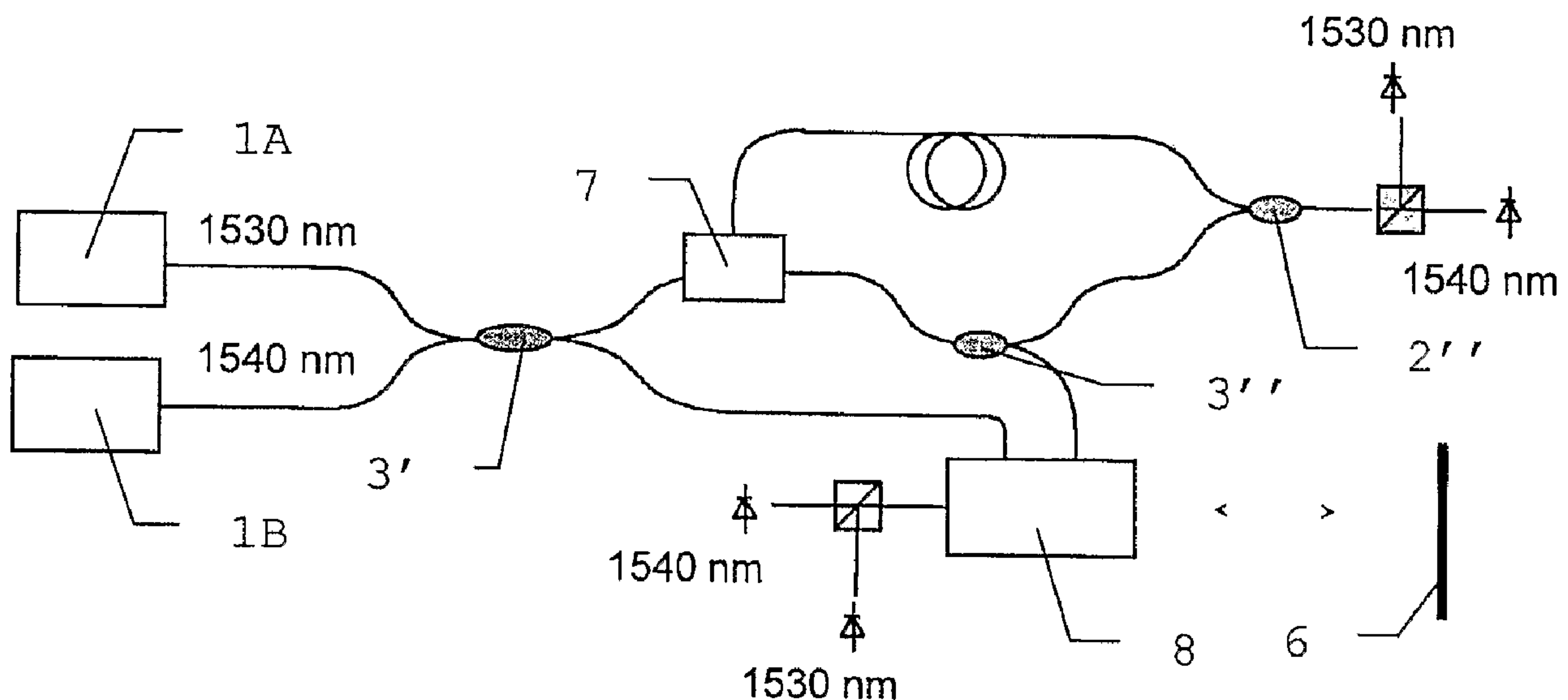




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MODULATION DE FREQUENCE COMPRESSEE SEPARABLE SPECTRALEMENT ET DISPOSITIF CONNEXE
(54) Title: INTERFEROMETRIC DISTANCE-MEASURING METHOD WITH SPECTRALLY SEPARABLE DOUBLE CHIRP
AND DEVICE



(57) Abrégé/Abstract:

In a distance-measuring method, chirped laser radiation with two separable radiation components is emitted to at least one target to be surveyed and via a local oscillator path, the radiation components having an opposite chirp as a time dependency of the modulated wavelengths (λ_1 , λ_2). After reception of the laser radiation scattered back from the target and passed via the local oscillator path, the laser radiation received is converted into signals and the distance to the at least one target is determined from the signals on the basis of interferometric mixing, separation of the radiation components being effected on the basis of their spectral characteristic.

