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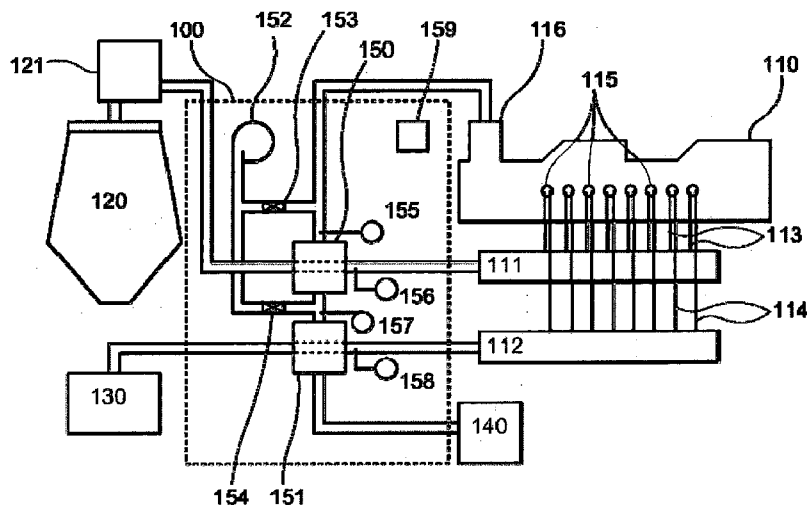
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(54) Title: METHOD FOR COMBUSTION OF A LOW-GRADE FUEL

Fig. 1



(57) Abstract: Method for combustion of a fuel using at least one industrial burner (115), which burner (115) is fed with a low-grade, gaseous fuel with a Lower Heating Value (LHV) of 8 MJ/Nm³ or less and an oxidant. The invention is characterised in that the combustion products from the combustion of the fuel with the oxidant are brought firstly through a first heat exchanging step (150; 201), in which thermal energy is transferred from the combustion products to the fuel which is thereby preheated, and in that the thus cooled combustion products thereafter are brought through a second heat exchanging step (151; 203), in which thermal energy is transferred from the cooled combustion products to the oxidant which is thereby also preheated. The invention also relates to a system for preheating fuel and oxidant.

Description

Method for combustion of a low-grade fuel

The present invention relates to a method and a preheating system for combustion of a low grade fuel using an industrial burner. More particularly, the invention relates to such combustion for heating of an industrial furnace.

In plants in which industrial furnaces are used to produce steel and other metals, various low-grade, gaseous fuels are often produced as byproducts. One example is so called top gas from blast furnaces, which are used for steel production. Another example is off-gas from converters. Such low-grade fuels typically contain a mixture of substances that may comprise for instance hydrocarbons, nitrogen gas, oxygen gas, hydrogen gas, carbon monoxide, carbon dioxide and water vapor. Because the energy density in such fuels is often limited, they are conventionally used for low temperature processes such as heating or power production. Alternatively, they may be mixed into fuels that are more energy dense. They may also be burned off into the atmosphere to no use.

Since such low-grade fuels are often produced in abundance in for instance steelworks, and are therefore comparatively cheap, it would be desirable to be able to use them to a larger extent also in high temperature processes, such as in heating furnaces for steel materials, where normally more high-grade fuels are used.

Moreover, using a low-grade fuel which already exists as a byproduct from another industrial process instead of using a conventional, externally supplied, fossil fuel will decrease the carbon footprint of a plant.

5

In order to be able to use low-grade fuels in such applications, it has for instance been proposed, in Swedish patent 553,731, to switch the supplies for fuel and oxidant in an existing air burner, and to at the same time use a
10 low-grade fuel.

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In the US patent application no 12/440,520, a method is described for making use of residual heat from a heating furnace by using part of the combustion products to preheat
the fuel, while another share of the combustion products is
used to preheat the oxidant.

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JP57198913, on the other hand, describes a burner exploiting the thermal energy in the combustion products by
preheating low-grade fuel and/or air in a heat exchanger.

