purpose hardware and program code run by the special purpose hardware.

25 In some alternative implementations of an illustrative embodiment, the function or functions noted in the blocks may occur out of the order noted in the figures. For example, in some cases, two blocks shown in succession may be performed substantially concurrently,
30 or the blocks may sometimes be performed in the reverse order, depending upon the functionality involved. Also, other blocks may be added in addition to the illustrated blocks in a flowchart or block diagram.

Turning now to **Figure 29**, an illustration of a block diagram of a product management system is depicted in accordance with an illustrative embodiment. Product management system **2900** is a physical hardware system. In
5 this illustrative example, product management system **2900** includes at least one of manufacturing system **2902** or maintenance system **2904**.

Manufacturing system **2902** is configured to manufacture products. As depicted, manufacturing system
10 **2902** includes manufacturing equipment **2906**. Manufacturing equipment **2906** includes at least one of fabrication equipment **2908** or assembly equipment **2910**. Fabrication equipment **2908** is equipment that used to fabricate the nonlinear optical waveguide structure.
15 Multiple copies or multiple versions of nonlinear optical waveguide structures can be fabricated on a substrate wafer.

The substrate wafer can comprise a material such as silicon or lithium niobate or quartz or sapphire or
20 silicon carbide. Fabrication equipment **2908** can be used to fabricate at least one of optical waveguide structures, nonlinear optical waveguides, laser transmitters, ultraviolet transmission systems, point-to-point communication devices, laser infrared
25 countermeasure sources, through water optical communication devices, or other suitable devices, antennas, or other suitable types of parts. For example, fabrication equipment **2908** can include machines and tools.

30 With respect to fabricating semiconductor components and optical waveguide components, fabrication equipment **2908** can comprise at least one of an epitaxial reactor, an oxidation system, a diffusion system, an etching system, a cleaning system, a bonding machine, a dicing

machine, a wafer saw, an ion implantation system, a physical vapor deposition system, a chemical vapor deposition system, a photolithography system, an electron-beam lithography system, a plasma etcher, a die attachment machine, a wire bonder, a die overcoat system, molding equipment, a hermetic sealer, an electrical tester, a burn-in oven, a retention bake oven, a UV erase system, or other suitable types of equipment that can be used to manufacture semiconductor structures.

10 Assembly equipment **2910** is equipment used to assemble parts to form a product such as a chip, an integrated circuit, a computer, an aircraft, or some other product. Assembly equipment **2910** also can include machines and tools. These machines and tools may be at least one of a robotic arm, a spinner system, a sprayer system, and elevator system, a rail-based system, or a robot.

 In this illustrative example, maintenance system **2904** includes maintenance equipment **2912**. Maintenance equipment **2912** can include any equipment needed to perform maintenance on and evaluation of a product. Maintenance equipment **2912** may include tools for performing different operations on parts on a product. These operations can include at least one of

25 disassembling parts, refurbishing parts, inspecting parts, reworking parts, manufacturing replacement parts, or other operations for performing maintenance on the product. These operations can be for routine maintenance, inspections, upgrades, refurbishment, or

30 other types of maintenance operations.

 In the illustrative example, maintenance equipment **2912** may include optical inspection devices, x-ray imaging systems, surface-profile measurement systems, drills, vacuum leak checkers, and other suitable devices.

In some cases, maintenance equipment **2912** can include fabrication equipment **2908**, assembly equipment **2910**, or both to produce and assemble parts that needed for maintenance.

5 Product management system **2900** also includes control system **2914**. Control system **2914** is a hardware system and may also include software or other types of components. Control system **2914** is configured to control the operation of at least one of manufacturing system
10 **2902** or maintenance system **2904**. In particular, control system **2914** can control the operation of at least one of fabrication equipment **2908**, assembly equipment **2910**, or maintenance equipment **2912**.

 The hardware in control system **2914** can be
15 implemented using hardware that may include computers, circuits, networks, and other types of equipment. The control may take the form of direct control of manufacturing equipment **2906**. For example, robots, computer-controlled machines, and other equipment can be
20 controlled by control system **2914**. In other illustrative examples, control system **2914** can manage operations performed by human operators **2916** in manufacturing or performing maintenance on a product. For example, control system **2914** can assign tasks, provide
25 instructions, display models, or perform other operations to manage operations performed by human operators **2916**. In these illustrative examples, the different processes for fabricating semiconductor structures, optical structures, nonlinear optical waveguides, laser
30 transmitters, photon generators, photon transmitters, photon detectors, ultraviolet transmission systems, point-to-point communication devices, laser infrared countermeasure sources, through water optical communication devices, or other suitable devices can be

manufactured using processes implemented in control system **2914**.

In the different illustrative examples, human operators **2916** can operate or interact with at least one
5 of manufacturing equipment **2906**, maintenance equipment **2912**, or control system **2914**.

This interaction can occur to manufacture semiconductor structures and other components for products such as semiconductor devices or components for
10 use in products such as aircraft, spacecraft, communications systems, computation systems, and sensor systems.

Further, control system **2914** can be used to adjust manufacturing of nonlinear optical waveguides, optical
15 waveguides, optical couplers, terminations, and other components dynamically during the manufacturing process. For example, many points in the process of fabricating the optical waveguide structure including the nonlinear optical waveguide as well as other components are present
20 at which adjustments can be made to control characteristics of components in an optical waveguide structure. These points are points during the application process in which changes can made to adjust the performance or characteristics of the different
25 structures being fabricated.

Some features of the illustrative examples are described in the following clauses. These clauses are examples of features not intended to limit other illustrative examples.

30 Clause 1

An optical waveguide structure comprising:

a main nonlinear optical waveguide, wherein a first light of a first wavelength travels in a first loop that extends through the main nonlinear optical waveguide;

a first extension optical waveguide;
a second extension optical waveguide;
a first wavelength selective coupler that couples
the main nonlinear optical waveguide and the first
5 extension optical waveguide to each other such that a
second light of a second wavelength is coupled between
the main nonlinear optical waveguide and the first
extension optical waveguide, wherein the second light of
the second wavelength travels in a second loop that
10 extends through the main nonlinear optical waveguide and
the first extension optical waveguide in which the second
loop has a second length for the second light of the
second wavelength; and
a second wavelength selective coupler that couples
15 the main nonlinear optical waveguide and the second
extension optical waveguide to each other such a third
light of a third wavelength is coupled between the main
nonlinear optical waveguide and the second extension
optical waveguide, wherein the third light of the third
20 wavelength travels in a third loop that extends though
the main nonlinear optical waveguide and the second
extension optical waveguide in which the third loop has a
third length for the third light of the third wavelength.

Clause 2:

The optical waveguide structure according to clause 1, wherein a first length of the first loop is selected such that at least one of a resonance matching is present
5 for the first light of the first wavelength or round-trip phase matching is present for the first light of the first wavelength.

Clause 3:

The optical waveguide structure according to any of
10 clauses 1-2, wherein the second length of the second loop is selected such that at least one of a resonance matching is present for the second light of the second wavelength or round-trip phase matching is present for the second light of the second wavelength.

15 Clause 4:

The optical waveguide structure according to any of clauses 1- 3, wherein third second length of the third loop is selected such that at least one of a resonance matching is present for the third light of the third
20 wavelength or round-trip phase matching is present for the third light of the third second wavelength.

Clause 5:

The optical waveguide structure according to any of clauses 1- 4 further comprising:
25 a set of phase shifters located adjacent to a set of optical waveguides comprising at least one of the main nonlinear optical waveguide, the first extension optical waveguide, or the second extension optical waveguide in the set of optical waveguides, wherein the set of tuning
30 electrodes applies a set of activations such that the set of activations changes a phase of at least one of the first light of the first wavelength, the second light of the second wavelength, or the third light of the third

wavelength traveling in the set of optical waveguides to which the set of activations is applied.

Clause 6:

The optical waveguide structure according to clause
5 5, wherein the set of phase shifters comprises at least one of a first tuning electrode located adjacent to a first portion of the main nonlinear optical waveguide; a second tuning electrode located adjacent to a second portion of the first extension optical waveguide; or a
10 third tuning electrode located adjacent to a third portion of the second extension optical waveguide, wherein at least one of the first tuning electrode, the second tuning electrode, or the third tuning electrode apply the set of activations to adjust phases of at least
15 one of the first light of the first wavelength, the second light of the second wavelength, or the third light of the third wavelength traveling in a set of loops through the set of optical waveguides.

Clause 7:

20 The optical waveguide structure according to any of clauses 5-6, wherein the set of activations is selected from at least one of a voltage, a thermal energy, or a strain.

Clause 8:

25 The optical waveguide structure according to any of clauses 1-7 further comprising:

an output optical waveguide that couples light out of one of the main nonlinear optical waveguide, the first extension optical waveguide, and the second extension
30 optical waveguide.

Clause 9

The optical waveguide structure according to clause 8 further comprising:

an output optical coupler for the output optical waveguide, wherein the output optical coupler has a configuration that results in a desired Q factor for the second loop and the second wavelength selective coupler
5 has the configuration that results in the desired Q factor for the third loop.

Clause 10:

The optical waveguide structure according to any of clauses 1-9 further comprising:
10 an input optical waveguide that couples input light into one of the main nonlinear optical waveguide, the first extension optical waveguide, and the second extension optical waveguide.

Clause 11:

15 The optical waveguide structure according to any of clauses 1-10, wherein the first loop, the second loop, and the third loop are loops that have lengths selected to cause roundtrip phase matching in which a generation of photons for at least one of the first light, the
20 second light, or the third light continues along a set of loops selected from at least one of the first loop, the second loop, or the third loop as travel time increases for the first light, the second light, and the third light in the set of loops.

25 Clause 12:

The optical waveguide structure according to any of clauses 1-11, wherein the first loop, the second loop, and the third loop have different lengths from each other.

30 Clause 13:

The optical waveguide structure according to clause 12, wherein a spontaneous four wave mixing occurs in the main nonlinear optical waveguide in which a pair of output photons is generated from a pair of input photons,

wherein the pair of output photons have different wavelengths from each other and have the different wavelengths from the pair of input photons.

Clause 14:

5 The optical waveguide structure according to clause 12, wherein a spontaneous parametric down conversion occurs in the main nonlinear optical waveguide in which the pair of output photons is generated from an input photon, wherein the pair of output photons have the
10 different wavelengths from each other and have the different wavelengths from the input photon.

Clause 15:

 The optical waveguide structure according to any of clauses 1-14, wherein the first wavelength selective
15 coupler is in a first location where a first portion of the main nonlinear optical waveguide and a second portion of the first extension optical waveguide are located and wherein the second wavelength selective coupler is in a second location where a third portion of the main
20 nonlinear optical waveguide and a fourth portion of the second extension optical waveguide are located.

Clause 16:

 The optical waveguide structure according to any of clauses 1-15, wherein the main nonlinear optical
25 waveguide has a cross-section with a dimension selected to achieve a resonance condition for the first light of the first wavelength traveling in the main nonlinear optical waveguide; wherein the first extension optical waveguide has a first cross-section with a first
30 dimension selected to achieve the resonance condition for the second light of the second wavelength traveling in the first extension optical waveguide; and wherein the second extension optical waveguide has a second cross-section with a second dimension selected to achieve the

resonance condition for the third light of the third wavelength traveling in the second extension optical waveguide.

Clause 17:

5 The optical waveguide structure according to any of clauses 1-16, wherein the first wavelength selective coupler and the second wavelength selective coupler are selected from at least one of a two-waveguide coupler, a multi-mode interference coupler, a pulley coupler, a
10 Mach-Zehnder interferometer, or a 4-port micro-optical waveguide resonator coupler.

Clause 18:

An optical waveguide structure comprising:

15 a main nonlinear optical waveguide, wherein a first light of a first wavelength travels in a first loop that extends through the main nonlinear optical waveguide in which the first loop has a first length for the first light of the first wavelength;
 an extension nonlinear optical waveguide; and
20 a wavelength selective coupler that couples a second light of a second wavelength between the main nonlinear optical waveguide and the extension nonlinear optical waveguide, wherein the second light of the second wavelength travels in a second loop that extends through
25 the main nonlinear optical waveguide and the extension nonlinear optical waveguide in which the second loop has a second length for the second light of the second wavelength.

Clause 19:

The optical waveguide structure according to clause 18, wherein the first length of the first loop is selected such that at least one of a resonance matching
5 is present for the first light of the first wavelength or round-trip phase matching is present for the first light of the first wavelength.

Clause 20:

The optical waveguide structure according to any of
10 clauses 18-19, wherein the second length of the second loop is selected such that at least one of a resonance matching is present for the second light of the second wavelength or round-trip phase matching is present for the second light of the second wavelength.

15 Clause 21:

The optical waveguide structure according to any of clauses 18-20, wherein the extension nonlinear optical waveguide is a first extension optical waveguide and wherein the wavelength selective coupler is a first
20 wavelength selective coupler and further comprising:

a second extension optical waveguide;

and

a second wavelength selective coupler that couples a third light of a third wavelength between the main
25 nonlinear optical waveguide and the second extension optical waveguide, wherein the third light of the third wavelength travels in a third loop that extends through the main nonlinear optical waveguide and the second extension optical waveguide in which the third loop has a
30 third length for the third light of the third wavelength.

Clause 22:

The optical waveguide structure according to clause 21, wherein the third length of the third loop is selected such that at least one of a resonance matching

is present for the third light of the third second wavelength or round-trip phase matching is present for the third light of the third second wavelength.

Clause 23:

5 The optical waveguide structure according to clause 21 , wherein the first loop, the second loop, and the third loop are loops that have lengths selected to cause roundtrip phase matching in which a generation of photons for at least one of the first light, the second light, or
10 the third light continues in a set of loops selected from at least one of the first loop, the second loop, or the third loop as travel time increases for the first light, the second light, and the third light along the set of loops.

