

1 567 071

(21) Application No. 353/77 (22) Filed 6 Jan. 1977  
 (31) Convention Application No. 647464 (32) Filed 8 Jan. 1976 in  
 (33) United States of America (US)  
 (44) Complete Specification Published 8 May 1980  
 (51) INT. CL. <sup>3</sup> H01J 47/02  
 (52) Index at Acceptance  
 H1D 13A3 13A5B 13A5Y 13B6B 13B6Y 13D  
 38 7A1A1 7A1C1 7A1C2 7A1C3 7A1CY  
 7A2F5 7A2FY 7A2G2 7A2G4 7A2GY 8G  
 9L 9Y



## (54) IMPROVED FILAMENT FOR ALKALI METAL IONISATION DETECTOR

(71) We, WESTINGHOUSE ELECTRIC CORPORATION of Westinghouse Building, Gateway Center, Pittsburgh, Pennsylvania, United States of America, a company organised and existing under the laws of the Commonwealth of Pennsylvania, United States of America, do hereby declare the invention, for which we pray that a patent may 5 be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:

This invention relates to an improved alkali metal ionization detector, including an oxide coated filament with extended operating life.

Conventional alkali metal ionization detectors, such as those used to monitor sodium, 10 potassium, lithium, etc., operate in vacuum and employ pure metal vacuum filaments and strive to minimize or avoid surface oxidation which has been considered to be detrimental to the useful operation of the detector filaments. Typical vacuum filament material used in alkali metal ionization detectors includes thoria-coated iridium, tungsten, platinum and rhodium. In alkali metal ionization detectors, such as that disclosed 15 in U.K. Patent Specification No. 1520749 the detector operating principle consists essentially of thermally ionizing particles or vapors contacting a heated filament to produce ions which are attracted to a collector electrode via an electric field thus producing a current flow which is an indication of the concentration of particles or vapors from 20 which the ions were formed. One of the major considerations in selecting the material composition for the heated filament for conventional alkali metal ionization detectors has been the material's capability of serving as an electron conductor free of surface 25 oxidation which would form an insulator coating thereby ostensibly reducing the effectiveness of the filament. While standard vacuum filament materials such as tungsten, platinum and platinum-rhodium, have operated satisfactorily in vacuum-type ionization detectors, the use of these conventional filament materials in alkali metal ionization 30 detectors operating in environments containing oxygen and at pressures above vacuum, such as atmospheric pressure, have proven unsatisfactory due to the drastic reduction in filament operating life.

It is the principal object of this invention to provide an improved alkali metal ionization 35 detector including an oxide coated filament with extended operating life.

This invention resides in an alkali metal ionization detector comprising; a thermal ionizer means consisting of a first electrode having an oxide protective coating for responding to impinging alkali metal atoms and compounds present in a carrier gas by producing positive alkali metal ions by thermal surface ionization of the alkali metal atoms and 40 compounds, said oxide protective coating being one of the group consisting of chromium oxide, aluminum oxide and silicon dioxide, first circuit means for maintaining the temperature of said thermal ionizer means at a temperature to ionize said alkali metal atoms and compounds, second electrode means, and second circuit means for establishing a flow of said positive alkali metal ions from said thermal ionizer means to said second electrode, said flow of positive alkali metal ions being indicative of the concentration of 45 said alkali metal present in said carrier gas.

As briefly stated above, the alkali metal ionization detector of this invention is capable of operating satisfactorily over an extended period of time in both an oxygen environment at pressures above or below atmospheric pressure, and a vacuum environment.

45 This eliminates the critical requirement for the vacuum conditions of conventional alkali

5

10

15

20

25

30

35

40

45

metal ionization detectors. An oxide coating is developed at the surface of the heating element material to produce a useful filament capable of supporting surface ionization and electron conductivity and having an operating life exceeding that offered by conventional filament materials.

5 There is disclosed herein with reference to the accompanying drawings a technique for utilizing conventional furnace heating element materials such as Nichrome, Kanthal A alloys, super Kanthal alloys, ("Nichrome" and "Kanthal" are Registered Trade Marks) as well as nickel-chromium-iron alloys, silicon carbide, iron-chromium-aluminum alloys and molybdenum disilicide for the filaments of alkali metal ionization detectors. Oxide

10 coatings are developed on the surface of the heating element material to produce an improved filament material which is substituted for conventional vacuum filaments for use in alkali metal ionization detectors operating in vacuum or in oxygen-containing environments at above vacuum pressures, including atmospheric pressure.