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The present invention offers a supplement or alternative to the above suggestions for making the exploitation of low-grade fuel possible in heating furnaces. Moreover, the
invention solves the problem of preheating an oxidant using
combustion products, also when the combustion products
leaving the combustion zone are very hot. Conventionally,
such preheating has been problematic, since hot combustion
products constitute a security hazard if the preheating
30 equipment breaks and they come into direct contact with the
oxidant.

Hence, the invention relates to a method for combustion of a fuel using at least one industrial burner, which burner is fed with a low-grade, gaseous fuel with a Lower Heating Value (LHV) of 8 MJ/Nm³ or less and an oxidant, which
5 method is characterised in that the combustion products from the combustion of the fuel with the oxidant are brought firstly through a first heat exchanging step, in which thermal energy is transferred from the combustion products to the fuel which is thereby preheated, and in
10 that the thus cooled combustion products thereafter are brought through a second heat exchanging step, in which thermal energy is transferred from the cooled combustion products to the oxidant which is thereby also preheated.

15 The invention also relates to a system for preheating a low-grade, gaseous fuel with a Lower Heating Value (LHV) of 8 MJ/Nm³ or less and an oxidant and feeding said preheated low-grade fuel and said preheated oxidant to at least one industrial burner using which the fuel is combusted with
20 the oxidant to produce hot combustion products, which system is characterised in that the system comprises a first heat exchanging device, arranged to transfer heat from the hot combustion products to the fuel, which is thereby preheated, and in that the system also comprises a
25 second heat exchanger, arranged to transfer thermal energy from the combustion products which have been cooled in the first heat exchanging step to the oxidant, which is thereby also preheated.

30 In the following, the invention will be described in detail, with reference to exemplifying embodiments of the invention and to the enclosed drawings, wherein:

Figure 1 is a simplified view of a preheating system according to the present invention; and
Figure 2 is a simplified view of a heat exchanger arrangement according to the invention.

5

Figure 1 illustrates an industrial furnace 110 operated according to the present invention using a preheating system 100, also according to the invention. Preferably, the industrial furnace 110 is a heating furnace for a metal
10 material, preferably steel, and is preferably arranged to maintain heating temperatures in the furnace atmosphere of at least about 1 000°C, such as for reannealing of steel products, more preferably at least about 1 200°C, for instance for reheating of steel products before hot
15 rolling.

In order to heat the furnace 110, at least one industrial burner 115 is used, which is or are mounted in a furnace wall. Each burner 115 comprises at least one each of a
20 supply opening for fuel and a supply opening for oxidant.

The oxidant may be air, but it is preferred that the oxygen contents of the oxidant are higher than those for air. Hence, according to a preferred embodiment, the oxidant
25 comprises at least 50% by weight oxygen, more preferably at least 85% by weight oxygen. Even more preferably, the oxidant comprises at least 95% oxygen, such as industrially pure oxygen. Combustion with an oxidant comprising high levels of oxygen in combination with a low-grade fuel
30 yields an especially cost-efficient heating. Also, preheating of the present type makes it possible to use combustion products to preheat even these types of high

oxygen oxidant without this resulting in any major safety hazards.

According to the invention, the burner or burners 115 are driven with a gaseous, low-grade fuel, such as top gas from a blast furnace.

Table 1 is a comparison of typical rates of different constituents between, on the one hand, a medium-grade fuel such as coke oven gas and, on the other hand, a low-grade fuel, such as top gas from a blast furnace and off-gas from a converter. All values are given in percentage by volume.

Table 1

	N ₂	O ₂	H ₂	CO	CO ₂	CH ₄	C _m H _n	H ₂ O
Coke oven gas	3.5	0.55	60	7.5	2.35	23.5	2.4	0.2
Top gas	52.5	0.55	2.3	23.5	20	-	-	1.15
Converter gas	17.2	0.1	2.5	64.5	15.6	-	-	0.1

Table 2 is a comparison of Lower Heating Values (LHV) for coke oven gas, top gas from a blast furnace and off-gas from a converter.

