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(54) Multi-roll cluster rolling apparatus

Vielwalzengerüst

Cage de laminoir à rouleaux multiples

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(73) Proprietor:
KAWASAKI STEEL CORPORATION
Chuo-Ku, Kobe-City Hyogo 651 (JP)

(72) Inventors:
- **Watanabe, Yuichiro**
1 Kawasakicho, Chiba-shi, Chiba 260 (JP)
- **Kenmochi, Kazuhito**
1 Kawasakicho, Chiba-shi, Chiba 260 (JP)
- **Yarita, Ikuo**
1 Kawasakicho, Chiba-shi, Chiba 260 (JP)

(74) Representative:
Henkel, Feiler, Hänzel
Möhlstrasse 37
81675 München (DE)

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Description

[0001] The present invention relates to a multi-roll cluster rolling apparatus of the 12-high or 20-high class having superior flatness control characteristic.

DESCRIPTION OF THE RELATED ART

[0002] In recent years, multi-roll cluster rolling apparatus of 12-high or 20-high class has usually been used for cold rolling of materials which are difficult to work, e.g., stainless steels and silicon steels. This type of multi-roll cluster rolling apparatus offers an advantage in that, since the work rolls can have a reduced diameter, rolling at a large reduction ratio is possible with a smaller rolling load than in conventional vertical rolling mills. On the other hand, however, this type of rolling apparatus suffers from a disadvantage in that the cross-sectional shape or flatness of the rolled products tends to be degraded due to greater tendency of work roll deflection attributable to the reduction in the diameter of the work rolls.

[0003] Hitherto, various countermeasures have been proposed to obviate this problem.

[0004] For instance, a method has been proposed in which the outermost backup rolls are axially divided into a plurality of segments and the amounts of axial displacements of these roll segments are suitably adjusted to control the profile of the rolled product. The merit of this method, however, could not be fully enjoyed when the rolling apparatus is of multi-roll type having many intermediate rolls, such as 12-high or 20-high rolling mills, because the effect of control of the outermost backup rolls is absorbed by such many intermediate rolls.

[0005] In order to overcome this problem, a method has been proposed in, for example, Japanese Patent Unexamined Publication No. 58-50108, in which work roll benders and intermediate roll benders are used in combination with the control of displacements of the outermost backup roll segments mentioned above. This method, however, requires a highly complicated control mechanism. In addition, appreciable control effect is obtained only at both breadthwise ends of the rolled material when the roll diameters are reduced and when the roll barrel lengths are increased, because in such cases the bending force effect can hardly reach the breadthwise central portion of the material.

[0006] A method has been proposed in, for example, Japanese Patent Unexamined Publication No. 63-207405 in which intermediate rolls are tapered in axial direction at one their ends, and such tapered intermediate rolls are independently shifted in the axial directions. In this method, the control effect can be obtained only in the regions near the tapered portions of these intermediate rolls. In addition, it is difficult to change the intermediate rolls to employ different degrees of tapers in accordance with a change in the rolling conditions, such as the type of the steel to be rolled and the width of the rolled product to be obtained.

[0007] A vertically-arranged rolling apparatus disclosed in, for example, Japanese Patent Unexamined Publication No. 63-30104 employs axially shiftable rolls provided with S-crowns the dimension of which can be approximated by cubic equations. This rolling apparatus, however, is not a multi-roll cluster rolling mill. In addition, this rolling apparatus can produce the control effect only on both breadthwise ends and the central portion of the rolled material, and cannot satisfactorily prevent defects such as quarter elongation and composite elongation which is produced by combination of a center buckle and an edge wave.

[0008] EP-A 0 255 714 discloses a multi-roll cluster rolling apparatus in which two levels of intermediate rolls are used between a pair of working rolls and a plurality of backup rolls. With respect to particularly improving the control range of the support given to the work rolls at the ends of the rolled strip material this reference teaches to use for the intermediate rolls at the first level following the work rolls such rolls which have a one-end taper (T-rolls) which are arranged manually opposite positions and which are independently axially shiftable. In order to additionally allow control of the support given to the work rolls in the center portion of the rolled material this reference teaches three alternative arrangements: a) one roll of each pair of intermediate rolls of the first level is provided with a contour which deviates from the cylindrical shape between the ends thereof; b) the middle intermediate roll of the second level supporting a pair of intermediate rolls of the first level is provided with such a contour; or c) the outer intermediate rolls of the second level supporting each pair of intermediate rolls of the first level are provided with such a contour. The shape of these contoured rolls should be nonsymmetrical with respect to the center of the roll or slightly parabolic with the apex out of the axial center.

[0009] EP-A 0 294 544 discloses crowned rolls having a configuration which is determined in accordance with high-order functions. Such determination is complicated and difficult.

SUMMARY OF THE INVENTION

[0010] Accordingly, an object of the present invention is to provide a multi-roll cluster rolling apparatus of the 12-high or 20-high class having superior profile control performance and capable of effecting correction of complicated profile defect such as quarter elongation and edge/center composite elongation, not to mention simple defects such as center buckle and edge wave, as well as correction of any edge drop, thereby overcoming the above-described problems of the known art.

[0011] This object is solved by a multi-roll cluster rolling apparatus as claimed in claims 1 and 3.

[0012] The above and other objects, features and advantages of the present invention will become clear from the following description of the preferred embodiments when the same is read in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0013]

Figs. 1a and 1b are a side elevational view and a front elevational view of a 20-high rolling apparatus to which the present invention is applied;
Figs. 2a to 2d are schematic illustrations showing a change in the roll gap as observed when parallel T-crown rolls, which are arranged in opposite directions, are shifted in the direction of the roll axis;
Figs. 3a to 3c are schematic illustrations showing a change in the roll gap as observed when parallel S-crown rolls, which are arranged in opposite directions, are shifted in the direction of the roll axis;
Figs. 4a to 4c are schematic illustrations showing a change in the roll gap as observed when parallel W-crown rolls, which are arranged in opposite directions, are shifted in the direction of the roll axis;
Fig. 5 is a graph showing profile control performance of the 20-high rolling apparatus obtained when a pair of T-crown rolls, a pair of S-crown rolls and a pair of W-crown rolls are used as first or second intermediate rolls, respectively;
Fig. 6 is a graph showing a profile-controllable range of the 20-high rolling apparatus as obtained when T-crown rolls are used as the work rolls while W-crown rolls and S-crown rolls are respectively used as the first and second intermediate rolls;
Figs. 7a, 7b and 7c are illustrations of tapers of a single-end-tapered rolls;
Fig. 8 is an illustration of a S-crown which can be approximated by one pitch of a sine-wave curve;
Fig. 9 is an illustration of a W-crown which can be approximated by two pitches of sine-wave curve;
Figs. 10a,10b,11a,11b and 12a, 12b are illustrations showing arrangements of T-crown rolls, W-crown rolls and S-crown rolls in a 20-high rolling apparatus, as well as profile controllable ranges; and
Figs. 13a, 13b and 14a, 14b are illustrations showing arrangements of T-crown rolls, W-crown rolls and S-crown rolls in a 12-high rolling apparatus, as well as profile controllable ranges.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0014] Preferred embodiments of the present invention will be described with reference to the drawings.

[0015] Figs. 1a and 1b are a side elevational view and a front elevational view of a multi-roll cluster rolling apparatus in accordance with the present invention. A material under rolling is denoted by 1. The rolling apparatus has work rolls 2, first intermediate rolls 3, second intermediate rolls 4 and divided-type backup rolls 5. More specifically, upper and lower work rolls 2, 2 are arranged to oppose each other across the rolled material 1. Two first intermediate rolls 3,3 are arranged behind each work roll 2. Thus, there are four first intermediate rolls 3 in total. There are three second intermediate rolls 4,4,4 behind the pair of first intermediate rolls 2,2 at each side of the rolled material 1. Thus, six second intermediate rolls 4 are employed in total. The three second intermediate rolls 4,4,4 on each side of the rolled material 1 are backed up by four divided-type backup rolls 5. Thus, there are eight backup rolls 5 in total. It will be seen that the pair of work rolls 2, four first intermediate rolls 3, six second intermediate rolls 4 and eight backup rolls 5, in cooperation, form the 20-high-rolling apparatus. The work rolls 2, first intermediate rolls 3 and the second intermediate rolls 4 are independently shiftable in the axial directions by conventional hydraulic or electrical shifting devices (not shown).

[0016] Numeral 6 designate roll bending devices.

[0017] Figs. 2a to 2d show the manner in which the roll gap between parallel single-end-tapered rolls is changed in accordance with axial shifts of these rolls. These rolls are tapered by grinding only at their one axial end regions which are opposite to each other, and will be referred to as "T-crown rolls" hereinafter.