15 It has been determined through detailed experimental analysis of sodium ionization detectors employing oxide coated heated filaments constructed from conventional heating element material, that an alkali metal ionization detector can be developed for use in atmospheric pressure conditions without encountering the reduction in operating life of the filament which was observed during evaluation of alkali metal ionization detectors employing conventional pure metal vacuum filaments.

20 A common belief that alkali metals would form stable compounds with an oxide, such that the ion formation and emission required for operation of the alkali metal ionization detector would not occur, has been dispelled by detailed studies of sodium ionization detectors employing oxide-coated filaments of typical heating element material operating in atmospheric conditions. These studies further indicate that the oxide coating of such materials does in fact support good electronic conductivity and that the oxide coating does not significantly limit the electron transfer as has been traditionally assumed.

25 The invention will become more readily apparent from the following exemplary description in connection with the accompanying drawings:

30 Figure 1 is a schematic illustration of the typical embodiment of an alkali metal ionization detector;

35 Fig. 2 is a section illustration of an oxide-coated filament or thermal ionizer electrode for use in the embodiment of Fig. 1;

40 Fig. 3 is a listing of process steps to produce the oxide-coated thermal ionizer electrode or filament;

45 and Fig. 4 is a graphical illustration of the operational characteristics of oxide-coated filaments in an embodiment of the invention as illustrated in Fig. 1.

50 While the following disclosure has general application to alkali metal ionization detectors operating in an oxygen-containing environment at pressures above vacuum including atmospheric conditions, the discussion for the purposes of clarity, will be directed in particular to a sodium ionization detector, inasmuch as such a device is of particular current interest for monitoring sodium coolant systems such as those used in the fast breeder nuclear reactors.

55 The sodium ionization detector, as is typically illustrated in Fig. 1, employs a heated filament, or thermal ionizer electrode, which responds to impinging sodium atoms or sodium-containing compounds (vapor or aerosol) to form positive sodium ions by thermal surface ionization, the resultant sodium ions being attracted to a collector electrode via an electric field to produce an ion current which is an indication of the sodium concentration of the environment to which the heated filament is exposed.

60 Referring to Fig. 1, a typical embodiment of an alkali metal ionization detector 10 is illustrated as consisting of a heated cathode filament 12, also hereinafter functionally referred to as a thermal ionizer electrode, a collector anode 14, a filament transformer 16 for coupling filament voltage supply 18 to heat the cathode filament 12, an ion current meter 20 to indicate the ion current flow between the cathode filament 12 and the anode collector 14 which is maintained by an electric field produced by the voltage supply 22 which is connected between the cathode filament 12 and the anode collector 14. The embodiment of Fig. 1 is described in detail in the above referenced U.K. Patent Specification.

65 Sodium particles, whether contained in a vapor, aerosol or sodium compound, transported by a carrier gas such as flowing air to the vicinity of the detector 10, are converted to free sodium ions at the surface of the heated cathode filament 12 which functions as a thermal ionizer. These ions are then collected by the collector anode 14 which is maintained at a negative potential relative to the heated cathode filament 12 by the voltage source 22. The flow of ions thus established produces an ion current which is measured by the ion current meter 20 as an indication of the concentration of sodium

ions present in the environment adjacent to the heated cathode filament 12. The process by which the sodium particles are converted to free sodium ions can be thought of as occurring in the following steps:

- 5 1. The collision of sodium particles with the surface of the heated cathode filament 12 and their subsequent melting;
- 5 2. The rapid surface diffusion of the melted sodium over the heated cathode filament 12 to form a layer of adsorbed sodium atoms;
- 10 3. The transfer of valence electrons from some of the adsorbed sodium atoms to the heated cathode filament 12, converting them to adsorbed sodium ions; and
- 10 4. The desorption of the sodium ions from the surface to become free ions.

The free sodium ions thus generated contribute to the ion current monitored by the ion current meter 20.

15 While the use of traditional filament materials, such as platinum, platinum-rhodium and tungsten, etc. have operated satisfactorily in vacuum environments, the useful life of such materials has been significantly reduced when used in alkali metal ionization detectors designed to operate in oxygen environments at pressures above vacuum as would be encountered in a flowing air system.