15 Clause 24:

The optical waveguide structure according to any of clauses 18-23 further comprising:

a tuning electrode located adjacent to a portion of the main nonlinear optical waveguide, wherein the tuning
20 electrode applies a voltage such that a phase shifts in the first light of the first wavelength to achieve a resonant condition for the first light of the first wavelength of.

Clause 25:

25 The optical waveguide structure according to according to any of clauses 21-24 comprising:

a tuning electrode located adjacent to a portion of the first extension optical waveguide, wherein the tuning electrode applies a voltage such that a phase shifts in
30 the second light of the second wavelength to achieve a resonant condition for the second light of the second wavelength.

Clause 26:

The optical waveguide structure according to
according to any of clauses 21-25 further comprising:

5 a tuning electrode located adjacent to a portion of
the second extension optical waveguide, wherein the
tuning electrode applies a voltage such that a phase
shifts in the third light of the third wavelength to
achieve a resonant condition for the third light of the
third wavelength.

10 Clause 27:

The optical waveguide structure according to
according to any of clauses 21-26 further comprising at
least one of a first tuning electrode located adjacent to
a first portion of the main nonlinear optical waveguide;
15 a second tuning electrode located adjacent to a second
portion of the first extension optical waveguide; or a
third tuning electrode located adjacent to a third
portion of the second extension optical waveguide,
wherein at least one of the first tuning electrode , the
20 second tuning electrode, or the third tuning electrode
apply a set of activations to adjust a set of phase
shifts in to achieve a phase matching condition.

Clause 28:

The optical waveguide structure according to
25 according to one of clauses 21-27 further comprising:
an output optical waveguide that couples light out
of one of the main nonlinear optical waveguide, the first
extension optical waveguide, and the second extension
optical waveguide.

30

Clause 29:

The optical waveguide structure according to
according to any of clauses 18-28 further comprising:

an input optical waveguide that couples input light
5 into one of the main nonlinear optical waveguide.

Clause 30:

The optical waveguide structure according to
according to any of clauses 21-29, wherein the first
loop, the second loop, and the third loop have different
10 lengths from each other.

Clause 31:

A method for a non-linear optical process
comprising:

routing a first light of a first wavelength in a
15 first loop in a main nonlinear optical waveguide, wherein
the first loop has a first length for the first light of
the first wavelength;

routing a second light of a second wavelength in a
second loop that includes portions of the main nonlinear
20 optical waveguide and a first extension optical
waveguide, wherein the second loop has a second length
for the second light of the second wavelength; and

routing a third light of a third wavelength in a
third loop that include the portions of the main
25 nonlinear optical waveguide and a second extension
optical waveguide, wherein the third loop has a third
length for the third light of the third wavelength.

Clause 32:

The method according to clause 31 further
30 comprising:

coupling the second light of the second wavelength
between the main nonlinear optical waveguide and the
first extension optical waveguide with a first wavelength
selective coupler that couples the second light of the

second wavelength of between the main nonlinear optical waveguide and the first extension optical waveguide causing the second light of the second wavelength of to travel in the second loop.

5 Clause 33:

 The method according to any of clauses 31-32, wherein the first length of the first loop is selected such that at least one of a resonance matching is present for the first light of the first wavelength or round-trip
10 phase matching is present for the first light of the first wavelength.

 Clause 34:

 The method according to any of clauses 31-33, wherein the second length of the second loop is selected
15 such that at least one of a resonance matching is present for the second light of the second wavelength or round-trip phase matching is present for the second light of the second wavelength.

 Clause 35:

20 The method according to any of clauses 31-34 further comprising:

 coupling the third light of the third wavelength between the main nonlinear optical waveguide and the second extension optical waveguide with a second
25 wavelength selective coupler that couples the third light of the third wavelength between the main nonlinear optical waveguide and the second extension optical waveguide causing the third light of the third wavelength to travel in the third loop.

30 Clause 36:

 The method according to clause 35, wherein third second length of the third loop is selected such that at least one of a resonance matching is present for the third light of the third second wavelength or round-trip

phase matching is present for the third light of the third second wavelength.

Clause 37:

The method according to any of clauses 31-36 further comprising:

applying an activation to a portion of the main nonlinear optical waveguide, wherein a phase shift occurs in the first light of the first wavelength to achieve a resonant condition for the first light of the first wavelength.

Clause 38:

The method according to any of clauses 31-37 further comprising:

applying an activation to a portion of the first extension optical waveguide, wherein a phase shift occurs in the second light of the second wavelength to achieve a resonant condition for the second light of the second wavelength.

Clause 39:

The method according to any of clauses 31-38 further comprising:

applying an activation to a portion of the second extension optical waveguide, wherein a phase shift occurs in the third light of the third wavelength to achieve a resonant condition for the third light of the third wavelength.

Clause 40:

The method according to any of clauses 31-39 further comprising:

applying an activation to a portion of the main nonlinear optical waveguide, the first extension optical waveguide, and the second extension optical waveguide such that phase shifts in wavelengths of a light in the

main nonlinear optical waveguide causing a value of a phase walk-off to change.

Thus, the illustrative examples provide a method and structure for nonlinear optical processes. In one
5 illustrative example, an optical waveguide structure can have a main nonlinear optical waveguide, a first extension optical waveguide, a second extension optical waveguide, a first wavelength selective coupler, and a second wavelength selective coupler. A first light of a
10 first wavelength travels in a first loop that extends through the main nonlinear optical waveguide and the wavelength selective coupler, in which the first loop has a first length for the first light of the first wavelength. The wavelength selective coupler couples a
15 second light of a second wavelength between the main nonlinear optical waveguide and the extension nonlinear optical waveguide. The second light of the second wavelength travels in a second loop that extends through the main nonlinear optical waveguide, the wavelength
20 selective coupler and the extension nonlinear optical waveguide, in which the second loop has a second length for the second light of the second wavelength.

The second wavelength selective coupler couples the main nonlinear optical waveguide and the second extension
25 optical waveguide to each other such that the third light of the third wavelength is coupled between the main nonlinear optical waveguide and the second extension optical waveguide. The third light of the third wavelength travels in a third loop within the main
30 nonlinear optical waveguide and the second extension optical waveguide in which the third loop.

Thus, the optical waveguide structures described in the different illustrative examples can be used for various purposes. For example, the optical waveguide

structures can be used as components for quantum communications. For example, these waveguide structures can operate as entangled photon sources for use in components in devices such as quantum repeater systems.

5 These quantum repeater systems can be used to teleport quantum states across different network nodes. As another example, the optical waveguide structures in the illustrative examples can be used in systems such as quantum emitters, bell-state entanglement measurement
10 devices, single-photon detectors, or other suitable systems that may employ a quantum repeater or other device capable of operating as a source of photons.

The description of the different illustrative embodiments has been presented for purposes of
15 illustration and description and is not intended to be exhaustive or limited to the embodiments in the form disclosed. The different illustrative examples describe components that perform actions or operations. In an illustrative embodiment, a component can be configured to
20 perform the action or operation described. For example, the component can have a configuration or design for a structure that provides the component an ability to perform the action or operation that is described in the illustrative examples as being performed by the
25 component. Further, to the extent that terms "includes", "including", "has", "contains", and variants thereof are used herein, such terms are intended to be inclusive in a manner similar to the term "comprises" as an open transition word without precluding any additional or
30 other elements.

Many modifications and variations will be apparent to those of ordinary skill in the art. Further, different illustrative embodiments may provide different features as compared to other desirable embodiments. The

embodiment or embodiments selected are chosen and described in order to best explain the principles of the embodiments, the practical application, and to enable others of ordinary skill in the art to understand the
5 disclosure for various embodiments with various modifications as are suited to the particular use contemplated.

CLAIMS:

What is claimed is:

- 5 1. An optical waveguide structure (100) comprising:
a main nonlinear optical waveguide (106), wherein a
first light (115) of a first wavelength (122) travels in
a first loop (142) that extends through the main
nonlinear optical waveguide (106);
10 a first extension optical waveguide (108);
a second extension optical waveguide (110);
a first wavelength selective coupler (112) that
couples the main nonlinear optical waveguide (106) and
the first extension optical waveguide (108) to each other
15 such that a second light (124) of a second wavelength
(126) is coupled between the main nonlinear optical
waveguide (106) and the first extension optical waveguide
(108), wherein the second light (124) of the second
wavelength (126) travels in a second loop (154) that
20 extends through the main nonlinear optical waveguide
(106) and the first extension optical waveguide (108) in
which the second loop (154) has a second length (158) for
the second light (124) of the second wavelength (126);
and
25 a second wavelength selective coupler that couples
the main nonlinear optical waveguide (106) and the second
extension optical waveguide (110) to each other such a
third light (128) of a third wavelength (130) is coupled
between the main nonlinear optical waveguide (106) and
30 the second extension optical waveguide (110), wherein the
third light (128) of the third wavelength (130) travels
in a third loop (162) that extends though the main
nonlinear optical waveguide (106) and the second
extension optical waveguide (110) in which the third loop

(162) has a third length (164) for the third light (128) of the third wavelength (130).

2. The optical waveguide structure (100) according to
5 claim 1, wherein a first length (144) of the first loop (142) is selected such that at least one of a resonance matching (165) is present for the first light (115) of the first wavelength (122) or round-trip phase matching (166) is present for the first light (115) of the first
10 wavelength (122).

3. The optical waveguide structure (100) according to any of claims 1-2, wherein the second length (158) of the second loop (154) is selected such that at least one of a
15 resonance matching (165) is present for the second light (124) of the second wavelength (126) or round-trip phase matching (166) is present for the second light (124) of the second wavelength (126).

20 4. The optical waveguide structure (100) of according to any of claims 1-3, wherein third second length (158) of the third loop (162) is selected such that at least one of a resonance matching (165) is present for the third light (128) of the third wavelength (130) or round-
25 trip phase matching (166) is present for the third light (128) of the third second wavelength (126).

5. The optical waveguide structure (100) according to any of claims 1-4 further comprising:
30 a set of phase shifters (300) located adjacent to a set of optical waveguides (102) comprising at least one of the main nonlinear optical waveguide (106), the first extension optical waveguide (108), or the second extension optical waveguide (110) in the set of optical

waveguides (102), wherein the set of tuning electrodes applies a set of activations (304) such that the set of activations (304) changes a phase of at least one of the first light (115) of the first wavelength (122), the
5 second light (124) of the second wavelength (126), or the third light (128) of the third wavelength (130) traveling in the set of optical waveguides (102) to which the set of activations (304) is applied.

10 6. The optical waveguide structure (100) according to claim 5, wherein the set of phase shifters (300) comprises at least one of a first tuning electrode (309) located adjacent to a first portion of the main nonlinear optical waveguide (106); a second tuning electrode (311)
15 located adjacent to a second portion of the first extension optical waveguide (108); or a third tuning electrode (313) located adjacent to a third portion of the second extension optical waveguide (110), wherein at least one of the first tuning electrode (309), the second
20 tuning electrode (311), or the third tuning electrode (313) apply the set of activations (304) to adjust phases of at least one of the first light (115) of the first wavelength (122), the second light (124) of the second wavelength (126), or the third light (128) of the third
25 wavelength (130) traveling in a set of loops (131) through the set of optical waveguides (102).

7. The optical waveguide structure (100) according to any of claims 5-6, wherein the set of activations (304)
30 is selected from at least one of a voltage, a thermal energy, or a strain.

8. The optical waveguide structure (100) according to any of claims 1-7 further comprising:

an output optical waveguide (182) that couples light (115) out of one of the main nonlinear optical waveguide (106), the first extension optical waveguide (108), and the second extension optical waveguide (110).

5

9. The optical waveguide structure (100) according to claim 8 further comprising:

an output optical coupler (186) for the output optical waveguide (182), wherein the output optical
10 coupler (186) has a configuration that results in a desired Q factor for the second loop (154) and the second wavelength selective coupler (114) has the configuration that results in the desired Q factor for the third loop (162).

15

10. The optical waveguide structure (100) according to any of claims 1-9 further comprising:

an input optical waveguide (178) that couples input light into one of the main nonlinear optical waveguide
20 (106), the first extension optical waveguide (108), and the second extension optical waveguide (110).

11. The optical waveguide structure (100) according to any of claims 1-10, wherein the first loop (142), the
25 second loop (154), and the third loop (162) are loops (131) that have lengths selected to cause roundtrip phase matching (166) in which a generation of photons for at least one of the first light (115), the second light (124), or the third light (128) continues along a set of
30 loops (131) selected from at least one of the first loop (142), the second loop (154), or the third loop (162) as travel time increases for the first light (115), the second light (124), and the third light (128) in the set of loops (131).

12. The optical waveguide structure (100) according to any of claims 1-11, wherein the first loop (142), the second loop (154), and the third loop (162) have different lengths from each other.

5

13. The optical waveguide structure (100) according to claim 12, wherein a spontaneous four wave mixing occurs in the main nonlinear optical waveguide (106) in which a pair of output photons (172) is generated from a pair of
10 input photons (174), wherein the pair of output photons (172) have different wavelengths from each other and have the different wavelengths from the pair of input photons (174).

14. The optical waveguide structure (100) according to claim 12, wherein a spontaneous parametric down
conversion occurs in the main nonlinear optical waveguide (106) in which the pair of output photons (172) is generated from an input photon, wherein the pair of
20 output photons (172) have the different wavelengths from each other and have the different wavelengths from the input photon.

15. The optical waveguide structure (100) according to any of claims 1-14, wherein the first wavelength
25 selective coupler (112) is in a first location where a first portion of the main nonlinear optical waveguide (106) and a second portion of the first extension optical waveguide (108) are located and wherein the second
30 wavelength selective coupler (114) is in a second location where a third portion of the main nonlinear optical waveguide (106) and a fourth portion of the second extension optical waveguide (110) are located.