Table 2

	LHV (MJ/Nm ³)	LHV (MJ/kg)
Coke oven gas	17.9	34
Top gas	3.2	2.4
Converter gas	8.0	6.0

According to the invention, the burner or burners 115 are driven with a gaseous fuel the LHV of which is equal to or lower than 8 MJ/Nm³. However, it is preferred that the gaseous fuel has an LHV of no more than 6 MJ/Nm³, more preferably no more than 4 MJ/Nm³. The fuel may comprise a

certain addition of another, more high-grade fuel, as long as the LHV of the total mixture does not exceed the said limits in terms of MJ/Nm³. In particular, lower LHV:s work better in combination with oxidants comprising high levels of oxygen. A preferred fuel example is a mixture of top gas and converter off-gas, which both originate from a local steel making installation comprising a blast furnace and a converter. For cost reasons, it is preferred not to mix in any high-grade fuels before combustion, in particular not to mix in any fuels that themselves have LHV:s of more than 8 MJ/Nm³, such as is the case for instance for coke oven gas.

The burner or burners 115 are provided, via conduits 113, with low-grade fuel from a fuel supply means 111, which receives the low-grade fuel from a source of such low-grade fuel. In figure 1, an exemplifying, simplified blast furnace 120 is shown, from which top gas is brought, via a gas cleaning step 121 and a pipe work, to the supply means 111. However, it is realized that the low-grade fuel source may be a source of converter off-gas or any other suitable source of low-grade fuel as exemplified above.

According to a preferred embodiment, the low-grade fuel comprises at least 50% by weight top gas originating from the operation of the blast furnace 120. Moreover, it is preferred that blast furnace 120 is locally arranged in the same industrial plant as the furnace 110, and consequently also the burner or burners 115. This way, the plant as a whole can be made more energy efficient.

Oxidant is supplied to the burner or burners 115, via conduits 114, from an oxidant supply means 112, to which

oxidant is supplied from an oxidant source 130, such as a conventional source of industrially pure oxygen or a conventional means for oxygen enriching air.

- 5 Both the fuel and the oxidant pass the preheating system 100 before reaching means 111 and 112, respectively.

The gaseous combustion products from the combustion, by burner or burners 115 and in furnace 110, of the fuel with
10 the oxidant, exit from the furnace 110 via flue 116, and are then led in a pipe work as shown in to figure 1.

According to the invention, the said combustion products are brought firstly through a first heat exchanging step
15 150, in which thermal energy is transferred from the said combustion products to the fuel, which is thereby preheated. Thereafter, the thus cooled combustion products are brought through a second heat exchanging step 151, in which thermal energy is transferred from the cooled
20 combustion products to the oxidant, which is thereby also preheated.

In other words, the low-grade fuel and the oxidant are preheated one after the other, in series. This means that
25 the oxidant is preheated using the thermal energy of the same combustion products that preheat the low-grade fuel, but after the combustion products have already been cooled to some extent by preheating the low-grade fuel. This way, the thermal energy content of the combustion products from
30 the furnace 110 can be exploited more fully, while at the same time minimizing any risks of explosion or the like relating to the preheating of oxidant, especially in case a high oxygen oxidant is used.

After having passed steps 150 and 151, the combustion products are preferably brought to a cleaning or processing step 140 arranged to take care of the cooled combustion products.

Of course, during the passage of the combustion products through steps 150, 151, the combustion products never come into direct physical contact with neither the low-grade fuel nor the oxidant to be preheated. Instead, only a thermal contact is established.

According to a preferred embodiment, the second heat exchanging step comprises a metal heat exchanger of recuperator type, in other words a heat exchanger which is not a regenerator, but one in which the thermal energy is transferred from one medium to another in a manner which is direct rather than indirect, in other words without any intermediate heating of some other medium prior to the sequential heating of the low-grade fuel or the oxidant. Preferred heat exchangers used in steps 150, 151 are counter-flow or cross-flow heat exchangers.