[0018] As will be seen from these Figures, it is possible to reduce any edge drop by varying the width (x) of the breadthwise end regions of the material rolled by the tapered portions of the roll, by suitably controlling the axial shift of the T-crown rolls.

[0019] Figs. 3a to 3c show the manner in which the roll gap between a pair of rolls is changed in accordance with axial shifts of these rolls, the rolls having a roll crown of a waveform approximated by one pitch of sine wave (referred to simply as "S-crown roll") and arranged in opposite directions.

[0020] In the state shown in Fig. 3a, both rolls are vertically aligned with each other so as to provide a constant gap therebetween along the length of these rolls. In the state shown in Fig. 3b, the rolls have been moved in opposite directions from the positions shown in Fig. 3a, so as to provide a roll gap which is large at the center and small at both breadthwise ends. In the state shown in Fig. 3c, the rolls have been moved in the directions counter to those in Fig. 3b, so as to provide a roll gap which is small at the center and large at both breadthwise ends.

[0021] Figs. 4a to 4c show the manner in which the roll gap between a pair of rolls is changed in accordance with axial shifts of these rolls, when the rolls have a roll crown of a waveform approximated by two pitches of sine wave (referred to simply as "W-crown roll") and are arranged in opposite directions.

[0022] In the state shown in Fig. 4a, both rolls are vertically aligned with each other so as to provide a constant gap therebetween along the length of these rolls. In the state shown in Fig. 4b, the rolls have been moved in opposite directions from the positions shown in Fig. 4a, so as to provide a roll gap which is large at the center and both breadthwise ends and small at the quater portions. In the state shown in Fig. 4c, the rolls have been moved in the directions counter to those in Fig. 4b, so as to provide a roll gap which is small at the center and both breadthwise ends and large at the quater portions.

[0023] A 20-high rolling apparatus of the type shown in Fig. 1 was built up by using pair of T-crown rolls as the first intermediate rolls, and a pairs of S- or W-crown rolls as the second intermediate rolls. A test was conducted to examine the profile control performance of this rolling apparatus by independently shifting these intermediate rolls. The result of this test are shown in Fig. 5 in comparison with the case where the backup roll sections corresponding to the quater portions are forced out.

[0024] The profile control performance can be expressed in terms of an elongation difference ratio Λ_2 representing the degree of difference between the elongation at the central portion and the elongation at breadthwise ends of the rolled material, and an elongation difference ratio Λ_4 representing the degree of difference between the elongation at the central portion and the elongation at quarter portions of the rolled material, the ratios Λ_2 and Λ_4 being respectively expressed by the following formulae:

$$\Lambda_2 = (\ell_2 - \ell_0)/\ell_0$$

where l_0 represents the length (mm) of the material after rolling as measured at breadthwise mid portion of the material and l_2 represents the length (mm) of the material after rolling as measured at breadthwise end portion of the material;

$$\Lambda_4 = (\ell_4 - \ell_0)/\ell_0$$

where l_4 represents the length (mm) of the material after rolling as measured at breadthwise quarter of the material.

[0025] In Fig. 5, lengths of straight lines represent the level of the profile control performance, while the gradients of the lines represent the ratios of controls of elongations.

[0026] For instance, large gradients of the lines representing the characteristics obtained when the T- or S-crown rolls are shifted alone show that such roll shifts are effective in the control of edge wave and center buckle but no substantial effect is expectable in regard to the control of the quater elongation and the edge/center composite elongation.

[0027] The control by force-out of the backup roll segments is represented by a line which has a very small gradient. Thus, this method can provide only a small effect in the control of the quater elongation and the edge/center composite elongation and cannot provide any substantial effect in the control of edge wave and center buckle.

[0028] Shifting of the W-crown rolls alone can provide an appreciable effect in the control of the quater elongation and the edge/center, but is quite ineffective in the control of the edge wave and the center buckle.

[0029] Another 20-high rolling apparatus of the type shown in Fig.1 was built up by using T-, S- and W-crown rolls as the work rolls, first intermediate rolls and the second intermediate rolls, respectively, and the profile correction performance of this rolling apparatus was examined. The result is shown in Fig. 6 together with the results of the same investigation conducted on a conventional apparatus which incorporated T-crown rolls as the first intermediate rolls in combination with roll benders and also with divided backup roll force-out method.

[0030] As will be understood from Fig. 6, the rolling apparatus of the present invention which employs T-, S- and W-crown rolls in combination and which relies upon suitable axial shifts of these rolls, exhibited superior effect in correcting quarter elongation, composite elongation and edge drop, not to mention simple edge wave and center buckle. It is thus understood that the apparatus of the present invention can conduct a flatness control over wide ranges. This should be contrasted to the conventional apparatus which could provide certain effects on the control of the edge wave and the center buckle but no substantial effect in the correction of edge/center composite elongation and quarter elongation.

[0031] Thus, in the rolling apparatus of the present invention, the merits of different types of roll crown are combined while demerits are canceled, thus overcoming the difficulty in the flatness control caused in current rolling apparatus having rolls of large length-to-diameter (L/D) ratio values and incorporating a large number of intermediate and backup rolls.

[0032] According to the invention, the roll pairs which are to be T-. S- and W-crowned may be any pair or pairs of rolls selected from the roll groups consisting of the work rolls, first intermediate rolls and the second intermediate rolls. It is, however, preferred that the pair of rolls to which the crown of the same type is applied belong to the same roll group, i.e., to the group consisting of the work rolls, group consisting of the first intermediate rolls or the group consisting of the third intermediate groups. The types and degrees of the rolling defects vary depending on the type of the steel material to be rolled and also on the rolling conditions. The types of roll crown and the rolls to which these crowns are imparted are determined in consideration of the types and degrees of such rolling defects. It is, however, generally recognized that a greater control effect is obtained when the T-, S- or W-crown rolls are disposed closer to the rolled material. In addition, greater, medium and smaller effects are obtained when the pair of the rolls of the same crown type are arranged in symmetry with respect to a point, a horizontal plane and a vertical plane.

[0033] The invention does not exclude a simultaneous use of roll benders. A greater effect on elongations at the edges such as edge wave will be obtained when roll benders are used in combination with the roll arrangement of the present invention.

Examples

Example 1

[0034] A 20-high rolling apparatus of the type shown in Fig. 1 was built-up using single-end-tapered T-crown rolls of Fig. 7a as the work rolls, S-crown rolls of the type shown in Fig. 8 approximated by one-pitch of a sine-wave curve as all the first intermediate rolls 3, and W-crown rolls of Fig. 9 approximated by two-pitch portion of a sine wave curve as selected second intermediate rolls which are hatched in Fig. 1.

[0035] A test rolling was conducted to roll a stainless steel sheet of 1000 mm wide from 1.2 mm down to 1.0 mm, while axially shifting the work rolls, first intermediate rolls and the second intermediate rolls in various manners.

[0036] Fig. 10a shows the above-mentioned roll arrangement, while Fig. 10b shows the range of profile control which can be covered by this rolling apparatus. Fig. 10b also shows the results of the same test rolling reduction conducted to examine the profile control performance of a known rolling apparatus which incorporated axially-shiftable single-end tapered rolls of the type shown in Figs. 7b and 7c as the first and second intermediate rolls, together with a control by force-out of segments of divided backup rolls.

[0037] As will be seen from Fig. 10b, the known apparatus could effect the profile control only in a small range. In particular, ability to correct composite elongation and quarter elongation is very small. Due to the small range of the profile control, this known apparatus require a change in the taper of the first or second intermediate rolls depending on conditions such as the kind and breadth of the material to be rolled.

[0038] In contrast, the rolling apparatus embodying the invention exhibited an ability to correct all types of elongations including composite and quarter elongations over wide ranges, and could effect a good profile control for a variety of types of the rolled material without requiring change of the intermediate rolls .

Example 2

[0039] A 20-high rolling apparatus of the type shown in Fig. 1 was built-up by using, as shown in Fig. 11a, T-crown rolls of Fig. 7b as the first intermediate rolls, W-crown rolls of Fig. 9 approximated by two-pitch portion of a sine-wave curve as the outer four intermediate rolls, i.e., left and right pairs of the second intermediate rolls, and S-crown rolls of Fig. 8 approximated by one-pitch portion of a sine-wave curve as the central pair of the second intermediate rolls. Using this rolling apparatus, a test rolling was conducted under the same conditions as Example 1 to examine the profile control ability of this apparatus, the results being shown in Fig. 11b.

