

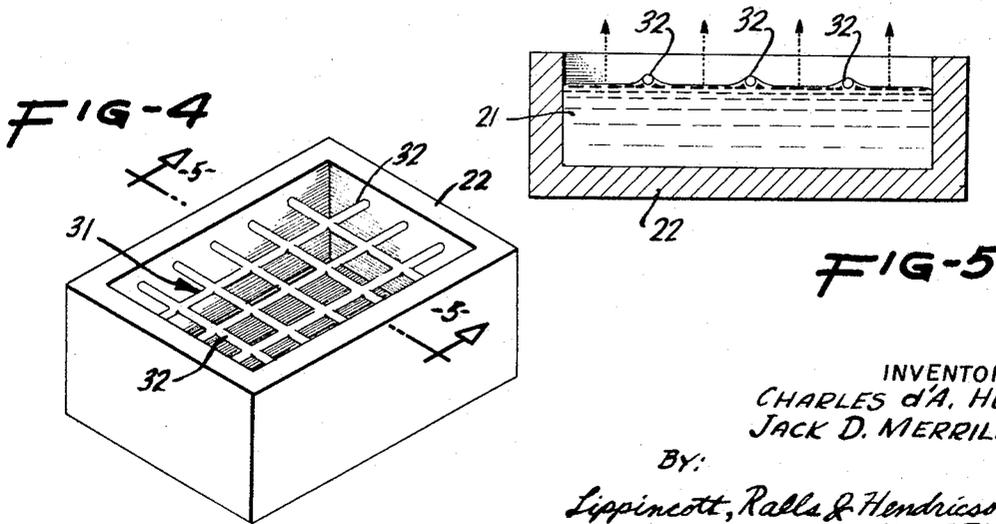
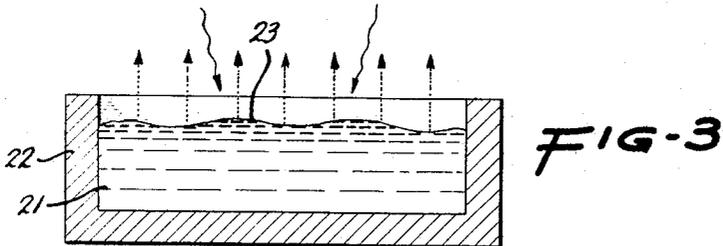
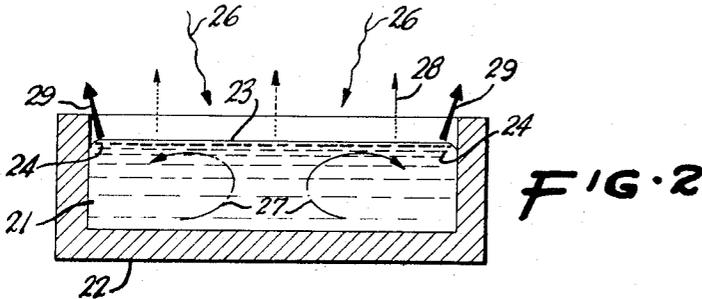
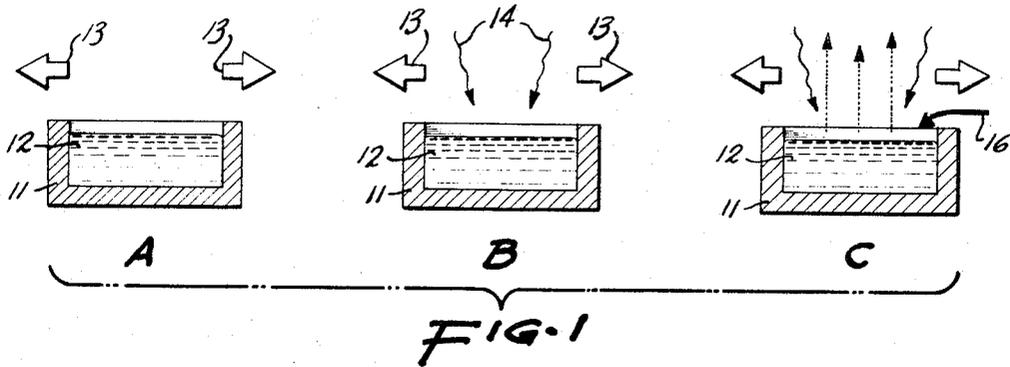
July 11, 1967

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3,330,647

PREVENTION OF SPLATTERING DURING VAPORIZATION PROCESSING

Filed June 18, 1963



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3,330,647

## PREVENTION OF SPLATTERING DURING VAPORIZATION PROCESSING

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 Filed June 18, 1963, Ser. No. 288,822  
 6 Claims. (Cl. 75-93)

The present invention relates to the prevention of splat-  
 tering during the vacuum evaporation of materials and  
 is particularly useful in connection with very rapid rates  
 of vaporization.