20 It has been determined experimentally that materials typically used for heating elements in furnace applications, if processed properly, can produce a filament not only capable of functioning to thermally ionize alkali metal atoms in accordance with the above steps, but can provide a significantly longer operating life than that available from conventional vacuum filament materials when operating in oxygen environments at pressures above vacuum. The superior operation of the heating element materials such as Nichrome, Kanthal A, and super Kanthal is attributed to the formation of an oxide coating 13 on the surface of the heating element material, as illustrated in Fig. 2, which acts as a protective filament coating, thus increasing the operating life of the material in non-vacuum conditions, while supporting the necessary surface ionization and electron conductivity required of the heated cathode element 12 of an alkali metal ionization detector of the type illustrated in Fig. 1. The protective oxide coating 13 developed on 25 the surface of the heating element materials when subjected to elevated detector operating temperatures, reduces the vaporization of the underlying metal and thus protects it from rapid oxidation. Such oxide-protected heating element materials, when employed as the heated cathode filaments of an alkali metal ionization detector, support the necessary operation of the alkali metal ionization detector as listed above while further providing operating lifetimes significantly longer than those achieved with the traditional pure metal vacuum electrode materials when operating in an oxygen environment.

30 35 Three specific oxide-protected filaments tested include chromium oxide, aluminum oxide and silicon dioxide-protected filaments. The aluminum oxide-protected filament is achieved by temperature cycling Kanthal A which is an alloy of iron, chromium and aluminum to a first temperature level of approximately 1100-1200°C to produce an aluminum oxide ( $Al_2O_3$ ) coating and to yet a higher temperature to bake out alkali metal impurities in accordance with the process steps of Fig. 3. Typically this temperature cycling occurs with the filament secured within a detector embodiment such as that 40 45 illustrated in Fig. 1 through the use of the filament voltage supply 18. The electric field established by the supply voltage 22 functions to remove the alkali metals produced during the bake-out of the filament. While the temperature cycling could be accomplished by inserting the filament in an oven, the oven heating elements would tend to generate more alkali metal impurities than would be removed from the filament.

50 55 Corresponding temperature cycling of super Kanthal, which consists of a binder, such as clay, and molydisilicide ( $MoSi_2$ ) produces a silicon dioxide protected filament while temperature cycling of a Nichrome heating element, which is an alloy of nickel and chromium, will produce a chromium oxide protected filament suitable for use in an alkali metal ionization detector operating in atmospheric conditions.

55 The following tabulation illustrates the improved filament lifetime achieved with filaments coated with chromium oxide, aluminum oxide or silicon dioxide, in contrast with traditional filament materials represented by thoria-coated iridium and the platinum group represented by platinum-10% rhodium.

## Lifetimes of Filament Materials in Air

	Material	No. Of Filaments	Temperature, °C	Average life, Hours	
5	Thoria-coated iridium	1	1000	0.2	5
	Platinum-10% Rhodium	1	1000	365	
10	Rhodium	4	1100	59	10
	Chromium oxide protected	2	1100	526	
15	Chromium oxide protected	1	1000	2,324	15
	Aluminum oxide protected	1	1200	680	
	Aluminum oxide protected	4	1100	5,024	
20	Silicon dioxide protected	1	1200	11,059*	20
	Silicon dioxide protected	1	1200	10,074*	

\* Life tests still in progress, 12/23/75.

25 The processing steps, as listed in Fig. 3, for super Kanthal to achieve the desired silicon dioxide protected filament consists of:

30 1. Heating a filament, or thermal ionizer electrode, constructed from super Kanthal in an oxygen environment, i.e. air, at a temperature between 1100 and 1200°C, which corresponds to the incandescent region, for approximately one-half hour to produce the desired silicon dioxide coating, and

35 2. Heating the silicon dioxide coated filament achieved in step 1 in an inert gas environment, such as nitrogen, at a temperature higher than that of step 1, i.e., 1300-1400°C, to bake out alkali metal impurities present in the filament.

40 The corresponding temperature processing of Nichrome to achieve a suitable chromium oxide protected nichrome filament consists of steps 1 and 2 above substituting the temperature of approximately 1100°C for step 1 and the temperature range of 1200-1300° for step 2. These same process parameters will produce an aluminum oxide protective coating on Kanthal A-1.