Example 3

[0040] A 20-high rolling apparatus of the type shown in Fig. 1 was built-up by using, as shown in Fig. 12a, T-crown rolls of Fig. 7b as the first intermediate rolls, and W-crown rolls of Fig. 9 approximated by two-pitch portion of a sine-wave curve as the outer four intermediate rolls, i.e., left and right pairs of the second intermediate rolls. Using this rolling apparatus, a test rolling was conducted under the same conditions as Example 1 to examine the profile control ability of this apparatus, the results being shown in Fig. 12b.

Example 4

[0041] A 12-high rolling apparatus was built-up by using, as shown in Fig. 13a, S-crown rolls of Fig. 8 approximated by one-pitch portion of a sine-wave curve as the work rolls, W-crown rolls of Fig. 9 approximated by two-pitch portion of a sine-wave curve as the rolls of one of the left and right pairs of the intermediate rolls, each pair including an upper roll and a lower roll, and T-crown rolls of Fig. 7b as the rolls of the other of the left and right pairs of the intermediate rolls. Using this rolling apparatus with simultaneous use of the divided backup roll force-out control and roll benders, a test rolling was conducted under the same conditions as Example 1 to examine the profile control ability of this apparatus. The result is shown in Fig. 13b. Fig. 13b also shows the results of the same test rolling reduction conducted to examine the profile control performance of a known rolling apparatus which incorporated axially-shiftable single-end tapered rolls of the type shown in Fig. 7b as the intermediate rolls, together with a control by force-out of segments of divided backup rolls.

Example 5

[0042] A 12-high rolling apparatus was built up by using, as shown in Fig. 14a, T-crown rolls of Fig.7a as the work rolls, and W-crown rolls of Fig. 9 approximated by two pitches of a sine-wave curve as the intermediate rolls of one of two pairs of intermediate rolls, each pair including two rolls which are in symmetry with each other with respect to a point on the pinched portion of the rolled material. At the same time, a control by force-out of segments of divided backup rolls was used simultaneously. Using this rolling apparatus, a test rolling was conducted under the same conditions as Example 4 to examine the profile control ability of this apparatus, the results being shown in Fig. 14b.

[0043] As will be understood from the foregoing description, the multi-roll cluster rolling apparatus of the present invention offers excellent performance for effecting correction of rolling defects such as quarter elongation and composite elongation, as well as edge drop, not to mention the simple deformation such as edge wave and center buckle, thus realizing a superior flatness control effect over a wide range.

Claims

1. A 20-high multi-roll cluster rolling apparatus having

a pair of work rolls (2),
a plurality of first intermediate rolls (3),
a plurality of second intermediate rolls (4) and a plurality of backup rolls (5) arranged successively behind each said work roll (2),
characterized in that
either said first intermediate rolls (3) include at least a pair of rolls which have a crown in which the diameter of each roll decreases toward one end thereof and said second intermediate rolls (4) include at least a pair of rolls which have a crown which is a two-pitch section of a sine wave curve,
or said first intermediate rolls (3) include at least a pair of rolls which have a crown which is a two-pitch section of a sine wave curve and said second intermediate rolls (4) include at least a pair of rolls which have a crown in which the diameter of each roll decreases toward one end thereof,
the rolls of each said pair being arranged in axially opposite directions to each other,
each roll of said at least a pair of first intermediate rolls (3) and said at least a pair of second intermediate rolls (4) being independently shiftable in the axial direction so as to realize a control of the profile of a rolled material in terms of end elongation difference ratio Λ_2 given by the following formula (1) and the quarter elongation difference ratio Λ_4 given by the following formula (2):

$$\Lambda_2 = (l_2 - l_0)/l_0$$

$$\Lambda_4 = (l_4 - l_0)/l_0$$

wherein

l_0: length (mm) of the material after rolling as measured at breadthwise mid portion of said material

l_2: length (mm) of the material after rolling as measured at breadthwise end portion of said material

l_4: length (mm) of the material after rolling as measured at breadthwise quarter of said material.

2. A 20-high multi-roll cluster rolling apparatus according to claim 1, wherein said first intermediate rolls (3) include at least a pair of rolls having said crown in which the diameter of each roll decreases toward one end thereof and another pair of rolls which have said crown which is a two-pitch section of a sine wave curve.

3. A 12-high multi-roll cluster rolling apparatus having

a pair of work rolls,
a plurality of intermediate rolls and
a plurality of backup rolls arranged successively behind each said work roll,
characterized in that
either said work rolls have a crown in which the diameter of each roll decreases toward one end thereof and said intermediate rolls include at least a pair of rolls which have a crown which is a two-pitch section of a sine wave curve
or said work rolls have a crown which is a two-pitch section of a sine wave curve and said intermediate rolls include at least a pair of rolls which have a crown in which the diameter of each roll decreases toward one end thereof,

the rolls of each said pair being arranged in axially opposite directions to each other,
each roll of said work rolls and said at least a pair of intermediate rolls being independently shiftable in the axial direction so as to realize a control of the profile of a rolled material in terms of end elongation difference ratio Λ_2 given by the following formula (1) and the quarter elongation difference ratio Λ_4 given by the following formula (2):

$$\Lambda_2 = (l_2 - l_0)/l_0$$

$$\Lambda_4 = (l_4 - l_0)/l_0$$

wherein

l_0: length (mm) of the material after rolling as measured at breadthwise mid portion of said material

l_2: length (mm) of the material after rolling as measured at breadthwise end portion of said material

l_4: length (mm) of the material after rolling as measured at breadthwise quarter of said material.

Patentansprüche

1. Zwanzigrollenwalzengerüst mit

zwei Arbeitswalzen (2),
mehreren ersten Zwischenwalzen (3),
mehreren zweiten Zwischenwalzen (4) und
mehreren Stützwalzen (5), die aufeinanderfolgend hinter jeder Arbeitswalze (2) angeordnet sind,
dadurch gekennzeichnet, daß
entweder die ersten Zwischenwalzen (3) mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, bei der sich der Durchmesser jeder Walze zu einem Ende derselben hin verkleinert, und die zweiten Zwischenwalzen (4) mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, welche ein Zwei-Perioden-Abschnitt einer Sinuswellenkurve ist,
oder die ersten Zwischenwalzen (3) mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, welche ein Zwei-Perioden-Abschnitt einer Sinuswellenkurve ist, und die zweiten Zwischenwalzen (4) mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, bei der sich der Durchmesser jeder Walze zu einem Ende derselben hin verkleinert,
wobei die Walzen jedes Paars in axial zueinander entgegengesetzten Richtungen angeordnet sind,
jede Walze des mindestens einen Paars der ersten Zwischenwalzen (3) und des mindestens einen Paars der zweiten Zwischenwalzen (4) unabhängig in der Axialrichtung verschiebbar ist, um eine Steuerung des Profils eines Walzguts bezüglich des durch nachstehende Formel (1) gegebenen Endstreckungsdifferenzverhältnisses Δ_2 und des durch nachstehende Formel (2) gegebenen Viertelstreckungsdifferenzverhältnisses Δ_4 zu realisieren:

$$\Delta_2 = (l_2 - l_0)/l_0$$

$$\Delta_4 = (l_4 - l_0)/l_0$$

wobei bedeuten:

l_0 = Länge (mm) des Guts nach dem Auswalzen an einem Mittelabschnitt des Guts in Breitenrichtung,
l_2 = Länge (mm) des Guts nach dem Auswalzen an einem Endabschnitt des Guts in Breitenrichtung,
l_4 = Länge (mm) des Guts nach dem Auswalzen an einem Viertelabschnitt des Guts in Breitenrichtung.

2. Zwanzigrollenwalzgerüst nach Anspruch 1, wobei die ersten Zwischenwalzen (3) mindestens ein Paar Walzen mit der Balligkeit aufweisen, bei der sich der Durchmesser jeder Walze zu einem Ende derselben hin verkleinert, sowie ein weiteres Paar Walzen, die die Balligkeit aufweisen, welche ein Zwei-Perioden-Abschnitt einer Sinuswellenkurve ist.