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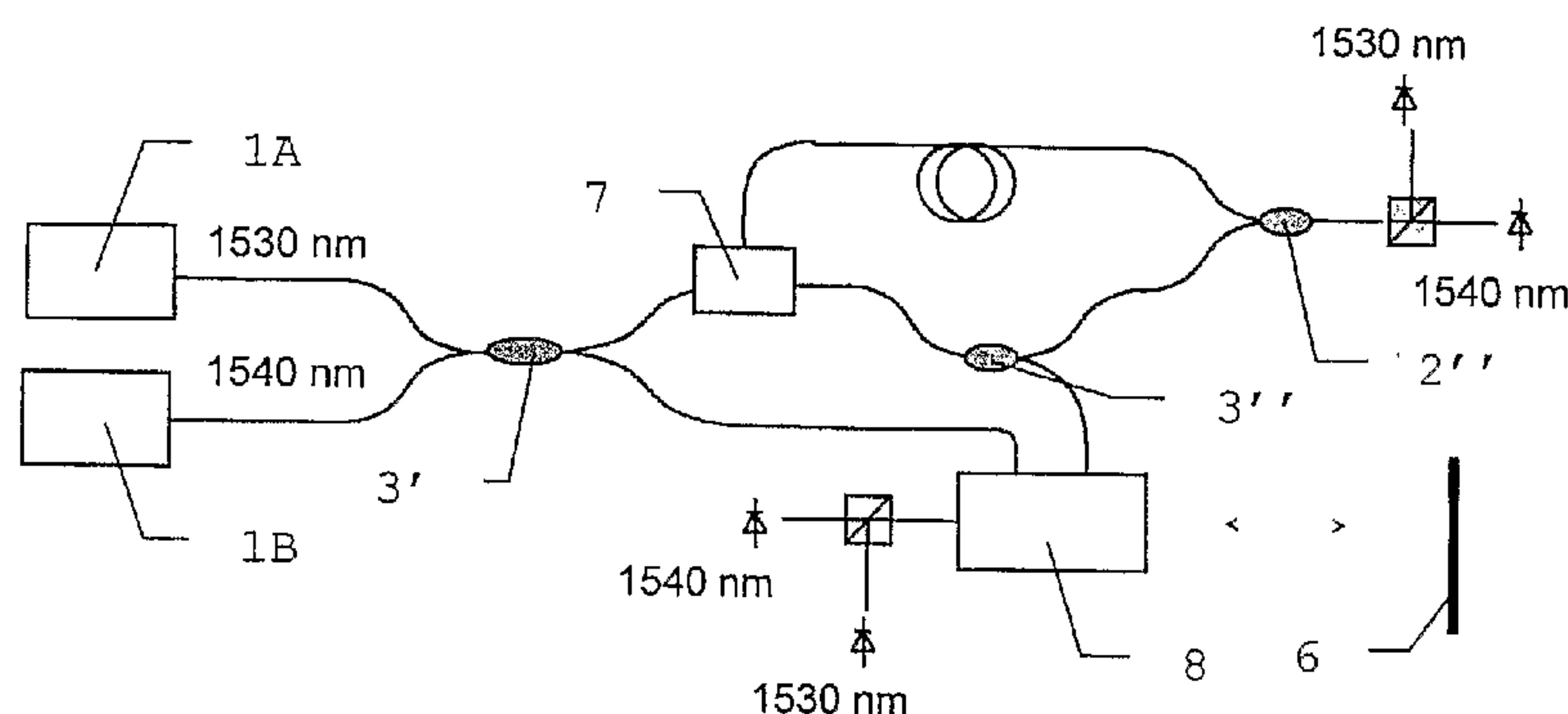


Fig. 5

(57) Abstract: In a distance-measuring method, chirped laser radiation with two separable radiation components is emitted to at least one target to be surveyed and via a local oscillator path, the radiation components having an opposite chirp as a time dependency of the modulated wavelengths (λ_1 , λ_2). After reception of the laser radiation scattered back from the target and passed via the local oscillator path, the laser radiation received is converted into signals and the distance to the at least one target is determined from the signals on the basis of interferometric mixing, separation of the radiation components being effected on the basis of their spectral characteristic.

**INTERFEROMETRIC DISTANCE-MEASURING METHOD WITH
SPECTRALLY SEPARABLE DOUBLE CHIRP AND DEVICE**

The invention relates to an interferometric distance-
5 measuring method with spectrally separable double chirp
and an interferometric distance-measuring apparatus.

10 In the area of electronic distance measurement, various
principles and methods are known. One approach
consists in emitting frequency-modulated
electromagnetic radiation, such as, for example light,
to the target to be surveyed and then receiving one or
15 more echoes from back-scattering objects, ideally
exclusively from the target to be surveyed, it being
possible for the target to be surveyed to have both a
reflective - for example retroreflectors - and a
diffuse back-scattering characteristic.

20 After reception, the optionally superposed echo signal
is superposed with a mixed signal and the signal
frequency to be analyzed is reduced thereby so that
less outlay is required with respect to the apparatus.
25 The mixing can be effected either as a homodyne method
with the signal sent or as a heterodyne method with a
periodic, in particular harmonic, signal of known
period. Thus, the methods differ in that mixing is
effected with the transmitted signal itself or with a
30 harmonic signal having its own frequency. The mixing
serves for transforming the received signal to lower
frequencies and for amplifying said signal.
Thereafter, the transit times and hence - in the case

of a known propagation velocity of the radiation used -
the distances to the targets to be surveyed are
determined from the resulting signal. In a heterodyne
interferometer arrangement, a tuneable laser light
5 source is used for the absolute distance measurement.
In the embodiment which is simplest in principle, the
tuning of the optical frequency of the laser source is
effected linearly. The received signal is superposed
with a second signal which is derived from the emitted
10 light signal. The resulting beat frequency of the
heterodyne mixed product, the interferogram, is a
measure of the distance to the target object. The
apparatuses used for implementing these methods usually
utilize a signal generator as a chirp generator, which
15 impresses a signal on a modulatable radiation source.
In the optical range, lasers which can be chirped by
modulation of the external (for example Bragg grating)
or internal cavity (for example Distributed Feedback
(DFB) or Distributed Bragg Reflector (DBR)) are
20 generally used as radiation sources. In the optical
range, transmitting and receiving optical systems to
which a detector or quadrature detector for heterodyne
mixing, A/D convertor and digital signal processor are
connected down-circuit are used for emission and for
25 reception.

An example of an optical, coherent FMCW distance-
measuring method is described in US 4,830,486, this
method having an accuracy in the region of phase-
30 measuring methods in combination with a short measuring
time. A chirp generator produces a linear frequency-
modulated signal which is divided into a measuring
signal and local oscillator signal, the two signals

being superposed in a receiver.

The change in the wavelength of the emitted light signal represents the scale of the measurement. This
5 is generally not known and therefore has to be determined in an additional measurement. For this purpose, in the prior art, for example, a part of the emitted light is passed via a reference interferometer having a defined reference length. The change in the
10 wavelength of the emitted light signal as a function of time can be inferred from the resulting beat product on the basis of the known reference length. If the reference length is not known or is unstable, for example owing to temperature influences, it can be
15 determined via an additional calibration unit, for example a gas cell or a Fabry-Perot element.

EP 1 696 201 discloses such a distance-measuring method comprising emission of frequency-modulated
20 electromagnetic radiation to at least one target to be surveyed and subsequent reception with heterodyne mixing of the radiation scattered back from the target, the radiation being passed in parallel over an interferometric reference length.

25 While a stationary target has a defined distance invariable as a function of time, moving or vibrating targets present some problems. A constant movement of the target leads, during tuning, to opposite Doppler
30 shifts for the different directions of the frequency ramp. Thus, a movement leads, for example, to a positive Doppler shift on passing through an ascending frequency ramp, whereas a negative Doppler shift is

produced in this case on passing through the descending ramp. By using successive ascending and descending ramps, this effect can be compensated.

