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Description

BACKGROUND OF THE INVENTION

[0001] The present invention relates to evaporators for use in air conditioners such as room air conditioners and motor vehicle air conditioners.

[0002] An evaporator of this kind is shown, for example, in document U5-A-5,323,851. This document comprises an evaporator unit including a pair of headers arranged one above the other in parallel and spaced apart by a distance, and parallel refrigerant tubes having a width oriented in a front-rear direction and opposite ends joined to the respect headers, each of the refrigerant tubes being in the form of a flat tube comprising flat left and right walls, front and rear walls positioned between and joined to front and rear side edges of the left and right walls, and a plurality of reinforcing walls positioned between and joined to the left and right walls and extending longitudinally thereof, the reinforcing walls being arranged at a predetermined interval between the front and rear walls, the flat tube having parallel refrigerant channels inside thereof and being formed from a metal plate, each of the reinforcing walls comprising a reinforcing wall forming portion inwardly projecting from the metal plate integrally therewith.

[0003] Moreover, document EP-A-0 617 250 discloses a refrigerant tube for use in heat exchangers, comprising a flat aluminium tube having parallel refrigerant passages in its interior and comprising flat upper and lower walls and a plurality of reinforcing walls which are formed with communication holes for causing the parallel refrigerant passages to communicate with one another. The flat aluminium tube is prepared from upper and lower two aluminium sheets by bending opposite side edges of the lower sheet to a raised form and joining the bent edges of the respective side edges of the upper aluminium sheet so as to form a hollow portion. The reinforcing walls are formed by joining to the inner surface of the upper wall ridges projecting inward from the lower wall. The communication holes are formed by cutouts formed in the edges of the ridges at a predetermined spacing and having their openings closed with the upper wall.

[0004] The term the "forward," "rearward" or "front-rear" direction as used herein refers to a direction parallel to the direction of flow of air through the evaporator, and the term the "left-right" direction to a direction orthogonal to the above direction. When described with reference to FIG. 3, the left-hand side of the drawing is referred to as "front," the right-hand side thereof as "rear," the lower side thereof as "left," and the upper side thereof as "right."

[0005] Moreover, conventional evaporators for use in motor vehicle air conditioners are layered evaporators such as those disclosed in JP-A-230064/1991. The disclosed layered evaporator comprises a plurality of tube elements each composed of a pair of vertically elongat-

ed plates which are prepared by press work, each formed on its inner side with projecting ribs extending vertically, opposed and fitted to each other with the ribs positioned inside, and brazed to each other at their peripheral edge portions. The tube elements each have a flat tubular portion extending vertically and are arranged side by side in the direction of the thickness thereof into a layered assembly with a fin interposed between each pair of adjacent elements. The tube elements each have a bulging tank portion formed at each of the upper and lower ends and communicating with the flat tubular portion, and are joined by brazing to one another at their tank portions as held in communication at the tank portions. With reference to FIG. 18 showing the tube element 70, the ribs 73, 74 of the vertically elongated plates 71, 72 project inward so as to be approximately U-shaped in cross section. The ribs 73 of the plate 71 are positioned between the ribs 74 of the other plate 72 and have their projecting ends brazed to the other plate 72, and the ribs 74 of the other plate 72 are brazed at their projecting ends to the plate 71, whereby a plurality of parallel refrigerant channels 75 are formed.

[0006] However, the conventional evaporator has the following problem. The ribs 73, 74 of the plates 71, 72 are U-shaped in cross section, so that useless space portions not contributing to the passage of the refrigerant occur as indicated at 76 in FIG. 18, consequently imposing a limitation on the increase in the number of refrigerant channels 75 when the tube element is given a specified width. Moreover, the elongation of the material in the manufacturing process is limited by the restriction involved in the press techniques, such that if the spacing between the adjacent ribs 73, 74 are diminished, the plates 71, 72 will develop cracks. The spacing between the adjacent ribs 73, 74 must therefore be made relatively large, consequently making it impossible to give a decreased equivalent diameter to the refrigerant channels 75 and to form an increased number of channels 75 if the tube element 70 has the specified width. Thus, there is a limit on the heat exchange performance, i.e., on the improvement in the evaporation efficiency of the refrigerant.

[0007] It appears that the above problem can be overcome by an evaporator which comprises at least one evaporator unit including a pair of headers arranged one above the other in parallel and spaced apart by a distance, and parallel refrigerant tubes having opposite ends joined to the respect headers, each of the refrigerant tubes being in the form of a hollow extruded member comprising flat left and right walls and a plurality of reinforcing walls positioned between and joined to the left and right walls, extending longitudinally thereof and arranged at a predetermined interval. With this evaporator, it is possible to provide an increased number of refrigerant channels and to give a decreased equivalent diameter to the channels unlike the flat tubular portion of tube element of the conventional evaporator. In order to achieve an improvement in heat exchange efficiency,

i.e., in refrigerant evaporation efficiency, and to provide a compacted evaporator, it is desired that the refrigerant tube be reduced in its wall thickness and given a minimized width in the left-right direction. In the case of extruded materials, however, the restriction involved in extrusion techniques imposes limitations on the reduction of the wall thickness while assuring the tube of dimensional accuracy and on the decrease of the lateral width of the tube with dimensional accuracy. In the case of extrudates, moreover, it is impossible to form communication holes in the reinforcing walls for holding the parallel refrigerant channels in communication with one another although these holes are considered to be effective for achieving an improved efficiency.

SUMMARY OF THE INVENTION

[0008] An object of the present invention is to overcome all the foregoing problems and to provide a compact evaporator which is improved over the conventional evaporator in heat exchange performance, i.e., in refrigerant evaporation efficiency, and also over the evaporator comprising extruded hollow members in heat exchange efficiency, i.e., in refrigerant evaporation efficiency.

[0009] The present invention provides an evaporator which is characterized by the features of claim 1.

[0010] The evaporator of the present invention has refrigerant tubes each in the form of a flat tube comprising flat left and right walls, front and rear walls positioned between and joined to front and rear ends of the left and right walls, and a plurality of reinforcing walls positioned between and joined to the

[0011] left and right walls, extending longitudinally thereof and arranged at a predetermined interval between the front and rear walls. The flat tube has parallel refrigerant channels inside thereof and is formed from a metal plate. Each of the reinforcing walls comprises a reinforcing wall forming portion inwardly projecting from the metal plate integrally therewith. Accordingly, unlike the flat tubular portion of tube element of the conventional evaporator disclosed in JP-A-230064/1991, the flat tube can be increased in the number of refrigerant channels, with a decreased equivalent diameter given to the channels. Consequently, the evaporator is improved over the evaporator of the publication in heat exchange performance, i.e., refrigerant evaporation efficiency. Moreover, the refrigerant tube can be diminished in wall thickness with dimensional accuracy unlike the extruded hollow member, with the width in the left-right direction decreased with dimensional accuracy. The present evaporator can therefore be improved in heat exchange performance, i.e., refrigerant evaporation efficiency, and compacted as compared with the evaporator comprising the hollow extrudate.

[0012] Preferably, the reinforcing walls of the present evaporator are formed with a plurality of communication holes for causing the parallel refrigerant channels to

communicate with one another. The communication holes are preferably in a staggered arrangement when seen from the left. Preferably, each of the reinforcing walls is 10 to 40% in opening ratio which is the ratio of all the communication holes in the reinforcing wall to the reinforcing wall.

[0013] The present invention will be described in greater detail with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0014]

FIG. 1 is a perspective view showing the overall construction of a first embodiment of an evaporator according to the state of the art;

FIG. 2 is a diagram showing the flow of refrigerant through the first embodiment;

FIG. 3 is a fragmentary perspective view partly broken away and showing a refrigerant tube included in the first embodiment;

FIG. 4 is an enlarged fragmentary view in cross section of the refrigerant tube;

FIG. 5 is a view in section taken along the line V-V in FIG. 4;

FIG. 6 is a perspective view showing the overall construction of a second embodiment of evaporator according to the state of the art;

FIG. 7 is a diagram showing the flow of refrigerant through the second embodiment;

FIG. 8 is a perspective view showing the overall construction of a third embodiment of evaporator according to the state of the art;

FIG. 9 is a diagram showing the flow of refrigerant through the third embodiment;

FIG. 10 is a perspective view showing the overall construction of a fourth embodiment of evaporator according to the state of the art;

FIG. 11 is a diagram showing the flow of refrigerant through the fourth embodiment;

FIG. 12 is a perspective view showing the overall construction of a fifth embodiment of evaporator according to the state of the art;

FIG. 13 is a diagram showing the flow of refrigerant through the fifth embodiment;

FIG. 14 is a perspective view showing the overall construction of a sixth embodiment of evaporator according to the state of the art;

FIG. 15 is a diagram showing the flow of refrigerant through the sixth embodiment;

FIG. 16 is a perspective view partly broken away and showing the overall construction of an embodiment of evaporator of the invention; and

FIG. 17 is a graph showing the results achieved in Example 2 and Comparative Example 3.

FIG. 18 is a fragmentary view in cross section of a tube element of the conventional evaporator.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0015] Throughout the drawings, like parts are designated by like reference numerals and will not be described repeatedly.

[0016] FIG. 1 shows the overall construction of an evaporator as a first embodiment according to the state of the art, FIG. 2 shows the flow of refrigerant through the evaporator, and FIGS. 3 to 5 are fragmentary views showing main components of the evaporator.

[0017] It is noted that the following embodiments of evaporators represent the state of the art and are merely described because of explanatory reasons. In particular, FIG. 1 to 15 show six known embodiments of the evaporator.

[0018] The term "aluminum" as used in the following description includes pure aluminum and other aluminum alloys.

[0019] With reference to FIG. 1, the evaporator 1 comprises two evaporator units 1A each including a pair of headers 2, 3 arranged one above the other in parallel and spaced apart by a distance, parallel flat refrigerant tubes 4 having a width oriented in the front-rear direction and opposite ends joined to the respective headers 2, 3, and a corrugated aluminum fin 5 disposed in an air passing clearance between each pair of refrigerant tubes 4 and brazed to the two tubes 4. The two evaporator units 1A are arranged in parallel as spaced apart in the front-rear direction. The upper headers 2 of the two evaporator units 1A are caused to communicate with each other and the lower headers 3 thereof are caused to communicate with each other by two communication pipes 6, 7, respectively. The communication pipes 6, 7 are connected at their opposite ends to the lengthwise midportions of the two upper headers 2 and to the lengthwise midportions of the two lower headers 3, respectively. A refrigerant inlet pipe 8 is connected to the underside of the lengthwise midportion of the lower communication pipe 7. A refrigerant outlet pipe 9 is connected to the upper side of the lengthwise midportion of the upper communication pipe 6. With reference to FIG. 2, the refrigerant flowing into the lower communication pipe 7 through the inlet pipe 8 in a liquid phase flows dividedly into the lower headers 3 of the two evaporator units 1A, changes into a vapor phase while flowing upward through the refrigerant tubes 4, enters the upper headers 2 and then flows out from the outlet pipe 9 via the upper communication pipe 6.