In vacuum evaporation processing it has been observed  
 that a substantial amount of explosive vaporization or  
 splatting is often experienced. In all instances this splat-  
 tering is undesirable, and in many circumstances it is  
 wholly unacceptable. Observation shows that the amount  
 of splatting increases with increasing vaporization  
 rates, and this has actually precluded the utilization of  
 vacuum vaporization in many commercial applications.  
 The problem of splatting, which is present even at low  
 vaporization rates and which is magnified at higher vapor-  
 ization rates, is overcome by the present invention.

Although the present invention is applicable to improve  
 all vacuum vaporization processes, it is primarily im-  
 portant in the vacuum vaporization of metals or metal  
 alloys having low or intermediate melting temperatures.  
 For most materials, such as metals, the surface tension  
 thereof is appreciable at vaporization temperatures and  
 this causes explosive vaporization from points of decreased  
 surface tension, such as may be provided by slag or im-  
 purities floating upon the surface of the molten material,  
 or the meniscus about the edge of same. In accordance  
 with the present invention, it is provided that the surface  
 tension of at least a substantial area of a molten pool  
 of material to be vaporized is reduced in the manner and  
 for the purposes set forth below.

The present invention is illustrated and described as  
 to the method and apparatus thereof in the accompany-  
 ing drawings, wherein:

FIGURE 1 schematically illustrates at A, B, C, thereof  
 successive steps in the method of the present invention;

FIGURE 2 is a sectional view of a container filled  
 with a molten material undergoing conventional vacuum  
 vaporization;

FIGURE 3 is a sectional view similar to FIGURE 2,  
 and illustrating one solution to the problem of splatting  
 as provided by the present invention;

FIGURE 4 is a perspective view of a crucible adapted  
 to contain material for vacuum vaporization, and illus-  
 trating one embodiment of the apparatus of this inven-  
 tion; and

FIGURE 5 is a sectional view taken in the plane 5-5  
 of FIGURE 4.

Careful consideration of the phenomena of explosive  
 vaporization or splatting of droplets from a molten pool  
 of material, such as metal, during vacuum evaporation,  
 shows that this splatting occurs from particular points  
 upon the pool surface. In the presence of floating impuri-  
 ties upon the pool, it is found that splatting occurs  
 about these impurities atop the pool. In the instance of  
 vacuum evaporation of extremely pure metal, for exam-  
 ple, it is found that splatting occurs from the meniscus  
 at the pool edges. It may be postulated that in the ap-  
 plication of heat to a molten pool of material for evapora-  
 tion of such material, there is unavoidably produced a  
 superheating of at least some portions of the molten ma-  
 terial. Convection currents in the molten material move  
 these superheated molecules about in the pool, and they  
 preferentially depart from the pool surface at points of

lowest surface tension. Under the circumstance wherein  
 very pure material is being operated upon so that no float-  
 ing impurities are present upon the pool thereof, it is  
 found that this explosive vaporization then occurs at the  
 curved pool surface formed by the meniscus between the  
 molten material and the container. It is provided by the  
 present invention that splatting of vacuum vaporized  
 material shall be prevented by lowering of the surface  
 tension of a substantial area of a molten pool of material  
 being vaporized. This lowering of the surface tension over  
 a substantial area of the pool is herein accomplished by  
 additions to the pool. In the instance of metal vaporiza-  
 tion, there is added to the pool a dissimilar metal, i.e.,  
 one which does not have substantially the same charac-  
 teristics. In particular, this dissimilar metal has a sub-  
 stantially different surface tension than the material be-  
 ing evaporated. As a further limitation upon the material  
 added to the pool, it is necessary for such added materi-  
 al to have a very low vapor pressure in comparison to  
 the pool material in the percentage of material added  
 thereto. It will be appreciated, of course, that combina-  
 tions of material may be evaporated, if this is the desire;  
 however, under most circumstances it is not intended to  
 evaporate any appreciable amount of the added material.