5 However, the use of ramps following one another as a function of time, i.e., different or opposite chirps of the laser radiation, also reduces the useable measuring rate by a factor of two, for example from 1 kHz to 500 Hz, i.e. to half. Moreover, this approach is based on
10 the fact that there is a constant target velocity during the time taken for passing through the two ramps. Accelerations of the target during the measuring process or vibrations cause errors in the measured distance.

15

In order to eliminate this problem, US 7,139,446 proposes using two simultaneous and opposite frequency ramps, i.e. emitting radiation having two radiation components with opposite chirp, which also avoids a
20 reduction of the measuring rate. In order to be able to separate these radiation components with respect to measurement, the emission and detection thereof is effected with different polarization. By means of this approach, accelerations can be detected and vibrations
25 eliminated. The separation of the two radiation components by the different polarization does however require that preservation of polarization is ensured within the setup. A setup using fibre optics therefore requires polarization-preserving fibres and is
30 susceptible to errors in the mutual orientation of the fibres relative to one another or the design of the connections. Moreover, this approach is based on the fact that the target too has polarization-preserving

properties, i.e. and the target results in no influences at all on polarization. For producing the two radiation components, two laser sources coupled in in orthogonal polarizations and two detectors oriented in orthogonal polarizations are used.

However, the use of polarized light has disadvantages in measurements to metallic surfaces. Metallic surfaces having a microroughness, as is usual in the case of technical surfaces, lead to depolarization in the case of obliquely incident light. This was investigated in detail in the prior art, both experimentally, cf. for example K.A. O'Donnell and E.R. Mendez, *"Experimental study of scattering from characterized random surfaces"*, J. Opt. Soc. Am. A/Vol 4, No. 7, July 1987, pages 1194 - 1205, or Gareth D. Lewis et al., *"Backscatter linear and circular polarization analysis of roughened aluminum"*, Applied Optics, Vol. 37, No. 25, September 1998, pages 5985 - 5992 and theoretically in simulations, cf. for example E.R. Mendez et al., *"Statistics of the polarization properties of one-dimensional randomly rough surfaces"*, J. Opt. Soc. Am. A, Vol. 12, No. 11, November 1995, pages 2507 - 2516, and G. Soriano and M. Saillard, *"Scattering of electromagnetic waves from two-dimensional rough surfaces with an impedance approximation"*, J. Opt. Soc. Am. A, Vol. 18, No. 1, January 2001, pages 124 - 133, so that a substantial limitation of the usability of the method described in US 7,139,446, results.

The usability of interferometric distance-measuring methods of the prior art with high measuring rates,

which are also suitable for surveying vibrating or moving targets, is therefore not possible or possible only under restricting conditions for metallic surfaces.

5

It is therefore the object of the invention to provide an improved distance-measuring method with double chirp and such an apparatus.

10 A further object of the invention is to provide a corresponding distance-measuring apparatus comprising a simplified and more robust setup, in particular without the use of polarization-preserving fibres.

15 A further object of the invention is to provide a solution which permits precise distance measurements by methods with double chirp even to metallic surfaces and avoids or reduces polarization-related error effects.

20

The solution according to the invention is based on an
25 interferometric distance-measuring arrangement, such as, for example, the heterodyne interferometer arrangement disclosed in EP 1 696 201. According to the invention, distinguishability between the two frequency curves is provided by a spectral separation,
30 this either being based on chromatic filtering of the different absolute optical frequencies or wavelengths of the chirped laser sources before or during detection or, with the use of a modulator (optical frequency

increase), being effected by electric filtering of the different beat frequencies of the up- and down-chirping laser sources in the detected signal.

5 In the case of chromatic filtering, the radiation generated has two radiation components with different absolute optical frequencies or wavelengths, which are chosen so that separation on the receiving side is possible. One embodiment uses, for producing these
10 radiation components, two separate and oppositely tuneable laser sources, e.g. distributed feedback laser diodes, with different average wavelength or frequency, e.g. 1530 nm and 1540 nm, onto which modulation is effected with opposite frequency ramps for producing a
15 double chirp. The radiation of these laser sources can therefore be chromatically filtered. A corresponding distance-measuring apparatus can be setup with standard single-mode fibres, preservation of polarization not being necessary, in contrast to devices of the prior
20 art. Since separation of the radiation components is possible chromatically, for example by means of a chromatic beam splitter or optical filtering with two separate detectors or with two spectrally selective detectors, the polarization-changing behaviour of
25 metallic target surfaces does not affect the measurements, so that undisturbed elimination of vibration influences is possible. As also described in EP 1 696 201, a reference interferogram can be recorded for both laser sources.

30

Electric filtering can be carried out by an analogue or digital method. In the case of analogue electric filtering, for example, high-pass and low-pass filters

are used for spectral separation of the up- and down-chirping signals. In the case of digital electric filtering, the spectral separation of the different beat frequencies is effected by suitable digital filters which in terms of hardware can be integrated in ASIC or FPGA components or in terms of software can be implemented in signal processing. In the case of electric filtering, spectral separation of the signals from the two laser sources is achieved in the frequency spectrum of the detected signal by discrimination of positive and negative signal frequencies, considered relative to the modulation frequency. In this way, chromatic filtering of the laser signals is not required. This method permits in particular the use of wavelengths which are close together, so that the central carrier wavelengths of the laser sources can also be identical. In particular, it is also possible to realize an overlapping region of the tuning curves, which makes it possible to match the wavelengths of the two optical sources relative to one another. In this case, a single detector is sufficient for detection.

For both forms of implementation of signal separation, i.e. both chromatic and electric filtering, a so-called quadrature detector can also be used in the detection for simple phase determination, either electrically or optically.

The distance-measuring method according to the invention and the distance-measuring apparatus according to the invention are described or illustrated in more detail below, purely by way of example, with reference to working examples shown schematically in

the drawing. Specifically,

Fig. 1 shows the schematic diagram of the time dependency of the wavelength for interferometric distance-measuring methods;

Fig. 2 shows the schematic diagram of the time dependency of the wavelength for interferometric distance-measuring methods with opposite chirp;

Fig. 3a-b show the schematic diagram of a first embodiment of the distance-measuring apparatus according to the invention;

Fig. 4 shows the schematic diagram of a second embodiment of the distance-measuring apparatus according to the invention and

Fig. 5 shows the diagram of a possibility for realizing the second embodiment, on the component side.

