**Title:** DEPOLYMERIZATION OF NYLON 6,6 (AND OPTIONALLY) NYLON 6 TO OBTAIN HEXAMETHYLENE DIAMINE (AND CAPROLACTAM)

**Abstract**

A process is disclosed for simultaneously depolymerizing nylon 6 and 6,6 and reclaiming the monomer values by steam distillation, in the presence of a basic nylon depolymerizing catalyst.
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Depolymerization of nylon 66 (and optionally) nylon 6 to obtain hexamethylene diamine (and caprolactam)

Background of the Invention

Field of the Invention

This invention relates to a process for simultaneously depolymerizing and reclaiming the component parts of, both, nylon 6 and nylon 6,6. The process includes nylon depolymerization to monomer components in a basic system followed by steam distillation of the monomers.

Description of the Prior Art

Nylon 6 has previously been depolymerized in the presence of both, acidic and basic catalysts. Acidic catalysts, particularly phosphoric acid and/or its alkali metal salts, have been preferred because they provide higher depolymerization rates. United States Patent No. 3,182,055, issued May 4, 1965 on the application of Bonfield et al., relates to an improved method of depolymerizing nylon 6 with steam in the presence of phosphoric acid. Depolymerization of nylon 6 using basic catalyst sodium amino caproate was disclosed in Japanese publication 56-4550 dated January 30, 1981.

Nylon 6,6 has previously been depolymerized in the presence of acidic and basic reagents and, to some extent, even water; but not in the presence of basic catalysts. Depolymerization of nylon 6,6 by previous methods has resulted in recovery of hexamethylene diamine and adipic acid, while depolymerization using a basic catalyst in accordance with the present invention yields hexamethylene diamine, cyclopentanone, and carbon dioxide, directly, for uncomplicated recovery.

Summary of the Invention

The present invention provides a process for depolymerizing a mixture of nylon 6 and nylon 6,6 comprising the steps of establishing a molten polymer
system including: (i) 0-75 weight percent nylon 6 and 25-
100 weight percent nylon 6,6; and (ii) basic nylon
depolymerizing catalyst in an amount of 1-50 weight
percent, based on the total weight of the polymer, at a
temperature of 250 to 400°C; conducting steam through the
molten polymer system; and condensing the steam to obtain
a mixture of water, caprolactam, and hexamethylene
diamine.

Detailed Description of the Invention

In the presence of an acid catalyst, nylon 6
yields caprolactam but nylon 6,6 yields a large variety
of relatively useless or difficult-to-isolate
decomposition products including pentyl amine, pentyl
nitrile, aminocapronitrile, and butyl amine. Simultaneous
depolymerization of a mixture of nylon 6 and nylon 6,6,
when conducted using a basic catalyst, results in a yield
of both, caprolactam and hexamethylene diamine with
little of the other products.

Steam stripping of a combination of nylon 6 and
nylon 6,6 was expected to yield the same variety of
decomposition products as above-named for nylon 6,6; but,
instead, it has been discovered that, so long as a basic
depolymerizing catalyst is used, depolymerization and
steam stripping of a combination of the two nyons can be
conducted simultaneously and in the same vessel to
recover essentially all of the monomer value of the nylon
6 (caprolactam) and essentially one-half of the value of
the nylon 6,6 (hexamethylene diamine). The
cyclopentanone and the carbon dioxide from the nylon 6,6
can, also, be recovered, if desired. Thus, the two
nylons can be depolymerized and the monomer values
recovered without any need for the initial separation of
nylon 6 from nylon 6,6. It is becoming increasingly
important to reuse waste polymeric materials. The
production of monomers from polymer sources in which the
monomers are already available in the proper chemical form reduces the need to convert raw material from petroleum to the monomer form at much greater time and expense.