Referring to FIGURE 1, there is illustrated at A there-  
 of, a crucible 11 containing a material 12 that is to be  
 vacuum evaporated. Evacuation of the volume above the  
 material 12 is indicated by the block arrows 13. Heat is  
 applied to the material 12, as indicated by the arrows  
 14 in FIGURE 1B, so as to thereby melt this material  
 12. It has been found that advantageous heating for melt-  
 ing and vaporization may be accomplished by the utiliza-  
 tion of bombarding electron beams directed onto the upper  
 surface of the pool. In accordance with the present inven-  
 tion, there is added to the molten material 12 an addi-  
 tional and dissimilar material, as indicated by the arrow  
 16 in FIGURE 1C. With regard to the identity of the  
 added material, it is provided hereby that there shall be  
 employed an additive material that reduces the surface  
 tension of at least a substantial area of the molten pool.  
 The material added may either dissolve in the molten  
 material of the pool to thereby form an alloy therewith,  
 or, alternatively, may remain in solid form but disposed  
 so as to deform the upper pool surface. At any rate, the  
 added material should be substantially dissimilar to the  
 material in the pool, and should have a low vapor pres-  
 sure at the evaporation temperature of the pool material,  
 at least in the concentration of additive material em-  
 ployed. Particular examples of suitable additive materials  
 are set forth below.

Considering further the present invention, reference is  
 made to FIGURE 2, wherein there is illustrated a molten  
 pool 21 of metal, such as copper or the like, contained  
 within a crucible 22. It will be seen that the upper sur-  
 face 23 of this pool 21 is generally planar under normal  
 circumstances, but at the edges thereof there is formed a  
 curved pool surface defining a meniscus 24. This curva-  
 ture may, of course, extend either upwardly or downward-  
 ly, depending upon the relative properties of the material  
 of the crucible and the metal of the pool. If the molten  
 pool of material or metal wets the crucible material, as  
 in the case of molten copper contained within a tungsten  
 crucible, the meniscus will curve upward, contrary to the  
 showing of FIGURE 2. Application of heat to the pool as,  
 for example, by electron beam bombardment or some  
 other suitable manner, as schematically illustrated by the  
 wavy arrows 26, unavoidably causes a certain amount of  
 superheating of molten metal. There are established with-  
 in the pool certain convection currents, as indicated by  
 the light arrows 27 within the pool, which serve then to  
 generally move superheated metal outwardly of the pool

under the circumstances wherein heating is accomplished as indicated, and this superheated metal is released at the meniscus of the pool surface. The curvature of the pool surface at the meniscus 24 provides a reduced surface tension area as the surface tension of a liquid is minimized at a region of curvature of the liquid. In the vaporization of metal from a liquid pool thereof, there is unavoidably present some limited areas of reduced surface tension upon the pool surface, for some type of meniscus must be present. With a very limited area of decreased surface tension, there is then produced an explosive evaporation of superheated metal from this limited area, so as to splatter droplets of molten metal from the pool. Normal vaporization of the metal is indicated by the dotted arrows 28 and the heavy arrows 29 indicate splattering from the meniscus.

As briefly noted above, this splattering is highly disadvantageous in many applications, and in particular, it has been found to almost preclude the utilization of vacuum vaporization processes with certain metals. The foregoing is particularly true when extremely pure metals are being operated upon to produce high-quality vapor-deposited films. In FIGURE 3, there is illustrated a manner of overcoming the difficulty discussed above in connection with FIGURE 2. In accordance with the present invention, there is provided in FIGURE 3 for the disturbing of the upper pool surface 23, so as to thereby produce curves thereon, and consequently to establish a plurality of areas of reduced surface tension. By the provision, in accordance herewith, of a sufficient area of reduced surface tension, the superheated material within the pool then readily escapes therefrom without concentration at minute areas and does then not explosively release from the pool to cause splattering.

One form of apparatus suitable for disturbing the upper pool surface to prevent splattering is illustrated in FIGURES 4 and 5. As shown therein, a grid 31 is disposed within the crucible 22. This grid may be stamped from a sheet of material or formed of rods or wires joined together. The individual elements or portions 32 of grid 31 are comprised of high-temperature metals, at least with respect to the evaporation temperature of material to be evaporated from the crucible. In this instance, and in accordance with the method of the present invention, the additive material is comprised of the grid itself. Under these circumstances, wherein the additive metal or material remains as a solid within the pool, it is necessary for this material to be disposed substantially at and, in fact, slightly above the upper pool surface. In this manner of carrying out the present invention, the added metal must not only have the above-identified properties, but in addition, must be capable of being "wetted" by the molten material of the pool. The grid 31 is disposed above the upper surface of the molten material of the pool so that it touches this upper surface and, consequently, the pool surface curves up and over the grid.