[0020] As shown in FIGS. 3 to 5, each refrigerant tube 4 is in the form of a flat tube 17 of aluminum which comprises flat left and right walls 11, 12, front and rear walls 13, 14 positioned between and joined to the front and rear side edges of the left and right walls 11, 12, and a plurality of reinforcing walls 15 positioned between and joined to the left and right walls 11, 12, extending longitudinally thereof and arranged at a predetermined interval between the front and rear walls 13, 14. The tube 4

has parallel refrigerant channels 16 inside thereof.

[0021] Between each pair of adjacent reinforcing walls 15, the left wall 11 of the flat tube 17 is formed on the inner surface thereof with a plurality of projections 18 projecting rightward from the left wall 11 integrally therewith and arranged longitudinally of the wall 11 at an interval so as to give an increased area of heat transfer. The reinforcing walls 15 are formed with a plurality of communication holes 19 for causing the parallel refrigerant channels 16 to communicate with one another. The communication holes 19 are in a staggered arrangement when seen from the left. When the holes 19 are formed, the fluid flowing through the parallel fluid channels 16 also flows through the holes 19 transversely of the flat tube 17, spreading over all the fluid channels 16 to become stirred and eliminating any difference in the temperature of the fluid between the channels 16. This achieves an improvement in heat exchange efficiency, i.e., in refrigerant evaporation efficiency. Each of the reinforcing walls 15 is 10 to 40%, preferably 10 to 30%, more preferably about 20%, in opening ratio which is the ratio of all the communication holes 19 in the reinforcing wall 15 to the reinforcing wall. The communication holes 19 formed then result in a remarkable improvement in heat exchange efficiency.

[0022] The flat aluminum tube 17 is formed by a left component 21 in the form of an aluminum plate and providing the left wall 11, front and rear walls 13, 14 and reinforcing walls 15; and a right component 22 in the form of an aluminum plate and providing the right wall 12, and front and rear walls 13, 14. The left component 21 comprises a left wall forming portion 23, rightward projecting walls 24 rightwardly projecting respectively from the front and rear side edges of the portion 23 integrally therewith, and reinforcing wall forming portions 25 inwardly projecting from the left wall forming portion 23 integrally therewith. A plurality of cutouts 26 are formed in the right edges of the reinforcing wall forming portions 25 and spaced apart at an interval longitudinally of the portions 25, the outer ends of the wall forming portions 25 are brazed to the right wall 12, and the openings of the cutouts 26 are closed with the right wall 12, whereby the communication holes 19 are formed. The left component 21 is externally formed at each of its front and rear side edges with a slope 27 slanting rightward externally of the front-rear direction.

[0023] The right component 22 comprises a right wall forming portion 28, and leftward projecting walls 29 leftwardly projecting respectively from the front and rear side edges of the portion 28 integrally therewith. The leftward projecting walls 29 have an original height slightly greater than the height of the reinforcing wall forming portions 25 of the left component 21 plus the thickness of the left wall forming portion 23 (see the broken line in FIG. 4). The front and rear walls 13, 14 of the flat tube 17 are formed by the rightward projecting walls 24 of the left component 21 and the leftward projecting walls 29 of the right component 22.

[0024] The left component 21 is prepared from an aluminum brazing sheet having a brazing material layer only on the outer side thereof. The right component 22 is prepared from an aluminum brazing sheet having a brazing material layer on each of opposite sides thereof.

[0025] The left component 21 and the right component 22 are fitted to each other so that the leftward projecting walls 29 of the right component 22 are positioned outside of and lap over the respective rightward projecting walls 24 of the left component 21. The left end of each leftward projecting wall 29 is bent inward toward the front-rear direction, and the inward bent portion 29a is engaged with the slope 27 in intimate contact therewith, thereby the two components 21, 22 are tacked together. In this state, each rightward projecting wall 24 and the corresponding leftward projecting wall 29 are brazed to each other, the outer ends of the reinforcing wall forming portions 25 are brazed to the right wall forming portion 28, and each inward bent portion 29a is brazed to the respective slope 27 to form the flat tube 17.

[0026] The left component 21 is formed by rolling. The right component 22 by roll forming. The left component 21 is rolled by a usual rolling mill. Alternatively the left component 21 may be formed by a rolling mill which comprises a central work roll, and a plurality of planetary work rolls arranged around the central work roll, equidistantly spaced apart circumferentially thereof and rotatable at the same peripheral speed as the central work roll. The central work roll or each of the planetary work rolls is formed with rightward projecting wall forming annular grooves and reinforcing wall forming annular grooves in its peripheral surface over the entire circumference thereof. The ridge portion between each pair of adjacent reinforcing wall forming grooves is formed with projection forming cavities as arranged at a spacing circumferentially of the roll, and the bottom surface defining each reinforcing wall forming groove has cutout forming projections. The aluminum brazing sheet for the left component 21 is continuously passed between the central work roll and all the planetary work rolls, whereby the configurations of the grooves, cavities and projections are transferred to the sheet to give the left component 21 of the desired shape.

[0027] FIGS. 6 and 7 show another evaporator 30.

[0028] With reference to FIG. 6, the evaporator 30 differs from the evaporator 1 according to the first embodiment in that a refrigerant inlet pipe 31 is connected to the upper side of the lengthwise midportion of the upper communication pipe 6, with a refrigerant outlet pipe 32 connected to the lower side of the lengthwise midportion of the lower communication pipe 7. With the exception of this feature, the second embodiment has the same construction as the first.

[0029] As seen in FIG. 7, the refrigerant flowing into the upper communication pipe 6 through the inlet pipe 31 in a liquid phase dividedly flows into the upper headers 2 of the two evaporator units 1A, is then converted into a vapor phase while flowing down the refrigerant

tubes 4, enters the lower headers 3 and flows out from the outlet pipe 32 via the lower communication pipe 7.

[0030] FIGS. 8 and 9 show another evaporator 35.

[0031] With reference to FIG. 8, the evaporator 35 comprises two evaporator units 1A, the upper headers 2 of which are interconnected at their right ends by a communication pipe 36 for holding the header right ends in communication with each other. The lower headers 3 of the two units 1A are held out of communication with each other. A refrigerant inlet pipe 37 is connected to the left end of lower header 3 of the rear evaporator unit 1A, and a refrigerant outlet pipe 38 is connected to the left end of lower header 3 of the front unit 1A. The third embodiment is the same as the first except this feature.

[0032] As shown in FIG. 9, the refrigerant flowing into the lower header 3 of the rear unit 1A through the inlet pipe 37 in a liquid phase flows upward through the refrigerant tubes 4 of the unit into the upper header 2, then flows into the upper header 2 of the front unit 1A by way of the communication pipe 36, subsequently flows down the refrigerant tubes 4 into the lower header 3 and flows out from the outlet pipe 38 in the form of a vapor phase.

[0033] FIGS. 10 and 11 show another evaporator 40.

[0034] With reference to FIG. 10, the evaporator 40 comprises two evaporator units 1A having upper and lower headers 2, 3. The upper headers 2 and the lower headers 3 are respectively interconnected at their left ends by communication pipes 41, 42 for communication. A refrigerant inlet pipe 43 is connected to the left side of lengthwise midportion of the lower communication pipe 42, with a refrigerant outlet pipe 44 connected to the left side of lengthwise midportion of the upper communication pipe 41. The fourth embodiment is the same as the first except this feature.

[0035] As shown in FIG. 11, the refrigerant flowing into the lower communication pipe 42 via the inlet pipe 43 in a liquid phase dividedly flows into the lower headers 3 of the two units 1A, is then converted to a vapor phase while flowing upward through the refrigerant tubes 4 of the two units 1A to flow into the upper headers 2 and thereafter flows out from the outlet pipe 44 by way of the upper communication pipe 41.

[0036] FIGS. 12 and 13 show another evaporator 45.

[0037] With reference to FIG. 12, the evaporator 45 comprises two evaporator units 1A, the upper headers 2 of which are held in communication with each other by a communication pipe 6 interconnecting the lengthwise midportions of these headers, while the lower headers 3 are held out of communication with each other. A refrigerant inlet pipe 46 is connected to the lower side of lengthwise midportion of the lower header 3 of the rear unit 1A, and a refrigerant outlet pipe 47 is connected to the lower side of lengthwise midportion of the lower header 3 of the front unit 1A. With the exception of this feature, the fifth embodiment is the same as the first.

[0038] Further with reference to FIG. 13, the refrigerant flowing into the lower header 3 of the rear unit 1A

through the inlet pipe 46 in a liquid phase flows upward through the refrigerant tubes 4 into the upper header 2, then flows into the upper header 2 of the front unit 1A via the communication pipe 6, subsequently flows down the tubes 4 into the lower header 3 and flows out from the outlet pipe 47 in the form of a vapor phase.

[0039] FIGS. 14 and 15 show another evaporator 50.

[0040] With reference to FIG. 14, the evaporator 50 comprises two evaporator units 1A, the upper headers 2 of which are held in communication with each other by a communication pipe 6 interconnecting the lengthwise midportions of the headers, with the lower headers 3 held out of communication. A refrigerant inlet pipe 51 is connected to the left end of the lower header 3 of the rear unit 1A, and a refrigerant outlet pipe 52 is connected to the left end of the lower header 3 of the front unit 1A. The sixth embodiment is the same as the first except this feature.

[0041] As seen in FIG. 15, the refrigerant flowing into the lower header 3 of the rear unit 1A via the inlet pipe 51 in a liquid phase flows upward through the refrigerant tubes 4 into the upper header 2, then flows into the upper header 2 of the front unit 1A through the communication pipe 6, thereafter flows down the refrigerant tubes 4 into the lower header 3 and flows out from the outlet pipe 52 in the form of a vapor phase.

[0042] FIG. 16 shows an evaporator 55 representing an embodiment of the invention.