Fig.1 illustrates, in a schematic diagram, the time dependency of the wavelength for interferometric distance-measuring methods. The radiation emitted by the rangefinder is frequency-modulated by a signal generator so that ascending and descending ramps form in the variation of the wavelength λ as a function of time. However, this modulation or emission form of the prior art produces ascending and descending ramps with a time separation, i.e. in sequence, so that the measuring rates are halved and changes within the

timescale of a ramp variation or with corresponding periodicities can lead to errors.

5 The prior art therefore proposes, for interferometric distance-measuring methods, the time dependency of the modulated wavelengths λ_1 , λ_2 with opposite chirp, as shown schematically in Fig.2. The radiation emitted to a target thus has two radiation components with different variations of the wavelength as a function of
10 time, i.e. opposite frequency ramps. The radiation components can be emitted in particular with a phase offset of the opposite chirp of exactly 180° , i.e. strictly with the opposite phase. The depth of modulation of the radiation components may be
15 different; in particular, it is also possible not to modulate a source - corresponding to the combination of the frequency modulation method with a classical incremental interferometer.

20 If both radiation components are emitted via a common optical system to a common target or are received by said optical system, separation must be permitted on the receiver side for evaluation of the two radiation components, which is solved in the prior art by
25 different polarizations. According to the invention, the radiation components are separated on the basis of their spectral characteristic on reception and/or evaluation or determination of the distance.

30 A first embodiment of the rangefinder according to the invention is shown schematically in Fig. 3a-b. The distance-measuring apparatus has a laser source for emission with at least two different average carrier

wavelengths, which in the first embodiment with two modulatable beam sources 1A or 1B for producing and for emitting chirped laser radiation to a target 6 to be surveyed, a signal generator 2 impressing two opposite
5 chirps onto the two beam sources 1A and 1B. In principle, however, the two radiation components of the laser radiation to be emitted can also be produced with the use of a single source, for example if subsequent spectral separation or downstream production of the two
10 radiation components, for example by an optically parametric oscillator, takes place. For example, 1530 nm and 1540 nm can be chosen as carrier wavelengths. Both a common signal generator 2 and a signal generator coordinated in each case with one of the laser sources
15 alone can be used for both beam sources 1A and 1B.

The laser radiation thus produced is coupled via a fibre coupler 3 or multiplexer, both into a measuring interferometer 4A and into a reference interferometer
20 4B having a defined reference length, it being possible for both interferometers to be designed, for example, as Mach-Zehnder interferometers. The interferometers each have a detector 5 for receiving the laser radiation scattered back from the target 6 or passed
25 via the local oscillator. The reference interferometer in, for example, etalon or Mach-Zehnder configuration serves for taking into account or compensating nonlinearities in the tuning behaviour of the laser source. If the behaviour of the laser source is
30 sufficiently linear or known and stable, it is also possible in principle to dispense with the reference interferometer. However, this is as a rule not the case. In addition to the reference interferometer, a

calibration unit not shown here, in particular in the form of a gas cell or Fabry-Perot element, can also be integrated in order to determine the length of the reference interferometer. The use of such a calibration component is disclosed, for example, in EP 1 696 201.

Measuring and reference interferometers may also have a common path geometry, i.e. may have a partly common interferometer beam path for measurement or reference arm and local oscillator arm. For the measuring interferometer, the local oscillator arm is defined here by a reflection at the optical exit surface, so that a constant, in particular known distance is determined, further back-reflections being avoided. The measuring arm of the measuring interferometer is on the other hand defined by the reflection at the target 6 to be measured. The back-reflected light of measuring arm and local oscillator arm is finally passed to a common detector in this alternative.

The setup of one embodiment of the detector 5 is shown in more detail in Fig.3b. In addition to the fundamentally possible use of chromatically selective detectors, separation of the laser radiation may also have, for example, a dielectric or dispersive element 5A for chromatic filtering of the back-scattered laser radiation, the radiation components being passed to the detector units 5B after separation. The signal evaluation can be carried out subsequently, for example, on the basis of a heterodyne interferometric mixing method, a corresponding mixer being provided or the detector units 5B being formed as such. The laser

source and the choice of the carrier wavelengths are dependent on the separability and the components which can be used on the detector side, so that the chromatic distance between the two lasers is adapted according to the separability in the detection, which is possible, for example, by a chromatic distance of 20 nm.

A second embodiment of the rangefinder according to the invention is shown in a schematic diagram in Fig.4. This embodiment corresponds in the basic concept of the first embodiment but has an acousto-optical modulator 7 for raising the local oscillator of the two interferometers by the modulation frequency of the modulator 7, for example 50 MHz which facilitates the detectability. The splitting of the radiation is therefore effected via a two-part fibre coupler 3' of altogether three exits for the two interferometers and the modulator 7. At the exit of the interferometers, combination is effected again, prior to detection, by fibre coupler 3'', the exit of which is connected in each case to the detector 5.

For the second embodiment, the optical system 8 used for emitting laser radiation to and receiving said laser radiation from a target 6 is shown schematically in the measuring interferometer.

Fig.5 shows a possibility for realizing the optical components for the second embodiment. The laser radiation is produced by two DFB laser diodes as beam sources 1A and 1B having carrier wavelengths of 1530 nm and 1540 nm, the connections between the optical components being in the form of single-mode fibres.

The laser radiation produced is coupled into the measuring interferometer, the reference interferometer and the acousto-optical modulator 7. The optical system 8 is in the form of a telescope having an at least partly common transmission and reception beam path, the target 6 to be surveyed being part of the measuring interferometer during the measurement. Via the optical paths, the signals are transmitted to the detectors with the detector units for the carrier wavelengths at 1530 nm and 1540 nm. The detector signals are then passed via electric cables to a signal processor. The signal processor performs the processing and evaluation of the signals and optionally controls the two beam sources as a signal generator via control cables.