Specifically, it is preferred to use metal heat exchangers, in which a metal separating means is used to keep the combustion products at all times separated from the low-grade fuel and the oxidant, respectively. Preferred metal materials for such means comprise stainless steels.

In particular, it is preferred that, in the second heat exchanging step 151, the oxidant is conveyed in one or several metal pipes through a chamber, through which chamber combustion products are arranged to flow, which

pipes are arranged to separate the oxidant from the combustion products and to convey heat from the combustion products in the chamber to the oxidant in the said pipes.

5 This is illustrated in figure 2, in which a first heat exchanging step 201, corresponding to the first heat exchanging step 150 as shown in figure 1 and comprising an entry 200 for hot combustion products, is connected, in series via a conduit 202, to a second heat exchanging step
10 203, corresponding to the second heat exchanging step 151 in figure 1 and comprising an exit 204 for cooled combustion products. Through the first heat exchanging step 201, heat exchanging pipes 212 run inside a chamber inside step 201, from an entry 210 for low-grade fuel to an exit
15 211 for preheated low-grade fuel. Similarly, in step 203, heat exchanging pipes 222 run inside a chamber inside step 203, from an entry 220 for oxidant to an exit 221 for preheated oxidant.

20 It is preferred that the metal material of separating means arranged to keep the oxidant separated from the combustion gases, that is pipes 222 in figure 2, is made of a metal material which is more acid resistant than the metal material of corresponding separating means arranged to at
25 all times keep the low-grade fuel separated from the combustion gases, that is pipes 212 in figure 2. Examples of suitable materials for the said separation means in the second heat exchanging step comprise sufficiently acid resistant stainless steel types.

30

It is furthermore preferred that only said separating means of heat exchanging step 151, hence in figure 2 only pipes 222, are made from such acid resistant stainless steel, and

that the rest of the heat exchanging step 150, 151 is constructed from other, less acid resistant stainless steels and/or non-metal material.

5 In figure 1 is furthermore illustrated an ambient air supply device 152, for instance in the form of a conventional fan with a suitable pipe work, preferably working in collaboration with and being controlled by, a control device 159 which is in communication (for instance
10 wired communication) with the air supply device 152.

The device 152 is arranged to supply ambient air to the flow of combustion products upstream of the first heat exchanging step 150, in order to cool the combustion
15 products before entering into the step 150. The supply takes place via a control valve 153, which may be controlled by control device 159 to effect the flow control.

20 Moreover, the device 152 is arranged to control the temperature of the combustion products flowing into the step 150 based upon a measured temperature of the combustion products upstream of the step 150 and/or a measured temperature of the low-grade fuel downstream of
25 the step 150. Such temperatures are measured using suitable temperature sensors 155 and 156, respectively.

According to a supplementary or alternative embodiment, the same or a different ambient air supply device 152 (only one
30 such device is shown in figure 1) is arranged to supply ambient air to the flow of combustion products downstream of the first heat exchanging step 150 but upstream of the second heat exchanging step 151, preferably via a control

valve 154 which may also be controlled by control device 159, in order to cool the combustion products before entering into the step 151. In this case, the device 152 is arranged to control the temperature of the combustion products flowing into the second heat exchanging step based upon a measured temperature of the combustion products upstream of the step 151 and/or a measured temperature of the oxidant downstream of the step 151. Such temperatures are measured using suitable temperature sensors 157 and 158, respectively.

According to a preferred embodiment, the control device 159 is arranged to read temperature inputs from at least two, preferably at least three, of the temperature sensors 155-158, respectively arranged to measure temperatures of combustion gases upstream of step 150 and between steps 150, 151; temperature of low-grade fuel downstream of step 150; and temperature of oxidant downstream of step 151. Based upon these measurement values, the control device 159 is then arranged to control the supply device 152 to supply a sufficient amount of ambient air to the combustion products upstream of the first heat exchanging step 150 in order to keep the temperature of the combustion products flowing into the second step 151 at or below a predetermined highest allowable temperature. Such control may be based upon a suitable control algorithm, for instance taking into account empirically and/or theoretically determined parameters regarding cooling of the combustion products when flowing through the first heat exchanging step 150. The control algorithm may also be based upon for instance the flow of low-grade fuel through step 150.