[0043] With reference to FIG. 16, the evaporator 55 comprises a single evaporator unit 55A. The unit 55A comprises a pair of headers 56, 57 arranged one above the other in parallel and spaced apart by a distance, and a plurality of refrigerant tube groups 58 each including a plurality of, e.g., three, refrigerant tubes 4 arranged at a spacing in the front-rear direction and having a width oriented in this direction and opposite ends joined to the respective headers 56, 57. The tube groups 58 are arranged side by side at an interval in the left-right direction.

[0044] The upper header 56 comprises a boxlike header body 59 opened downward, and a header plate 60 closing the lower opening. The refrigerant tubes 4 are joined at their upper ends to the header plate 60.

[0045] The lower header 57 corresponds to the upper header 56 as turned upside down and has a header plate 60 with the lower ends of the tubes 4 joined thereto. The lower header 57 is provided at the lengthwise midportion thereof with a partition 61, which divides the interior of the lower header 57 in two. A refrigerant inlet pipe 62 is connected to the bottom wall of the lower header 57 at the right side of the partition 61, and a refrigerant outlet pipe 63 is connected to the bottom wall at the left side of the partition.

[0046] With this evaporator 55, the refrigerant flowing into the unit 55A at the right side of the partition 61 via the inlet pipe 62 in a liquid phase flows upward through all the tubes 4 at the right of the partition 61, then passes through the upper header 56, further flows into all the

tubes 4 at the left of the partition 61, flows down these tubes into the lower header 57 at the left of the partition 61 and flows out via the outlet pipe 63 in a vapor phase.

5 EXAMPLES AND COMPARATIVE EXAMPLES

Example 1

[0047] The evaporator 55 was used in this example.

[0048] The evaporator 55 was 227 mm in length L in the left-right direction, 60 mm in width W in the front-rear direction, and 235 mm in height H. The flat tube 17 serving as each refrigerant tube 4 was 18 mm in width in the front-rear direction and 1.7 mm in thickness in the left-right direction. The tube groups 58 each comprising three refrigerant tubes 4 was 22 in number.

[0049] First, the air-side heat transfer area A (m²) and the refrigerant-side heat transfer area B (m²) were determined. Using HFC134a as the refrigerant, the quantity of heat exchange, Q (kcal/h), and the air-side resistance to the passage of air, ΔPa (wet) (mm Aq), were measured under the conditions of: air inlet temperature (dry bulb: 25 deg C, wet bulb: 17.8 deg C), pressure before expansion valve: 16.5 kg/cm² G, subcooling: 5 deg, evaporator outlet pressure: 1.8 kg/cm² G, superheat: 5 deg and inlet air delivery: 450 m³/h.

Comparative Example 1

[0050] An evaporator was used which comprised refrigerant tubes of hollow aluminum extrudate in place of the flat refrigerant tubes used in the above example. The size of the evaporator was the same as the one used in the above example, the refrigerant tubes of hollow extrudate were of the same size as the flat tubes of the example.

[0051] First, the air-side heat transfer area A (m²) and the refrigerant-side heat transfer area B (m²) were determined. Using HFC134a as the refrigerant, the quantity of heat exchange, Q (kcal/h), and the air-side resistance to the passage of air, ΔPa (wet) (mm Aq), were measured under the same conditions as in the foregoing example.

Comparative Example 2

[0052] Used in this comparative example was the same evaporator as used in the above example except that the evaporator had the construction disclosed in JP-A-230064/1991 and measured 75 mm in width in the front-rear direction.

[0053] First, the air-side heat transfer area A (m²) and the refrigerant-side heat transfer area B (m²) were determined. Using HFC134a as the refrigerant, the quantity of heat exchange, Q (kcal/h), and the air-side resistance to the passage of air, ΔPa (wet) (mm Aq), were measured under the same conditions as in the foregoing example.

[0054] The results are collectively given in the table below

	A	B	Q	ΔPa (wet)
Example	77	137	100	66
Comp. Ex. 1	77	116	88	72
Comp. Ex. 2	100	100	100	100

[0055] The values given in the table for the heat transfer areas A and B, heat exchange quantity Q and resistance ΔPa (wet) are each expressed in a ratio relative to the corresponding value of Comparative Example 2 which is taken as 100.

[0056] The table reveals that the evaporator of Example 1 is equivalent to the evaporator of Comparative Example 2 in the quantity of heat exchange although smaller in width and smaller in its entirety, presumably because the former has an increased heat transfer area on the refrigerant side although smaller than the latter in width in the front-rear direction. Furthermore, the evaporator of Example 1 is smaller than that of Comparative Example 2 in air-side resistance to the passage of air, consequently permitting passage of an larger amount of air and leading to an increased quantity of heat exchange. The evaporator of Comparative Example 1, is smaller than that of Example 1 in the quantity of heat exchange although of the same size as the evaporator of Example 1. This appears attributable to the smaller refrigerant-side heat transfer area of the comparative evaporator and to the absence of the communication holes formed in the reinforcing walls for holding the parallel channels in communication with one another.

Example 2

[0057] The refrigerant tube 4 of Example 1 was used to determine the relationship between the average quality of the refrigerant (mass proportion of the vapor in the refrigerant) X (%) and the heat transfer coefficient h by the following method. The refrigerant tube was disposed in a cooling water channel, and HFC134a serving as the refrigerant was passed through the tube, with cooling water caused to flow through the channel. After the lapse of a specified period of time, the heat transfer coefficient h was measured at varying average quality values of the refrigerant under the conditions of: refrigerant flow rate, 400 kg/m²·s; heat flux between refrigerant and cooling water, 8 kW/m²; refrigerant saturation temperature T, 40 deg C; and cooling water flow rate to give a Reynolds number of 1500.

Comparative Example 3

[0058] The refrigerant tube of Comparative Example 1 was used to establish the relationship between the average quality of the refrigerant, HFC134a, X (%) and the

heat transfer coefficient h by the same method as in Example 2.

[0059] FIG. 17 shows the results of Example 2 and Comparative Example 3.

[0060] FIG. 17 reveals that Example 2 involving an increased refrigerant-side heat transfer area and the presence of communication holes formed in the reinforcing walls is greater in heat transfer coefficient h than Comparative Example 3 which is small in refrigerant-side heat transfer area and has no communication holes.

Claims

1. An evaporator (55) comprising a single evaporator unit (55A) including a pair of headers (56,57) arranged one above the other in parallel and spaced apart by a distance, and parallel refrigerant tubes (4) having a width oriented in a front-rear direction and opposite ends joined to the respective headers (56,57), each of the refrigerant tubes (4) being in the form of a flat tube (17) comprising flat left and right walls (11,12), front and rear walls (13,14) positioned between and joined to front and rear side edges of the left and right walls (11,12), and a plurality of reinforcing walls (15) positioned between and joined to the left and right walls (11,12) and extending longitudinally thereof, the reinforcing walls (15) being arranged at a predetermined interval between the front and rear walls (13,14), the flat tube (17) having parallel refrigerant channels (16) inside thereof and being formed from two metal plates (21,22), each of the reinforcing walls (15) comprising a reinforcing wall forming portion (25) inwardly projecting from one (21) of the metal plates integrally therewith, **characterized in that** the evaporator unit (55A) comprises a plurality of refrigerant tube groups (58) each comprising a plurality of refrigerant tubes (4) arranged at an interval in the front-rear direction, and the refrigerant tube groups (58) are arranged side by side in a left-right direction.
2. An evaporator according to claim 1 wherein the flat tube (17) is formed by a platelike left component (21) having a left wall forming portion (23) and a platelike right component (22) having a right wall forming portion (28), and each of the front and rear walls (13,14) of the flat tube (17) comprises at least one of a rightward projecting wall (24) projecting rightward from each of front and rear side edges of the left component (21) integrally therewith and brazed to the right component and a leftward projecting wall (29) projecting leftward from each of front and rear side edges of the right component (22) integrally therewith and brazed to the left component (21), each of the reinforcing walls (15) of the flat tube (17) comprising a reinforcing wall forming portion (25) projecting inward from at least one of

the left wall forming portion (23) of the left component (21) and the right wall forming portion (28) of the right component (22) integrally therewith and having an outer end brazed to the other wall forming portion.

3. An evaporator according to claim 2 wherein the reinforcing walls (15) are formed with a plurality of communication holes (19) for causing the parallel refrigerant channels (16) to communicate with one another. 10
4. An evaporator according to claim 3 wherein the communication holes (19) are in a staggered arrangement when seen from the left. 15
5. An evaporator according to claim 3 or 4 wherein each of the reinforcing walls (15) is 10 to 40 % in opening ratio which is the ratio of all the communication holes (19) in the reinforcing wall to the reinforcing wall (15). 20

Patentansprüche

1. Verdampfer (55), mit einer einzigen Verdampfereinheit (55A) mit einem Paar von Sammelrohren (56,57), die übereinander parallel und voneinander beabstandet angeordnet sind, und parallelen Kühlmittel-Rohren (4), deren Breite in der Richtung von vorn nach hinten ausgerichtet ist und deren gegenüberliegende Enden mit den jeweiligen Sammelrohren (56,57) verbunden sind, wobei jedes der Kühlmittel-Rohre (4) die Form eines flachen Rohrs (17) aufweist, mit flachen linken und rechten Wänden (11, 12), vorderen und hinteren Wänden (13,14), die zwischen den vorderen und hinteren Seitenkanten der linken und rechten Wände (11,12) angeordnet und mit diesen verbunden sind, und einer Anzahl von Verstärkungswänden (15), die zwischen den linken und rechten Wänden (11,12) angeordnet und mit diesen verbunden sind und sich in deren Längsrichtung erstrecken, welche Verstärkungswände (15) in einem vorbestimmten Abstand zwischen den vorderen und hinteren Wänden (13,14) angeordnet sind, wobei das flache Rohr (17) parallele Kühlmittel-Kanäle (16) in seinem Inneren aufweist und aus zwei Metallplatten (21,22) gebildet wird, und jede der Verstärkungswände (15) einen eine Verstärkungswand bildenden Bereich (25) aufweist, der nach innen von einer (21) der Metallplatten vorspringt und einstückig mit dieser ausgeformt ist, **dadurch gekennzeichnet, dass** die Verdampfereinheit (55A) eine Anzahl von Kühlmittelrohr-Gruppen (58) aufweist, von denen jede eine Anzahl von Kühlmittel-Rohren (4) umfaßt, die in einem Abstand in der Richtung von vorn nach hinten angeordnet sind, welche Kühlmittelrohr-Gruppen 25

(58) nebeneinander in einer Richtung von links nach rechts angeordnet sind.