16. The optical waveguide structure (100) according to any of claims 1-15, wherein the main nonlinear optical waveguide (106) has a cross-section (204) with a dimension (204) selected to achieve a resonance condition (208) for the first light (115) of the first wavelength (122) traveling in the main nonlinear optical waveguide (106); wherein the first extension optical waveguide (108) has a first cross-section (210) with a first dimension (212) selected to achieve the resonance condition (208) for the second light (124) of the second wavelength (126) traveling in the first extension optical waveguide (108); and wherein the second extension optical waveguide (110) has a second cross-section (214) with a second dimension (216) selected to achieve the resonance condition (208) for the third light (128) of the third wavelength (130) traveling in the second extension optical waveguide (110).

17. The optical waveguide structure (100) according to any of claims 1-16, wherein the first wavelength selective coupler (112) and the second wavelength selective coupler (114) are selected from at least one of a two-waveguide coupler, a multi-mode interference coupler, a pulley coupler, a Mach-Zehnder interferometer, or a 4-port micro-optical waveguide resonator coupler.

18. An optical waveguide structure (100) comprising:
a main nonlinear optical waveguide (106), wherein a first light (115) of a first wavelength (122) travels in a first loop (142) that extends through the main nonlinear optical waveguide (106) in which the first loop (142) has a first length (144) for the first light (115) of the first wavelength (122);
an extension nonlinear optical waveguide; and

a wavelength selective coupler that couples a second light (124) of a second wavelength (126) between the main nonlinear optical waveguide (106) and the extension nonlinear optical waveguide, wherein the second light
5 (124) of the second wavelength (126) travels in a second loop (154) that extends through the main nonlinear optical waveguide (106) and the extension nonlinear optical waveguide in which the second loop (154) has a second length (158) for the second light (124) of the
10 second wavelength (126).

19. The optical waveguide structure (100) according to claim 18, wherein the first length (144) of the first loop (142) is selected such that at least one of a
15 resonance matching (165) is present for the first light (115) of the first wavelength (122) or round-trip phase matching (166) is present for the first light (115) of the first wavelength (122).

20. The optical waveguide structure (100) according to any of claims 18-19, wherein the second length (158) of the second loop (154) is selected such that at least one of a resonance matching (165) is present for the second light (124) of the second wavelength (126) or round-trip
25 phase matching (166) is present for the second light (124) of the second wavelength (126).

21. The optical waveguide structure (100) according to any of claims 18-20, wherein the extension nonlinear
30 optical waveguide is a first extension optical waveguide (108) and wherein the wavelength selective coupler is a first wavelength selective coupler (112) and further comprising:

a second extension optical waveguide (110);

and

a second wavelength selective coupler (114) that couples a third light (128) of a third wavelength (130) between the main nonlinear optical waveguide (106) and
5 the second extension optical waveguide (110), wherein the third light (128) of the third wavelength (130) travels in a third loop (162) that extends through the main nonlinear optical waveguide (106) and the second extension optical waveguide (110) in which the third loop
10 (162) has a third length (164) for the third light (128) of the third wavelength (130).

22. The optical waveguide structure (100) according to claim 21, wherein the third length (164) of the third
15 loop (162) is selected such that at least one of a resonance matching (165) is present for the third light (128) of the third second wavelength (126) or round-trip phase matching (166) is present for the third light (128) of the third second wavelength (126).

20

23. The optical waveguide structure (100) according to claim 21, wherein the first loop (142), the second loop (154), and the third loop (162) are loops (131) that have lengths selected to cause roundtrip phase matching (166)
25 in which a generation of photons for at least one of the first light (115), the second light (124), or the third light (128) continues in a set of loops (131) selected from at least one of the first loop (142), the second loop (154), or the third loop (162) as travel time
30 increases for the first light (115), the second light (124), and the third light (128) along the set of loops (131).

24. The optical waveguide structure (100) according to any of claims 18-23 further comprising:

5 a tuning electrode located adjacent to a portion of the main nonlinear optical waveguide (106), wherein the tuning electrode applies a voltage such that a phase shifts in the first light (115) of the first wavelength (122) to achieve a resonant condition for the first light (115) of the first wavelength (122) of.

10 25. The optical waveguide structure (100) according to according to any of claims 21-24 further comprising:

a tuning electrode located adjacent to a portion of the first extension optical waveguide (108), wherein the tuning electrode applies a voltage such that a phase
15 shifts in the second light (124) of the second wavelength (126) to achieve a resonant condition for the second light (124) of the second wavelength (126).

26. The optical waveguide structure (100) according to
20 according to any of claims 21-25 further comprising:

a tuning electrode located adjacent to a portion of the second extension optical waveguide (110), wherein the tuning electrode applies a voltage such that a phase shifts in the third light (128) of the third wavelength
25 (130) to achieve a resonant condition for the third light (128) of the third wavelength (130).

27. The optical waveguide structure (100) according to according to any of claims 21-26 further comprising at
30 least one of a first tuning electrode (309) located adjacent to a first portion of the main nonlinear optical waveguide (106); a second tuning electrode (311) located adjacent to a second portion of the first extension optical waveguide (108); or a third tuning electrode

(313) located adjacent to a third portion of the second extension optical waveguide (110), wherein at least one of the first tuning electrode (309) , the second tuning electrode (311), or the third tuning electrode (313)

5 apply a set of activations (304) to adjust a set of phase shifts in to achieve a phase matching condition.

28. The optical waveguide structure (100) according to according to any of claims 21-27 further comprising:

10 an output optical waveguide that couples light out of one of the main nonlinear optical waveguide (106), the first extension optical waveguide (108), and the second extension optical waveguide (110).

15 29. The optical waveguide structure (100) according to according to any of claims 18-28 further comprising:

 an input optical waveguide that couples input light into one of the main nonlinear optical waveguide (106).

20 30. The optical waveguide structure (100) according to according to any of claims 21-29, wherein the first loop (142), the second loop (154), and the third loop (162) have different lengths from each other.

25 31. A method for a non-linear optical process comprising:

 routing (2200) a first light (115) of a first wavelength (122) in a first loop (142) in a main nonlinear optical waveguide (106), wherein the first loop

30 (142) has a first length (144) for the first light (115) of the first wavelength (122);

 routing (2202) a second light (124) of a second wavelength (126) in a second loop (154) that includes portions of the main nonlinear optical waveguide (106)

and a first extension optical waveguide (108), wherein the second loop (154) has a second length (158) for the second light (124) of the second wavelength (126); and

routing (2204) a third light (128) of a third wavelength (130) in a third loop (162) that include the portions of the main nonlinear optical waveguide (106) and a second extension optical waveguide (110), wherein the third loop (162) has a third length (164) for the third light (128) of the third wavelength (130).

10

32. The method according to claim 31 further comprising: coupling (2300) the second light (124) of the second wavelength (126) between the main nonlinear optical waveguide (106) and the first extension optical waveguide (108) with a first wavelength selective coupler (112) that couples the second light (124) of the second wavelength (126) of between the main nonlinear optical waveguide (106) and the first extension optical waveguide (108) causing the second light (124) of the second wavelength (126) of to travel in the second loop (154).

15

20

33. The method according any of claims 31-32, wherein the first length (144) of the first loop (142) is selected such that at least one of a resonance matching (165) is present for the first light (115) of the first wavelength (122) or round-trip phase matching (166) is present for the first light (115) of the first wavelength (122).

25

30

34. The method according to any of claims 31-33, wherein the second length (158) of the second loop (154) is selected such that at least one of a resonance matching (165) is present for the second light (124) of the second wavelength (126) or round-trip phase matching

(166) is present for the second light (124) of the second wavelength (126).

35. The method according to any of claims 31-34 further comprising:

coupling (2400) the third light (128) of the third wavelength (130) between the main nonlinear optical waveguide (106) and the second extension optical waveguide (110) with a second wavelength selective coupler (114) that couples the third light (128) of the third wavelength (130) between the main nonlinear optical waveguide (106) and the second extension optical waveguide (110) causing the third light (128) of the third wavelength (130) to travel in the third loop (162).

15

36. The method according to claim 35, wherein third second length (158) of the third loop (162) is selected such that at least one of a resonance is present for the third light (128) of the third second wavelength (126) or round-trip phase matching (166) is present for the third light (128) of the third second wavelength (126).

20

37. The method according to any of claims 31-36 further comprising:

applying (2500) an activation to a portion of the main nonlinear optical waveguide (106), wherein a phase shifts occurs in the first light (115) of the first wavelength (122) to achieve a resonant condition for the first light (115) of the first wavelength (122).

30

38. The method according to any of claims 31-37 further comprising:

applying (2600) an activation to a portion of the first extension optical waveguide (108), wherein a phase

shifts occurs in the second light (124) of the second wavelength (126) to achieve a resonant condition for the second light (124) of the second wavelength (126).

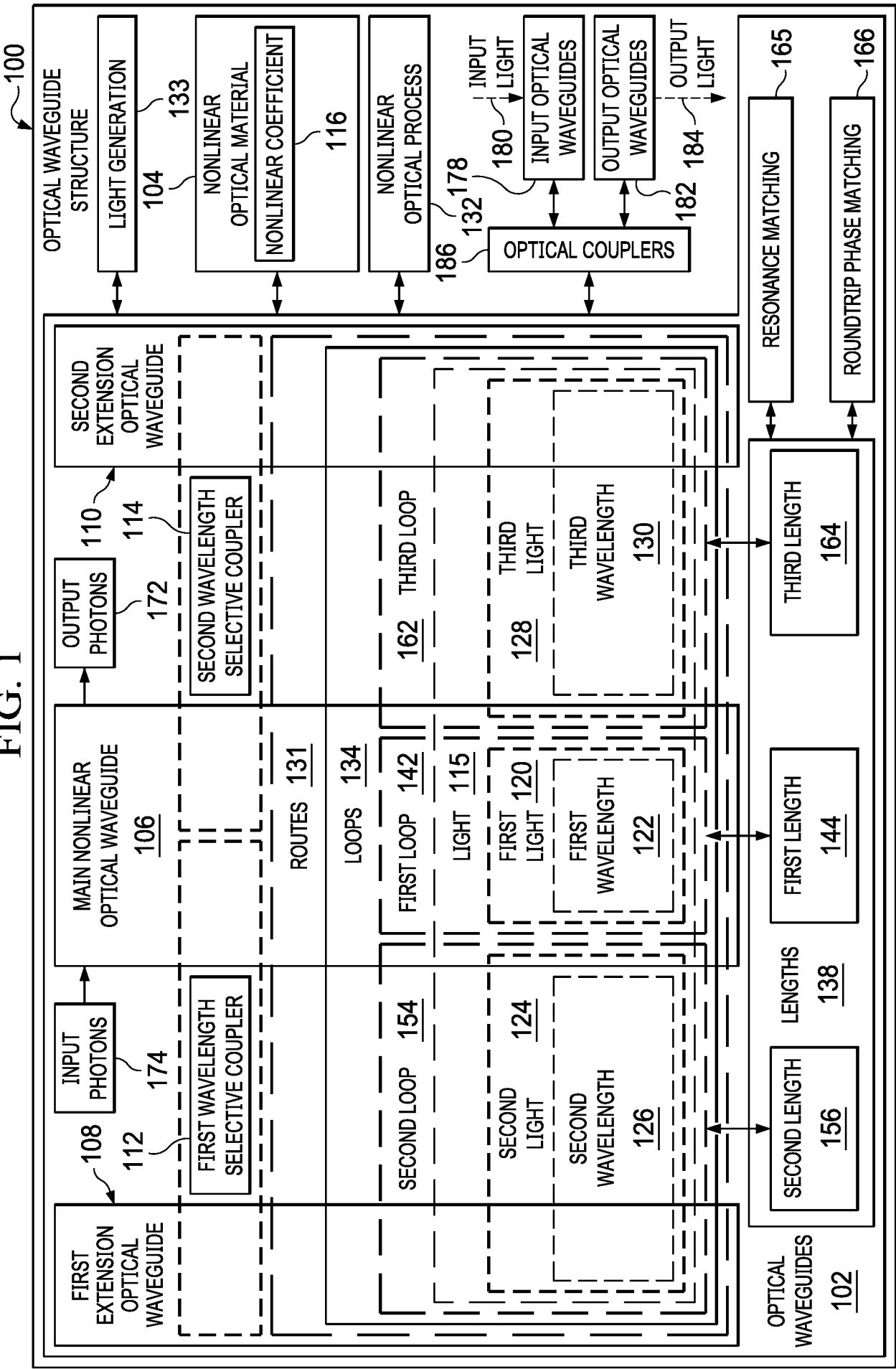
5 39. The method according to any of claims 31-38 further comprising:

applying (2700) an activation to a portion of the second extension optical waveguide (110), wherein a phase shifts occurs in the third light (128) of the third
10 wavelength (130) to achieve a resonant condition for the third light (128) of the third wavelength (130).

40. The method according to any of claims 31-39 further comprising:

15 applying (2800) an activation to a portion of the main nonlinear optical waveguide (106), the first extension optical waveguide (108), and the second extension optical waveguide (110) such that phase shifts in wavelengths of a light (115) in the main nonlinear
20 optical waveguide (106) causing a value of a phase walk-off to change.