In a third embodiment, which in principle is the same as the setup of the diagram in Fig.4, the frequency increase of the local oscillator by, for example, 50 MHz is utilized for achieving spectral separation of the opposite chirp signals by electric filtering in the frequency spectrum of the signal. The up- and down-chirping signals appear, depending on direction, to the left and right, respectively of the central modulation frequency. By analogue or digital electric frequency filtering, the signals can easily be separated and can then be further processed as two separate detector signals. The electric filtering of the chirps in the frequency spectrum can thus be effected, for example, digitally and by means of software in the signal processing or by analogue filtering of the electrical detector signals. Since the frequency in the spectrum is determined by the chirp rate but not by the carrier

wavelength of the two laser sources, the central carrier wavelengths λ_1 and λ_2 may also be identical. In this embodiment, too, it is possible completely to dispense with polarization fibres. A standard PIN
5 diode is sufficient for detection, chromatic filtering of the detection as in Fig.5 not being necessary.

CLAIMS:

1. A distance-measuring method comprising the steps
 - emission of chirped laser radiation with two separable radiation components to at least one target to be surveyed and a local oscillator path, the radiation components having an opposite chirp,
 - reception of the laser radiation scattered back from the target and passed via the local oscillator path and determination of at least one distance to the at least one target from the radiation scattered back from the target based on interferometric mixing,wherein the radiation components are separated on the basis of their spectral characteristic.
2. The distance measuring method according to claim 1, wherein the radiation components are separated on reception.
3. The distance measuring method according to claim 1, wherein the radiation components are separated on determination.
4. The distance measuring method according to claim 1, wherein the radiation components are separated on reception and determination.
5. The distance-measuring method according to any one of Claims 1 to 4, wherein the radiation components are emitted with a phase offset of the opposite chirps of 180°.

6. The distance-measuring method according to any one of Claims 1 to 5, wherein the radiation components have different depths of modulation.

7. The distance-measuring method according to any one of Claims 1 to 6, wherein the radiation components are separated on reception by discrimination of positive and negative frequencies around a modulation frequency.

8. The distance-measuring method according to any one of Claims 1 to 7, wherein the radiation components are emitted with different average carrier wavelengths.

9. The distance-measuring method according to Claim 8, wherein the radiation components are separated on reception spectrally.

10. The distance-measuring method according to Claim 9, wherein the radiation components are separated chromatically.

11. The distance-measuring method according to any one of Claims 1 to 10, wherein one of the radiation components is emitted without modulation.

12. The distance-measuring method according to any one of Claims 1 to 11, wherein, on determination of the at least one distance, a reference interferometer serves for taking into account or compensating nonlinearities in the production of the chirp.

13. A distance-measuring apparatus for carrying out the method according to any one of Claims 1 to 8, comprising at least,

- a modulatable laser source for producing and for emitting laser radiation with two separable radiation components to a target to be surveyed,
- a signal generator for modulation of the laser source of the radiation components with two opposite chirps,
- a receiver comprising
 - a measuring interferometer consisting of a measuring arm and a local oscillator arm with at least one detector for receiving the laser radiation scattered back from a target,
 - a mixer for carrying out a heterodyne interferometric mixing method,

wherein the radiation components are separated on the receiver side on the basis of their spectral characteristic.

14. The distance-measuring apparatus according to claim 13, wherein the mixer comprises a reference interferometer for taking into account or compensating nonlinearities in the production of the chirp.

15. The distance-measuring apparatus according to Claim 13 or 14, further including an acousto-optical modulator for raising the local oscillator of the measuring interferometer around a modulated frequency of the modulator.

16. The distance-measuring apparatus according to Claim 15, wherein the separation of the radiation components is achieved by discrimination of higher and lower frequencies around the modulation frequency.

17. The distance-measuring apparatus according to any one of Claims 13 to 16, wherein the laser source has two laser diodes with different average carrier wavelengths.