2. Verdampfer gemäß Anspruch 1, bei welchem das flache Rohr (17) durch ein plattenartiges linkes Bauteil (21) mit einem linken wandbildenden Bereich (23) und ein plattenartiges rechtes Bauteil (22) mit einem rechten wandbildenden Bereich (28) gebildet wird, und jede der vorderen und hinteren Wände (13,14) des flachen Rohrs (17) entweder eine nach rechts vorspringende Wand (24) umfaßt, die nach rechts von jeder der vorderen und hinteren Seitenkanten des linken Bauteils (21) vorspringt und einteilig mit diesem ausgebildet ist und an das rechte Bauteil angelötet ist, oder eine nach links vorspringende Wand (29), die nach links von jeder der vorderen und hinteren Seitenkanten des rechten Bauteils (22) vorspringt und einteilig mit diesem ausgebildet ist und an das linke Bauteil (21) angelötet ist, wobei die Verstärkungswände (15) des flachen Rohrs (17) einen eine Verstärkungswand bildenden Bereich (25) umfassen, der nach innen entweder vom linken wandbildenden Bereich (23) des linken Bauteils (21) oder dem rechten wandbildenden Bereich (28) des rechten Bauteils (22) vorspringt, einteilig mit diesem ausgebildet ist und ein äußeres Ende aufweist, das mit dem anderen wandbildenden Bereich verlötet ist. 30
3. Verdampfer gemäß Anspruch 2, bei dem die Verstärkungswände (15) mit einer Anzahl von Verbindungslöchern (19) versehen sind, durch welche die parallelen Kühlmittel-Kanäle (16) miteinander in Verbindung stehen. 35
4. Verdampfer gemäß Anspruch 3, bei dem die Verbindungslöcher (19) von links betrachtet versetzt angeordnet sind. 40
5. Verdampfer gemäß Anspruch 3 oder 4, bei dem jede der Verstärkungswände (15) ein Öffnungsverhältnis von 10 bis 40 % aufweist, welches das Verhältnis aller Verbindungslöcher (19) in der Verstärkungswand zur Verstärkungswand (15) darstellt. 45

Revendications

1. Evaporateur (55) comprenant une unité d'évaporateur unique (55A) comprenant deux collecteurs (56, 57) disposés parallèlement et à distance l'un au dessus de l'autre, et des tubes à réfrigérant parallèles (4) ayant une largeur orientée dans une direction avant - arrière et des extrémités opposées reliées aux collecteurs (56, 57) respectifs, chacun des tubes à réfrigérant (4) se présentant sous la forme d'un tube plat (17) comprenant des parois gauche et droite (11, 12) plates, des parois avant et arrière 50

(13, 14) positionnées entre les bords latéraux avant et arrière des parois gauche et droite (11, 12) et reliées à ceux-ci, et plusieurs parois de renforcement (15) positionnées entre les parois gauche et droite (11, 12), reliées à celles-ci et s'étendant longitudinalement par rapport à elles, les parois de renforcement (15) étant disposées à un intervalle prédéterminé entre les parois avant et arrière (13, 14), le tube plat (17) renfermant des canaux à réfrigérant parallèles (16) et étant formé à partir de deux plaques métalliques (21, 22), chacune des parois de renforcement (15) comprenant une partie (25) formant paroi de renforcement, faisant saillie vers l'intérieur à partir de l'une (21) des plaques métalliques en étant solidaire de celle-ci, **caractérisé en ce que** l'unité d'évaporateur (55A) comprend plusieurs groupes de tubes à réfrigérant (58) comprenant chacun plusieurs tubes à réfrigérant (4) espacés dans la direction avant - arrière, les groupes de tubes à réfrigérant (58) étant disposés côte à côte dans une direction gauche - droite.

quel chacune des parois de renforcement (15) présente un rapport d'ouverture de 10 à 40%, qui est le rapport de tous les trous de communication (19) de la paroi de renforcement sur la paroi de renforcement (15).

2. Evaporateur selon la revendication 1, dans lequel le tube plat (17) est formé par un élément gauche en forme de plaque (21) ayant une partie (23) formant paroi gauche et un élément droit en forme de plaque (22) ayant une partie (28) formant paroi droite, et chacune des parois avant et arrière (13, 14) du tube plat (17) comprend l'une au moins d'une paroi (24) faisant saillie vers la droite, en saillie vers la droite à partir de chacun des bords latéraux avant et arrière de l'élément gauche (21) en étant solidaire de celui-ci et brasée sur l'élément droit, et d'une paroi (29) en saillie vers la gauche, faisant saillie vers la gauche à partir de chacun des bords latéraux avant et arrière de l'élément droit (22) en étant solidaire de celui-ci et brasée sur l'élément gauche (21), chacune des parois de renforcement (15) du tube plat (17) comprenant une partie (25) formant paroi de renforcement faisant saillie vers l'intérieur à partir de l'une au moins de la partie (23) formant paroi gauche de l'élément gauche (21) et de la partie (28) formant paroi droite de l'élément droit (22) en étant solidaire de celui-ci et ayant une extrémité extérieure brasée sur l'autre partie formant paroi.
3. Evaporateur selon la revendication 2, dans lequel les parois de renforcement (15) sont pourvues de plusieurs trous de communication (19) destinés à obliger les canaux à réfrigérant parallèles (16) à communiquer entre eux.
4. Evaporateur selon la revendication 3, dans lequel les trous de communication (19) sont disposés en quinconce lorsqu'on les regarde depuis le côté gauche.
5. Evaporateur selon la revendication 3 ou 4, dans le-