3. Zwölfrollenwalzengerüst mit

zwei Arbeitswalzen,
mehreren Zwischenwalzen, und
mehreren Stützwalzen, die aufeinanderfolgend hinter jeder Arbeitswalze angeordnet sind,
dadurch gekennzeichnet, daß
entweder die Arbeitswalzen eine Balligkeit aufweisen, bei der sich der Durchmesser jeder Walze zu einem Ende derselben hin verkleinert und die Zwischenwalzen mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, welche ein Zwei-Perioden-Abschnitt einer Sinuswellenkurve ist,
oder die Arbeitswalzen eine Balligkeit aufweisen, welche ein Zwei-Perioden-Abschnitt einer Sinuswellenkurve ist, und die Zwischenwalzen mindestens ein Paar Walzen umfassen, die eine Balligkeit aufweisen, bei der sich der Durchmesser jeder Walze zu einem Ende derselben hin verkleinert,
wobei die Walzen jedes Paars in axial zueinander entgegengesetzten Richtungen angeordnet sind,
jede Walze der Arbeitswalzen und des mindestens einen Paars der Zwischenwalzen unabhängig in der Axialrichtung verschiebbar ist, um eine Steuerung des Profils eines Walzguts bezüglich des durch nachstehende Formel (1) gegebenen Endstreckungsdifferenzverhältnisses Δ_2 und des durch nachstehende Formel (2) gegebenen Viertelstreckungsdifferenzverhältnisses Δ_4 zu realisieren:

$$\Delta_2 = (l_2 - l_0)/l_0$$

$$\Delta_4 = (l_4 - l_0)/l_0$$

wobei bedeuten:

l_0 = Länge (mm) des Guts nach dem Auswalzen an einem Mittelabschnitt des Guts in Breitenrichtung,
l_2 = Länge (mm) des Guts nach dem Auswalzen an einem Endabschnitt des Guts in Breitenrichtung,

l_4 = Länge (mm) des Guts nach dem Auswalzen an einem Viertelabschnitt des Guts in Breitenrichtung.

Revendications

1. Une cage 20 de laminoir à rouleaux multiples, comportant :

une paire de rouleaux travailleurs (2),
une pluralité de premiers rouleaux intermédiaires (3),
une pluralité de seconds rouleaux intermédiaires (4), et
une pluralité de rouleaux d'appui (5), disposés successivement derrière chacun desdits rouleaux travailleurs (2),
caractérisée en ce que
soit lesdits premiers rouleaux intermédiaires (3) comprennent au moins une paire de rouleaux présentant une couronne dans laquelle le diamètre de chaque rouleau va en diminuant en direction de l'une de ses extrémités, et lesdits seconds rouleaux intermédiaires (4) comprennent au moins une paire de rouleaux présentant une couronne qui constitue une section à deux périodes de sinusoïde,
soit lesdits premiers rouleaux intermédiaires (3) comprennent au moins une paire de rouleaux présentant une couronne qui constitue une section à deux périodes de sinusoïde, et lesdits seconds rouleaux intermédiaires (4) comprennent au moins une paire de rouleaux ayant une couronne dans laquelle le diamètre de chaque rouleau va en diminuant en direction de l'une de ses extrémités,
les rouleaux de chaque dite paire étant agencés en des directions axialement opposées l'une à l'autre,
chaque rouleau de ladite au moins une paire des premiers rouleaux intermédiaires (3) et de ladite au moins une paire des seconds rouleaux intermédiaires (4) étant déplaçable indépendamment dans la direction axiale, de manière à réaliser un contrôle du profil du matériau laminé, en terme de rapport Λ_2 de différence d'allongement aux extrémités, donné par la formule (1) suivante et de rapport Λ_4 de différence d'allongement au quart de largeur, donné par la formule (2) suivante :

$$\Lambda_2 = (l_2 - l_0)/l_0$$

$$\Lambda_2 = (l_4 - l_0)/l_0$$

dans lequel

1_0 : longueur (mm) du matériau après laminage, mesurée dans la partie médiane en largeur dudit matériau,

1_2 : longueur (mm) du matériau après laminage, mesuré sur la partie finale en largeur dudit matériau,

1_4 : longueur (mm) du matériau après laminage, mesuré au quart de la largeur dudit matériau.

2. Cage de 20 de laminoir à rouleaux multiples selon la revendication 1, dans laquelle lesdits premiers rouleaux intermédiaires (3) comprennent au moins une paire de rouleaux ayant la dite couronne dans laquelle le diamètre de chaque rouleau va en diminuant en allant en direction d'une de ses extrémités et une autre paire de rouleaux ayant ladite couronne dotée d'une section sur deux périodes d'une sinusoïde.

3. Une cage 12 de laminoir à rouleaux multiples, comportant :

une paire de rouleaux travailleurs,
une pluralité de rouleaux intermédiaires, et
une pluralité de rouleaux d'appui, disposés successivement derrière chacun desdits rouleaux travailleurs,
caractérisée en ce que
soit lesdits rouleaux travailleurs comprennent une couronne dans laquelle le diamètre de chaque rouleau va en diminuant en direction de l'une de ses extrémités, et lesdits rouleaux intermédiaires comprennent au moins une paire de rouleaux ayant une couronne constituant une section à deux périodes de sinusoïde,
soit lesdits rouleaux travailleurs ont une couronne constituant une section à deux périodes de sinusoïde et lesdits rouleaux intermédiaires comprennent au moins une paire de rouleaux ayant une couronne, dans laquelle le diamètre de chaque rouleau va en diminuant en direction de l'une de ses extrémités,
les rouleaux de chaque paire étant disposés suivant des sens opposés axialement entre eux,
chaque rouleau, parmi lesdits rouleaux travailleurs et ladite au moins une paire de rouleaux intermédiaires, étant déplaçable indépendamment dans la direction axiale, de manière à réaliser un contrôle du profil du matériau laminé, en terme de rapport Λ_2 de différence d'allongement aux extrémités, donné par la formule (1) suivante et de rapport Λ_4 de différence d'allongement au quart de largeur, donné par la formule (2) suivante :

$$\Lambda_2 = (l_2 - l_0)/l_0$$

$$\Lambda_2 = (l_4 - l_0)/l_0$$

dans lequel

l_0 : longueur (mm) du matériau après laminage, mesurée dans la partie médiane en largeur dudit matériau,

l_2 : longueur (mm) du matériau après laminage, mesuré sur la partie finale en largeur dudit matériau,

l_4 : longueur (mm) du matériau après laminage, mesuré au quart de la largeur dudit matériau.

FIG. 1(a)

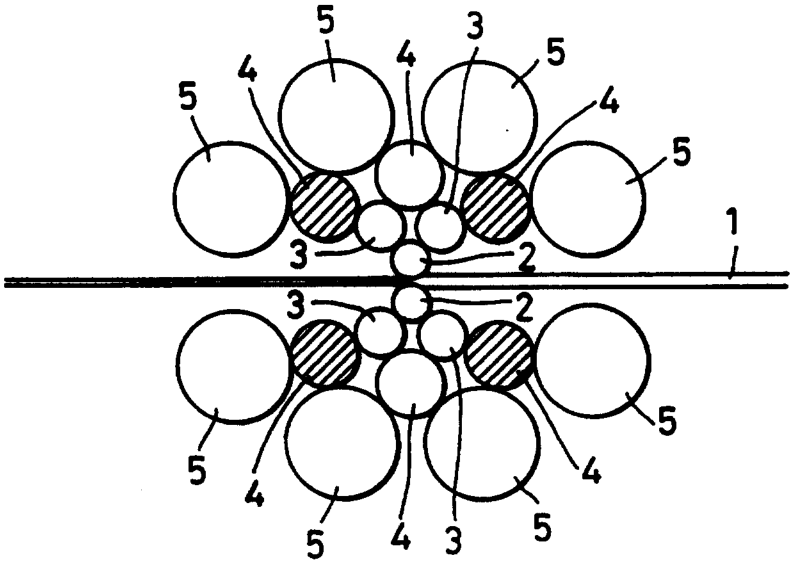

FIG. 1(b)

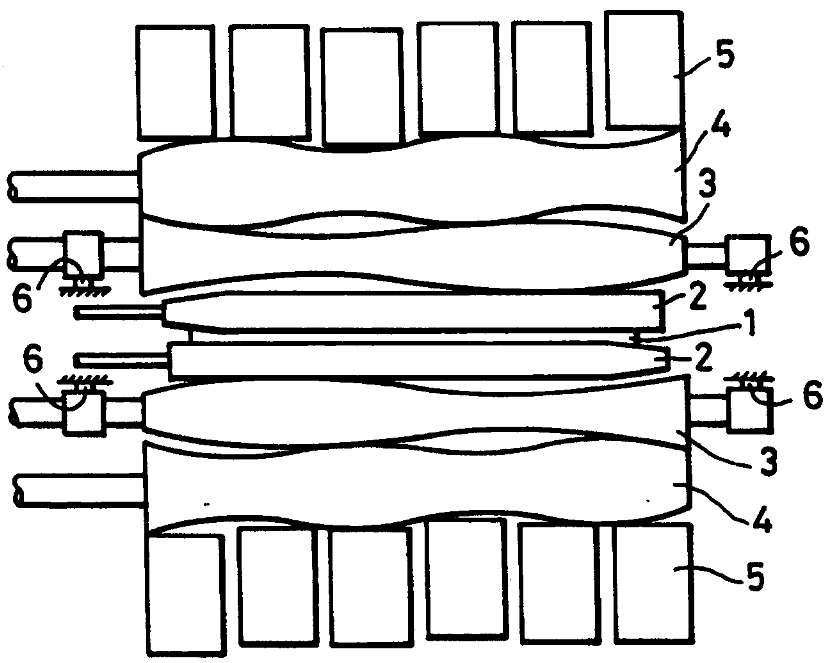

FIG. 2(a)