FIG. 1



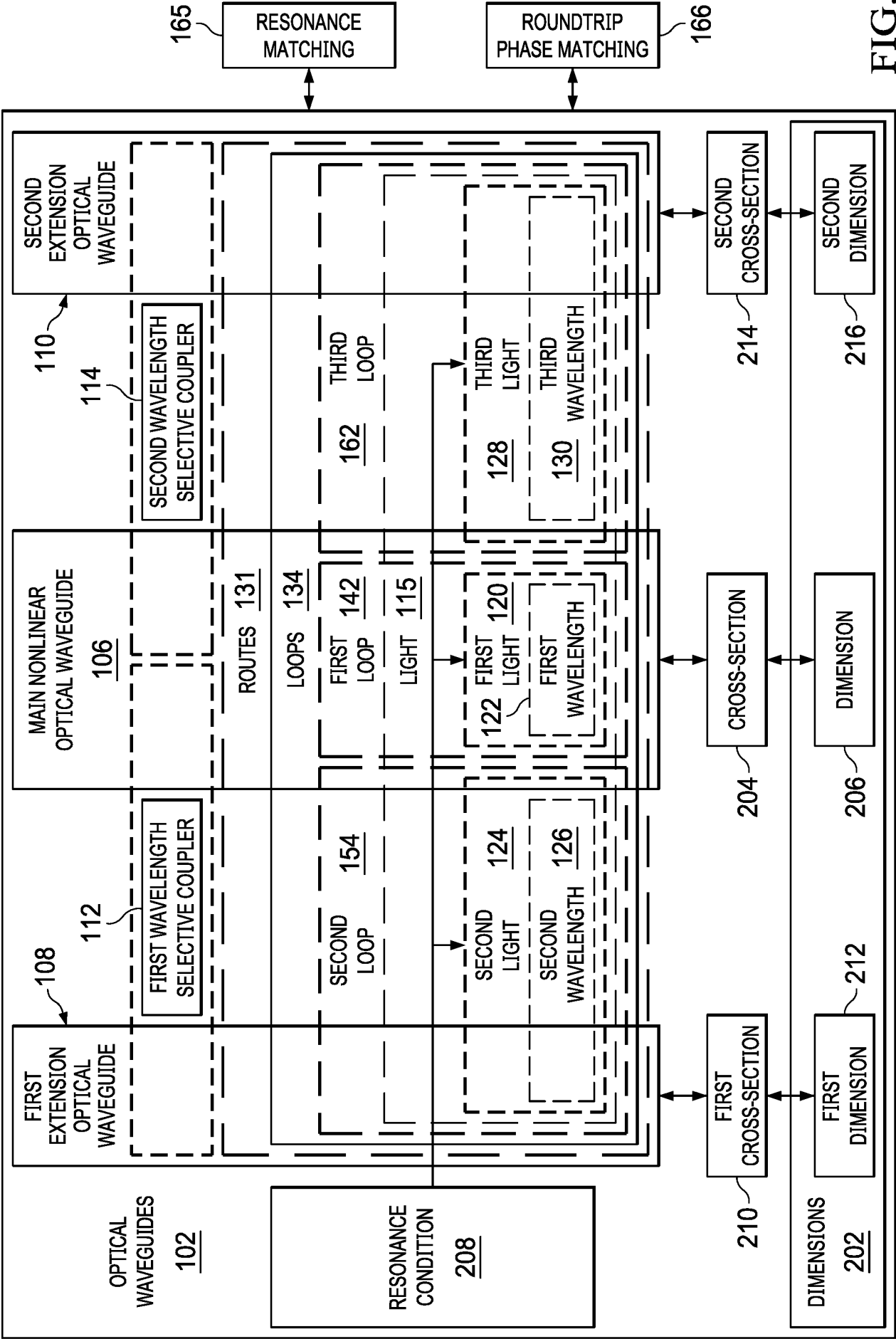
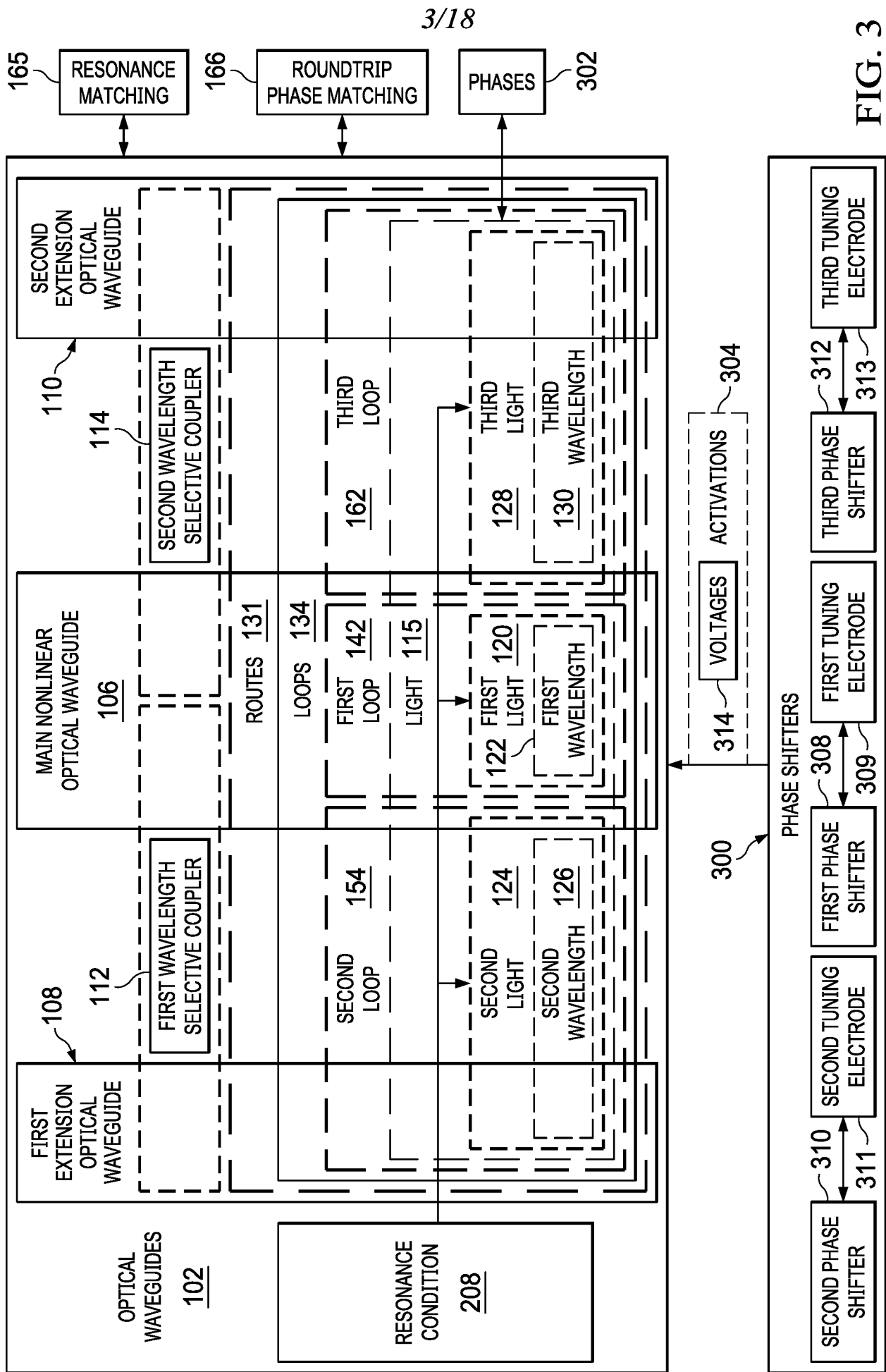


FIG. 2



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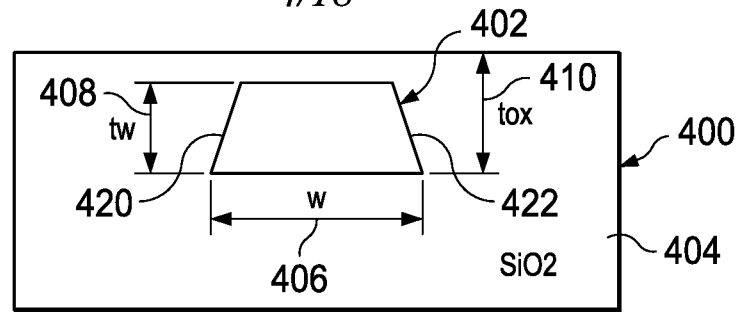


FIG. 4

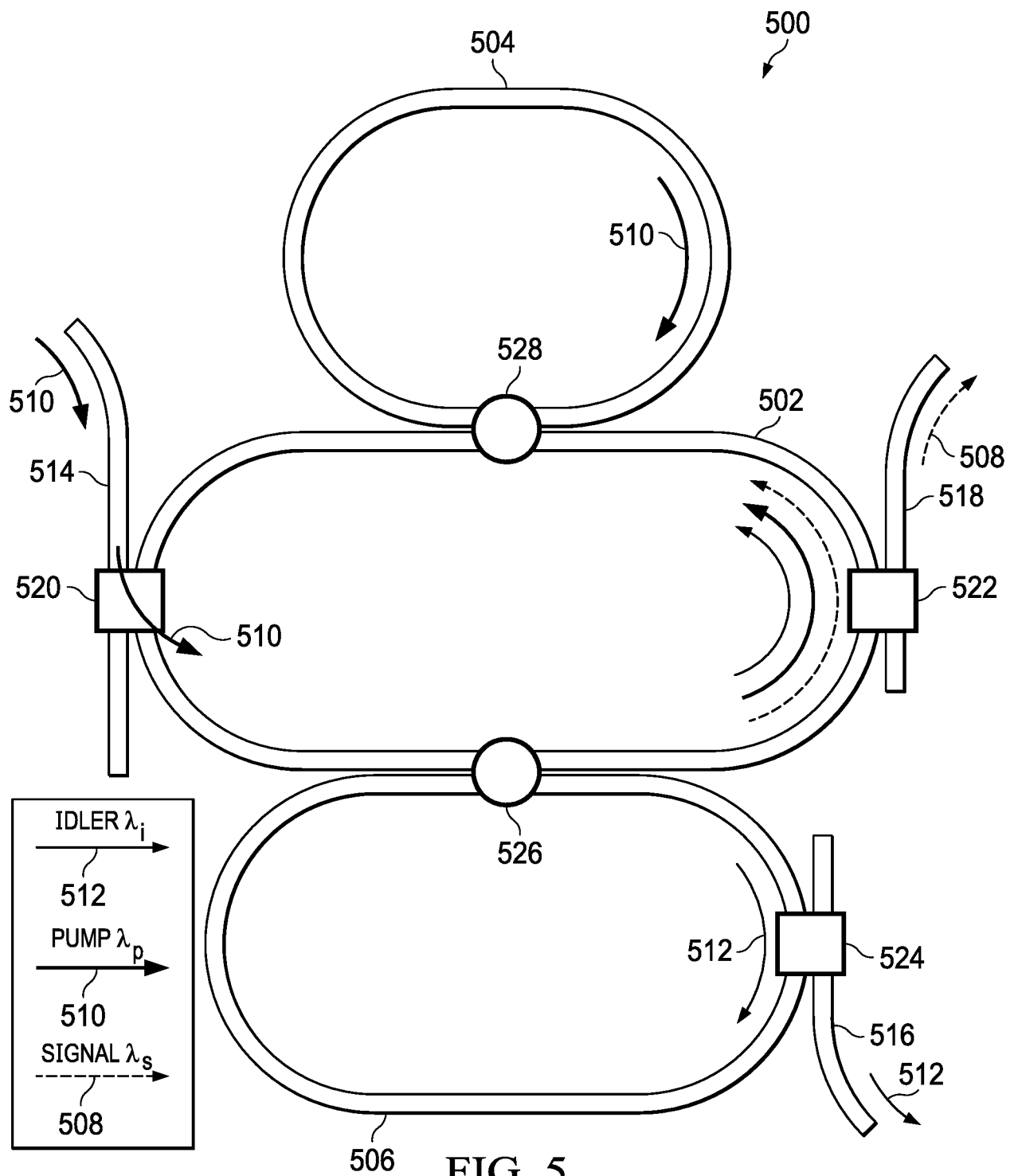


FIG. 5

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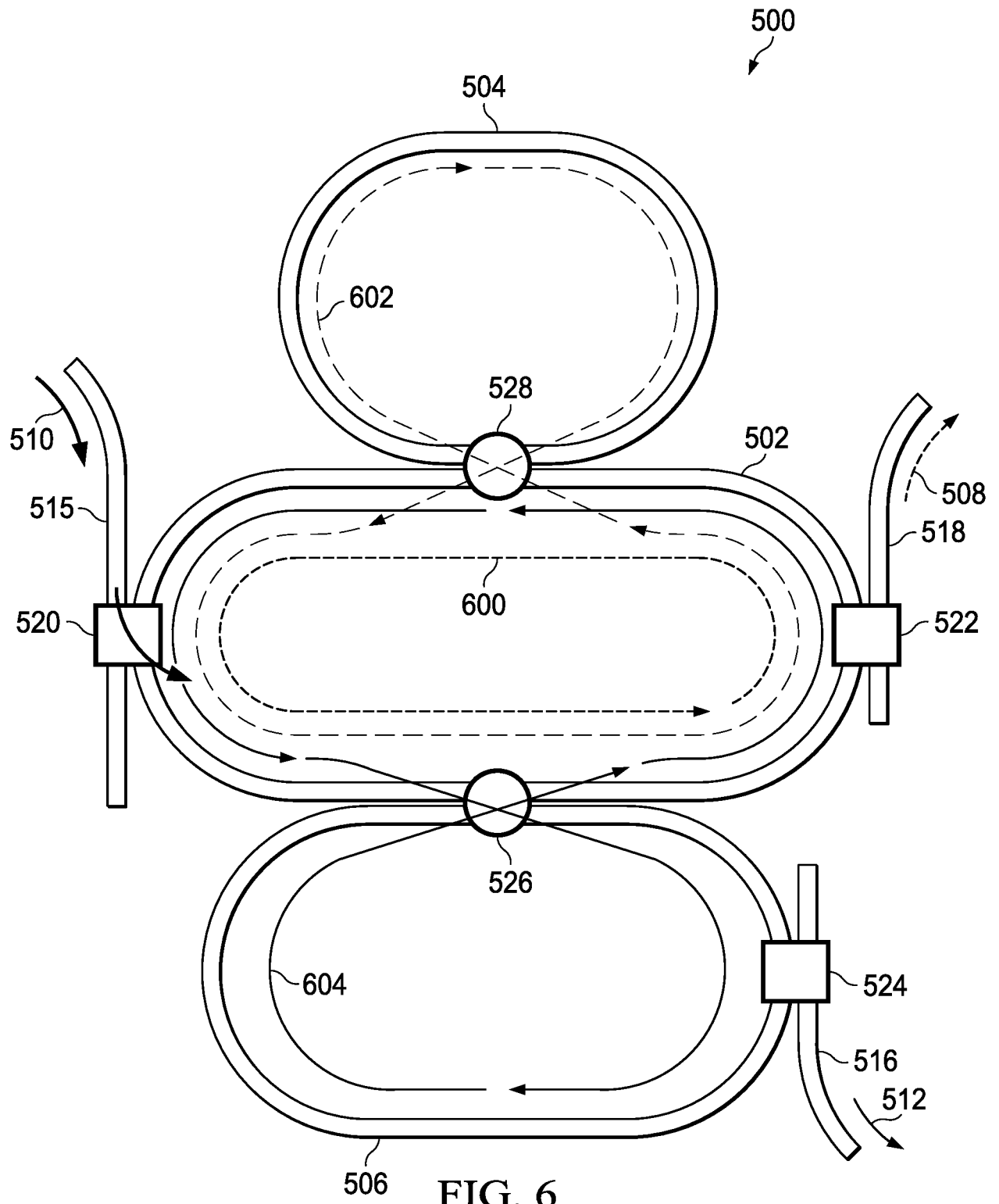