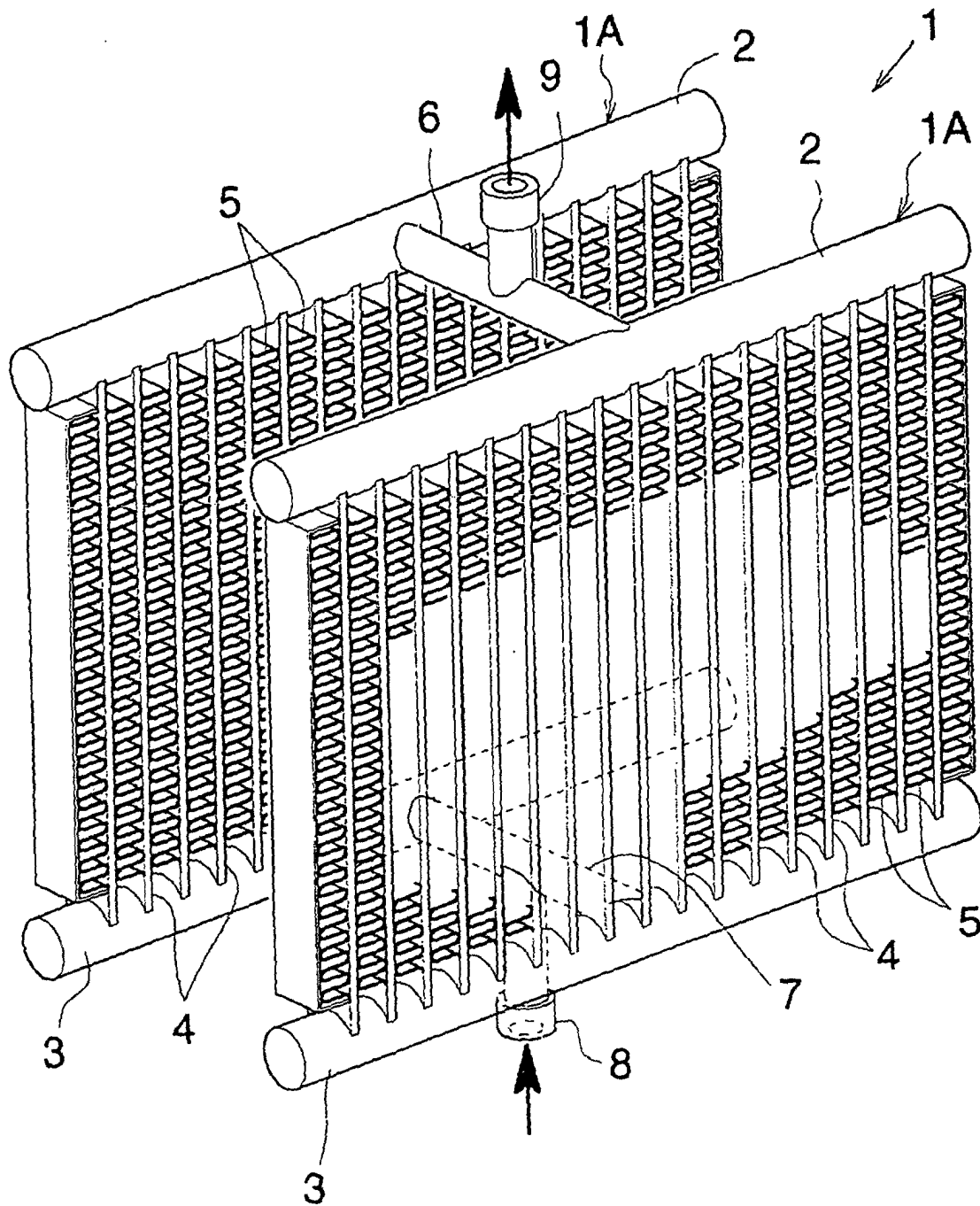


FIG.1

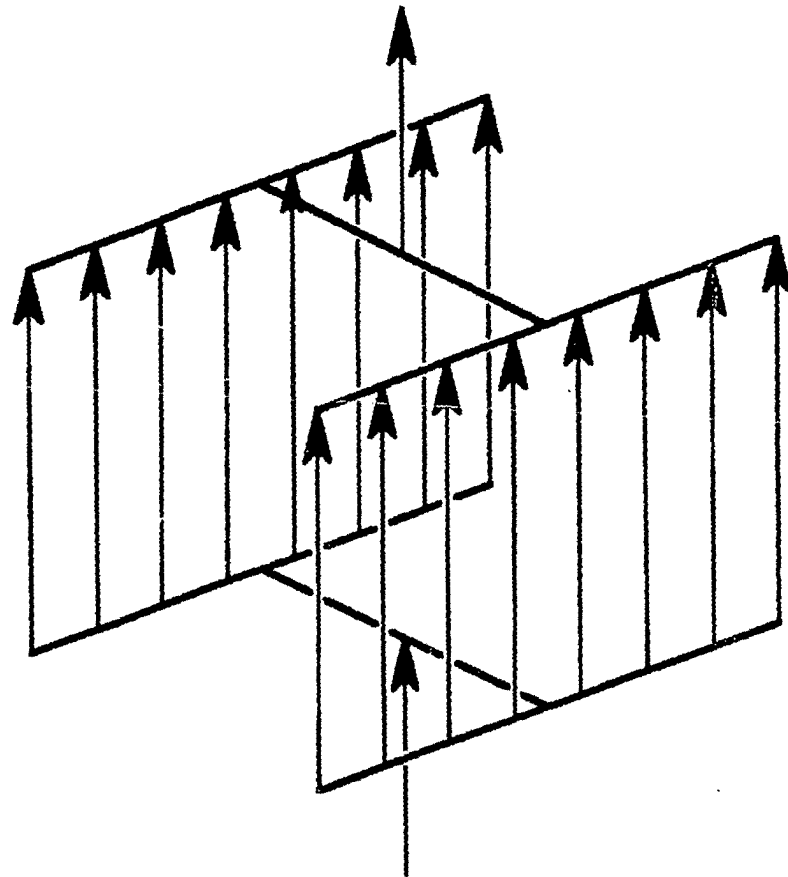


FIG.2

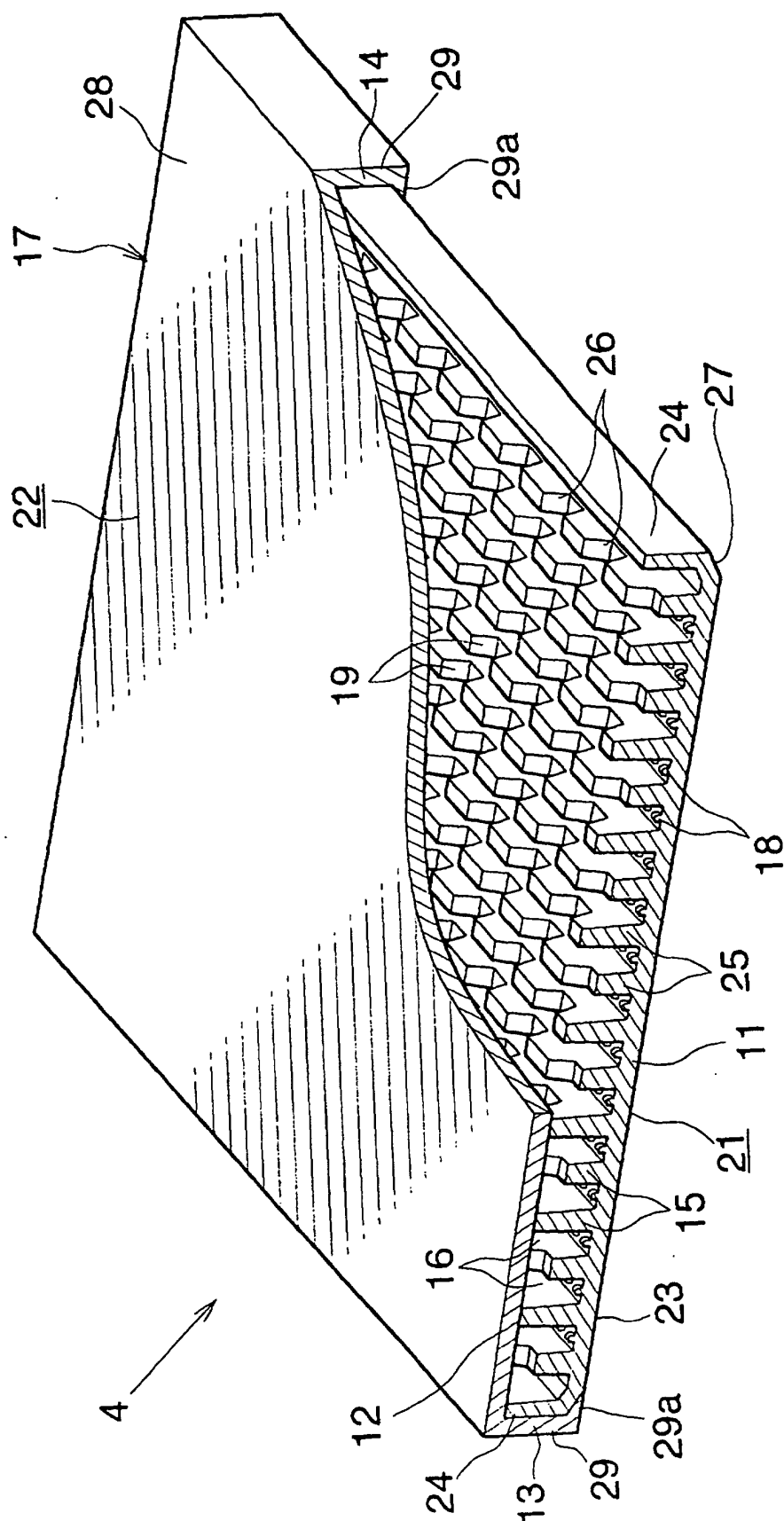


FIG. 3

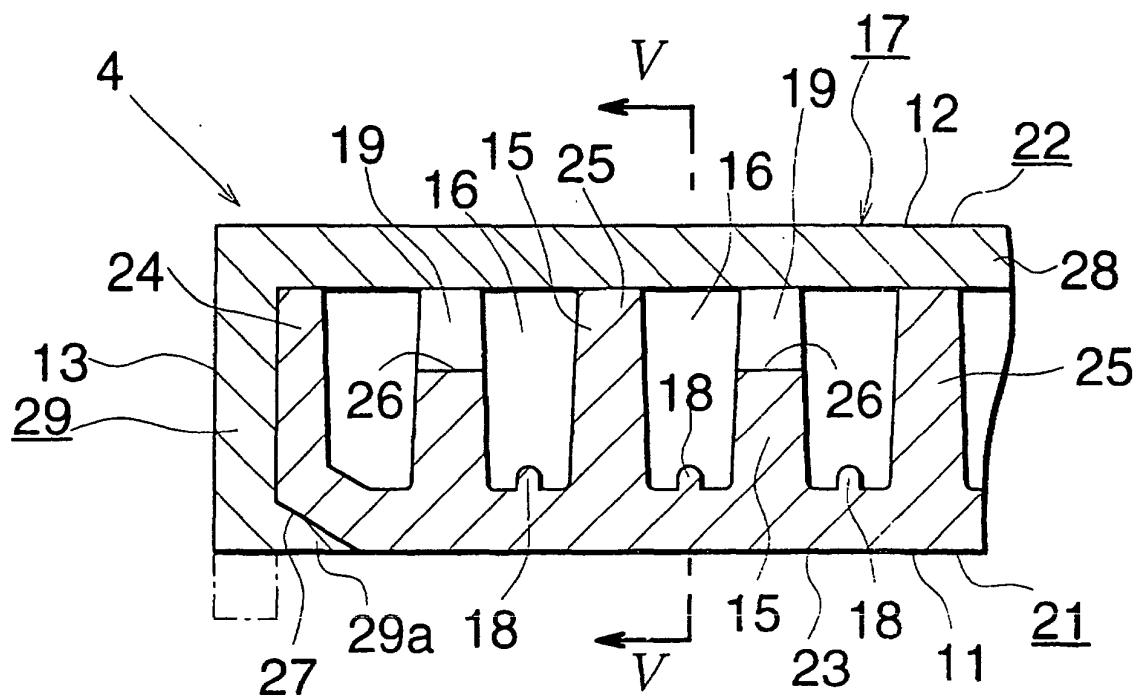


FIG. 4

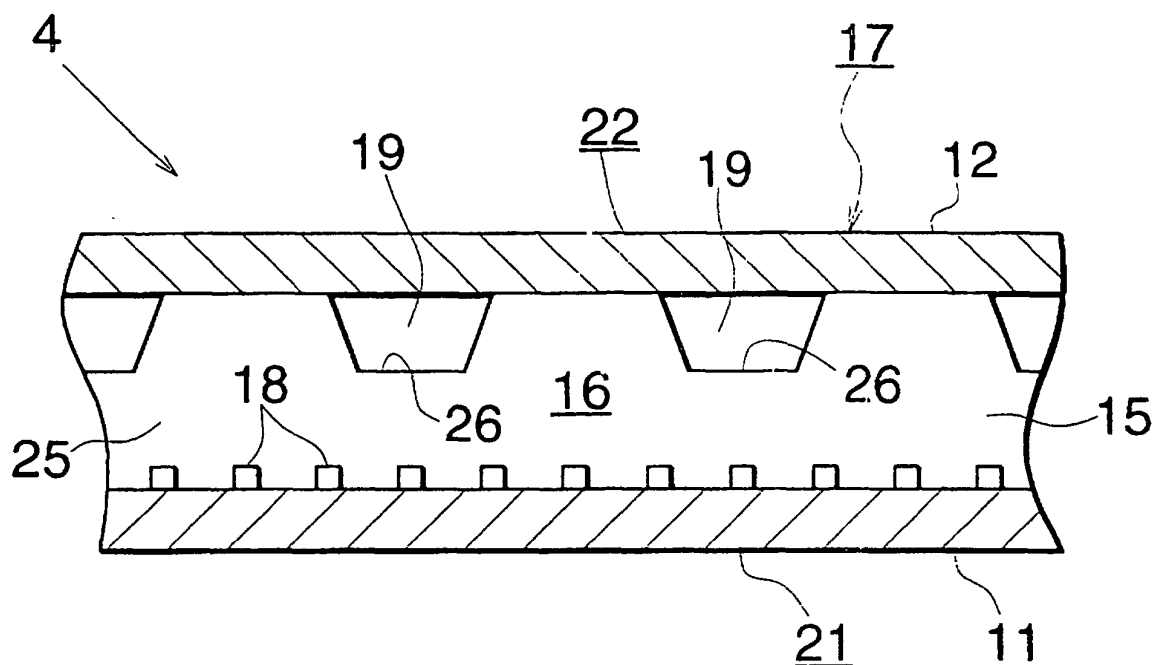
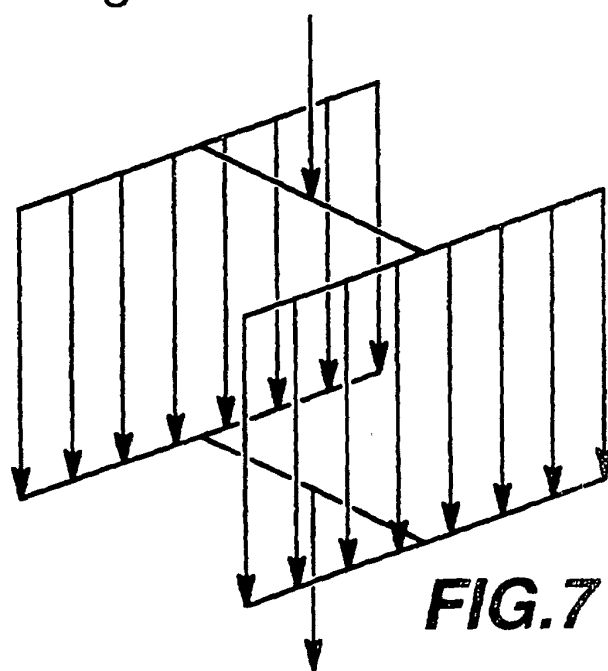