45 In addition to the advantages of the silicon dioxide coating of the super Kanthal, the operating temperature for the super Kanthal oxide protected filament is approximately 900°C which is significantly less than the temperature range for producing the oxide coating in accordance with process step 1 which further improves the operating life of the silicon dioxide super Kanthal filament.

50 Inasmuch as the oxide-coating filaments are derived from conventional heating element materials, such as those identified above, the detector operating temperatures in excess of 700°C required for dissociating sodium atoms from sodium compounds such as sodium hydroxide, in order to appropriately monitor the sodium concentration of a gas, vapor, or aerosol, are well within the temperature capabilities of the heating element material used to construct the filaments for the alkali metal ionization detector 10.

55 The results of Fig. 4 of filaments constructed in accordance with the above processes, clearly indicates that the oxide coating does in fact support sodium diffusion at rates which render the oxide protected heating element materials most desirable for use in alkali metal ionization detectors.

60 The section view of a typical oxide-coated heating element material used as the heated cathode filament of an alkali metal ionization detector is illustrated in Fig. 2.

65 While the above discussion clearly supports the operational status of oxide-coated filaments for alkali metal ionization detectors, the embodiments disclosed by way of example rely on the reaction of the inherent material composition of the filament in an oxygen atmosphere, i.e. air, at elevated temperatures to develop the desired oxide coating. A similar result can also be achieved via a process which deposits a coating of a

selected composition on the surface of the filament via any one of several well known techniques such as evaporation in vacuum, cathode sputtering, chemical vapor deposition, chemical solution deposition and ion plating.

WHAT WE CLAIM IS:

5 1. An alkali metal ionization detector comprising: a thermal ionizer means consisting 5  
of a first electrode having an oxide protective coating for responding to impinging alkali 10  
metal atoms and compounds present in a carrier gas by producing positive alkali metal 10  
ions by thermal surface ionization of the alkali metal atoms and compounds, said oxide 15  
protective coating being one of the group consisting of chromium oxide, aluminum oxide 15  
and silicon dioxide, first circuit means for maintaining the temperature of said thermal 20  
ionizer means at a temperature to ionize said alkali metal atoms and compounds, second 20  
electrode means, and second circuit means for establishing a flow of said positive alkali 25  
metal ions from said thermal ionizer means to said second electrode, said flow of positive 25  
alkali metal ions being indicative of the concentration of said alkali metal present in  
said carrier gas.

2. An alkali metal ionization detector as claimed in claim 1 wherein said carrier gas  
is an oxygen-containing carrier gas.

3. An alkali metal ionization detector as claimed in claim 1 wherein said thermal  
ionizer means is exposed to atmospheric pressure.

4. An alkali metal ionization detector as claimed in claim 1 wherein said carrier gas  
contains oxygen and the pressure to which the thermal ionizer means is subjected is  
above vacuum.

5. An alkali metal ionization detector substantially as described hereinbefore with  
reference to, and as shown in Figs. 1 and 2 of the accompanying drawings.

25 Agent for the Applicants  
RONALD VAN BERLYN

Printed for Her Majesty's Stationery Office, by Croydon Printing Company Limited, Croydon, Surrey, 1980.  
Published by The Patent Office, 25 Southampton Buildings, London, WC2A 1AY, from  
which copies may be obtained.