FIG. 6

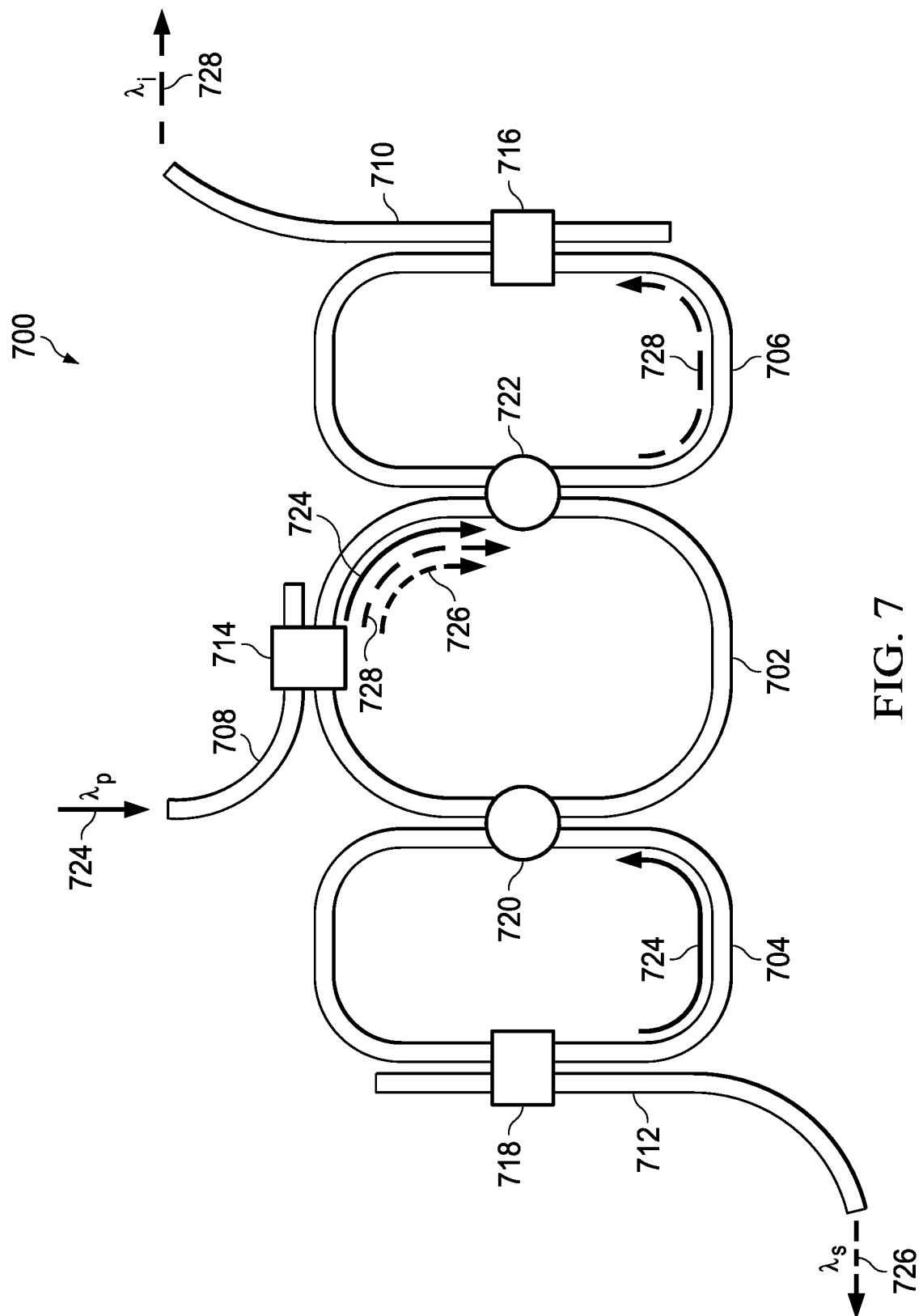


FIG. 7

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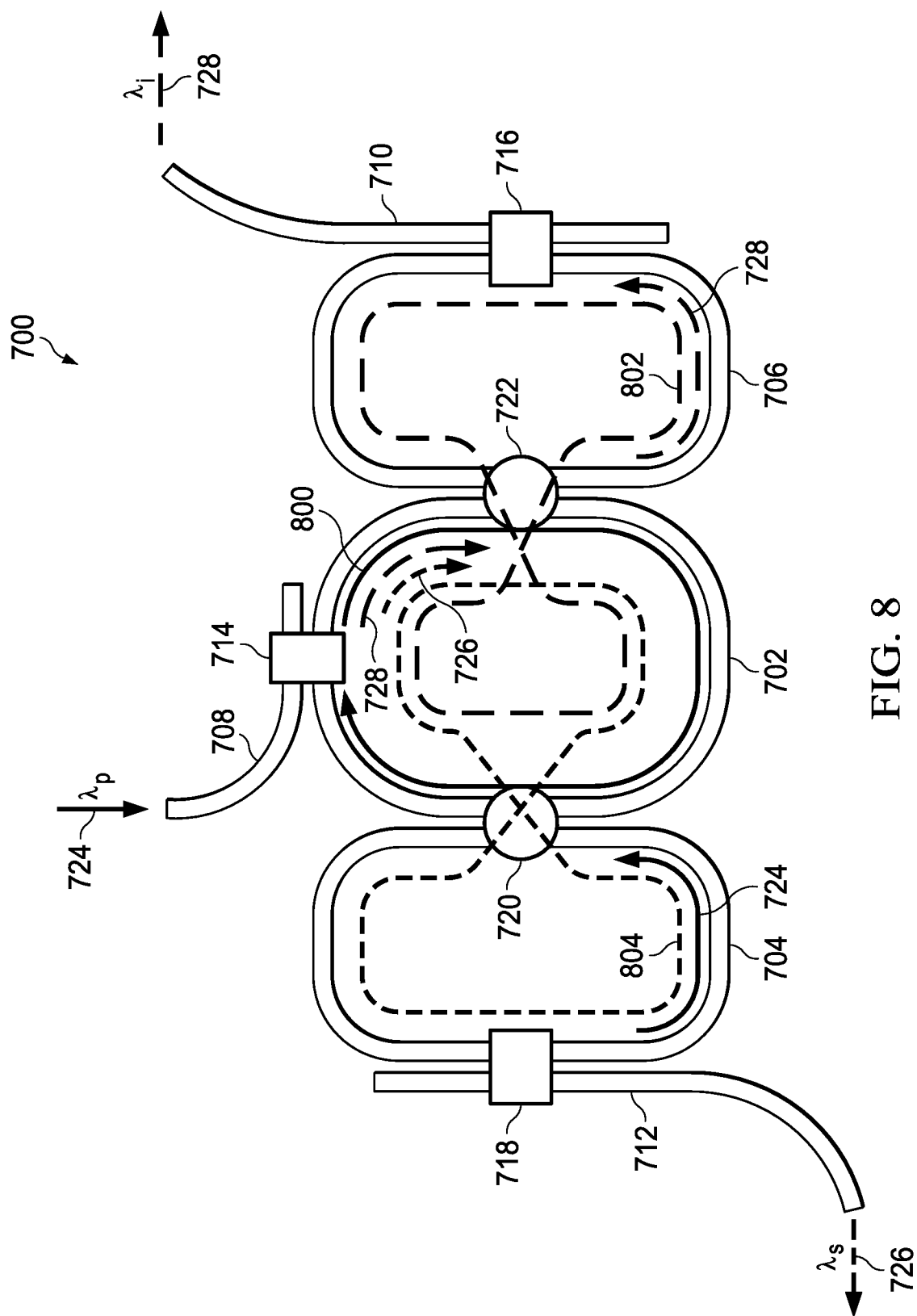


FIG. 8

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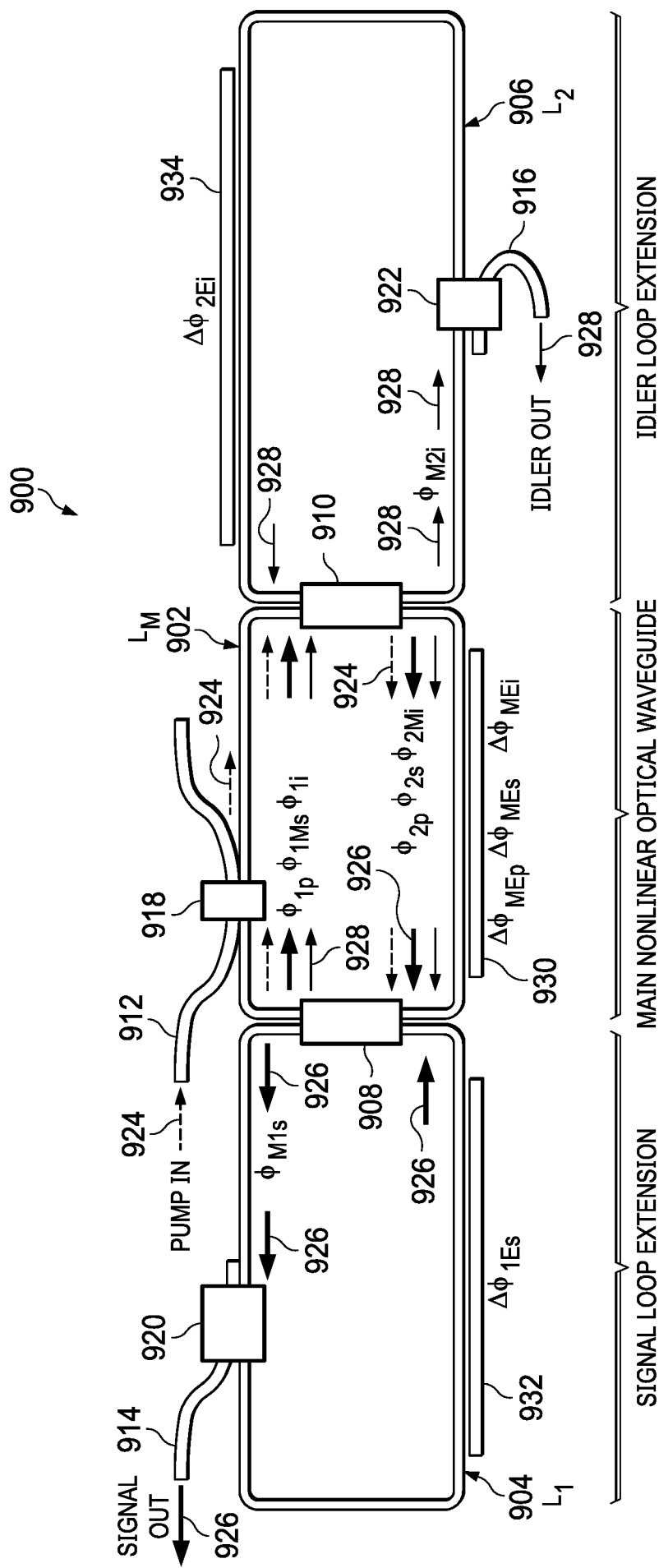