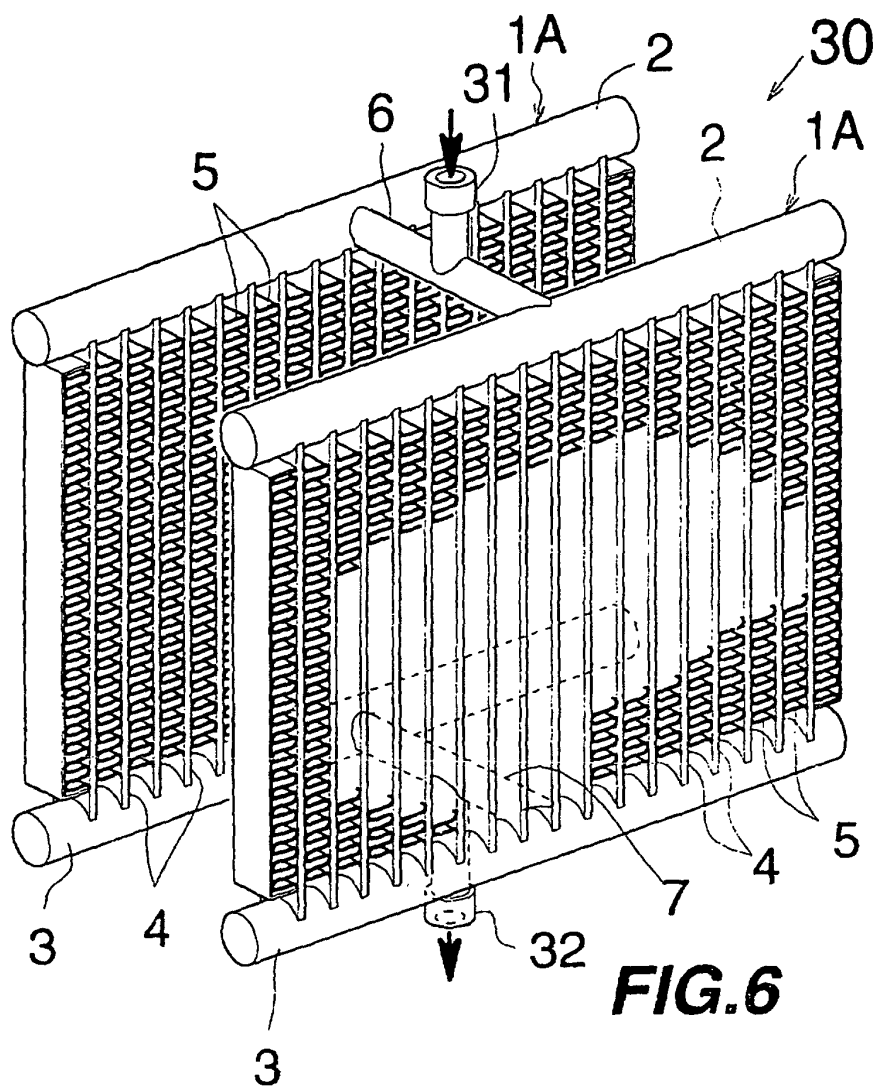
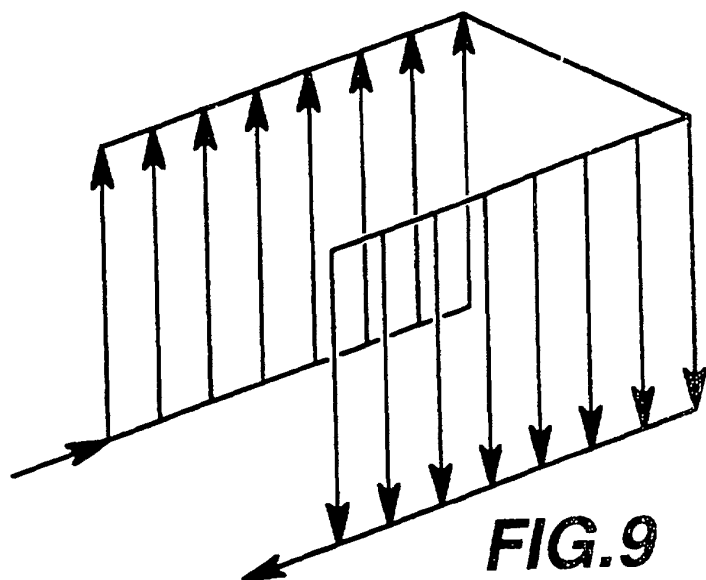
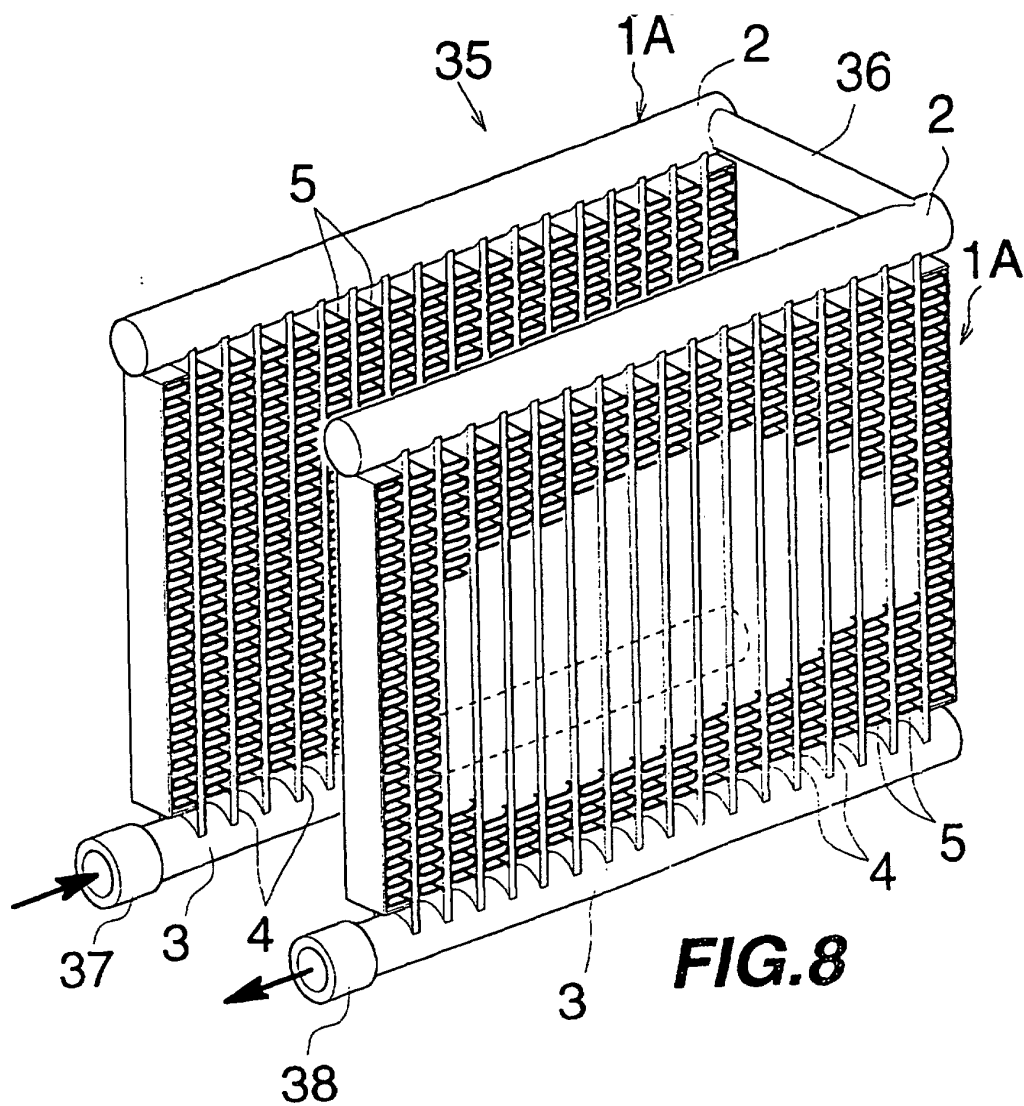
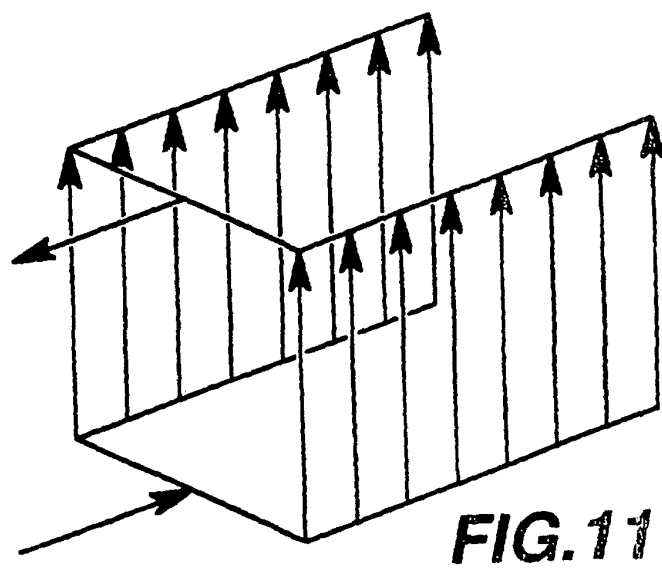
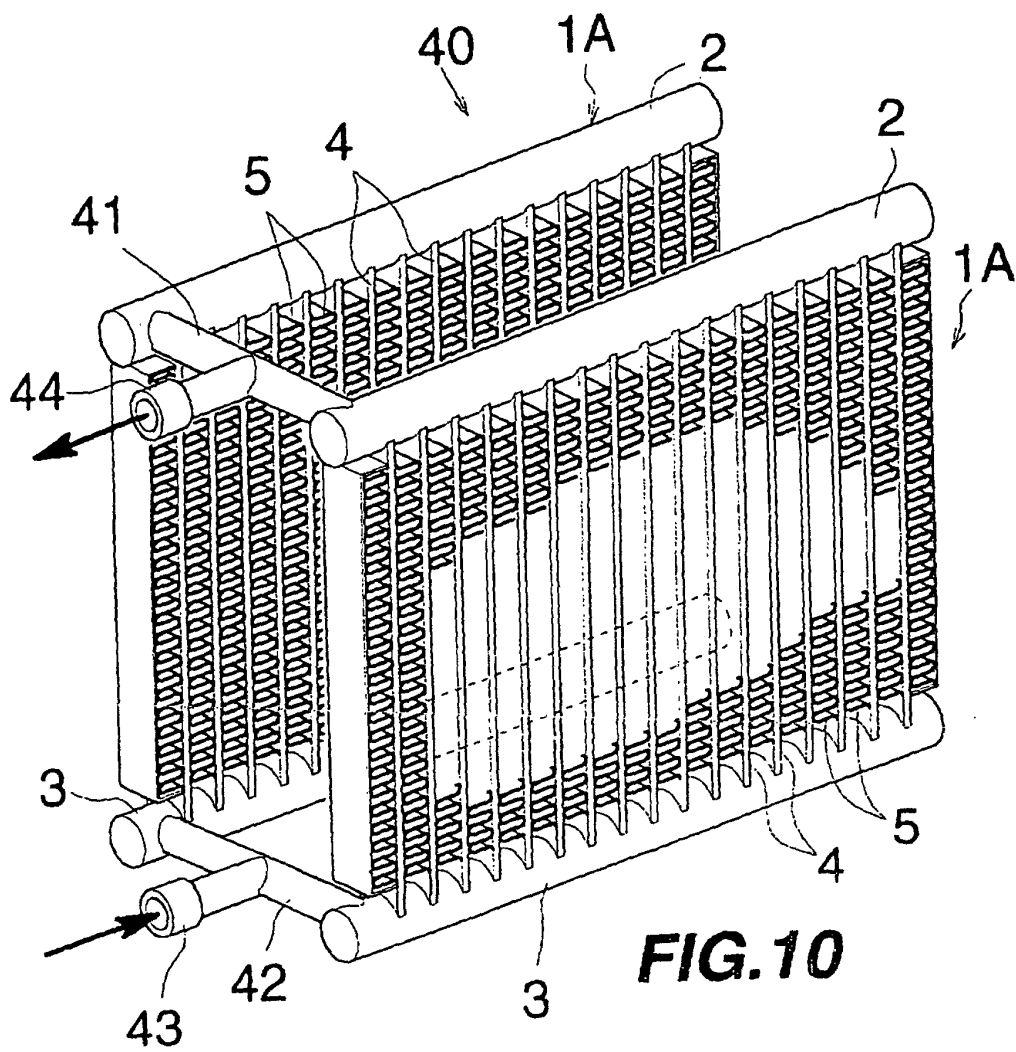
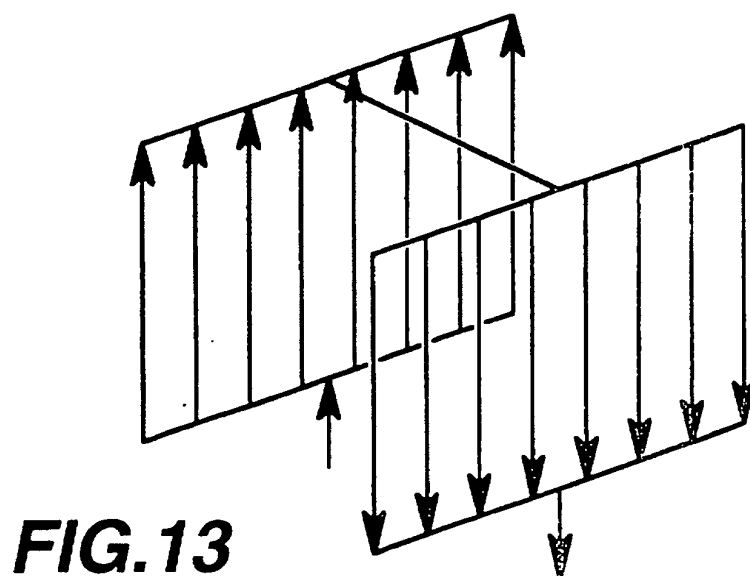
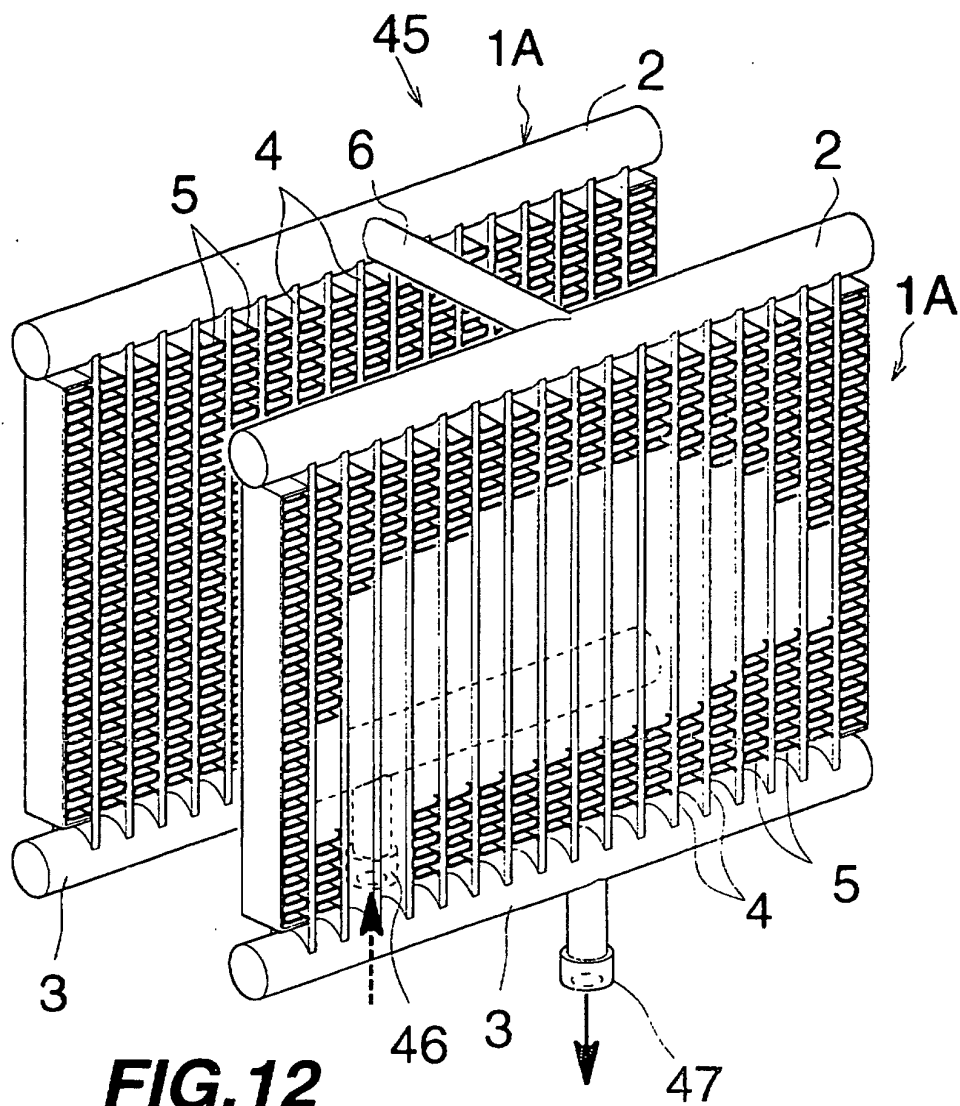