It is, also, becoming increasingly important to reduce the volume of scrap material, such as nylon carpeting, sent to landfills. By this invention, improving on the reclamation of nylon values, petroleum raw materials can be preserved and the burden on landfills can be lessened. Nylon 6 mill waste is routinely recovered in the form of caprolactam by most nylon 6 producers. The recovery of nylon 6 waste is an important aspect of its production because, in the polymerization step, about 10% of the product consists of water soluble caprolactam monomer and low molecular weight oligomers. Fortunately, nylon 6 is easily depolymerized to caprolactam especially in the presence of phosphoric acid, which is also the preferred polymerization initiator. The depolymerized caprolactam can be steam distilled affording a way to recover otherwise lost raw material.

In the production of nylon 6,6, the polymerization is more efficient and there has not been a need to recover unpolymerized monomer. Nylon 6,6 producers generally treat mill waste, depending on quality, by remelting.

Before the present invention, there was no way to efficiently recycle post consumer nylon waste. Since nylon 6 and 6,6 generally share market applications, consumer products might be either. Therefore, post consumer nylon waste will comprise a mixture of the types. Methods to distinguish between and separate the two types of nylon are expensive and time consuming. Thus, recovery of monomers from mixtures of nylon 6 and 6,6 is useful when recycling used consumer products due
to the difficulty and expense of separating thenylons into their individual types.

In accordance with the present invention, there is provided a process for obtaining caprolactam from the nylon 6 portion and hexamethylenediamine from the nylon 6,6 portion of a mixture of the two nylons. The process comprises introducing into a reaction zone unsorted waste nylon and enough alkali metal or alkaline earth hydroxide catalyst to make up the amount of catalyst being withdrawn from the reaction zone in the process of purging non-volatile decomposition products. The process includes continuously introducing high temperature steam into said reaction zone; continuously withdrawing from said reaction zone, steam, polymer degradation products and undecomposed polymer melt; maintaining said reaction zone at a temperature of at least 275°C; and recovering caprolactam and hexamethylenediamine from the degradation products.

The process of this invention can be used to process either nylon 6 or nylon 6,6 alone or in any combination of the two. The process, thereby, accommodates the variability of feed which would be expected to occur when mixed consumer and industrial nylon waste is being processed. In order to realize the benefits of the invention, the combination of nylons should include at least 25 weight percent nylon 6,6. On the other hand, the melt viscosity and the melting temperature of nylon 6,6 are higher than the viscosity and melting temperature of nylon 6; and it has been found advantageous to use a combination of nylon 6 and nylon 6,6 with at least 25 weight percent nylon 6.

The basic nylon depolymerizing catalyst used in this invention is generally taken from the group consisting of alkali metal hydroxides and alkaline earth metal hydroxides, whether used in the hydroxide form or
in some other form which, during the depolymerization, is converted to the hydroxide form.

The above-mentioned basic nylon depolymerizing catalysts are, as stated, useful in polymerizing nylon 6; and, therefore, might be expected to be useful in depolymerization of nylon 6. In the polymerization of nylon 6,6, however, only acidic catalysts have previously been found to be useful. It was completely unexpected that these basic nylon depolymerizing catalysts would be useful in depolymerizing nylon 6,6, also.

Description of the Preferred Embodiments

In the examples which follow, the nylon depolymerizations were conducted in a reaction vessel fitted with a heating means, a nitrogen purging means, a stirring means, and a steam distillation means including a steam condensing means. Steam was generated by metered delivery of deoxygenated water in a stainless steel tube through a heated sand bath and into the reaction vessel.

EXAMPLE 1

One hundred grams each of nylon 6 and nylon 6,6 were charged into the reaction vessel, along with 85.6 grams of 6-aminocaproic acid and 26.1 grams of sodium hydroxide. When the temperature of the charge reached 291 C, water flow for steam generation was started at 1.5 ml/minute. The process was run for four hours and, after each hour, 12.7 grams of each of nylon 6 and nylon 6,6 were added to the vessel. The condensate was weighed and analyzed every hour. Caprolactam and hexamethylene diamine were each found in the distillate. Results are summarized in Table 1, below.

While the basic depolymerizing catalyst for this example was sodium 6-aminocaproate, substantially the same results would be expected when sodium hydroxide,
alone, is used, as will be shown in Examples 2 and 3, below.