As an example of the present invention, in accordance with the above-described manner of carrying out same, there may be utilized a tantalum or molybdenum grid with a molten pool of copper evaporant. This grid may, for example, be stamped or otherwise formed of a tantalum sheet, for example. The grid is immersed in the molten copper and the level of the molten copper is then adjusted to be disposed slightly below the top of the grid. Inasmuch as copper wets tantalum, there thus appears from the top of the crucible a complete copper surface, but with a pattern of disturbed surface tension wherever the grid provides a curvature of the copper surface. It is particularly noted that both tantalum and molybdenum, identified above as suitable materials for the grid in this instance, are essentially insoluble in molten copper, and furthermore have a very low vaporization rate at the temperature of a molten copper pool. In one instance of operation of the present invention, the grid was disposed no more than  $\frac{1}{4}$ " above the free horizontal surface of molten copper

in the pool, so that the copper entirely covered the grid to form a plurality of curved surfaces atop of the pool. Vaporization of the copper at copper vapor pressures of about 5-10 mm. of mercury at the pool surface produced no observable splatter of the copper.

This manner of carrying out the present invention requires relatively careful location of the pool surface relative to the grid. If the grid becomes unduly exposed above the surface of the molten material in the pool, a bombarding electron beam utilized to vaporize the material, will actually melt the upper surface of the grid and splatter will occur. On the other hand, if the grid is entirely submerged in the pool so that there is no observable ripple upon the pool surface, it is found that the grid has substantially no effect in eliminating splatter. There is thus provided by the present invention for the addition to a molten pool of material being vaporized of a partially submerged grid of insoluble material that is wet by the molten evaporant in order to thereby substantially entirely preclude explosive evaporation. The foregoing example of the present invention relating to the evaporation of copper is noted to be particularly significant, inasmuch as prior art attempts to evaporate copper at commercially feasible rates have proven wholly unsatisfactory because of the problem of splattering. This same problem appears to be of minimal importance in the evaporation of aluminum, and it may be postulated that splattering of aluminum is inherently minimized because of the exceptionally low surface tension of aluminum at temperatures required for substantial evaporation rates. Apparently, aluminum does not superheat to any great extent because of the inherent relationship between normal surface tension and vapor pressure as functions of temperature. It is furthermore noted that in the vacuum evaporation of so-called "high temperature" metals, the problem of splattering does not appear particularly significant, possibly because of radiation losses from the molten pool at the temperatures required for vaporization. In the vapor deposition of copper, for example, heat is released from the molten pool by conduction, convection and evaporation, while at higher temperatures these same effects are present with the addition of radiation losses. Investigation has indicated that vaporization processes proceeding at a temperature of 3000° F. or lower, are particularly susceptible to the problems overcome by this invention, inasmuch as substantial superheat apparently occurs because of the minimization of radiation losses. The present invention, as described above, overcomes the problem of splattering by providing a sufficient area of low surface tension for the steady release of superheat without explosive evaporation, as would otherwise occur.

It is additionally provided by this invention that splattering may be eliminated through the addition of a material which dissolves in and, in fact, alloys with the molten material of the pool, i.e., the evaporant. The properties of this added material are those set forth above, i.e., such material shall be substantially dissimilar to the material being evaporated, and furthermore shall have a very small evaporation rate at the process temperature. With regard to this latter limitation, it is noted that the critical evaporation rate is that of the material in the proportion employed. The process hereof requires only the addition of very minute amounts of alloying materials which dissolve in the evaporant and, for example, 1 to 10% of additive material may be employed. With regard to the degree of dissimilarity between the evaporant and the added material, it is noted that the effect upon surface tension increases with increasing dissimilarities between the materials. As a general proposition, and speaking only of pure metals at this point, all alloys have lower surface tensions than do the constituents of the alloys. The addition of tantalum to columbium could be expected to produce but very little difference in surface tension, inasmuch as these two metals are quite similar, while the addition

of zirconium to beryllium or copper produces a very marked difference in surface tension.