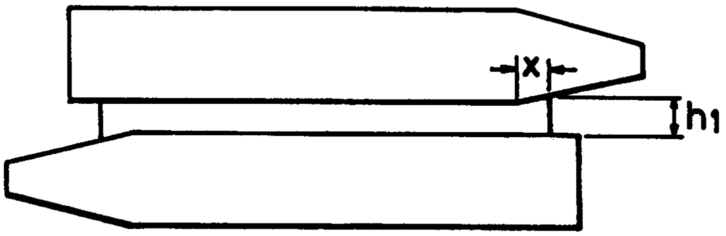

FIG. 2(b)

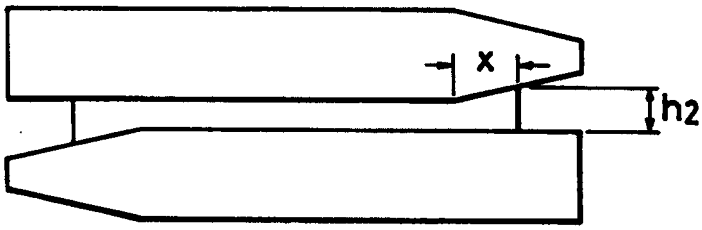

FIG. 2(c)

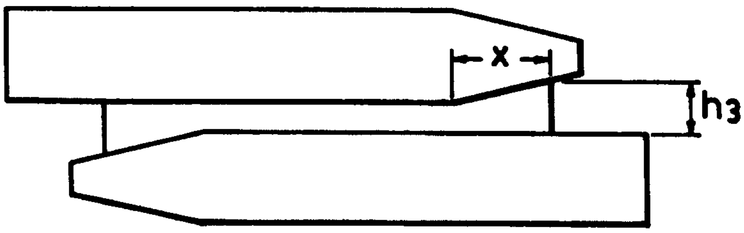

FIG. 2(d)

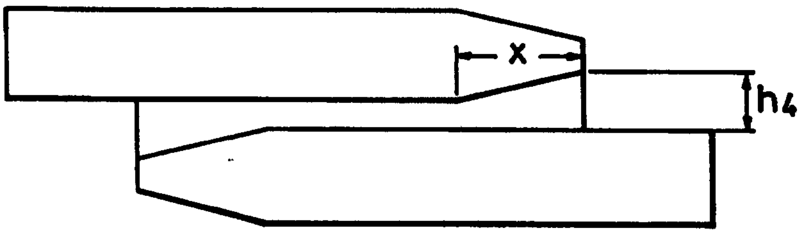

FIG. 3(a)

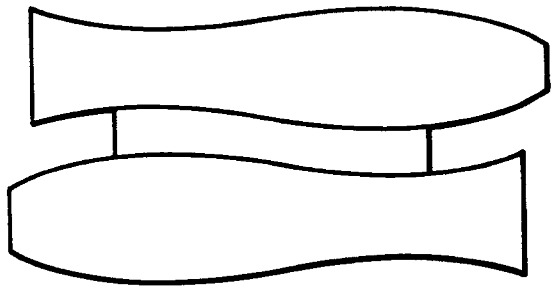

FIG. 3(b)

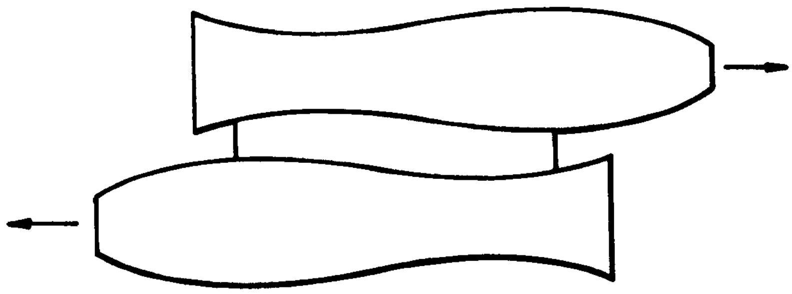

FIG. 3(c)

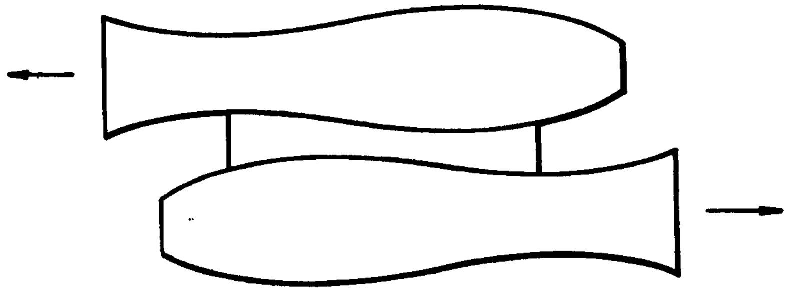

FIG. 4(a)

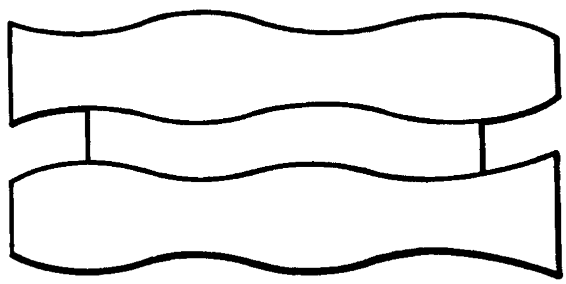

FIG. 4(b)

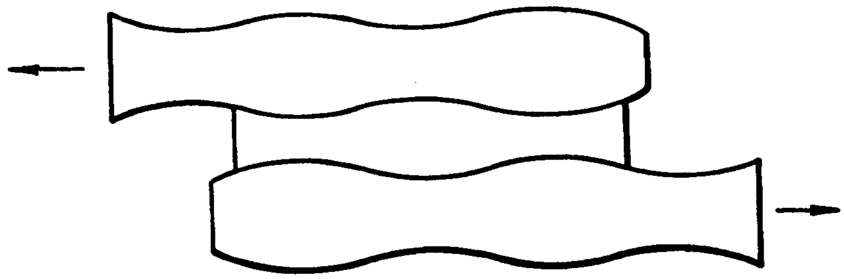

FIG. 4(c)