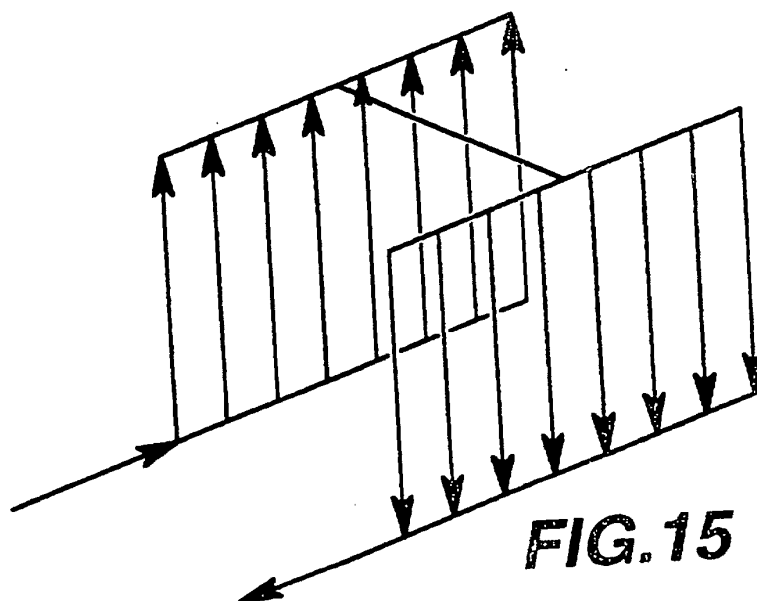
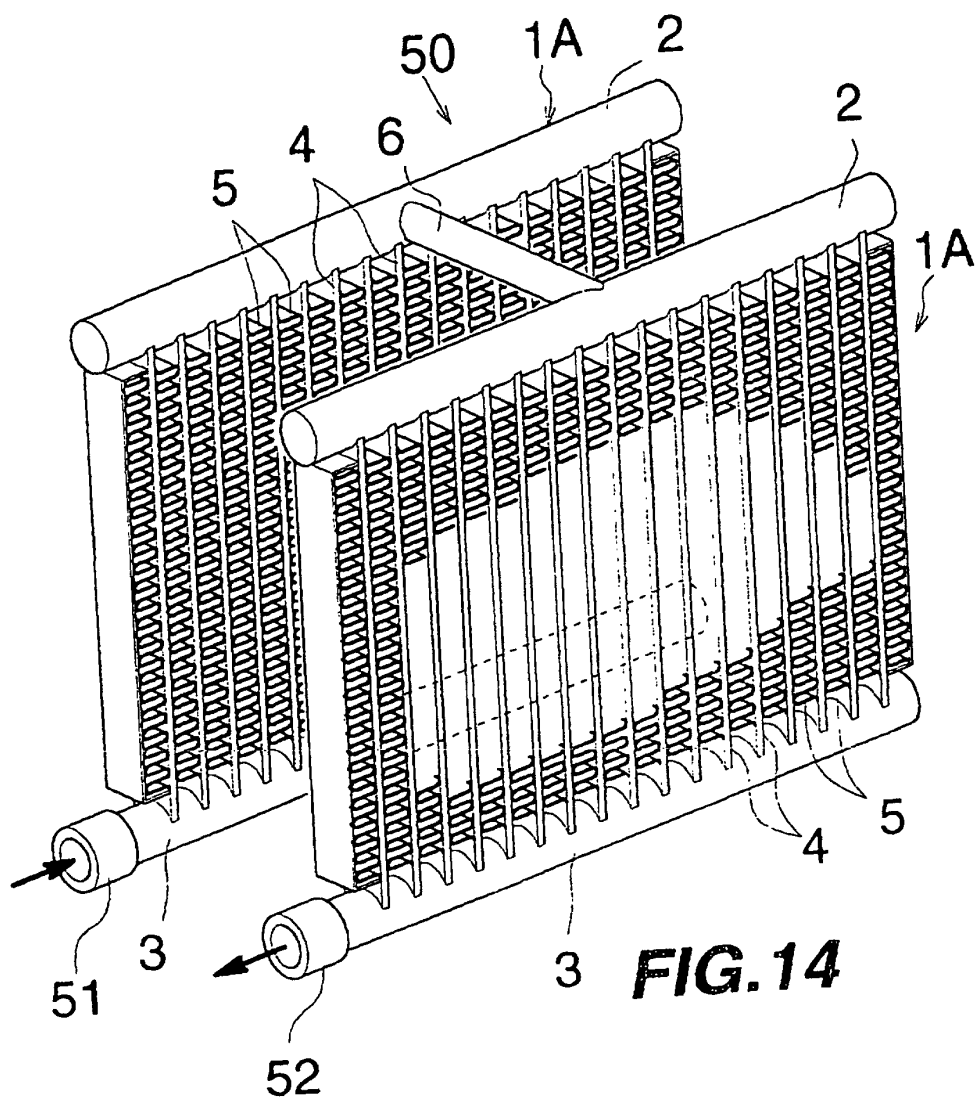
FIG. 5