The ambient air may be of about room temperature, but is at least cooler than the combustion gases with which it is mixed.

5 As described above, the combustion products may have a temperature of about 1 000°C when leaving the flue 116. According to a preferred embodiment, the temperature of the combustion products at the entry into the first heat exchanging step 150, after possible mixing with ambient
10 air, is at least 800°C. Similarly, the temperature of the combustion products at the entry into the second heat exchanging step 151, after cooling in step 150 and possible additional mixing with ambient air, is not more than 400°C. This will result in efficient preheating but still minimize
15 security hazards.

By first preheating the low-grade fuel and thereafter, using the already partly cooled-off combustion products, preheating the oxidant, a number of advantages are
20 achieved.

Firstly, in many applications a larger share of the energy contents of the hot combustion products can be transferred to the fuel and oxidant than what is possible when only
25 heat exchanging thermal energy in one single step to the fuel and/or to the oxidant.

Secondly, the density of the hot combustion products decreases when they are cooled by the fuel in the first
30 heat exchanging step 150, which results in that the second heat exchanger step 151, transferring thermal energy to the oxidant, can be designed with lower capacity. This, in turn, results in a more cost-efficient installation.

Thirdly, it is possible to preheat even a high oxygen oxidant without running into safety risks.

5 Above, preferred embodiments have been described. However, it is apparent to the skilled person that many modifications may be made to the described embodiments without departing from the basic idea of the invention.

10 For example, it is realized that the heat exchanging step 150, 201 may be of the corresponding or a different type than the heat exchanging step 151, 203, as long as the principles herein are honored.

15 It is also realized that burners 115, supplied with preheated low-grade fuel and preheated oxidant, may be supplemented by other burners also heating the same furnace 110, such as conventional oxyfuel burners. However, it is preferred that the burners 115 constitute the only heat
20 source of the furnace 110.

Thus, the invention shall not be limited to the described embodiments, but may be varied within the scope of the enclosed claims.

25

C L A I M S

1. Method for combustion of a fuel using at least one industrial burner (115), which burner (115) is fed with a low-grade, gaseous fuel with a Lower Heating Value (LHV) of 8 MJ/Nm³ or less and an oxidant, **characterised in** that the combustion products from the combustion of the fuel with the oxidant are brought firstly through a first heat exchanging step (150;201), in which thermal energy is transferred from the combustion products to the fuel which is thereby preheated, and in that the thus cooled combustion products thereafter are brought through a second heat exchanging step (151;203), in which thermal energy is transferred from the cooled combustion products to the oxidant which is thereby also preheated.

2. Method according to claim 1, **characterised in** that the combustion reaction between the oxidant and the low-grade fuel heats an industrial furnace (110).

3. Method according to claim 1 or 2, **characterised in** that the low-grade fuel comprises at least 50% by weight top gas from a blast furnace (121).

4. Method according to claim 3, **characterised in** that low-grade fuel is caused to originate from the operation of a blast furnace (121) which is caused to be arranged in the same industrial plant as the burner (115).

5. Method according to any one of the preceding claims, **characterised in** that the oxidant comprises at least 85% by weight oxygen.

6. Method according to any one of the preceding claims, **characterised in** that the second heat exchanging step (151;203) comprises a metal heat exchanger of recuperator type.

5

7. Method according to claim 6, **characterised in** that, in the second heat exchanging step (151;203), the oxidant is conveyed in one or several metal pipes (222) through a chamber, through which chamber combustion
10 products are arranged to flow, which pipes (222) are arranged to separate the oxidant from the combustion products and to convey heat from the combustion products in the chamber to the oxidant in the said pipes (222).

15

8. Method according to any one of the preceding claims, **characterised in** that the temperature of the combustion products at the entry into the first heat exchanging step (150;201) is at least 800°C, and that the temperature of the combustion products at the entry into
20 the second heat exchanging step (151;203) is less than 400°C.