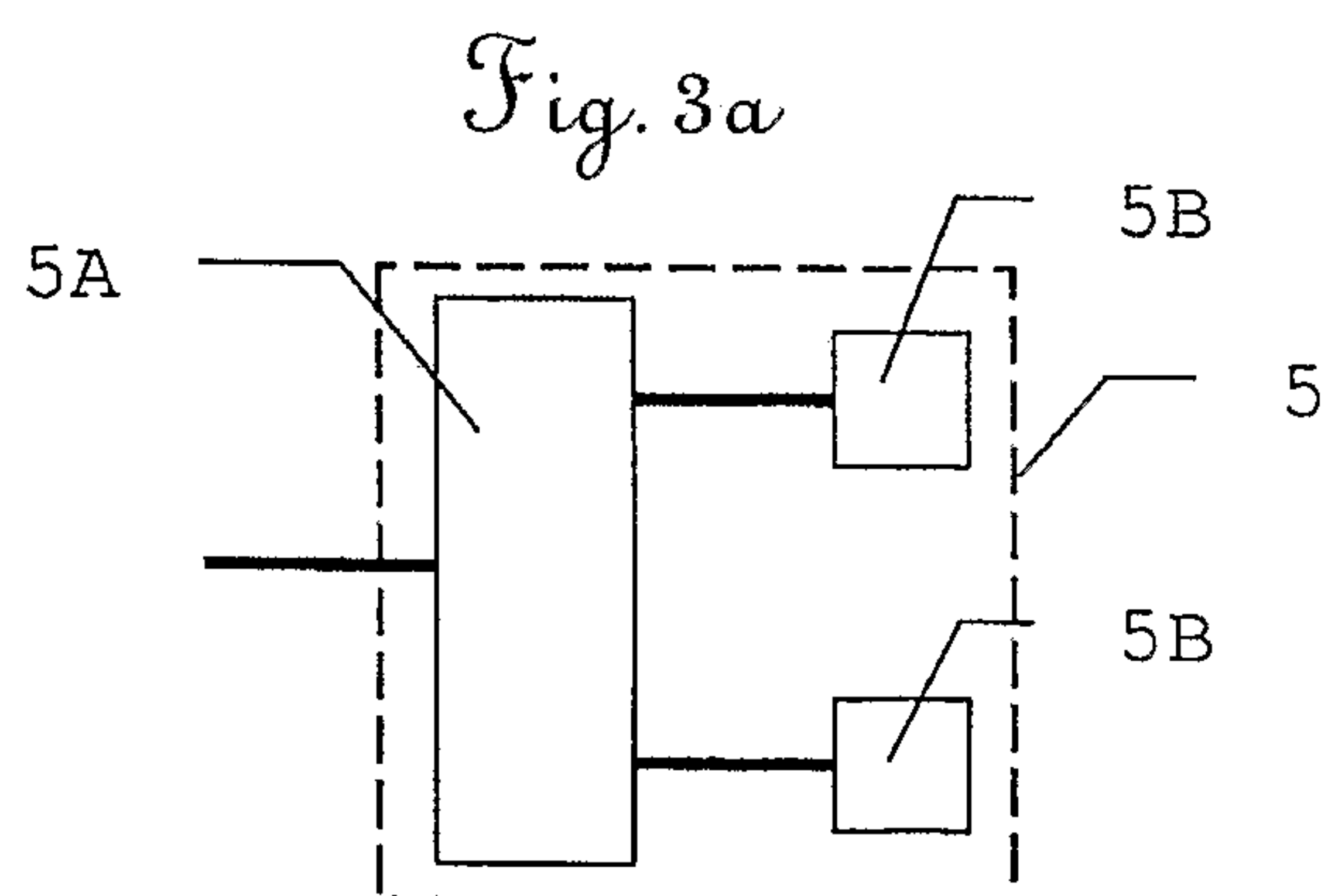
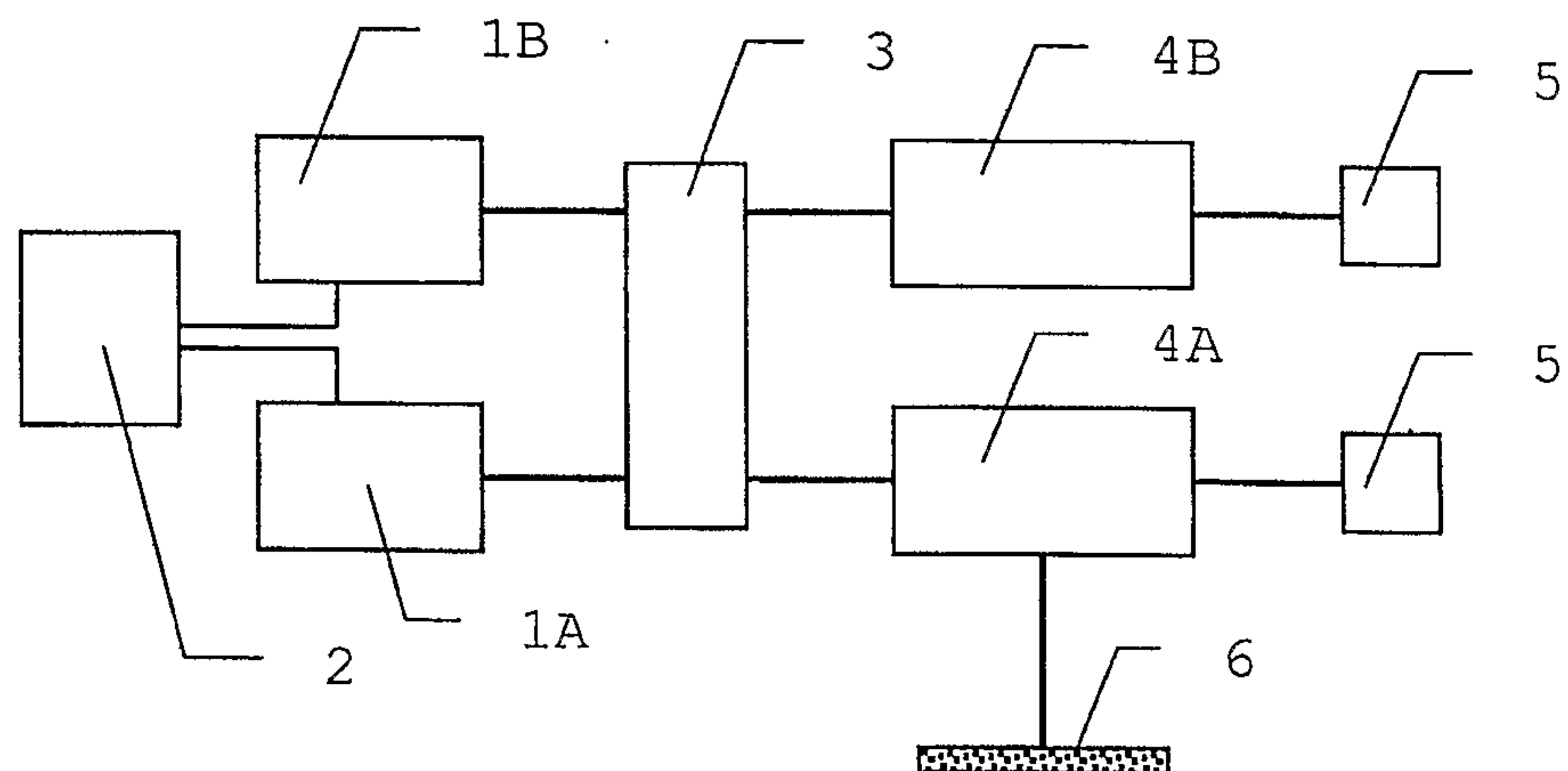
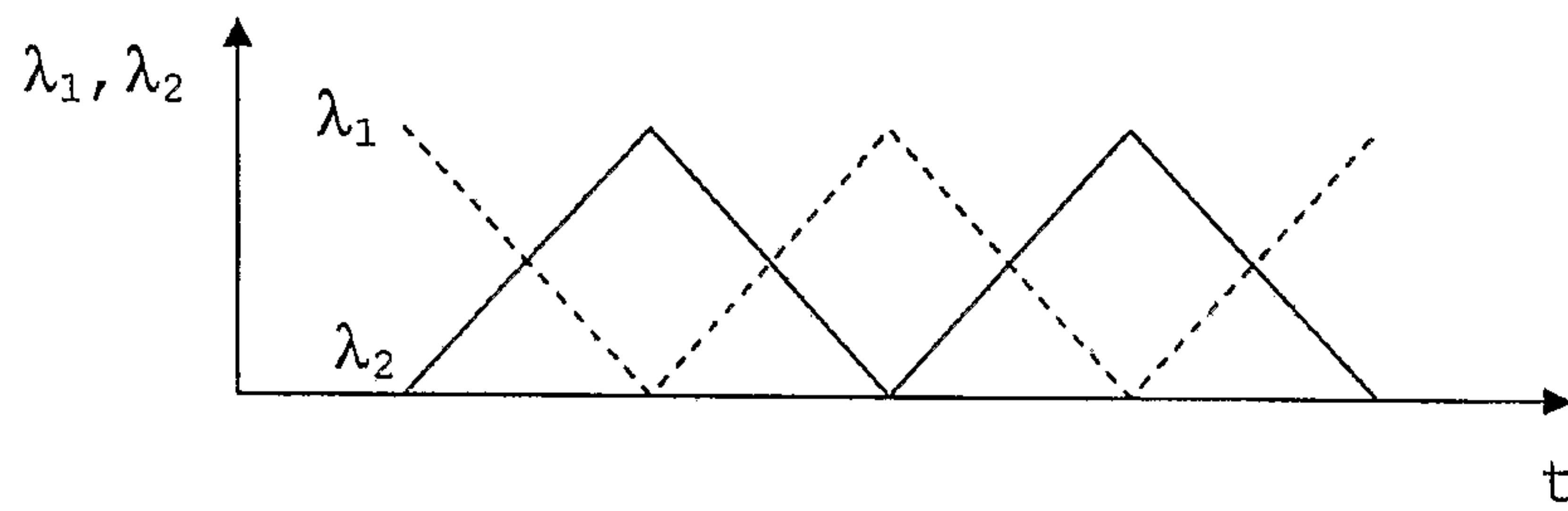
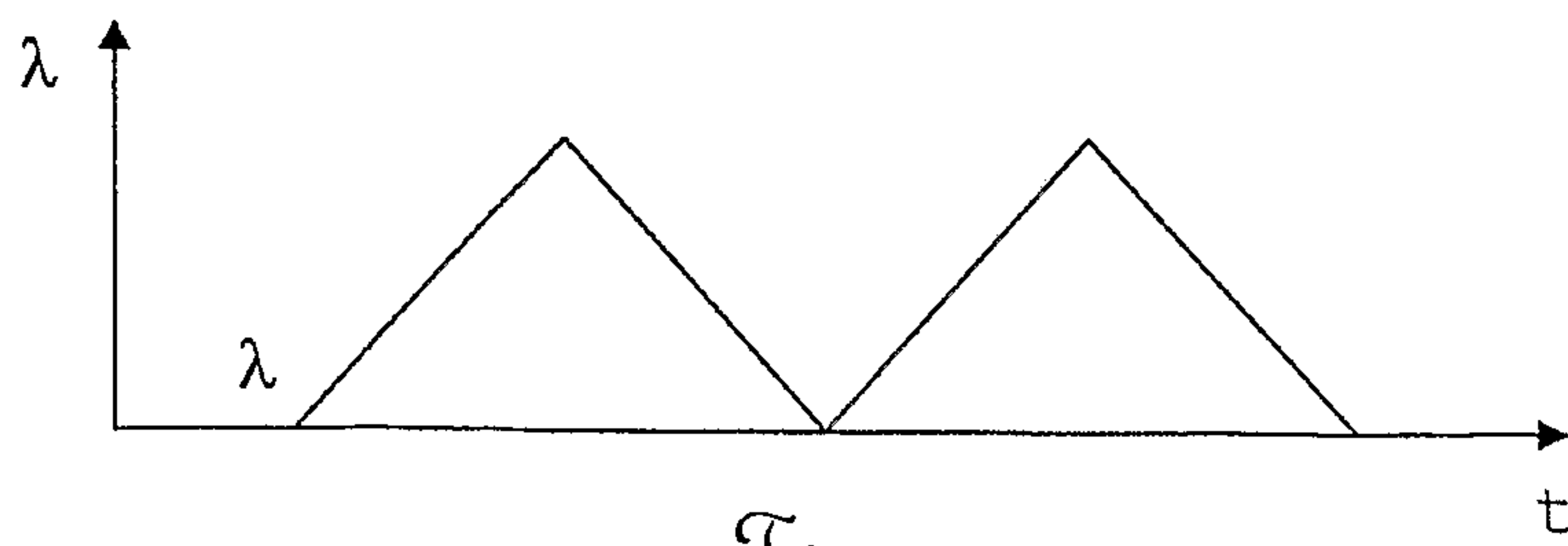
18. The distance-measuring apparatus according to Claim 17, wherein the average carrier wavelengths comprise 1530 nm and 1540 nm wavelengths.