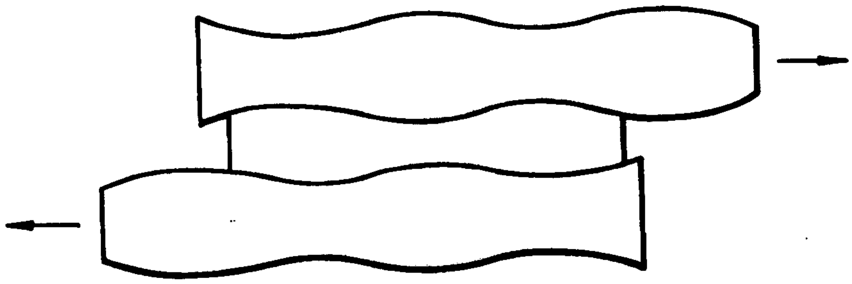

FIG. 5

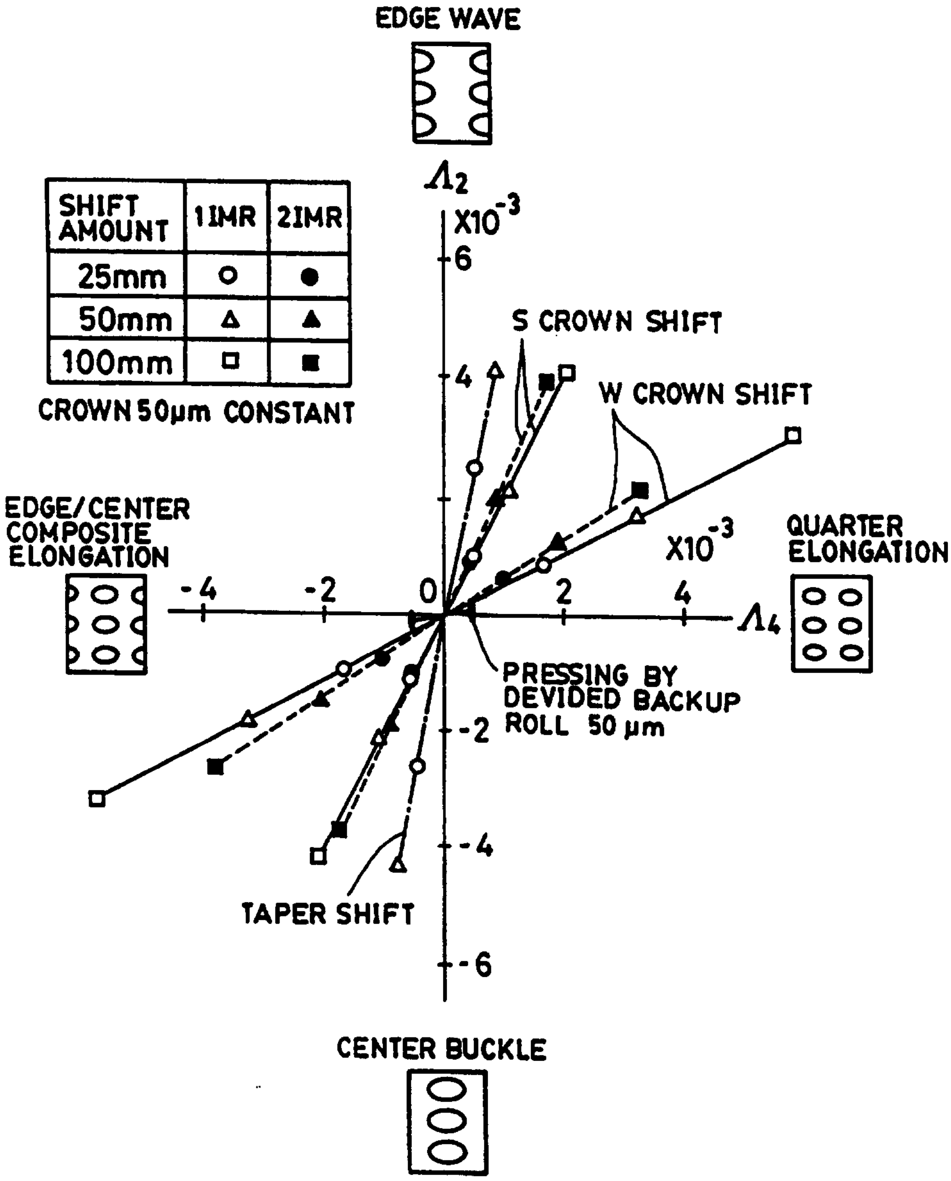
EDGE WAVE
Λ2
X10-3
6
4
-2
-4
-6
SHIFT AMOUNT
1IMR
2IMR
25mm
50mm
100mm
CROWN 50μm CONSTANT
S CROWN SHIFT
W CROWN SHIFT
EDGE/CENTER COMPOSITE ELONGATION
QUARTER ELONGATION
X10-3
-4
-2
0
2
4
Λ4
PRESSING BY DEVIDED BACKUP ROLL 50 μm
TAPER SHIFT
CENTER BUCKLE

FIG. 6

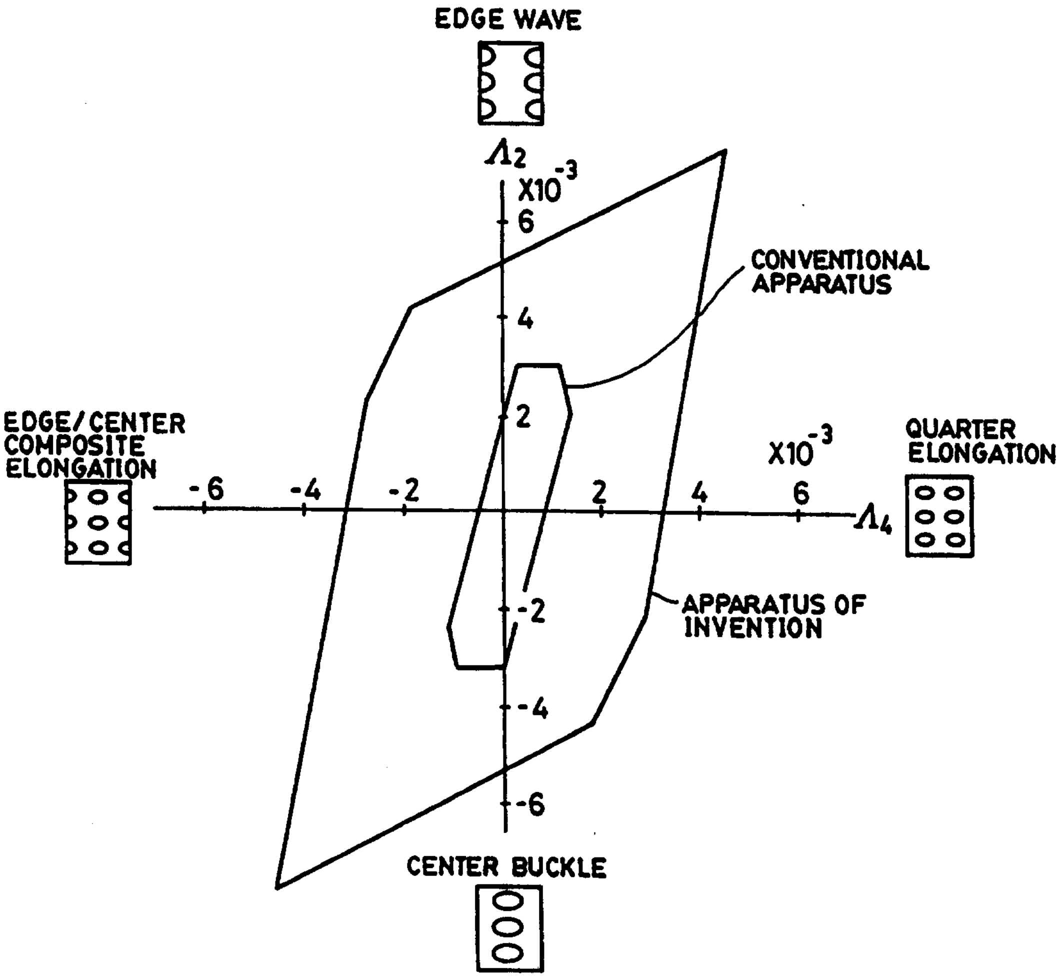
EDGE WAVE
Λ2
X10^-3
6
4
2
-2
-4
-6
CONVENTIONAL APPARATUS
EDGE/CENTER COMPOSITE ELONGATION
-6
-4
-2
2
4
6
X10^-3
Λ4
QUARTER ELONGATION
APPARATUS OF INVENTION
CENTER BUCKLE

FIG. 7 (a)

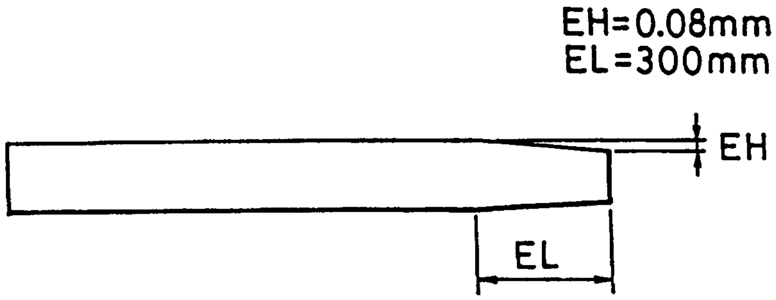

FIG. 7 (b)

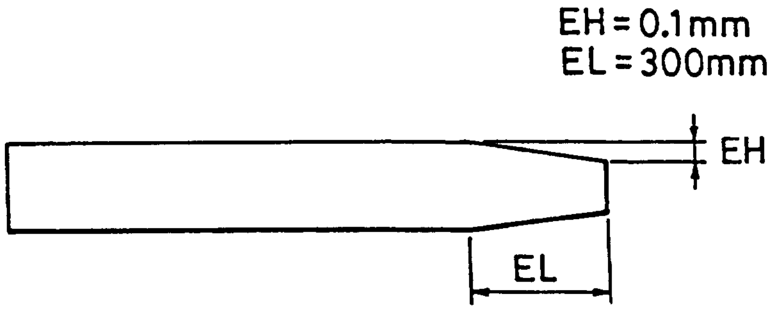

FIG. 7 (c)