Table 1

<table>
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<tr>
<th>Time (hr)</th>
<th>Weight (g)</th>
<th>Percent</th>
<th>Percent</th>
<th>Average Temperature in Distill. of Melt (°C)</th>
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<td></td>
<td>of Distill. Collected in Distill.</td>
<td>Caprolactam</td>
<td>Diamine</td>
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</table>

EXAMPLE A (Comparative)

One hundred grams each of nylon 6 and nylon 6,6 were charged into the reaction vessel, along with 41.6 grams of sodium phosphate monobasic and 8.4 grams of 85% phosphoric acid. When the temperature of the charge reached 291 °C, water flow for steam generation was started at 1.5 ml/minute. The process was run for five hours and, after each hour, 12.7 grams of each of nylon 6 and nylon 6,6 were added to the vessel. The condensate was weighed and analyzed every hour. Caprolactam was the only depolymerized value found in the distillate.

Results are summarized in Table A, below.

Table A

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<thead>
<tr>
<th>Time (hr)</th>
<th>Weight (g) Collected</th>
<th>Percent</th>
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<tr>
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<td>Caprolactam</td>
<td>in Distillate</td>
<td>of Melt (°C)</td>
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<td>11.1</td>
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<td>35</td>
<td>99.6</td>
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EXAMPLE 2

Two hundred grams of nylon 6,6 and 74 grams of nylon 6 were charged into the reaction vessel, along with 26.1 grams of sodium hydroxide. When the temperature of the charge reached 250°C, water flow for steam generation was started at 1.5 ml/minute. After one hour, 115 grams of distillate were collected containing 2.5 weight percent caprolactam and 12.5 weight percent hexamethylene diamine. The average temperature of the melt during this run was 280°C.

EXAMPLE 3

Two hundred grams of nylon 6,6 were charged into the reaction vessel, along with 26.1 grams of sodium hydroxide. When the temperature of the charge reached 260°C, water flow for steam generation was started at 1.5 ml/minute. After one hour, 155 grams of distillate were collected containing 22.3 weight percent hexamethylene diamine. No other depolymerized values were found in the distillate. The average temperature of the melt during this run was 292°C.
Claims

1. A process for depolymerizing a mixture of nylon 6 and nylon 6,6 comprising the steps of:
   (a) establishing a molten polymer system including: (i) 0-75 weight percent nylon 6 and 25-100 weight percent nylon 6,6; and (ii) basic nylon depolymerizing catalyst in an amount of 1-50 weight percent, based on the total weight of the polymer, at a temperature of 250 to 400°C;
   (b) conducting steam through the molten polymer system;
   (c) condensing the steam to obtain a mixture of water, caprolactam, and hexamethylene diamine.

2. The process of Claim 1 wherein the basic nylon depolymerizing catalyst is selected from the group consisting of alkali metal hydroxides and alkaline earth metal hydroxide.

3. The process of Claim 1 wherein the molten polymer system includes 25-75 weight percent nylon 6 and 25-75 weight percent nylon 6,6.
### INTERNATIONAL SEARCH REPORT

**A. CLASSIFICATION OF SUBJECT MATTER**  
**IPC 5** C07C209/62 C07D201/12

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
**IPC 5** C07C C07D C08J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

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Week 7901,  
Derwent Publications Ltd., London, GB;  
AN 79-00869B  
& JP, A, 53 132 585 (TOYOBO) 18 November 1978  
cited in the application  
see abstract --- | 1-3 |

| A          | GB, A, 963 368 (IMPERIAL CHEMICAL INDUSTRIES)  
see claims; examples --- | 1-3 |

| A          | BE, A, 518 416 (VEREINIGTE GLANZSTOFF-FABRIKEN A.G.) 18 February 1955  
see the whole document --- | 1-3 |

Further documents are listed in the continuation of box C.  
Patent family members are listed in annex.

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Date of the actual completion of the international search  
15 December 1993

Date of mailing of the international search report  
29. 12. 93

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Authorized officer  
Heywood, C

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