FIG. 9

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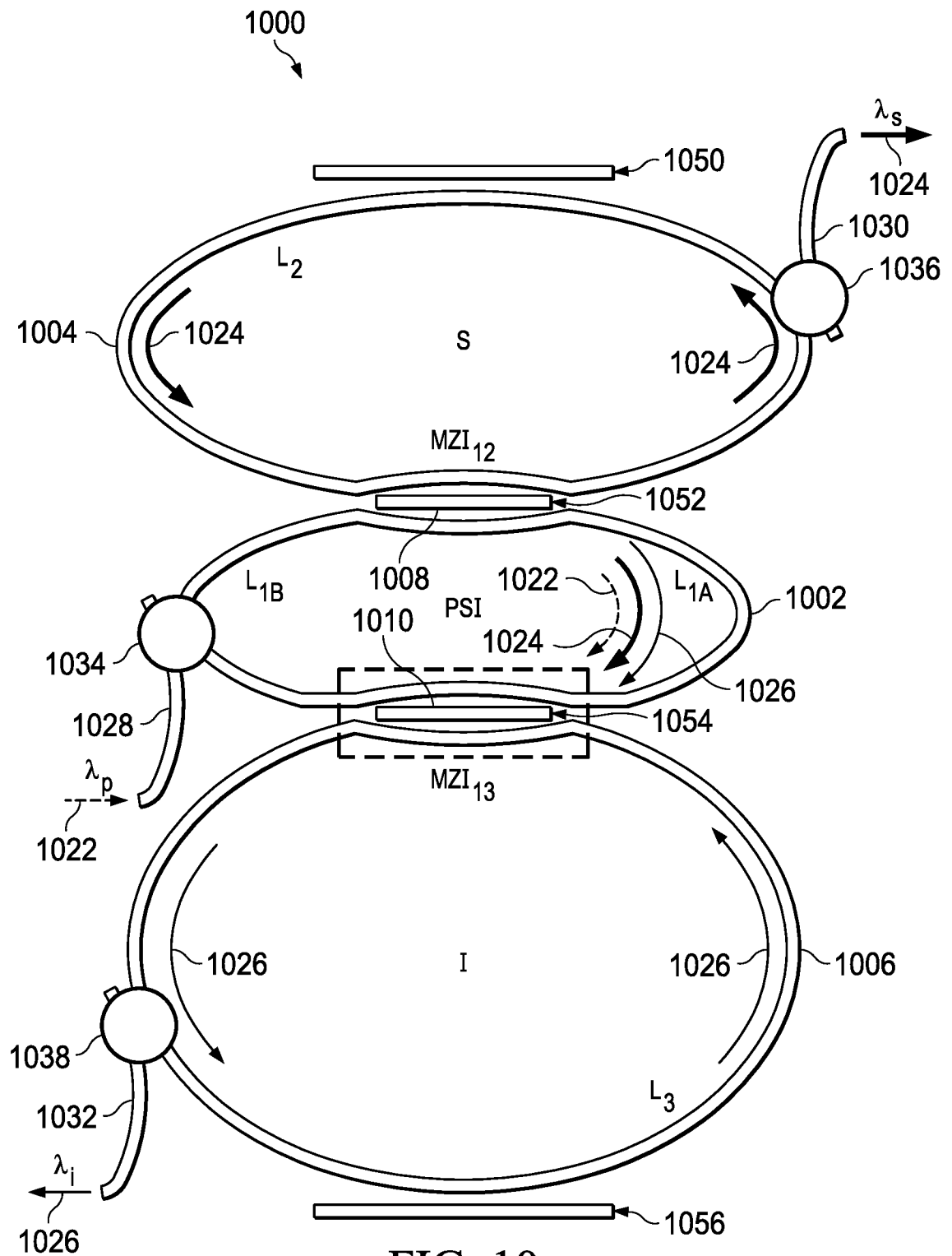
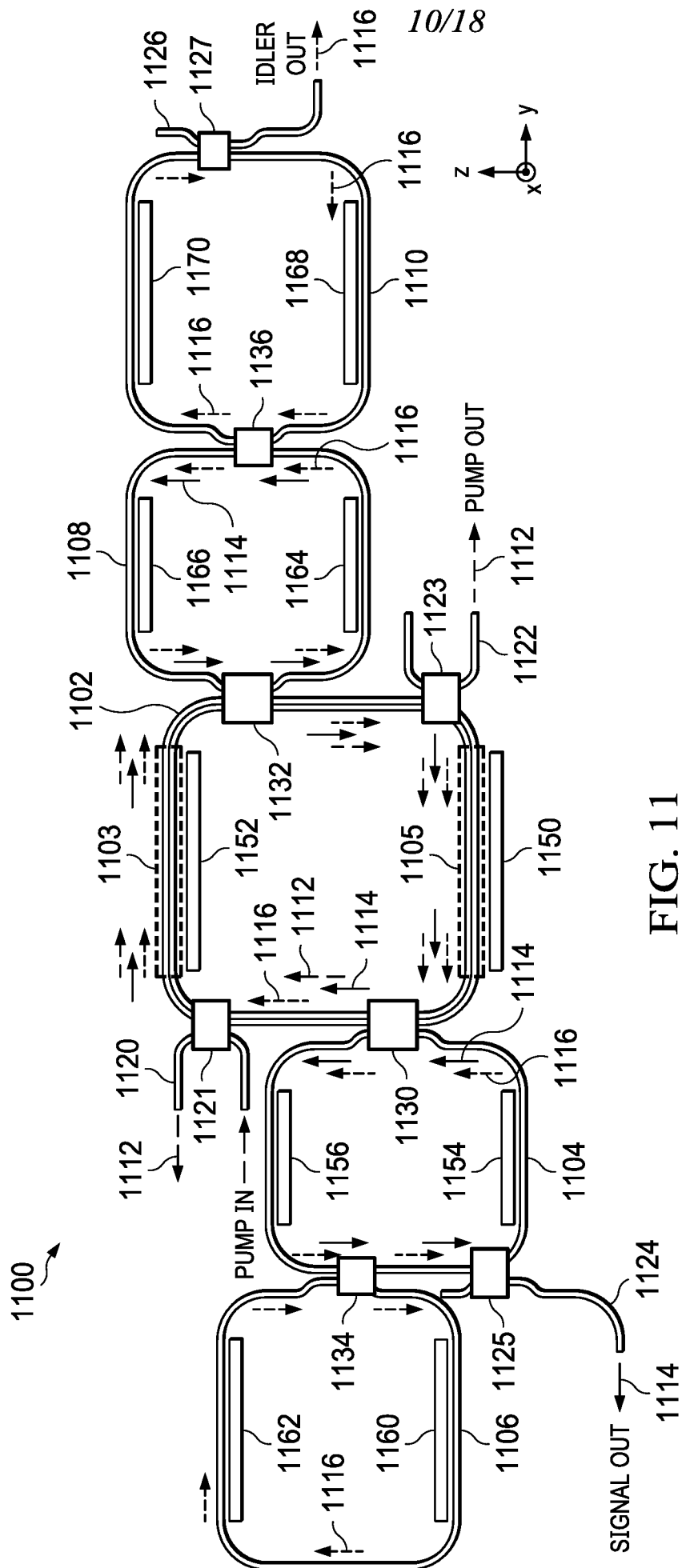
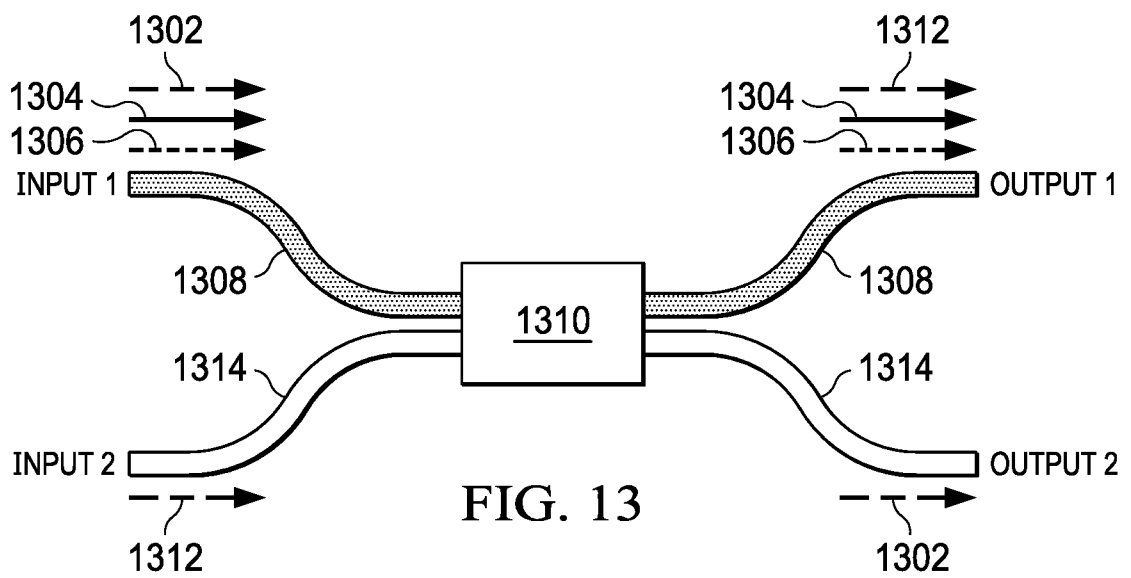
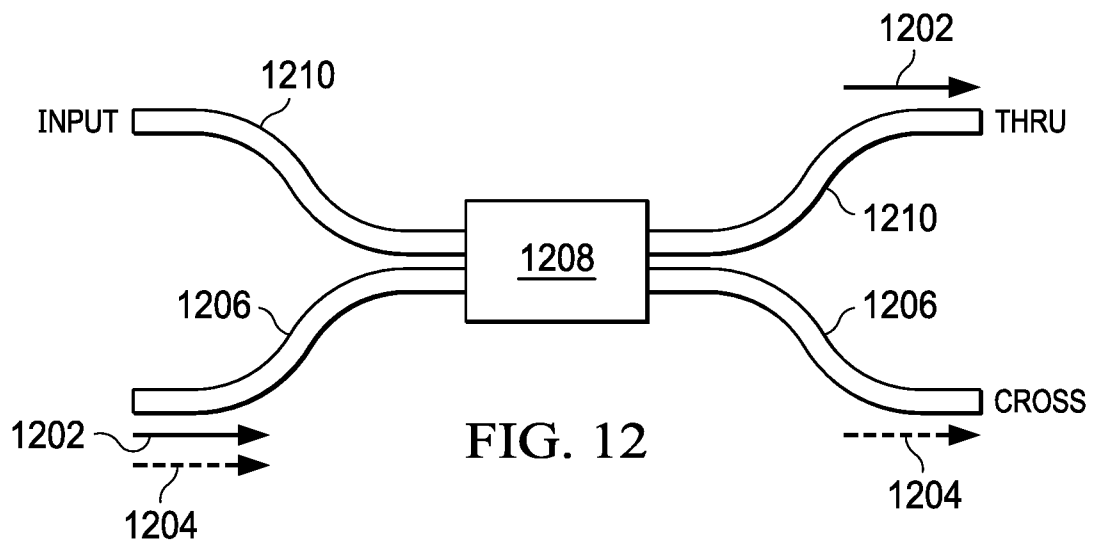


FIG. 10



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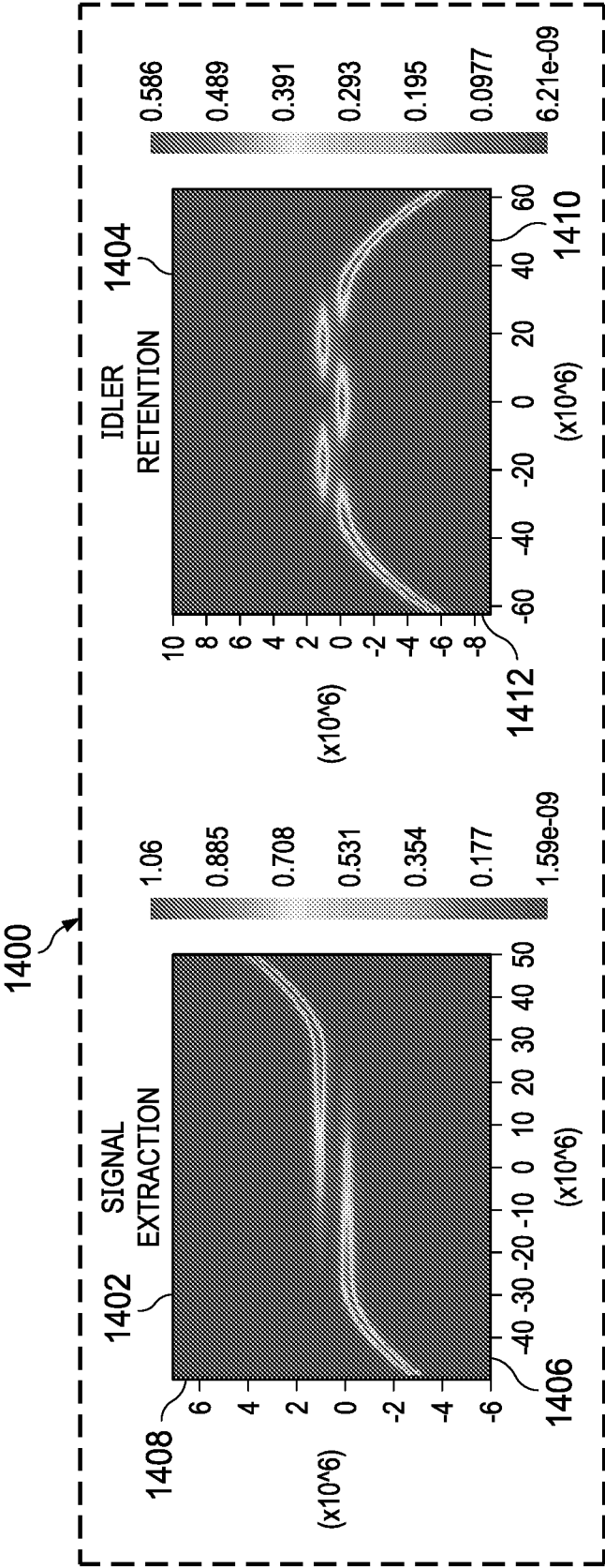