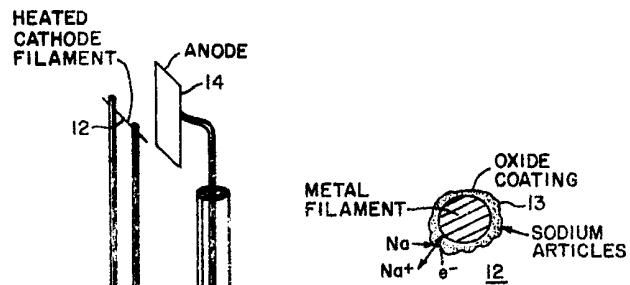


FIG. 2

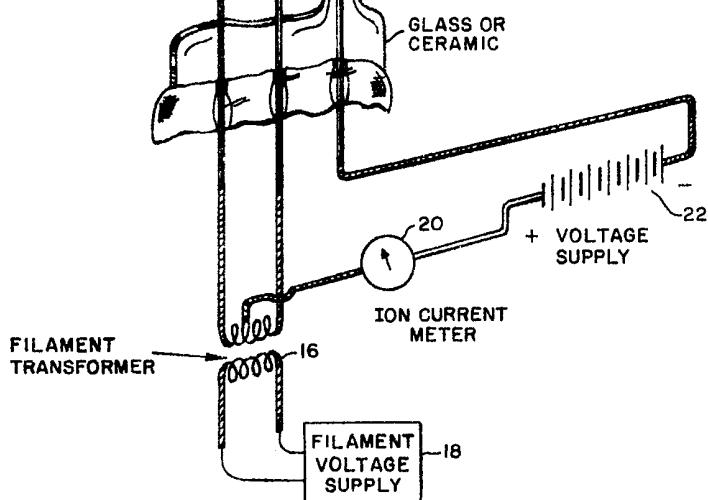


FIG. 1

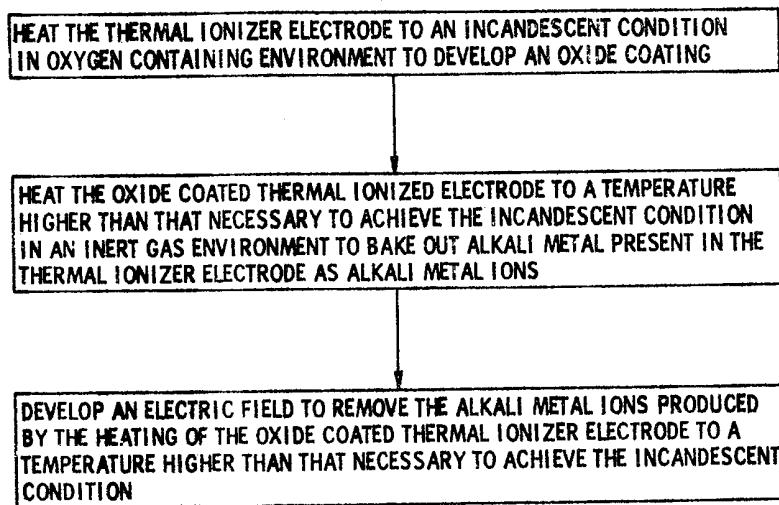


FIG. 3

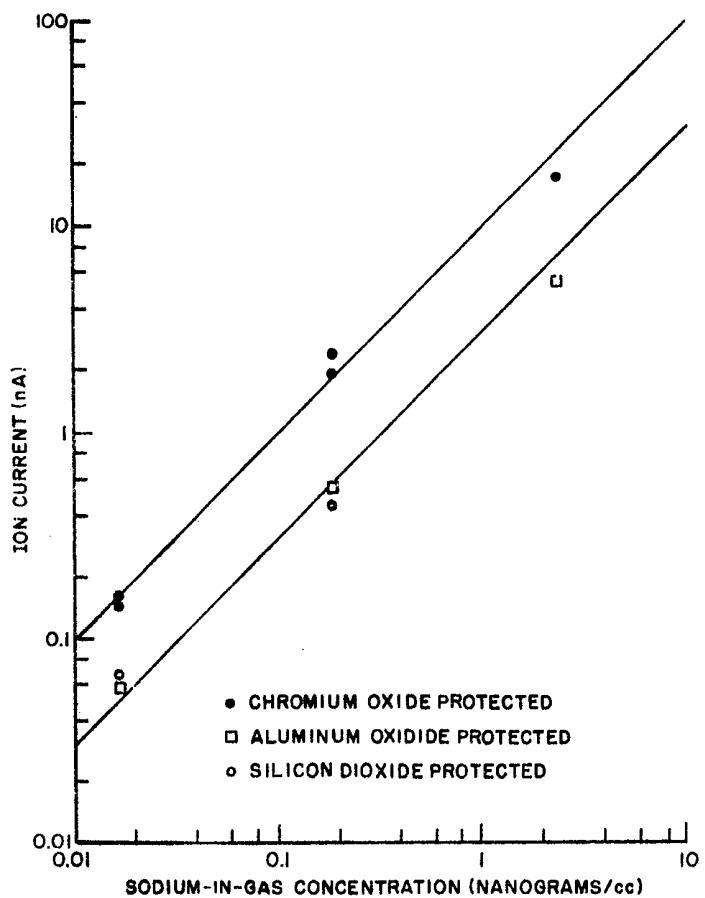


FIG. 4