25

9. Method according to any one of the preceding claims, **characterised in** that a first ambient air supply device (152) is arranged to supply ambient air to the flow of combustion products upstream of the first heat exchanging step (150;201) in order to cool the combustion products before entering into the first heat exchanging step (150;201), and in that the first air supply device
30 (152) is arranged to control the temperature of the combustion products flowing into the first heat exchanging step (150;201) based upon a measured temperature of the combustion products upstream of the first heat exchanging

step (150;201) and/or a measured temperature of the fuel downstream of the first heat exchanger step (150;201).

10. Method according to claim 9, **characterised**
5 **in** that a second ambient air supply device (152) is arranged to supply ambient air to the flow of combustion products downstream of the first heat exchanging step (150;201) but upstream of the second heat exchanging step (151;203), in order to cool the combustion products before
10 entering into the second heat exchanging step (152;203), and in that the second air supply device (152) is arranged to control the temperature of the combustion products flowing into the second heat exchanging step (151;203) based upon a measured temperature of the combustion
15 products upstream of the second heat exchanging step (151;203) and/or a measured temperature of the oxidant downstream of the second heat exchanger step (151;203).

11. System (100) for preheating a low-grade, gaseous fuel
20 with a Lower Heating Value (LHV) of 8 MJ/Nm³ or less and an oxidant and feeding said preheated low-grade fuel and said preheated oxidant to at least one industrial burner (115) using which the fuel is combusted with the oxidant to produce hot combustion products, **characterised**
25 **in** that the system (100) comprises a first heat exchanging device (150;201), arranged to transfer heat from the hot combustion products to the fuel, which is thereby preheated, and in that the system (100) also comprises a second heat exchanger (151;203), arranged to transfer
30 thermal energy from the combustion products which have been cooled in the first heat exchanging step (150;201) to the oxidant, which is thereby also preheated.

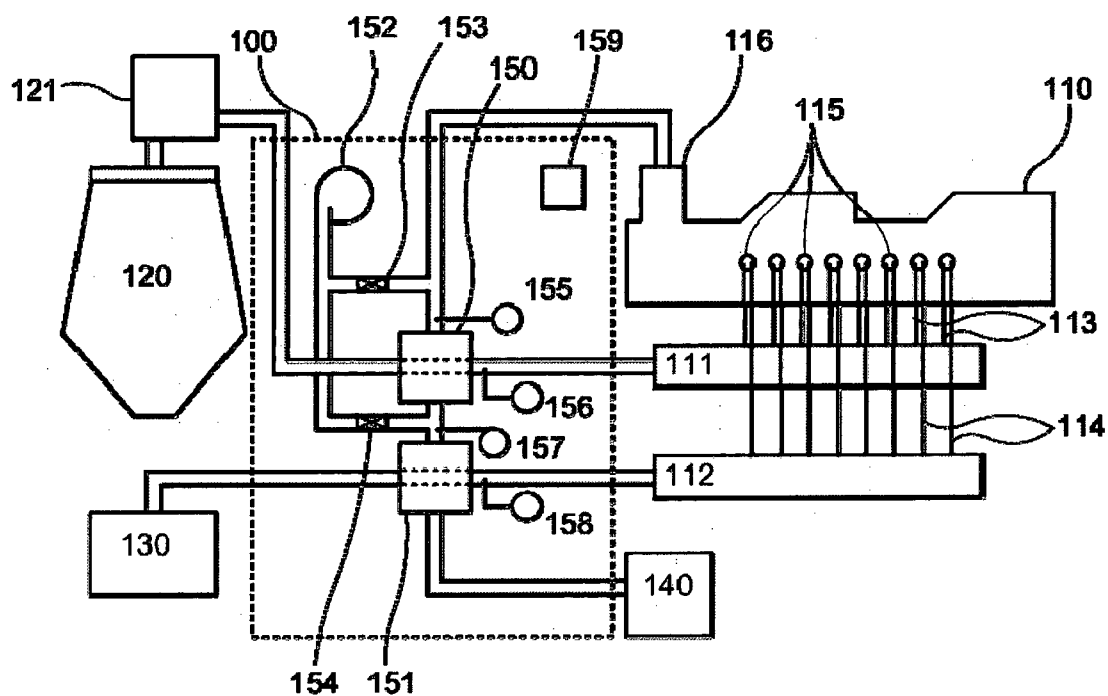
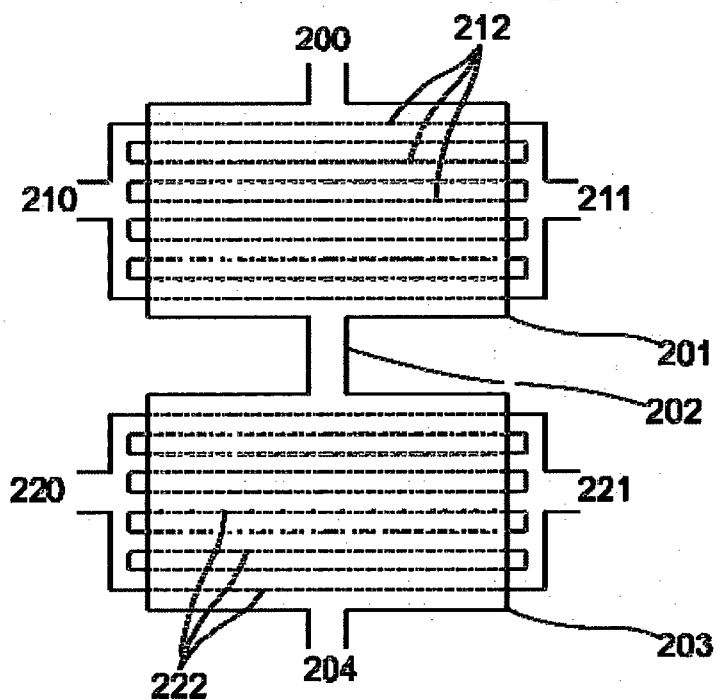
12. System (100) according to claim 11, **characterised in** that the oxidant comprises at least 85% by weight oxygen.