FIG. 14

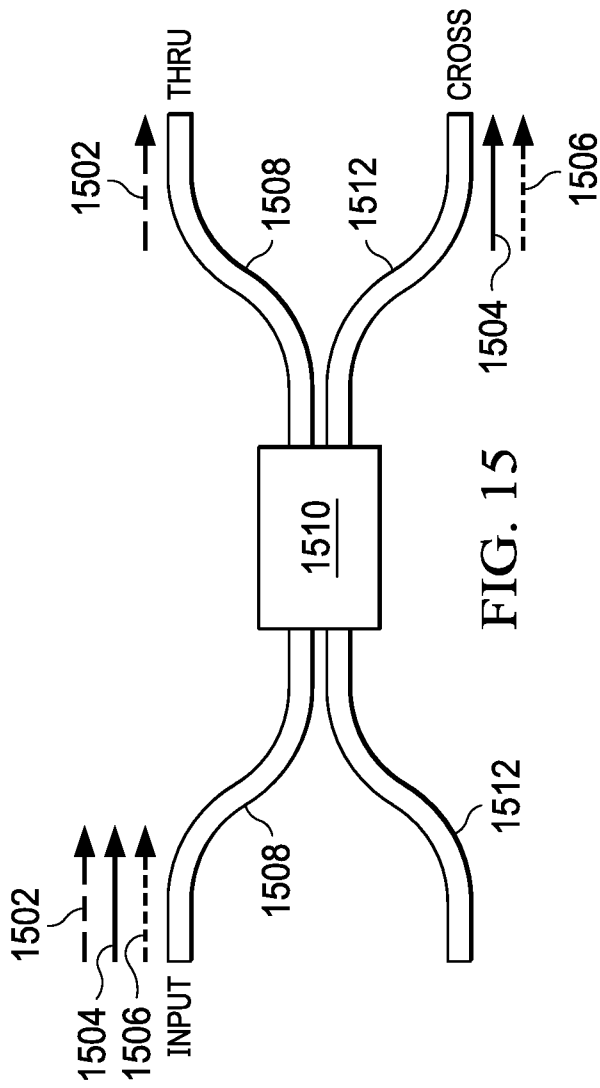


FIG. 15

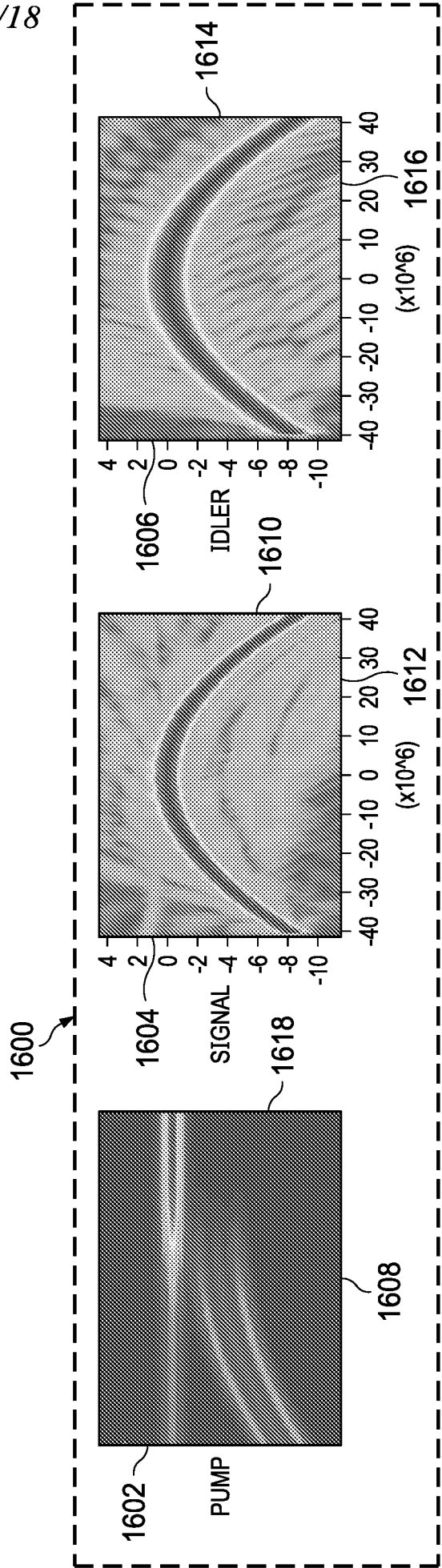


FIG. 16

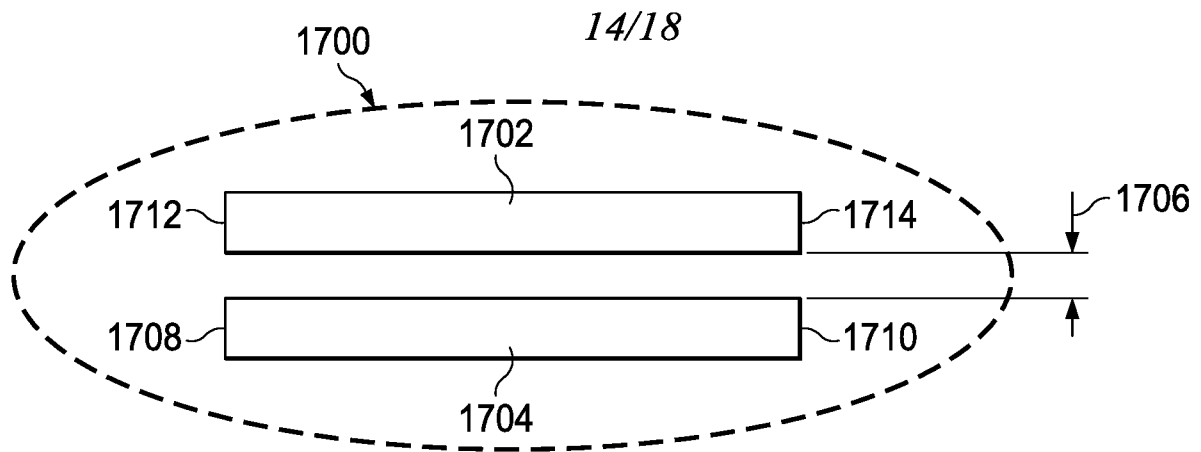


FIG. 17

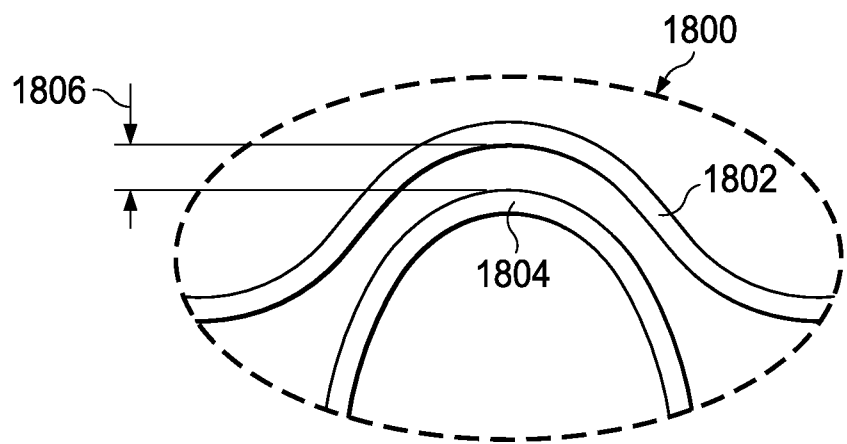


FIG. 18

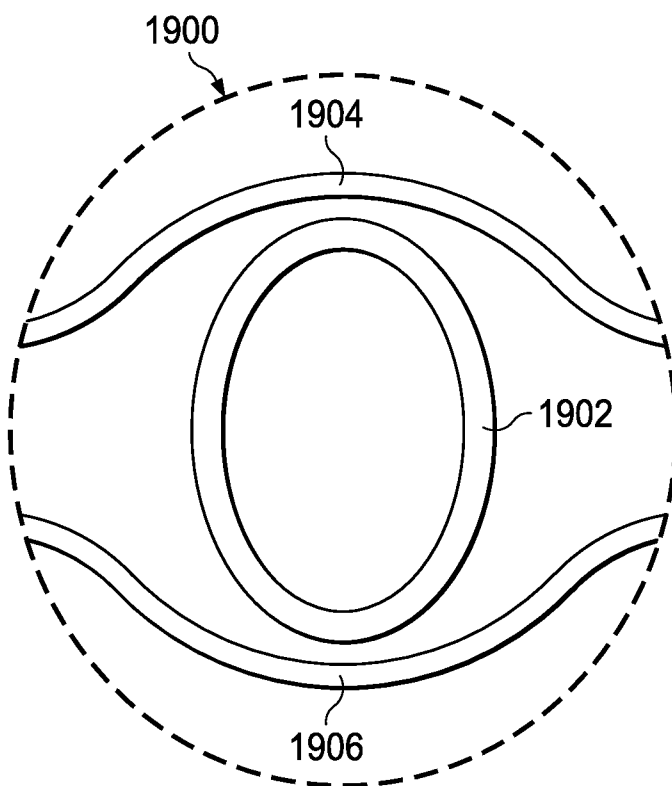


FIG. 19

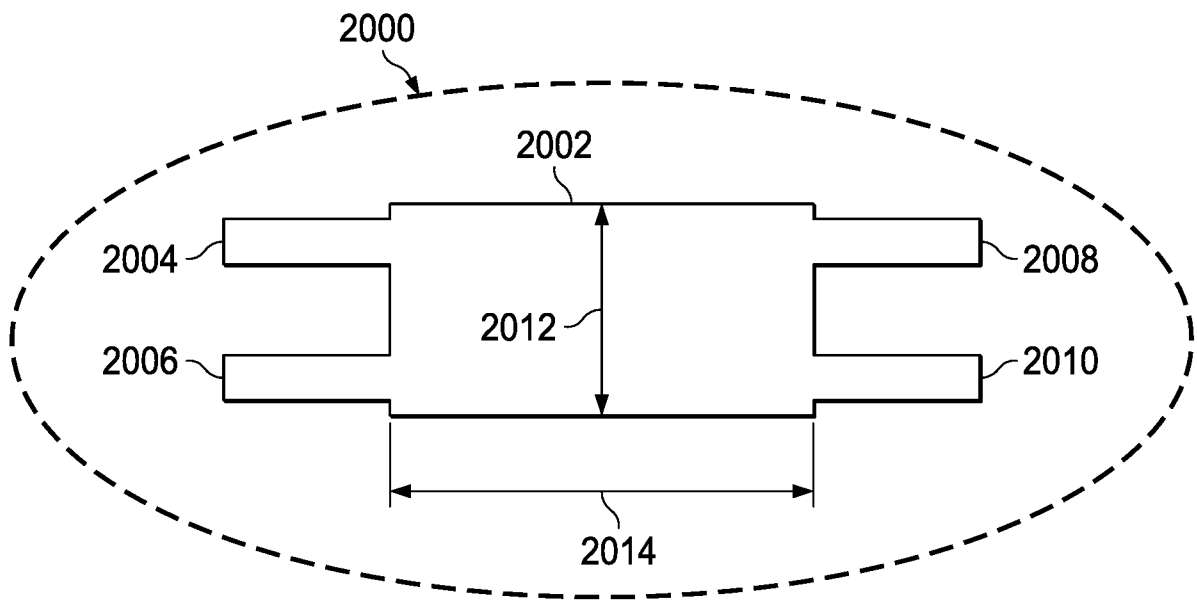


FIG. 20

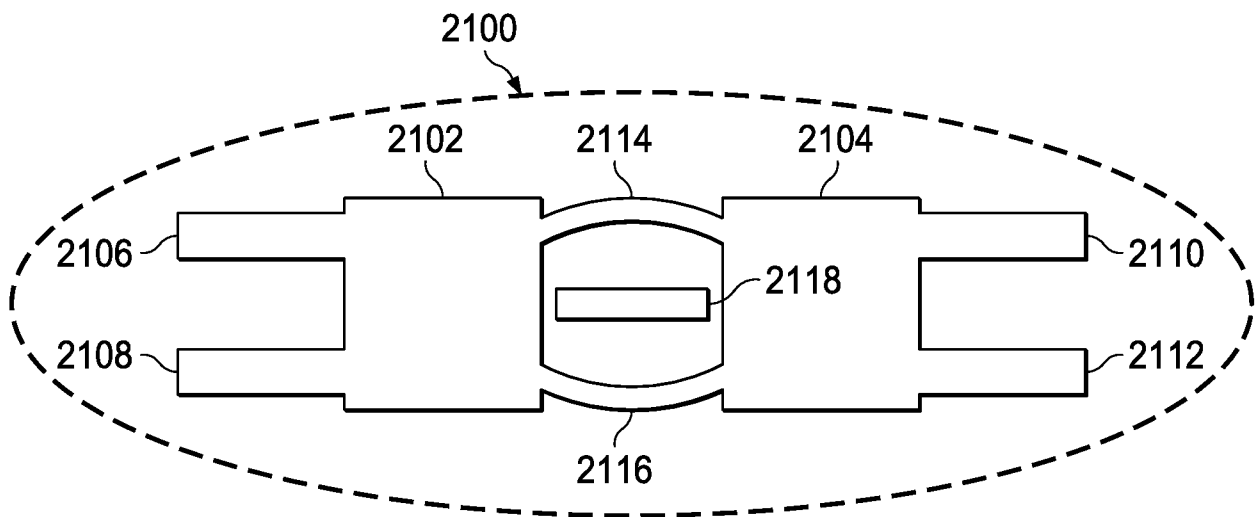


FIG. 21

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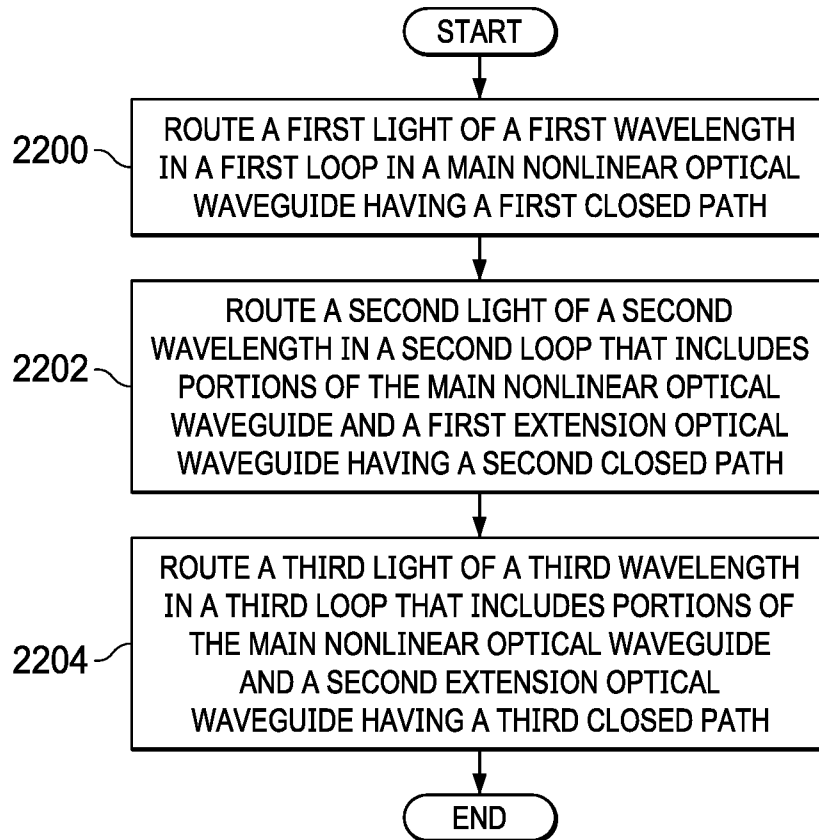