The present invention thus provides, in addition to the previously described manner of prevention splatter, for the addition to the molten evaporant of a dissimilar material which dissolves in the evaporant. This added material, in the proportion employed has a very low vapor pressure at the process temperature. As an example of the foregoing, a small amount of zirconium was added to a molten pool of copper heated to establish a suitable vapor pressure thereof for vapor processing. This addition provided a material reduction in the surface tension of the molten pool, and was observed to prevent splattering of the copper. As regards further examples of the present invention, either tungsten or tantalum in a very small proportion may be added to a molten pool of iron to prevent splattering of the iron during vaporization. In the evaporation of zirconium, a tungsten additive may be utilized to prevent splattering. With tungsten added to zirconium evaporant in an amount of 5% of the zirconium, there is produced a zirconium vapor containing about ten parts per million of tungsten. Under most circumstances this minute contamination of the vapor is not critical and does not limit its utilization. In each of the foregoing examples the additive material will be seen to dissolve in the evaporant and to have a very low vapor pressure in the proportion added.

Although, as noted above, the present invention is particularly advantageous in the prevention of splattering during vapor processing on a commercial scale, it is also advantageous in precluding splattering at lower vaporization rates. In this respect it may be considered that vapor pressure of the order of 0.1 mm. of mercury of the evaporant provides a low evaporation rate, a vaporization pressure of about 1 mm. of mercury is representative of a generally typical evaporation rate, and a vapor pressure of 10 mm. of mercury provides a commercially feasible evaporation rate for very large-scale operations. In all of the foregoing situations, the present invention provides a material advancement in the art. Inasmuch as the surface tension of pure metals is substantial at the melting point thereof, it is highly important that means be provided for the release of superheat from a molten pool of this material during evaporation. Of the common metals, only aluminum appears to have such a low vapor pressure in the temperature range of substantial surface tension that the problem of superheat at high vaporization rates does not occur. Even in the instance of aluminum, however, there may be particular circumstances wherein reduction in the surface tension thereof, in accordance herewith, will be found to be advantageous.

There has been described above particular preferred steps of the process of this invention together with preferred apparatus in accordance herewith. It is believed to be clear that the present invention provides a marked and important advancement in the art which substantially extends the utility and applicability of vacuum vaporization. It is not intended to limit the present invention by the terms of the foregoing description but instead reference is made to the appended claims for a precise delineation of the present invention.

What is claimed is:

1. An improved vacuum vaporization method for vaporizing a metal from the surface of a molten pool of significant depth comprising, heating a metal to be vaporized within a crucible with an electron beam to form a molten pool, said crucible including an open topped container having a plurality of rod-like members extending at least partially across the open top of the crucible in a generally horizontal plane, said rod-like members being formed from a metal having a negligible vaporization rate at the condition necessary for vaporization of said metal and having the characteristic of being wet by said

metal, heating the surface of the molten pool to vaporize said metal, and controlling the level of the molten pool within the crucible so that the surface of the molten pool lies just below the upper surface of said rod-like members, whereby the metal may be rapidly vaporized from the areas of reduced surface tension adjacent the rod-like members.

2. An improved vacuum vaporization method for vaporizing a metal from the surface of a molten pool of significant depth comprising, heating a metal to be vaporized within a crucible with an electron beam to form a molten pool, said crucible including an open topped container having a horizontal grid at least partially spanning the open top of the crucible, said grid being formed from a metal having a negligible vaporization rate at the conditions necessary for vaporization of said metal and having the characteristic of being wet by said metal, heating the surface of the molten pool to vaporize said metal, and controlling the level of the molten pool within the crucible so that the surface of the molten pool lies just below the upper surface of said grid, whereby the metal may be rapidly vaporized from the area of reduced surface tension adjacent the grid.

3. An improved vacuum vaporization method for vaporizing a metal from the surface of a molten pool of significant depth comprising, heating a metal having a vaporization temperature below 3000° F. with an electron beam to form a molten pool of said metal, said crucible including an open topped container having a horizontal grid at least partially spanning the open top of the crucible, said grid being formed from a metal having a negligible vaporization rate at the conditions necessary for vaporization of said metal and having the characteristic of being wet by said metal, heating the surface of the molten pool to vaporize said metal, and controlling the level of the molten pool within the crucible so that the surface of the molten pool lies just below the upper surface of said grid, whereby the metal may be rapidly vaporized from the areas of reduced surface tension adjacent the grid.

4. A method in accordance with claim 3 wherein the metal is copper, beryllium, iron or tantalum or mixtures thereof.

5. A method in accordance with claim 3 wherein the grid is zirconium, tungsten or tantalum or mixtures thereof.

6. A method in accordance with claim 3 wherein the metal is copper and the grid is zirconium.

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