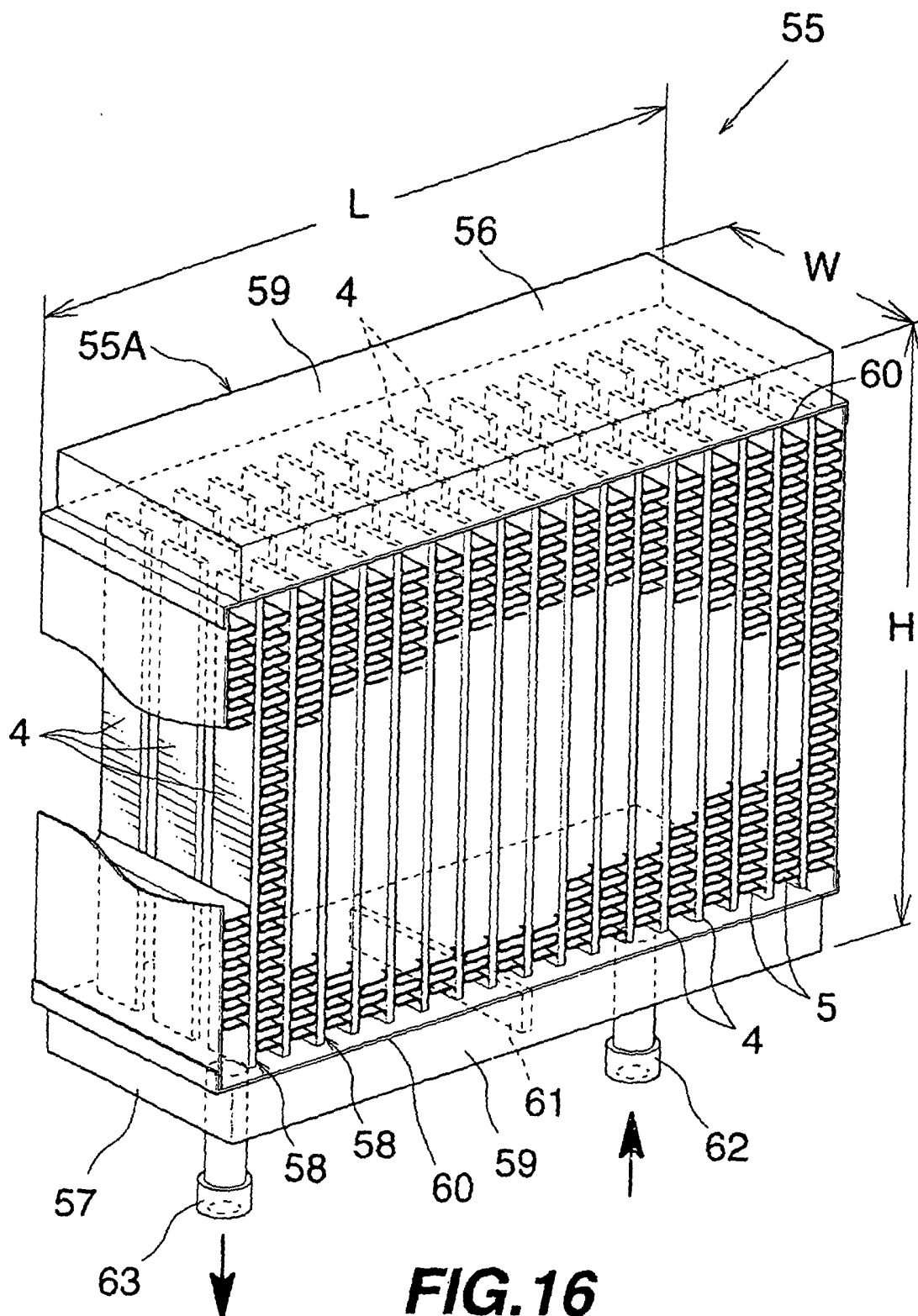


FIG. 16

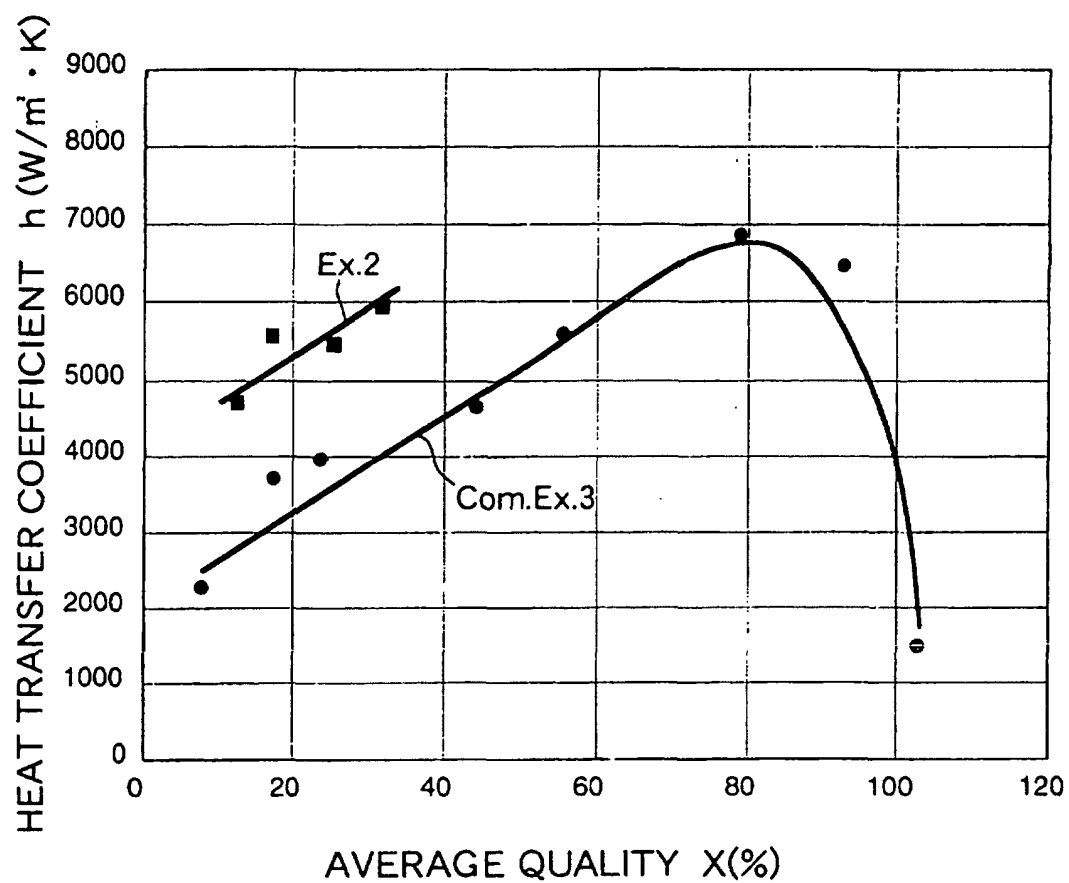


FIG.17

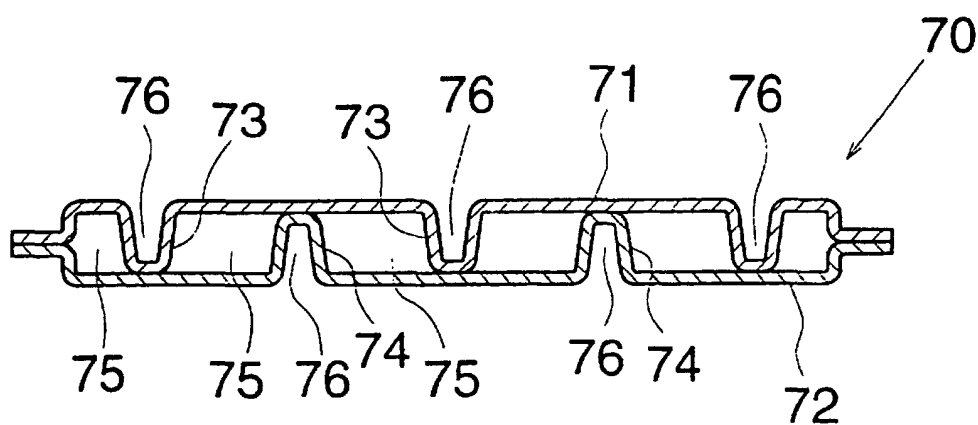


FIG.18

PRIOR ART