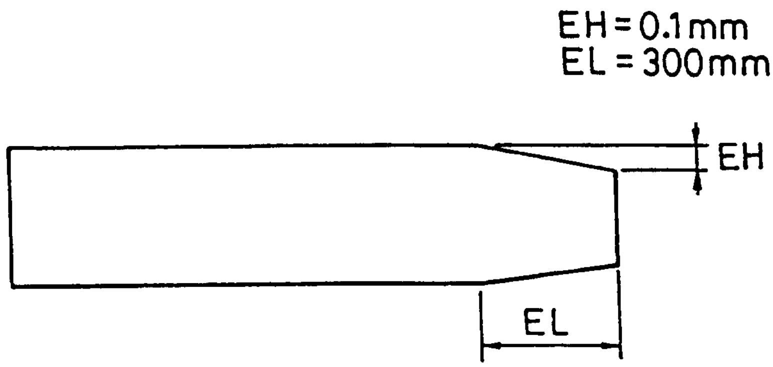

FIG. 8

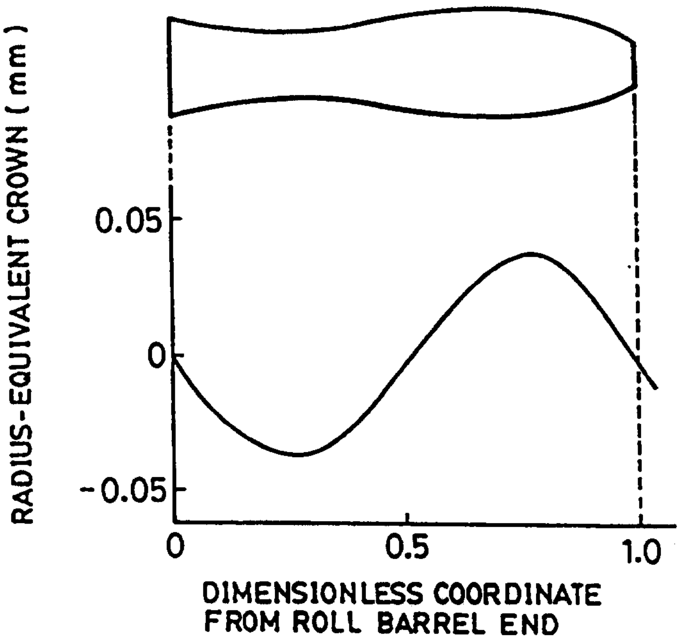
RADIUS-EQUIVALENT CROWN (mm)
0.05
0
-0.05
0
0.5
1.0
DIMENSIONLESS COORDINATE
FROM ROLL BARREL END

FIG. 9

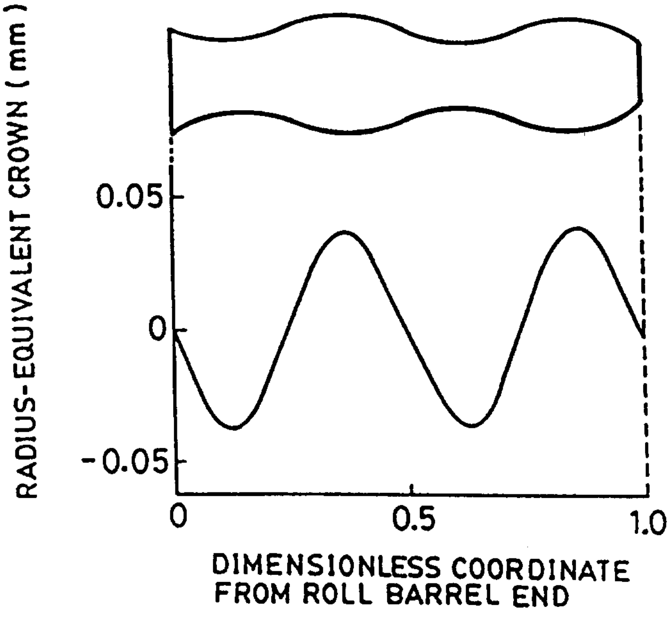
RADIUS-EQUIVALENT CROWN (mm)
0.05
0
-0.05
0
0.5
1.0
DIMENSIONLESS COORDINATE
FROM ROLL BARREL END

FIG. 10(a)

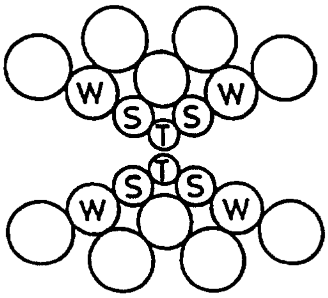

FIG. 10(b)

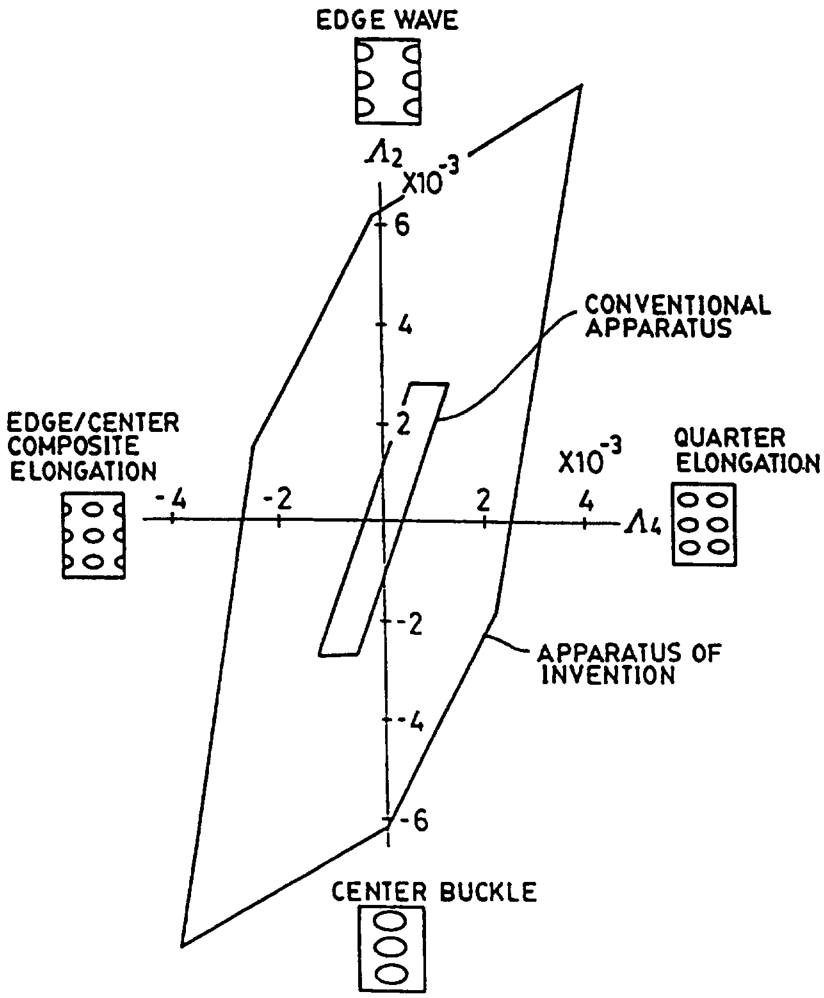

FIG.11 (a)

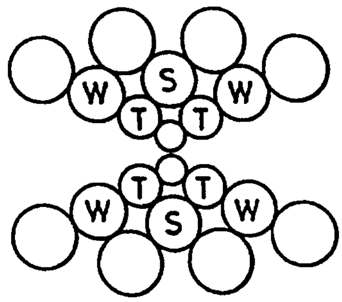

FIG.11 (b)