19. Distance-measuring apparatus according to any one of Claims 13 to 18, wherein optical connections between components of the distance-measuring apparatus are in the form of single-mode fibres.

20. The distance-measuring apparatus according to any one of Claims 13 to 19, wherein the detector has two detector units for spectrally separate reception of the radiation components.

21. The distance-measuring apparatus according to any one of Claims 13 to 20, wherein the detector has a dielectric or dispersive element for chromatic separation of the back-scattered laser radiation into the radiation components.

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- 2/2 -

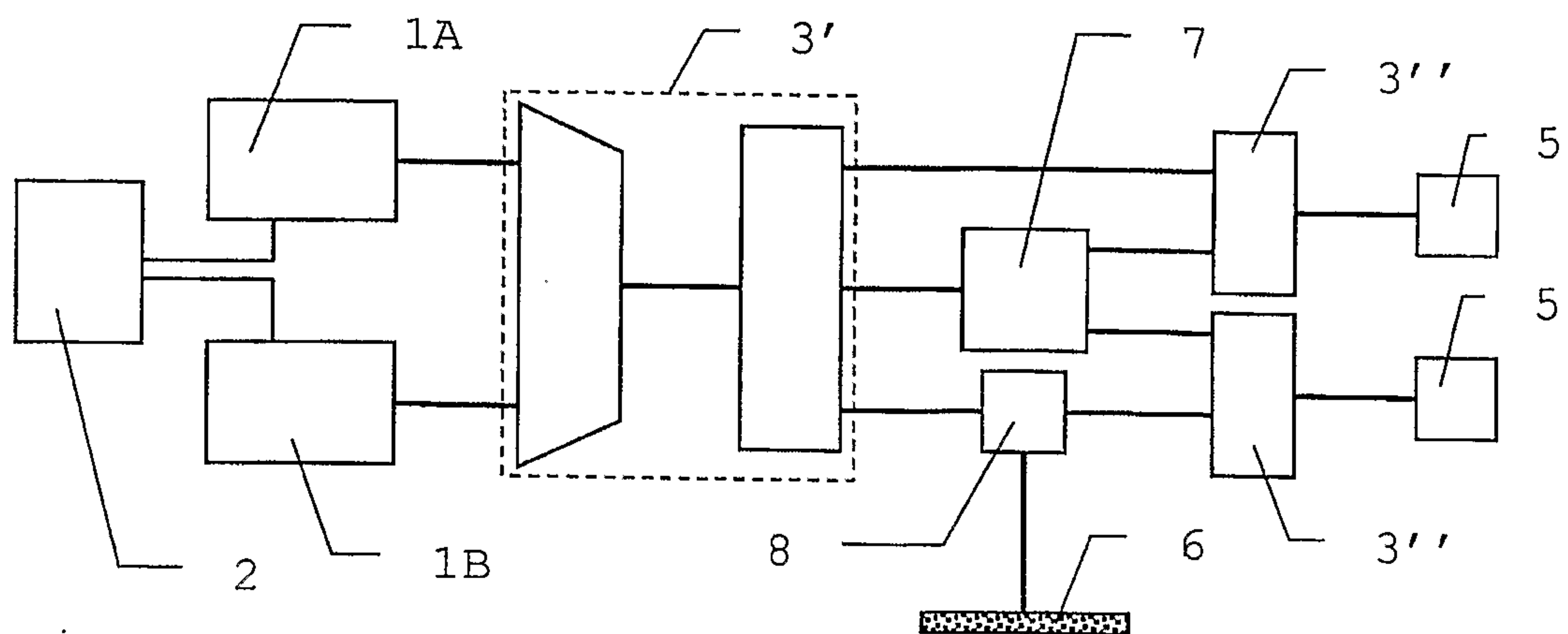


Fig. 4

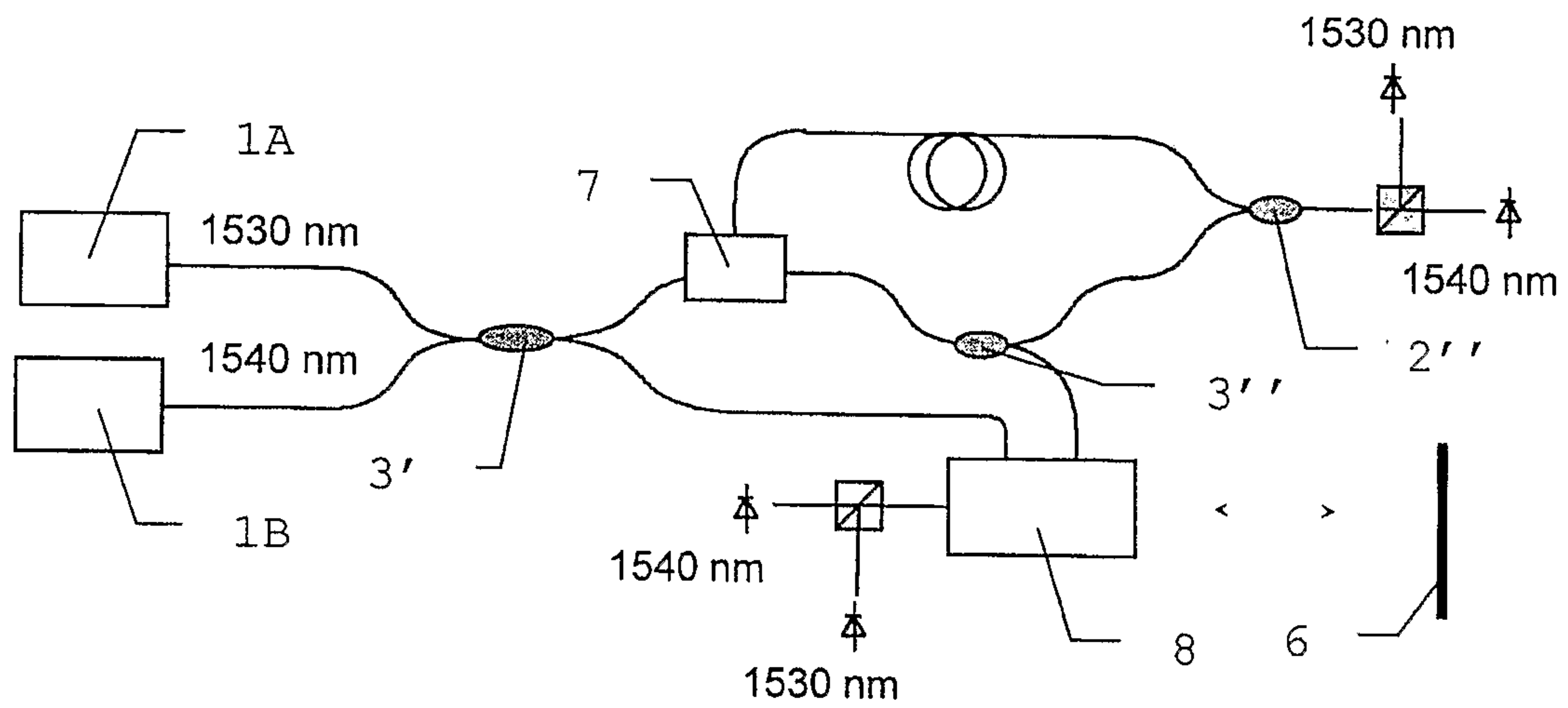


Fig. 5