5 13. System (100) according to claim 11 or 12, **characterised in** that the second heat exchanging step (151;203) comprises a metal heat exchanger of recuperator type.

10 14. System (100) according to claim 13, **characterised in** that, in the second heat exchanging step (151;203), the oxidant is conveyed in one or several metal pipes (222) through a chamber, through which chamber combustion products are arranged to flow, 15 which pipes (222) are arranged to separate the oxidant from the combustion products and to convey heat from the combustion products in the chamber to the oxidant in the said pipes (222).

20 15. System (100) according to any one of claim 11-14, **characterised in** that an ambient air supply device (152) is arranged to supply ambient air to the flow of combustion products upstream of the first heat exchanging step (150;201) and to the flow of combustion 25 products downstream of the first heat exchanging step (150;201) but upstream of the second heat exchanging step (151;203), in that one or several temperature sensors (155,156,157,158) is or are arranged to measure the temperature of the combustion gases upstream of the first 30 heat exchanging step (150;201) and/or downstream of the first heat exchanger step (150;201) and/or the temperature of the fuel downstream of the first heat exchanging step (150;201) and/or the temperature of the oxidant downstream of the second heat exchanging step (151;203), and in that a

control device (159) is arranged to control the ambient air flow provided by the ambient air supply device (152) based upon measurement data from said at least one temperature sensor (155,156,157,158).

Fig. 1**Fig. 2**

INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2014/000072

A. CLASSIFICATION OF SUBJECT MATTER
INV. F23G7/06
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
F23G F23K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JP S57 198913 A (ECHIGO RIYOUZOU) 6 December 1982 (1982-12-06) cited in the application the whole document	1-15
A	US 2011/059410 A1 (GLYNN PATRICK JOSEPH [AU]) 10 March 2011 (2011-03-10) paragraph [0035]; figure 2	1-15



Further documents are listed in the continuation of Box C.



See patent family annex.

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
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