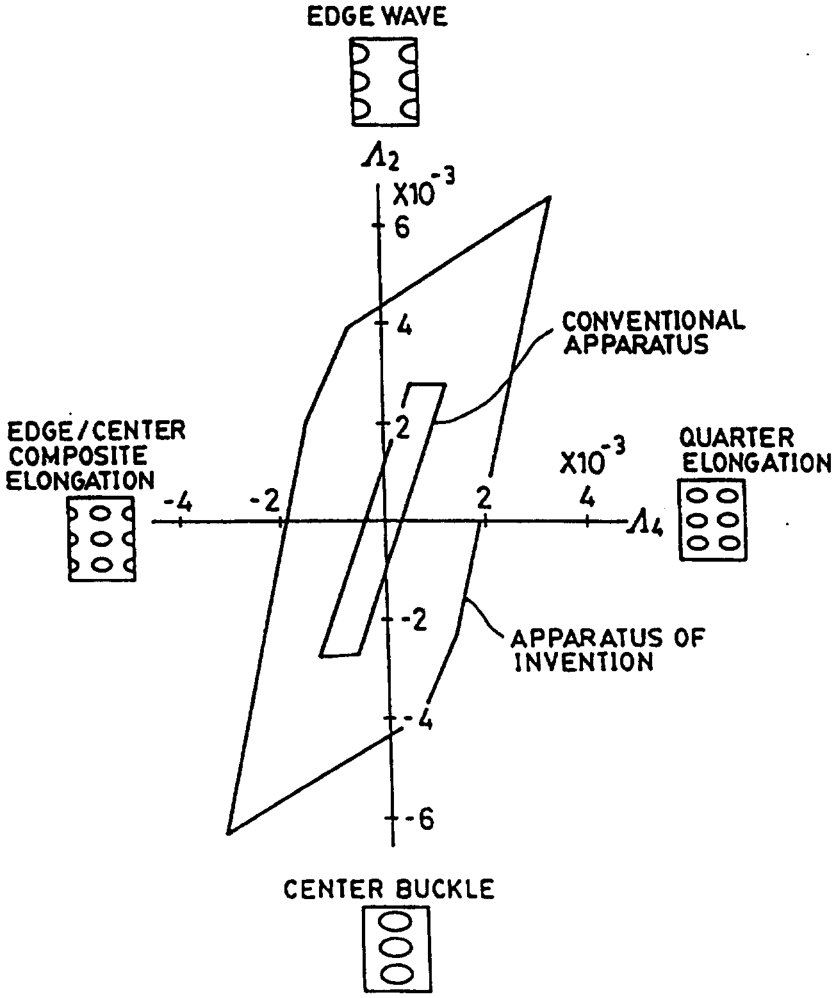

FIG. 12 (a)

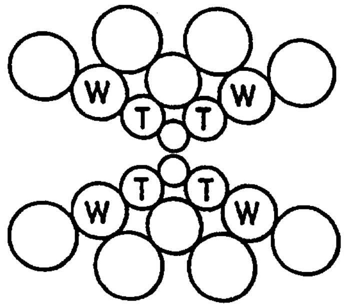

FIG. 12 (b)

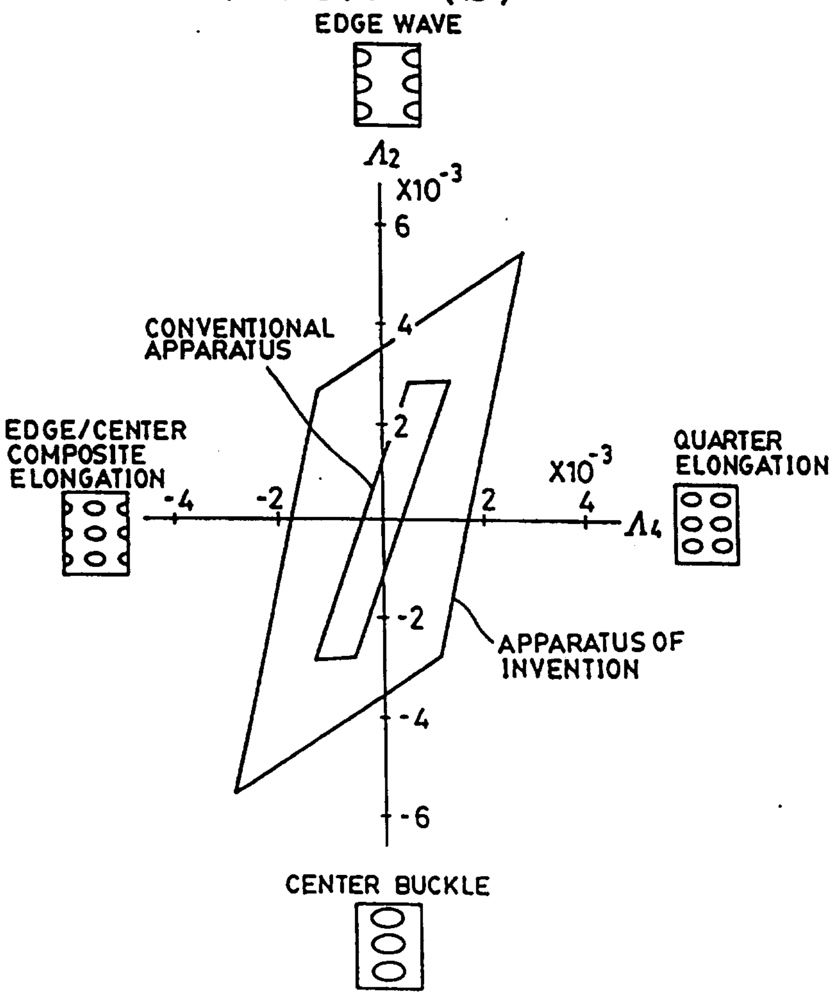

FIG. 13 (a)

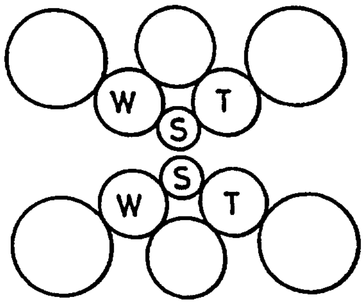

FIG. 13 (b)

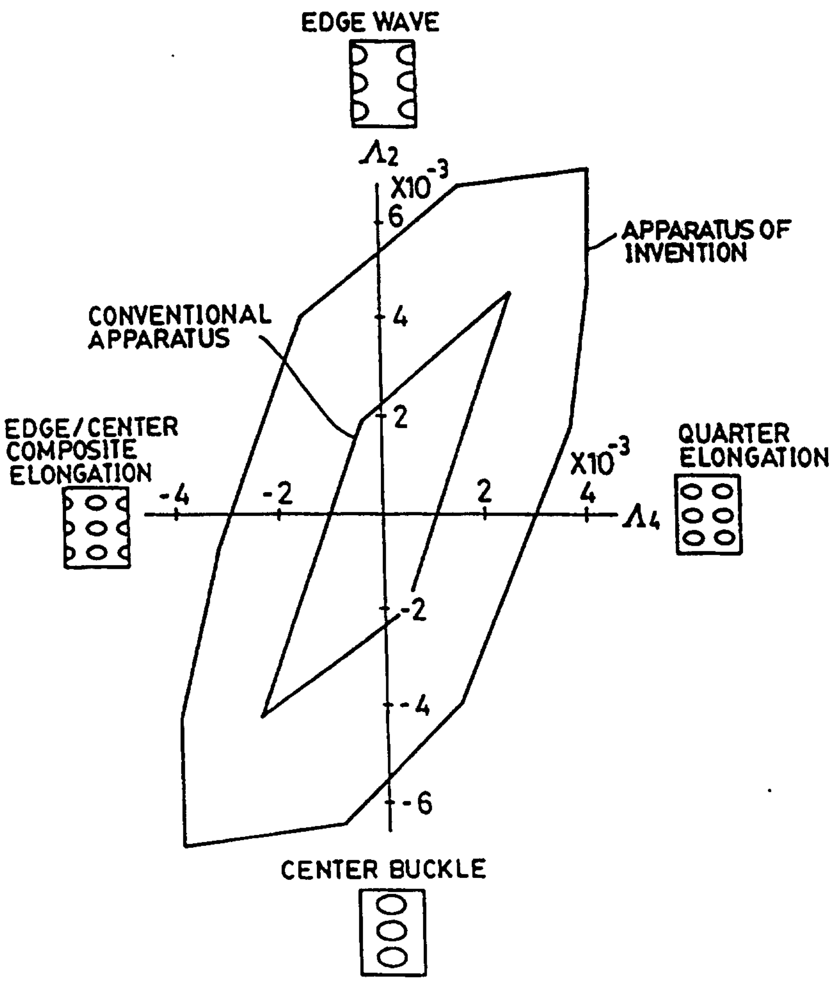

FIG. 14 (a)

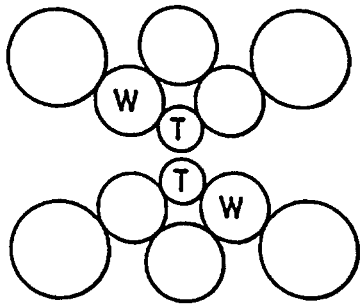

FIG. 14 (b)