FIG. 22

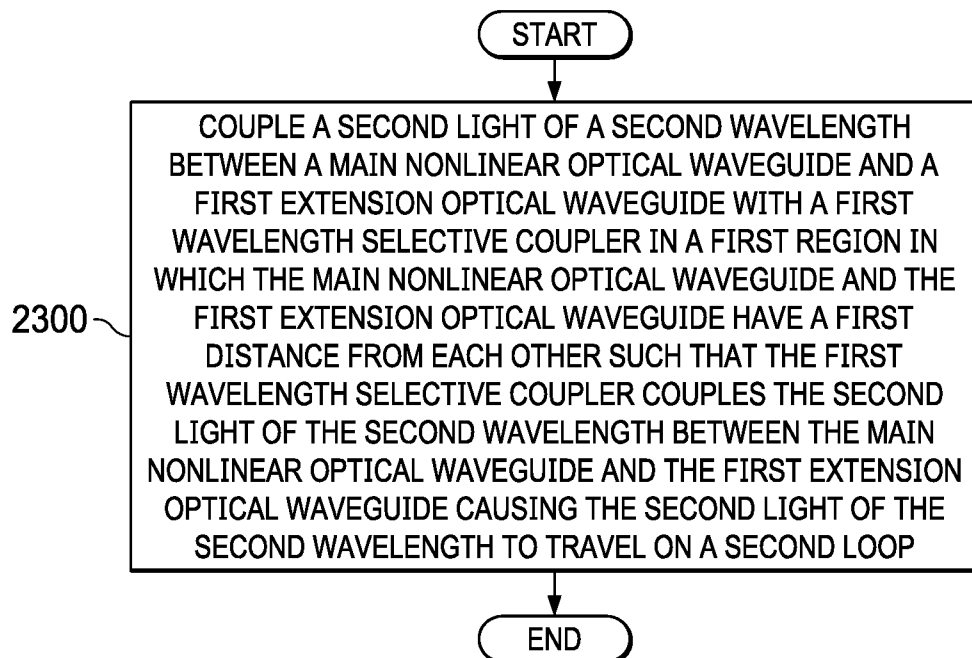


FIG. 23

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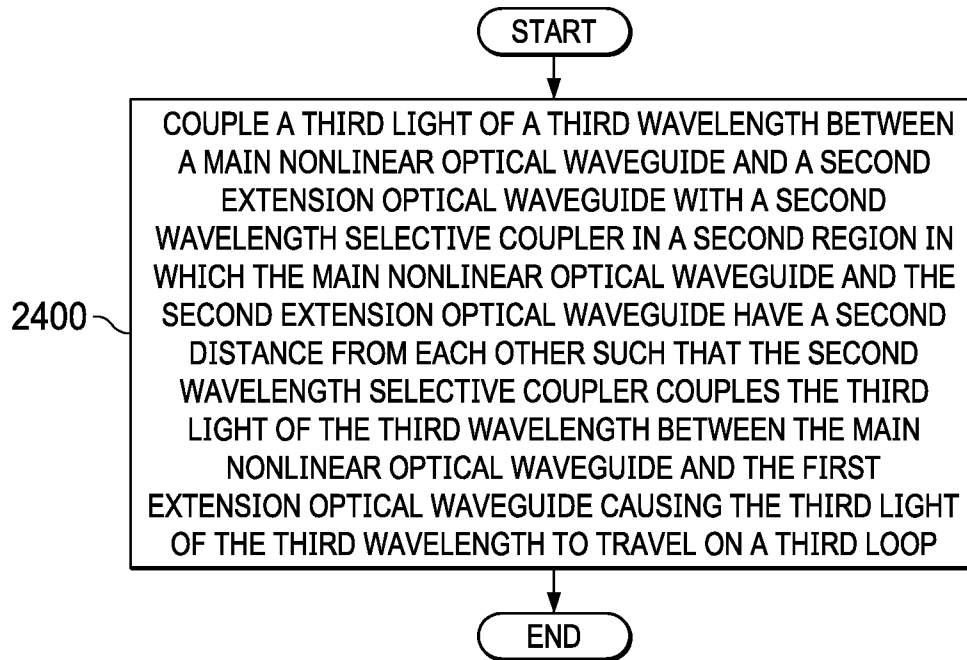


FIG. 24

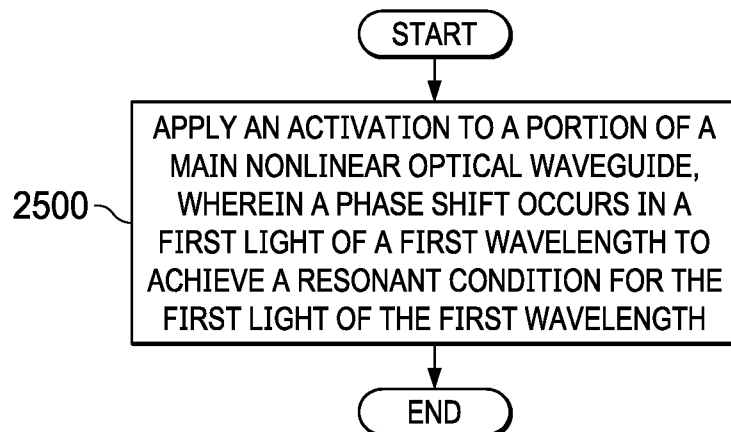


FIG. 25

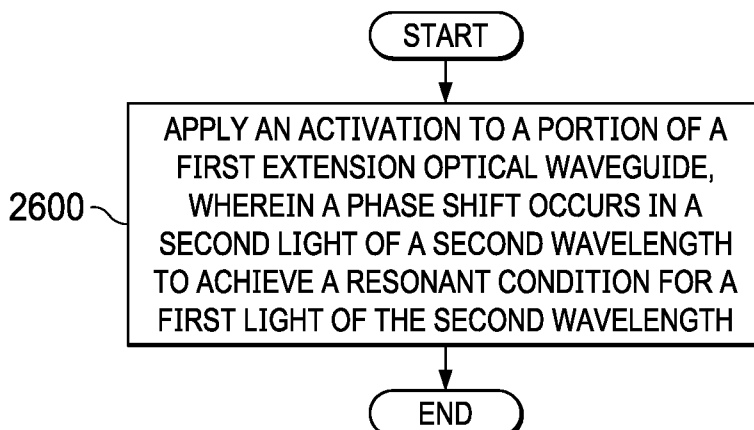


FIG. 26

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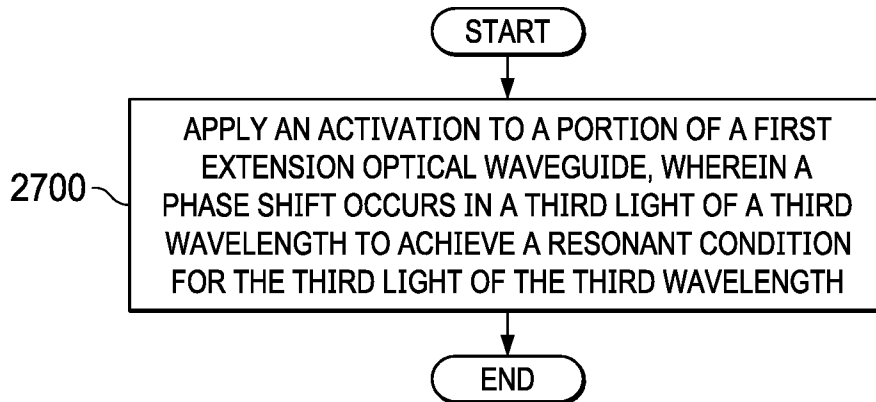


FIG. 27

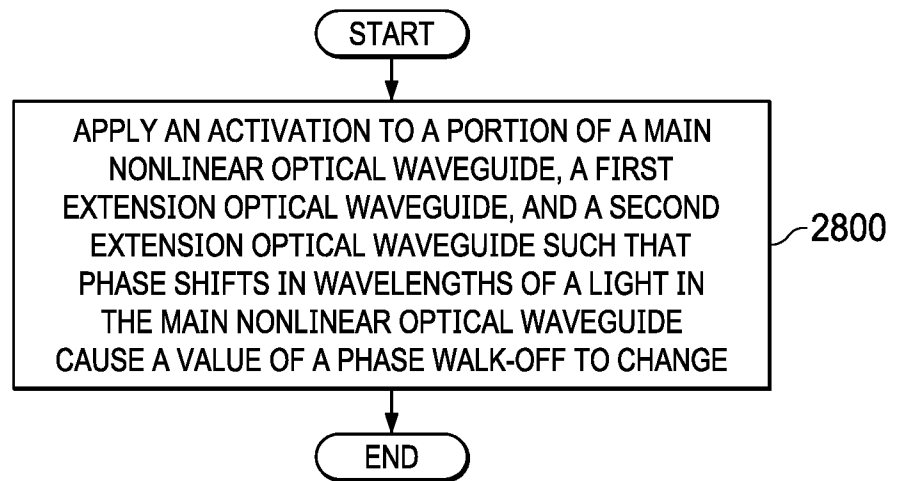


FIG. 28

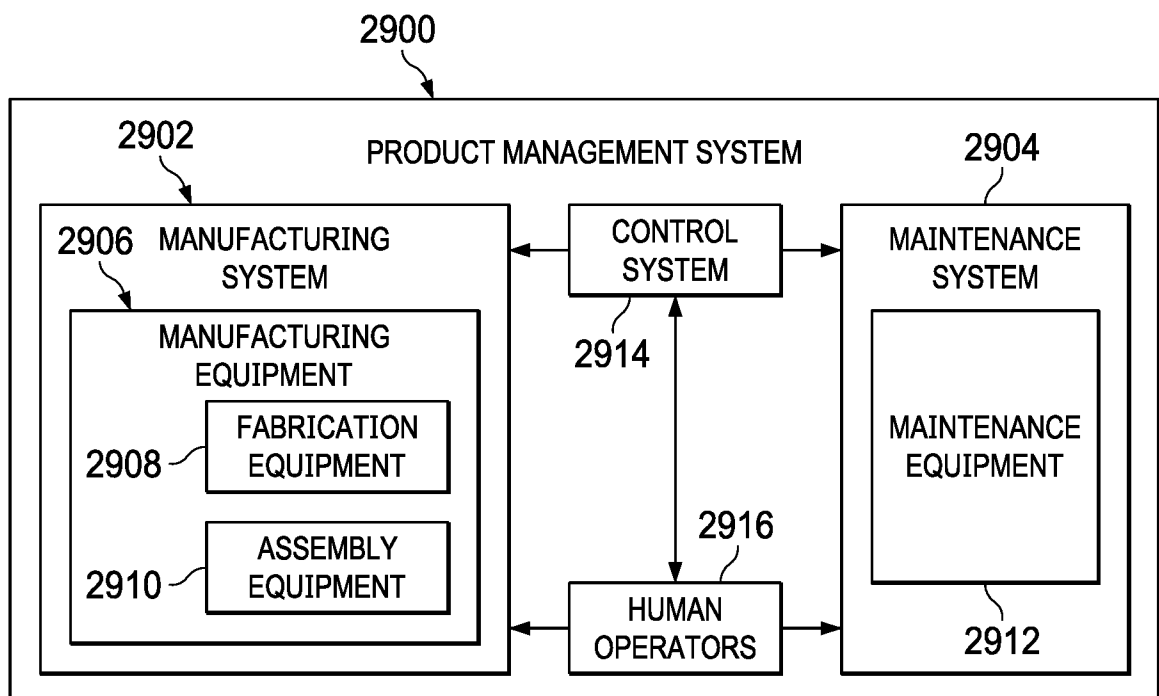


FIG. 29

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2021/071723

A. CLASSIFICATION OF SUBJECT MATTER		
INV.	G02F1/377	G02F1/35
	G02F1/39	G02F1/21
		G02F1/37
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ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED		
Minimum documentation searched (classification system followed by classification symbols)		
G02F G02B		
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* Special categories of cited documents : "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance;; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance;; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family		
Date of the actual completion of the international search		Date of mailing of the international search report
8 February 2022		16/02/2022
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016		Authorized officer Votini, Stefano

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